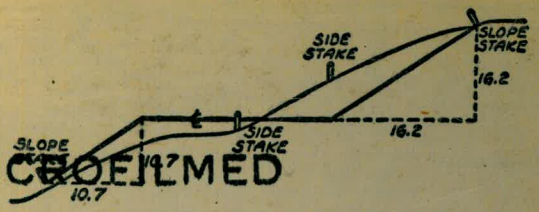
#772



MICROFILMED

Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

500' N on hot line

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

MAR. 11 1949

PROPOSED PIPELINE
VENTURA BLVD

BEATTY
BAKER
ROGERS

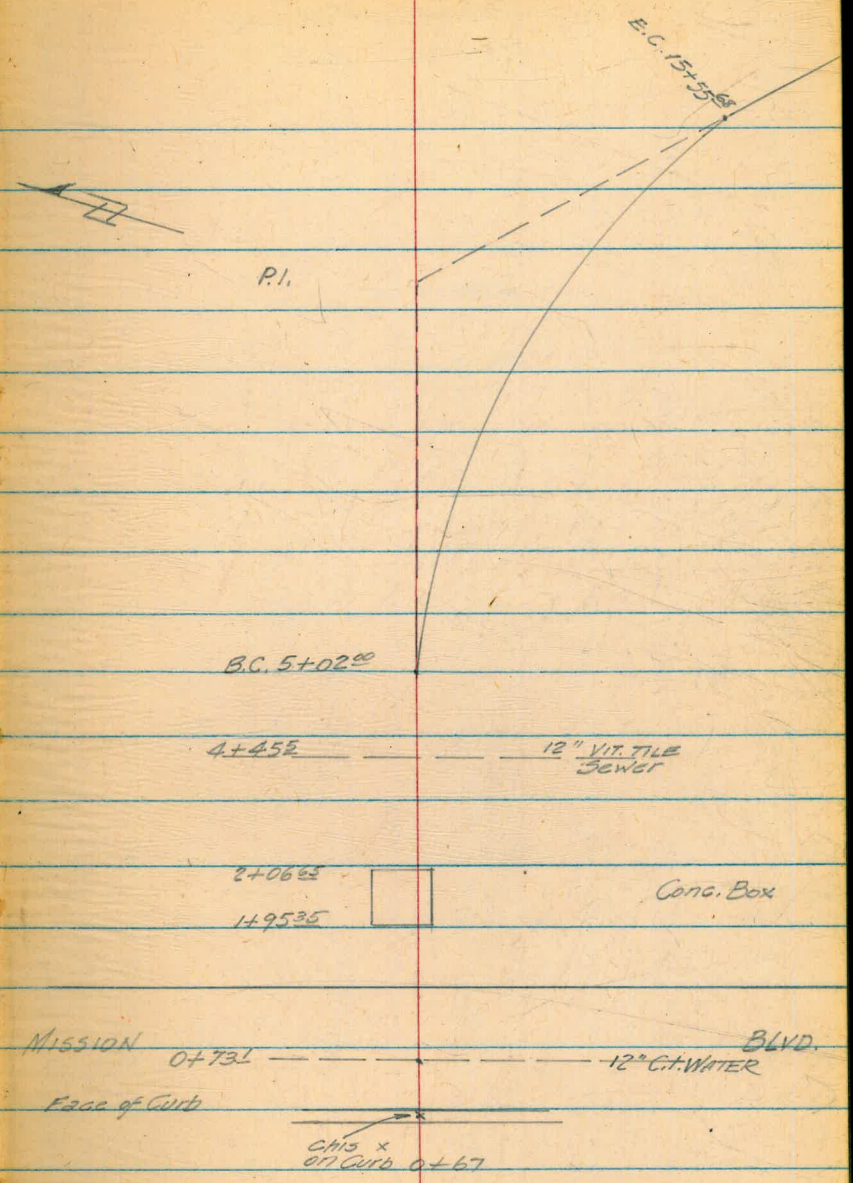
ELEVATIONS - WATER & SEWER - VENTURA BLVD

BM	3.90	06.28		02.38	USC&GS 11.39 Δ COASTER CITY 02.38
TP	3.44	05.36	4.36	01.92	
	Top 12" VIT Sewer ℄ 4+45±		8.01	Minus 02.65	
TBM.	6.31	05.49	6.81	Minus 0.82	Chis + Curb 0+67±
	Top 12" C.I WATER 0+73± on ℄		9.57	Minus 04.08	
TP	5.08	10.44	0.13	05.36	
CK B.M (gone)			2.91	07.53 = 07.51	Sea w311 S.W B.P. (Ventura)

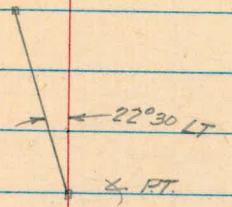
℄ PROFILE

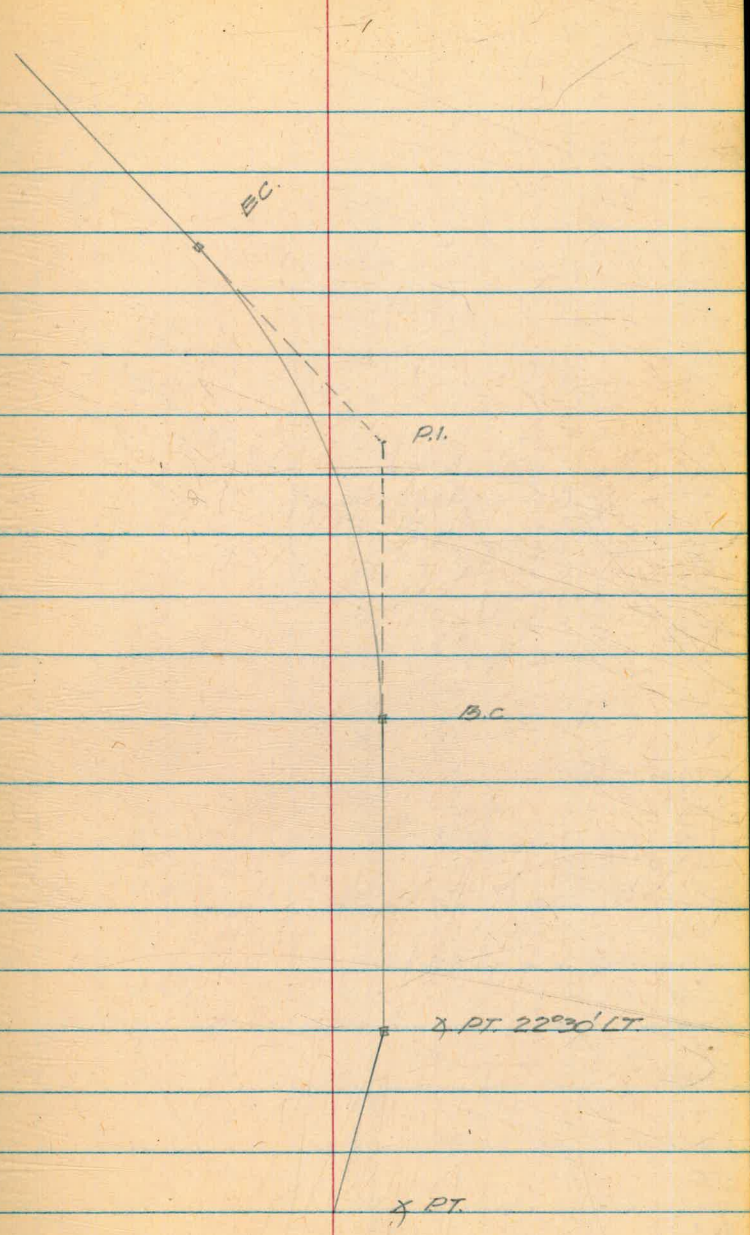
TBM.				Minus 0.82	Chis X on Curb
0+00					
+50					
1+00					
+50					

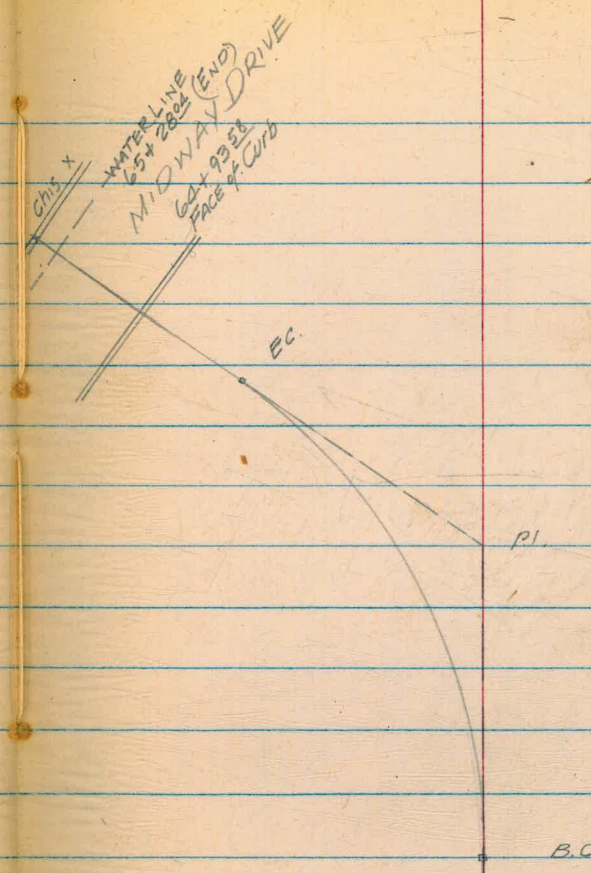
MAR. 7, 1949



PROPOSED PIPE LINE
VENTURA BLVD




E.C.
P.I.
B.C.
℄ PT. 22°30' LT.
℄ PT.

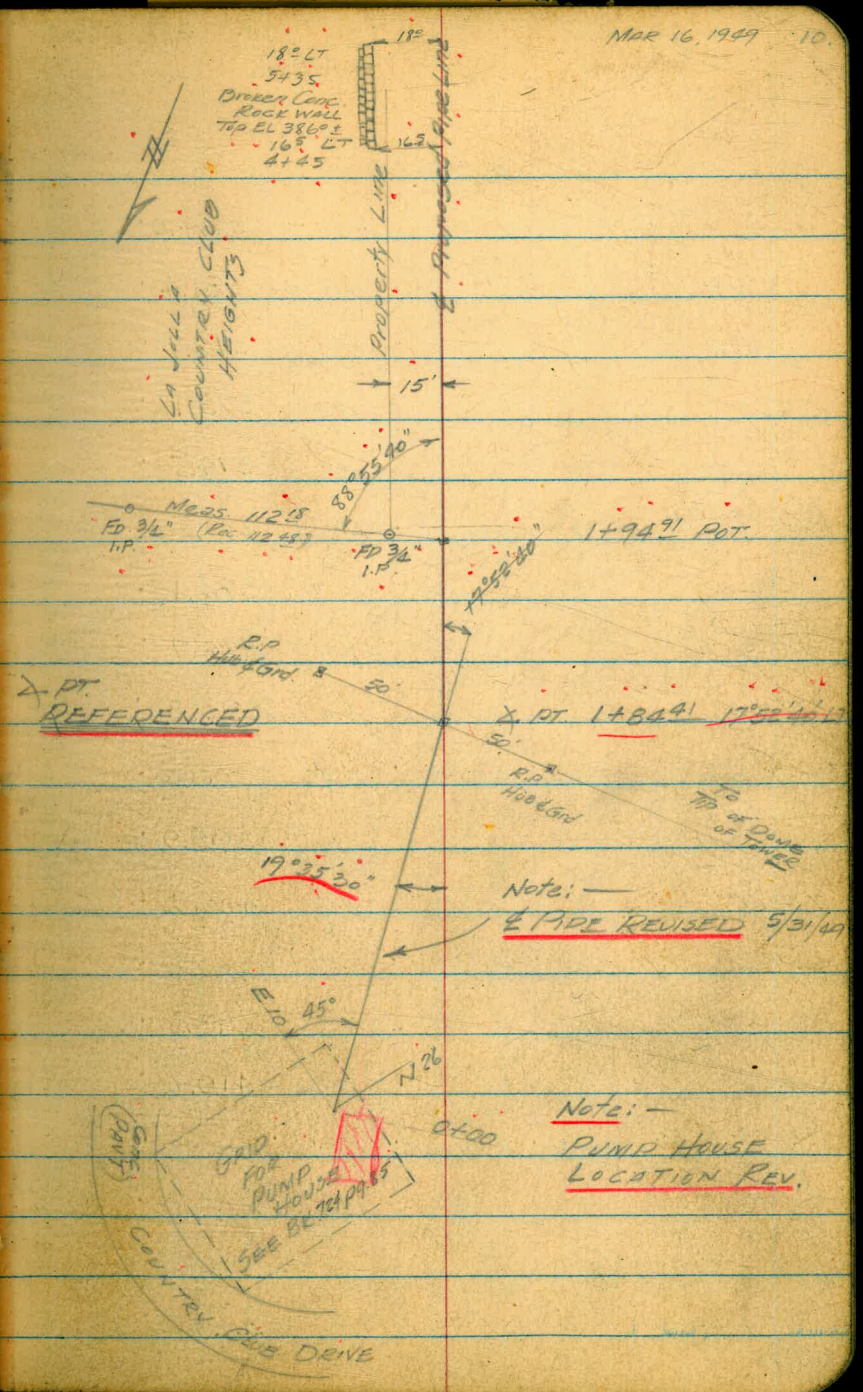

Chis. x
WATER LINE
6+280± (END)
MIDWAY DRIVE
6+93.58
FACE of Curb
Ec.
P.I.
B.C.

MAR. 21, 1942
Beatty
Baker
Rogers

PRELIMINARY FOR MUIRLANDS PIPELINE EXT.
FROM
℄ PROFILE

			54 Cr. Cyl.	
D	12.19	401.29		389.10
			8.0	393.25 SE. COR. GRID
0+00	(N26 E10)		9.7	391.59
+50			10.9	390.39
P	12.01	401.10	12.20	389.09
1+00	Profile revised		9.8	391.3
+50	See pg. 18.		7.5	393.6
+84.41	(℄ PT)		6.4	394.7
2+00			4.4	396.7
+08			3.3	397.8
+50			2.9	398.2
+82			6.5	394.6
3+00			9.4	391.7
P	1.01	392.15	9.96	391.14
+40			6.0	386.2
+50			6.5	385.7
+68			7.9	384.3
4+00			7.4	384.8
+20			6.4	385.8
+36			6.8	385.4

MAR 16, 1949 10.



Note: — Pump House Location Rev.

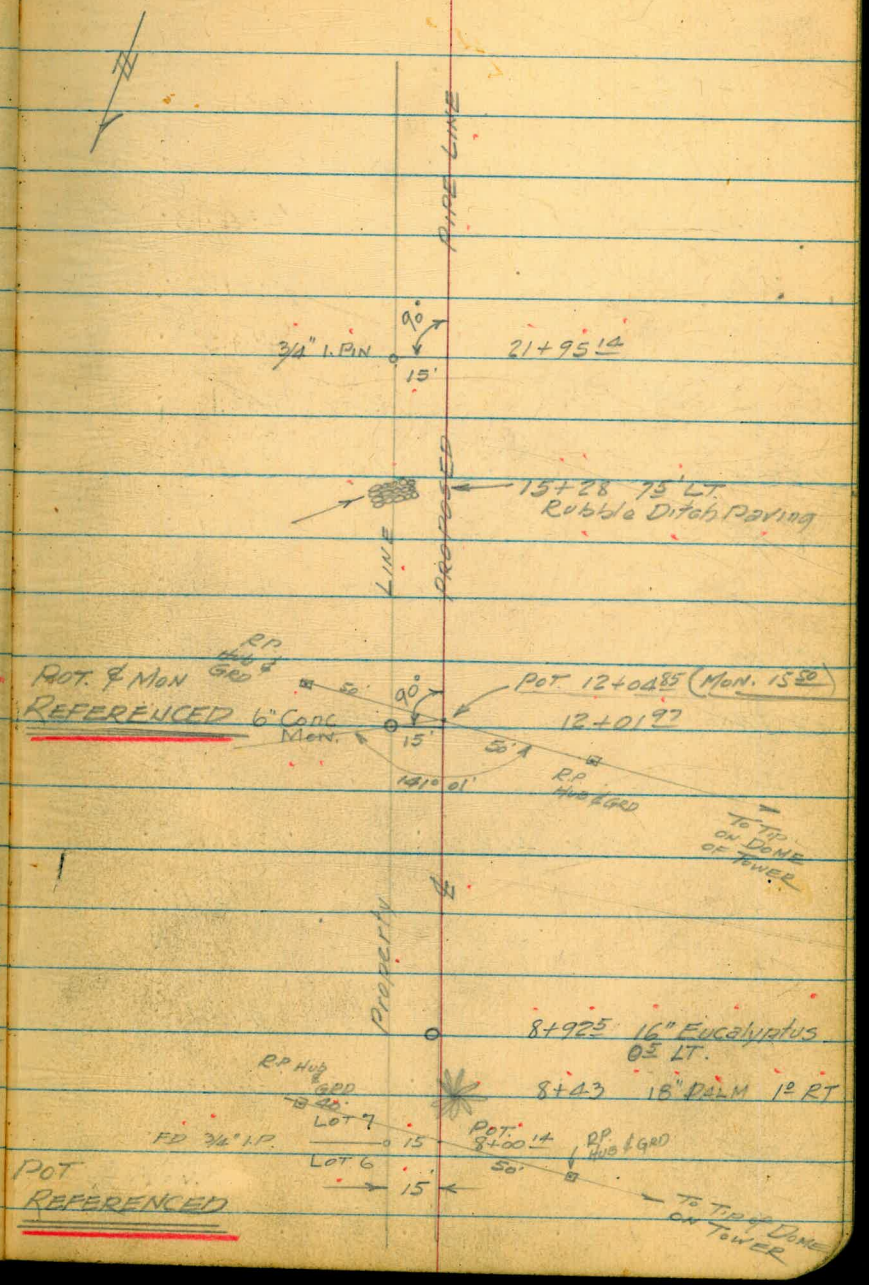
MAR 21 1949

℄ PROFILE

		392.15		
4+50			8.2	384.0
+68			10.8	381.4
+84			13.5	378.7
5+00			17.1	375.1
+07			17.7	374.5
P Rock in Wall	11.73	396.75	7.13	385.62
+40			10.7	386.1
+50			8.1	388.7
6+00			3.0	393.8
P (Rock)	12.66	408.86	0.55	396.20
+50			9.0	399.9
7+00			2.0	406.9
P (Rock)	11.95	420.05	0.76	408.10
+50			6.8	413.3
8+00			0.5	419.6
P Top Grd Stk.	6.25	426.24	0.06	419.99
SET TBM.			2.56	423.68
+50			+0.4	426.6
+69			+3.0	429.2

3/4" I.P. 15' LT STA 8+00 LOT 6-7

MAR. 16, 1949 11.

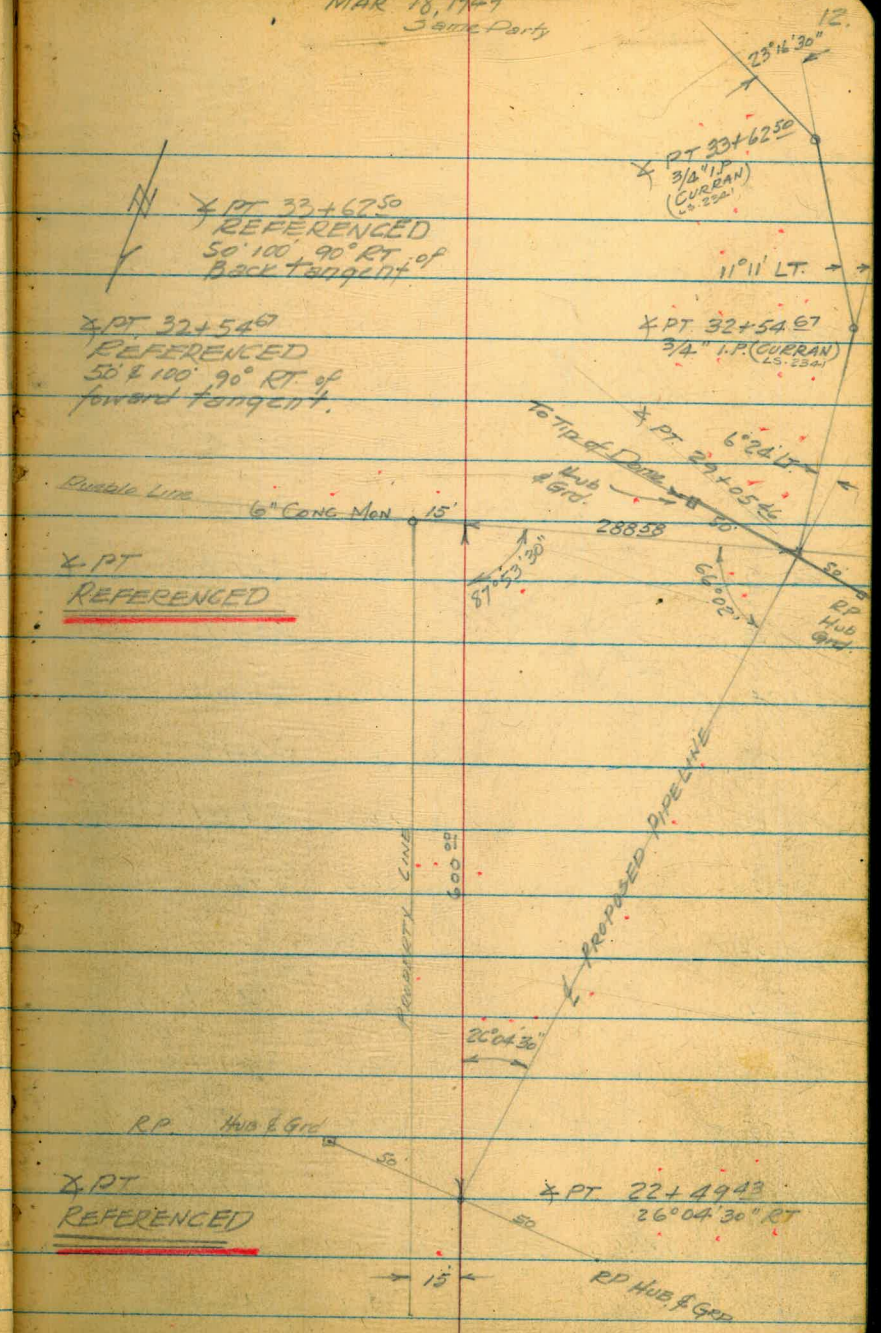


MAR 18, 1949
Same Party

℄ PROFILE
426.24

9+00			+5.6	431.8
P Rock	7.88	433.63	0.49	425.75
+50			+0.8	434.43
+78			+1.0	434.6
10+00			+0.7	434.3
+50			0.5	433.1
11+00			2.0	431.6
+25			2.5	431.1
+50			4.7	428.9
12+00			9.1	424.5
Set T.B.M.			6.66	426.97
+13			9.9	423.7
P (Rock)	1.51	422.51	12.63	421.00
+50			3.1	419.4
+80			7.2	415.3
13+00			11.3	411.2
P	0.57	410.26	12.82	409.69
+25			4.9	405.4
13+50			12.1	398.2
P	1.16	398.35	13.07	397.19

Top Conc Mon. 15' RT 12+01.95



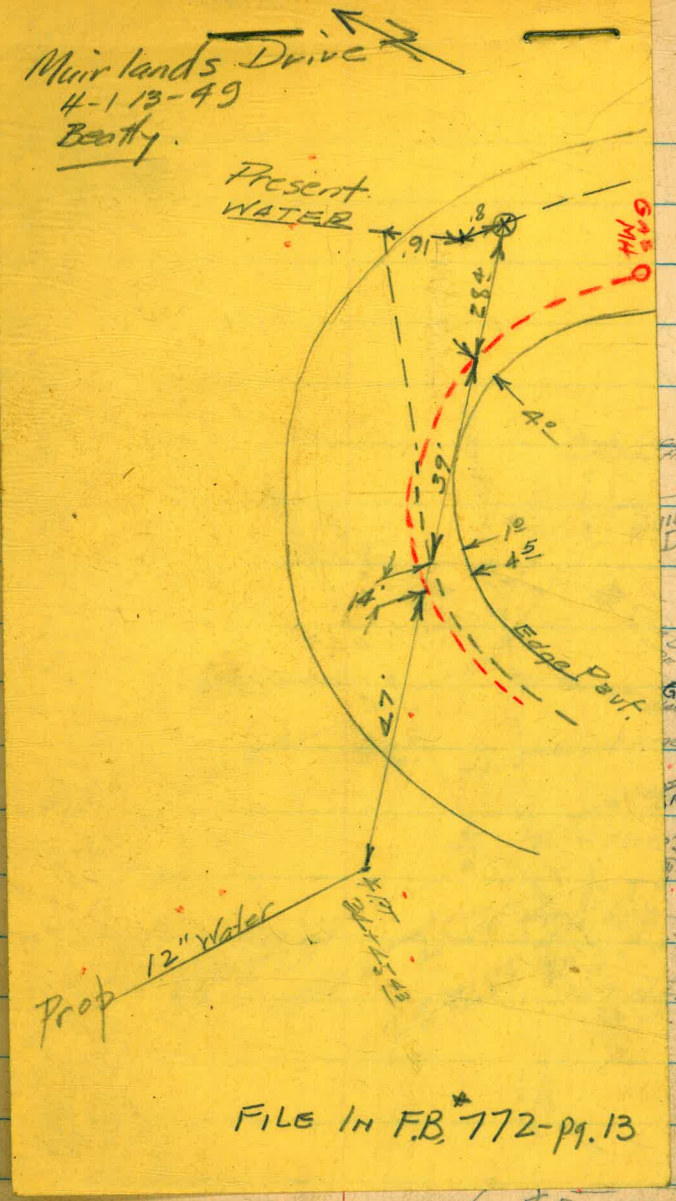
MAR. 21, 1949

& PROFILE

		398.35		
13+67			5.7	392.7
P	0.43	385.97	12.81	385.54
14+00			5.9	380.1
P	0.66	373.88	12.75	373.22
+25			2.0	371.9
+50			8.4	365.5
+69			12.1	361.8
+88			18.2	355.7
+95			21.3	352.6
15+00			24.3	349.6
+20			28.8	345.1
+29			30.5	343.4
+32			30.0	343.9
+40			28.5	345.4
+50			24.5	349.4
+85			9.4	364.5
16+00			4.0	369.9
P	12.65	386.44	0.09	373.79
+21			9.7	376.7

13.

Muirlands Drive
4-13-49
Beatty.



FILE IN F.B. 772-pg. 13

GATED finder

MUIRLANDS DRIVE

GAS EE.

POWER LINE

E PAVT.

POWER LINE

GAS EE.

"S8"

P.P. CHISS Cross on Pavt.

CONC. (PAVT.)

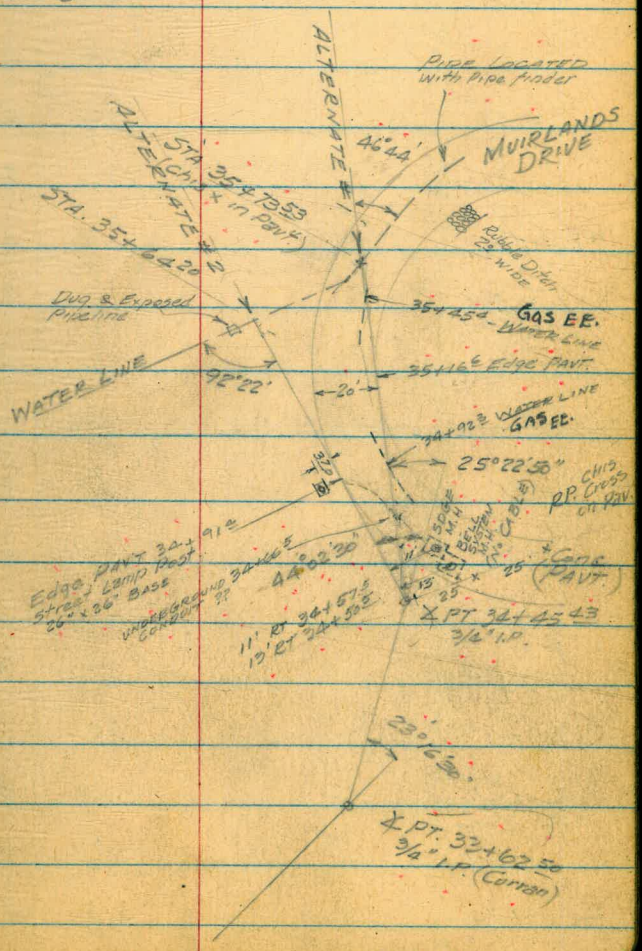
45 43

℄ PT. 32+62.50
¾" I.P. (Curran)

℄ PROFILE
398.35

13+67			5.7	392.7
P	0.43	385.97	12.81	385.54
14+00			5.9	380.1
P	0.66	373.88	12.75	373.22
+25			2.0	371.9
+50			8.4	365.5
+69			12.1	361.8
+88			18.2	355.7
+95			21.3	352.6
15+00			24.3	349.6
+20			28.8	345.1
+29			30.5	343.4
+32			30.0	343.9
+40			28.5	345.4
+50			24.5	349.4
+85			9.4	364.5
16+00			4.0	369.9
P	12.65	386.44	0.09	373.79
+21			9.7	376.7

15+78. 75. Ct.



℄ PROFILE

		386.44		
16+50			4.4	382.0
+73			1.1	385.3 ✓
PI	12.25	398.57	0.12	386.32
17+00			10.6	388.0
+30			9.0	389.6
+50			8.2	390.4
+84			7.0	391.6
18+00			6.6	392.0
+50			7.6	391.0
19+00			9.7	388.9
~~PI (at 19+00)~~	~~10.69~~	~~403.38~~	~~5.88~~	~~392.69~~ 15°LT 19+00
+21			13.0	385.6
+38			16.9	381.7
+50			21.5	377.1
+64			27.2	371.4
+69			30.2	368.4
+72			30.9	367.7
+73				
+74			34.2	364.4
+75			31.8	366.8

MAR. 21 1949
22,

℄ PROFILE
~~403.38~~
398.57

19+78			30.8	367.8
+82			28.4	370.2
20+00			18.4	380.2
+05			16.4	382.2
+25			10.5	388.1
H (on old hub)	10.69	403.38	5.88 ~~12.56~~	392.69
H. (Rock)	12.64	403.46	12.56	390.82
+35			13.2	390.3
+50			10.8	392.7
+75			7.5	396.0
+89			4.6	398.9
21+00			4.1	399.4
+35			5.3	398.2
+50			4.1	399.4
+60			5.0	398.5
P (Rock)	5.60	408.06	1.00	402.46
88 +38			8.2	399.9
22+00 ~~+50~~ +19 +69			7.5	400.6
			6.6	401.5

See Revised Yellow Slip 6-15-49 L.E.

Set TBM

22+49 43

+90

P (Rock)

23+00

+25

+40

+56

+73

+81

+92

24+00

+09

+50

+68

25+00

P

+13

+23

5.8	389.1
6.2	388.7

15.

June 1949

Profile Sta. 22+88 to Sta. 25+00

MUIRLANDS Drive

H. 393.95
1.04
N. 394.99

Station	Rod	℄ Elev.	Cut
22+88	– 0.6	394.4	– 1.9
23+00	– 2.2	392.8	– 1.9
+25	– 6.5	388.5	–
+50	– 9.5	385.5	– 0.4
+66	– 11.5	383.5	
+81	– 12.3	382.7	
24+00	– 11.5	383.5	– ℄ 1.3
+33	– 9.1	385.9	
+50	– 8.8	386.2	– ℄ 1.8
25+00	– 8.7	386.3	– 2.4
25+50	–	385.6	– 2.3
26+00		385.1	– 2.4
26+25		384.4	– 1.8
26+50		382.8	– 2.4
27+00		379.3	– 2.6

19+35 dropped 1.5

REVISED 6-15-49

MAR. 21 1949
22,

℄ PROFILE

19+78			30.5	367.8
+82			28.4	370.2
20+00			18.4	380.2
+05			16.4	382.2
+25			10.5	388.1
P (on old hub)	10.69	403.38	5.88 ~~12.56~~	392.69
P. (Rock)	12.64	403.46	12.56	390.82
+35			13.2	390.3
+50			10.8	392.7
+75			7.5	396.0
+89			4.6	398.9
21+00			4.1	399.4
+35			5.3	398.2
+50			4.1	399.4
+60			5.0	398.5
P (Rock)	5.60	408.06	1.00	402.46
88 +38			8.2	399.9
~~22+00~~ ~~+50~~ +19			7.5	400.6
+69			6.6	401.5

See Revised Yellow Slip 6-15-49 EE.

℄ PROFILE

408.06

Set TBM			3.78	404.28	3/4" I.P.in 15' Lt 21+95±
22+49 43 (± DT.)			8.3	399.8	
+90			12.9	395.2	
P (Rock)	0.25	395.41	12.90	395.16	
23+00			1.8	393.6	
+25			5.2	390.2	
+40			6.5	388.9	
+50			8.1	387.3	
+73			11.9	383.5	
+81			12.2	383.2	
+92			11.8	383.6	
24+00			10.5	384.9 ~~385.9~~	A.R.
+09			9.4	386.0	
+50			7.3	388.1	
+68			7.0	388.4	
25+00			7.2	388.2	
P	4.73	394.87	5.27	390.12	
+13			5.8	389.1	
+23			6.2	388.7	

See Revised Yellow Slip 6-15-49 EE.

3/22/49

		℄ PROFILE 394.87		
25+30			7.4	387.5
+50			7.31	387.6
26+00			8.0	386.9
+25			8.6	386.3
+50			10.8	384.1
TP (BCH)	1.47	384.15	12.19	382.68
27+05			4.5	379.7
+25			5.5	378.7
+50			7.8	376.4
TP (BCH)	0.41	371.60	12.96	371.19
28+00			2.2	369.4
+25			5.2	366.4
+30			6.6	365.0
+50			10.3	361.3
+56			11.3	360.3
+57			12.7	358.9
+59			12.2	359.4
+85			13.5	358.1
TP	1.23	359.94	12.89	358.71

See Revised Yellow Slip 6-15-49 EE

		℄ PROFILE 359.94		
29+00			3.4	356.5
29+05.46 (℄ PT.)			4.4	355.5
+20			6.6	353.3
TP (BCH)	0.07	347.23	12.78	347.16
+50			1.5	345.7
+60			4.5	342.7
+77			11.3	335.9
TP	0.08	335.33	11.98	335.25
+90			4.8	330.5 A.R. ~~329.5~~
30+00			9.3	326.0
TP	0.33	323.20	12.46	322.87
TP	0.89	311.46	12.63	310.57
+50			9.4	302.1
TP	0.25	298.81	12.90	298.56
+80			11.6	287.2
31+00			18.1	280.7
+06			20.1	278.7
+25			20.9	277.9
+42			19.8	279.0

Mar. 23, 1949
Same Party

℄ PROFILE
298.81

TP (Rock)	10.32	296.98	12.15	286.66	1.5' LT. STA 30+75±
+45			22.0	275.0	
+52			21.6	275.4	
+52			21.3	275.7	
+53			17.9	279.1	
+65			12.9	284.1	
+67			11.4	285.6	
+70			11.0	286.0	
+71			10.8	286.2	
+76			7.4	289.6	
TP (Rock)	12.27	309.01	0.22	296.74	
+95			11.6	297.4	
32+00			10.6	298.4	
+24			3.7	305.3 ~~295.3~~	A.R.
+26			2.3	306.7	
+31			1.5	307.5	
+32			0.5	308.5	
TP	10.18	319.10	0.09	308.92	
32+54.67 (℄ PT.)			2.0	317.1	
SET. TBM	12.77	329.87	2.00	317.10	Top 3/4" LP

℄ PROFILE
329.87

TP (Rock)	12.01	341.87	0.01	329.86	
33+00			4.2	337.7	
TP (Rock)	12.34	353.94	0.27	341.60	
+23			4.9	349.0	
TP	11.60	364.98	0.56	353.38	
+50			2.4	362.6	
TP	12.19	377.07	0.10	364.88	
33+62.50 (℄ PT.)			8.0	369.1	
TP	12.32	388.99	0.40	376.67	
34+00			0.2	388.8	
TP	12.77	401.72	0.04	388.95	
+08			8.7	393.0	
TP	12.82	412.89	1.65	400.07	
+29			10.2	402.7	
+42			0.6	412.3	
on ℄ PT Set TBM	10.46	423.14	0.21	412.68	3/4" I.P. Lot 13.2
34+45.43 ℄ PT.			10.5	412.6	
+58	on ALTERNATE #2		9.0	414.1	
+91.2			7.01	416.1	on Conc Post
CK 13.N1	BR. PIN IN LAMP POST STD. Between Lots 1 & 2		4.63	418.51	C.I.T.V. = 418.98

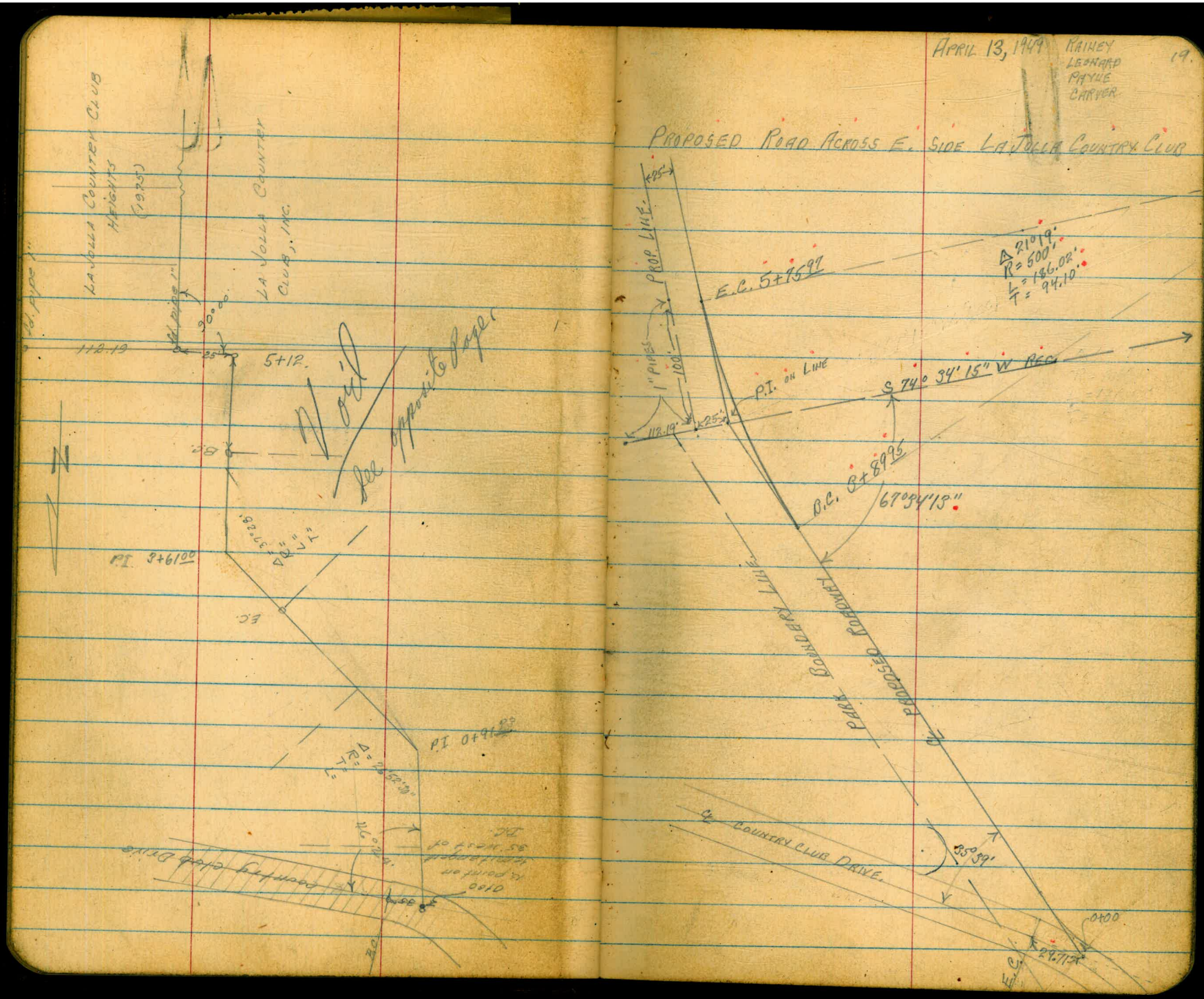
MAY 31, 1929.

		423.14			
35+00			6.4	416.7	
+32			5.3	417.8	
P.I.	3.94	414.18	12.90	410.24	
35+64.20	Top of Pipe		8.16	406.02	Approx 42% grade on pipe
35+64.30	(End)		5.6	408.6	
P.I.	12.90	423.14	3.94	410.24	edge Conc.
34+61.5	on ALTERNATE #1		9.16	413.98	Pavt
34+80.9			8.36	414.78	℄ Conc Pavt
35+16.6			6.68	416.46	edge Conc. Pavt
35+62.6			2.39	420.75	℄ Conc Pavt
35+73.53	(End)		1.51	421.63	Chis X on Pavt
BM	0.30	418.81		418.51	
	Rim STORM M.H.			5.84	
	Bottom Conc Box	(4E x 6E)		13.00	
	Rim Bell System M.H.			5.90	
	Bottom Conc. Box	(4E x 6E)		13.25	
P.I.	1.01	407.02	12.80	406.01	
P.I.	0.73	395.09	12.66	394.36	
P.I.	0.83	383.04	12.88	382.21	
CK BM	Pg Pin Lamp Post Std El Camino Del Teatro & Muirlands Drive		10.23	372.81	C.I. = 373.40 Adj. 0.59

REVISED PROFILE 0+00 to 1+84

	6.50	399.79	3.25	393.29	page 10 SE Cor. Grid
				396.54	NAIC
0-00.87	3' E of SE Cor		11.3	388.5	
0+05			11.3	388.5	
0+06			7.2	392.6	
0+50			8.6	391.2	
1+00			8.0	391.8	
1+50			5.8	394.0	
1+84.21			5.05	394.74	= 394.7 pg. 10

PROPOSED ROAD ACROSS E. SIDE LA JOLLA COUNTRY CLUB

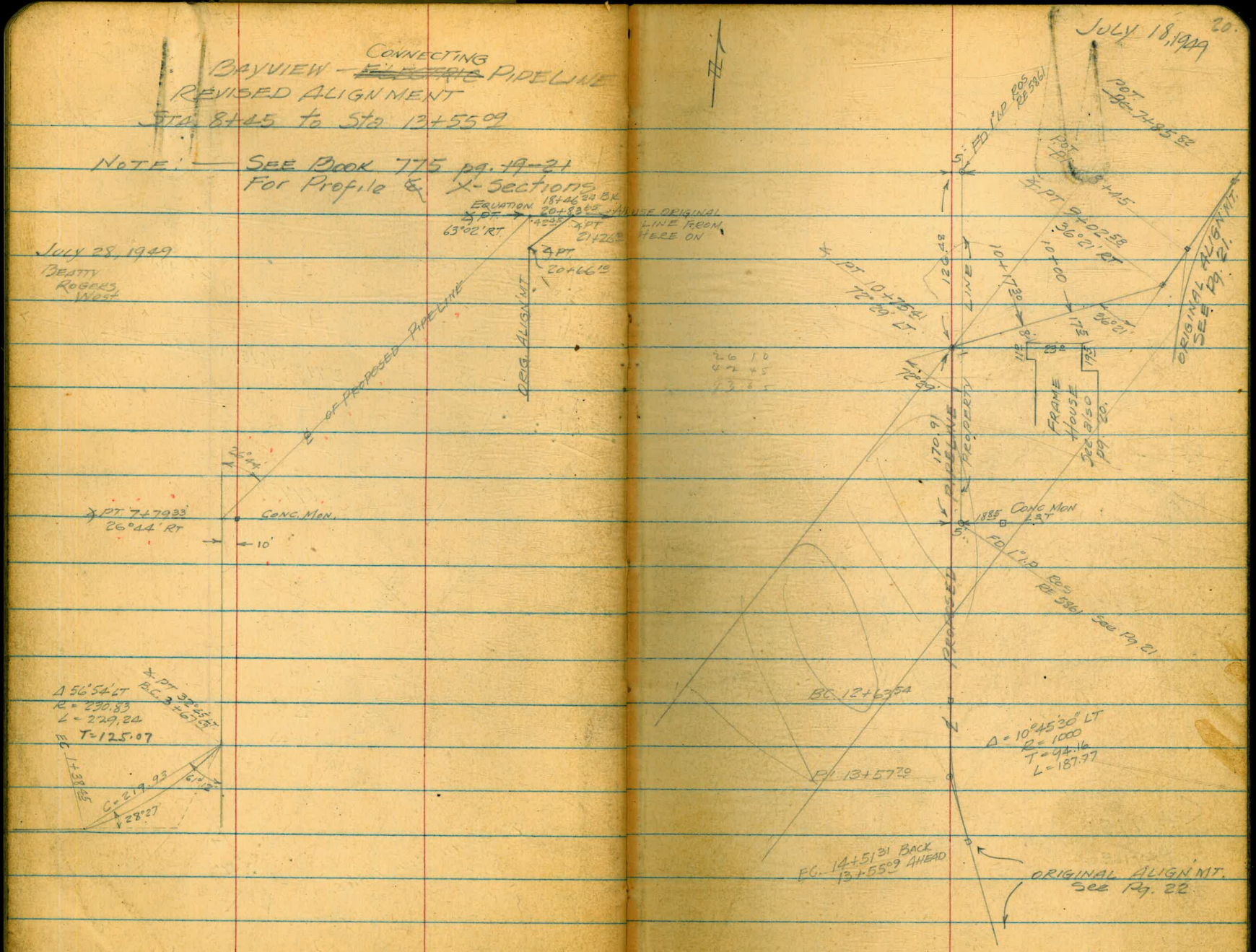


JULY 18, 1949

BAYVIEW – CONNECTING ~~ELECTRIC~~ PIPELINE
REVISED ALIGNMENT
STA. 8+45 to Sta 13+55.09

NOTE:— SEE BOOK 775 pg. 19-21 For Profile & X-Sections

JULY 28, 1949
BEATTY
ROGERS
WEST



PROPOSED PIPELINE SURVEY
FROM BAY VIEW RESERVOIR SITE TO CONNECTING ELECTRIC AVE PIPELINE

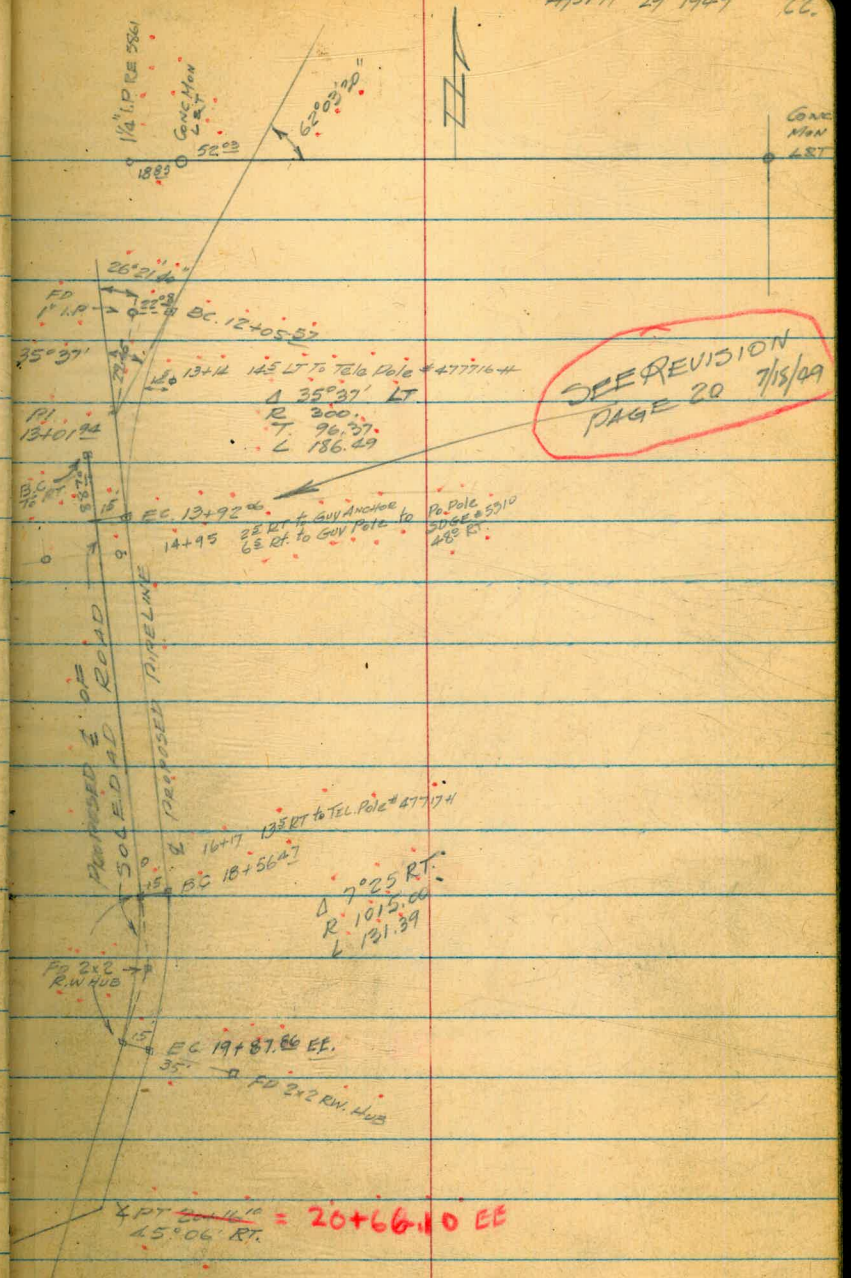
REVISED MAY 10, 1949

April 28, 1949 21
BEATTY
BAKER
ROGERS
MAY 9 1949
REV.

BAY VIEW RESERVOIR SITE

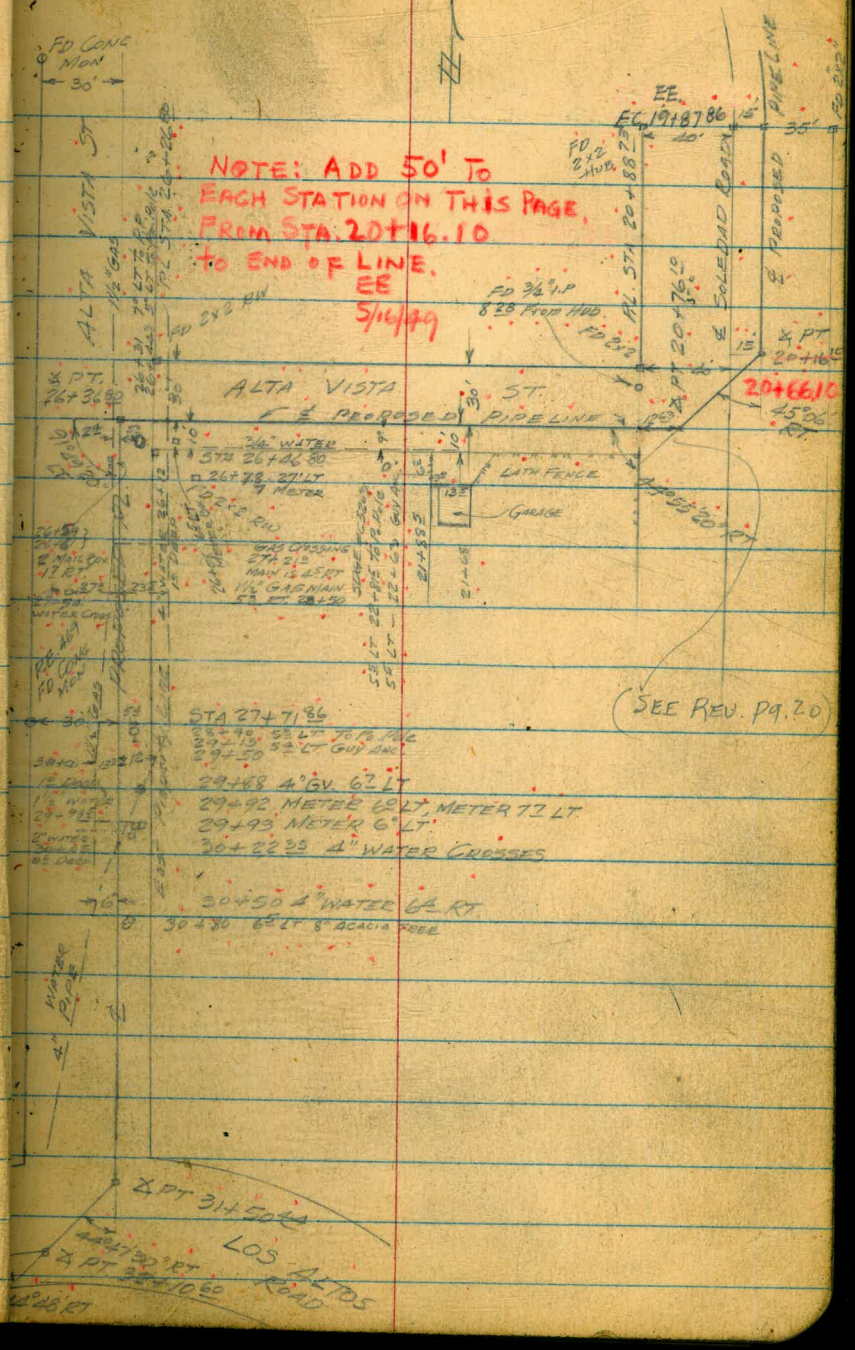
Begin Pipeline at Reservoir 0-25.55
0+00
0+94.49
1+38.45
1+77.50
1+77.50
3+25
3+49
3+47.5
3+25
3+38.5
1+20.35
64°58'30" LT.
14°36' RT.
RESERVIOR PROPERTY SITE
FD 2x2 Prop Cor
FD 2x2
B.W. FENCE P.L.
484.04
569.19
FD Conc Mon
D.C. 7+85.52
P.I. 8+45
Δ = 11°16'30" LT
R = 600
T = 59.18
L = 118.07
See Revision 7/18/49 Page 20
55° RT. to Centerline of Curve Tree
9 Pkt. 2 Spikes
10 Lds. 9 FT. 85
10+39
2-Story Frame House
FD Conc Mon
See F.B. 775 For Profile
P.I. 5+20
Δ = 20°
R = 600
T = 105.62
L = 209.22
584.17
490.23
172.94
L1°38'30"
Conc Mon L&T
3"φ Pipe
3+40 (N 44° W)
3+40.35
Pipe
2"φ Pipe
Δ = 50°22'40" LT
PROPOSED PIPE LINE
VOID
SEE SKETCH BELOW FOR REVISION
P.C. 7+85.52
P.I. 8+45
E.C. 9+03.57
C2°09'30"
Δ = 11°16'30" LT
R = 600
T = 59.18
L = 118.07
1+39.27 Int. W. #1 P.L.
52.03
Conc Mon L&T
1½" I.P. Rose see Sec.
476.89
BEGIN PIPE LINE 0+17.13
1+37.13
Fd Hub M&D Prop Cor
177.22
325
B.W. FENCE 3+79.10 P.L. STA 3+83.70
484.04
480.34
Conc Mon L&T
4PT 5+13.43
50°22'40" LT

CONNECTING BAYVIEW – ~~ELECTRIC~~ AVE PIPELINE



CONNECTING
BAYVIEW-ELECTRIC AVE PIPELINE

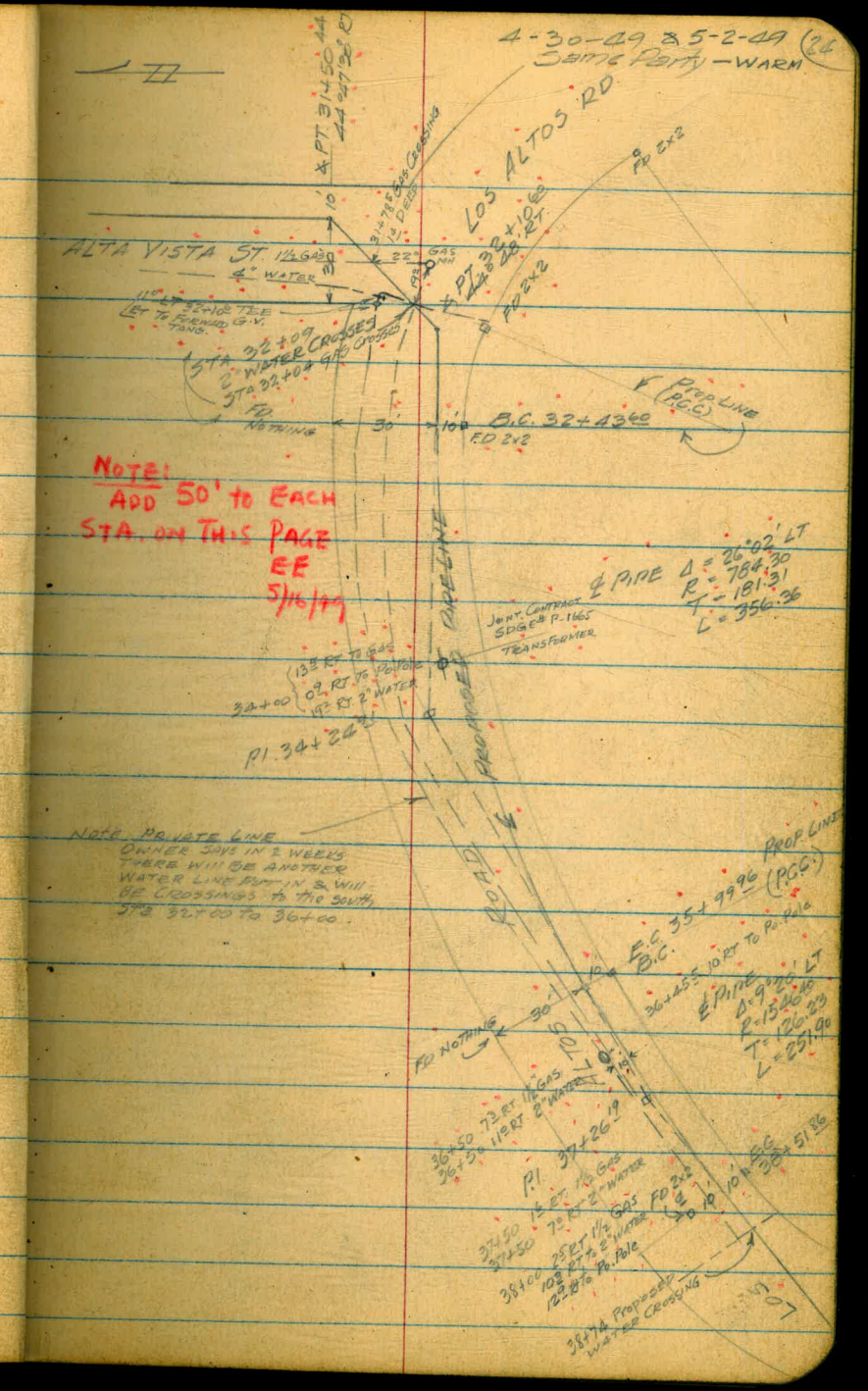
4-29-49
4-30-49



CONNECTING
BAYVIEW – ELECTRIC AVE PIPELINE

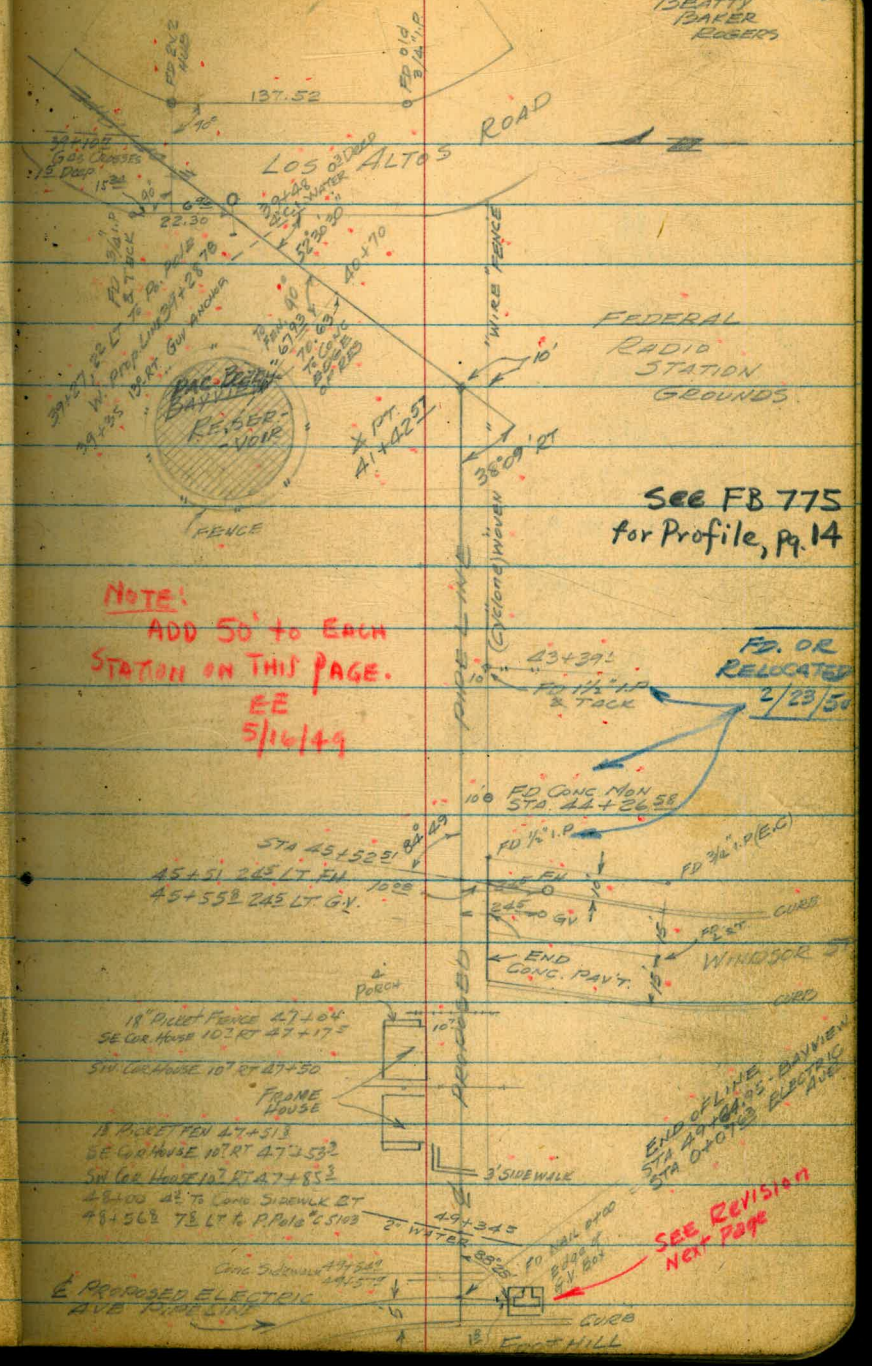
4-30-49 & 5-2-49 (26
Same Party – WARM

II



MAY 6 1949
BEATTY
BAKER
ROGERS
25

CONNECTING BAYVIEW – ELECTRIC AVE PIPE LINE



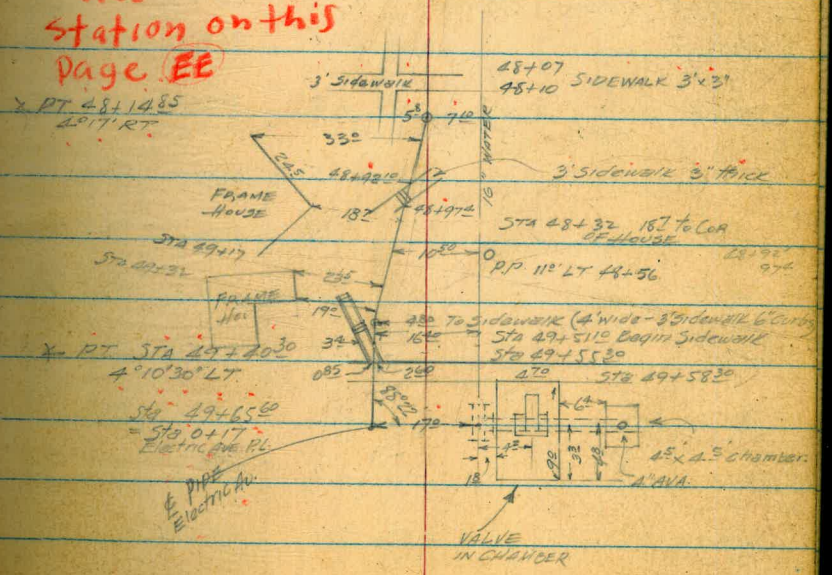
July 11, 1929

REVISED ALIGNMENT - BAYVIEW ELECTRIC CONNECTION

P on	Use 6.21 +50	201.62		195.41	BK 775 pg 17
48+14.85	48+65		+0x8	202.4	
+50	49+00		0.9	200.7	
orig 48+50) CK			(1.1	200.5	= 200.4
+88	49+38		6.4	195.5	
+89	49+39		6.9	194.7	
+92.10	49+42 Sidewalk		7.00	194.62	
+96±	49+46.4 Top step		7.21	194.41	
+96±	Bot. 49+46±		7.71	193.91	
+97±	Sidewalk 49+47±		7.84	193.78	
49+00	49+50		8.2	193.4	
P	0.91	189.71 ✓	12.82	188.80 ✓	
+30	49+80		3.2	186.5	
+33	49+83		4.7	185.0	
+37	49+87		4.6	185.1	
+40.30	49+90	F	6.1	183.6	
+43			7.9	181.8	
+46	49+96		8.4	181.3	
+51.10	Sidewalk 50+01		10.55	179.16	
+58.30	"		10.50	179.11	
49+65.60	50+15.60		10.95	178.76	
CK orig 49+64.95			11.30	178.40 = 178	
			14.90		

7-11-29 26

NOTE! Add 50' to each station on this page EE



JUNE 14, 1949
Beaty
Baker
Rogers

GRADES SET MIDLANDS PIPELINE

					I.P.N 15 LT 71+
TBM	2.33	406.61		404.28	
IP	2.62	396.57	12.66	393.95	
IP	0.70	385.07	12.20	384.37	
IP	0.34	373.06	12.35	372.72	
IP	0.26	360.84	12.48	360.58	
IP	6.93	354.72	13.05	347.79	
SET. TBM			5.84	348.88	ROCK
29+50			10.2	344.5	341.6 C29
+05.49	& Ot		0.5	354.2	351.2 C30
IP 29+00	12.46	367.10	0.08	354.64	352.4 C22
+63			8.4	358.7	355.6 C31
28+50			6.6	360.5	357.5 C30
IP	11.85	378.67	0.28	366.82	
28+00			10.6	368.1	365.1 C30
+50			4.3	374.4	372.6 C18
IP	11.92	389.72	0.87	377.80	
27+00			10.5	379.2	376.6 C24
+50			6.9	382.8	380.4 C24
+25			5.4	384.3	382.5 C18
26+00			4.6	385.1	382.7 C24
+50			4.2	385.5	383.2 C23
25+00			3.7	386.0	383.6 C24
+50			3.8	385.9	384.1 C18
24+00			6.5	383.2	384.5 F13

6/14/49

GRADES — MUIRLANDS PL.

		389.72				
23+50			4.4	385.3	384.9	C 0.4
+45			3.9	385.8	385.0	C 0.8
TP	11.49	400.52	0.69	389.03		
23+00			8.1	392.4	390.5	C 1.9
+88			6.6	393.9	392.0	C 1.9
22+49 47	℄ PT.		2.6	397.9	394.9	C 3.0
TP.	0.58	400.82	0.28	400.24		
22+30			2.5	398.3	396.4	C 1.9
22+00			2.9	397.9	396.0	C 1.9
+50			3.6	397.2	395.1	C 2.1
21+00			5.1	395.7	394.2	C 1.5
+87			5.9	394.9	394.0	C 0.9
TP						
+50	0.43	390.82	10.43	390.39	389.0	C 1.4
20+10			9.6	381.2	380.0	C 1.2
D						
20+00	7.92	386.11	12.63	378.19	375.0	C 3.2
+84			11.7	374.4	369.0	C 5.4
+58			12.4	373.7	369.0	C 4.7
+35			6.2	379.9	380.0	F 0.1
TP	12.33	398.27	0.17	385.94		
19+00			12.0	386.3	385.0	C 1.3
+50			8.8	389.5	386.6	C 2.9
18+00			8.1	390.2	388.2	C 2.0

393.9

396.0 -

Rev. Grade

378.5 C 1.4

6/14/49

GRADES — Muirlands PL.

		398.27			
17+50			9.5	388.8	386.1 C 2 7
17+00			12.0	386.3	384.0 C 2 3
SET. TBM			8.25	390.02	HUB 15' LT 16+80±
P	10.78	406.55	2.50	295.77	
CK TBM			2.23	404.32	= 404.28

GRADES SET JUNE 20, 1949

TBM	0.68	390.70		390.02	HUB 15' LT 16+80±
17+00			4.6	386.1	384.0 C 2 1
+50			10.6	380.1	378.2 C 1 3
II	1.61	381.68	10.63	380.07	
+25			6.7	375.0	373.2 C 1 8
II	0.49	369.83	12.34	369.34	
16+00			1.5	368.3	365.0 C 3 3
+70			12.4	357.4	355.0 C 2 4
II	0.57	358.05	12.35	357.48	
+40			10.0	348.1	340.0 C 8 1
15+15			10.8	347.3	340.0 C 7 3
14+80			1.6	356.5	355.0 C 1 5
II	12.17	369.33	0.89	357.16	
+63			8.1	361.2	359.0 C 2 2
+50			4.7	364.6	362.5 C 2 1
II	11.96	380.95	0.14	369.19	
14+00			0.6	380.4	376.0 C 4 4
II	12.11	392.42	0.64	380.31	
+75			3.1	389.3	387.0 C 2 3

377.5

6-14-49

GRADES — Muirlands PL.

TP	11.70	392.47 403.94	0.18	392.24	
13+50			5.9	398.0	393.6 C 4.4
TP	10.97	414.62	0.29	403.65	
13+00			3.9	410.7	406.8 C 3.9
TP	12.19	426.72	0.09	414.53	
+50			8.5	418.2	414.4 C 3.8
+25			5.8	420.9	418.2 C 2.7
12+00			3.4	423.3	420.4 C 2.9
TP	1.20	427.57	0.35	426.37	
CK TBM (Conc Mon)			0.67	426.90	= 426.97

REVISED & ADDITIONAL GRADES SET 6/22/49

15+75	359.4	355.8 C 3.6	
15+58.3	353.4	348.8 C 4.6	
15+00	350.4	344.2 C 6.2	Note: CUT TO 342.6
14+83.3	355.5	351.2 C 4.3	" " 350.2
14+66.3	360.6	357.2 C 3.4	" " 356.5
14+49 ± 99' ?	365.0	362.5 C 2.5	
14+36	369.3	366.8 C 2.5	
14+17	374.4	372.4 C 2.0	
14+00	380.4	377.5 C 2.9	
13+83	386.7	383.5 C 3.2	
13+66	392.8	389.3 C 3.5	
13+17	406.7	401.9 C 4.8	
13+00	410.7	406.0 C 4.7	
12+83	414.1	409.6 C 4.5	

JUNE 23 1949
BEATTY
ROGERS

GRADES SET — MUIRLANDS PL

TBM	7.29	436.26		496.27	
11+50			8.3		428.8 C32
+25			6.9		427.0 C24
11+00			5.9		427.7 C27
+50			4.8		429.0 C25
10+00			3.7		430.4 C27
+75			3.3		430.8 C22
+50			3.9		430.4 C20
9+00			5.8		428.0 C25
TP.	0.56	428.67	8.15	428.11	
+50			3.5	425.2	427.6 C26
CK TP			4.97	423.70	= 428.68
8+00			10.6		418.6 C25
TP	1.88	417.60	12.95	415.72	
+50			6.5	411.1	409.2 C19
7+00			12.7		403.0 C19
TP	0.51	405.46	12.65	402.95	
+50			7.0		396.4 C21
6+00			13.2		390.0 C23
TP ROCK			9.19	396.27	

6-22-69

GRADES SET Muirlands PL

PI	0.10	396.37		396.27	
5+86			5.9	390.5	388.0 C25
+67			8.0	388.4	385.1 C33
+50			10.9	385.5	381.7 C38
PI	0.92	386.43	10.86	385.51	
+33			4.8	381.6	377.8 C38
+14			9.3	377.1	371.0 C61
5+02			10.4	376.0	371.0 C50
4+50			3.4	383.0	381.0 C32 ✓ NG
4+00			2.9	383.5	381.1 C24
3+63			2.9	383.5	381.2 C23
PI	12.06	395.57	2.92	383.51	
3+38			9.8	385.8	382.2 C36
3+00			4.9	390.7	387.3 C34
PI	5.03	399.70	0.90	394.67	
2+50			3.9	395.8	394.2 C16
2+30			3.9	395.8	394.7 C11
2+13			4.6	395.1	394.0 C11
1+84.41	2 PT		6.3	393.4	391.8 C16
+50			7.6	392.1	389.6 C25
1+00			9.6	390.1	388.0 C21

GRADES SET Muirland P.L.

399.70

0+50		9.8	389.9	387.3 C 2.6
0+00		11.2	388.5	386.7 C 1.8
0-20.12		13.49	386.21 = TEE IN PLACE	386.50 = PLAN

12.18
1.31
13.49

July 5 1929
BEATTY
ROGERS
WEST

7/5/29 34

MUIRLANDS P.L.

ELEVATIONS TOP OF 12" C.I. PIPE IN PLACE (See also Note page 30.)

PI	0.77	390.79		390.02	pg 29
PI	0.03	378.06	12.76	378.03	
PI	0.52	366.87	11.71	366.35	Bot Pipe
PI	0.00	354.29	12.58	354.29	
15+16			13.4	340.9	339.8
15+39			13.4	340.9	339.8
15+58.3			4.6	349.7	348.6
PI	12.05	366.34	0.00	354.29	
15+75			9.7	356.6	355.5
PI	10.14	376.48	0.00	366.34	
16+00			11.1	365.4	364.3
+25			3.9	372.6	371.5
PI	11.46	387.24	0.70	375.78	
+50			9.4	377.8	376.7
17+00			2.5	384.7	383.6
PI	6.62	392.76	1.10	386.14	
+50			5.7	387.10	386.0
+96			4.0	388.8	387.7
18+00			3.9	388.9	387.8
+50			4.9	387.9	386.8
19+00			7.5	385.3	384.2

(Cont'd)

392.76

19+35			13.1	379.7	378.6
PI	0.11	379.95	12.92	379.84	
19+59			9.9	370.1	369.0
19+87			10.0	370.0	368.9
20+00			4.2	375.8	374.7
PI	11.99	390.60	1.34	378.61	
+11			9.4	381.2	380.1
+50			1.2	389.4	388.3
PI	12.52	402.12	1.00	389.60	
20+87			7.8	394.3	393.2
21+00			6.7	395.4	394.3
+50			6.0	396.1	395.0
22+01			5.1	397.0	395.9
+26			5.1	397.0	395.9
+30			5.1	397.0	395.9
+48.43			6.6	395.5	394.4
+88			10.9	391.2	390.1
23+00			12.4	389.7	388.6
PI	2.30	391.99	12.43	389.69	

ELEV.'S TOP 12" C.I. PIPE IN PLACE (CONT'D)

		391.99		
23+17	4.6	387.4	386.3	
+38	7.6	384.4	383.3	
+50	8.6	383.4	382.3	
+59	9.2	382.8	381.7	
+85	9.6	382.4	381.3	
24+00	9.8	382.2	381.1	
CK. (45) HD)	8.79	383.20	= 383.20 pg. 27	

GRADES SET — MUIRLANDS P.L.

H.I.	3.06	351.94		348.88	pg. 27
CK 29+50			7.44	344.5 =	344.5 pg 27
29+60			11.3	340.6	337.4 C3
H.I. Bob	0.25	340.02	12.17	339.77	
+77.4			5.6	334.4	330.2 C4
+93.9			12.0	328.0	323.0 C5
H.I. Bob.	0.07	327.68	12.41	327.61	
30+10			6.5	321.2	315.7 C5
H.I. Bob	0.51	315.27	12.92	314.76	
+27			1.8	313.5	308.3 C5
+43			9.9	305.4	300.5 C4
H.I. Bob	0.44	303.07	12.64	302.63	
+59			6.1	297.0	292.0 C5
H.I. Bob	0.76	291.12	12.69	290.38	
+76			2.7	288.4	283.4 C5
+94.7			9.9	281.2	279.0 C2
31+12			14.3	276.8	275.5 C1
+30			14.0	277.1	272.0 C5
+55	offsets: (45) — EAST, WEST		12.0	279.1	272.0 C7
			9.5	281.6	272.0 C6
+72			4.6	286.5	280.5 C6
H.I. Bob	18.79	303.60	0.33	290.81	
+88			9.6	294.0	287.8 C2
32+05			4.3	299.3	294.8 C5
H.I.	12.72	316.24	0.68	303.52	
+22			11.2	305.0	301.0 C4
+39			5.0	311.2	306.8 C4
H.I.	11.61	327.80	0.05	316.19	
32+54.67	(4 PT.)		10.6	317.2	313.6 C3
CK TBM on 3/4" I.P.			10.61	317.19	= 317.10 pg 17

7/6/49

GRADES SET — MUIRLANDS PL.

	12.11	327.80 339.79	0.12 10.7	327.68 329.1	325.9	C32
32+83						
33+00			2.3	337.5	334.0	C35
PI.	12.35	352.04	0.10	339.69		
+17			6.3		341.7	C40
PI.	11.50	363.39	0.15	351.89		
+50			0.7	362.7	359.0	C37
PI. Top Stk	9.89	373.16	0.12	363.27		
+62.5	(& PT)		3.9	369.3	365.6	C37
CK & PT STA.			4.08	369.08	= 369.10	
SET PI STK	12.06	383.21	2.01	371.15		
+83			3.4	379.8	376.3	C35
PI	12.26	395.36	0.11	383.10		
34+00			7.0	388.4	384.0	C41
PI.	11.00	405.51	0.85	394.51		
+17			8.2	397.3	392.1	C52
+32			1.3	404.2	399.0	C52
PI	11.19	415.94	0.76	404.75		
CK TON			3.15	412.79	= 412.68	
+45.43	& PT	22½° Spec	3.7	412.2	405.1	C72
+54	(22½° Spec)		2.1	413.8	409.1	C47
+70	(on point)		1.2	414.7	410.2	C45
PI Rock	8.13	423.23	0.84	415.10		
35+00			7.2	416.0	412.3	C37
+25			5.6	417.6	414.1	C35
+58			2.7	420.5	416.4	C42
CK BM			4.59	418.64	= 418.51	= 418.93
					pg. 17	City BM.

July 21 1949

MURLANDS PIPELINE

ELEVATIONS TAKEN ON TOP 12" C.I. PIPE

BM.	0.39	419.03 ✓		418.64	Jeepa 37
34+61.80	at edge of Pavt.		8.6	410.4	Bot. Pipe 409.3
+55.65			8.9	410.1	409.0
+53	(Top 11¼° Bend)		9.4	409.6	408.5
+46	(℄ PT Top 22½° Bend)		11.5	407.5	406.3
P	6.22	413.54 ✓	11.71	407.32 ✓	
+30.32			12.5	401.0	399.8 ✓
P	0.04	401.17 ✓	12.41	401.13 ✓	
+05.32			0.0	389.3 ~~401.2~~ ?	388.1 ✓
P	0.42	389.32 ✓	12.27	388.90 ✓	
P	0.34	377.36 ✓	12.30	377.02 ✓	
30+78.74			1.6	375.8	374.5 ✓
+61.86	(℄ PT Top 22½° Bend)		10.8	366.6	365.3
P	3.50	368.12 ✓	12.74	364.62 ✓	
+40.03	(So. edge bulkhead)		12.80	355.32	354.1 ✓
P	0.00	355.68 ✓	12.44	355.68 ✓	
+16.03			12.2	343.5	342.3
P	0.16	343.34 ✓	12.50	343.18 ✓	
33+00			7.4	335.9	334.7

Elevation Taken on Top of 12" C.I. Pipe (Cont'd.)

		343.34			
PI	0.88	331.50 ✓	12.72	330.62 ✓	
32+83			3.6	327.9	326.7
32+68			10.5	321.0	319.8
PI	0.97	319.77 ✓	12.70	318.80 ✓	
32+53.58	℄ PT		5.2	314.6	313.4 ✓
+45.78	(So. edge bulkhead)		7.4	312.4	311.2
+34.75			13.35	306.4	305.2 ✓
PI	0.61	307.41 ✓	12.97	306.80 ✓	
+23.50			5.3	302.1	300.9 ✓
+06.41			11.0	296.4	295.2 ✓
PI	0.50	294.86 ✓	13.05	294.36 ✓	
31+87.87			3.94	290.9	289.7 ✓
+70.99			12.4	282.5	281.2 ✓
PI	1.86	284.36 ✓	12.36	282.50 ✓	
+54	Top 22½° Bend		10.9	273.5	272.4
+35.50	Top 12"x6" Cross		11.3	273.1 ✓	272.0
+29.30	Top 11¼° Bend		11.3	273.1 ✓	272.0
PI	4.00	288.76 ?	0.00	284.36 ✓	
OK. ℄ 30+76.20			0.40	288.36 =	288.40 − 129.36

Oct. 3 1949
Beatty
Rogers
Finney

Const. Grades Set — Bayview Connecting P.L.

B.M.	11.95	173.32		161.37	Top F.H. Fanuel at Tourmaline	
T.P.	12.62	185.35	0.59	172.73	GRADE CUT	
OK TBM	Top. F.H. Foothill @ Tourmaline		5.86	179.49	= 179.47	
50+03.67	Begin Work		4.6	180.8	172.4	C8
50+00			3.8	181.6	172.4	C9
49+95.64			2.9	182.5	174.1	C8
+90.16			1.2	184.2	176.0	C8
T.P.	12.07	197.30	0.12	185.23		
+60.14			7.3	190.0	185.2	C4
T.P. +29.50	11.25	208.53	0.02	197.28	191.8	C5
49+00.00			7.2	201.3	196.0	C5
+98.54			7.1	201.4	196.0	C5
+67.04			5.6	202.9	196.2	C6
+35.61			6.0	202.5	196.7	C5
48+04.11			6.2	202.3	197.0	C5
47+72.67			5.3	202.2	198.7	C4
+41.23			2.4	206.1	200.7	C5
T.P.	11.64	219.81	0.36	208.17		
+10.85			10.3		203.5	C6
~~+07.73~~					~~203.8~~	
+05.00			8.6	211.2	205.1	C6
T.P. +03.95			8.5	211.3	203.5	C5
	12.46	232.10	0.17	219.64		
46+75.39			11.8	220.3	218.8	C1
46+65.63			4.7	227.4	223.3	C4

6.1 = 179.25

179.47 BM
10.46
189.93 Ni

Top
12.1 = 177.83 175.71

2.9 = 187.03 184.91

.0.4.

CK
10/14/49

✓
✓
✓
✓
✓
✓

10-3-49

CONST. GRADES SET — BAYVIEW CONNECTING P.L.

			232.10		GRADE CUT			
11+46+62				2.7	229.4	225.0 C44	(C32 Replaced) ✓	
+58 40				2.1		225.0 C50	✓ ✓	
+26 90				1.9		225.3 C49	✓ ✓	
P +04 48	2.15	234.02		0.23	231.87	225.5 C69	✓	
11+46+00				1.7		225.5 C68	(69 Replaced) 26.90	25.5
+96 54				0.9		227.5 C54	(C86 Replaced 31.50 5.40	6.4 31.9
P Top FH.	10.72	242.81		1.93	232.09		SET OCT. 4 1949	2.8
+69 32	12.25	254.76		0.30	242.51			34.7
				8.5	246.3	240.2 C61	✓	25.5
P.	11.96	266.66		0.06	254.70			C 9.2
+37 80				11.31	255.4	249.4 C62	✓	25.5 6.4 31.9
+07 38				4.0	262.7	257.6 C51	✓	4.2 36.1
P.	12.03	278.24		0.45	266.21			27.5
11+44+76 69				6.7	271.5	264.2 C73	✓	C 8.6
+47 09				3.3	274.9	268.0 C69	✓	
+14 20				4.0	274.2	268.1 C61	✓	
10+83+68				4.6	273.6	268.7 C49	✓	
+51 28				3.0	275.2	271.1 C41	✓	
+19 84				1.4	276.8	273.1 C37	✓	
P.	12.70	290.91		0.03	278.21			
10+88 40				10.8	280.1	275.3 C48	✓	
+57 25				6.2	282.7	280.0 C47	✓	
P.	12.09	302.17		0.83	290.08			
+26 51				10.0	292.2	286.9 C53	✓	
D.	10.87	312.44		0.60	301.57			
9+95 93				12.0	300.4	294.7 C57	✓	

10-3-49

CONST. GRADES ℄ Bayview Connecting P.L.

					REV. ℄ PROFILE Rec.	El.	REVISED GRADES		10/14/49
41+89.33 ℄ PT.	312.44				10.3	302.1			
41+88.69		11.7	300.7	296.5 C42	10.2	302.2			✓
+57.77		7.6	304.8	301.7 C31	6.0	306.4	✓		✓
+26.54		4.7	307.7	304.8 C29	3.1	309.3	✓		✓
40+95.20		3.0	309.4	305.4 C40	2.2	310.2	✓		✓
CK TP ROCK		2.48	309.96	= 309.99					
+63.70		2.9	309.5	305.2 C43	2.9	309.5	✓	(Replaced 309.3 C41)	✓
+32.21		3.7	308.7	304.2 C45	3.2	309.2	303.9 ✓	C48	✓
40+00.73		4.8	307.6	303.0 C46	4.8	307.6	302.0 ✓	C56 ✓	✓ ✓
TP 1" I.P.	4.74 31/.92	5.26	307.18						
+69.25		4.8	307.1	301.7 C54	5.0	306.9	300.3 ✓	C68 ✓	✓ ✓
+37.77		5.8	306.1	300.5 C56	6.0	305.9	298.7 ✓	C74 ✓	✓ ✓
+06.33	H.P.=0.08'	7.5	304.4	299.2 C52	7.7	304.2	297.7 ✓	C67 ✓	✓ ✓
39+01.86 EQ.									
CK TP NAIL IN POLE		12.07	299.85	= 299.87					

REVISED

King
Skipman
West

10-18-49

Const GRADES Set — Bayview Connecting R.L

						Cut	Revised Grades			
B.M.	2.55	302.40			299.85	Nail in T.P. Rt. 12'	R+3 0+47			
38+74.92			0.4	302.0	296.1	5.9 ✓	296.1		✓	10/24/49
38+43.49			3.4	299.0	293.7	5.3 ✓	293.7		✓	✓
38+11.98			6.4	296.0	291.3	4.7 ✓	291.3		✓	✓
37+80.47			8.3	294.1	290.0	4.1 ✓	290.2	C 32 ✓	✓	✓
37+48.96			9.3	293.1	289.4	3.7 ✓	290.0	C 31 ✓	✓	✓
37+17.45			9.3	293.1	288.7	4.4 ✓	289.9	C 32 ✓	✓	✓
36+85.90			9.2	293.2	288.7	4.5 ✓	289.7	C 35 ✓	✓	✓
36+54.34			8.9	293.5	289.1	4.4	289.5	C 40 ✓	✓	✓
36+22.80			8.6	293.8	289.5	4.1 ✓	289.3	C 45 ✓	✓	✓
35+91.26			8.1	294.3	289.9	4.4 ✓	289.1	C 52 ✓	✓	✓
35+59.72			7.7	294.7	290.4	4.3	288.9	C 58 ✓	✓	✓
35+28.18			7.0	295.4	290.9	4.5	288.8	C 66 ✓	✓	✓
34+96.64			6.1	296.7	291.4	4.9	288.6	C 72 ✓	✓	✓
34+65.10			5.0	297.4	291.8	5.6	288.4	C 90 ✓	✓	✓
T.P.	4.81	302.30	4.99	297.49		On Gin Hem - 34+65				
34+33.56			4.5	297.8	291.5	6.3	288.2	C 95 ✓	✓	✓
34+02.02			4.4	297.9	291.4	6.5	288.1	C 98 ✓	✓	✓
33+70.48			5.3	297.0	291.0	6.0	287.9	C 91 ✓	✓	✓

REVISED

REVISED

10/18/49

Construction GRADES Set – Bayview Connecting P.L.

302.30

						REVISED GRADES	
33 +39 94			6.3	296.0	290.7	5.3	287.7	C 8 3 ✓ ✓
33+07 40			6.7	295.6	290.3	5.3	287.5	C 8 1 ✓ ✓
32+75 89			7.4	294.9	289.9	5.0	287.4	C 7 5 ✓ ✓
TP	8.08	302.99	7.39	294.91		ON QUINNEY 32+75 86		OCT. 24 1949
	MEAS. 10 22							Beatty Rogers Finney
32+64 60			8.2	294.8	289.8	45	287.3	C 7 5 ✓ ✓
32+56 40			8.3	294.7	289.7	45	287.2	C 7 5 ✓
32+25 10			9.2	293.8	288.3	45	287.1	C 6 7 ✓
32+01 62			9.0	294.0	289.0	45	287.0	C 7 0 ✓ ✓
31+93 62 AH			9.1	293.9	289.3	45	287.3	C 6 6 ✓ ✓
31+96 44 BK								
+50			7.4	295.6	291.1	45	289.1	C 6 5 ✓ ✓
31+00			5.1	297.9	293.4	45	291.4	C 6 5 ✓ ✓
+50			2.4	300.6	295.7	49	293.7	C 6 9 ✓ ✓
TP	11.16	313.43	0.72	302.27				
30+00			10.2	303.2	298.0	52	296.0	C 7 2 ✓ ✓
+50			7.1	306.3	301.0	53	299.0	C 7 3 ✓ ✓
29+00			4.0	309.4	304.0	54	302.0	C 7 4 ✓ ✓
TP	9.02	322.21	0.24	313.19				
+50			8.6	313.6	307.0	56	304.0	C 9 6 ✓ ✓
28+00			5.3	316.9	310.0	59 ✓	306.0	C 10 2 ✓ ✓
+50			4.8	317.4	310.5	59	306.9	C 10 5 ✓ ✓
27+00			5.3	316.9	310.9	60	307.7	C 9 2 ✓ ✓
CR TBM	5.16	322.14	5.16	317.05	316.98			

REVISED

REVISED

OCTOBER 24, 1949
Beatty
Rogers
Finney

CONST. GRADES SET — Bayview Connecting P.L.

322.14

26+92.95			5.3	316.8	311.0
26+88.80 ⊥ PT.					311.0
PI NAIL IN STUB POLE	2.69	321.30	3.53	318.61	
26+83.50 ΔH			4.5	316.8	311.0
26+79.50 CK					
26+76.50			4.5	316.8	311.0
					311.0
26+69.00			4.5	316.8	311.0
+62			4.4	316.9	310.9
+50			4.1	317.2	310.7
26+00			4.8	316.5	309.7
+50			8.3	313.0	307.7
+25			9.1	312.2	307.0
25+11.51			9.4	311.9	307.0
24+79.98			9.7	311.6	307.0
+50			9.6	311.7	307.0
24+00			9.0	312.3	307.0
PI +50	8.58	322.82	7.06	316.24	308.2
CK TON			6.94	315.88	= 315.86 NAIL IN PO. POLE
23+00			6.0	316.8	309.4
+75			5.5	317.3	310.0
+50			5.3	317.5	310.3
23+00			4.7	318.1	310.8

REVISED

REVISED

	Revised Grades	
C58	307.8	C92 ✓ ✓
C58	308.0	C88
C58	308.0	C88
C58	308.0	C88
C6°	308.0	C82
C65	307.9	C93
C73	307.5	C90
C53	307.1	C59
C52	307.0	C52
C49		
C47		
C53		
C6°		
C74		
C73		
C72		
C73		

Oct. 24, 1969

Const. Grades Set — Bayview Connecting P.L.

		322.82				
21+50			4.1	318.7	311.3	C7.4
21+01.98			4.1	318.7	311.8	C6.9
TP						
20+88.41	MEAS. 3.74 (PIPE 2.72)		3.96	318.86	311.9	C7.0
TBM	9.17			315.86		
20+84.67	(X-PT)	325.03				
18+48.48					312.8	
18+41.99			6.3	318.7	312.3	C6.4
18+10.57			4.0	321.0	314.5	C6.5
17+79.12			2.3	322.7	316.3	C6.4
TP	5.88	328.83	2.08	322.95		
17+47.65			3.9	324.9	317.7	C7.2
17+16.18			2.9	325.9	319.2	C6.7
16+83.18			3.0	325.8	319.10	C6.7
16+52.06			7.7	321.1	314.7	C6.4
TP	0.29	316.15	12.97	315.86		
16+23.78			0.9	315.3	304.8	C10.5
15+94.22			9.7	306.5	293.9	C12.6
TP	0.62	302.06	12.71	303.44		
15+73.91	20.31		5.2	298.9	286.4	C12.5
15+70			6.3	297.8	285.0	C12.8
15+40			12.9	291.2	285.0	C6.7
15+06.67			2.3	301.8	297.2	C4.6
TP	12.99	316.64	0.41	303.65		
TP	12.86	329.35	0.15	316.49		
14+50			6.5	322.9	315.0	C7.9
TP	12.65	341.83	0.17	329.18		

Oct. 26, 1969

E of Pipeline after Bulldozer got thru. Benching out.

Rod	Elev.	
3.4	325.4	
8.1	320.7	
1.9	314.3	
11.9	304.3	
6.9	297.2	
7.9	296.2	
13.4	290.7	(+52)
13.1	291.0	
1.4	302.7	
6.4	323.0	

October 26, 1949

Const. Grades Set — Bayview Connecting P.L.

		341.83			
14+00			11.9	329.9	325.3	C46
13+50			3.4	336.4	332.7	C57
P.I.	12.29	354.00	0.12	341.71		
13+00			9.2	344.8	340.1	C47
P.I. +50	13.07	366.91	0.11	353.89	347.5	C64
12+00			4.0	362.9	355.2	C77
P.I.	12.74	379.49	0.16	366.75		
+50			10.3	369.2	363.0	C62
11+00			6.4	373.1	367.7	C54
+50			1.3	378.2	372.5	C57
P.I.	12.15	390.94	0.70	378.79		
10+00			6.3	384.6	378.7	C59
P.I. +50	13.11	403.90	0.15	390.79	385.0	C58
9+00			7.2	396.7	391.2	C55
P.I.	8.06	410.29	1.67	402.23		
8+54.30			8.1	402.2	397.0	C52
8+22.98			5.1	405.2	399.3	C59
7+91.55			3.5	406.8	401.4	C54
7+83.32			3.0	407.3	402.0	C53
7+79.33 & PT						
CK & A			2.70	407.6 =	407.6	
P.I.	12.56	420.87	1.98	408.31	NAIL IN Post	

OCTOBER 31, 1949

Construct Grades Set - Bayview Connecting Pl.

4+		420.87					
7+75 34			13.0	407.9	402 5	C 5 4	
+50			11.6	409.3	404 7	C 5 1	
7+00			8.3	412.6	407 5	C 5 1	
+50			5.4	415.5	410 8	C 4 7	
6+00			1.6	419.3	412 9	C 6 4	
P Rock	7.88	428.57	0.18	420.69			
+50			6.2	422.4	415 0	C 7 4	
5+00			5.1	423.5	415 1	C 8 4	
+50			4.0	424.6	415 3	C 9 3	
4+00					415 4		
3+97 70			5.9	422.7	415 4	C 7 3	
+71 69			7.0	421.6	415 5	C 6 1	
3+67 69 (℄ PT) (EC)							
3+63 69			7.0	421.6	415 5	C 6 1	
3+33 62			7.1	421.5	415 6	C 5 9	
3+02 12			5.6	423.0	415 7	C 7 3	
2+70 62			6.5	422.1	415 7	C 6 4	
2+39 12			6.2	422.4	415 8	C 6 4	
2+07 62			5.7	422.9	415 9	C 7 0	
P Rock	11.43	438.98	1.02	427.55			
1+75 96			13.8	425.2	416.0	C 9 2	

℄ of PIPE after benching by Bull dozer		
	Rod	Elev
C 5 4		
C 5 1		
C 5 1		
C 4 7	5.3	415.6
C 6 4	1.4	419.5
C 7 4	6.3	422.3
C 8 4	5.3	423.3
C 9 3	4.1	424.5
C 7 3	5.7	422.9
C 6 1	6.9	421.7
C 6 1	6.9	421.7
C 5 9	7.0	421.6
C 7 3	6.4	422.2
C 6 4	6.1	422.5
C 6 4	6.5	422.1
C 7 0	6.1	422.5
C 9 2	4.3	424.7

Bayview Conn. Pipeline

	438.98			
1+43.86		10.5	428.5	421.2
1+13.96		7.2	431.8	426.7
1+09.01		5.9	433.1	426.7
1+01.50		4.1	434.9	426.8
0+98.50		3.3	435.7	426.9
P 0+90.00	8.75	446.87	0.86	438.12 427.0
CK TBM (-0+25.55)			2.53	444.34 = 444.32
P	4.31	448.63		444.32
CK IP on Rock			1.15	447.48 =

C 7.3		10.8	428.8
C 5.1	(Replaced C 7a)	7.3	431.7
C 6.4		6.6	432.4
C 8.1		4.7	434.3
C 8.8		3.8	435.2
C 9.1		1.2	437.8
	(0+70)	+1.8	440.8

Bayview Conn. Pipeline

offsets moved to south of Ditch + Grade

TBM	5+46	324.07		318.61	NAIL IN STUB Pole	
26+88 80 ℄						
26+83 50 AH 26+79 50 BK			6.2	317.9	308.0	C 9 9 ✓
26+76 50			6.4	317.7	308.0	C 9 7 ✓
26+69 00			6.3	317.8	308.0	C 9 8 ✓
26+62 00			6.8	317.3	308.0	C 9 3 ✓
+50			6.8	317.3	307.9	C 9 1 ✓
26+00			8.0	316.1	307.5	C 8 6 ✓
+50			11.8	312.3	307.1	C 5 2 ✓
25 ~~26~~+25			12.2	311.9	307.0	C 4 9 ✓
(CFC TBM IN PP 23+31)			8.17	315.90	= 315.86	

Nov. 7 1949

Bayview Conn. Pipeline.

Construction Layout of Valve Chamber Sta 26+78.0

℄ (Pg. 45)	3.57	322.18		318.61	Nail in Pole
NNE (4)			4.47	317.71	~~305.85~~
ENE (7)			5.60	316.58	~~305.85~~
ESE (7)			5.00	317.18	~~306.00~~
SSE (4)			4.91	317.27	~~306.00~~
SSW (4)			4.72	317.46	~~305.85~~
WSW (7)			5.18	317.00	~~305.85~~
WNW (7)			5.17	317.01	~~305.60~~
NNW (4)			4.16	318.02	~~305.60~~

Val. Chamber Sta 1+00.

BM (pg 49)	0.98	445.30		444.32	
NNE (4)	(76.7 Rt. Sta 0+96.67)		9.23	436.07	424.65
ESE (4)	(8.17 Lt Sta 0+96.67)		8.90	436.40	424.80
SSW (4)	(8.17 Lt Sta 1+04.51)		11.22	434.08	424.65
NNW (4)	(7.67 Lt Sta 1+04.51)		10.61	434.69	424.40

E. Face of Chamber 26+84.07
W " " " 26+76.57

Rev. Grd

C11 86	305.60	(313.40 / 32)	(4)	NNE
C10 73	305.60	(313.44 / 17)	(4)	ESE
C11 18	305.75	313.69 / 17	(4)	(SSE)
C11 27	305.75			
C11 61	305.60	(313.13)	(8)	SSW
C11 15	305.60	(313.13)	(8½)	W.SW
C11 41	305.35	(313.36)	(4)	(NNW)
C12 42	305.35			

Top 20" 11.50
Bott 20" 13.60 = 307.74 = 308.0

(Drop all corners .25)

E. Face Chamb. = 0+96.67
W Face " = 1+04.51

Nov 30 1949 Reset
Nov. 22 1949 Reset

318.61 (4) → 318.61 (4)
2.73 → 2.67
321.34 Ni → 322.28 Ni

9.14	312.20	C6 60		F 20
~~5.60~~	~~316.62~~	C10 72		
4.34	317.00	C11 25		C 383
29.6	318.38	C12 63		
~~4.00~~	~~318.25~~	~~C12 55~~		~~C 524~~
6.82	314.52	C8 92		
~~4.52~~	~~317.76~~	~~C11 91~~		~~C 139~~
2.05	317.29	C11 67		C 416
8.57	312.77	C7 42		
~~5.55~~	~~316.73~~	~~C11 12~~		~~F 0.57~~

Reset Dec. 1 1947

(41 / 437.90)

Rev. Grd

C11 42	424.25	1.92	435.98	C11 73
C11 60	424.40	1.85	436.05	C11 65
C9 43	424.25	4.01	433.89	C9 64
C10 29	424.00	3.39	434.51	C10 51

OM 444.32 / 2.56 / Ni 446.86 / 12.35 / ℄ 434.51 / 3.39 / ℄ 437.90

Top 20" Pipe W 9.40 = 428.5
Bott 20" Pipe S 9.38 = 426.4 = 426.8

(Ppr 0.4 low Drop all corners 0.4)

428.5 / 426.4 / 426.1

TBN 316.98 on Nail
6.21
323.19 Ni
4.59 ℄ Pin in Pole
318.60 = 318.61

323.19 / 312.96 / 7.69 / 5.0 / 10.33

Nov. 18 1949
Beatty
Rogers
Finney

BAYVIEW CONN. PIPELINE

GRADES FOR 12" C.I. LINE & VALVE BOX FROM 20" CONC. PIPE TO PAC. BEACH RES.
RIGHT STA 41+20.37

					Pg. 42 NAIL IN
℄	12.74	312.59		299.85	Pole
Top. 20" Conc. Pipe			5.43		
Both. " " "			7.51	305.08 = 305.00 (GRD)	
Top (inside) Bell 12" S.D.			6.00	306.59	
Bott (inside) Bell 12" S.D.			7.19	305.40	
	= 1.36 RT. STA 41+20.37				GRD Bott Pipe
0+00	= SPIGOT END 12" C.I.				305.4
0+04			4.5	308.1	305.4 C2.7
0+25			6.9	305.7	301.6 C4.1 ~~305.3~~ C5.4
℄					
~~0+50~~	0.78	302.07	11.30	301.29	~~297.0 C4.3~~
0+51.50					296.8 C4.5
VALVE CHAMBER 0+62.13 - 0+68.13					SUB GRD
SW Cor Box (4)			4.92	297.15	295.35 C1.80
NW Cor Box (3)			5.25	296.82	295.25 C1.57
NE " " "			5.23	296.84	294.96 C1.94
SE " " "			4.87	297.20	295.15 C2.05
SET ℄ on RP Hub			7.32	294.75	
℄	19.65	312.82	0.90	301.17	
CK ℄			12.97	299.85	

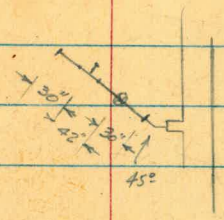
296.75 C1.50

3.054
297.0
46) 8.4 (.1826
46
380
368
120
92
280
276

1826
36E2
5833 4C

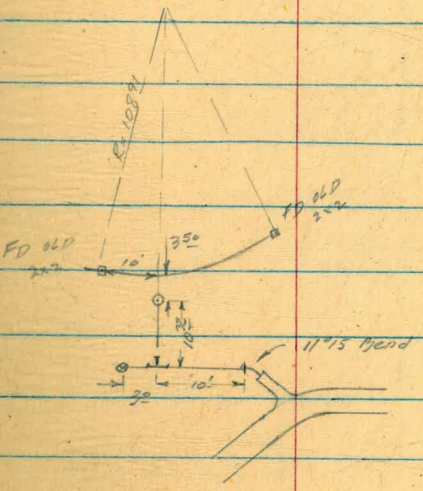
FIRE HYDRANT FROM SIDE OUTLET 39+40

BM		13.10	312.95		299.85	NAIL IN POLE
0+00	Top of 6" SO Bott of 6" SO				299.6	
0+04.5	② FOR GV.		7.3	305.7	300.0	C 5.7
0+08	③ FOR TEE		5.4	307.6	300.3	C 7.3
0+10.5	③ FOR END OF PIPE		5.5	307.5	300.6	C 6.9



FIRE HYDRANT FROM SIDE OUTLET 32+60.6

①		3.95	298.75		294.80	
0+00	Bott. 6" outlet Top 6" "			10.74 10.04	288.01 288.70	
0+11.10	TEE			3.9	294.9	289.0 C 5.9
0+14.10	G.V.			6.1	294.7	289.3 C 5.4
0+21.42	F.H.		④	3.7	295.1	293.70 C 1.4 Fg 290.20 C 4.5
"	F.H.		⑤	2.9	295.9	C 2.2 Fg C 5.7



Nov. 30 1929

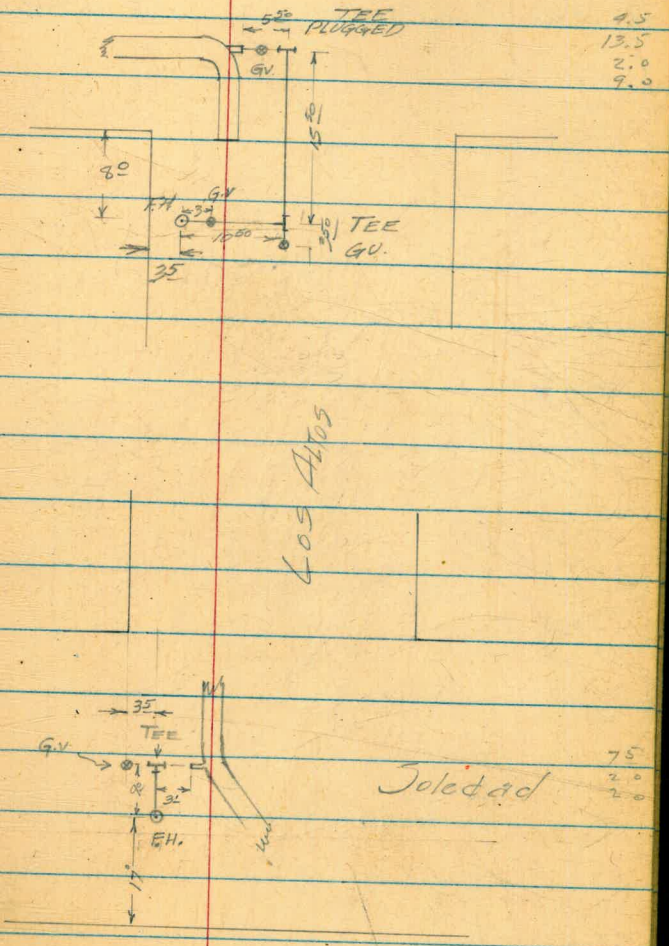
FIRE HYDRANT CONN - FROM 6" S.O STA 26+86.30

TBM		2.73	321.34	318.61	NAIL IN POLE
0+00	Top 6" S.O Bott 6" S.O			309.4 308.7	
0+05.50	(5) TEE 5.50		4.6	316.7	309.0
0+21°	(6) TEE		5.4	315.9	309.8
0+24°	(4) G.V.		3.4	317.9	312.0
0+31.50	F.H.				313.80 310.30
0+36.50	(5)		2.3	319.0	

FIRE HYDRANT FROM 6" S.O STA 20+84.7 AH.

11		4.52	323.38	318.86	
0+00	Top 6" SIDE OUTLET Bott 6" SIDE OUTLET		9.9 10.6	313.50 312.80	
0+23.1	(5) TEE		5.1	318.3	313.0
0+06.6	(6) G.V.		5.8	317.6	313.3
0+12.1	F.H.				
	(4) N		3.6	319.8	314.8
	(4) S		3.1	320.3	314.8

C7.7
C6.1
C7.0
C5.2 Flange
C8.7 Butt
C6.5
C7.0
C6.8
C6.2
C4.5
C3.3



4.5
13.5
2.0
9.0
7.5
2.0
2.0

Set Top B.O. Chamber			24+68.28	
B.M.	2.72	318.58	315.86	Nail in Pole
④ offset B.O Chamber	5.14	313.44	312.34	Grd. F.G.

Muirlands Pipeline Ext.
& Proposed 12" Water Line

Jan. 12, 1953
Booth
Williams
Kemp
Alexander

Δ 11°08' RT
R = 1009.
L = 196.66

Reverse Curve

2+128 P.R.C.

Δ = 9°20 LT
R = 741.00
L = 125.01

Compound Curve

0+87 80 (P.C.C.)

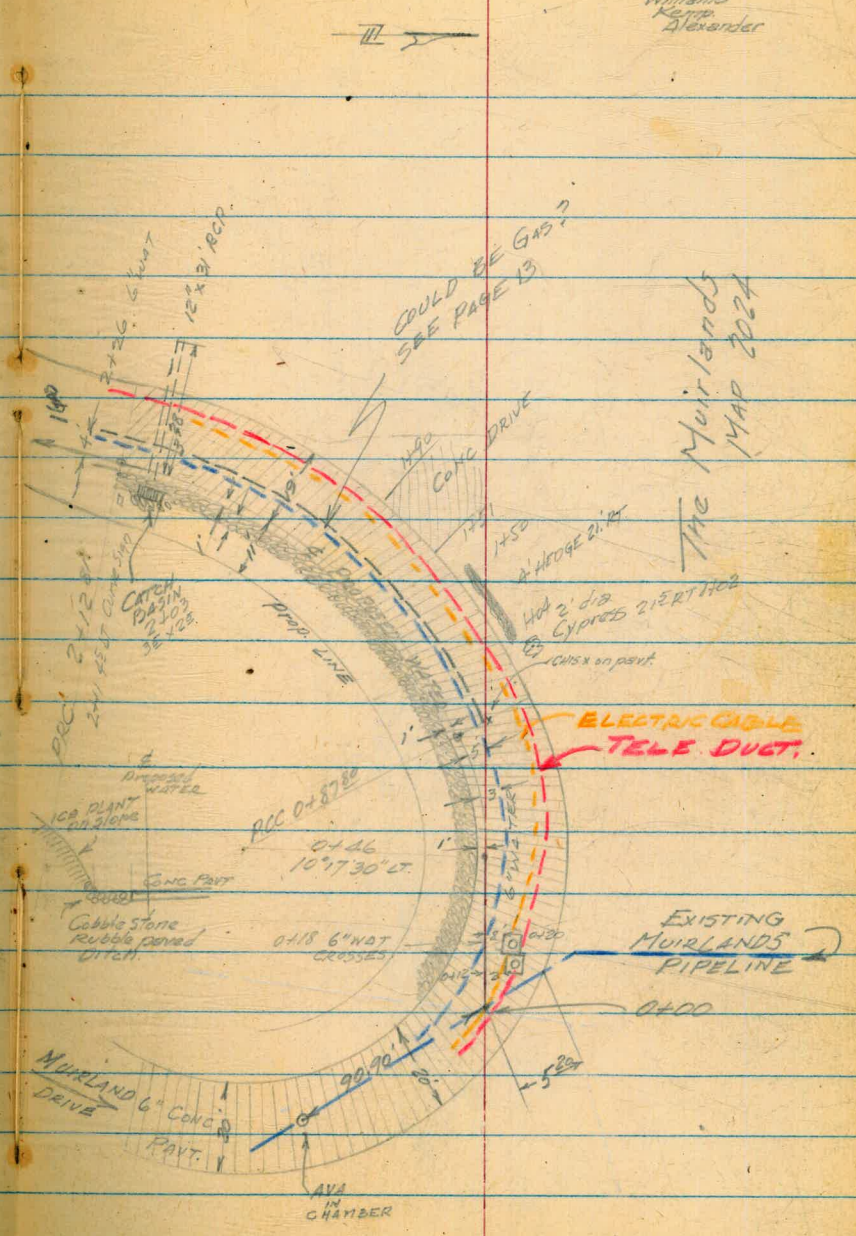
Δ Wilson
(29°29' LT.)
Δ = 20°35' LT.
R = 81.
L = 41.80

(10°17'30" LT. To P.C.C.)

0+46 P.C.

{ 112° 25' RT from Fwd Tang
{ 67°35' LT from Bk Tang

0+00



MUIRLANDS PIPE LINE
℄ Proposed 12" WATER

Δ - 26°58'15" RT
R - 810.
L - 381.29

5+78.55 BC.

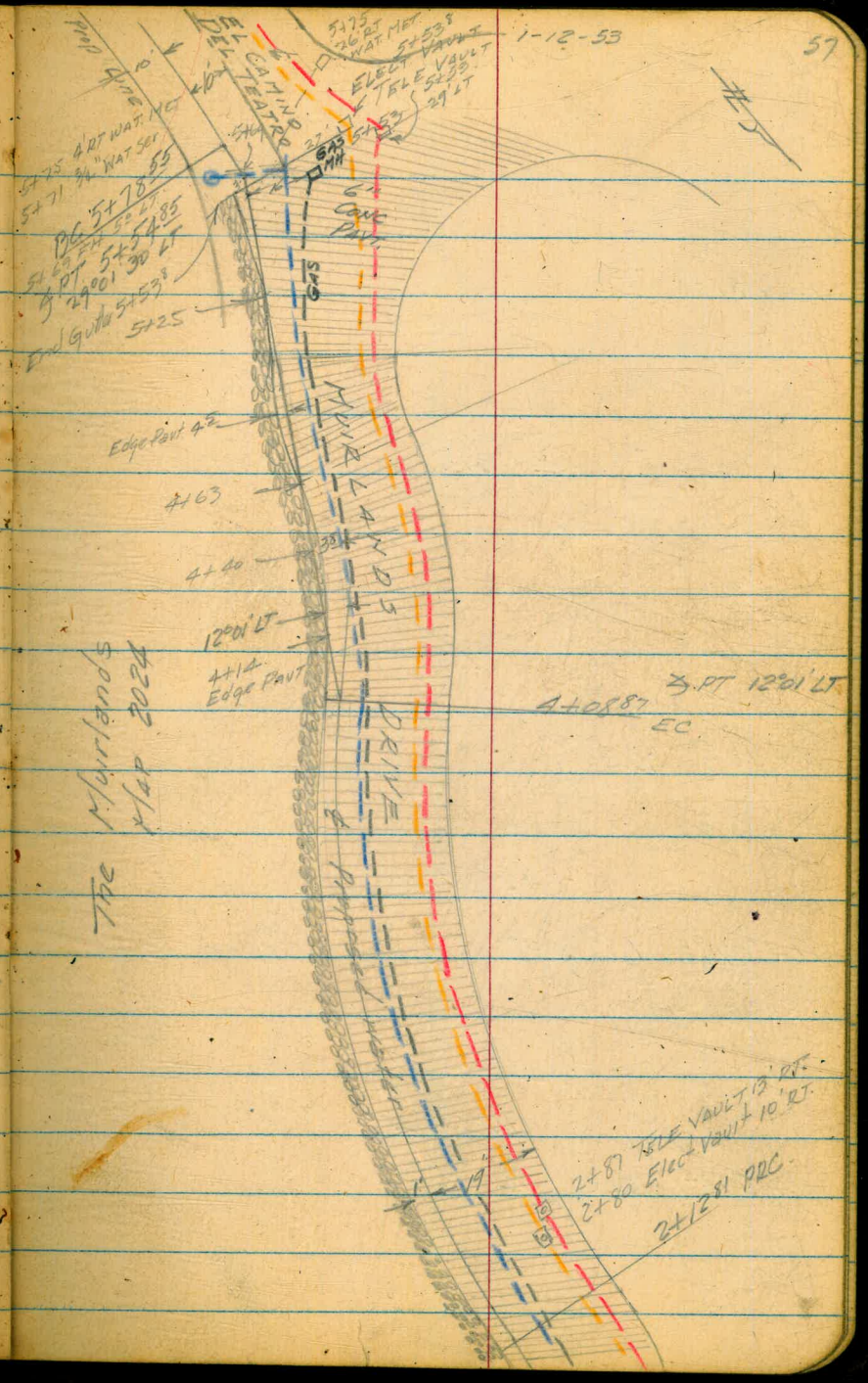
29°01'30" LT

5+54.85 ℄ PT.

5+53.60 POT. (this x on pavt.)

12°01' LT

4+08.87 EC. & ℄ PT.



MUIRLANDS PIPE LINE
Cont'd.

1-13-53

58.

14+81.58 E.C.

Δ - 36°37'45" LT.
R - 490
L - 313.2
T. 162.20

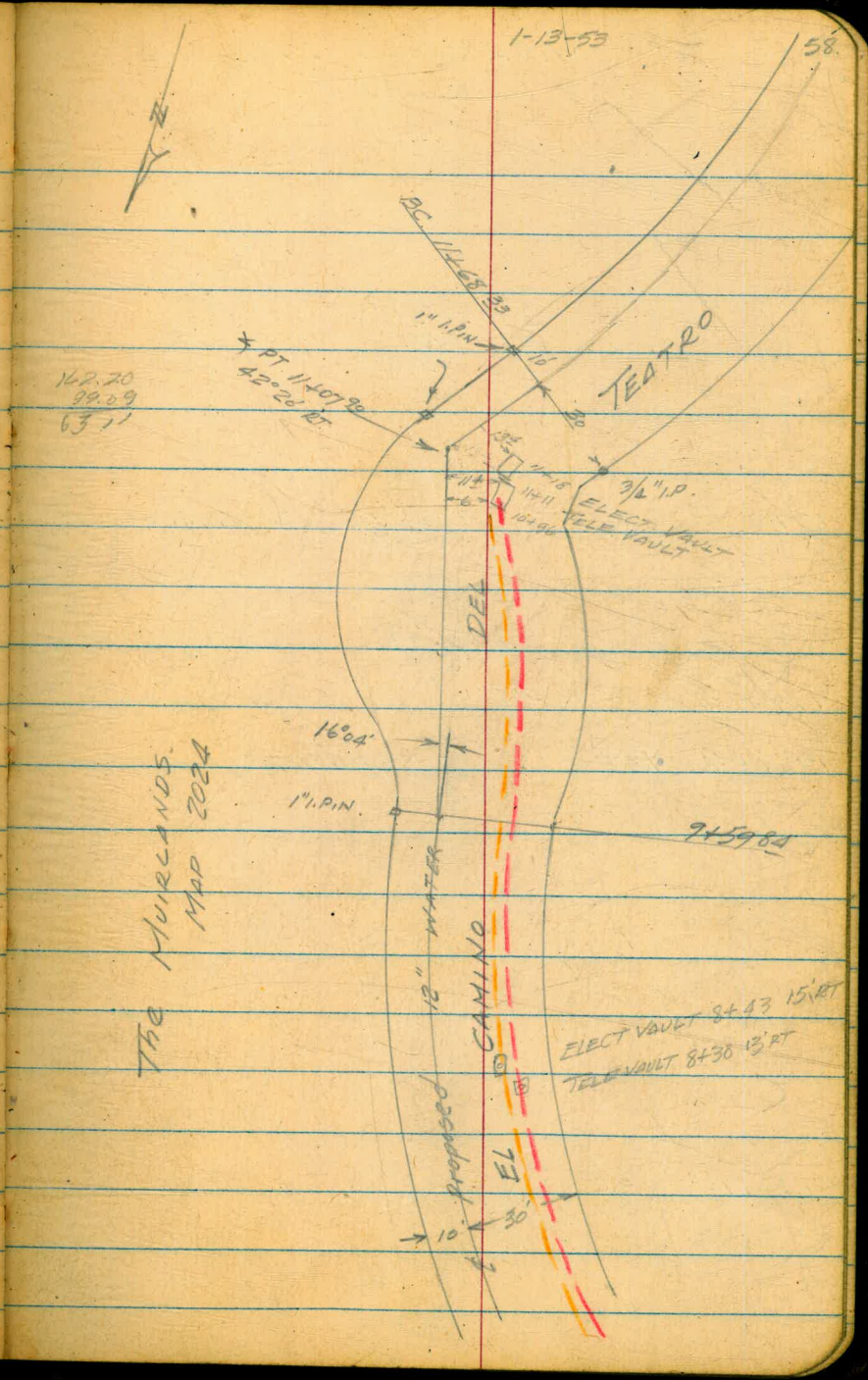
11+68.33 B.C

42°20' RT.

11+07.90 ℄ PT

16°04' LT

9+59.84 E.C & ℄ PT



1-14-53

Δ = 21°51' LT
R = 510.
L = 194.50

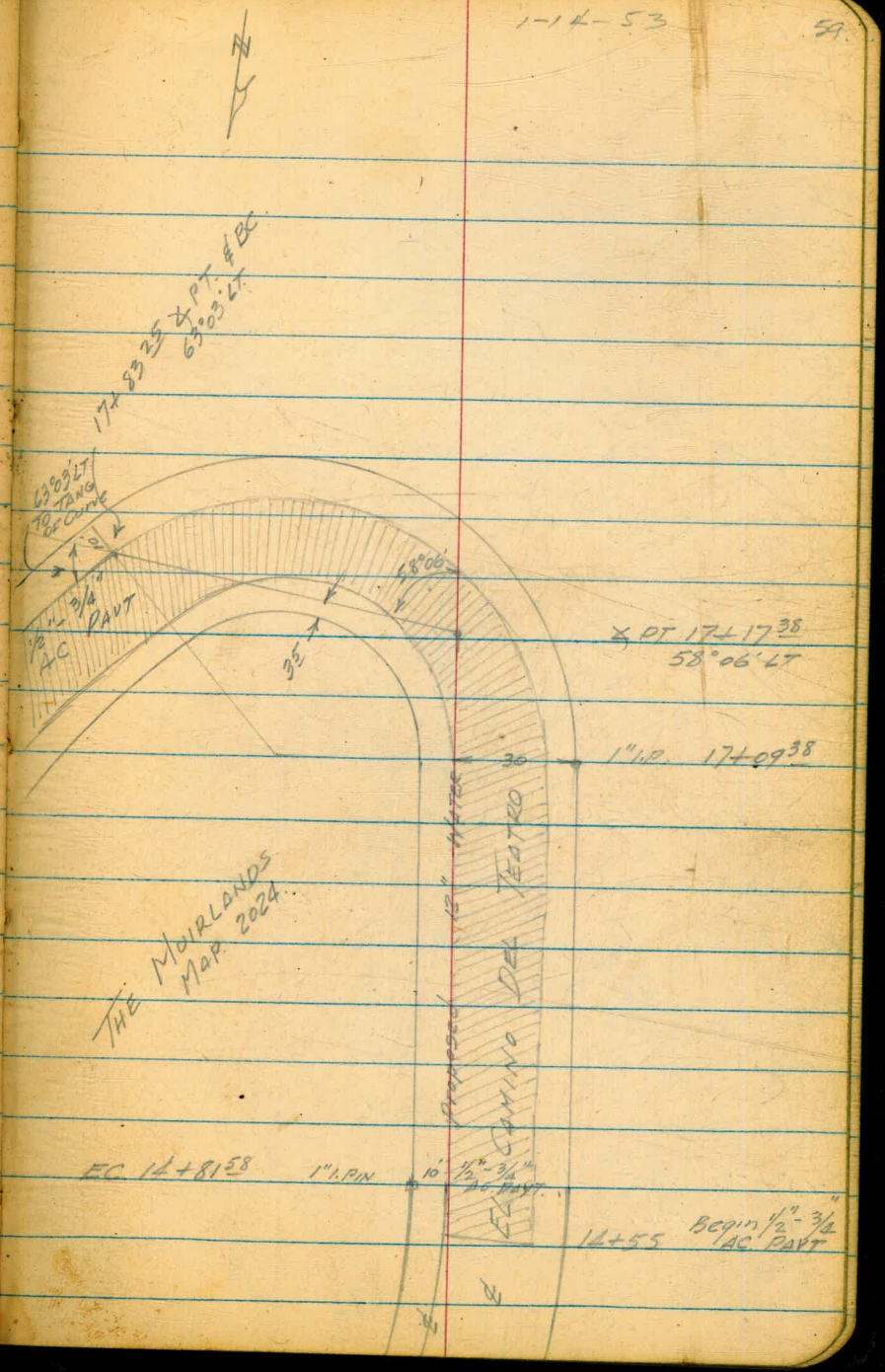
17+83 25 ℄ PT 63°03' LT. (To Tang. of curve)

58°06' LT.

17+17 38 ℄ PT

17+09 38 POT (BC of Roadway)

14+81 58 E.C



MUIRLANDS PIPELINE EXT.

21+98° ℄ P.T. 76°27'30" RT (Turned)
(76°14' REC.)

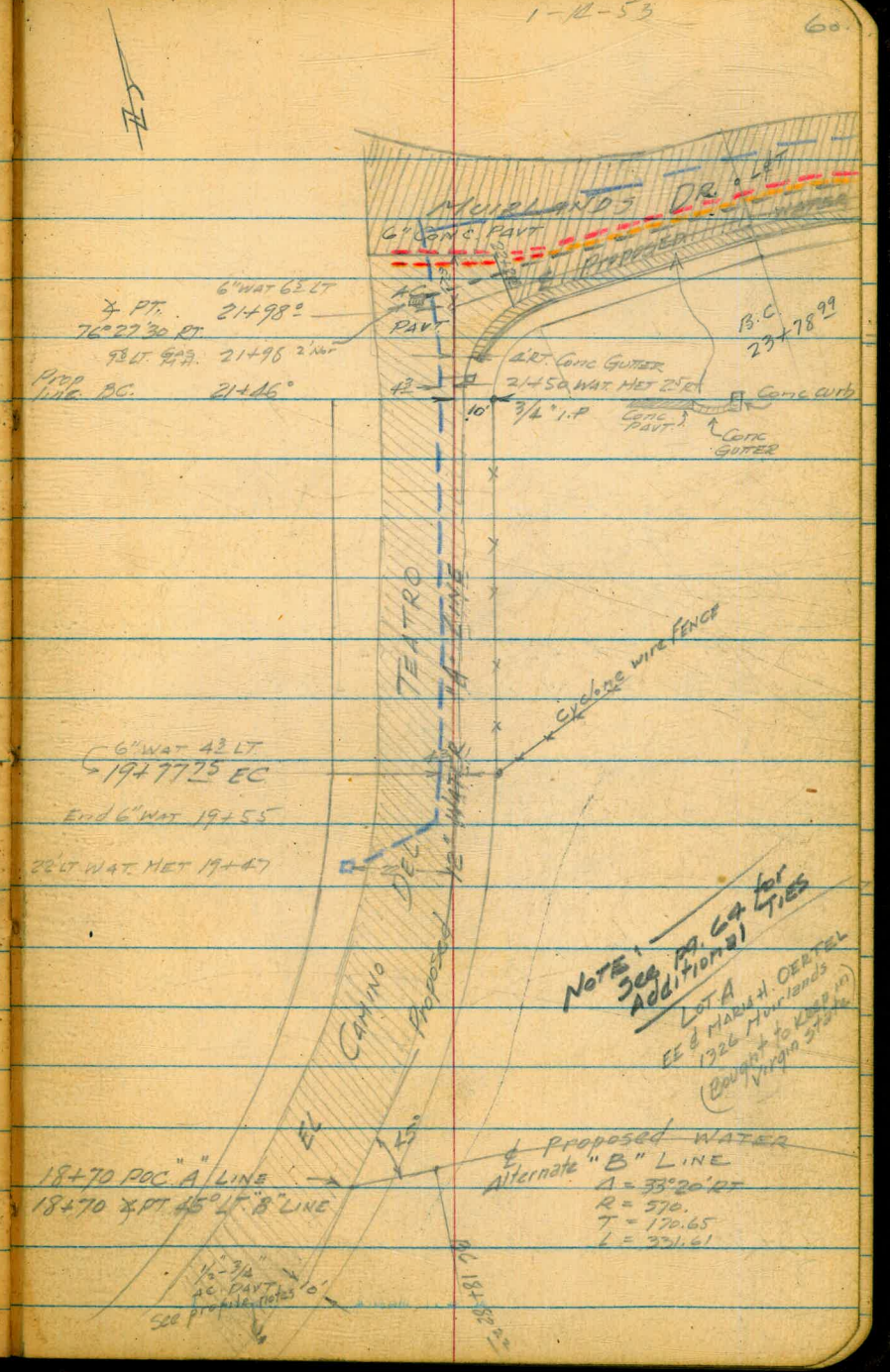
21+46° POT (prop. Line B.C.)

19+77.75 E.C.

"B LINE

℄ PT. 22+72.70
EC. 22+13.83
BC 18+82.22

18+70 POC. "A" LINE
18+70 E.C. ℄ ℄ PT. 45° RT.



MUIRLANDS PIPELINE

28+20 } 5' RT Sandstone wall
28+16 }

28+05 } 4' RT Sandstone wall
27+97 }

27+80 WAT. GV 11' LT

27+58 } 4' RT Sandstone wall 1' high
27+42 }

27+29 WAT. MET 5' RT

26+96 Mail Box 4.5' RT
Sand Stone Wall 4.5' RT

28+26.27 ℄ PT. ∠I. 146°30'

26+95 } 1.5' RT Edge of Elect Vault
26+88 }

26+96 } Gravel Drive
26+79 }

26+79 End 4' AC Pav
26+60 End Conc Drive

28+26.27 = 24+42.98 "B" LINE.
28+26.27 EC. ℄ ℄PT. "A" LINE

(5' RT To Conc
Mail Box 4.5' RT
End Conc Gutter
& AC Conc
26+13
26+14 WAT. MET 6' RT
25' To FACE Curb
End Conc Gutter
25+68 Begin Conc Gutter
25+66 End 4' AC Driveway
25+43 Begin 4' AC Drive
End Conc Gutter
25+43 & Rough Curb

Δ 8.7°50'
R 291.00
L 44.7.28

24+85 Gas MH 7.5' RT

24+87 } Brick Walk
24+83 } 2.3' RT

24+73 WAT MET 4' RT
24+25 33' RT To Curb
Conc Gutter

24+21 } Cement
24+00 } Gravel Drive
5' RT

23+66 } Conc Driveway
23+44 } No Curb

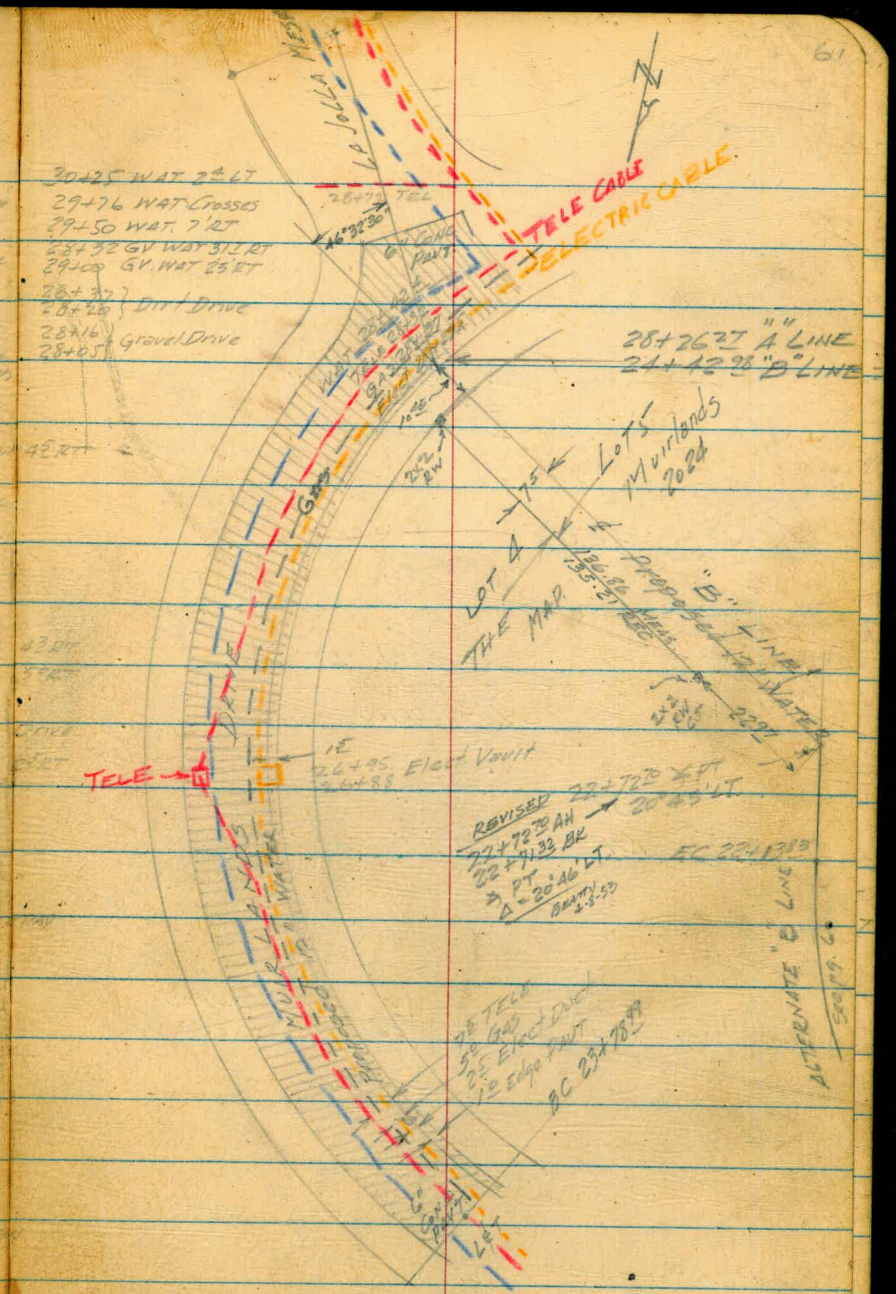
23+78.99 BC

22+28 } 3.2' RT
22+25 } Brick Walk with
4 ft Shrubbery outside

22+46 33' RT To Face Curb
Conc Gutter

30+25 WAT 2' LT
29+76 WAT Crosses
29+50 WAT. 7' RT
29+32 GV WAT 3.1' RT
29+00 GV. WAT 2.5' RT

28+37 } Dirt Drive
28+28 }
28+16 } Gravel Drive
28+05 }



MUIRLANDS PIPE LINE
Cont'd.

1-15-53

62

Δ - 24°08' LT
R = 475.00
L - 200.00
201.07

34+48 32

34+56 85 P.C.C.

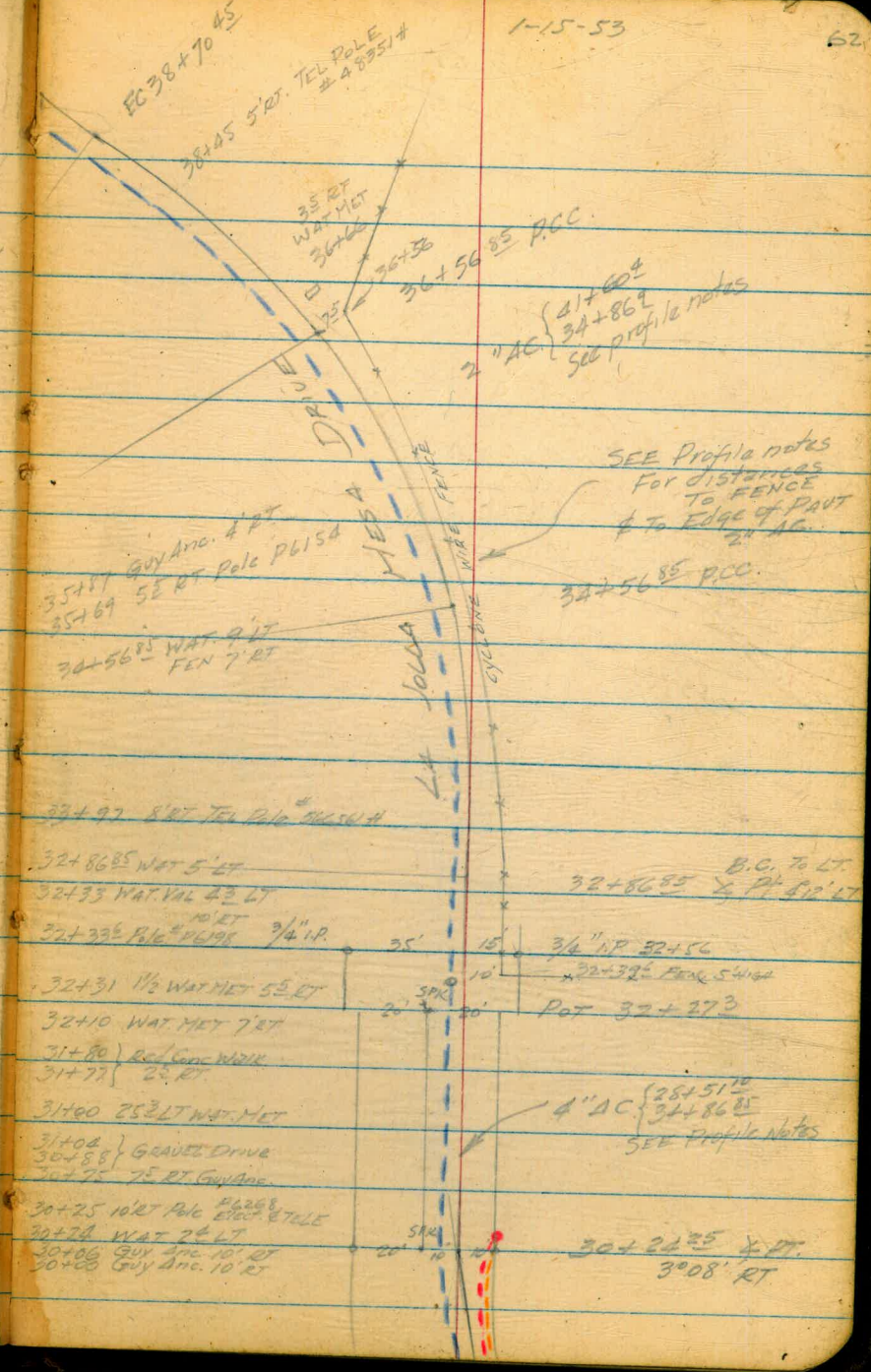
Δ - 13°14' LT
R - 700.00
L - 170.00
162.05

B.C
32+86 85 ℄ RT 4°12' LT

32+56 POT

32+27 3 POT Road { 50' WIDE AHEAD / 40 WIDE BACK

30+24 25 ℄ RT 3°08' RT



MUIRLANDS Pipe line

1-22-53

63.

41+49 51

41+60 40 END of LINE.

?
40+62 83 POT

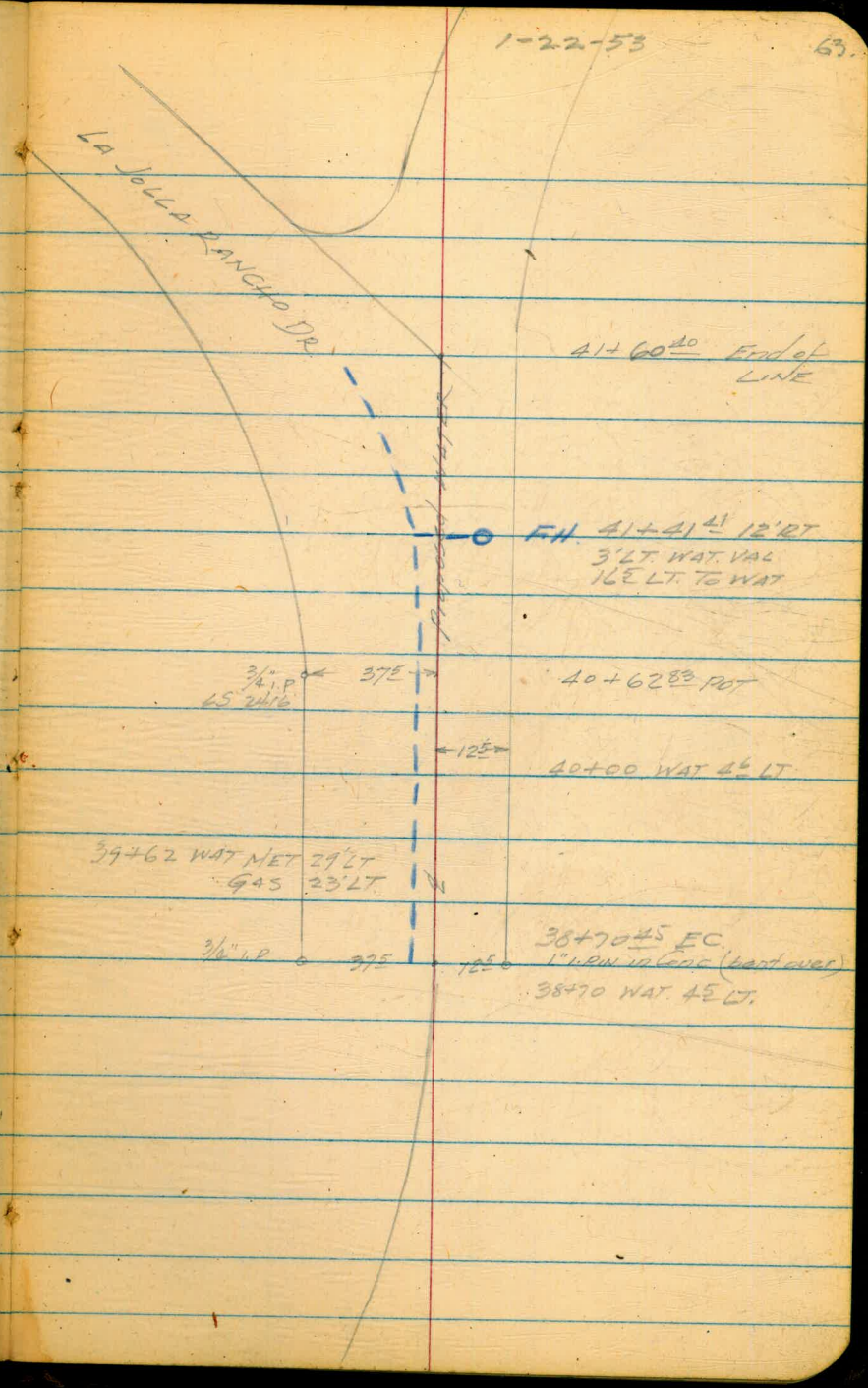
38+67 21

38+70 45 E.C

Δ 20°41'
Δ - 20°23'30" LT
R - 600
L - 213.60
L = 217.24

36+49 27

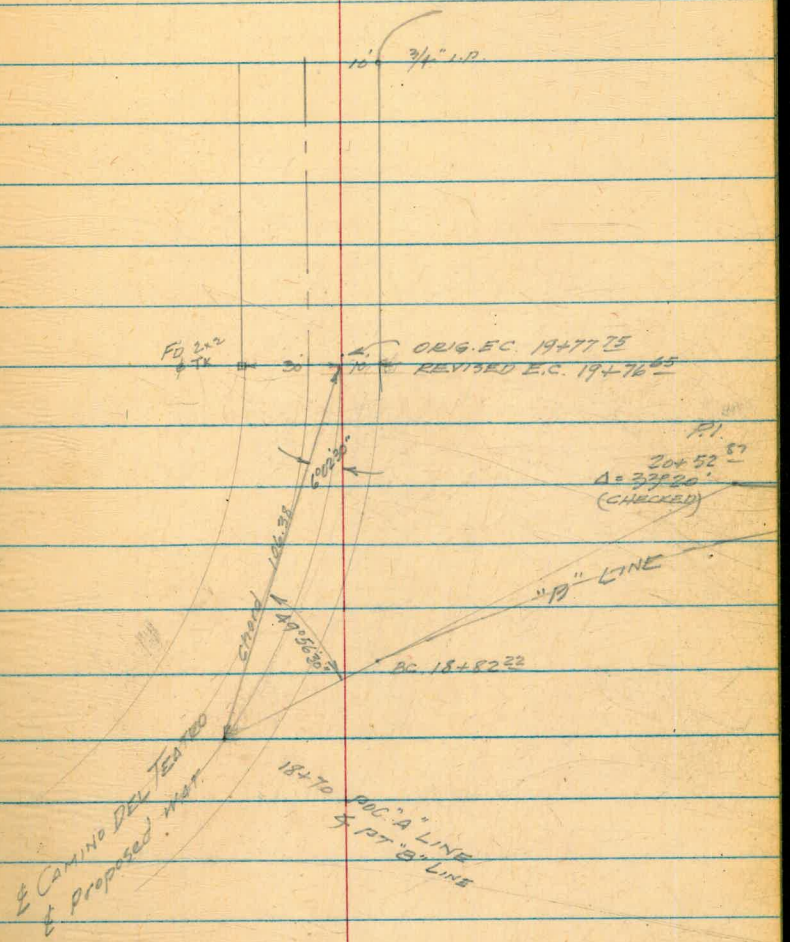
36+56 85 P.C.C



MUIRLANDS PIPE EXT.
Additional Ties

APRIL 8 1953
BEATTY MARTELL ALEXANDER

64



CONTINUED FROM Pg. 79 THIS BOOK

MUIRLANDS DIPELINE EXT
& Profile
"B LINE PROFILE"

	480.18		
21+44		9.1	471.08
21+39		7'	473.08
21+29		7.4	472.78
21+00		5.7	474.48
20+82		2.7	477.48
20+59		2.7	477.48
20+30		1.5	478.68
20+47		4.1	476.08
20+00		8.4	471.78
19+93		9.7	470.48
19+85		8.7	471.48
19+62		5.2	474.98
19+50		5.5	474.68
19+10		4.5	475.68
19+38		1.4	478.78
19+22		2.1	478.08
19+10		0.7	479.48
PI	7.23	487.23	0.18 480.00
19+00		3.2	484.03

Muirlands Pipeline Ext. & Profile

1-26-53

"B" Line Profile

		487.23		
18+97		0.3	487.2	
+93		0.0	487.23	
+84		0.9	487.14	
+84		3.4	483.83	
18+82.22 ± B.C.		3.4	483.83	
+73		5.9	481.33	
18+70 ± P.T.		5.2	481.93	
C.E. P		5.26	481.77 = 481.81	Pg. 74
BM	0.18	500.24	500.06	(From Pg. 74.
P	1.03	488.33	12.94 487.30	
P	0.11	475.36	13.08 475.25	
P	0.57	462.77	13.16 462.20	
P	0.15	450.07	12.85 449.92	
P	0.25	437.05	13.27 436.80	
P	0.14	425.63	11.56 425.49	
C.L. orig. BM			7.13 418.50 = 418.51	see next page

BP Nor end of curb inlet, Muirlands & Camino del Teatro 150' NW 21+98.± PT.

on Base of Lamp Post Lot 1-3 Blk 19

Proposed Muirlands Pipeline Ext & Profile

Jan. 23 1953

			Page 17	City Datum	
BM	0.37	418.88	418.51	418.33	BP in Base of Lamp Post Lots 1/2 Blk 19
0+00			4.74	414.14	
+46			8.55	410.33	0.0 4.5 8.63 13 7 1. Edge Pavt
+50			8.90	409.98	Rubble Ditch overgrown
+75			10.84	408.04	
0+87.80	P.C.C.		11.89	406.99	3.2 7.1 11.92 11 8 1.
1+00			12.84	406.04	6.9 13.0 12.88 8 1.6 1.
P	0.11	405.67	13.32	405.56	
+25			1.43	404.24	+2.0 1.6 1.47 8 3.0 1. Bottom Edge Par. Ditch Pavt.
+50			3.23	402.44	+1.3 3.5 3.26 8 3. 1
+75			5.25	400.42	1.5 5.45 5.27 8 3. 1
2+00			7.19	398.48	2.7 7.6 7.20 8. 3. 1.
	Catch Basin	2+03.4 2+06.8 } 2½ Lt. ℄			394.99 392.27 10.68 (Inv. 12" RCP) 13.40 3.0 28.0

Muirland's Pipeline Ext & Profile Cont'd

						+ Bottom Trench Elev.	+ Edge Pvmt	
		405.67						
2+12.81	PRC		8.23	397.44		4.0 / 8	8.4 / 3.	8.23 / 1.
+25			9.24	396.43		4.5 / 9	9.5 / 3.	9.26 / 1
+50			11.20	394.47		6.0 / 8	11.4 / 3.	11.22 / 1
+75			13.14	392.53		End ICE PLANT on Slope 9.6 / 8.	13.4 / 3	13.15 / 1
EP		0.66	393.06	13.27	392.40	2.7 Pool 2 Pvmt = 2.45		
3+00			2.54	390.52			+1.2 / 7.	2.8 / 3.	2.54 / 1.
+25			4.58	388.48			0.9 / 6.5	4.9 / 3.	4.59 / 1.
+50			6.63	386.43			2.8 / 7.	6.8 / 3.	6.63 / 1.
+75			8.68	384.38		Begin Ice Plant on Slope 5.9 / 7.	8.9 / 3.	8.68 / 1
4+00			10.69	382.37			2.0 / 8.	11.0 / 3.	10.72 / 1.
+08.87	EC. & PT PRC		11.38	381.68			2.7 / 9.	11.7 / 3.	11.41 / 1.

Murlands Pipeline Ext
& Profile Contd

		393.06	
4+25		12.96	380.10
P	0.34	380.41	12.99 380.07
+50		2.36	378.05
+75		4.03	376.38
5+00		5.10	375.3
+25		5.85	374.56
5+53?	End Conc Pavt	5.92	374.49
5+54.85	℄ PT	5.9	374.5
CK B.M.		7.64	372.77 = 372.40 / 372.61 / C 372.81 / 99.18
5+78.55	B.C	5.0	375.41
6+00		4.4	376.01
6+50		0.6	379.81

6.6 11.0 — 12.75 1.6 Edge Pavt
6. 0.5 Bottom Past Ditch

+4.6 2.4 — 2.18 " "
9. 0.5 Bott. Dit. 1.6

0.3 4.29 4.12
17.5 4.8 2.8
Bott Ditch Edge Pavt

2.3 5.3 5.14
13.5 6.3 4.3
Edge Pavt

0.0 6.0 — 5.85
9. 1.8 — 0.2
Bott Ditch Edge Pav.

0.6 6.1 5.85
11. 4.7 2.7
Edge Pav

BP on Conc Lamp Post Base
50± RT 5+54.85

0.9 4.8
8. 3.

0.5 4.4
6 1.5

+4.1 0.9
6. 23

Muirlands Pipeline Ext
E Profile
Contd

			380.41		
4	P	12.53	392.78	0.16	380.25
4	7+00			9.4	383.38
	+50			5.1	387.68
	8+00			1.0	391.78
5	P	12.81	405.58	0.01	392.77
	+50			9.3	396.28
	9+00			4.8	400.78
5	+50			0.7	404.88
5	P	13.02	418.44	0.16	405.42
ok	9+59.84 E.C.			12.7	405.74
5	10+00			9.1	409.34
	+50			5.1	413.34

2.0 / 8 — 10.0 / 3.5 x

0.0 / 65 — 5.5 / 3 x

+50 / 9 — 1.5 / 25 x

7.0 / 9 — 9.6 / 25 x

00 / 11 — 4.0 / 7 — 5.3 / 3 x

+7.2 / 12 — 1.2 / 4 x

7.7 / 7 — 13.7 / 5 x

5.0 / 12 — 8.8 / 7 — 10.1 / 6 — 10.1 / 4 — 9.3 / 3 x

6.2 / 11 x

: MUIRLANDS PIPELINE EXT
& Profile
Cont'd.

		418.44		
4	11+00		2.5	415.94
4				
	11+07.9 ± PT		0.5	417.94
	TBM. set	13.00	431.00	0.44	418.00
	+50			11.7	419.3
5	+75			9.5	421.5
	12+00			7.3	423.7
5	+25			5.4	425.6
5	+50			3.2	427.8
0	(4)	12.92	443.74	0.18	430.82
3	+75			13.1	430.64
6	13+00			10.6	433.14
6	+25			9.75	433.99

0.0 / 5.	2.0 / 0.5	×	2.9 / 2	0.4 / 10
+4.4 / 5		×	1.4 / 3	2.2 / 1	0.3 / 16
+00 sta. of SDGE MH Eastside				
10.6 / 5	11.4 / 2.	12.4 / 2.	×	
5.2 / 10.	9.2 / 2	10.0 / 2	×	
2.0 / 10	5.3 / 4.	7.6 / 1	×	
4.3 / 7	5.1 / 35	6.1 / 2.	×	
+2.5 / 8	2.3 / 2.	4.2 / 1.	×	
10.2 / 4		×	14.0 / 1	13.5 / 7
5.6 / 8	10.6 / 2	×	11.8 / 2	11.0 / 10
3.0 / 3	9.0 / 1	×		

Muirlands Pipeline Ext.
& Profile
Cont'd.

		443.74		
13+50		7.3	436.44	
+75		5.3	438.44	
14+00		3.1	440.64	
+25		0.6	443.13	
P.	13.15	456.70	0.19	443.55
+50	(Edge A.C. Pavt)		11.1	445.6
+75			8.5	448.2
+81.58	E.C.		7.9	448.8
15+00	(Edge A.C. Pavt)		6.5	450.2
+50			2.3	454.4
P.	13.31	469.98	0.03	456.67
16+00	Edge A.C.		11.1	458.88
+50	on A.C.		6.5	463.48
17+00	(A.C. 2' RT.)		2.3	467.68
+09.38	(BC of Road.) (on A.C.) Edge AC. 18 LT		1.5	468.48
+17.38	4 RT on AC (Edge AC. 3.5 LT.)		0.6	469.38

3.1 7.0 7.9
7.1 3

0.0 4.5 5.7
9 4 2

+2.0 2.5 3.7
8 4 3

+3.2 1.7 1.2
8 4 2

8.4 11.8
5 0.5
1.5

1+455 Begin AC. ½"-¾" thick.

8.3 9.3 8.6
3 2 0.5
Edge AC

7.9 8.6 8.1
4 3
Edge AC

1+455 Begin Scattered ICE PLANT on Slope to Left.

2.1 6.6
8 3

+1.7 1.8
3 3

7.1 11.6
5 1

2.9 6.9
8 2

+2.0 1.5
8 2

+1.0 1.1
7 4

+1.0 0.8
8 2
on AC.

Muirland Pipeline Ext. & Profile Contd

		469.98		
PK	12.55	482.47	0.06	469.92
17+24	Edge A.C. Pavt		13.0	469.47
+50			10.6	471.87
+77	Edge A.C. Pavt		6.6	475.87
17+83.25	℄ PT. & BC.		6.2	476.27
18+00			5.4	477.07
+50	on edge A.C.		2.3	480.17
PK (NAIL)	12.88	494.69	0.66	481.81
18+70	("A" LINE Continues "B" LINE ℄ PT To PT.)		12.7	481.99
19+00	("A" LINE)		10.5	484.19
+50	("A" LINE)		5.85	488.84
19+77.75	E.C.		3.85	490.84
20+00			1.9	492.79
PK	12.76	507.30	0.15	494.54
+50			10.6	496.7
21+00			6.5	500.8
+46			2.3	505.0
PK (NAIL)	6.12	512.95	0.47	506.83
CK BM			12.89	City Datum 500.06 = 500.62

(NOTE: See pg 67 for closure from this BM To Starting BM.)

99 / 4 × 709 1.5 Edge AC 19.2

63 / 4 × 7.2 / 5 6.0 / 5 SCATTERED ICE PLANT

Edge Pavt

8.5 / 3 Edge Pavt × 6.0 / 3 5.4 / 5 2.2 / 4 " "

2.0 / 2 × 2.3 / 2 1.4 / 5 1.6 / 5 "

12.7 / 2 13.3 / 2 12.7 / 4 9.2 / 8 "

0.6 Edge A.C

10.1 / 2 Edge A.C. × 10.7 / 3 6.7 / 8 " "

19+30 and Scattered for plant To Lef

6.1 / 3 6.9 / 3 Edge AC 2.6 / 9

19+75 Begin ice plant on Lt growing out in Street.

4.1 / 22 BC 4.2 / 5 0.9

2.0 Edge AC × 19+1.2 / 8 5

6.1 / 7 10.6 / 3. 10.6 / 15 Edge AC

6.2 / 3 Edge AC 6.5 / 2. × 0.4 / 7

2.5 / 2 Edge AC × 4.5 / 2. 4.03 / 2. Top Cobblestone Wall

B.P. Nor End Curb Inlet Muirlands Drive & Camino Del Teatro.

Murlands Pipeline Ext & Profile Cont'd.

		512.95		
21+66	Edge A.C. Pavt.		6.3	506.65
21+98	℄ PT.		2.8	510.15
22+218	Begin Conc. Pavt		1.55	511.4
+25	" "		1.60	511.55
+50			+0.06	513.01
11 Deg Nav Edge Pavt 2+25		12.47	524.97	0.45 512.50
23+00			8.60	516.37
+50			5.78	519.19
23+78.99	BC		4.49	520.48
24+00			4.12	520.85
+25			3.99	520.98
+50			3.88	521.09
+75			3.80	521.17
25+00			3.60	521.37
+25			3.41	521.56
+50			3.27	521.7
+75			3.05	521.92
26+00			2.84	522.13
11 Deg		6.69	528.81	2.84 522.13

Edge pavt + 6E PT

1.68
5.6 Edge Pavt
11.93 Edge Pavt
8.61 1. Edge Pavt
5.80
4.49
4.16 End Conc Gutter & Curb
4.02
3.93
3.86
3.64
3.48
3.36
3.11
2.90

MUIRLAND PIPELINE EXT.
& Profile
Cont'd

				Cut to 6" Thick Edge Pavt
	528.81			
26+25		6.75	522.06	6.81
+50		6.73	522.08	6.80
+75		6.75	522.06	6.81
27+00		6.80	522.01	6.88
+25		6.88	521.93	6.92
+50		6.98	521.83	7.05
+75		7.20	521.61	7.25
28+00		7.44	521.37	7.50
+25		7.71	521.10	7.77
28+26.27 = {A. LINE EC & PT. / B. LINE & PT.}		7.72	521.09	7.78
SET TBM (on Nail)		7.72	521.09	
28+50	on Conc. Pavt	7.00	521.81	
+51.10	End Conc. Pavt Begin A.C. Pavt	6.98	521.83	
29+00	on A.C. 4" Thick	6.28	522.53	
+50	" "	5.36	523.45	
30+00	" "	4.72	524.09	
30+21.25 & PT.	" "	4.31	524.50	
+50	" "	3.91	524.9	
31+00	" "	3.14	525.67	

Muirlands Pipeline Ext. & Profile Cont'd

	528.81		
31+50		2.44	526.37
(11) Encr.	8.18	534.55	2.44 526.37
32+00		7.8	526.75
32+273 POT		7.5	527.05
+50		7.25	527.30
+60		7.20	527.35
32+8685 P.C. & PT		6.95	527.60
33+00		6.95	527.60
+50		6.3	528.25
34+00		5.5	529.05
+5685 P.C.C.		4.8	529.75
35+00		4.2	530.35
+50		3.3	531.25
36+00		2.7	531.85
36+5685 P.C.C. Edge AC		2.0	532.55
SET BM.	8.06	541.03	1.58 532.97
37+00			7.9 533.13
+50 Edge A.C. Pavt.			7.1 533.93
38+00 Edge " " "			6.4 534.63

2.5 / 3 Edge A.C. 2" Thick

7.95 / 3 Edge AC

7.6 / 2 " "

7.35 / 2 " "

7.3 / 2 " "

7.2 / 3 " "

6.85 / 4 " "

6.4 / 4 " "

5.5 / 2E " " 2.0 / 5 2.0 / 7.5 FEN

4.8 / 0.5 " " 1.2 / 3.5 4.3 / 7 FEN

Edge 2" Thick A.C.

4.4 / 1 × 3.8 / 2 4.0 / 5 FEN

" " 3.55 / 1 × 3.1 / 2 3.6 / 6 FEN

" " 2.85 / 1 × 2.4 / 2 3.0 / 8 FEN

2.0 / 1 × 2.4 / 4 / 7 FEN

on 3/4" I.P. in Conc. 7½ RT. 36+98±

7.95 / 1. Edge AC 2" Thick 8.6 / 10

7.1 / 1 on AC. × 7.5 / 10

6.2 / 1 on AC 6.1 / 3 6.6 / 10

Muirlands Pipe Extension & Profile Contd

	541.03.			
38+50	on A.C.	5.5	535.53	
+70.85 (EC)	on A.C.	5.15	535.88	
39+00	" "	4.8	536.23	
+50	" "	4.3	536.73	
40+00	" "	3.8	537.23	
+50		3.25	537.78	
41+00	on edge A.C.	2.85	538.18	
+50		2.5	538.53	
+60.4	End line	2.3	538.73	
Set TBM. 2.16	540.81	2.38	538.65	
Ck TBM. 0.67	533.63	7.85	532.96 = 532.97	
Ck TBM 0.93	522.01	12.55	521.08 = 521.09	

"B" Line Profile

28+26.27 "A" Line 24+12.98 "B" Line		0.93	521.08
24+42		0.95	521.06
+27		0.9	521.92
24+00		3.2	518.81
+58		4.7	517.31
+50		7.5	514.31
TP 0.46	511.44	11.03	510.98

3/4" I.P. 37.5 LT
40+67.83

3/4" I.P. TERT
36+98.=

NAIL IN PAVT. & LT
28+26.27

on Conc pavt

Edge Conc pavt.

545 5.2 3.4 / 0.8 / 4 / 10 / Edge AC

5.3 / 1.2 / 4.7 / 6 / 5.0 / 10 / Edge AC

4.9 / 1.5 / 4.9 / 10 / Edge AC

4.4 / 1.0 / 4.4 / 10 / Edge AC

3.9 / 0.5 / 4.0 / 3 / 3.5 / 10 / Edge AC

3.4 / 0.5 / 3.6 / 4 / 3.2 / 10 / Edge AC

2.1 / 5 / 2.9 / 10

2.45 / 1 / Edge AC / 2.2 / 10

2.1 / 1 / Edge AC / 2.1 / 2 / 2.4 / 10

0.3 / 6 / 0.9 / 3

2.0 / 6 / 3.2 / 3

6.3 / 6 / 6.2 / 3 / DIKE RAMP / 4.7 / 4 / 6.2 / 2

Muirland Pipeline Ext & Profile

"B" Line Profile

511+24

23+00		2.9	508.54
22+84		4.6	506.84
22+72.70	X PT	6.9	504.54
22+68		8.9	502.54
PI	0.15 499.14	12.45	498.99
22+67		7.3	491.84
PI	0.69 487.39	12.44	486.70
22+50		3.0	484.39
22+21		9.1	478.29
22+20		9.0	478.39
22+18		6.9	480.49
22+13.83	E.C.	6.1	481.29
22+04		6.6	480.79
22+00		8.8	478.59
21+87		10.8	476.59
PI	3.25 480.18	10.46	476.93
21+83		7.4	472.78
21+80		6.3	473.88
21+61		7.0	473.18
+50		8.1	472.08

Continued on Page 66-67 This Book

3.0/4 23+09 { End 2.5 RT. To RET. Brick Wall 1.0 High

Brick Ret. Wall 1.5 High

22+92.5 2.5 RT. To End of 3.5 Brick Wall

9.5/10 8.5/5 × 0.2/2 2.6/3

1.5/2 × 11.2/5

6.4/7 × 8.9/6 9.9/7

5.0/5 × 6.1/6

Bayview Con Line
7/28/49

Sta 1438.5

IP	0.19	432.88	432.69
1438^{45} BC		2.5	430.4
+50		4.3	428.6
2+00		13.7	419.2
+37		12.8	420.1
+50		13.9	419.0
3+00		11.0	421.9
+50		12.7	420.2
$3+67^{69}$ EC A		11.4	421.5
4+00		7.1	425.8
P	2.91	430.84	4.95 427.93
+25		2.8	428.0
+50		2.7	428.1
5+00		3.5	427.3
+50		6.7	424.1
6+00		10.4	420.4
+50		14.1	416.7
P Fence Post		13.04	417.80

$\frac{1.5}{30}$ $\frac{3.2}{23}$ $\frac{19.5}{10}$ $\frac{10.2}{30}$

$\frac{4.7}{30}$ $\frac{8.3}{17}$ $\frac{21.0}{30}$

$\frac{3.0}{25}$ $\frac{8.3}{6.0\ \text{Fen}}$ $\frac{13.0}{30}$

$\frac{3.6}{7.2\ \text{Fen}}$

$\frac{7.1}{7}$

$\frac{10.6}{7}$

$\frac{14.4}{7\ \text{Fen}}$

"P" Sta 30+36

BM #70 (City Dat) Elev. 112.155

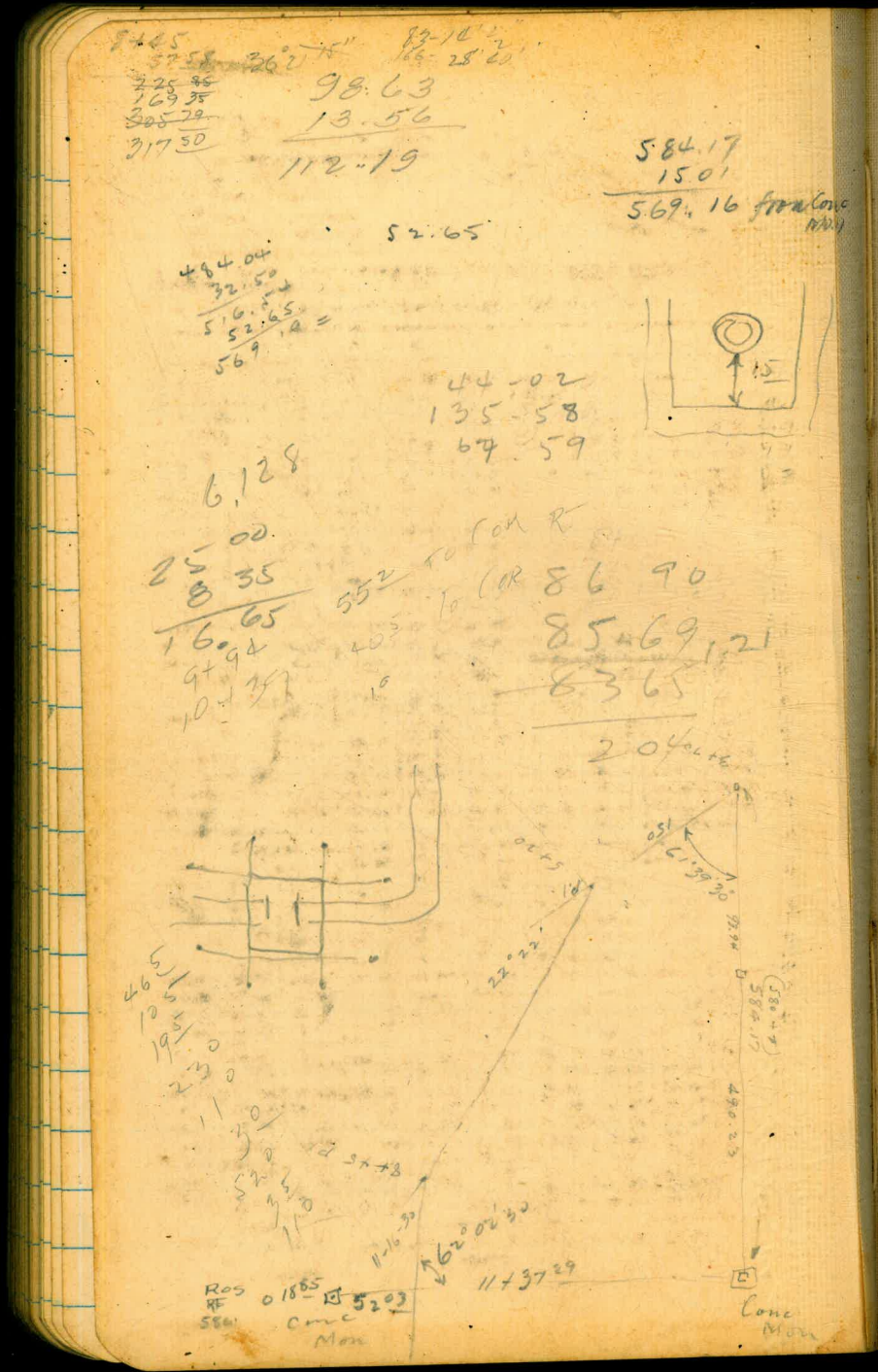
619
+30

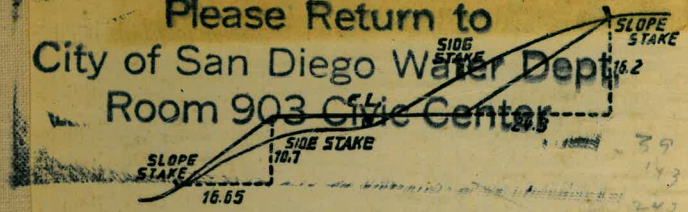
26+83.50 ← .89 Back of split

+79.50	
+76.50	3.00
+69.00	7.50
+62.00	7.00
+50	12.00
26+00	50.00
25+50	50
+25	25
	154.50

12.65 Bottom

79.50
25.00
54.50





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
HOLYOKE MASSACHUSETTS
NEW YORK CHICAGO BOSTON SAN FRANCISCO