

JAN 1 4 1965

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

1.67
75
0.92
10 15.92
2.90
12.90

See sketch Pg. 13
Culvert Elev. between
Sta 103 & 104 - Flow Line

See sketch Pg. 14
Guard Rail Location
on Bridge approaches

6x3' Box Drain S/L of Rosecrams
Under Sidewalk Near Sta 173+00
Depth - ? **Covered up - Can't find!**

Location of 24" CPSD (Drain) TP to Existing
Sta. 68+24 or 68+20 16" water crossing
(This drain is shown on Harbor Ref. Draw.)
See (Pg. 12)

See sketch Pg. 14
Run new line - Sta. 132+24⁶⁸
(1st & left at West end
of Bridge) - To make
minimum Horizontal &
of Pipe line - ~~(11/4)~~
22/2

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.20	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

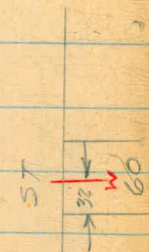
FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.054	.060	.065
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

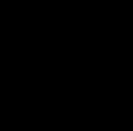
R 31 Francis to 39' East 9th to Atlas 67 ✓
 Alley BIK 89 N of Main to E of Wilson 68-69 ✓
 Alley BIK 92 N of Main to E of Wilson 70-75 ✓
 Alley BIK 53 N of Wightman to E of Main 73-75 ✓
 Alley BIK 43 N of University to E of Main 76 ✓
 N & S Alley in BIK 66 Ocean Beach 5th to Main ✓
 Location of Water Meter - HUBNER PARK 112 ✓
 Location of Water Meter - HUBNER KNOLLS 3 ✓
 " " " " HUBNER KNOLLS ANNEX 2 ✓
 " " " " REDWOOD VILLAGE UNIT 1 5 ✓
 " " " " " " " " 6 ✓
 " " " " " " " " Unit 2 7 ✓
 " " " " " " " " " " 8 ✓
 " " " " " " " " " " 9 ✓
 " " " " " " " " " " 10 ✓
 " " " " " " " " " " MEDINA TERRACE 11 ✓
 " " " " " " " " " " REDWOOD VILLAGE #3 12-14 ✓
 " " " " " " " " " " " " 15-16 ✓
 Proposed E of Water. GERTRUDE, DORCAS to Vicks 17 ✓
 E Profile " " GERTRUDE, Vicks to Lillian 18-19 ✓
 Proposed " " Alley 39th-40th, Dwight Martin 21 ✓
 " " " " BETA ST ALPHA to 41st 22-23 ✓
 " " " " BENSON ST, WOODMAN-65th 25-27 ✓
 Proposed Water PL 1202-Chester on Tank North 29 ✓
 E Profile " " " " " " " " 30-32 ✓
 Newton St 331' west of 43rd to city pl 35-36 ✓
 Calle Aguadulce Rannoke to Cumberland 37-40 ✓
 Calle Tacan (New Profile) 41 ✓
 Newton St 331' west of 43rd to city Prop. 42 ✓
 BALTIC ST LINDA VISTA RD TO ATLAS, Proposed 16" WAT 43-46 ✓
 Revised Alignment, Profile, etc.
 Harbor Dr Proposed 16" PL 47-62 ✓
 Baltic St Linda Vista Rd to Atlas 63 ✓

LOCATION OF WATER METERS
IN HUBNER PARK

METERS ARE AS PER PLAN
8254-L SHEET 7, EXCEPT
AS NOTED.



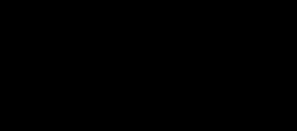
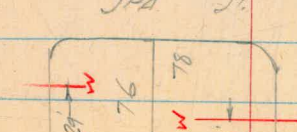
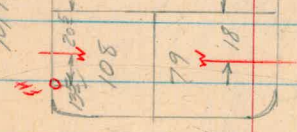
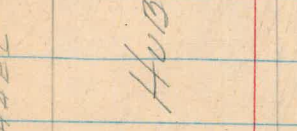
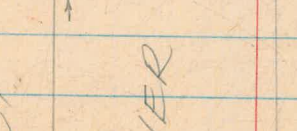
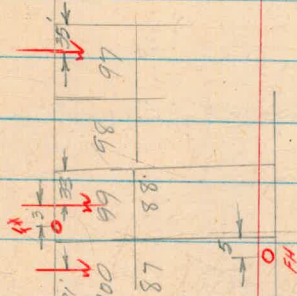
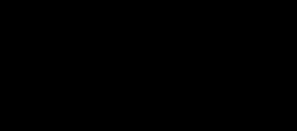
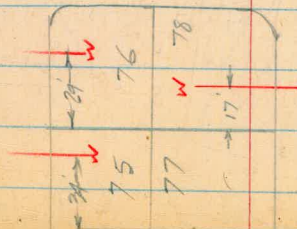
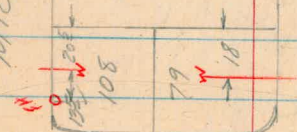
DWIGHT ST



DAY

MICHAEL ST

HUBNER

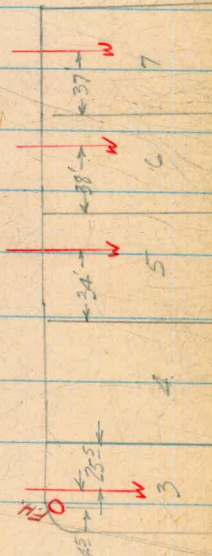


MAY 15 1951
BEATTY
LEONARD
NELSON

27

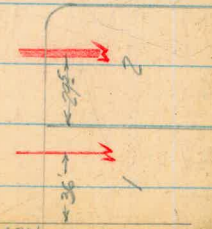
PARK

VIEW



SPA

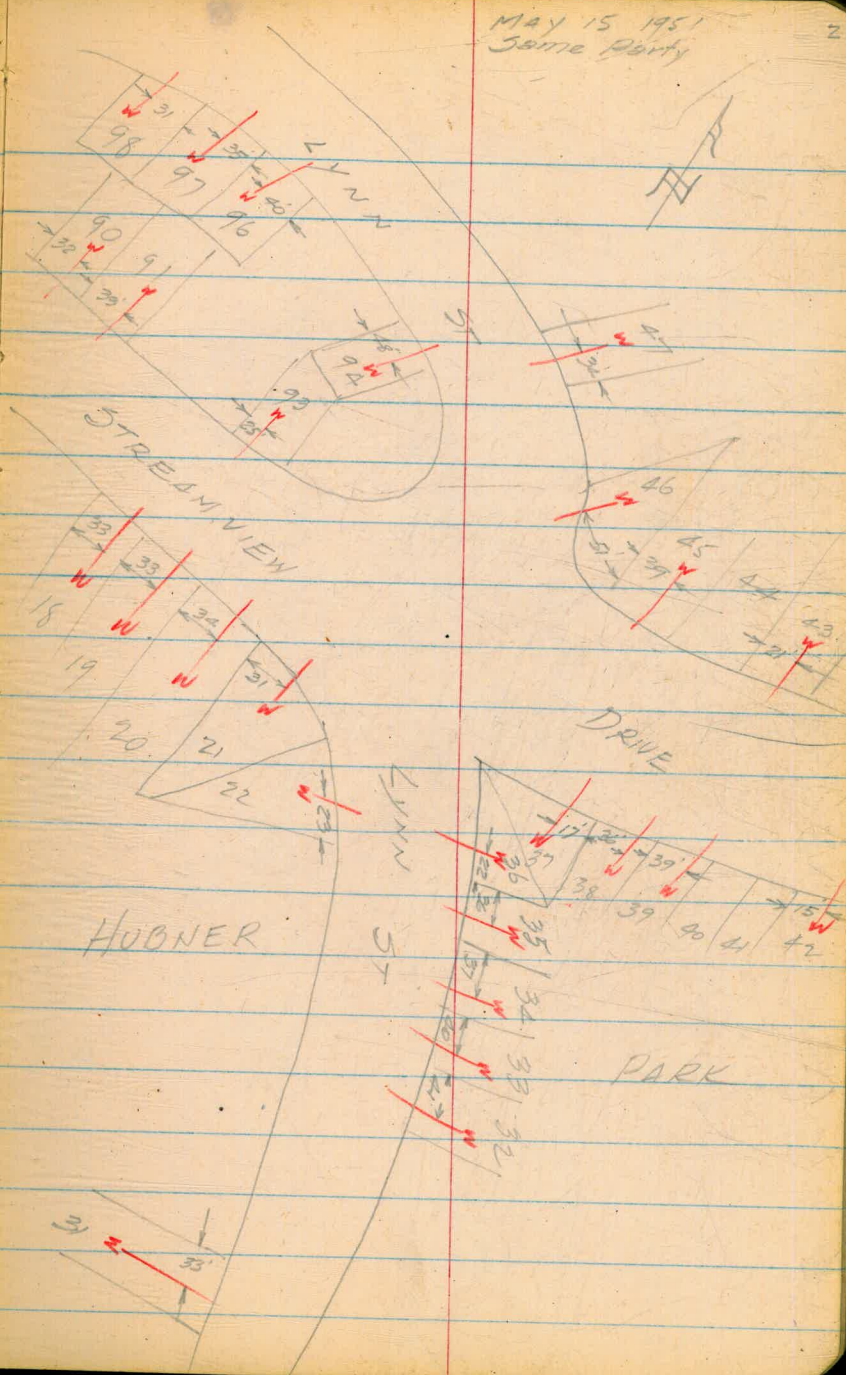
Stream



SUB-DIV. BOUNDARY

LOCATION OF WATER METERS
IN HUGNER PARK

Meters are located as per plan
8255-L Sheet 8, Except as
noted.

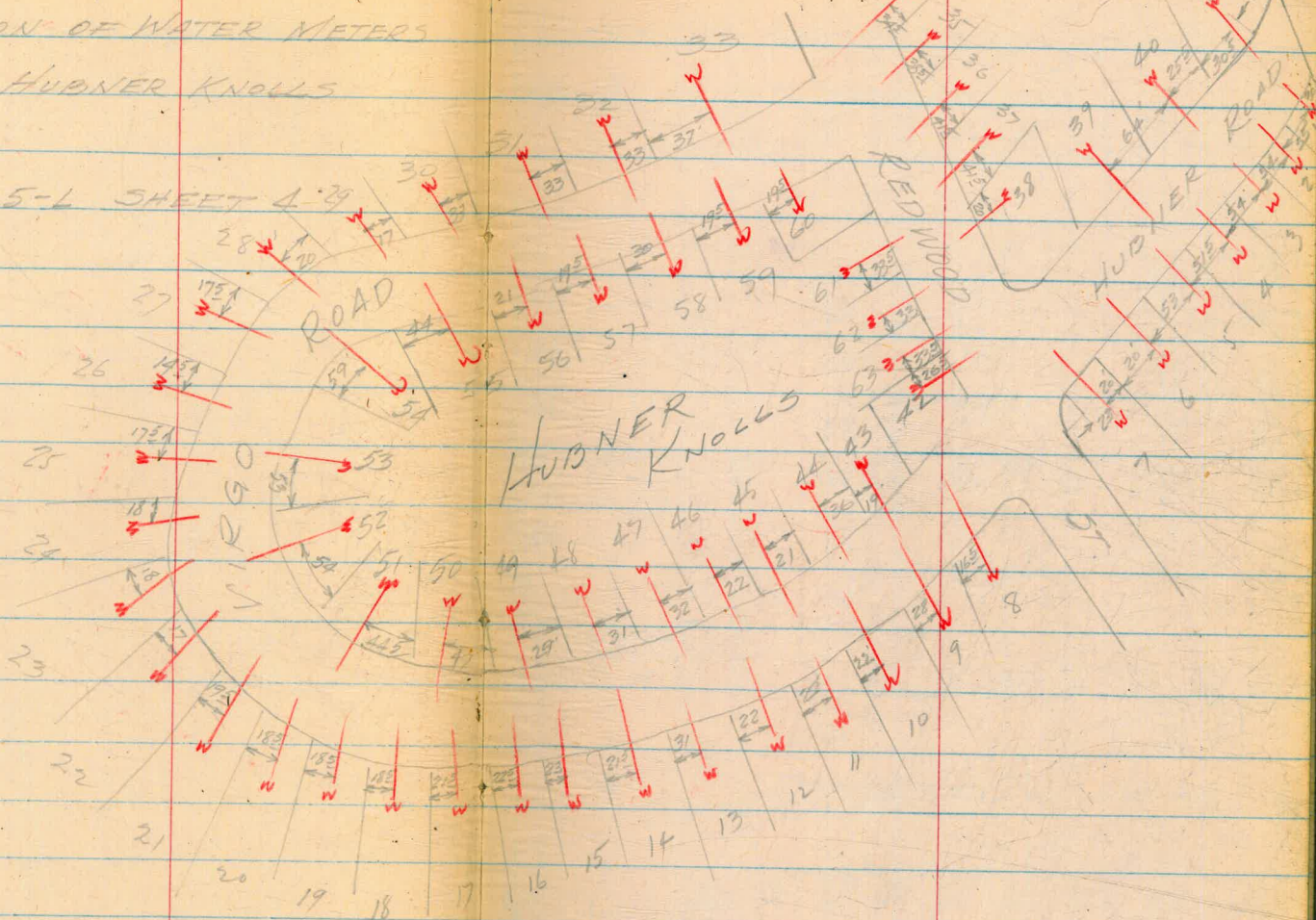


May 15, 1951

BETTY
LEONARD
NELSON

LOCATION OF WATER METERS
IN HUBNER KNOLLS

PLAN 7965-L SHEET 4-39



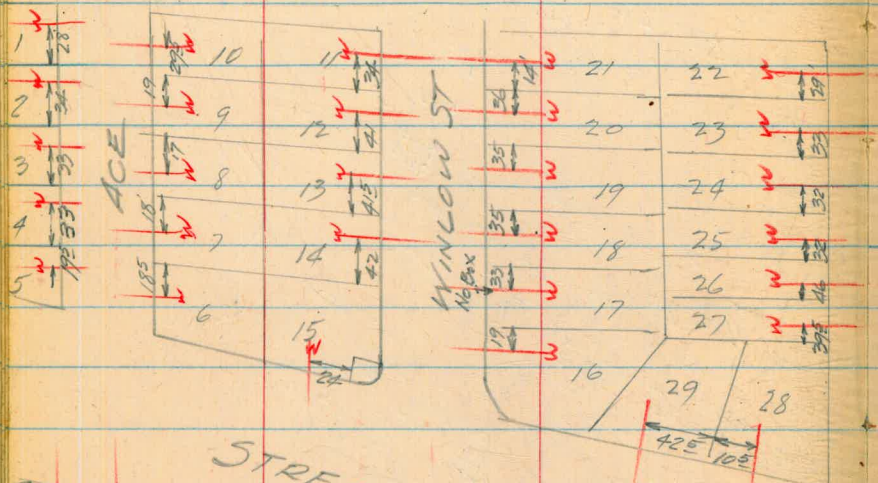
May 16, 1951

H. BRATTY
D. LEONARD
S. NELSON

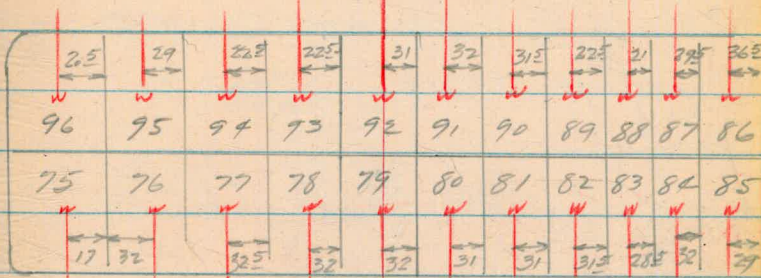
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LOCATION OF WATER METERS
IN HUBNER KNOLLS ANNEX

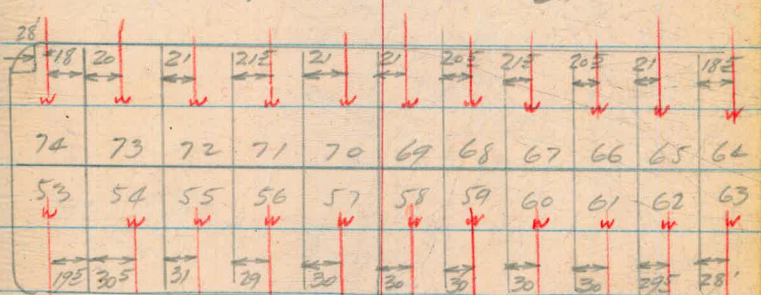
PLAN 8092 L Sheet 7



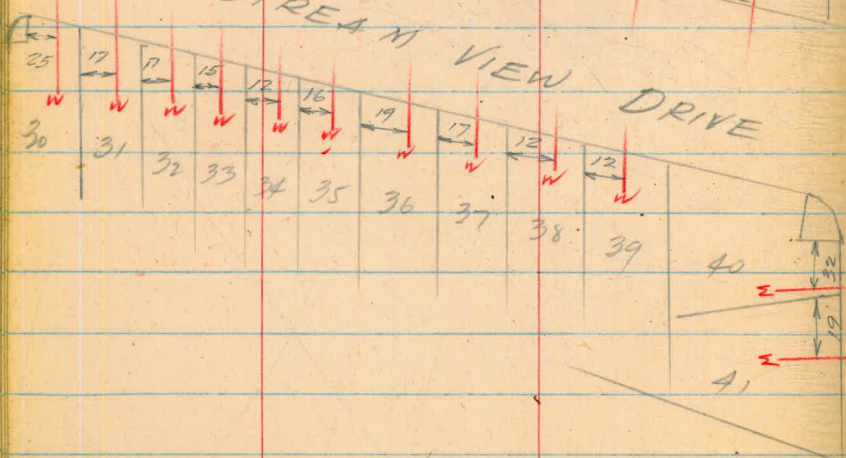
DWIGHT ST



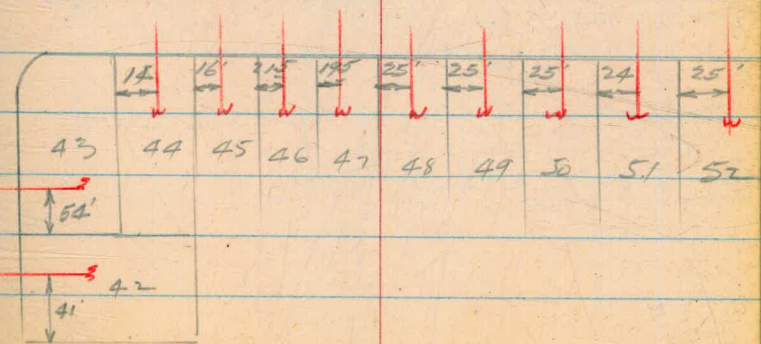
MICHAEL ST



STREAM VIEW DRIVE



STREAM VIEW DRIVE



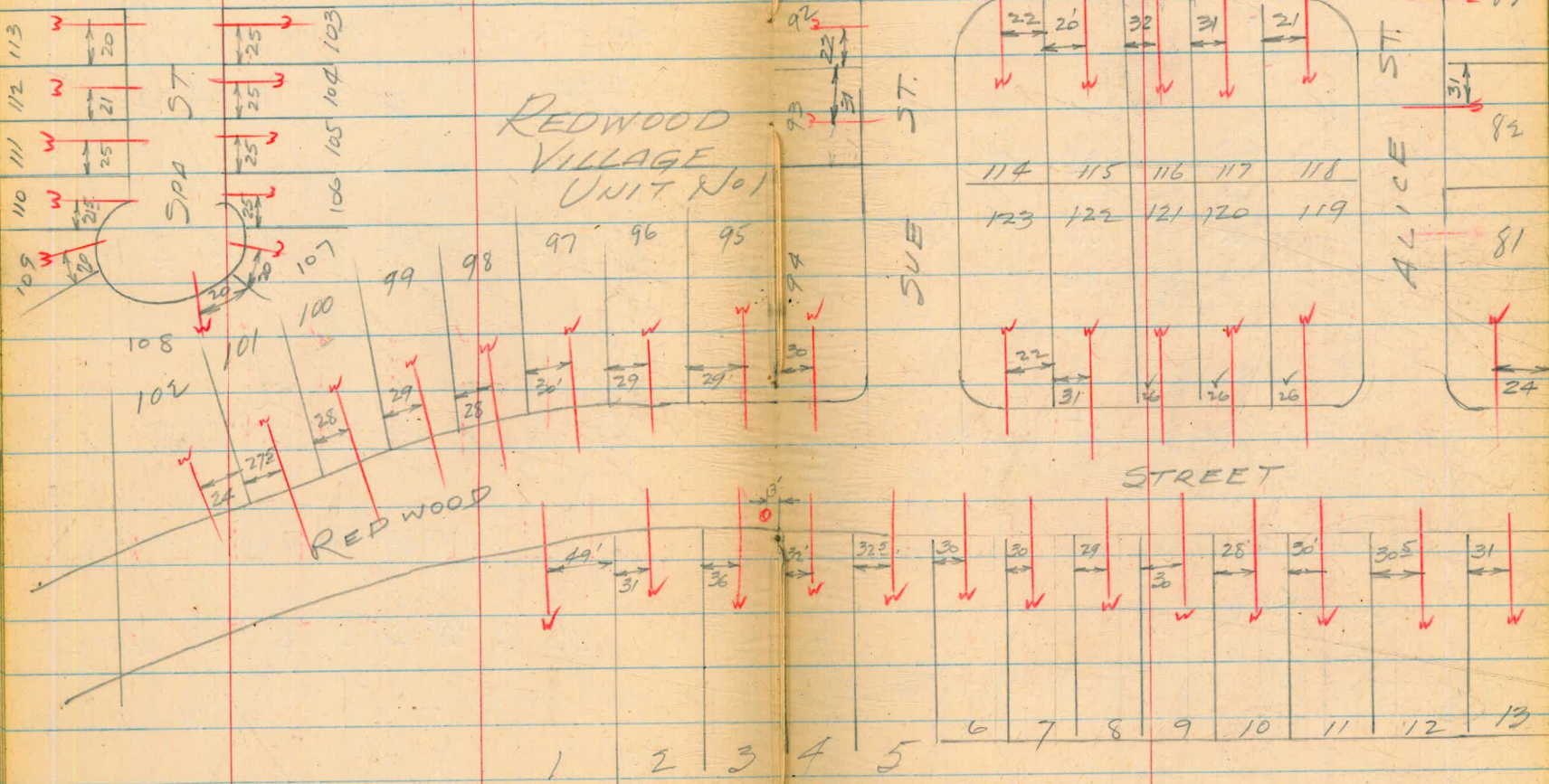
May 21, 1951

BEATTY.
LEONARD.
NELSON.

LOCATION OF WATER METERS

IN REDWOOD VILLAGE UNIT No. 1

PLAN 8297-L Sheet 7



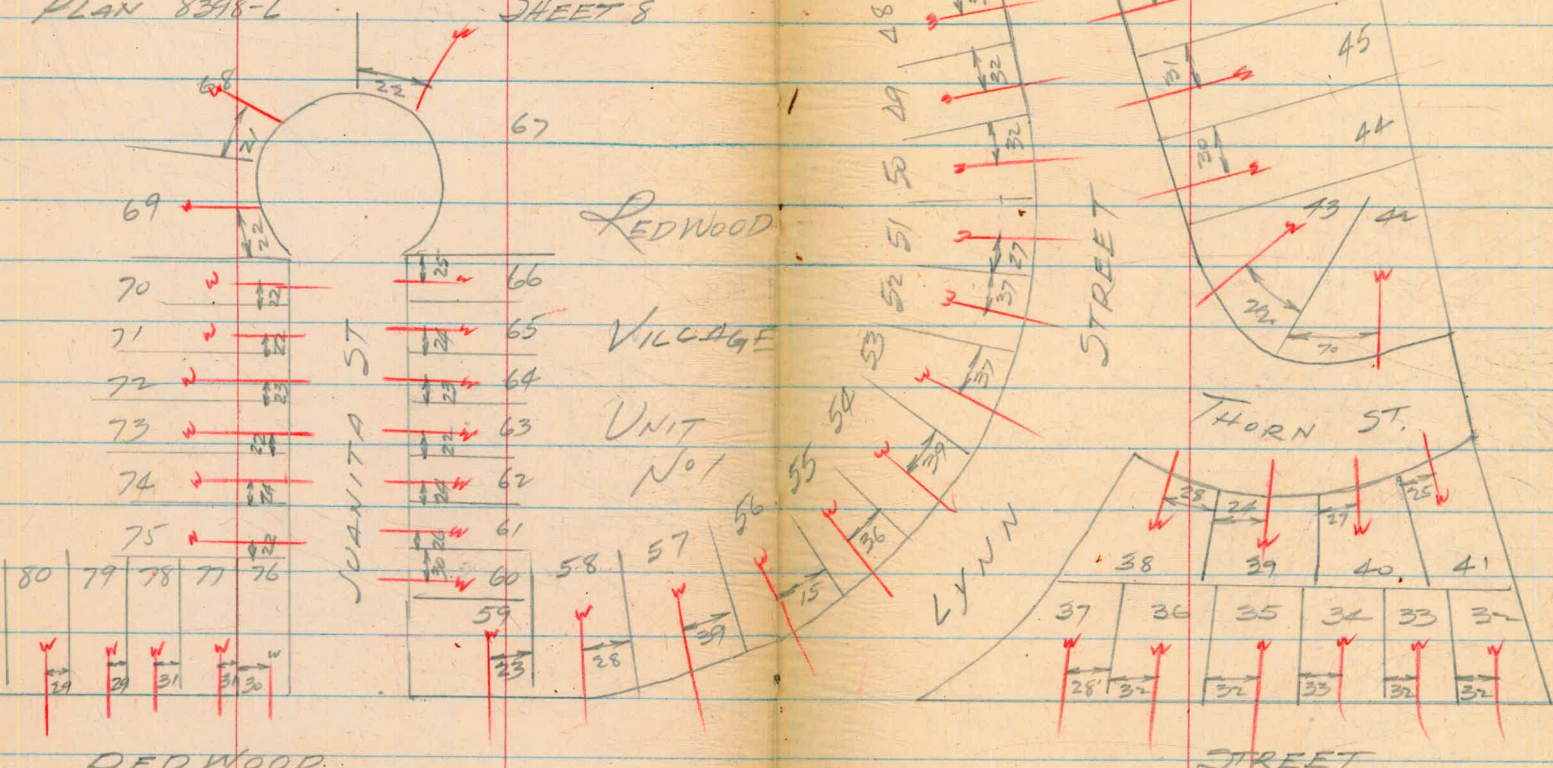
MAY 2/ 1951
SAME PARTY

6

LOCATION OF WATER METERS IN REDWOOD VILLAGE

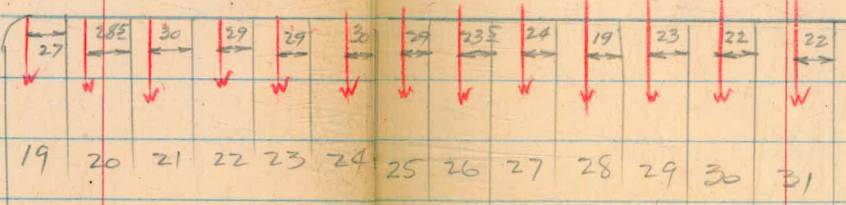
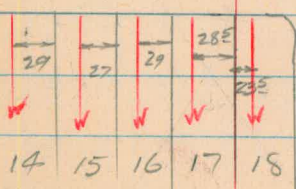
PLAN 8398-L

SHEET 8



REDWOOD STREET

REDWOOD STREET

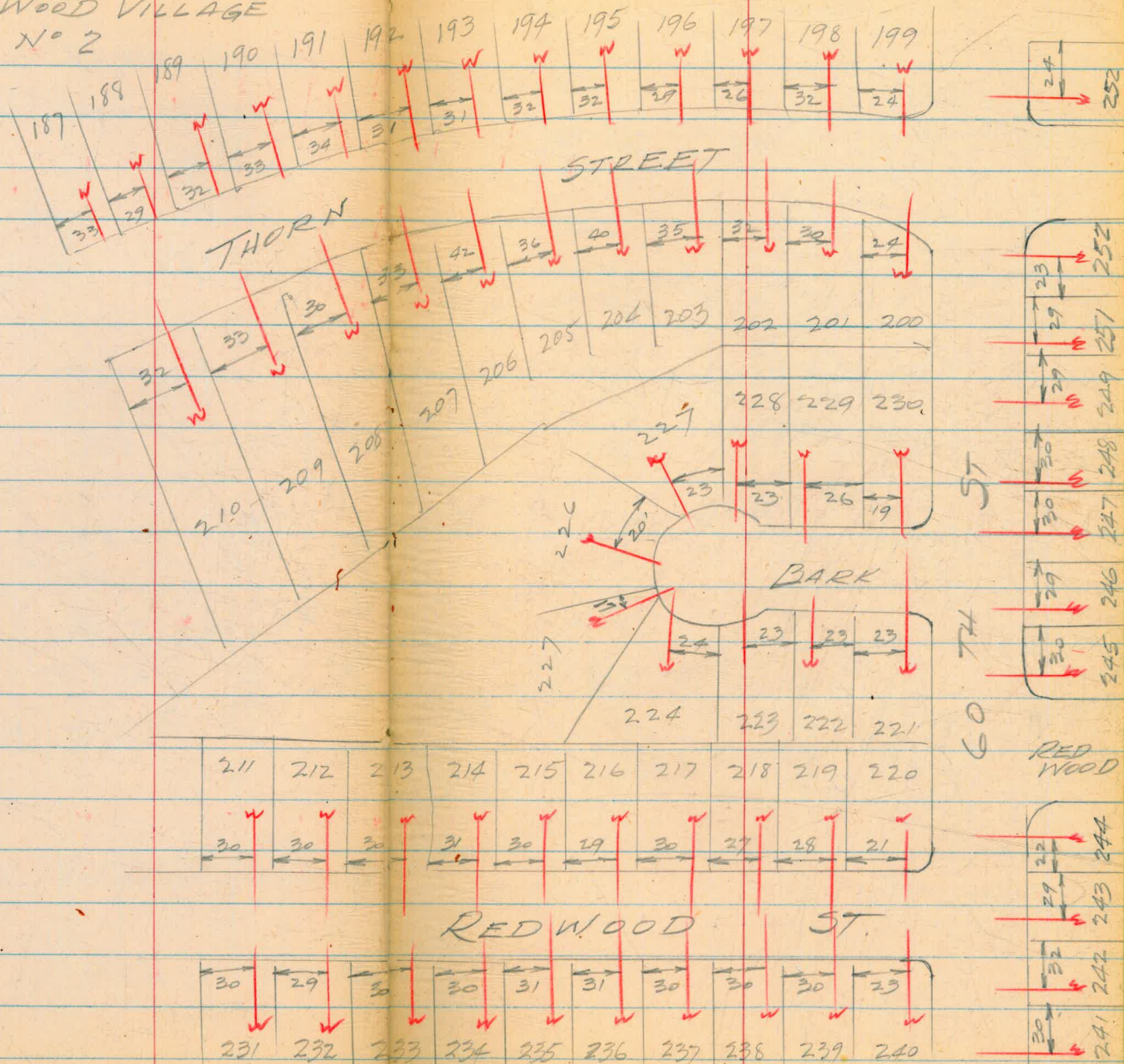


LOCATION OF WATER METERS
IN REDWOOD VILLAGE
UNIT N° 2

MAY 21 1951
SAME PARTY

PLAN 8483-L

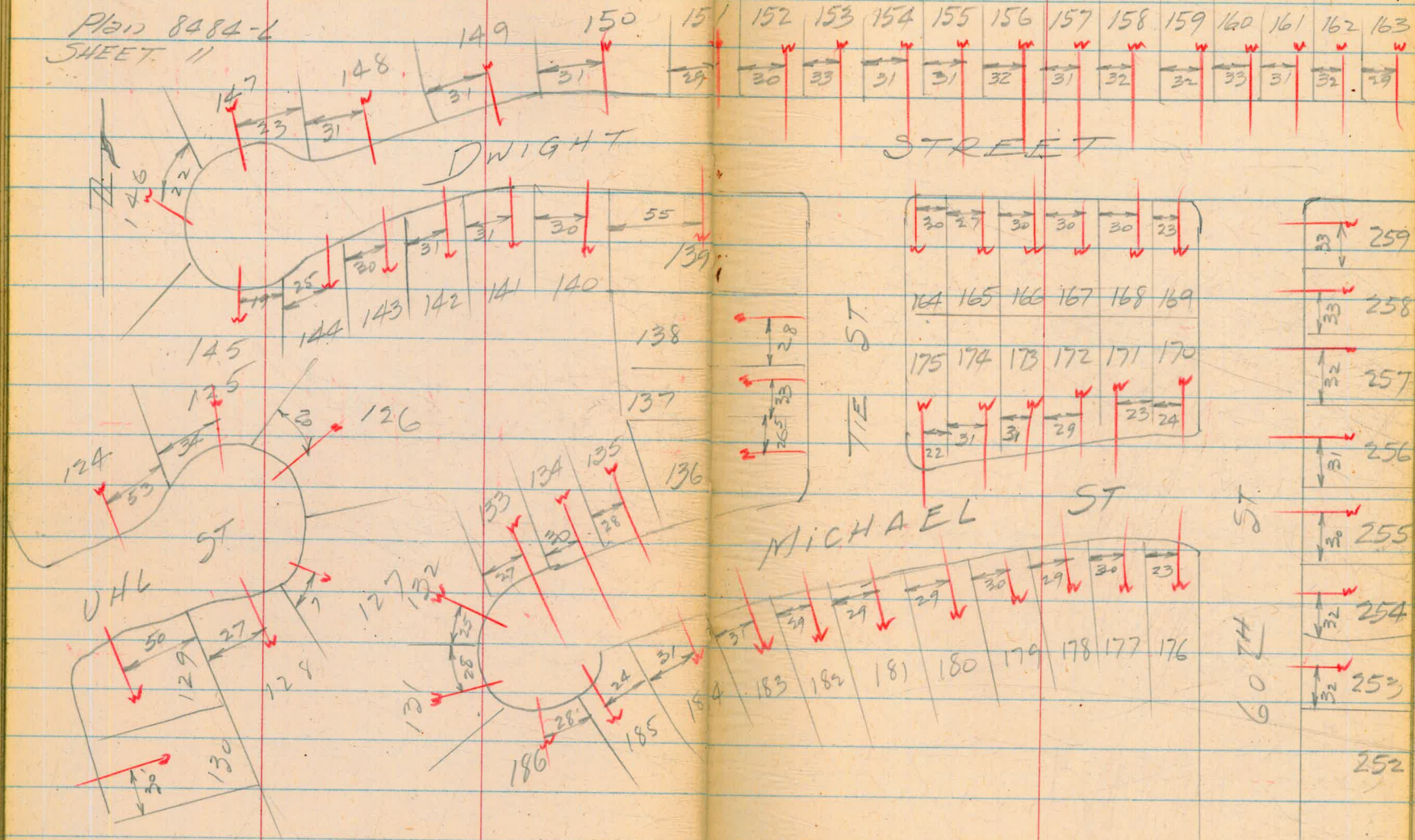
SHEET N° 10



LOCATION OF WATER METERS
REDWOOD VILLAGE
UNIT No 2

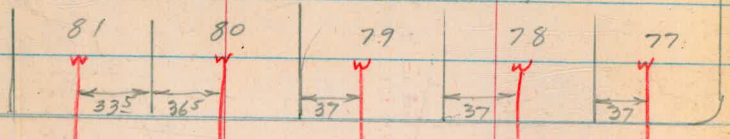
May 21, 1951
Same Party

Plan 8484-1
SHEET 11

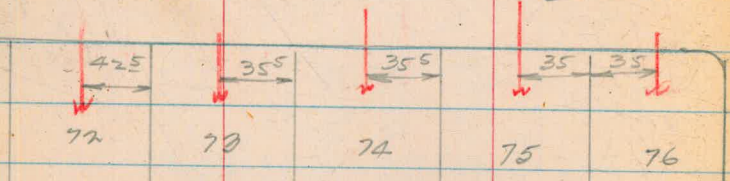


LOCATION OF WATER METERS
IN WOODLAND TERRACE
UNIT No 1

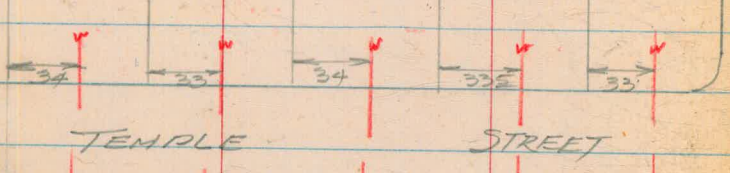
PLAN 8063-6 SHEET 9



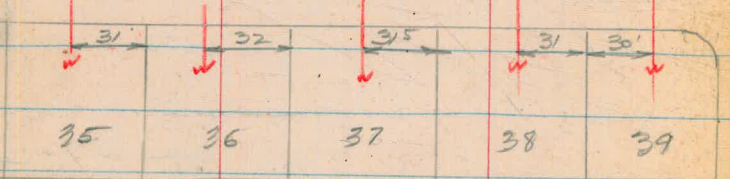
TARENTO DRIVE



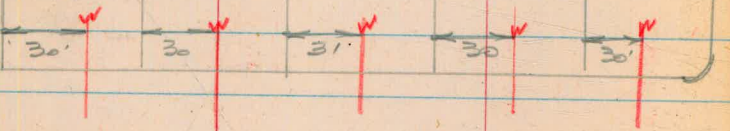
TEMPLE STREET



TEMPLE STREET



30 29 28 27 26

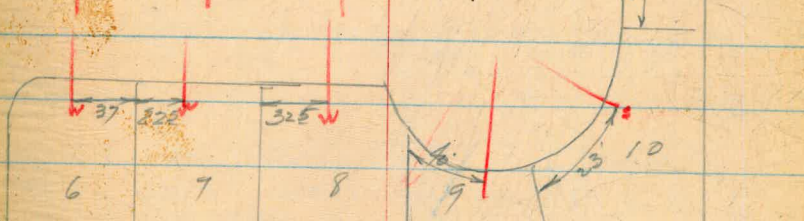
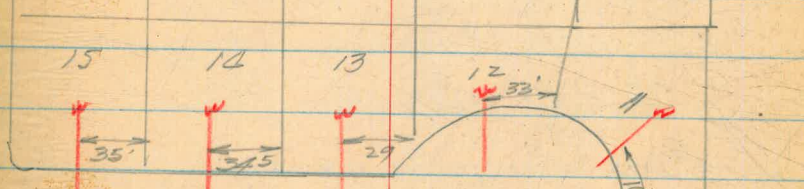
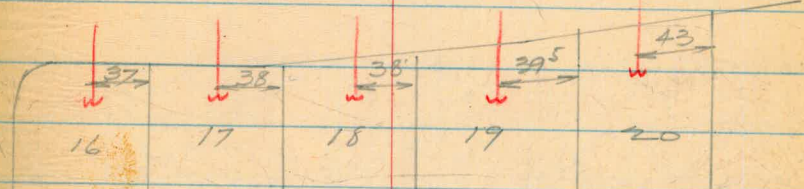
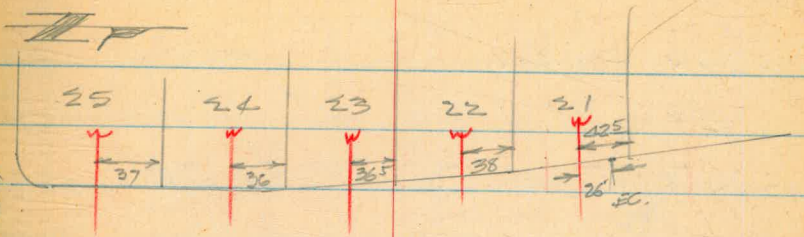


GATALINA BLVD

MAY 22, 1951

BEATTY
LEONARD

9.



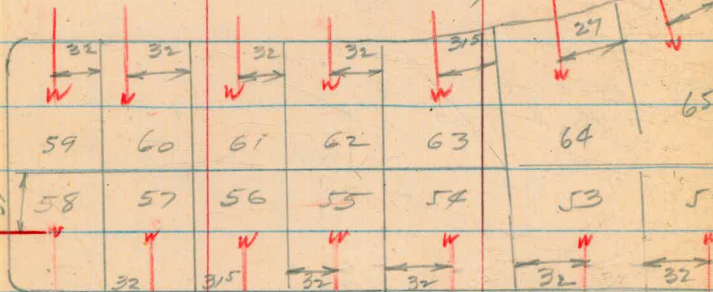
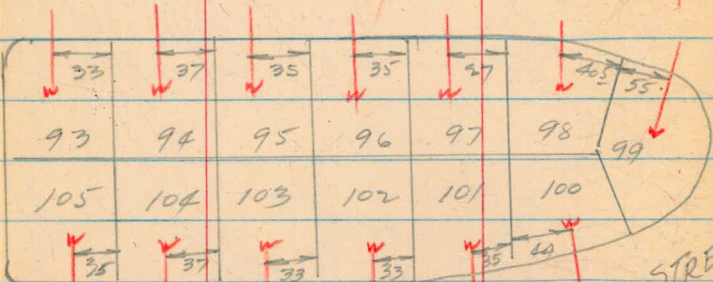
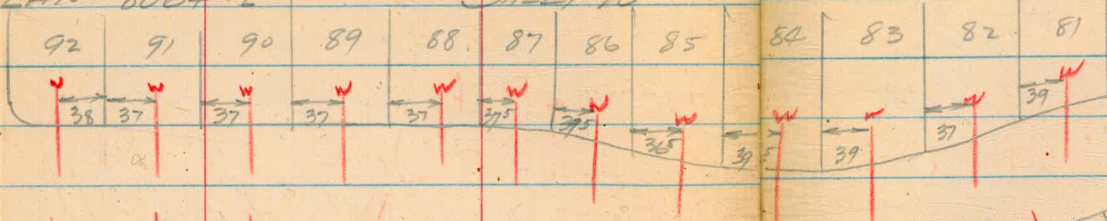
LOCATION OF WATER METERS
IN WOODLAND TERRACE
UNIT N° 1

May 23 1951
BEATTY
LEONARD

10

PLAN 8064-L

SHEET 10



SAVOY

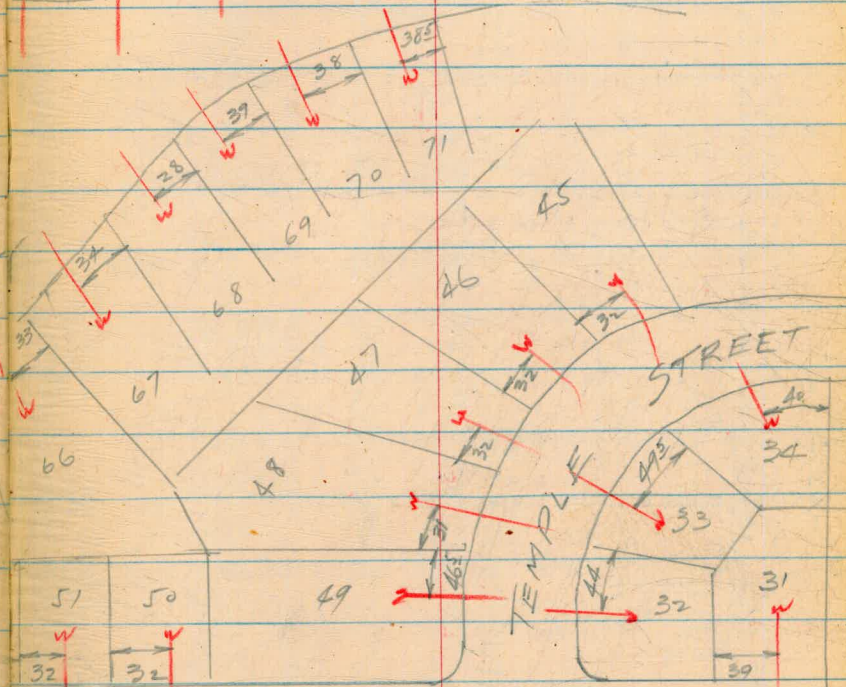
STREET

STREET

TEMPLE

CATALINA

STREET



LOCATION - WATER METERS
IN
MEDINA TERRACE

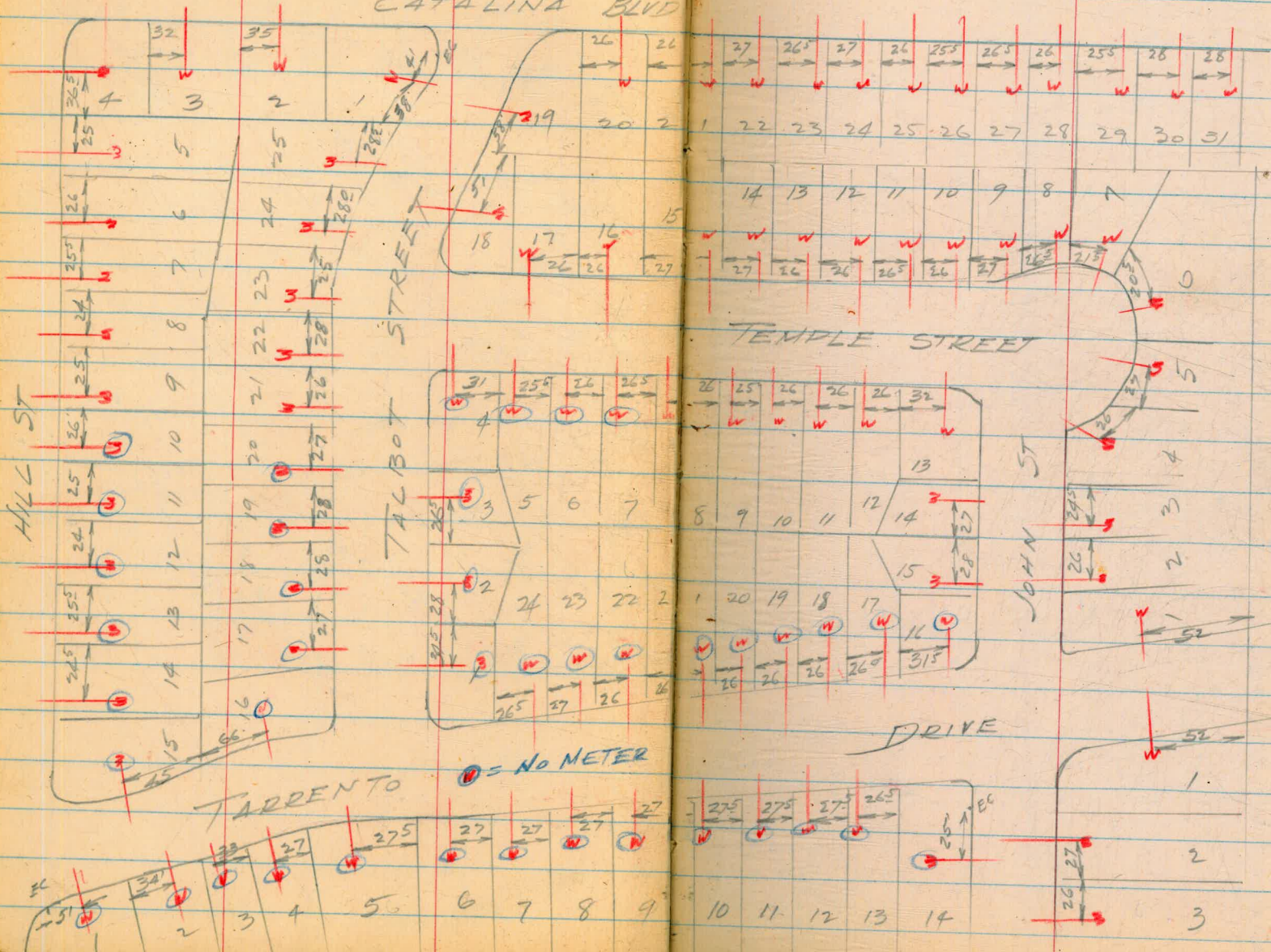
MAY 23 1951
BEATTY
LEONARD

11.

PLAN 8125-L

SHEET 6

CATALINA BLVD

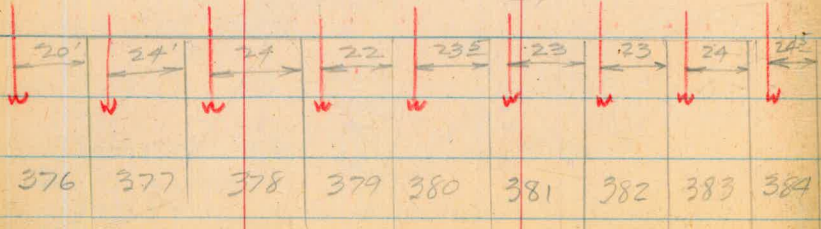
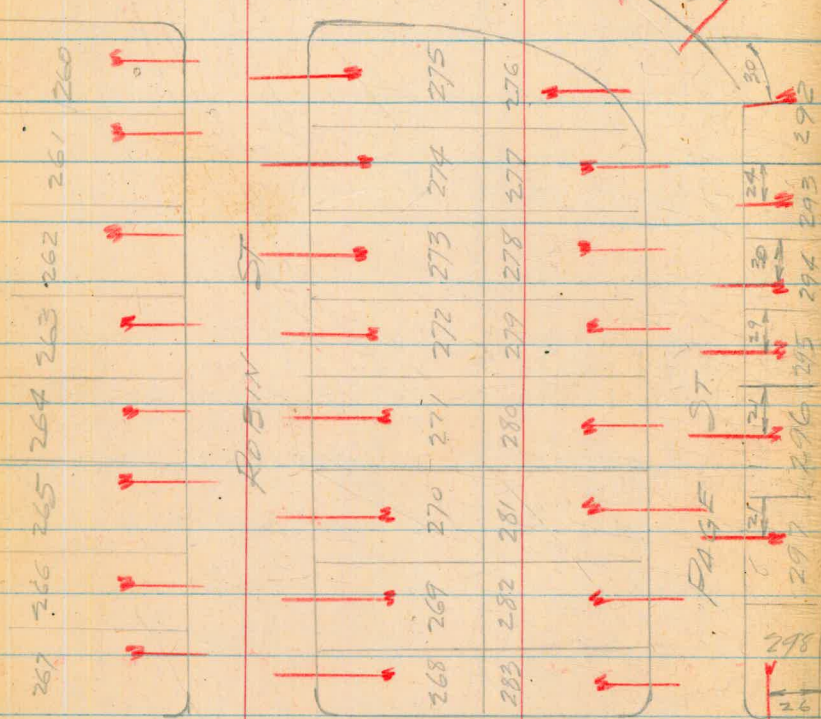


○ = NO METER

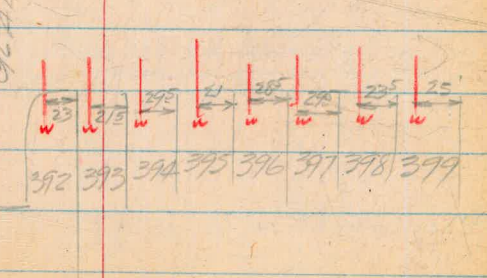
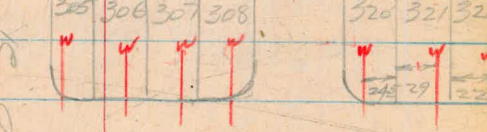
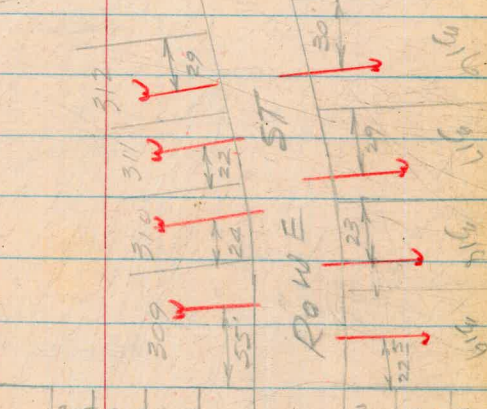
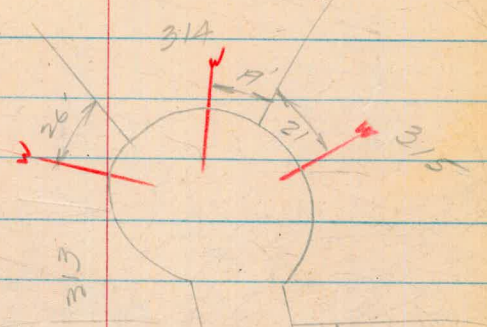
TARDENTO

LOCATION - WATER METERS
IN REDWOOD UNIT #3

PLAN 8693-L SHEET II



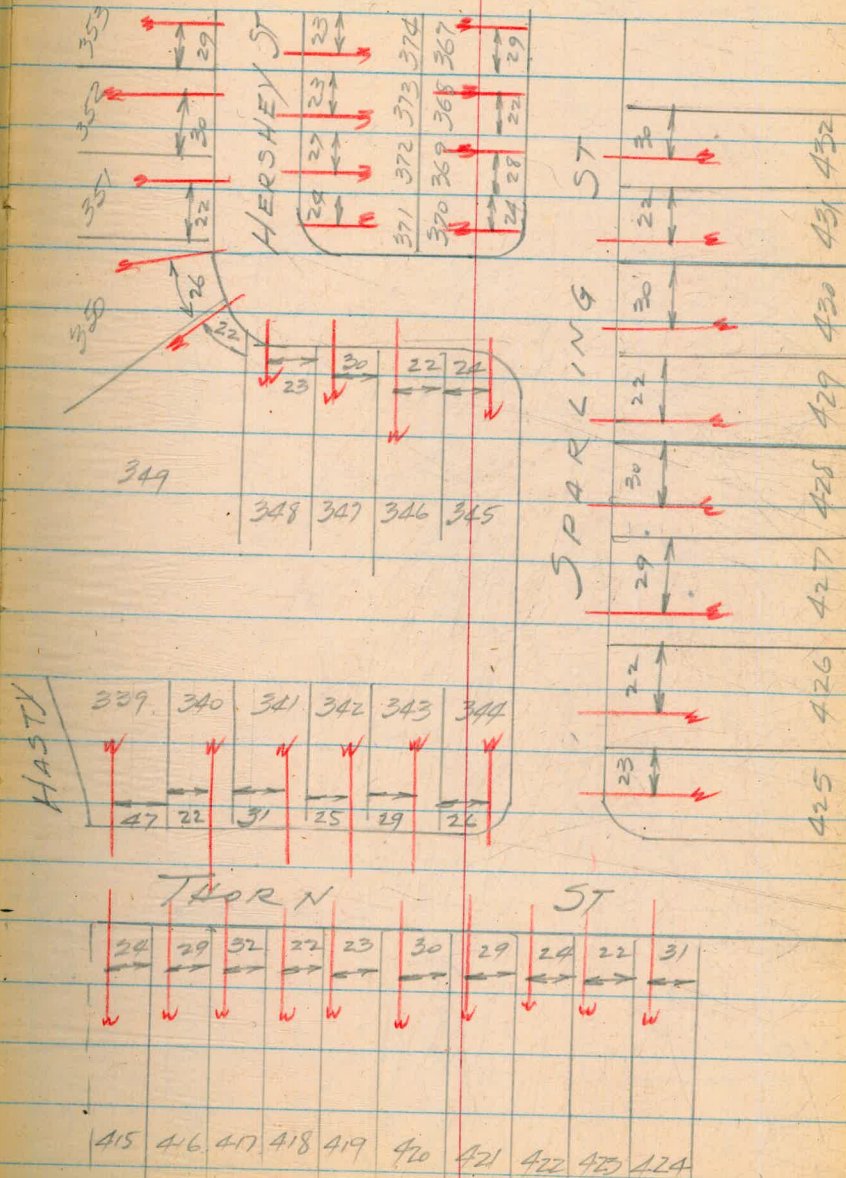
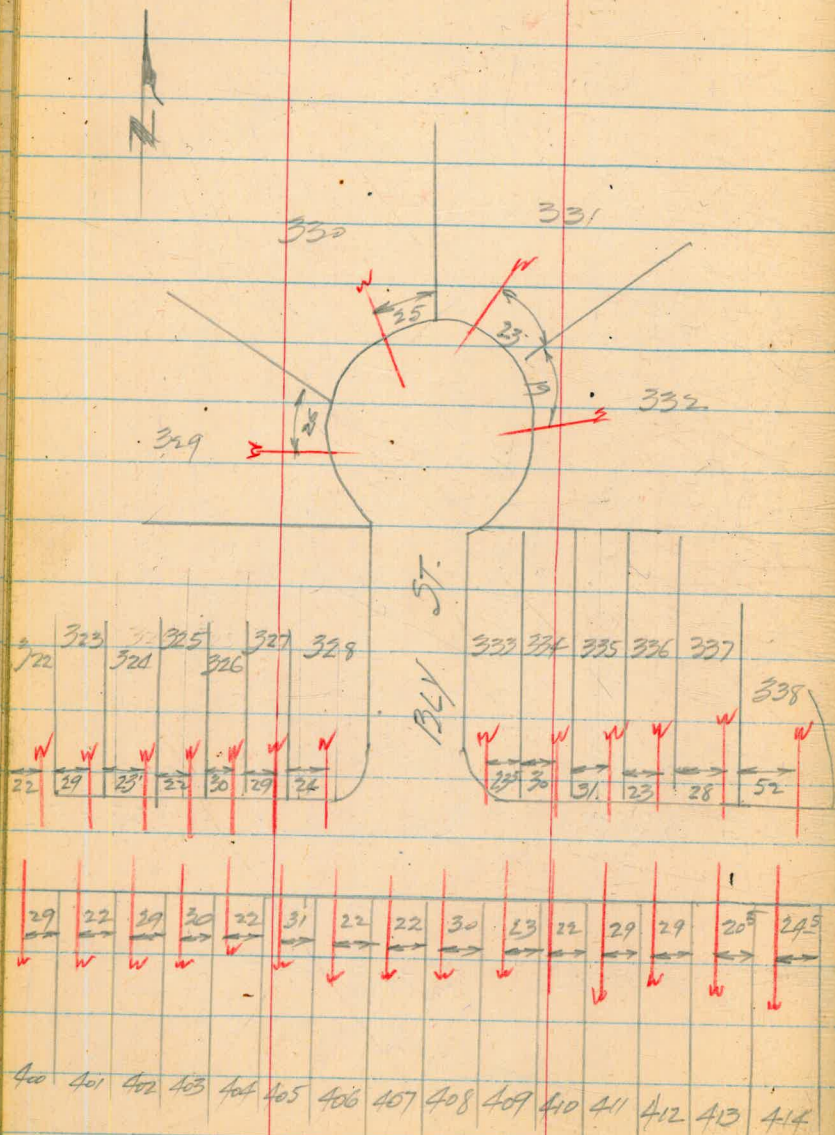
May 28, 1951
BETTY
LEONARD
Boyd 12



LOCATION - WATER METERS
IN REDWOOD VILLAGE #3
PLAN 8624-1 Sheet 12

May 28 1951

13

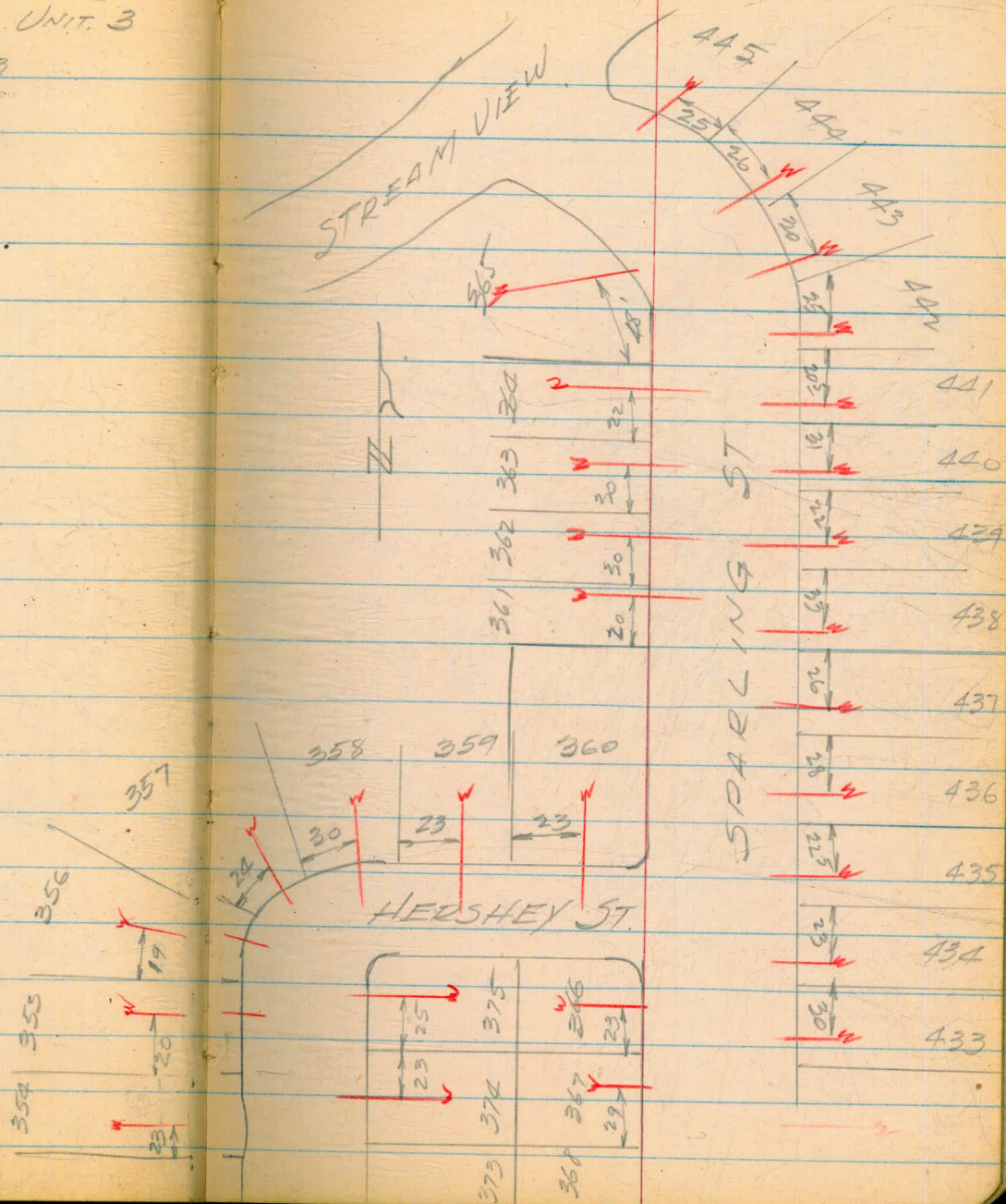


LOCATION - WATER METERS
RED WOOD VILLAGE UNIT 3

PLAN 8625-L SHEET 13

May 28 1951

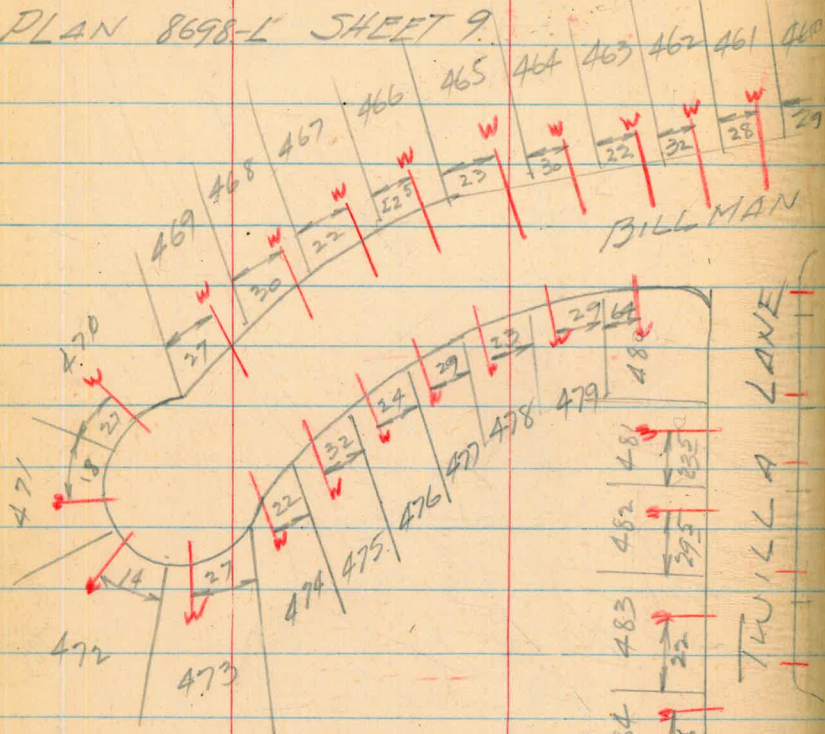
14.



May 28 1951

LOCATION - WATER METERS
REDWOOD VILLAGE
UNIT No 4

PLAN 8698-L SHEET 9



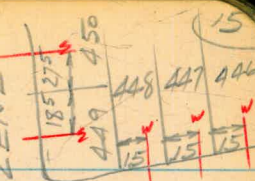
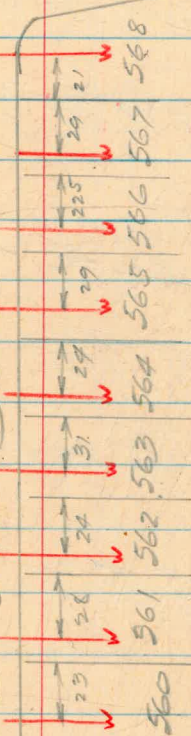
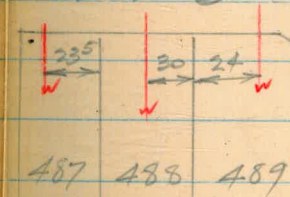
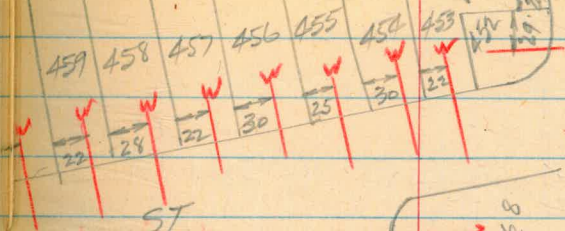
BILLMAN ST

TWILLA LAKE

ODOM ST.

NEW SOME DRIVE

ZEN 1



SERVICES ON COLLEGE AVE
NOT EXPOSED IF 1' IN
NO METERS OR CURBS YET

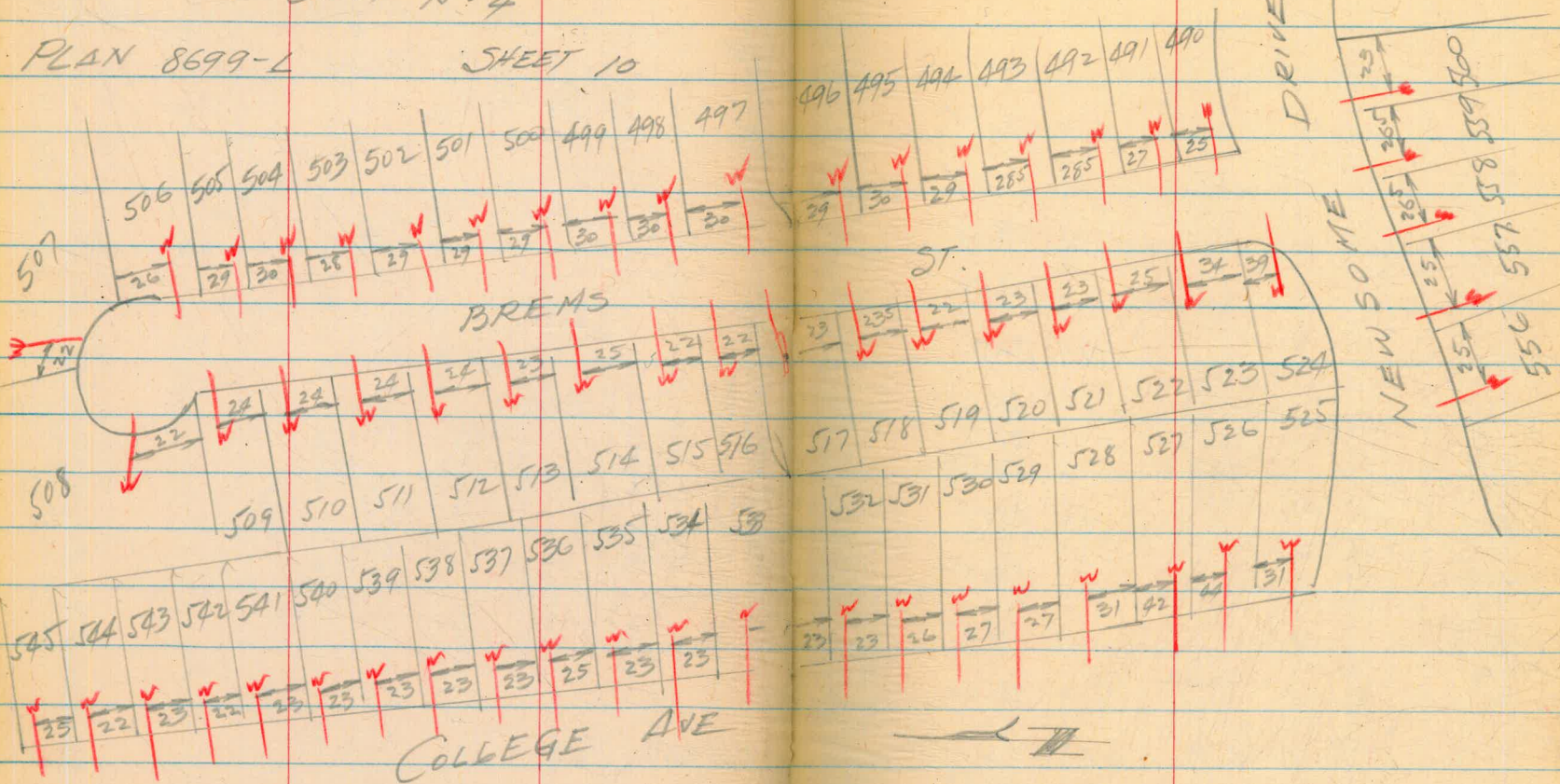
LOCATION - WATER METERS
 REDWOOD VILLAGE
 UNIT NO 4

MAY 28 1951

16

PLAN 8699-L

SHEET 10



Worked 182.
3-6-52

GERTRUDE ST
DORCAS to VIOLA
& PROFILE PROPOSED 6" WATER
E = 10'

B.M.	9.97	26.16 ✓	16.19
P	10.58	36.61 ✓	0.13 26.03 ✓
SET TOM		2.76	33.85 ✓
0+00		7.0	29.61
+13		7.1	29.51
+19		5.7	30.91
+50		6.0	30.61
+95		Rim 5.42	31.19
		Inv. 12.63	23.98
1+00		5.1	31.51
+50		4.1	32.51
2+00		2.6	34.01
+50		0.9	35.71
P	8.54	44.92 ✓	0.23 36.38 ✓
		Rim 7.33	37.59
2+95		Inv. 14.88	30.04
3+00		7.3	37.62
+50		5.2	39.72
4+00		3.0	41.92
+45		0.6	44.32
4+51		0.8	44.12
SET TOM		4.93	39.99 ✓

FEB. 20 1952

17.

CONC MON SW COR Naples & Dorcas

NW Cor End curb, E side Driveway 50' E 0+25

& Dorcas & C of W.V. on 8" A.C.
1/2 35' RT W.V. on 8" A.C.
Edge road; 40' LT WAT MET

0+87 7" RT WAT MET

SEW. M.H. 10' LT, 26" LT WAT MET

1+08 7' RT Po Pole

1+05 Gas Ser. Xing

1+46 25" LT WAT MET

1+74 6" RT WAT MET

2+02 Gas Ser. Xing

2+25 5" RT WAT MET

2+06 } 4' RT MAIL BOXES
2+07 }

2+41 - 7' RT Guy Aric.

2+58 - 7' RT Po. Pole

2+615 7" RT WAT MET

3+05 Gas Xing

10' LT SEW. M.H.

3+41 6' RT MAIL BOX

3+60 Gas Xing

3+70 8" RT WAT MET

3+83' 7' RT Po. Pole

4+09 7' RT Guy Aric.

CONC MON SW COR GERTRUDE & Viola.

worked 554
3-6-52

GERTRUDE ST
VIOLA TO LILLIAN
& PROFILE PROPOSED 6" WATER
& = 10' Easterly & ST.

44.92

0+25		13.2	31.72
0+25		Rim 12.01	30.91
+36		Inv. 22.81	22.11
		13.5	31.42
+50		12.6	32.32
1+00		9.9	35.02
+50		5.6	39.32
2+00		3.4	41.52
P	11.28	55.31 ✓	0.89 44.03 ✓
+50		9.3	46.01
3+00		4.3	51.01
+50		1.7	53.61
+75		1.1	54.21
+73		Rim 1.21	54.10
		Inv. 11.21	44.10
4+00		0.4	54.91
P	7.47	62.65 ✓	0.13 55.18 ✓
+25		7.2	55.45
+50		6.7	55.95
+75		6.1	56.55
5+00		5.7	56.95
+25		5.4	57.25

2/20/52

18.

± Viola St
10' LT. SEW M.H.

Not prop line Viola W.V on &

0+77 & MAIL BOX
0+90 GAS SER XING

WAT. MET 2+91 7" RT
3+30 Gas Xing
3+22 Gas Xing

2+51 8' RT P. & TEL Pole
2+95 & MAIL BOX
3+38 6" RT WAT. MET
3+42 3" RT MAIL BOX
3+84 GAS XING
3+77 5" RT P. & TEL Pole

11' LT. SEW M.H.

4+12 6" RT WAT. MET
4+20 23" LT WAT. MET
4+29 6" RT MAIL BOX
4+35 5" RT WAT. MET
4+34 GAS XING
4+62 23" LT. WAT. MET

5+34 6" RT P. Pole

GERTRUDE ST
 VIOLA TO LILLIAN
 & PROFILE PROPOSED 6" WATER

2/20/50

19

	62.65		
5+50		44	58.25
+75		40	58.65
+87° EC		3.8	58.85
		lm 3.41	59.24
6+12°		124 11.86	50.79
	61.34		.38
SET TBM	0.96	2.27	60.25
	49.32		48.07
D	1.25	13.27	48.04
	36.31		35.95
P	0.36	13.37	35.92
	25.56		24.53
D	1.03	11.78	24.50
			16.18
CK BM		9.38	16.15 = 16.19

5+57 5° RT Guy Anchor

5+89 9° RT Po. Pole

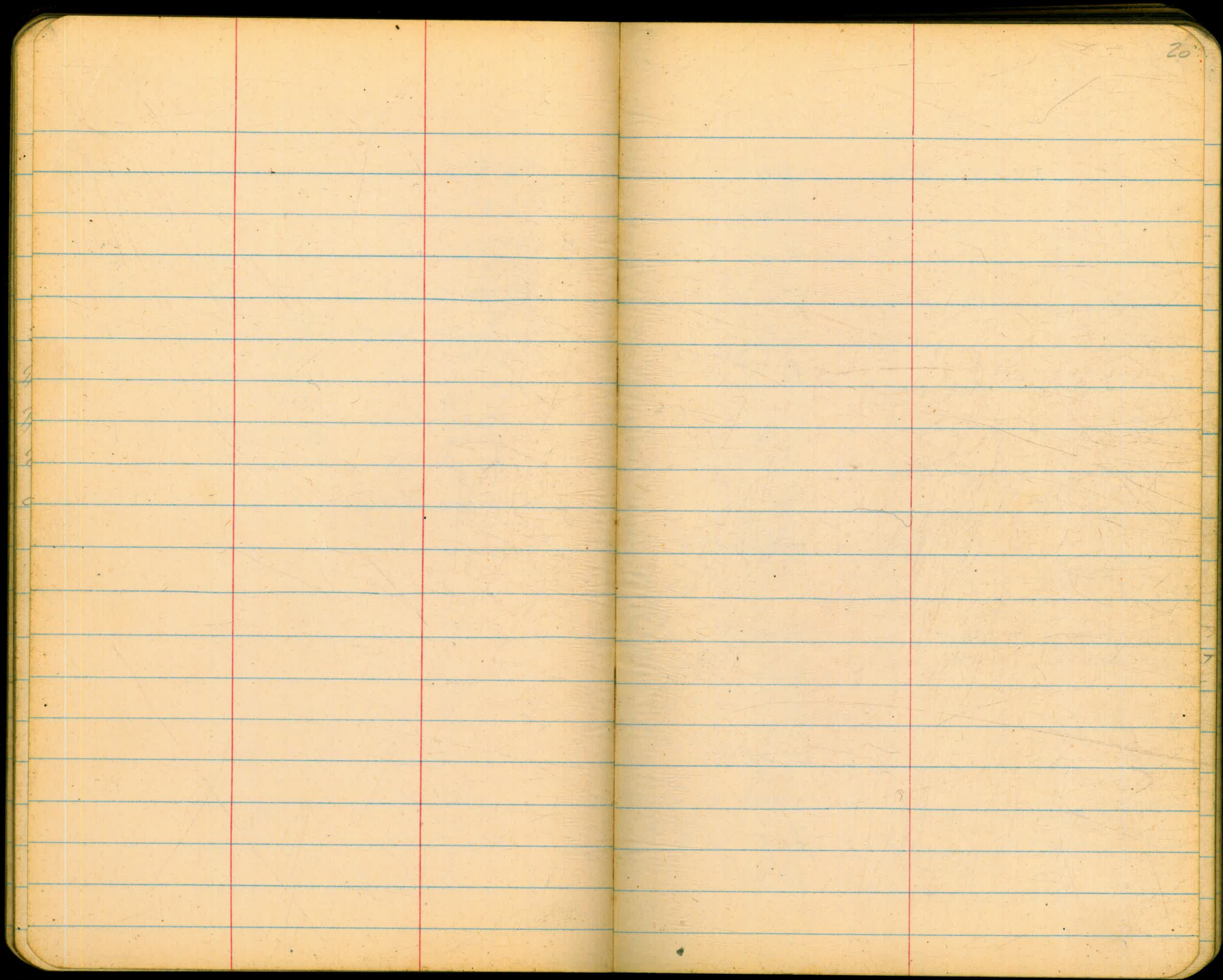
5+96 16° RT 2" FH.

10' LT SEW M.H.

30" I.P. SE

CORC MON NE Cor Gertrude & Lillian

CORC MON SW Cor Naples & Morena & Dorcas.



worked Met
3-6-52

ALLEY BIK 94
BETWEEN 39TH & 40TH ST.
FROM DWIGHT TO MYRTLE
& PROFILE PROPOSED 6" WATER

FEB. 21, 1952

BEATTY
POWELL
BERGER

21

B.M. 5.30 332.83 327.53

BR SW Cor 40TH & DWIGHT

0+00 5.0 327.83

So. prop. line DWIGHT

+50 5.4 327.43

0+21 3' LT. WAT MET

1+00 6.0 326.83

0+58 12' RT " "

+50 6.6 326.23

0+70 32' LT " "

2+00 7.6 325.23

1+42 32' LT " "

+50 8.6 324.23

1+65 20' LT " "

3+00 9.3 323.53

2+73 30' LT " "

+50 10.0 322.83

3+09 11' RT " "

Rm. 10.17 322.66

3+46 4' LT " "

10V 18.57 314.26

SEN MH 3+58 5' LT

4+00 11.5 321.33

3+74 11' RT " "

IP 0.47 321.91 11.39 321.44

4+20 2' LT

+50 2.1 319.81

4+45 13' RT 2-WAT MET

5+00 3.3 318.61

4+45 Gas Ser Xing LT

+50 5.0 316.91

4+71 30' LT WAT MET

5+99 7.2 314.71

5+23 13' RT " "

4) 13.24 7.17 314.21

5+32 30' LT " "

OK B.M. 0.43 321.48

Net. prop. line MYRTLE

5+63 } 30' LT " "

5+64 } " "

5+95 12' RT " "

5+96

BR SW Cor 40TH & MYRTLE

(318.18)

worked P&T
3-6-52
P&T

BETA ST
ALPHA TO 41ST
& PROFILE PROPOSED 6" WATER

2/28/52

BM	13.29	76.58 ✓	63.29
P	12.14	88.44 ✓	0.28 76.30 ✓
P	7.78	96.11 ✓	0.11 88.33 ✓
P	0.27	85.72 ✓	10.66 85.45 ✓
P	0.40	72.82 ✓	13.30 72.42 ✓
	1.87	62.36 ✓	12.33 60.49 ✓ = 60.53
0+00		1.7	60.66 !
+43		3.7	58.66
0+8381	X PT	33°37'45" RT	5.7 56.66
1+5042	X PT	33°37'45" RT	8.9 53.46
+74 ³⁰		10.3	52.06
+98 ⁶⁵ B.C.		11.6	50.76
P	1.97	52.68 ✓	11.65 50.71 ✓
2+05		2.6	50.08
+50		4.4	48.28
+85		5.7	46.98
3+00		6.7	45.98
+50 ¹⁰⁸ E.C.		8.7	43.98
+77 ⁰² B.C.		11.1	41.58

$\Delta = 24^{\circ}25'30"$
 $R = 310.$
 $T = 67.0$
 $L = 132.15$

BP NW Cor 40th & DELTA

CR P NAIL IN Pole (NOD LINE OF ALPHA WEST LINE 41ST)

E. Prop Line 41ST

0+57 }
0+58 } 17' RT 4" WAT. MET
0+59 }
0+60 }
0+60 WAT LINE 35' RT
0+66 } 42' LT. 2" WAT MET
0+67 }
0+80 145' RT 2" WAT
1+50 16° RT 2" WAT
1+78 WAT SET XING
1+78 435' LT. WAT. MET

3+70⁰⁰
1+98⁶⁵
31 03

3+07 21° RT WAT MET
3+29 GAS SET XING
4+31 38° LT. WAT. MET

BETA ST
ALPHA TO 41ST

± PROFILE PROPOSED 6" WATER

52.68

4+07⁸² (x PT 26°47'RT) 12.8 39.88

P 3.01 42.47 ✓ 13.22 39.46 ✓

4+50 4.0 38.47

Run 3.61 38.86
Inv. 8.73 33.74

SEW. M.H. 68 LT 4+50

4+90⁸¹ (x PT 26°47'RT) 5.2 37.27

5+20⁸¹ 6.2 36.27

5+75⁸¹ (Int. 6" WATER) 6.7 35.77
ALPHA ST

SET TBM 9.09 48.98 ✓ 2.58 39.89 ✓

P 12.10 60.98 ✓ 0.10 48.88 ✓

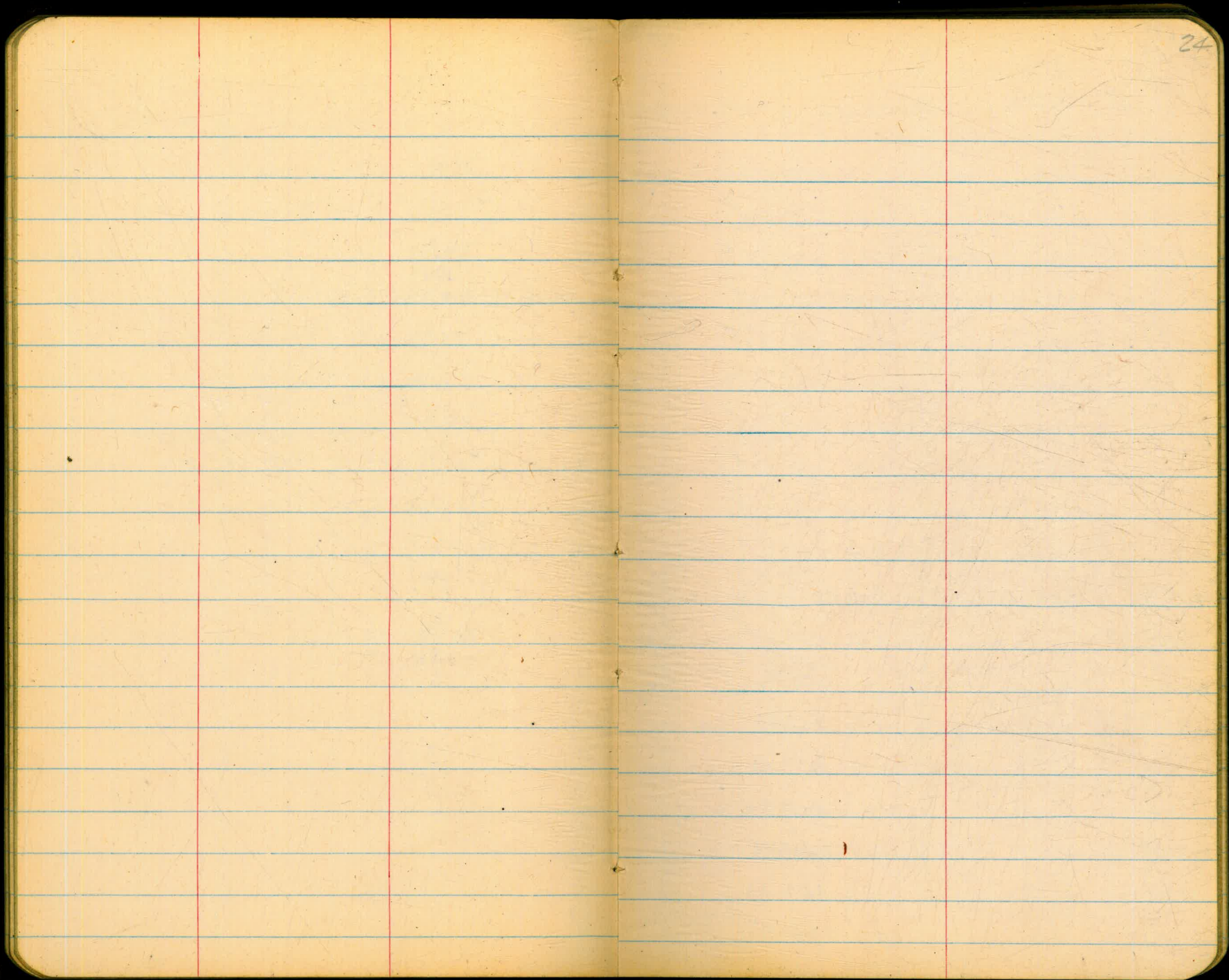
ck P 0.47 60.51 ✓ = 60.53 NAIL IN POLE

42.47

SEW. M.H. Run 6.90 54.08
9° RT 5+69 Inv. 11.95 49.03

5+19 10° RT FH
5+20 7° RT WV.

5+69 9° RT SEW M.H.
Top FH. 5+73 24° RT WV.



Worked 684.
3-16-52
Plotted 87.

BENSON ST.
WOODMAN TO 65TH ST
& PROFILE PROPOSED 6" WATER

FEB. 28, 1952

25

BM	0.60	480.31 ✓		479.71		BM □ NW Cor Val Box ENCANTO TANK
IP	0.56	268.06 ✓	12.81	467.50 ✓		
IP	0.06	454.90 ✓	13.22	454.84 ✓		
IP	0.87	442.70 ✓	13.07	441.83 ✓		
IP	0.54	430.26 ✓	12.98	429.72 ✓		
IP	0.39	417.38 ✓	13.27	416.99 ✓		
IP	0.14	404.32 ✓	13.20	404.18 ✓		
IP	0.15	391.13 ✓	13.24	390.98 ✓		
IP	0.22	378.48 ✓	12.87	378.26 ✓		
IP	0.70	365.84 ✓	13.34	365.12 ✓	(v)	
SET. TBM	0.43	359.39 ✓	6.88	359.25 ✓	Corr. Elev	Top FH SW Cor BENSON & WOODMAN
CK BM			7.41	351.98 ✓	= 352.27	SW Cor (Nail in Lead) Valve Chamber NE { BENSON WOODMAN
TBM	9.03	368.28 ✓ 367.99 ✓		359.25 ✓ 358.96 ✓	Corrected Elev	FH
0+00			9.45	358.83		on A.C.
+30			11.15	357.13		on A.C.
+53			12.45	355.83		Edge A.C.
+60			13.1	355.18		20' LT. To prop. Cor SW Cor Woodman, BENSON
1+00			14.6	353.68		
+50			14.4	353.88		

BENSON ST.
WOODMAN TO 65TH
E PROFILE PROPOSED 6" WATER

MAR. 3 1952

26

		367.99 368.28		
1+00			14.3	353.98
2+00			11.5	356.5 ^{.78}
+25 +50			6.7	361.58
+50 +75			3.4	364.88
+75 +100			0.5	367.78
R	11.02	378.96 [✓] 378.67	0.34	367.94 [✓] 367.65
3+25 +50			6.4	372.56
3+75 +100			4.4	374.56
4+25 +50			3.0	375.96
+60 +85	E 66th		2.2	376.76
4+75 +100			1.9	377.06
R	1.90	378.70 [✓] 378.41	2.16	376.80 [✓] 376.51
5+25 +50			1.3	377.4
5+75 +100			1.5	377.2
6+25 +50			2.3	376.40
6+75 +100			4.4	374.30
7+25 +50			6.5	372.20
7+75 +100			9.1	369.60
8+25 +50			11.8	366.90

2" WAT. ON E

BENSON ST
WOODMAN TO 65TH
& PROFILE PROPOSED 6" WATER

MAR. 5 1952

27

8+75		378.41		
9+00		378.70	14.5	364.20
8+94			14.9	363.80
9+19			14.8	363.90
9+02				366.21 ✓
SET TBM			12.49	365.92
P	2.22	367.67 ✓		365.45 ✓
		367.38	13.25	365.16
CK TBM			8.42	359.25 ✓
				358.96
				359.25
BM	0.02	358.98		358.96
TP	0.00	345.76	13.22	345.76
TP	0.01	332.69	13.08	332.68
TP	0.06	319.53	13.22	319.47
TP	0.33	306.56	13.30	306.23
TP	0.09	293.56	13.09	293.47
TP	0.64	281.05	13.15	280.41
CK BM			6.85	274.20 = 274.45
				274.49

at G.V. 10' E & 65TH ST.

& 65TH ST.

NAIL IN POLE SW COR. 65TH & BENSON ✓

TOP P.H. SW COR. BENSON & WOODMAN

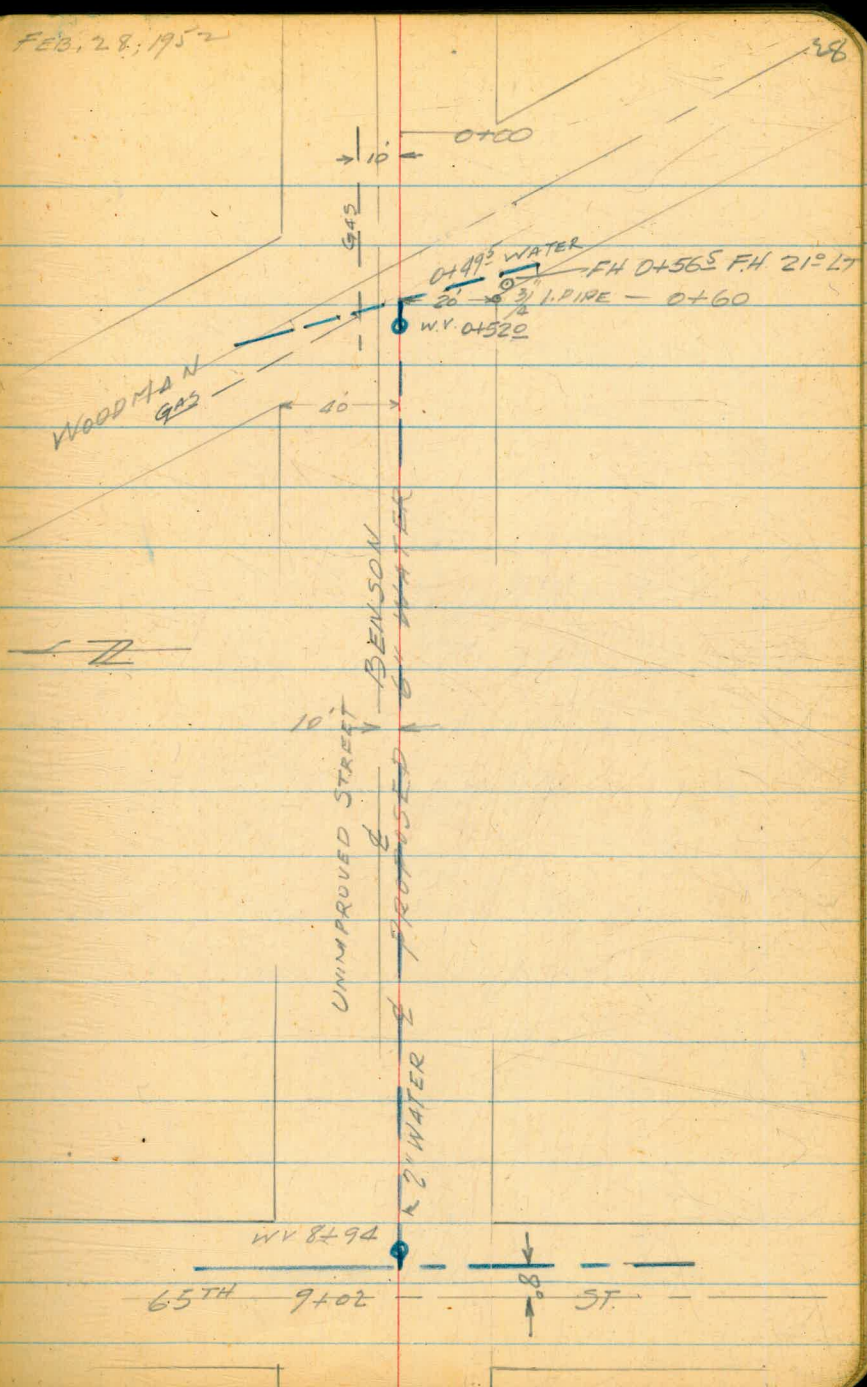
3 MEN FH BENSON & WOODMAN

NAIL IN PO. POLE SW COR. MADRONE & WOODMAN

BENSON ST
WOODMAN TO 65TH

FEB. 28, 1952

28



P.L. LOT 1202
 & PROPOSED WATER LINE

30+98⁰² Intersection P.L.

1214	1215
1203	1202

29+60⁰² P.I. 1°01' RT

20+76¹⁰ Edge of A.C. Pavt

20+60⁴⁵ & Pavt

20+44¹⁰ Edge of A.C. Pavt.

20+05²⁸ E Prop line Linda Vista Rd (64°05' LT)

17+63¹⁸ W. Row Line State Hwy (73°22' LT)

16+98⁰ POT W. Edge Conc. part

16+18⁶⁹ POT E. Edge Conc. part

15+52⁶⁵ POT (33° E & H. To Row State Hwy)

14+75⁸⁸ P.I. 42°13'30" LT

12+81⁴¹ P.I. 56°48' LT

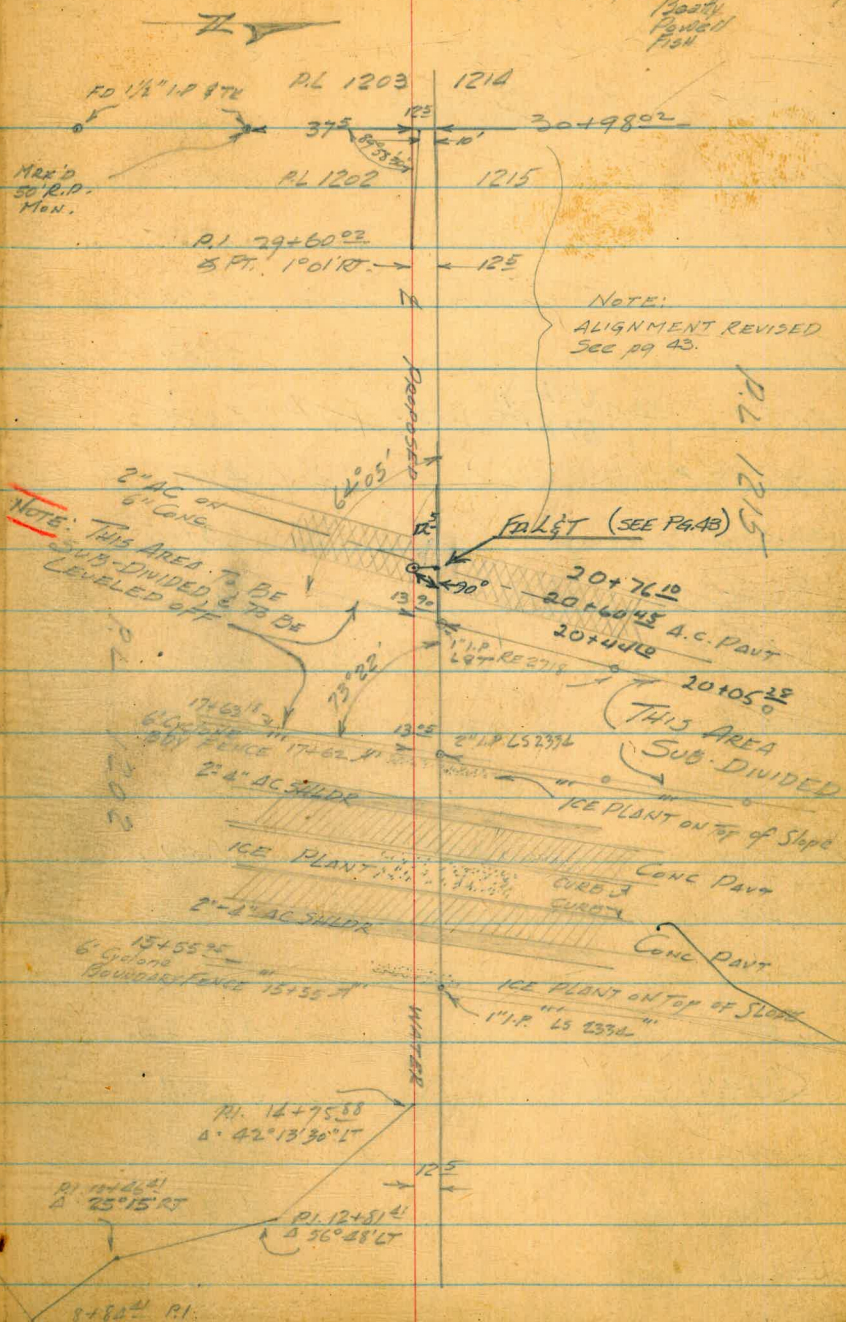
10+46⁴¹ P.I. 25°15' RT

8+84⁴¹ P.I. Existing 24" C.I. TEE

SEE
 FILE
 5358

Aug 2, 1952

Positively
 Found
 Fish



P.L. 1202
PROPOSED WATER
& Profile

8-5-52 BEATTY
TAVELL
FISH

30.

see pg 63 for staking

BM	5.65	457.47 ✓	451.82
11.2	0.85	452.90 ✓	5.42 452.05 ✓
14	0.52	440.38 ✓	13.06 439.84 ✓
11	0.79	427.88 ✓	13.29 427.09 ✓
8+82 ⁴¹		Should be 41 8+84 ⁴¹ Bob.C.	14.85 413.03
8+82 ⁴¹			6.4 421.5 ✓
9+00			6.4 421.5 ✓
7.50			8.6 419.3 ✓
10+00			9.6 418.3 ✓
+46 ⁴¹ ✗			9.7 418.2 ✓
11+00			12.0 415.9 ✓
11	11.32	426.01 ✓	13.19 414.69 ✓
+50			11.7 414.3 ✓
12+00			13.7 412.3 ✓
+50			15.7 410.3
+81 ⁴¹ ✗ PT			17.3 408.7
13+00			16.2 409.8
+50			12.2 413.8
14+00			7.7 418.3

00. FTG OF CHESTERTON TANK

Top of 24" C.I. TEE

Nat. Geo

TEE Appears to be
12' Eastly of FWD. TANG

6.33
8.62
14.85

30 + 9.8
428.2
22 16

8-5-52.

31

P.L. 1202

± Profile
Cont'd

426.01

14+50		2.0	424.0
TP	12.42	437.89 ✓	0.52 425.47 ✓
14+75 ⁸⁸	3 PT.	11.1	426.8
15+00		7.8	430.1
+32		3.0	434.9
+39		0.6	437.3
+52 ⁶⁵		0.21	437.68
TBM	1.90	439.17 ✓	0.62 437.27 ✓
15+62		0.9	438.3
TP	1.38	427.54 ✓	13.01 426.16 ✓
16+04		10.8	416.7
16+10 ³		10.55	416.99
16+18 ⁶⁹		10.03	417.51
+44		9.79	417.75
+41 ⁵		9.28	418.26
+50		9.5	418.0
+72		9.28	418.26
+72 ⁵		9.77	417.77
16+98 ^e		9.98	417.56

1" LP 13' RT 15+55

Toe cut slope

E. Edge A.C. Slidr

E. Edge Conc. Pavt

Edge Conc. Pavt at curb line

Top Conc Curb

± Hwy 16+58²⁵

Top curb

Edge Conc pavt

W. Edge Conc Pavt

PL 1202

± Profile
Cont'd

427.54 ✓

17+06 10.37 417.17

W. Edge A.C. Shldr

+12 10.6 416.9

Top cut slope

P 11.81 439.10 ✓ 0.25 427.29 ✓

P 9.18 447.97 ✓ 0.31 438.79 ✓

17+54 2.9 445.1

TBM 0.80 446.20 ✓ 2.57 445.10 ✓

on 2" I.P. 13' RT 17+63

+63'8 1.0 445.2

18+00 6.3 439.9

+50 11.4 434.8

P 0.22 433.06 ✓ 13.36 432.80 ✓ (7)

19+00 3.5 432.6 429.6

+50 7.4 428.7 425.7

20+00 11.1 425.0 422.0

+05'28 11.3 424.8 421.8

+33 13.3 422.8 419.8

P 0.48 420.88 ✓ 17.66 420.40 ✓ (2)

+35 2.0 418.9

20+22'10 2.23 418.65

E Edge A.C. Pavt

+60'45 2.16 418.72

± A.C. Pavt

See pg. 63 for stationing
Dated 7/28/51

P.L. 1202
 ± Profile
 (Cont'd)

	420.88			
20+76 ¹⁰		2.95	417.93	W. Edge A.C. Pavt
21+00		4.2	416.7	
CK TBM		6.33	414.55 = 414.57	W. End of curb return, on Conc. Curb 40' LT 21+35±
+50		7.6	413.3	
22+00		11.1	409.8	
P	0.16	407.82 ✓	13.22	407.66 ✓
+50		2.2	405.6	
23+00		6.5	401.3	
+50		10.7	397.1	
24+00		13.2	394.6	
P	0.94	395.77 ✓	12.99	392.82 ✓
+50		3.0	392.8	
25+00		4.4	391.4	
+50		5.8	390.0	
26+00		7.2	388.6	
+50		8.9	386.9	
27+00		10.2	385.6	
+50		11.4	384.4	
28+00		12.3	383.5	

P.L. 1202
& Profile
(Cont'd)

	395.77	12.8	383.0
28+50			
IP	3.86	386.91 ✓	12.72 383.05 ✓
29+00		4.6	382.3
+50		5.1	381.8
+60 ⁰² X PT		5.1	381.8
30+00		5.2	381.7
+50		5.6	381.3
+98 ⁰²		6.9	380.0
SET TBM	11.30	393.60 ✓	4.61 382.30 ✓
IP	13.32	406.78 ✓	0.14 393.46 ✓
IP	11.82	417.10 ✓	1.50 405.28 ✓
CK TBM		2.54	414.56 ✓ = 414.57

on 1/4" I.P. 40' LT. 30+98⁰²

on curb return 40' t 21+35^t

Newton St See Page 42

Q Proposed Pl. Profile

From a point 331' west of the west line of 43rd
to the east Bdry of PL 1345

	1.92	67.50		
0+00			10.2	57.3
0+10 OK				58.4
0-12-			9.10	+10.1 to Flow Line
0+50			12.0	55.5
	14.9	56.91	12.19	55.32
1+00			4.6	52.2
+50			10.6	46.2
	16.0	45.36	12.55	44.26
2+00			6.5	39.3
+50			11.9	33.9
2+61.8			13.77	+11.1 to Flow Line
2+99	3.05	36.55	12.36	32.69
				33.50
3+00			6.5	30.0
+50			11.0	25.5
+61 ⁴²			12.0	24.5
	12.79	49.54	0.80	35.75
	12.21	58.58	2.17	46.37
	10.14	68.56	0.16	58.42
			2.98	65.58 = 65.57

West
Martell
Voronovski

Dec 15, 52 35

BM NE BP 43+Newton 65.58
331' West of the west Prop line 43rd St
Top south edge sewer MH 18R1

Top of Road out Bank

$$\begin{array}{r} 13.6 \\ 8.2 \\ \hline 5.9 \\ 12.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ 6.2 \\ \hline 11.9 \\ 8.2 \\ \hline \end{array}$$

End of Road out

Top South edge sewer MH

Newton St

36

Pueblo Lands City of San Diego

3+61-42

end of st Begin City lands

24" J.C. Sewer

2+51 ^{3"} end of 2" Main

2+64
25.5
39.0

2+97.24
25
22.44

28.50

0+00

= 331' West of the west line of 43rd St

See FB 853 Page #1 For

elevation to top of existing 6" Main

Ed 3rd Ave Cur
0+00 end of existing
6" Main begin 2" Main

Proposed Pl.

existing 2" Main
Newton St (Dist 50)

to 43rd St

3+00 10" Sewer Xing
OK

2+89.2 Sewer MH 10" R
OK

2+24 Wat Met 39 R

2+00 Wat Met 39 R

1+50 Wat Met 39 R

1+20 Wat Met 39 R

0+75 Wat Met 39 R

0+22 Wat Met 39 R

0+10 Sewer MH 10" R
OK

Ed 6" LIT NW 0-45

Q.P.L. Profile
Calle Aguadulce
Roanoke to Cumberland

	10.78	280.60		269.82
	7.10	286.26	1.44	279.16
	6.95	293.08	0.13	286.13
	9.20	289.73	12.55	280.53
	10.70	300.07	0.36	289.37
0+00			12.5	287.5
+50	BC		7.8	292.2
+59	TBM		7.95	292.12 ^{0.12} 296.12
1+00			3.3	296.7
	11.53	310.11	1.49	298.59
+50			9.3	300.8
2+00			5.2	304.9
+50			0.8	309.3
	11.59	321.42	0.28	309.83
3+00			8.4	313.0
+50			6.4	315.0
+54 ³⁰	IC		6.4	315.0
4+00			5.6	315.8
+50			5.0	316.4

West
Martell
Varenfakis

38

17 Dec 52

BM NW cor Winchester + Calle Suena 041617

Q Roanoke St

Top 3/4 1P 15' RT of 0+50

$\frac{2.6}{10.21}$ $\frac{5.3}{10.21}$

$\frac{5.5}{10.21}$ $\frac{5.8}{10.21}$

5+00	321.42	4.0	317.4
+50 th BL		4.6	317.8
6+00		5.0	316.4
+50		4.6	317.8
	8.43	326.09	3.77
7+00		7.8	318.2
+50		7.0	319.0
8+00		6.2	319.8
+50		6.6	319.4
9+00		7.8	318.2
+50		10.8	315.2
+70 th EC		12.2	313.8
	2.46	316.97	11.57
10+05 th = 0+00	coll. Tapon	6.1	308.8
+50		10.3	306.6
	1.23	305.27	12.93
11+00		3.4	301.8
+50		8.0	297.2
12+00		11.7	293.5

Top $\frac{3}{4}$ " IR 15' RT 9+70th

$\frac{5.7}{10.11}$ $\frac{3.7}{10.25}$

$\frac{5.3}{10.21}$ $\frac{6.1}{10.25}$

$\frac{7.7}{10.11}$ $\frac{5.3}{10.25}$

$\frac{8.7}{10.11}$ $\frac{6.8}{10.25}$

$\frac{10.8}{10.11}$ $\frac{9.6}{10.25}$

$\frac{6.2}{10.25}$
 $\frac{11.2}{6.25}$ $\frac{8.6}{10.25}$

2 Colla Agua dulce

Cont

40

12+50 305.27 13.1 292.1

12.7
80 RT

11.6
100 RT

1.50 293.83 12.94 292.33

+87 4.23 289.6

edge AC Pav

13+00 4.46 289.3

+15⁷⁶ 4.46 289.3

13+35 5.01 288.8

Gutter line

+36 4.75 289.0

Top rail Ob

+45⁷⁶ 5.2 288.6

North prop line Cumberland

5.38 286.43 12.78 281.05

8.37 278.06 =

278.15

abisel □

Sirena + Cumberland

Q P2 Profile
Calle Tocan

	5.43	319.94	314.51
0+00		9.1	
+50		7.0	
1+00		5.9	
+50		5.4	
2+00		4.9	
+40 ²⁵		6.7	
	5.43		314.51 - 314.51

West
Martell
Varonakis

16 Dec 52 41

TBM Top $\frac{3}{4}$ in. Sec Page 39

0+00 Calle Tocan = 10+05²⁵ Calle Agua dulce

9.0	5.5
10.1	10.0R
6.6	4.5
10.1	10.0R
5.8	4.0
10.2	10.0R
5.6	4.4
10.1	10.0R
7.5	6.0
10.1	10.0R

Prop Line

Newton St
 & Proposed P2. Profile

From a point 331' west of the west line
 of 4th St to the east Bdry of R. 15th

West
 Martell
 Varonakis

13 Jan 53

42

Sta	+	Hi	-	
	3.44	69.02		65.58
0+00			10.8	58.2
+50			12.4	56.6
	2.20	58.75	12.47	56.55
1+00			4.6	54.1
+50			9.1	47.6
	1.55	47.55	12.75	46.00
2+00			4.9	42.6
+50			10.9	36.6
	3.00	38.51	12.04	35.41 35.51
3+00			6.7	31.8
+50			10.8	27.7
+61 ⁴²			11.6	26.9
	12.57	50.27	0.71	37.80
	11.38	60.95	0.70	49.57
	8.35	68.89	0.51	60.44
			3.31	65.58 = 65.58

BM NE BP 43 & Newton

8.4 12.0
 8°11' 6°11'

10.8 5.2
 7° 5°11'

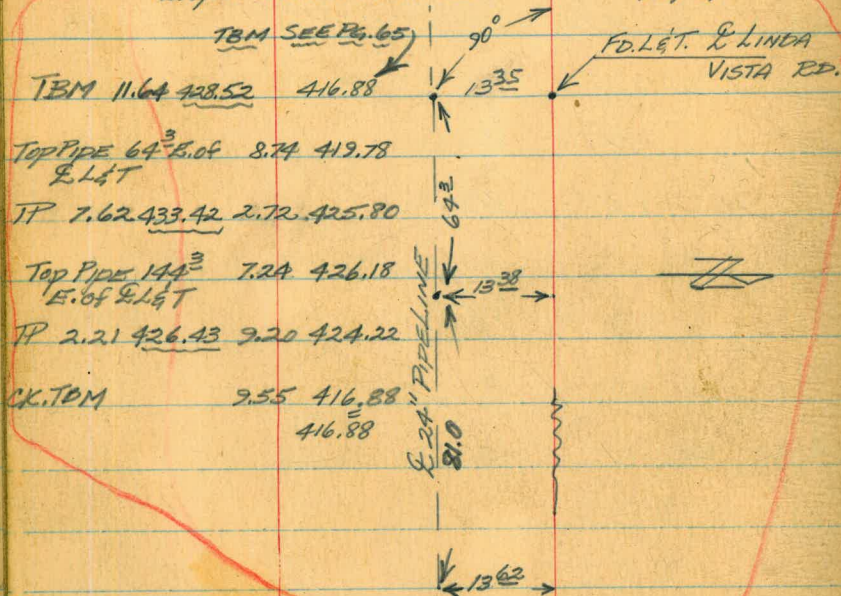
12 8.1 10.5
 10 8° 4°11'

6.3
 10°11'

BALTIC ST.
LINDA VISTA ROAD TO ATLAS ST.
PROPOSED 16" C.I. WATER
REVISED ALIGNMENT (See pg 29)

29+74.20 EXISTING TREE (?) (GV. 685 LT)
29+68.59 x PT 22 1/2° RT
29+05.88 x PT 22 1/2° LT

ELEVATIONS
NOTE: LOCATION OF 24" MAIN
ELY. OF LINDA VISTA RD. 4/3/57



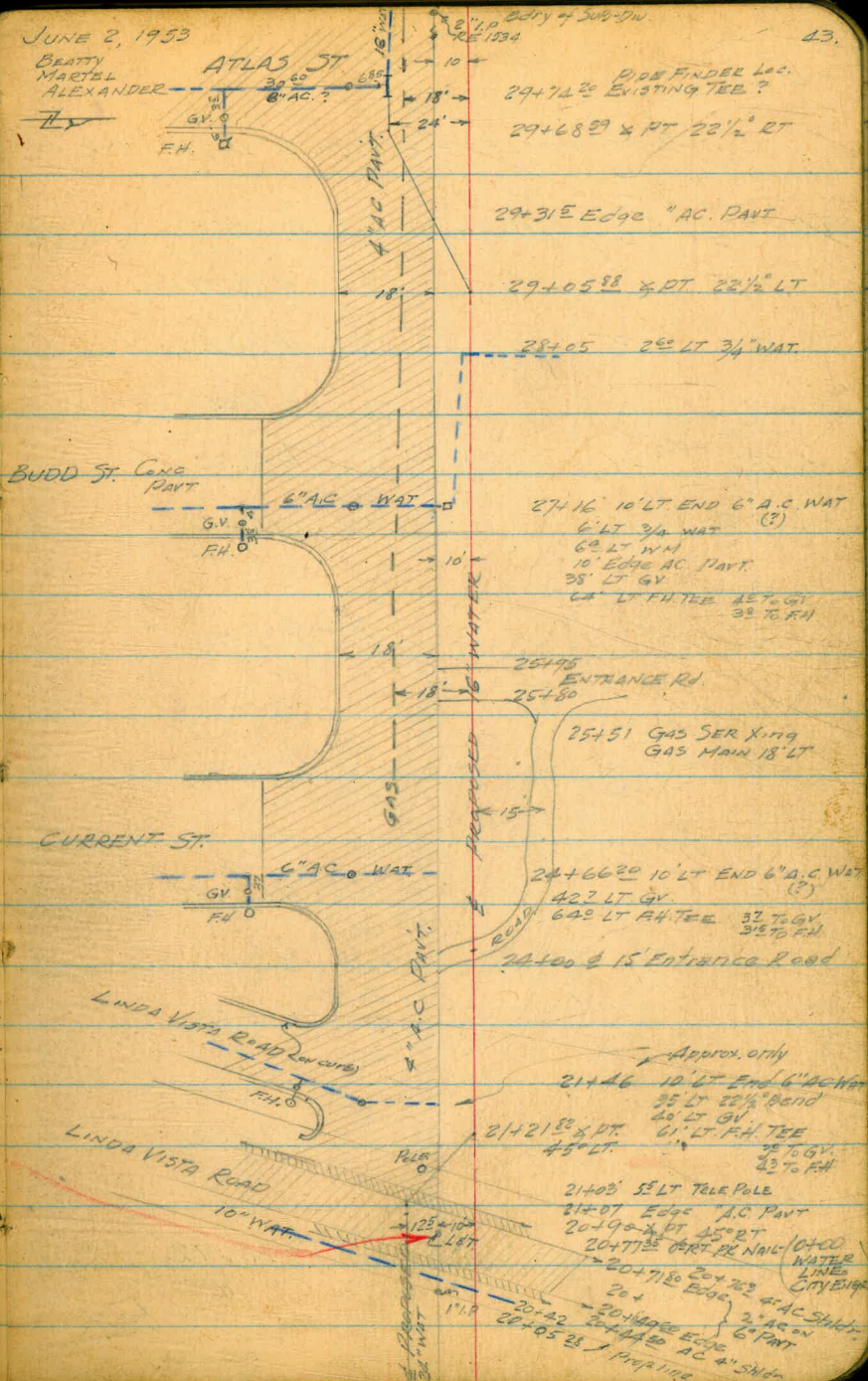
21+2182 x PT 45° LT

20+90 x PT 45° RT

20+0528 Ely Prop. Line Linda Vista Rd

JUNE 2, 1953

BRATTY
MARTEL
ALEXANDER



29+31E Edge "AC. PAVT

29+0588 x PT 22 1/2° LT

28+05 26° LT 3/4" WAT.

27+16 10' LT END 6" A.C. WAT
6' LT 3/4" WAT
60' LT W/M
10' Edge AC PAVT.
38' LT GV
60' LT FH TEE 45° GV
30' TO FH

25+95 ENTRANCE RD
25+80

25+51 GAS SER X-ING
GAS MAIN 18' LT

CURRENT ST.

24+6620 10' LT END 6" A.C. WAT
422' LT GV
640' LT FH TEE 32° GV
315° FH

24+00 @ 15' ENTRANCE ROAD

Approx. 0.7114
21+46 10' LT END 6" A.C. WAT
35' LT 22 1/2° BEND
60' LT GV
61' LT FH TEE
45° LT 35° GV
32° FH

21+03 35' LT TELE POLE
21+07 Edge "AC PAVT
20+90 x PT 45° RT
20+77E CRT. PL NAIL (OFCO)
20+71E Edge "AC PAVT
20+71E Edge "AC PAVT
20+71E Edge "AC PAVT
20+71E Edge "AC PAVT

20+42 20' WAT
20+0528 x Prop. Line

43.

BALTIC ST.
(Cont'd)
± PROFILE PROPOSED 16" WATER

STATION	PT	Distance	Elevation
20+77		4.65	419.22
20+77.35		1.25	417.97
20+90	X PT	1.50	417.72
21+07		1.37	417.85
21+14		1.7	417.52
21+21.82	X PT	4.2	415.02
21+50		6.5	412.72
22+00		10.2	409.02
22+50		13.4	405.82
23+00	P	0.30	406.72
23+00		4.7	402.02
23+50		9.2	397.52
24+00		9.8	396.92

W/4 E.C. CURB RET Linda Vista (access road)
(Pg. 33 this book)

on f.A.C Pavt

Edge 4' A.C Pavt

LT. Sky

RT. Nly.

417.47

(x-section 1/2
to Fwd. Tang.

17.5	2.0	4.2	6.0	6.3
10	6	5	5	15

Edge AC

416.02

3.2	2.2	6.5	8.5	8.9
10	6	5	5	15

Edge A.C.

411.67

7.5	7.5	10.2	13.0	13.3
10	6	5	9	15

Edge AC

407.55

11.67	11.8	13.4	16.5	16.6
10	6	5	7	15

Edge AC

403.30

3.22	3.3	4.7	6.3	6.4
10	5	5	5	15

Edge AC

399.60

7.12	7.1	9.2	9.6
10	5	5	15

Edge AC

396.37

± 15' Entrance Road

10.35	7.8	9.5
10	5	15

Edge AC

6/2/53

44

BALTIC ST
(Cont'd.)

6/2/53

25

	406.72		
24+50		9.7	397.02
24+66		5.6	401.12
25+00		8.7	398.02
P 0.02	399.18	7.56	399.16
25+50		1.7	397.48
25+75		2.8	396.38
25+80		6.0	393.18
25+95	Entrance Road	6.3	392.88
		4.2	394.98
25+97		4.2	394.98
26+00		7.4	395.78
26+50		5.4	393.78

394.27

12.45 92 97 8.5
10 4 0 15
Edge AC

393.77

12.95 10.0 6.4 5.6 6.4
10 9 3 0 15
Edge AC

394.07

Should be 392.5
Rob E.
See 9427-L

12.65 10.6 9.0 8.7 9.1
10 8 2 0 15
Edge AC

391.48

7.70 2.0 1.7 1.7
10 8 0 15
Edge AC

390.78

8.40 2.9 2.8 2.9
10 7 0 15
Edge AC

390.63

8.55 6.0 3.6
10 0 15
Edge AC

390.08

9.1 6.3 3.6
10 0 15
Edge AC

389.94

9.24 6.0 4.2 3.2
10 9 0 15
Edge AC

389.88

9.30 5.2 3.4 3.1
10 9 0 15
Edge AC

388.43

10.75 4.9 5.4 5.5
10 5 0 15
Edge AC

BALTIC ST
(Cont'd)

6/2/53

46

	399.18		
27+00		10.3	388.88
27+50		12.2	386.98
P	3.00	13.26	385.92
28+00		4.1	384.82
28+50		7.9	384.02
29+00		5.4	383.52
29+05.88 (X PT)		5.5	383.42
29+31.5 Edge AC Pavt		6.05	382.87
29+68.59 X PT		6.50	382.42
29+74.20 (TEE)		6.58	382.34
SET TBM.	6.26	391.38	3.80 385.12
P	11.97	403.15	0.20 391.18
P	12.61	415.56	0.20 402.95
CK TBM			0.96 414.60 = 414.57

386.83

12.35 10.8 10.3 10.7
10 7 8 15
Edge AC

386.50

12.60 12.2 12.1
10 2 15
Edge AC

384.32

4.60 6.1 3.8
10 8 15
Edge AC

383.75

5.17 4.9 4.8
10 8 15
Edge AC

383.17

5.75 5.4 5.4
10 8 15
Edge AC

Top FH SE Cor BALTIC & ATLAS.

W/4 EC Curb RET
Linda Vista Rd.

Harbor Dr P.L.
Proposed 16" P.L.

149+84.13 BC

Note:

To much local interference to pin
down actual location of conduit

Conduit Line 43' from Harbor Dr

141+56.47 EC

= 458+87.77 Hwy Sta

For total curve = $\Delta 24^{\circ} 16' 30''$

For this portion = $\Delta 6^{\circ} 31' 03''$

$R = 3957$

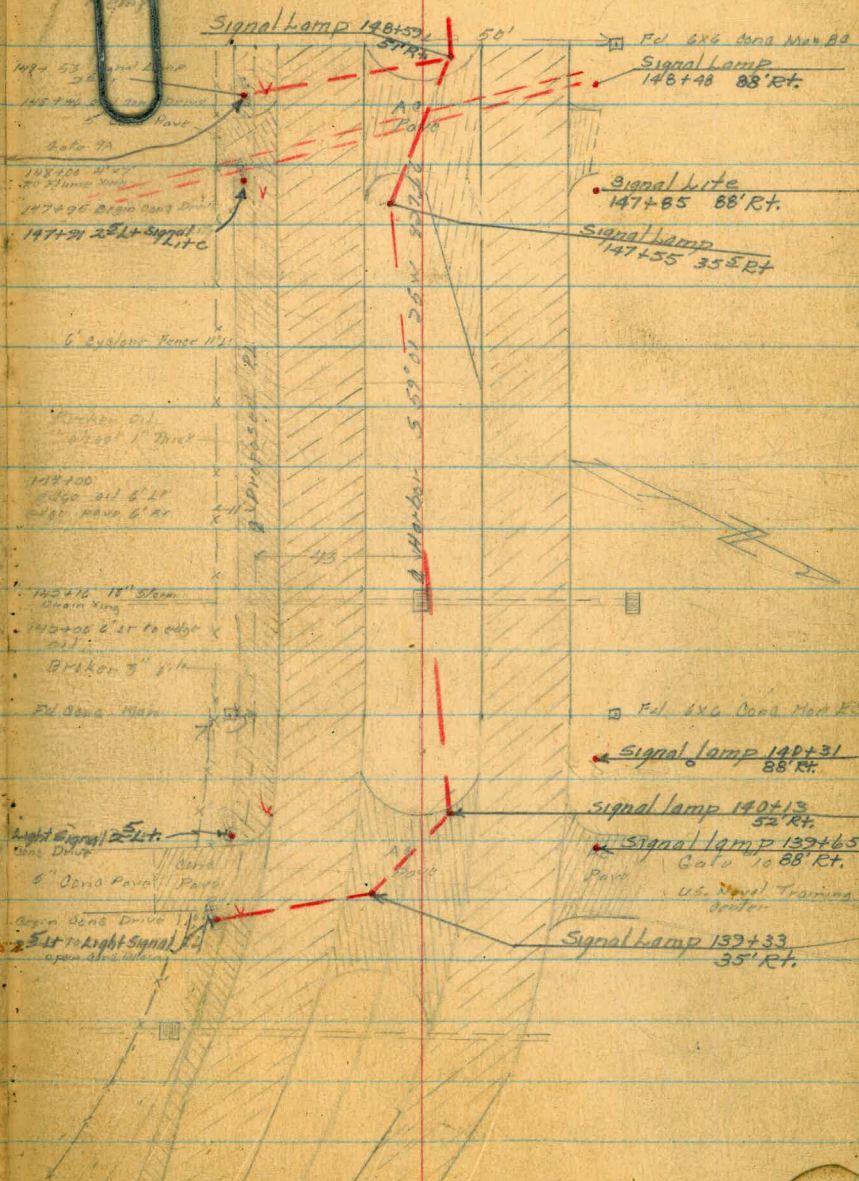
$L = 900.14$

139+21 18" Storm Drain
2' x 2' square
138+00 2' x 1' to edge
10' x 1' to 2nd gate
136+00 6" cyclone
Fence 11' x 1' edge of
50' x 1' edge of Pave 16' x 1'

West
Williams
Vardakis

47

6-30-53



Q Pipe Line 43' from Q Harbor Dr.

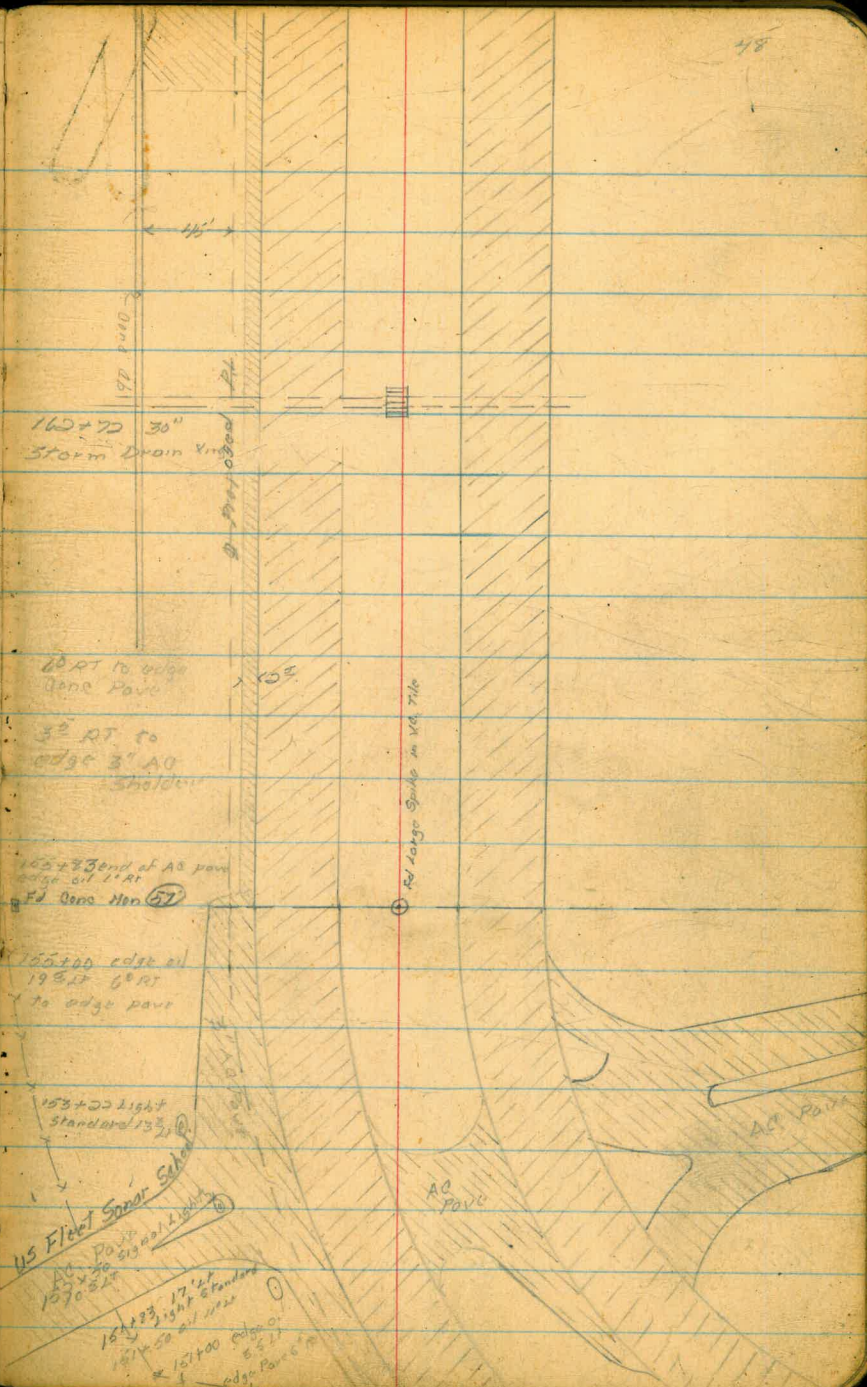
155 + 00.37

$\Delta 51^{\circ} 30'$

$R = 943'$

$L = 516.24$

Def pct 182277135



162+70 30"
Storm Drain 4' inside

60 RT to edge
Gene Pave

32 RT to
edge 3' AQ
Shoulder

152+73 end of AQ pave
edge at 1' RT
Fd Gene Man 57

155+00 edge at
19.5 RT
to edge pave

153+00 Light
Standard 135

US Fleet Support Station
AC Pave
1070 52'

154+73 Light Standard
1514 50 edge at
x 151400 edge at
edge Pave 6'

AC Large Spikes in V.G. Tile

AC Pave

AC Pave

10
11
12

173+93 73

15° 06' 45" L West Prop Line

Rosecrans

172+90 14

15° 08' RT East Prop Line

Rosecrans

Line is New 27' From A. Mass

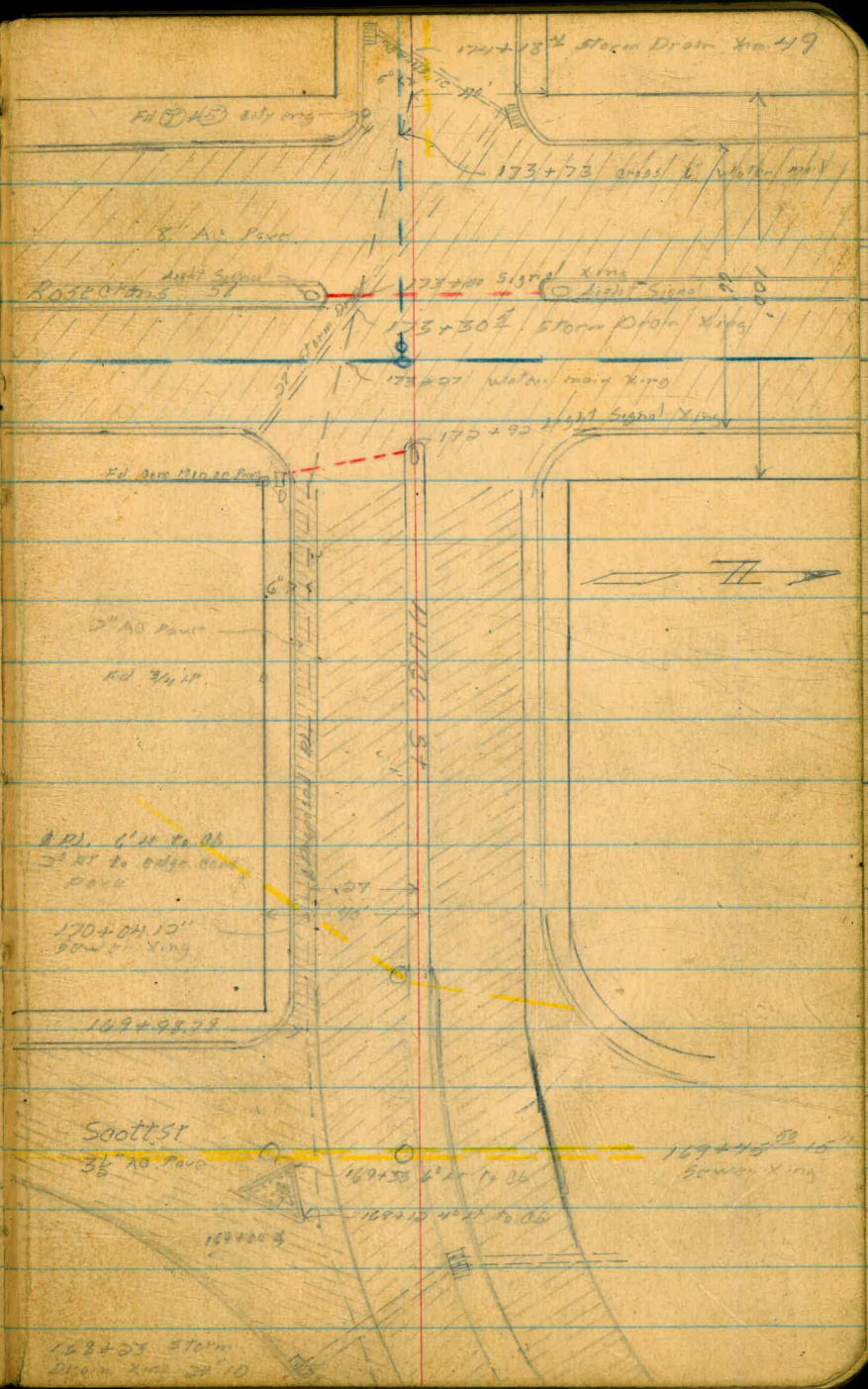
169+90.78

19° 17' 30 RT

Scott St

169+00 3

16° 02' 15" RT



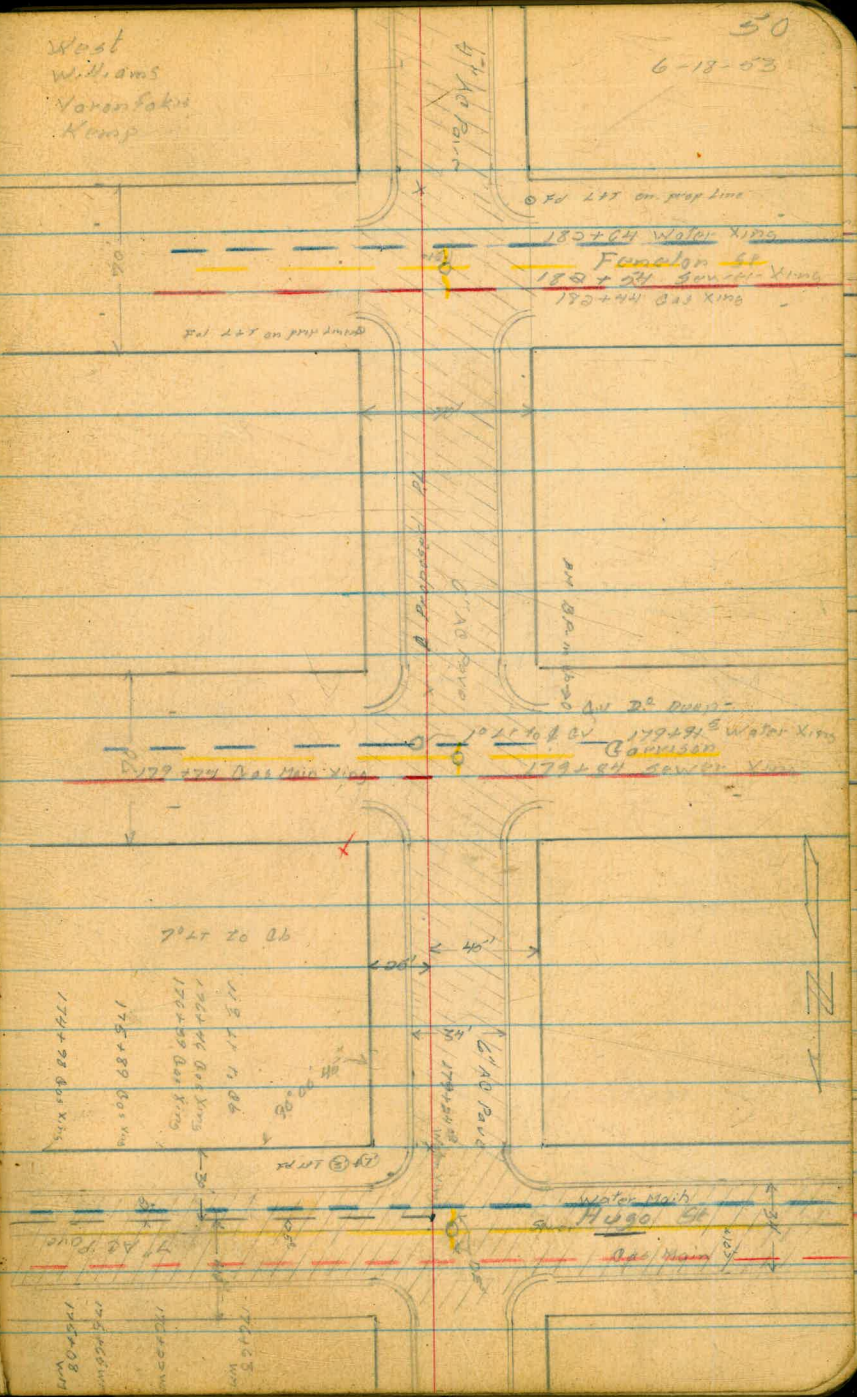
168+03 Storm Drain Xing 37' 10"

Proposed 16" Harbor Dr
Pl. Cont

West
Williams
Varenfaku
Kemp

30

6-18-53



4 Pl. 10" St of Q Street

177+19.09

89° 59' 15" Lt

177+22.81
178+89.50
179+75.00
180+59.00
181+44.00
182+29.00
183+14.00
184+00.00
185+15.00
186+30.00
187+45.00
188+60.00
189+75.00
190+90.00
191+05.00
192+20.00
193+35.00
194+50.00
195+65.00
196+80.00
197+95.00
198+10.00
199+25.00
200+40.00
201+55.00
202+70.00
203+85.00
204+00.00
205+15.00
206+30.00
207+45.00
208+60.00
209+75.00
210+90.00
211+05.00
212+20.00
213+35.00
214+50.00
215+65.00
216+80.00
217+95.00
218+10.00
219+25.00
220+40.00
221+55.00
222+70.00
223+85.00
224+00.00
225+15.00
226+30.00
227+45.00
228+60.00
229+75.00
230+90.00
231+05.00
232+20.00
233+35.00
234+50.00
235+65.00
236+80.00
237+95.00
238+10.00
239+25.00
240+40.00
241+55.00
242+70.00
243+85.00
244+00.00
245+15.00
246+30.00
247+45.00
248+60.00
249+75.00
250+90.00
251+05.00
252+20.00
253+35.00
254+50.00
255+65.00
256+80.00
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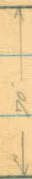
190+75 water Main Xing

part of
190+642 Sewer Xing
190+582 Gas Xing



188+29 Begin Cone Pass

188+04 Water Xing
187+92 Sewer Xing
187+84 Gas Main Xing

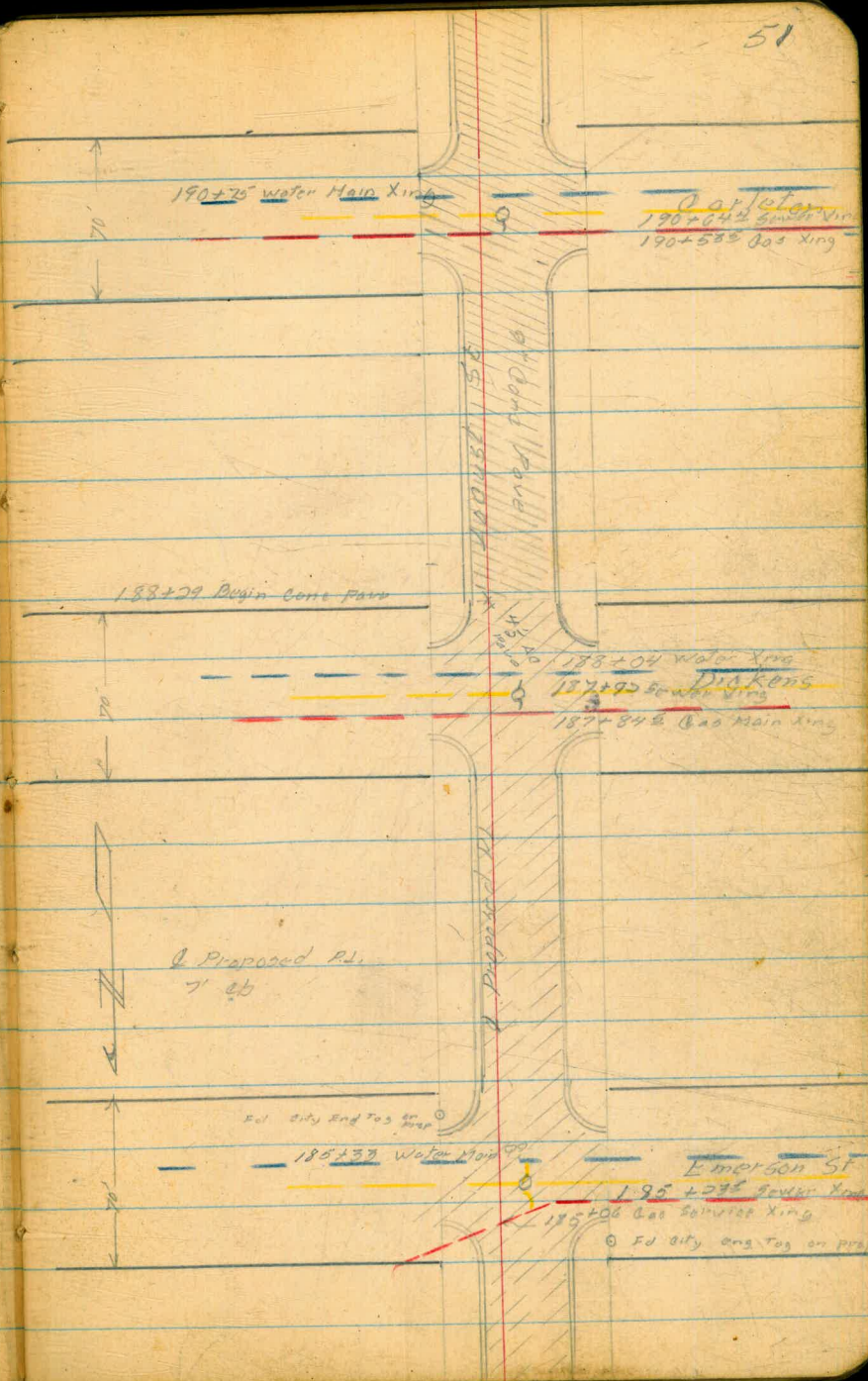


Proposed Rd.
7' ab

Ed City Eng Tog or Prop

185+33 Water Main

Emerson St
195+296 Sewer Xing
185+06 Gas Sewer Xing
Ed City Eng Tog or Prop

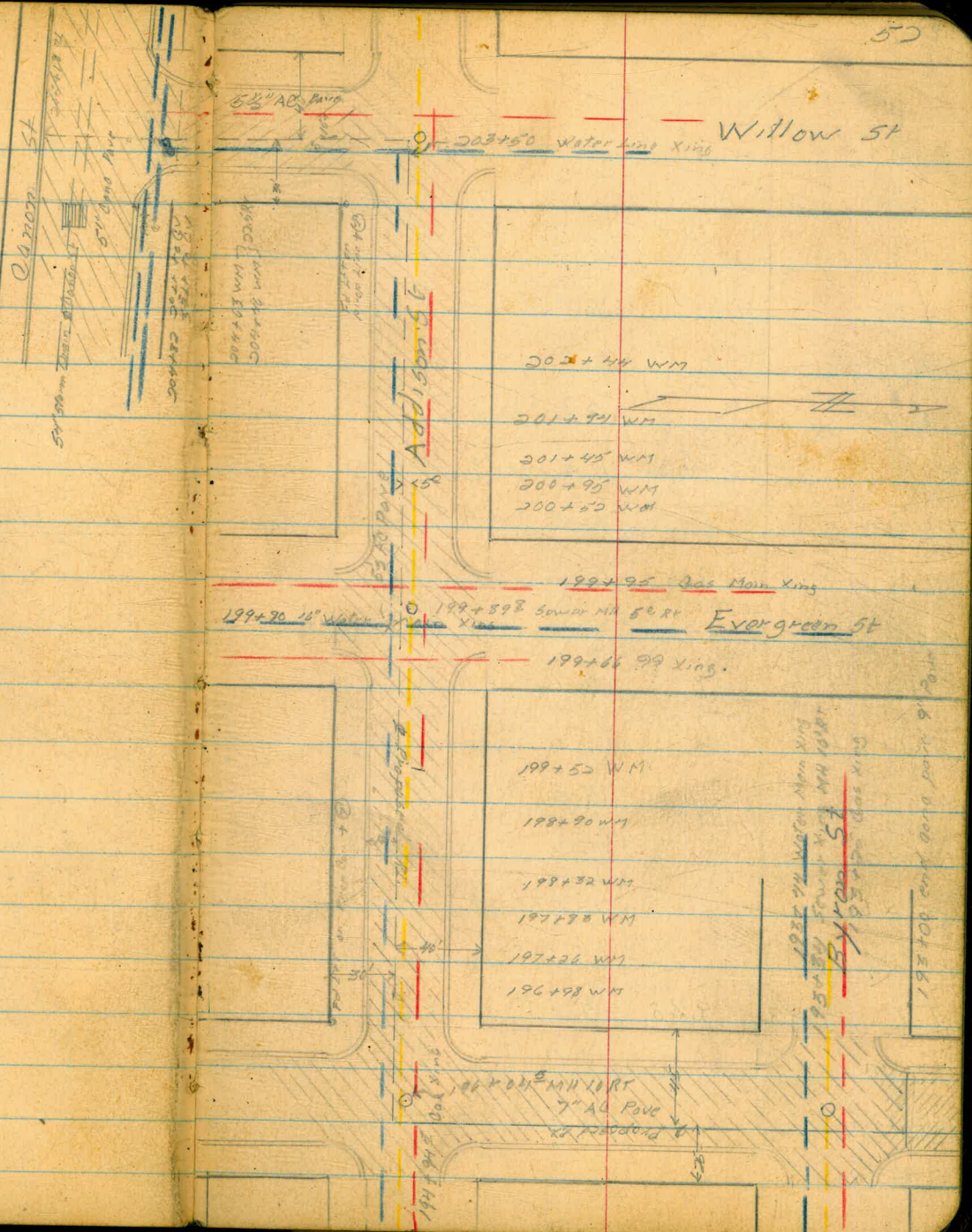


Proposed Harbor Drive
16' P.L. 80ft

204+85± existing 16' P.L.

203+55± 89° 58' 45" RT

196+09± 90° 00' 15" RT



6-19-53

STA	+	HI.	-	FL.
T.B.M	1.64	16.70		15.06
133+00			5.9	10.8
+50			7.8	8.9
134+00			9.6	7.1
+50			11.0	5.7
135+00			11.9	4.8
+50			11.9	4.8
T.P	2.12	8.70	10.12	6.58
136+00			4.3	4.4
+50			4.7	4.0
137+00			5.0	3.7
+50			5.0	3.7
138+00			5.3	3.4
138+21			FLOW LINE 12.57	-4.13
+50			5.6	3.1
T.P	4.83	8.68	4.85	3.85
139+00			5.4	3.3
139+18.5			5.53	3.2
139+50			5.39	3.3
				3.29

Old 2x2 Hub 10' RT BC 132+56.47

14.0	2.7
22' LT	8' RT
13.7	4.1
18' LT	8' RT
13.1	6.1
12' LT	8' RT
12.8	7.8
11' LT	8' RT
12.9	9.3
11' LT	7' RT
12.9	9.2
11' LT	6' RT

4.8	3.4
11' LT	5' RT
4.8	4.1
12' LT	4' RT
5.1	4.4
11' LT	2' RT

18' DRAIN

12.40 = FLOW LINE
47' RT

5.5	5.0
4' LT	2' LT

EDGE CON.

CENT. CON.

6-19-53

54

STA	+	8.68 H _i	-	EL.
139+76			5.27	3.4
140+00			5.1	3.6
+50			5.0	3.7
141+00			4.9	3.8
+50			4.8	3.9
E.C.				
141+56.47			4.8	3.9
142+00			4.6	4.1
+16			4.6	4.1
T.P.	5.03	9.70	4.01	4.67
142+50			5.5	4.2
143+00			5.4	4.3
+50			5.2	4.5
144+00			5.1	4.6
+50			5.0	4.7
145+00			4.9	4.8
+50			4.7	5.0
146+00			4.6	5.1
+50			4.5	5.2
147+00			4.4	5.3

EDGE CON

2

<u>5.1</u>	<u>4.7</u>
5' LT.	3' LT.
<u>4.9</u>	<u>4.4</u>
5' LT.	3' LT.

<u>4.9</u>	<u>4.3</u>
6' LT.	4' LT.
<u>4.6</u>	<u>4.1</u>
5' LT.	3' LT.

18'	8.29
DRAIN	0

<u>8.26</u>	<u>8.23</u>
47' RT.	97' RT.

<u>5.2</u>	<u>4.8</u>
5' LT.	3' LT.

<u>5.0</u>	<u>4.6</u>
5' LT.	3' LT.

<u>4.6</u>	<u>4.4</u>
5' LT.	3' LT.

<u>4.4</u>	<u>4.1</u>
5' LT.	3' LT.

<u>4.5</u>	<u>3.9</u>
5' LT.	3' LT.

6-19-53

55

STA	+	9.70 H ₁	-	E ₁
147+50			4.3	5.4
T.P.	4.96	10.58	4.02	5.68
147+95			5.27	5.3
148+00			5.32	5.3
148+46			5.16	5.4
+50			5.1	5.5
149+00			4.9	5.7
+50			4.4	6.2
B.C.				
149+84.13			3.8	6.8
T.B.M.	7.11	11.96	5.73	4.85
150+00			5.2	6.8
+50			4.9	7.1
151+00			4.8	7.2
+50			5.0	7.0
152+00			5.1	6.9
+50			5.2	6.8
153+00			5.4	6.6
+50			5.5	6.5
154+00			5.8	6.2
+50			6.1	5.9

BEGIN CON. DR.
10.62 = FLOW LINE
4X7 FLUME 10' LT.
END CON. DR.

6X6 CON. MAN. 149+84.13 B.C. North Side Harbor

6.7	5.1
10	4.0
6.6	5.1
10	3.0
5.1	4.6
10	3.5
4.4	5.1
9.0	7.0

155+00 EC	11.96	6.7	5.3
+50		7.7	4.26
155+33		8.5	3.5
	3.82	7.47	8.31
			3.65
156+00		4.2	3.3
+50		4.5	3.0
157+00		4.6	2.9
+50		4.8	2.7
158+00		4.9	2.6
+50		5.0	2.5
159+00		5.1	2.4
+50		5.2	2.3
160+00		5.3	2.2
+50		5.2	2.3
161+00		5.2	2.3
+50		5.4	2.1
	4.83	7.12	5.18
			2.29
162+00		5.2	1.9
+50		5.0	2.1
+72		5.0	2.1

West
 Williams
 Varon Fakas

6-22-53 56

$\frac{71}{15}$ $\frac{70}{20}$ $\frac{77}{5.047}$

to edge oil as walk

edge oil

8.7 to Flow line Grate on E Harbor
 43 RTW 30 Storm drain line

163+00	7.10	5.0	2.1
+50		5.0	2.1
164+00		4.9	2.2
+50		4.9	2.2
165+00		4.9	2.3
+50		4.9	2.2
166+00		5.0	2.1
+50		5.0	2.1
166+95		5.2	1.9
167+00		5.2	1.9
+50		5.14	2.0
+23		5.0	2.1
168+00		5.0	2.1
+50		5.0	2.1
169+00		4.2	2.9
+50		3.9	3.2
4.78	8.47	3.43	3.69
169+45		5.1	3.4
+48		5.57	2.90
+77			
+90		5.2	3.3
170+00		5.1	3.4
+50		5.6	2.9
171+00		6.0	2.5

Bust
168+23

Begin AD Pave

43 RT Storm Drain 10.60

43 LT to to Orate - 11.4 to Flow Line
43 RT

847
533
314

3.33 Top MH + 6" To Flow Line
34 LT TO MH 15" Sewer Line
6.46 + 0.3 To Flow Line
26 RT to Top MH 15" Sewer

Edge AD Pave 3' 50" + 50 Top of Sewer Joff

Q Profile Harbor
Dr Proposed Pl.

West
Williams
Varon Factors

6-27-53

58

171+50	3.49	6.5	2.0
172+00		6.6	1.9
+50		6.5	1.9
	5.87	8.68	5.66
			2.81
172+90 th X		6.4	2.3
173+00		6.0	2.7
+50		5.4	3
193 th X		5.7	3
+98 ²		5.7	3
174+00		5.7	3
+27			
+50		4.7	4
175+00		3.7	5
+50		2.5	6.2
176+00		1.2	7.5
	8.92	16.68	0.92
			7.76
+50		7.7	8.98
177+00		6.4	10.3
177+19 th X		6.0	10.7

6.1 to Grate +34 to Flow Line
26' RT to Ch Inlet storm Drain
+30 to Flow Line

5.6 + 3.0 To Flow Line
102'

177+19 ⁰⁵	16.68	5.70	10.98
+50		6.1	10.6
178+00		6.1	10.6
+50		6.2	10.5
179+00		6.5	10.2
+50		6.8	9.9
+84		6.54	10°RT 10.2
180+00		6.9	9.8
+50		6.6	10.1
	5.84	15.98	6.54 10.14
		3.54	12.44 - 12.61
181+00		5.7	10.3
+50		5.4	10.6
182+00		5.2	10.8
+50		5.4	10.6
+54		5.31	10.7
183+00		5.1	10.9
+50		5.4	10.6
184+00		5.6	10.4
+50		5.8	10.2

+ 6.0 To Flow Line 5°RT + 10°RT
 Top East edge sewer MH of Laoust + Hugo

+ 6.4 To Flow Line
 Top East edge sewer MH

B.P. SW Cor Barrison + Laoust

Top east edge sewer MH 10°RT
 + 6.3 To Flow Line

Sta	+	HI	-	Flow
185+00		16.99	5.9	10.1
	10.67	20.75	5.90	10.08
+25 ⁵			10.50	10.3
+50			10.2	10.6
186+00			9.3	11.5
+50			8.4	12.4
187+00			7.4	13.4
+50			6.3	14.5
187+92			5.37	15.4
189+00			5.4	15.4
+50			4.8	16.0
189+00			3.8	17.0
+50			2.8	18.0
190+00			1.8	19.0
+50			0.6	20.2
+64 ⁴	11.64	32.30	0.09	20.66
191+00			11.3	21.0
+50			10.2	22.1
192+00			8.9	23.4
+50			7.5	24.8

Top east edge sewer MH + 5.1 to Flow Line Sewer

Top east edge Sewer^{MH} + 8.8 to Flow Line

+ 5.4 to Flow Line
Turn on Top east edge sewer MH

Sta	+	H _i	-	Elev
193+00		32.30	6.3	26.0
+34			5.60	26.7
+50			5.6	26.7
194+00			5.2	27.10
+50			4.9	27.5
195+00			4.4	27.9
+50			4.0	28.3
196+00			3.6	28.7
+04	12.74	41.57	3.49	28.81
+09	³⁹ 7		12.8	28.8
+50			12.2	29.4
197+00			10.4	31.2
+50			8.5	33.1
198+00			6.7	34.9
+50			4.8	36.8
199+00			2.9	38.7
+50			1.1	40.5
199+89	12.67	54.15	0.09	41.48
200+06			12.3	41.9
+50			9.1	45.1

10" RV
Top east edge MH + 4.6 to Flow line

Top east edge MH + 3.8 To Flow line

+ 5.1 to Flow line

Profile Harbor Dr

West
Williams
Varonakis

6-22-53 62

Sta	+	W		
201+00		54.15	4.5	49.7
	12.41	65.97	0.59	53.56
+50			11.7	54.3
202+00			6.9	59.2
+50			2.4	63.6
	8.26	73.95	0.28	65.69
203+00			5.8	68.2
+50			2.3	71.7
+55			1.99	72.0
204+00			5.1	68.9
+50			10.4	63.6
	4.03	65.35	12.63	61.32 =
204+85			5.2	60.2
205+15 ⁶			5.07	60.3
			4.03	61.32

10° RT + 50 RT
Top South side MH + 6' To Flow Line

61.20 BM BP NW Cor Canon & Valley St

Existing 16' Pl

Bottom South Side Canon St

Baltic Pl 24"
 stks for Construction

West
 Varonfakis
 Kemp

63

	130	438.57		437.27		1" IP 13' RT 13+53" See page 31
	158	427.64	12.51	426.06		
8+84"			5.05	422.59	410.6	C 12 ⁰
794			5.2	422.4	410.3	C 12 ¹
9+00			5.5	422.1	410.2	C 11 ⁹
+50			7.7	419.9	409.4	C 10 ⁵
10+00			8.7	418.9	408.6	C 10 ³
+47 ⁹⁶			8.9	418.7	407.8	C 10 ⁹
+50			9.0	418.6	407.7	C 10 ⁹
11+00			11.3	416.3	406.9	C 9 ⁴
+50	4.94	419.60	12.98	414.66	406.1	C 8 ⁶
(Break for 75)						
+76			5.9	413.7	405.7	C 8 ⁰
12+00			6.8	412.8	404.9	C 7 ⁹
+50			9.0	410.6	403.3	C 7 ³
+77 ⁶³			10.1	409.5	403.0	C 6 ⁵
+88			10.0	409.6	403.0	C 6 ⁶
13+00			9.1	410.5	403.4	C 7 ¹
+50			5.1	414.5	407.0	C 7 ⁵
	11.42	430.07	0.95	418.65		

Begin Work

split of 8

Finish Floor Change 9+00

410.3
 1.5
 408.8

422.59
 2.95
 425.44

2.17 NW 422.77
 2.99 NW 422.45
 4.57 SE 420.97
 5.14 NW 420.30

split of 8

422.77 407.80 013.97
 422.45 403.80 013.65
 420.87 408.80 012.07
 420.30 408.80 012.50

Line Check
 Casing 0.12 To Face 64
 North on West Side

895
 305
 1200

		430.07			
14+00			11.3	418.8	412.3
150			5.6	424.5	417.7
175 ⁸¹			3.2	426.9	420.6
15+00	8.97	439.03	0.01	430.06	424.0
150			1.3	437.7	428.0
			1.76	437.27	432.27
	2.21	439.48		437.27	
15+65			1.0	438.5	427.9
171 ²			4.2	435.3	427.5
188	1.16	427.86	12.78	426.70	410.7
16+03			11.24	416.62	410.70
118 ⁶⁹			10.34	417.52	410.70
159 ⁰³			9.91	417.95	410.70
16+98			10.28	417.68	410.70
17+13			10.86	417.00	410.70
125 ¹			3.5	424.4	410.70
	12.79	440.21	0.44	427.42	
	7.33	447.19	0.35	439.86	
17+50 ¹⁰			5.8	441.4	435.5
750			2.32	444.87	435.7
			9.91	437.28	437.27

C6 ⁵/₈
 C6 ³/₁
 C6 ¹/₁
 C9 ¹/₁

1" IP 13' RT 10' + 55'

C10 ⁶/₈
 C7 ⁸/₀
 C16 ⁰/₀
 C5 ⁹²/₈₂
 C6 ⁸²/₂₅
 C7 ⁸⁸/₃₀
 C6 ⁷⁰/₇₀
 C13 ⁷⁰/₇₀

Ø Begin Jacking

Ø Hub

Ø End Jacking

412.52
 + 5.03
 422.60
 15.00 E side
 410.60 Bottom

891
 305
 1796

422.60
 - 11.96

410.64 Flow Line
 Casing West Side

410.60 Flow Line
 Casing E Side

TP 20' Below

Baltic Ave Cont.

West
Williams
Varonfakis
Kemp

490
60
5/50
11.97
65
8.24
2.9
17.70

	1.50	446.37		444.87		449	422.69	418.20						
17+70			1.8	444.6	436.2	C8	4		41	4.30	419.39	402.80	08.59	
+75			1.7	444.7	436.0	C8	7		"	3.99	419.70	409.80	08.90	
18+00			6.0	440.4	433.5	C6	0	C6	9	"	3.87	418.82	409.80	09.02
+50	0.84	436.16	12.05	434.32	428.8	C3	9	C5	5	"	4.11	419.58	409.30	08.78
19+00			5.6	429.6	424.0	C3	1	C5	6	"	4.40	419.24	408.70	08.49
+50			9.9	425.2	420.0	C3	7	C5	2	"	4.68	419.01	409.30	08.21
	0.42	422.87	12.71	422.45						"	4.70	417.99	409.80	08.19
20+00			1.4	421.5	415.8	C4	8	C5	7	"	4.49	417.20	408.20	
+50			4.48	418.39	411.8	C6	6							
+60			4.44	418.43	411.4	C7	0							
+69			4.67	418.20	411.3	C6	9							
+85			5.5	417.3	410.3	C6	6	C6	5					
+90			5.54	417.33	410.7	C6	6	C7	2					
21+00			5.3	417.6	410.4	C8	7							
21+22			5.40	417.47	408.8	C8	7							
+46			6.5	416.4	407.3	C9	1							
+50			6.8	416.1	407.0	C9	1							
22+00			11.2	411.7	403.7	C8	0							
	0.62	411.04	12.45	410.40										
+50			3.6	407.4	400.0	C7	4							
23+00			7.7	403.3	395.5	C7	8							

2 of pipe is in
plan position
125' SLY P.L. line.

2/28/57
Kerath

split of X
split of X 43

Tag 30

Top P.L. AS BUILT

TBM	1.08	446.29	11.97	445.20
TD	0.60	435.11	11.97	429.51
18+50	(0.3)	5.50	429.61	T/P
19+00	(5.3)	9.43	425.68	T/P
19+50	7.6	13.34	421.77	T/P
20	0.10	424.07	12.14	423.97
CRDM		2.19	416.88	416.88
		7.59		
Cor. Curb	8.55	415.52		415.52

	411.04					
23+50		11.5	399.5	391.2	C8	
	0.55	398.70	12.89	398.15		
24+00		2.4	396.3	389.5	C6	
+50		4.5	394.2	388.1	C6	
+66		4.9	393.8	387.6	C6	
25+00		5.9	392.8	386.6	C6	
+50		7.3	391.4	385.2	C6	
26+00		8.8	389.9	383.8	C6	
+50		10.4	388.3	382.3	C6	
27+00	1.83	388.61	11.92	386.77	380.8	C6
+16		2.3	286.3	380.3	C6	
+50		3.3	285.3	379.3	C6	
28+00		4.3	384.3	378.9	C5	
+50		5.0	383.6	378.5	C5	
29+00		5.5	383.1	378.1	C5	
+50 ⁸⁸		5.6	383.0	378.0	C5	
+50		6.1	382.5	377.7	C4	
+68 ⁵⁸		6.28	382.33	377.4	C4	
+74 ²⁸		6.41	382.20	377.3	C4	
		3.57	385.04			

C8 ³
C6 ⁸
C6 ¹
C6 ²
C6 ²
C6 ²
C6 ¹
C6 ⁰
C6 ⁰
C6 ⁰
C6 ⁰
C5 ⁴
C5 ¹
C5 ⁰
C5 ⁰
C5 ⁸
C4 ⁹
C4 ⁹
C4 ⁹

C ¹
Tec

Tec

split of X

end of work
see page 46
Total FH SE Co, Bolivia & Altos

Kst Francis Co 100[±]E
 Stks for 6" AD Main

West
 Williams
 Varonakis
 Kemp

10-8-03

67

11.96 93.76 81.80

TBM 9+00

0+00 = 8+9225

12.4 81.4 77.0

C4 ⁴

+20

11.2 82.6 78.5

C4 ¹

+28

8.7 85.1 79.0

C6 ¹

+35

5.9 87.9 81.2

C6 ¹

+44

5.8 88.0 84.1

C3 ⁹

CR. To

T.B.M.

11.96 81.80 = 81.80

Alley Blk 89
N of Myrtle E of Wilson
Stks for 6" AO Main

WEST
WILLIAMS
VARONFAKIS
KEMP

10/13/53

68

	1.93	329.48	327.55		BP NW Cor Dwight + 36" 51
0+00			3.4 326.1 320.6	C5 $\frac{5}{5}$	
+50			4.4 325.1 319.4	C5 $\frac{7}{7}$	
1+00			5.6 323.9 318.8	C5 $\frac{1}{1}$	
+39			6.7 322.8 322.1	C0 $\frac{7}{7}$	WM E
+50			6.8 322.7 317.8	C4 $\frac{9}{9}$	
2+00			8.8 320.7 314.8	C5 $\frac{9}{9}$	
+25			11.3 318.2 318.0	C0 $\frac{2}{2}$	WM W
+50	215	319.27	12.30 317.12 311.8	C5 $\frac{4}{4}$	
+50			1.9 317.4 316.6	C0 $\frac{2}{2}$	WM E
+45			2.4 316.9 316.8	C0 $\frac{1}{1}$	WM W
3+00			4.1 315.2 308.7	C6 $\frac{5}{5}$	
+05			4.2 315.1 313.8	C1 $\frac{3}{3}$	WM E
3+00			5.8 313.5 314.0	F0 $\frac{5}{5}$	WM W
+50			6.4 312.9 306.4	C6 $\frac{5}{5}$	
+58			7.4 311.9 310.8	C1 $\frac{1}{1}$	WM E
+65			8.1 311.2 310.6	C0 $\frac{6}{6}$	WM W
+79			8.9 310.4 309.9	C0 $\frac{5}{5}$	WM E
4+00			9.9 309.4 304.0	C5 $\frac{4}{4}$	

ALLEY BLK. 89
 N. OF MYRTLE E. OF WILSON
 (CONT.)
 319.27

4+1230 10.6 308.7 303.3

+15 11.0 308.3 307.9

+30 11.4 307.9 307.2

+50 11.6 307.7 302.8

+72 12.8 306.5 306.5

+87 11.2 308.1 306.4

5+100 12.9 306.4 302.2

+50 12.8 306.5 302.0

+55 12.8 306.5 302.0

14.1 305.2 305.5

+87.7 13.1 306.2 302.0

+92.7 13.2 306.1 302.0

11.50 329.48 0.29 318.98

1.90 327.58 = 327.55

WEST
 WILLIAMS
 VARONFAKIS
 KEMP

10/13/53

69

C5 ⁴

C0 ⁴

C0 ⁷

C4 ⁹

C0 ⁰

C1 ⁷

C4 ²

C4 ⁵

C4 ⁵

F0 ³

C4 ²

C4 ¹

WM W

WM E

WM E

WM W

FH TCO

(5) FH TCO

Alley BIK 92 N of Myrtle
E of 37th

West
Williams
Varon fakro
Kemp

Hot

70

10-28-53

234	322.33		319.99		BM BP NW	Cor Dwight + 37 th
0+55		5.3	317.0	313.6	C3 ⁴	Begin work
1+00		7.0	318.3	312.8	C5 ⁵	
+09		4.1	318.2	316.7	C1 ⁵	
+19		5.0	317.3	316.0	C1 ³	WME
+25		4.5	317.8	312.2	C5 ⁶	WME
+50		6.6	315.7	310.0	C5 ⁷	
0.76	313.04	10.05	312.28			
+87		3.2	309.8	305.0	C4 ⁸	
+90		3.4	309.6	308.4	C1 ²	WME
2+00		9.1	303.9	300.4	C3 ⁵	
2+12		13.9	299.1	296.4	C2 ⁷	
0.50	300.66	12.88	300.16			
+50		10.7	290.0	286.5	C3 ⁵	
+53		15.1	285.6	301.4	F15 ⁸	WME
+60		11.0	289.7	300.5	F10 ⁸	WME
0.10	287.76	13.01	287.65			
2+90	20¹/₂ Bend	10.8	277.0			
+93	22 ¹ / ₂ BEND	11.6	276.2	271.5	C4 ⁷	
3+00		13.9	273.9	271.5	C2 ⁴	
+25		13.0	274.8	271.5	C3 ³	

ALLEY BLK. 92 CONT.

28775

3+28 (22 1/2 BEND) 12.6 275.2 271.5

~~+33~~ ~~11.4 276.4 271.5~~

+43 0.3 287.5 300.0

+62 +2.3 290.1 301.0

+50 7.6 280.2 276.0

+75 11.24 296.96 2.03 285.72 281.41

+88 6.6 290.4 287.0

4+00 2.3 294.7 292.7

12.70 309.10 0.56 296.40

4+13 7.9 301.2 302.6

+25 9.8 299.3 297.0

+50 6.7 302.4 299.6

5+00 6.2 302.9 299.6

+24 3.3 305.8 304.6

+37 5.0 304.1 304.2

+50 4.8 304.3 298.9

7.56 312.05 4.61 304.49

+75 7.7 304.4 296.6

+75 8.0 304.1 304.0

WEST
WILLIAMS
VARONFAKIS
KEMP

HOT

71

10/28/53

C3 ⁷

C4 ⁹

F12 ⁵

F10 ⁹

C4 ²

C4 ³

C3 ⁴

C2 ⁰

F1 ⁴

C2 ³

C2 ⁸

C3 ³

C1 ²

F0 ¹

C5 ⁴

C7 ⁸

C0 ¹

FH Tee

(5)

Fire Hyd

WNW

WNW

WNW

WNW

WNW

ALLEY BLK. 92 CONT.

WEST
WILLIAMS
VARONFAKIS
KEMP

HOT

72

10/28/53

6100 312.05 8.7 303.4 294.3 C9 ¹

110 12.1 300.0 293.6 C6 ⁴

116 9.6 302.5 304.1 F1 ⁶

WM W

10.55 320.51 2.09 309.96

0.52 319.99 = 319.99

Alley BIK 54
 N of Wightman
 E of 39th
 strike for 6" AD Main + Masters

West
 Williams
 Varonakis
 Kemp

11/17/53

73

	6.00	353.30	347.30		
	4.00	349.82	7.48	345.82	
0+80		8.4	341.4	337.8	C3 $\frac{6}{0}$ Begin work
+90		7.3	342.5	341.5	C1 $\frac{0}{4}$ WME
1+00		4.9	344.9	338.5	C6 $\frac{4}{1}$
+05		4.9	344.9	342.8	C2 $\frac{1}{8}$ WME
+19		4.6	345.2	343.4	C1 $\frac{8}{7}$ WMW
1+37		4.5	345.3	339.6	C5 $\frac{7}{3}$
+50		4.7	345.1	339.8	C5 $\frac{3}{9}$
+55		4.8	345.0	344.1	C0 $\frac{9}{9}$ WME
+79		4.6	345.2	344.3	C0 $\frac{9}{5}$ WMW
2+00		5.2	344.6	340.1	C4 $\frac{5}{7}$
+09		4.6	345.2	344.5	C0 $\frac{7}{1}$ WME
+50		5.1	344.7	340.6	C4 $\frac{1}{0}$
+62		5.0	344.8	344.8	C0 $\frac{0}{4}$ WME
+59		4.8	345.0	344.6	C0 $\frac{4}{1}$ WMW
+95		5.0	344.8	344.9	F0 $\frac{1}{8}$ WME
+93		5.2	344.6	344.7	F0 $\frac{1}{8}$ WMW
3+00		5.0	344.8	341.0	C3 $\frac{8}{8}$

911 NW BP 39th + University

ALLEY BLK. 54 CONT

349.82

WEST
WILLIAMS
VARON FAKIS
KEMP

NW 13M. 80 39th + University 71
347.30

11/17/53

3+25	4.7	345.1	345.0	C0 ¹	WME
+50	4.2	345.6	341.4	C4 ²	
+59	4.9	345.0	345.0	C0 ⁰	WMW
+60	4.2	345.6	345.2	C0 ⁴	WME
+95	3.6	346.2	345.6	C0 ⁶	WME
4+00	3.8	346.0	341.9	C4 ¹	
+12	3.9	345.9	345.5	C0 ⁴	WMW
+37	3.6	346.2	345.7	C0 ⁵	WMW
+50	3.4	346.4	342.3	C4 ¹	
+63	2.9	346.9	346.3	C0 ⁶	WME
5+00	2.9	346.9	342.8	C4 ¹	
+06	3.0	346.8	346.7	C0 ¹	WME
6.38	2.85	353.35	346.97		
+11	6.6	346.8	346.4	C0 ⁴	WMW
+31	6.2	347.2	346.6	C0 ⁶	WMW
+50	6.1	347.3	343.2	C4 ¹	
+79	5.1	348.3	347.3	C1 ⁰	WME
+92	5.2	348.2	347.2	C1 ⁰	WMW
6+00	4.7	348.7	343.6	C5 ¹	
+17	4.9	348.5	347.7	C0 ⁸	WME

ALLEY BLK. 54 CONT

WEST
WILLIAMS
VARONFAKIS
KEMP

11/17/53

75

553.35

6.50

4.9 34 8.5 344.0

C4 $\frac{5}{}$

4.85

4.9 34 8.5 344.2

C4 $\frac{3}{}$

End of work

6.00 54 7.35 = 547.30

Alley BIK 43
 N of University SIXS Fair Meters
 E of Marlborough

West
 Williams
 Varonakis
 Kemp

(Cool)
 11-18-53 76

5.53 369.09 363.56

SW RD El Cajon + Van Dyke

4.20 368.57 4.72 364.37

4.63 366.96 6.24 362.33

5.39 363.81 8.54 358.42

0+26

7.9 355.9 355.6

CO $\frac{3}{3}$

W

+34

7.3 356.5 356.2

CO $\frac{3}{3}$

E

1+25

6.6 357.2 357.0

CO $\frac{2}{2}$

E

+30

6.3 357.5 356.8

CO $\frac{1}{1}$

W

+73

6.2 357.6 357.2

CO $\frac{4}{4}$

E

+72

6.0 357.8 356.9

CO $\frac{9}{9}$

W

+74

5.9 357.9 356.9

CI $\frac{0}{0}$

W

+82

6.0 357.8 357.3

CO $\frac{5}{5}$

E

2+27

5.8 358.0 357.4

CO $\frac{6}{6}$

E

+31

5.7 358.1 357.4

CO $\frac{7}{7}$

E

+22

5.8 358.0 356.9

CI $\frac{1}{1}$

W

+77

5.8 358.0 357.5

CO $\frac{5}{5}$

E

3+22

5.3 358.5 357.4

CI $\frac{1}{1}$

W

3+40

4.8 359.0 357.8

CI $\frac{2}{2}$

E

+52

5.0 358.8 357.5

CI $\frac{3}{3}$

W

+94

5.2 358.6 358.0

CO $\frac{6}{6}$

E

+96

5.0 358.8 357.6

CI $\frac{2}{2}$

W

ALLEY BLK. 43 CONT.

WEST
WILLIAMS
VARONFAKIS
KEMP

11/18/53

77

363.81

4+21	5.0	359.8	358.1	CO ¹	E
+33	5.2	358.6	357.8	CO ⁸	W
+56	5.5	358.3	357.8	CO ⁵	W
+82	5.2	358.6	358.3	CO ³	E
5+02	5.4	358.4	358.3	CO ¹	E
+29	5.5	358.3	358.4	FO ¹	E
+33	5.5	358.3	358.0	CO ³	W
+52	5.8	358.0	358.1	FO ¹	W
+67	5.7	358.1	358.5	FO ⁴	E
+70	5.7	358.1	358.2	FO ¹	W

2.61 367.1 4.31 359.50

6.11 369.61 3.61 363.50

4.90 368.02 6.49 363.12

4.45 363.57 = 363.56

North + South Alley in BK
66 Ocean Beach
Stks for 6" Main

West
Williams
Vorontakis
Kemp 11-20-53

78

BP SE Cor Cable + Coronado

	8.74	37.32		28.58
	12.75	49.39	0.68	36.64
0+00			8.2	41.2 37.8
+50			6.8	42.6 39.6
1+00			5.0	44.4 41.7
+35			2.9	46.5 46.6
+50			4.0	45.4 42.9
+54			3.3	46.1 43.0
1+58			3.0	46.4 46.8
1+54			3.1	46.3 43.0
+75			3.8	45.6 41.0
2+00			5.1	44.3 40.6
+04			5.7	43.7 40.5
+50			4.1	45.3 41.2
+70			2.1	47.3 46.8
	1.30	48.31	2.38	47.01
3+00			2.2	46.1 41.6
+47 ²⁰			2.2	46.1 42.8
	1.44	36.71	13.04	35.27
	4.18	34.68	6.21	30.50
			6.16	28.52 = 28.58

C 3 4

C 3 0

C 2 7

F 1 0

C 2 5

C 3 1

F 0 4

C 3 3

C 4 6

C 3 7

C 3 2

C 4 1

C 0 5

C 4 5

C 3 3

C 3 5

WM W

90° Bend

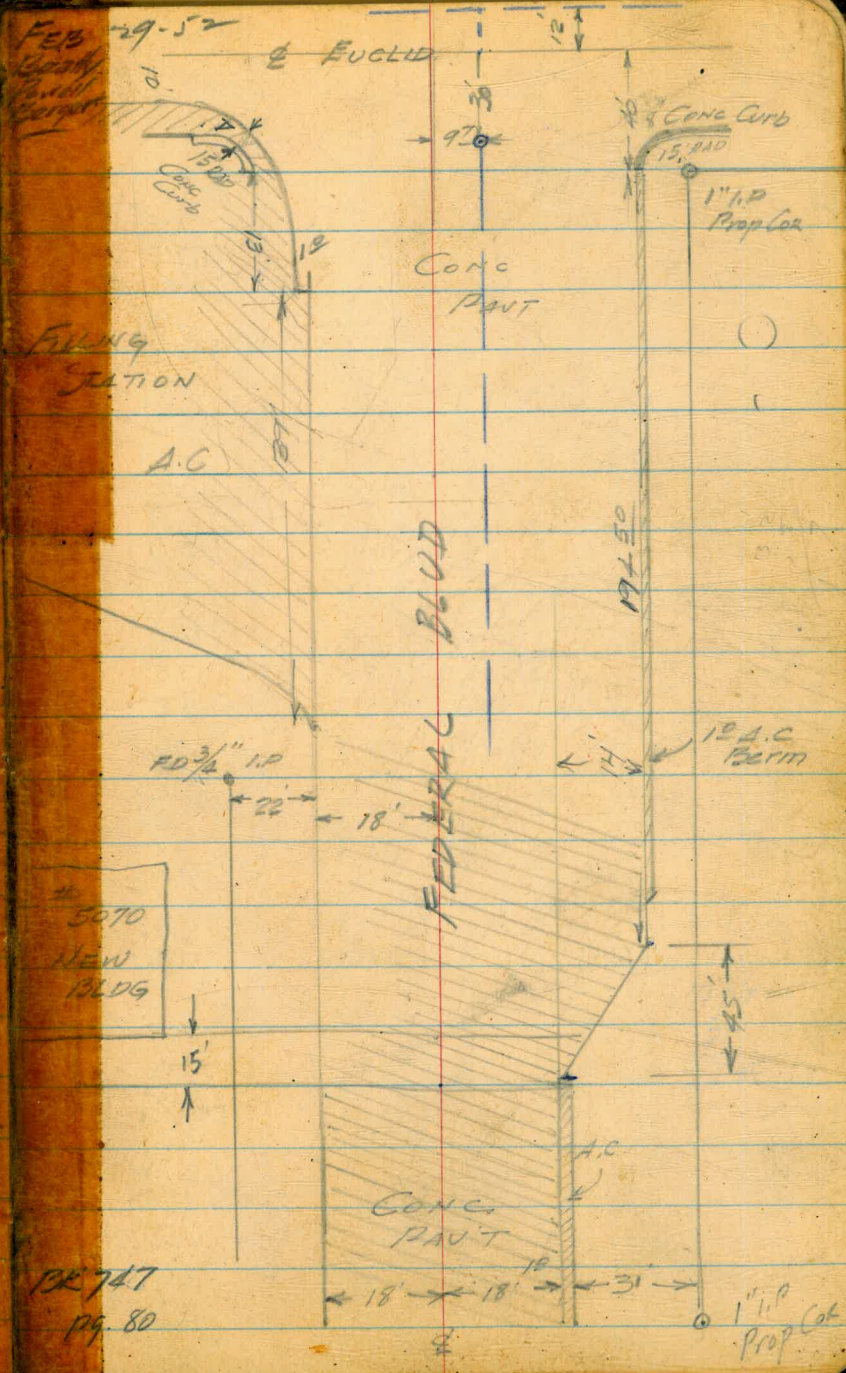
WM South

90° South

90° Bend

WM W

S II



23x5
22x5
21x5
20x5
19x5
18x5
17x5
16x5
15x5
14x5
13x5
12x5
11x5
10x5
9x5
8x5
7x5
6x5
5x5
4x5
3x5
2x5
1x5

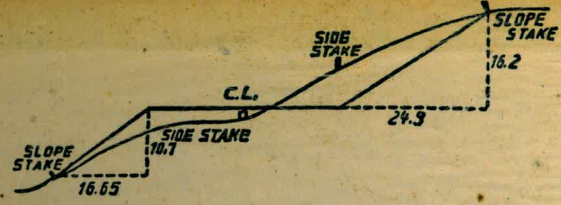
12787
1980

$\frac{113}{100}$
 $\frac{24}{1000}$
 $\frac{411}{1000}$



Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

657
 44
 1.97
 11.9
 1377



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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