

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.890	.984	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEXED *etc* 1-30-51

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MARCH 14, 1950 LEONARD
CARVER

B.M.'s AROUND PLANT SITE: (SEE F.R. 744, P. 148, 149)

S.E. COR. SALT STG. TANK. 546.66
 S.E. COR. WASH WATER CONTROL STR. 541.48
 RIM OF M.H. AT S 181.83 W 100.17 538.197 or 538.20
 RIM OF M.H. AT S 177 E 60. 530.32
 □ IN CONC. AT S. ENTRANCE TO ZEOLITE 534.52 ✓
 S.E. COR. OF E. BRINE DILUTION BOX IN H.H. 540.464
 □ W. END CURB CHAMBER, S. SIDE, IN H.H. 541.74
 NAIL IN ROUGH CONC. AT 0+00 OF AXES. 549.755
 □ IN CONC. MAN. AT 5+80 E. 538.47
 W. END OF CURB ON TRUCK SCALES. 546.58

KYE LEVEL #106546 MARCH 14, 1950 LEONARD-K
CARVER - ROD 1.

CHECK LIPS OF TROUGHS IN ZEOLITE BED'S BEFORE REMOVING
 FORMS. TROUGHS ARE NUMBERED FROM N. TO S., 1 TO 4.

R.M., SE. COR. BRINE DILUTION CHAMBER: 540.464
 + 9.242 549.706

TROUGH #1, N. LIP, W. END -8.746
 " " CENTER -8.718
 " " E. END -8.738
 " S. LIP W. END -8.747
 " " CENTER -8.718
 " " E. END -8.720

TROUGH #2, N. LIP W. END -8.748
 " CENTER -8.698
 " E. END -8.716
 S. LIP W. END -8.737
 " CENTER -8.712
 " E. END -8.730

TROUGH #3 N. LIP W. END -8.735
 CENTER -8.715

N.E. LEVEL #106346.
*DIETZEN ROD.

APRIL 24, 1950
LEONARD
CARVER

R.

ZEOLITE BEDS

CHECK LIPS OF TROUGHS AFTER FORMS REMOVED

R.M. +3.581 544.045 540.464

RED #1. TROUGH #1

N. LIP W. END -9.070

S. LIP " -9.070

H. LIP CENTER -9.070

S. " " -9.070

H. " E. END -9.070

S " E. " -9.063

TROUGH #2

N LIP E. END -9.068

S " E. " -9.062

H " CENTER -9.072

S " " -9.080

N " W. END -9.070

S " W " -9.072

TROUGH #3

N. LIP W. END -9.058

S. " W. " -9.061

* NOTE: USED A NEW DIETZEN ROD BELONGING TO GOLDEN
CO. FOR ALL ZEOLITE BED READINGS - A BETTER ROD TO READ

CHECK LIPS OF ZEOLITE TROUGHS IN RED #3, CONT'D

H.S. 545.706

TROUGH #3, N. LIP, E. END -8.716

" S. LIP, W. END -8.733

" " CENTER -8.710

" " E. END -8.710

TROUGH #4, N. LIP, W. END -8.724

" " CENTER -8.700

" " E. END -8.712

S. LIP W. END -8.723

" CENTER -8.704

" E. END -8.694

CHECK R.M. -3.242

APRIL 24

8.

TROUGH #3 - Cont'd 544045

N. SIDE CENTER -9.058

S. " " -9.063

N. " E. END -9.059

S. " E. " -9.048

TROUGH #4

N. SIDE E. END -9.062

S. " E. " -9.061

N. " CENTER -9.062

S. " " -9.062

N. " W. END -9.058

S. " W. " -9.069

RED #3 TROUGH #1

N. SIDE W. END -9.075

S. " W. " -9.081

N. " CENTER -9.052

S. " " -9.055

N. " E. END -9.067

S. " E. " -9.050

RED #3, TROUGH #2 544045

N. SIDE E. END -9.045

S. " E. " -9.060

N. " CENTER -9.035

S. " " -9.050

N. " W. END -9.077

S. " W. " -9.068

TROUGH #3

N. SIDE W. END -9.066

S. " W. " -9.066

N. " CENTER -9.053

S. " " -9.053

N. " E. END -9.041

S. " E. " -9.040

TROUGH #4

N. SIDE E. END -9.041

S. " E. " -9.026

N. " CENTER -9.040

S. " " -9.052

APRIL 24.

4.

BED #3 TROUGH #4. 544.045 CONT'D

N. SIDE W. END -9.060

S. " W. " -9.055

BED #5, TROUGH #1.

N. SIDE W. END -9.055

S. " W. " -9.052

H. " CENTER -9.055

S. " " -9.050

H. " E. END -9.070

S. " E. " -9.070

TROUGH #2

N. SIDE E. END -9.068

S. " E. " -9.070

H. " CENTER -9.060

S. " " -9.055

H. " W. END -9.060

S. " W. " -9.068

TROUGH #3.

N. SIDE W. END -9.070

S. " W. " -9.067

BED #5
TROUGH #3, CONT'D 544.045

N. SIDE CENTER -9.051

S. " " -9.049

H. " E. END -9.045

S. " E. " -9.045

TROUGH #4

N. SIDE E. END -9.048

S. " E. " -9.040

H. " CENTER -9.050

S. " " -9.048

N. " W. END -9.071

S. " W. " -9.065

BED #7, WITH SUPPORTS IN PLACE UNDER CENTER

OF EACH TROUGH, AND APPROX 4" OF WATER IN BED.

TROUGH #1:

N. SIDE W. END -9.065

S. " W. END -9.065

H. " CENTER -9.055

S. " " -9.060

H. " E. END -9.065

S. " E. END -9.060

APRIL 24

5.

RED #7, CONT'D.	TROUGH #2,	
N. SIDE E. END	544.045	-9.051
S. " E. "		-9.050
N. " CENTER		-9.045
S. " "		-9.052
N. " W. END		-9.065
S. " W. "		-9.060
TROUGH #J.		
N. SIDE W. END		-9.062
S. " W. "		-9.070
N. " CENTER		-9.055
S. " "		-9.050
N. " E. END		-9.068
S. " E. "		-9.062
TROUGH #4 N. SIDE E. END		-9.048
S. SIDE E. END		-9.045
N. " CENTER		-9.048
S. " "		-9.048
N. " W. END		-9.070
S. " W. "		-9.066
CHECK R.M.	-3.581	540.464

CHECK ELEV. OF ZEOLITE TROUGH LINES, CONT'D. (NO SUPPORTS)

R.M. +3.546 544.010 540.464

RED #2 TROUGH #1

N. SIDE E. END	-9.021
S. " "	-9.012
N. " CENTER	-8.990
S. " "	-8.998
N. " W. END	-9.014
S. " "	-9.014

TROUGH #2,

N. SIDE W. END	-9.000
S. " "	-8.995
N. " CENTER	-8.990
S. " "	-8.992
N. " E. END	-9.010
S. " "	-9.010

TROUGH #J.

N. SIDE E. END	-9.005
S. " E. "	-9.010
N. " CENTER	-8.992

APRIL 24

6.

TROUGH #3, CONT'D. 544.010

S. SIDE CENTER -8.988
 N. " W. END -9.004
 S. " " -9.000

TROUGH #4,

N. SIDE W. END -9.002
 S. " " -9.000
 N. " CENTER -8.995
 S. " " -8.995
 N. " E. END -9.006
 S. " " -9.002

BED #4 TROUGH #1,

N. SIDE E. END -9.002
 S. " " -9.000
 N. " CENTER -8.985
 S. " " -8.985
 N. " W. END -8.992
 S. " " -8.990

BED #4, TROUGH #2, 544.010

N. SIDE W. END -8.976
 S. " " -8.988
 N. " CENTER -8.975
 S. " " -8.977
 N. " E. END -9.003
 S. " " -9.008

TROUGH #3,

N. SIDE E. END -9.000
 S. " " -9.002
 N. " CENTER -8.990
 S. " " -8.989
 N. " W. END -8.997
 S. " " -8.995

TROUGH #4,

N. SIDE W. END -8.985
 S. " " -8.980
 N. " CENTER -8.995
 S. " " -8.996
 N. " E. END -8.995
 S. " " -9.002

APRIL 24

7.

RED^{#6} TROUGH^{#1} 544.010

N. SIDE E. END	-9.030
S. " "	-9.031
H. " CENTER	-9.016
S. " "	-9.020
H. " W. END	-9.015
S. " "	-9.018

TROUGH^{#2}

H. SIDE W. END	-9.014
S. " "	-9.025
H. " CENTER	-9.015
S. " "	-9.015
H. " E. END	-9.030
S. " "	-9.041

TROUGH^{#3}

H. SIDE E. END	-9.030
S. " "	-9.023
H. " CENTER	-9.018
S. " "	-9.020
H. " W. END	-9.022
S. " "	-9.018

RED^{#6} TROUGH^{#4} 544.010

N. SIDE W. END	-9.024
S. " "	-9.022
H. " CENTER	-9.027
S. " "	-9.020
H. " E. END	-9.028
S. " "	-9.028

RED^{#8} TROUGH^{#1}

H. SIDE E. END	-9.030
S. " "	-9.028
H. " CENTER	-9.025
S. " "	-9.024
H. " W. END	-9.030
S. " "	-9.030

TROUGH^{#2}

H. SIDE W. END	-9.010
S. " "	-9.020
H. " CENTER	-9.020
S. " "	-9.020
H. " E. END	-9.030
S. " "	-9.033

APRIL 24.

CHECK ELEV. OF ZEOLITE TROUGH LIPS, CONT'D.

BEAM #3 TROUGH #3.

N. SIDE E. END -9.050

S. " " -9.074

N. " CENTER -9.025

S. " " -9.025

N. " W. END

S. " "

TROUGH #4

N. SIDE W. END

S. " "

N. " CENTER

S. " "

N. " E. END

S. " "

NOTE: AT LAST READING ABOVE, LEVEL WAS RUMPED

BY WORKMAN MOVING TIMBERS, SPOILING SET-UP.

IMPOSSIBLE TO TAKE FURTHER READINGS BECAUSE OF

WORKMEN CLEANING UP AREA.

MARCH 16, 1950 LEONARD 8.
CARVER

CHECK BEAMS IN ROOF OVER ZEOLITE TERRACE.

R.M. ON PARAPET S.W. COR. COLOR. BLDG. 564.505

+ 2.70 567.205

T.P. BOLT, WEST WALL 13'5. -4.88 562.325

+ 4.97 567.295

BEAM #16 E. END -7.24 560.055

CENTER -7.225 60.07

W. END -7.22 60.075

BEAM #17 N. END -7.39 59.90

S. " -7.38 59.91

BEAM 15: W. SECT. W. END -7.38 59.91

" " E. " -7.40 59.89

" CENTER, W. END -7.40 59.89

" " E. " -7.42 59.87

" E. SECT. W. END -7.42 59.87

" E. " -7.40 59.89

UNDER SIDE OF ROOF, AVERAGE -5.24 562.05

B.M. Bolt Head, W47, 513		562.325
Mid. + 4.85	567.175	
Read. ¹⁸ 71 H. End	- 5.925	561.250
S. "	- 5.935	61.240
² H. "	- 5.93	61.245
S. "	- 5.925	61.250
³ H. "	- 5.925	61.250
S. "	- 5.915	61.260
⁴ H. "	- 5.92	61.255
S. "	- 5.925	61.250
⁵ H. "	- 5.93	61.245
S. "	- 5.925	61.250
	AVERAGE	
OUTSIDE EDGE OF MOLD A	- 4.80	562.375

MARCH 17, 1950 LEONARD
CARVER

RECHECK BEAM SOFFITS IN ZEOHITE ROOF SLAB

R.M.	+ R.65	553.32	550.67	
580.29	E12	45.72	-7.64	545.68 .01 LOW
"	E46	"	-7.65	545.67 .05 LOW
585.92	E12	45.69	-7.685	545.635 .05 LOW
"	E29	"	-7.65	545.67 .02 LOW
"	E46	"	-7.685	545.635 .06 LOW
591.54	E12	45.66	-7.72	545.60 .06 LOW
"	E29	"	-7.68	545.64 .02 LOW
"	E46	"	-7.715	545.615 .04 LOW
597.17	E12	45.63	-7.74	545.58 .05 LOW
"	E29	"	-7.695	545.625 .01
"	E46	"	-7.75	545.57 .06 LOW
5102.79	E12	45.60	-7.78	545.54 .06 LOW
"	E29	"	-7.745	545.575 .02 LOW
"	E46	"	-7.785	545.535 .06 LOW
5108.42	E12	45.59	-7.825	545.495 .07 LOW
"	E29	"	-7.78	545.54 .03 LOW
"	E46	"	-7.825	545.495 .07 LOW

MARCH 16, 1950 LEONARD
CARVER 10.

CHECK BEAM SOFFITS IN ZEOHITE ROOF SLAB.

R.M.	+ R.65	553.30	550.67	ON BASINS WALL
STATION:	CORRECT GRADE	-	ACTUAL GRADE	
574.58	E12	545.75	-7.55	545.75
"	E29	"	-7.54	45.76
"	E46	"	-7.54	45.76
580.29	E12	45.72	-7.63	45.67 .05 LOW
"	E29	"	-7.57	45.73
"	E46	"	-7.63	45.67 .05 LOW
585.92	E12	45.69	-7.67	45.63 .06 LOW
"	E29	"	-7.64	45.66 .03 LOW
"	E46	"	-7.67	45.63 .06 LOW
591.54	E12	45.66	-7.70	45.60 .06 LOW
"	E29	"	-7.69	45.61 .05 LOW
"	E46	"	-7.70	45.60 .06 LOW
597.17	E12	45.63	-7.74	45.56 .07 LOW
"	E29	"	-7.71	45.59 .04 LOW
"	E46	"	-7.74	45.56 .07 LOW
5102.79	E12	45.60	-7.77	45.53 .07 LOW
"	E29	"	-7.74	45.56 .04 LOW
"	E46	"	-7.77	45.53 .07 LOW

MARCH 17, 1950

RECHECK - CONT'D

H.S.		353.32		
5114.04	E12	545.54	-7.865	545.465 .07 low
"	E29	"	-7.82	545.50 .04 low
"	E46	"	-7.865	545.455 .08 low
		72.66		

MARCH 16, 1950

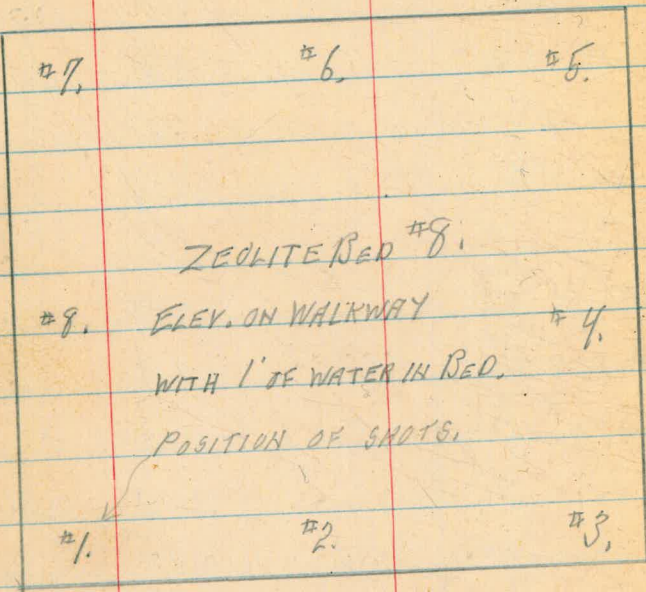
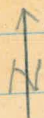
LEONARD
CARVER

11.

CHECK BEAM SOFFITTS IN ZEOLITE ROOF, CONT'D.

		553.90		
\$ 108.42	E12	545.57	-7.82	545.48
"	E29	"	-7.79	45.51
"	E46	"	-7.82	45.48
5114.04	E12	545.54	-7.85	45.45
"	E29	"	-7.83	45.47
"	E46	"	-7.86	45.44
TOP DZ 190		545.12	-8.18	546.12
TOP LOUVER VENT	38" 50 Box	545.35	-8.06	545.24
"	" "	"	-8.06	545.24
"	" "	"	-8.06	545.24
"	ROUND PART	545.12	-8.29	546.01
"	" "	"	-8.30	545.00
"	" "	"	-8.30	545.00

MARCH 17, 1950 LEONARD CARVER 12.



ELEV. ON WALKWAY OF ZEOLITE BED #8 WITH APPROX 1' OF WATER IN IT.

R.M.	GRADE	ROD	ELEV.
+10.06	548.26		538.20
Point #1,	539.00	-9.272	538.988
#2,	"	-9.279	538.981
#3,	"	-9.284	538.976
#4,	"	-9.278	538.982
#5,	"	-9.278	538.982
#6,	"	-9.275	538.985
#7,	"	-9.275	538.985
#8,	"	-9.282	538.978

CHECK R.M. 538.20 -10.06 538.20

SEE NEXT PAGE FOR 2ND SET OF ELEVATIONS
AFTER TESTING TANK WITH WATER.

CHECK ELEV. ON WALKWAY OF ZEOULITE BED #8 AFTER TANK WAS FILLED WITH WATER AND EMPTIED AGAIN: SEE PAGE 12 FOR 1ST LEVELS.

NOTE: IMPOSSIBLE TO TAKE ELEVATIONS WHILE TANK WAS FILLED BECAUSE OF FORMS FOR ROOF ABOVE.

R.M. +5.35	543.55	538.20	R.M.H. 583.1100
POINT #1.	-4.575	538.975	
" #2.	-4.585	538.965	
" #3.	-4.585	538.965	
" #4.	-4.575	538.975	
" #5.	-4.580	538.97	
" #6.	-4.580	538.97	
" #7.	-4.575	538.975	
" #8.	-4.582	538.968	
CHECK R.M. S-END ZEOULITE BLDG.	-9.033	534.517-534.62	

MARCH 17, 1950 LEONARD CARYER 13.

BEAMS IN ROOF OVER BAG STG., CHECK SOFFITS.

+11.60	576.10	564.50	
T.B.M. ON CURB NEAR ELEVATOR.	-4.61	571.49	
+16.02	597.51		
BEAM 408 AT TOP	-9.50	584.01-584.02	
" 400 " "	-9.15	584.36	
400 " "	-9.12	584.39	
405A N.E. COR.	-9.92	577.59	
403 E. SIDE	-9.53	577.98	
404 " "	-9.42	578.09	
TOP OF DOOR FRAME	578.12	-9.42	578.9
402	-9.44	578.07	
400	577.99	-9.53	577.98
WINDOW, TOP OF FRAME 303	-10.84	576.67	
400	-9.53	577.98	
401	578.10	-9.44	578.07
400	-9.53	577.98	
WINDOW, TOP OF FRAME 304	-10.85	576.66	
400	-9.53	577.98	
401	-9.43	578.08	

H.I.		587.51	
BEAM 404		-9.53	577.98
WINDOW, TOP OF FRAME	305	-10.85	576.66
	403	-9.55	577.96
405	S.E. COR	-9.89	577.62
403	S. END	-9.43	578.08
404	"	-9.45	577.06
WINDOW,	"	306	-10.85
			576.66
BEAM 406	"	-9.76	577.75
WINDOW	"	307	-9.85
			577.66
404	"	-9.41	578.10
403	"	-9.42	578.09
405	S.W. CORNER	-9.87	577.64
403	W. SIDE	-9.54	577.95
WINDOW	"	308	-10.84
			576.67
404	"	-9.54	577.95
401	"	-9.42	578.09
400	"	-9.53	577.98
WINDOW	"	309	-10.85
			576.66

H.d.	587.51		
400	W. SIDE	-9.55	577.96
401	"	-9.41	578.10
400	"	-9.56	577.95
WINDOW	" 310	-10.84	376.67
400		9.52	577.99
T.P. TOP OF 4x4 IN ELEVATOR SHAFT		-7.50	580.01 = 580.005 (LARRY'S)
TOP OF LEDGE, S. END		-12.78	574.73 .02 LOW
" " " "		-12.78	574.73 "
" " " "		-12.795	574.725 .025 LOW
" " " "		-12.79	574.72 .02 LOW
" " " "	IN CENTER	-6.55	580.96
" " " "	" "	-6.54	580.97
" " " "	" "	-6.54	580.97
SOFFITS AT Cn. B-5, 406		-3.59	583.92
Beam 401		-3.14	584.37
" 401		-3.15	584.36
" 407.		-3.50	584.01 - 584.02
" 407 MIDSPAN		-3.50	584.01 - 584.02

MARCH 22, 1950 LEONARD CARVER 16.

CHECK BEAM SOFFITS IN LEOLITE ROOF SLAB ON BASINS

	B.M. +2.69	553.30		550.67	WALL
S 74.58	W12	545.75	-7.55	545.75	O.K.
"	W29	"	-7.53	545.77	.02 HI
"	W46	"	-7.55	545.75	O.K.
S 80.79	W12	45.72	-7.60	545.70	.02 LOW
"	W29	"	-7.585	545.715	O.K.
"	W46	"	-7.60	545.70	.02 LOW
S 85.92	W12	45.69	-7.63	545.67	.02 "
"	W29	"	-7.635	545.665	.025 "
"	W46	"	-7.625	545.675	.015 "
S 91.54	W12	45.66	-7.66	545.64	.02 "
"	W29	"	-7.65	545.65	.01 "
"	W46	"	-7.66	545.64	.02 "
S 97.17	W12	45.63	-7.71	545.59	.04 LOW
"	W29	"	-7.69	545.61	.02 "
"	W46	"	-7.695	545.605	.025 "
S 102.79	W12	45.60	-7.72	545.58	.02 "
"	W29	"	-7.70	545.60	O.K.
"	W46	"	-7.72	545.58	.02 LOW

MARCH 22, 1950

17.

CHECK BEAM SOFFITS IN ZEOLITE ROOF - CONT'D.

	H. I. =	353.30	ROD	Elev.	
5108.42	W12	545.57	-7.73	545.57	0.00
"	W29	"	-7.75	545.55	.02 Low
"	W46	"	-7.76	545.54	.02 "
5114.04	W12	545.54	-7.77	545.52	.02 "
"	W29	"	-7.75	545.55	.01 High
"	W46	"	-7.79	545.51	.03 Low
Top Door			-8.19	545.11	0.00
Top VENT			-8.29	545.01	
"	"		-8.28	545.02	
"	"		-8.29	545.01	
CHECK R.M. IN FILTERS			-3.56	549.74 = 549.705	

MARCH 27, 1950 LEONARD
CARYER

18.

ZEOLITE GALLERY ROOF FORMS, SOUTH HALF elev.

RM. +10.54	561.21		550.67
Beam S-2	Grade	rod	
N ₄₅ 575.58	557.13	-4.05	557.16
" 596.08	"	-4.05	557.16
Arch #2			
N ₄₅ 597.08	556.85	-4.37	556.84
Beam S-2			
N ₄₅ 598.08	557.13	-4.05	557.16
" 5118.58	"	-4.03	557.18
Arch #1			
N ₄₅ 5119.58	556.85	-4.34	556.87
N ₄₅ 5119.58	559.00	-2.15	559.06
N _{12.00}			
" 578.34	553.75 (WZ/180)	-7.44	553.77
" 593.83	" "	-7.44	"
" 5100.33	" (WZ/179)	-7.44	"
" 5115.82	" "	-7.44	"
E. 12.00			
" 578.34	" (WZ/177)	-7.44	"
" 593.83	" "	-7.44	"
" 5100.33	" (WZ/178)	-7.44	"
" 5115.82	" "	-7.44	"
ck. BM.	550.67	-10.54	550.67

March 29, 1950

Leonard 100 19.

Coover T

KV 116396

East Hill - 207c48

Filter Gallery Roof Forms, West Hill

R.M. +4.895	566.92		562.925
CHECK R.M. SET BY LARRY FRANK		-4.39	562.53
S.I. 2.00 W. 118.25	557.11	(WF) 156	-9.80 557.12
" W. 125.26	" "		-9.80 557.12
" W. 126.43	"	(WF) 157	-9.80 557.12
" W. 136.60	" "		-9.80 557.12
" W. 137.77	"	(WF) 158	-9.79 557.13
" W. 144.78	" "		-9.79 557.13
" W. 151.84	"	(WF) 159	-9.78 557.14
" W. 158.42	" "		-9.79 557.13
" W. 159.58	"	(WF) 160	-9.80 557.12
" W. 169.75	" "		-9.79 557.13
" W. 170.92	"	(WF) 161	-9.79 557.13
" W. 177.92	" "		-9.77 557.15
N. 12.00 W. 118.25	"	(WF) 168	-9.79 557.13
" W. 125.26	" "		-9.79 557.13
" W. 126.43	"	(WF) 167	-9.79 557.13
" W. 136.60	" "		-9.79 557.13
" W. 137.77	"	(WF) 166	-9.79 557.13

Nov. 29, 1950

Leonard Rod
Carter

.20

Filter Gallery Roof Faems West Half

	H.I. = 566.92		rod elev.
N1200 W. 144.78	62002 557.11 (WF/160)		-9.78 557.14
" W. 151.84	" (WF/165)		-9.79 557.13
" W. 158.42	" "		-9.79 557.13
" W. 159.58	" (WF/164)		-9.80 557.12
" W. 169.75	" "		-9.80 557.12
" W. 170.92	" (WF/163)		-9.80 557.12
" W. 177.92	" "		-9.80 557.12
E402 " W. 114.42	(F-11)		-5.71 561.21
" W. 115.42	562.43		-4.45 562.47
" W. 125.33	"		-4.45 562.47
" W. 125.83	561.54 (F-9)		-5.32 561.60
" W. 126.33	562.43		-4.44 562.48
" W. 127.17	"		-4.46 562.46
" W. 126.66	"		-4.46 562.46
" W. 137.50	"		-4.46 562.46
" W. 137.16	561.54 (F-9)		-5.34 561.58
" W. 137.66	562.43		-4.45 562.47
" W. 147.08	"		-4.46 562.46
" W. 148.08	(F-10)		-5.72 561.20
" W. 149.08	562.43		-4.46 562.46

Nov. 29, 1950

Leonard
Carver

21.

	HI	GRADE	ROD	LEV.
"	W. 158.50	562.45	-4.45	562.47
"	W. 159.00	561.54 (F-9)	-5.32	561.66
"	W. 159.50	562.43	-4.45	562.47
"	W. 169.83	"	-4.45	562.47
"	W. 170.33	561.54 (F-9)	-5.35	561.57
"	W. 171.83	562.43	-4.47	562.45
"	W. 180.75	"	-4.45	562.47
"	W. 181.25	(F-11)	-5.72	561.20
cb BM		562.375	-4.595	562.375

Nov. 30, 1950
Clear, W. Bern

Leonard
Carver
K+E 106346

22.

Filter Walkways North-Half of Beds #1+3

R.M.	+5.07	554.82	ROD	549.75
W.4708	512.00	GRADE 550.00	-4.84	549.98
"	514.83	"	-4.835	549.985
"	521.06	"	-4.83	549.99
"	528.62	"	-4.82	550.00
"	531.62	"	-4.83	549.99
"	539.19	"	-4.82	550.00
"	546.75	"	-4.82	"
"	548.25	"	4.82	"
W.4908	512.00	"	4.86	549.96
"	514.83	"	-4.82	550.00
"	521.06	"	-4.82	"
"	528.62	"	4.82	"
"	531.62	"	4.82	"
"	539.19	"	4.82	"
"	546.75	"	4.82	"
"	548.25	"	4.81	550.01
W.6192	512.00	"	4.82	550.00
"	514.83	"	4.81	550.01

Filter Walkways (cont'd)

MS-554.82

W6142	521.06	550.00	-4.82	550.00
"	528.62	"	-4.82	"
"	531.62	"	-4.82	"
"	539.19	"	-4.83	549.99
"	546.75	"	-4.82	550.00
"	548.25	"	-4.82	"
W6692	512.00	"	-4.82	"
"	514.83	"	-4.81	550.01
"	521.06	"	-4.81	550.01
"	528.62	"	-4.82	550.00
"	531.62	"	-4.82	"
"	539.19	"	-4.82	"
"	546.75	"	-4.82	"
"	548.25	"	-4.82	"
W7955	512.00	"	-4.82	"
"	514.83	"	-4.83	549.99
"	521.06	"	-4.82	550.00
"	528.62	"	-4.82	"

Filter Walkways (cont'd)

H.I. = 554.82

W79.25	531.62	550.00	-4.82	550.00
"	539.19	"	-4.82	"
"	546.75	"	-4.82	549.99
"	548.25	"	-4.82	550.00
W82.25	512.00	"	-4.82	"
"	514.83	"	-4.82	"
"	521.06	"	-4.82	"
"	528.62	"	-4.82	"
"	531.62	"	-4.81	550.01
"	539.19	"	-4.82	550.00
"	546.75	"	-4.82	"
"	548.25	"	-4.82	"
W94.58	512.00	"	-4.82	"
"	514.83	"	-4.82	"
"	521.06	"	-4.82	"
"	528.62	"	-4.82	"
"	531.62	"	-4.82	"
"	539.19	"	-4.81	550.01
"	546.75	"	-4.82	550.00
"	548.25	"	-4.82	"

Filter Walkways (cont'd)

H.I. = 554.82

W100.0852.00	550.00	-4.82	550.00
" 514.83	"	-4.82	"
" 521.06	"	-4.82	"
" 528.62	"	-4.82	"
" 531.62	"	-4.81	550.01
" 539.19	"	-4.82	550.00
" 546.75	"	-4.82	"
" 548.25	"	-4.82	"
W112.42.512.00	"	-4.82	"
" 514.83	"	-4.81	550.01
" 521.06	"	-4.82	550.00
" 528.62	"	-4.82	"
" 531.62	"	-4.82	"
" 539.19	"	-4.83	549.99
" 546.75	"	-4.82	550.00
" 548.25	"	-4.82	"
CEBM.	549.75	-5.07	549.75

MOC. 311950

Leonard 26
 Corner
 K+E Level 106346

Check Sub-grade and grade on floor of
 Gardner's shed under right entrance

BM 16.355	544.555		538.20
Sub-Grade		-5.87	538.68
"		-5.88	538.67
"		-5.86	538.69
T.P. ^{Iron} Pin		-5.865	538.69
+ 5.08	543.77		
N.W. Cor.	539.08	-4.69	539.08
N. center	539.06	-4.71	539.06
N.E. Cor.	539.04	-4.73	539.04
S.W. Cor.	539.08	-4.69	539.08
S. center	539.04	-4.73	539.04
S.E. Cor.	539.00	-4.77	539.00

N.E. LEVEL 106346

APRIL 4, 1950 LEONARD P. CARYER

CHECK FORMS FOR WEIR WALL IN BRINE DILUTION CHAMBER:

B.M.	+3.83	542.79		540.46
TOP OF WALL - E. SIDE			-9.56	534.23 .02 LOW
"	"		-9.56	534.23 .02 LOW
TOP OF STEEL PLATE E. SIDE			-9.36	534.43 } HELD LOW FOR PIER, WILL BE SET TO GRADE LATER
"	"		-9.38	534.41
TOP OF WALL, W. SIDE			-9.57	534.22 .03 LOW
"	"		-9.57	534.22 .03 LOW
TOP OF STEEL PLATE, W. SIDE			-9.40	534.39 } SAME AS E. SIDE.
"	"		-9.39	534.40
CHECK B.M.			-3.83	540.46

SETTLING BASIN, CHECK ELEV'S. OVER COLUMNS

NOTE: READINGS AT 568.92 WERE TAKEN INSIDE
OF OVERFLOW TROUGHS, OVER COLUMN CENTERS.
ALL OTHER READINGS WERE TAKEN ON CREST
OF ROUND TOP OF DIVIDING WALLS, OVER COLUMNS
AS LOCATED BY PLANT COORDINATES. A SMALL
SQUARE OF YELLOW PAVEMENT PAINT WAS PLACED
AT POINTS WHERE READINGS ARE TAKEN, TO
ASSURE TAKING FUTURE READINGS AT SAME
POSITIONS.

R.M.	ELEV.		SE. COR. SALT STG. TANK.
551.21			546.66
E65.08 568.92		-5.360	545.85
" 590.42		-8.820	542.39
" 5111.92		-8.830	542.38
" 5183.42		-8.842	542.368
E82.08 568.92		-5.341	545.869
" 590.42		-8.812	542.398
" 5111.92		-8.838	542.372
" 5183.42		-8.825	542.385
E99.08 568.92		-5.368	545.842.
" 590.42		-8.852	542.378
" 5111.92		-8.835	542.375
" 5183.42		-8.830	542.38
E116.08 568.92		-5.388	545.822
" 590.42		-8.825	542.385
" 5111.92		-8.828	542.382
" 5183.42		-8.865	542.345
E206.08 5183.42		-8.820	542.39

ELEV. OVER COLUMNS IN BASINS, CONT'D.

N.d.	561.21		
E133.08	568.92	-5.812	545.838
"		-8.850	542.36
"		-8.840	542.37
"		-8.845	542.365
E150.08	568.92	-5.812	545.838
"		-8.850	542.36
"		-8.870	542.34
"		-8.842	542.368
E167.08	568.92	-5.808	545.907
"		-8.840	542.37
"		-8.845	542.365
"		-8.850	542.36
E184.08	568.92	5.846	545.865
"		-8.830	542.38
"		-8.828	542.382
"		-8.835	542.375
E201.08	568.92	-5.81	545.90
"	590.42	-8.830	542.38
"	511.92	-8.822	542.388

LAST LINE ON PAGE 28.

APRIL 4, 1950 LEONARD 30
CARVER

ELEV. ON TOP OF CURB ON SOUTH WALL OF SETTLING BASIN #1

H.d.	551.21	
E48	-0.71	550.50
E68	-0.715	550.495
E88	-0.705	550.505
E108	-0.725	550.485
E128	-0.730	550.48
E148	-0.690	550.52
E168	-0.695	550.515
E188	-0.720	550.49
E208	-0.730	550.48
CHECK B.M.	-4.55	546.66

MAIN ENTRANCE STAIRWAY, FORM ELEV'S.

R.M.	+1.86	553.10		551.24	TOP OF PARAPET NEAR STAIRS.
S. WALL	W 47.	549.41	-3.70	549.40	
"	W 54	"	-3.71	49.39	
"	W 54	547.33	-5.80	47.30	
"	W 61	"	-5.80	47.30	
"	W 61	545.25	-7.875	45.225	
"	W 68	"	-7.875	45.225	
N. WALL	W 47	550.96	-2.135	50.965	
"	"	550.08	-3.00	50.10	
"	"	551.25	-1.84	51.26	
"	W 54	550.96	-2.13	50.97	
"	"	550.08	-3.00	50.10	
"	"	551.25	-1.84	51.26	
"	W 61	550.96	-2.12	50.98	
"	"	550.08	-3.00	50.10	
"	"	551.25	-1.835	51.265	
"	W 68	550.96	-2.12	50.98	
"	"	550.08	-3.00	50.10	
"	"	551.25	-1.83	51.27	
CHECK	R.M.		-1.86	551.24	

April 19, 1960
A.M.

Leonard 32
Coover
K45 Level 4106346

ELEV. ON WALKWAY OF ZEOLITE BED #7 BEFORE FLOODING

B.M. 9 E. CO. BRINE DILUTION BOX IN H.H.

540.464

+3.501 543.965

POINT #1,

-4.990 538.975

#2,

-4.984 538.981

#3,

-4.963 539.002

#4,

-4.940 539.025

#5,

-4.963 539.002

#6,

-4.978 538.987

#7,

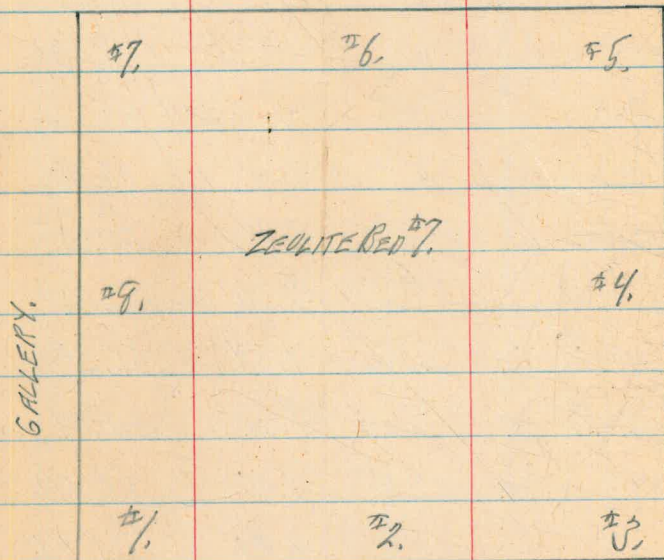
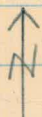
-5.000 538.965

#8,

-4.990 538.975

CHECK B.M.

-3.501 540.464



S. END OF RIDGE.

POINTS ON WALKWAY AT 539 LEVEL, AS CLOSE
AS POSSIBLE TO SUPPORTING WALLS BENEATH.

April 10, 1950
P.M.

Leonard Carver 33
K+E level 106346

Filter Walkways North-half Beds #2+4.

<u>Bent</u>	<u>Location</u>	<u>Grade</u>	<u>rod</u>	<u>Elev.</u>
BM+509		554.825		549.735
	W.47.08 N49.75	550.00	-4.825	
"	N57.85	"	-4.825	
"	N64.87	"	-4.825	
"	N67.87	"	-4.82	
"	N75.93	"	-4.82	
"	N83.50	"	-4.82	
"	N85.50	"	-4.825	
	W.49.08 N49.75	"	-4.82	
"	N57.85	"	-4.82	
"	N64.87	"	-4.825	
"	N67.87	"	-4.83	
"	N75.93	"	-4.83	
"	N83.50	"	-4.82	
"	N85.50	"	-4.82	
	W61.42 N49.75	"	-4.82	
"	N57.85	"	-4.825	
"	N64.87	"	-4.83	
"	N67.87	"	-4.83	
"	N75.93	"	-4.825	

Filter Walkways (cont'd)

HI - 554.825			
Location	Grade	- ROD	Elev.
W61.42 N83.50	550.00	-4.825	550.00
" N85.50	"	-4.825	"
W66.92 N49.75	"	-4.825	"
" N57.85	"	-4.825	"
" N64.87	"	-4.83	549.995
" N67.87	"	-4.83	"
" N75.93	"	-4.83	"
" N83.50	"	-4.83	"
" N85.50	"	-4.82	550.005
W79.25 N49.75	"	-4.82	"
" N57.85	"	-4.82	"
" N64.87	"	-4.825	550.00
" N67.87	"	-4.825	"
" N75.93	"	-4.82	550.005
" N83.50	"	-4.82	"
" N85.50	"	-4.83	549.995
W82.25 N49.75	"	-4.83	"
" N57.85	"	-4.825	550.00
" N64.87	"	-4.825	"

Filter Walkways (Cont'd)

Location	H.I. = 554.825 Grade	rod	Elev.
" N67.87	550.00	-4.825	550.00
" N75.95	"	-4.825	"
" N83.50	"	-4.82	550.005
" N85.50	"	-4.82	"
W99.58 N49.75	"	-4.82	"
" N57.85	"	-4.82	"
" N64.87	"	-4.82	"
" N67.87	"	-4.82	"
" N75.95	"	-4.83	549.995
" N83.50	"	-4.825	550.00
" N85.50	"	-4.82	550.005
W100.08 N49.75	"	-4.82	"
" N57.85	"	-4.82	"
" N64.87	"	-4.82	"
" N67.87	"	-4.82	"
" N75.95	"	-4.83	549.995
" N83.50	"	-4.83	"
" N85.50	"	-4.83	"

Filter Walkways (cont'd)

HI = 554.825

Location	Grade	rod	Elev
W112.42N49.75	550.00	-4.825	550.00
" N57.85	"	-4.825	"
" N64.87	"	-4.83	549.995
" N67.87	"	-4.83	"
" N75.93	"	-4.825	550.00
" N83.50	"	-4.82	550.005
" N85.50	"	-4.825	550.00
ch BM	549.735	-5.09	549.735

B.M. + 9.76

544.16

534.40

-5.74

-5.76

APRIL, 18 1950

Leonard
Carter

38

Zeolite main entry staves

B.M. +10.58	548.78		538.20
	537.95	- 11.01	537.77
	"	- 10.95	537.83
	"	- 11.04	537.66 ⁷²
	539.28	- 9.53	539.14 ²⁵
	"	- 9.54	539.16 ²⁴
	541.29	- 7.66	541.04 ¹²
	541.29	- 7.68	541.07 ¹⁰
^{5.0} Sub-Grade	540.79	- 8.12	540.58 ⁶⁶
"	"	- 8.05	540.64 ⁷³
"	"	- 8.09	540.69
"	"	- 8.06	540.64 ⁷²
"	"	- 8.03	540.67 ⁷⁵
"	"	- 8.04	540.66 ⁷⁴
"	"	- 8.05	540.65 ⁷³
300m E-W	539.71	- 9.11	539.59 ⁶⁷
"	"	- 9.10	539.68
"	"	- 9.15	539.55 ⁶³
300m	542.79	- 6.07	547.63 ⁷¹
"	"	- 6.06	547.64 ⁷²

Zeolite main Entry Stoies

beam	542.79	- 6.05	542. ⁷³ 65
	542.79	- 6.06	542. ⁷² 64
flow	543.79	- 5.05	543.73
ck. BM		- 10.58	538.20

Apr. 120, 1950
A.M.

Leonard
Corvee
K+E Level 1106346 40

Filter Floor at Elev 539.00 Filters #3+5

South Half of Sub-Grade + Finished Grade

B.M. + 5.13	543.33		538.20 (M.H.) ^{21m}
W3075 548.25	Sub-Grade 538.50	-4.83	538.50
" 568.25	"	-4.83	" .50
" 568.25	"	-4.84	" .49
" 578.25	"	-4.85	" .48
" 584.50	"	-4.83	" .50
W93.52 548.25	"	-4.84	" .49
" 558.25	"	-4.84	" .49
" 568.25	"	-4.86	" .47
" 578.25	"	-4.86	" .47
" 584.50	"	-4.86	" .47
W103.52 548.25	"	-4.84	" .49
" 558.25	"	-4.83	" .50
" 568.25	"	-4.81	" .52
" 578.25	"	-4.83	" .50
" 584.50	"	-4.84	" .49
W112.42 548.25	"	-4.87	" .46
538.25	"	-4.86	" .47
568.25	"	-4.86	" .47

H.I. = 543.33 Filter Floor (cont'd)

W112.42	578.25	538.50	-4.23	538.50
"	584.50	"	-4.84	.49
W116.42	548.25	"	-4.25	.48
"	558.25	"	-4.25	.48
"	568.25	"	-4.25	.48
"	578.25	"	-4.25	.48
"	584.50	"	-4.26	.47
W129.75	548.25	"	-4.27	.46
"	558.25	"	-4.25	.48
"	568.25	"	.25	.48
"	578.25	"	-4.24	.49
"	584.50	"	-4.20	.53
W135.00	548.25	"	-4.20	.53
"	558.25	"	-4.22	.51
"	568.25	"	-4.24	.49
"	578.25	"	-4.24	.49
"	584.50	"	-4.25	.48
W148.33	548.25	"	-4.25	.48
	558.25	"	-4.23	.50
	568.25	"	-4.24	.49

#2

HT=543.33 (Filter Floor (Cont'd))

W14833	578.25	538.50	-4.85	538.48
	584.50	"	-4.86	".47
W6997	548.25	^{Finished P. 60e} 539.00	-4.33	539.00
"	558.25	"	-4.33	"
"	568.25	"	-4.33	"
"	578.25	"	-4.33	"
"	584.50	"	-4.33	"
W9476	548.25	"	-4.33	"
"	558.25	"	-4.33	"
"	568.25	"	-4.34	538.99
"	578.25	"	-4.33	539.00
"	584.50	"	-4.33	"
W100.09	548.25	"	-4.34	538.99
"	558.25	"	-4.33	539.00
"	568.25	"	-4.33	"
"	578.25	"	-4.33	"
"	584.50	"	-4.32	539.01
W13.42	548.25	"	-4.32	"
"	558.25	"	-4.33	539.00
"	568.25	"	-4.33	"

H.J. = 543.33 Filtered Floor (cont'd)

W113.425	78.75	539.00	-4.33	539.00
"	584.50	"	-4.33	"
W115.425	48.25	"	-4.33	"
"	558.25	"	-4.33	"
"	568.25	"	-4.33	"
"	578.25	"	-4.34	538.99
"	584.25	"	-4.34	"
W127.75	548.25	"	-4.33	539.00
"	558.75	"	-4.33	"
"	568.75	"	-4.33	"
"	578.75	"	-4.33	"
"	584.50	"	-4.32	539.01
W133.08	548.25	"	-4.33	539.00
"	558.25	"	-4.33	"
"	568.25	"	-4.33	"
"	578.25	"	-4.33	"
"	584.25	"	-4.33	"
W145.425	48.25	"	-4.34	538.99
"	558.25	"	-4.33	539.00
"	568.25	"	-4.33	"

HT = 543.33 Filter Floor (cont'd)

W14.42	578.25	539.00	-4.33	539.00
"	584.50	"	-4.32	539.01
W17.42	548.25	"	-4.33	539.00
"	558.25	"	-4.33	"
"	568.25	"	-4.33	"
"	578.25	"	-4.32	539.01
"	584.50	"	-4.33	539.00
W15.31	548.25	"	-4.33	"
"	558.25	"	-4.33	"
"	568.25	"	-4.33	"
"	578.25	"	-4.33	"
"	584.50	"	-4.33	"
cbm			-5.13	538.20

Apr. 24, 1960

Leander
Covee

46

Sub-Grade South-Half. Filter #5

P.M. +5.94

544.14

538.20

5192
P.M.H. W100

538.50

-5.64

538.50

"

-5.64

538.50

"

-5.67

538.47

"

-5.70

538.44

"

-5.68

538

"

-5.63

"

-5.64

"

-5.67

"

-5.69

"

-5.64

"

-5.65

"

-5.65

"

-5.66

"

-5.64

"

-5.67

"

-5.64

"

-5.69

"

-5.64

"

HS - 54414

536.00	-8.14	536.00
"	-8.42	
"	-8.37	
"	-8.26	
"	-8.42	
"	-8.05	
538.20	-5.94	538.20

A 3m.

April 24, 1950

Leandro
Corvee

47

Beam Soffit in Retaining Wall Stairs

BM +1.61	536.13		534.52
N-END	532.67	-3.46	532.67
S-END	"	-3.47	532.66
N-END	533.67	-2.46	533.67
S-END	"	-2.46	533.67
cbm	534.52	-1.61	534.52

April 29, 1950:

STEP ELEV IN RETAINING WALL STAIRS:

BM +4.98	545.18		538.20	RIM M.H. S192, W100
TOP LANDING	CORRECT GRADE 538.75	-4.45		
1ST STEP	538.16	-5.02		
2ND "	537.56	-5.62		
3RD "	536.97	-6.21		
4TH "	536.37	-6.81		
5TH "	535.78	-7.41		
6TH "	535.18	-8.00		
BOTTOM STEP	534.59	-8.59		
KEY UNDER WALK	533.67	-9.51		
CA. BM.		-4.98		

April 24, 1950

Leonard
Corvee

48

Filter Gallery Roof Forms - East Half ^{West Half 74089}

B.M. 4.985	567.31		562.325
(F-11)	567.31 561.19	cod -6.13	elev 561.18
	562.43	-4.90	562.41
	562.43	-4.88	562.43
(F-9)	561.54	-5.76	561.55
	562.43	-4.88	562.43
	562.43	-4.87	562.44
(F-9)	561.54	-5.76	561.55
	562.43	-4.88	562.43
	562.43	-4.89	562.42
(F-10)	561.19	-6.15	561.16
	562.43	-4.90	562.41
	562.43	-4.89	562.42
(F-9)	561.54	-5.76	561.55
	562.43	-4.89	562.42
	562.43	-4.88	562.43
(F-9)	561.54	-5.76	561.55
	562.43	-4.89	562.42
	562.43	-4.87	562.44
(F-11)	561.19	-6.12	561.19

Filter Gallery Roof forms - (cont'd)

H.I. =	567.31		
(WF)	5600e	18.0	det.
150	567.11	-10.22	557.09
"	"	-10.22	"
(WF)	"	-10.22	"
151	"	-10.21	557.10
(WF)	"	-10.22	557.09
152	"	-10.21	557.10
(WF)	"	-10.21	"
153	"	-10.22	557.09
(WF)	"	-10.21	557.10
154	"	-10.21	"
(WF)	"	-10.21	"
155	"	-10.21	"
(WF)	"	-10.21	"
169	"	-10.20	557.11
(WF)	"	-10.20	"
170	"	-10.21	557.10
(WF)	"	-10.21	"
171	"	-10.21	"

Fitter Gallery Roof forms (cont'd)

H.I. -	567.31		
(WF 172)	557.11	-10.21	557.10
"	"	-10.21	"
(WF 173)	"	-10.21	"
"	"	-10.20	557.11
(WF 174)	"	-10.20	"
"	"	-10.20	"

cb B.N. 562.33 -4.18 562.33

FILTER WASH WATER FLUME, S. SIDE, SUB. GRADE 2 FORMS.

		548.90		
W109	GROUND	538.71	-5.90	538.00
	N. FORM	538.87	-5.02	538.88
	S. FORM	"	-5.02	538.88
W114.58	GROUND	538.19	-5.82	538.05
	" EXIST. CONC.	538.87	-5.04	538.86
	" BOTTOM CURTAIN WALL		-6.43	537.47
W108	" "	"	-6.47	537.43
W98	" "	"	-6.42	537.48
W88	" "	"	-6.26	537.64
W88.4	" "	" STAIRS	-6.43	537.47
CHECK B.M.			-5.70	538.20

B.M.	+5.70	548.90		538.20
				<small>R.M.M.H. SIDE, W100</small>
W47.75	GROUND	538.33	-5.85	538.05
"	FORM	539.00	-4.90	539.00
W58	GROUND	538.31	-5.85	538.05
"	N. FORM	538.98	-4.92	538.98
"	S. FORM	"	-4.92	538.98
W68	GROUND	538.29	-5.99	537.91
"	N. FORM	538.96	-4.95	538.95
"	S. FORM	"	-4.94	538.96
W78	GROUND	538.27	-5.98	537.92
"	N. FORM	538.94	-4.96	538.94
"	S. FORM	"	-4.96	538.94
W88	GROUND	538.25	-5.87	538.03
	N. FORM	538.92	-4.97	538.93
	S. FORM	"	-4.98	538.92
W98	GROUND	538.23	-5.92	538.08
	N. FORM	538.90	-5.00	538.90
	S. FORM	"	-5.00	538.90

← Control

Filter Plant
Check Levels
West 200 ltr Chambers

August 1-1950
Poincy-Notes
King &
Leonard
Baker

52.

B.m.

540.465

3.588 544.053

531 W 12.1

5.085

574 W 12.2

5.065

575 W 12.2

5.062

5118.3 W 12.3

5.061

5118.3 W 45.7

5.049

575 W 45.0

5.064

574.1 W 45.0

5.065

531.6 W 45

5.083

East zeolite chamber
Allarado filtration plant

Aug. 1, 1950

Rainey - Notes 53.
King &
Leonard
Baker

540465

3.59.0 540455

531 E12.3

5.064

574.1 E12.6

5.073

575.0 E12.6

5.079

517.1 E12.5

5.091

517.0 E45.6

5.042

574.9 E45.7

5.077

574.3 E45.7

5.077

531.1 E45.7

5.046

Levels Top Wall
Settling Basin

August 1-1950 - Hot
King T
Leonard
Baker

54.

B. 121

8.32

554.98

546.66

East End Salt Storage Tank

0.60N E4883

4.970

42N 82'E

5.085

116'E

4.950

150'E

5.045

184'E

4.985

218E E

4.980

253'E

4.992

287'E

4.983

321'E

4.965

355'E

4.985

389E E

4.960

389E E 4.55

4.962

52.5

4.981

15'S

4.955

15'S

4.955

40S

4.945

T = 554.98

309.5E	58.5	4.960	
	58.5	4.960	
	80.5	4.985	
	100.5	4.965	
	101.5	4.940	
	120.5	4.960	
	143.5	4.925	
	143.5	4.925	
	153.5	4.958	
153.5	355E	4.975	550.005
	321E	4.988	549.992
	287E	4.962	550.018
	252E	4.980	550.000
1	218.6E	5.019	549.961
	184.0E	4.990	549.990
	161.0E	4.978	550.002
	116.0E	4.988	549.992
	82.0E	5.001	549.979
	48.00E	4.965	550.015

Notes reduced
 1-20-1959
 C.O. NELSON

$\pi = 554.98$

48 E	143.65	4.990
	143.25	4.995
	120.05	5.020
	101.45	5.001
	101.05	5.000
	80.05	4.964
	68.45	4.970
	68.05	4.990
	40.05	5.016
	15.45	5.015
	15.05	5.010
	9.05	5.001
	8.75	4.992
218.6E	4.55	4.985
	5.05	5.000
	15.05	5.011
	15.35	5.008
	40.05	4.980
	58.05	4.975

554.98

218.65583

4.970

80.5

5.005

101.5

4.980

101.45

4.972

120.5

5.002

143.25

5.015

143.65

5.015

B.M.

8.32 54600

SEPT. 8, 1950

BEATTY
LEONARD

58.

SIDEWALK, W. END FILTERS, GRADES FOR TOP SURFACE

WASH WATER

R.M. + .11 40.92 542.40 541.48 CONTR. STR.

CENTERED ON AXIS:

	FIN. GRADE:		HUB ELEV.	COT OR FILL
W 182.5 BEGIN	537.70	-4.70	537.70	GRADE ON WALL.
W 205.0	537.86	-5.04	537.86	GRADE HUB.
W 227.5	537.03	-5.09	537.21	C.O. ¹⁸
W 250.0 LOW POINT	536.70	-5.32	537.08	C.O. ³⁸
W 281.25 END.	536.90	-5.57	536.83	F.O. ²⁷
CHECK R.M.		-0.92	541.48	

NOTE: WALK IS 4' WIDE, 4" THICK, AND LIES CENTERED

ON PLANT E-W AXIS.

INDEXED

ALVARADO FILTER PLANT

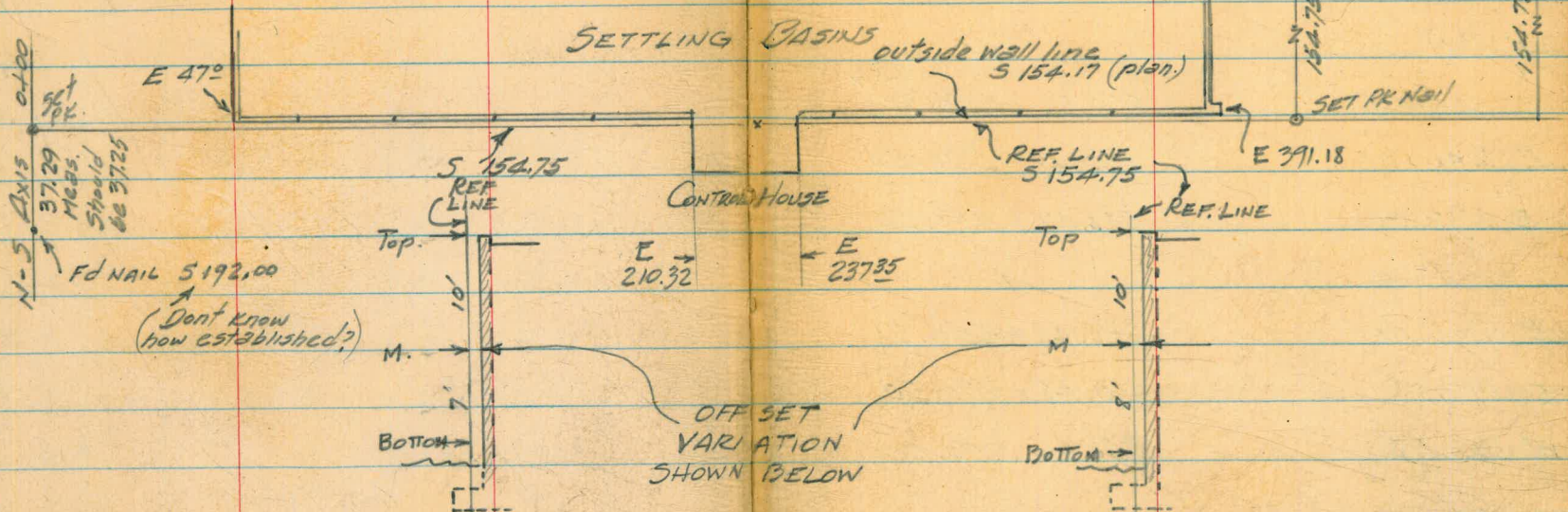
ALIGNMENT CHECK ON SOUTH WALL
SETTLING BASINS No 1 & 2

JUL 23 1959

JAN. 26, 1959

BEATTY
O'BRIEN
FROST

89.



	Top	M	BOTTOM		Top	M	BOTTOM
E 47.0 SW COR	0.41	0.42	0.46	2+37 ³⁵ EAST side Control House	0.46	0.45	0.46
E 68.78	0.29	0.35	0.48	2+44 ⁶⁶ Ex. JT.	0.49	0.44	0.49
E 90.56 Ex. JT.	0.19	0.32	0.44	2+61.71	0.32	0.44	0.505
E 107.62	0.17	0.31	0.43	2+78 ⁷⁶ Ex. JT.	0.37	0.40	0.46
E 124.68 Ex. JT.	0.21	0.34	0.45	2+95 ⁶⁷	0.375	0.49	0.52
E 141.61	0.24	0.34	0.47	3+12 ⁵⁸ Ex. JT.	0.42	0.46	0.50
E 158.54 Ex. JT.	0.30	0.34	0.42	3+29 ⁶¹	0.435	0.49	0.52
E 175.52	0.32	0.36	0.44	3+46 ⁶⁵ Ex. JT.	0.46	0.49	0.52
E 192.50 Ex. JT.	0.36	0.43	0.47	3+68 ⁹¹	0.50	0.48	0.50
E 210.32 W. Side Control House	0.49	0.43	0.49	3+91 ¹⁸ SE COR.	0.485	0.46	0.445

Alvarado Filter Plant
 Check Elev. Top of South Wall
 SETTLING BASINS N°1 & N°2

JAN. 27, 1959
 Beatty
 O'Brien
 Frost

61.

CK BM 546.66
 E 244.58 550.50 = 550.50
 E 240.08 550.48 = 550.50
 E 232.08 550.47 = 550.50

Elev.s from F.B. 741-106

E 205.08 550.48 = 550.51
 E 197.08 550.48 = 550.50
 E 192.58 550.49 550.50

Elev.s from This Book pp. 30

E E 208 550.48 = 550.48
 E E 188 550.49 = 550.49
 E E 168 550.51 = 550.515
 E E 148 550.51 = 550.52
 E E 128 550.48 = 550.48
 E E 108 550.49 = 550.485
 E E 88 550.51 = 505.505
 E E 68 550.51 = 550.495
 E E 48 550.52 = 550.50

E BM 546.66
 (Direct Reading Rod used.)

SE Cor SALT STORAGE

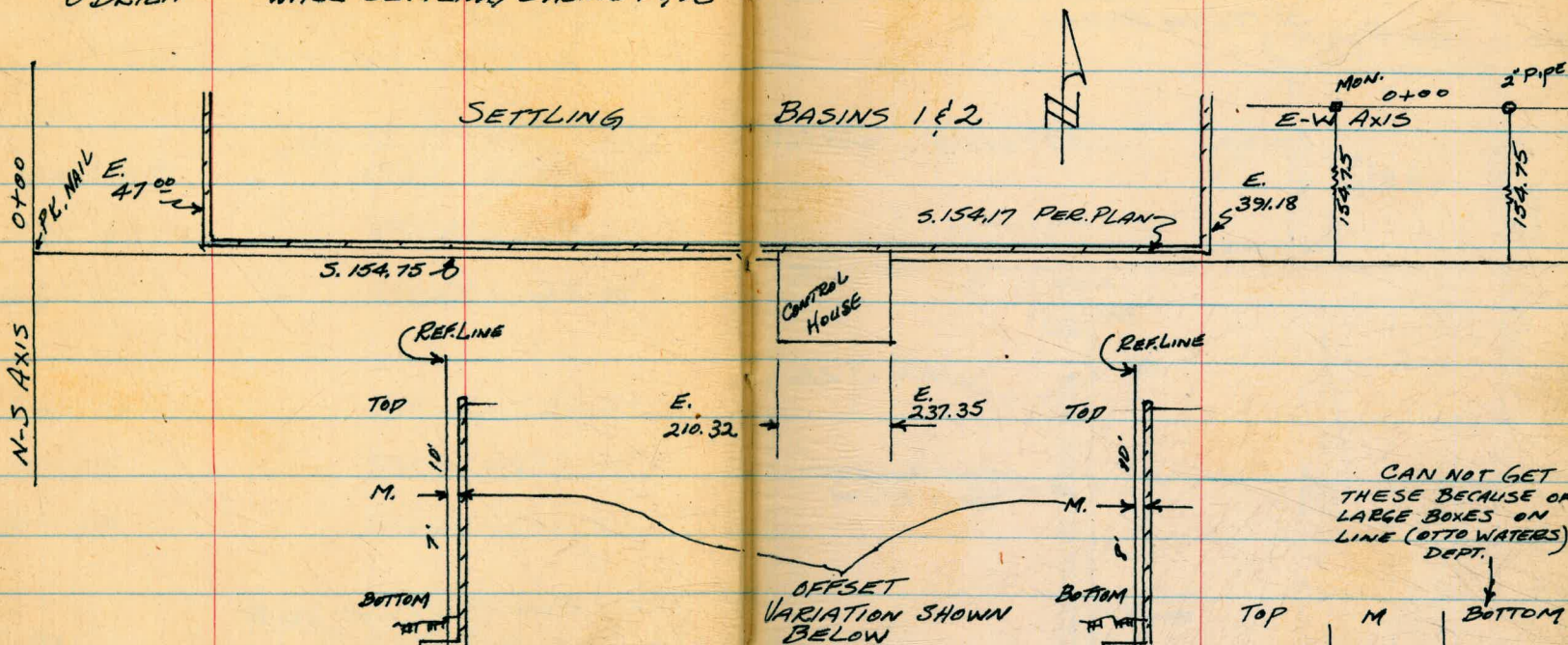
SHOREY
KEMP
O'BRIEN

ALVARADO FILTER PLANT
ALIGNMENT CHECK ON SOUTH
WALL SETTLING BASINS 1 & 2

5/18/60

OVERCAST & COOL

(61)



CAN NOT GET
THESE BECAUSE OF
LARGE BOXES ON
LINE (OTTO WATERS)
DEPT.

OFFSET
VARIATION SHOWN
BELOW

	TOP	M	BOTTOM		TOP	M	BOTTOM
E. 47.0 S.W. COR.	0.41	0.40	0.44				
E. 68.78	0.285	0.345	0.45				
E. 90.56 EX. JT.	0.185	0.31	0.41				
E. 107.62	0.16	0.305	0.405				
E. 124.68 EX. JT.	0.21	0.33	0.41				
E. 141.61	0.25	0.35	0.45				
E. 158.54 EX. JT.	0.30	0.35	0.405				
E. 175.52	0.315	0.36	0.43				
E. 192.50 EX. JT.	0.39	0.43	0.47				
E. 210.32 W. SIDE CONTROL HOUSE	0.50	0.45	0.48				
				E. SIDE HOUSE	0.45	0.45	
				2+37.35 EX. JT.	0.43	0.43	
				2+61.71	0.325	0.44	
				2+78.76 EX. JT.	0.34	0.38	0.46
				2+95.67	0.36	0.48	0.52
				3+12.58 EX. JT.	0.405	0.46	0.50
				3+29.61	0.42	0.48	0.54
				3+46.65 EX. JT.	0.45	0.48	0.53
				3+68.91	0.485	0.47	0.50
				3+91.18 S.E. COR.	0.565	0.455	0.445

ALVARADO FILTER PLANT
ALIGNMENT CHECK ON SOUTH WALLS
SETTLING BASINS 1 & 2

S-N AXIS 0+00 P.K. NAIL

E. 47.00

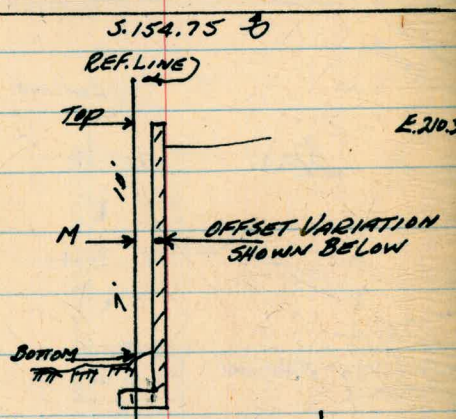
SETTLING BASIN 5 1 & 2

5.154.17 PER PLAN

MAN. E/W AXIS 0+00 2" PIPE

E. 391.18
154.75

164.95



CONTROL HOUSE

E. 210.32

E. 237.35

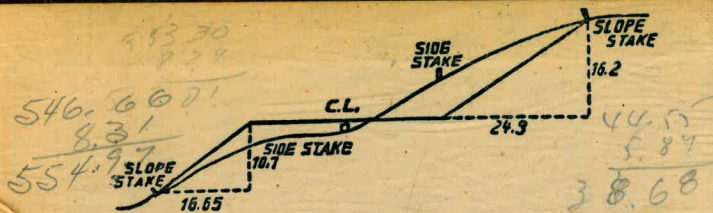
OFFSET VARIATION SHOWN BELOW



	TOP	M	BOTTOM		TOP	M	BOTTOM
E. 47.0 = S.W. COR				E. 237.35 = E. SIDE CONTR. HOUSE			
E. 68.78				E. 244.66 = EX. JT.			
E. 70.56 = EX. JT.				E. 261.71			
E. 107.62				E. 278.76 = EX. JT.			
E. 124.68 = EX. JT.				E. 295.67			
E. 141.61				E. 312.58 = EX. JT.			
E. 158.54 = EX. JT.				E. 329.61			
E. 175.52				E. 346.65 = EX. JT.			
E. 192.50 = EX. JT.				E. 368.91			
E. 210.32 = W. SIDE CONTR. HOUSE				E. 391.18 = S.E. COR.			

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DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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Handwritten notes and calculations on the left page of the notebook. The page is filled with various numbers, including '153.30', '66.92', '572', '546.6601', '8.31', '554.977', '16.65', '10.7', '24.3', '16.2', '44.55', '38.68', '38.20', '36.13', '34.98', '33.18', '32.75', '31.43', '30.09', '29.09', '28.09', '27.09', '26.09', '25.09', '24.09', '23.09', '22.09', '21.09', '20.09', '19.09', '18.09', '17.09', '16.09', '15.09', '14.09', '13.09', '12.09', '11.09', '10.09', '9.09', '8.09', '7.09', '6.09', '5.09', '4.09', '3.09', '2.09', '1.09', '0.09'. There are also several small diagrams and sketches, some with circled numbers like '3.82', '5.68', and '1.4'. The handwriting is in cursive and appears to be a field notebook or a set of working notes for a surveying project.