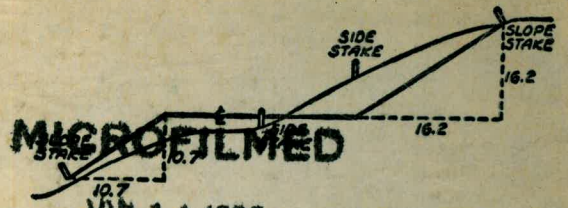


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	49.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

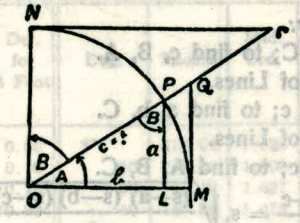


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \text{sos } B = LP$$

$$\text{sos } A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C'}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

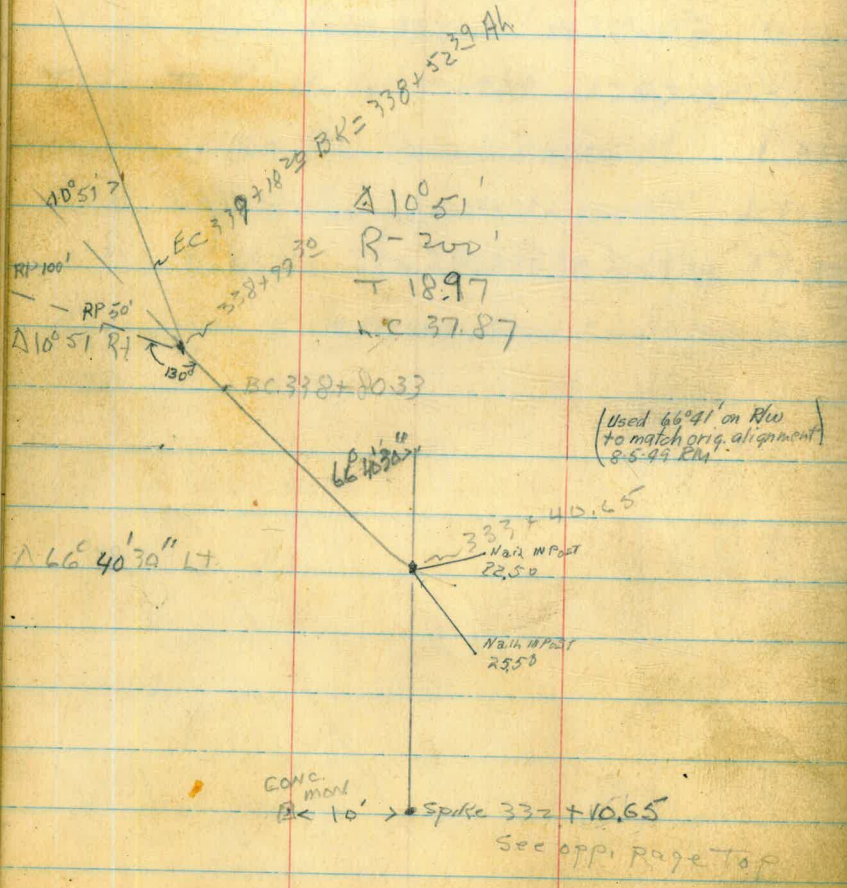
Indexed to p. 12 mgd 4/18/99

Page

Kearney Mesa P.L.
Alignment

Cont. from RK 771

Relocation - Sta 338+13.57 - 339+18.20



8-27-49
King Shipman West

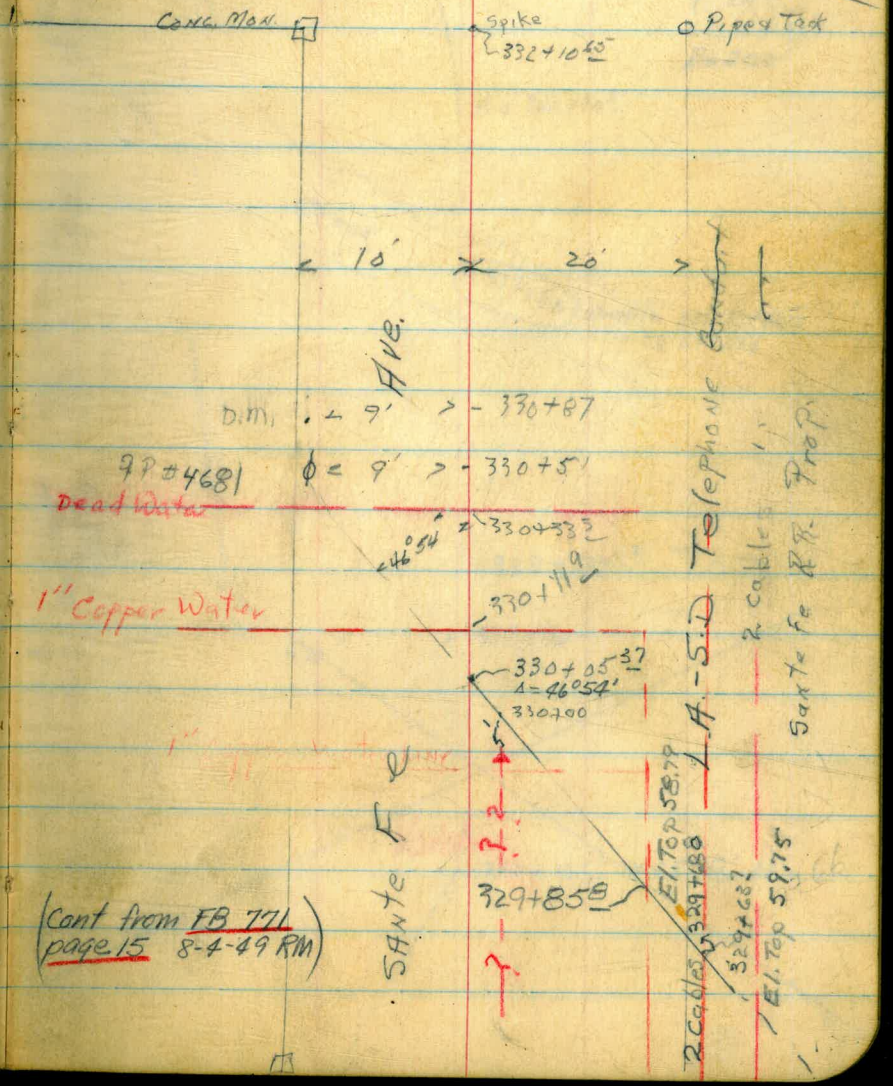
Void

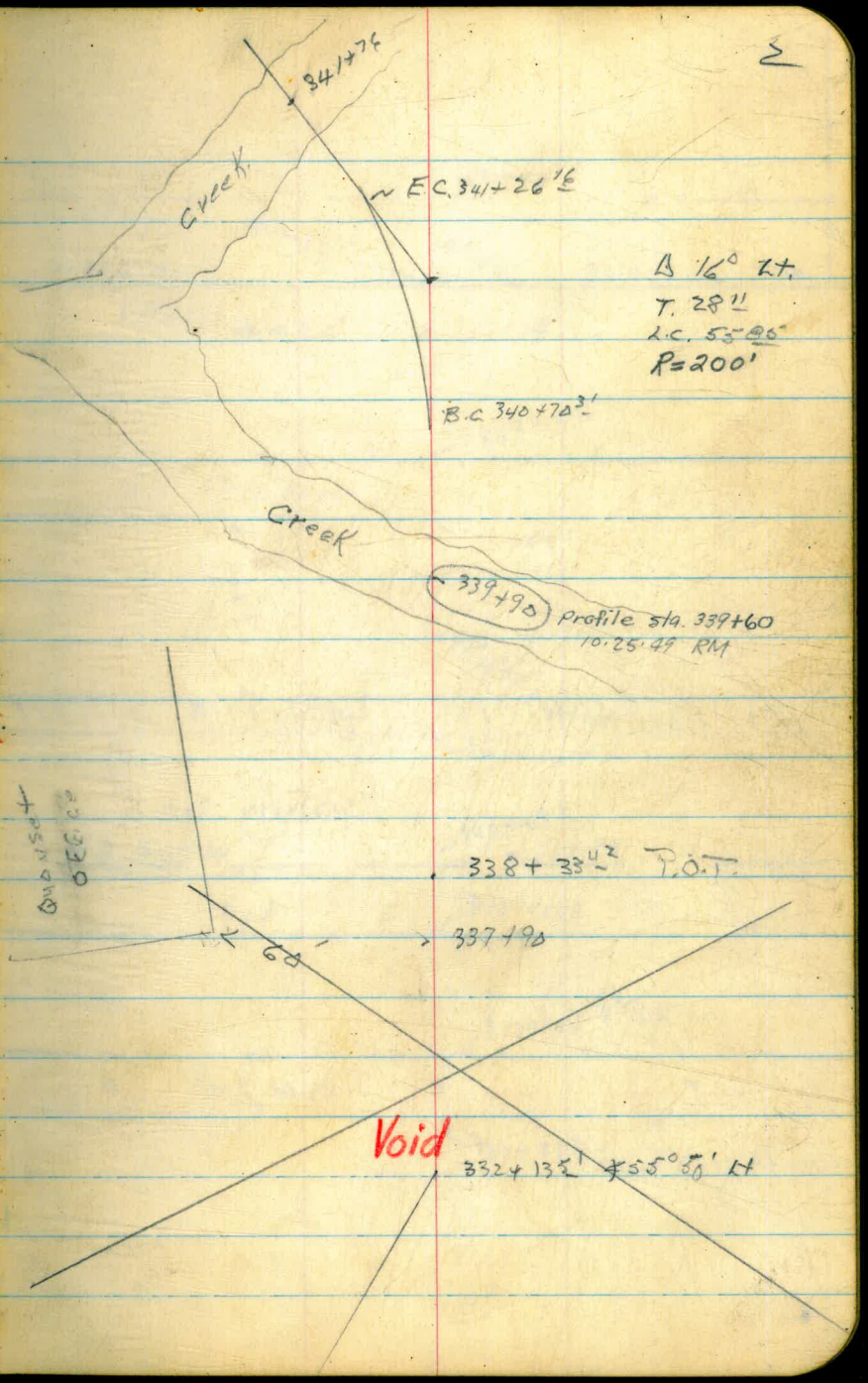
Cont from FB 771 pg. 15 RM

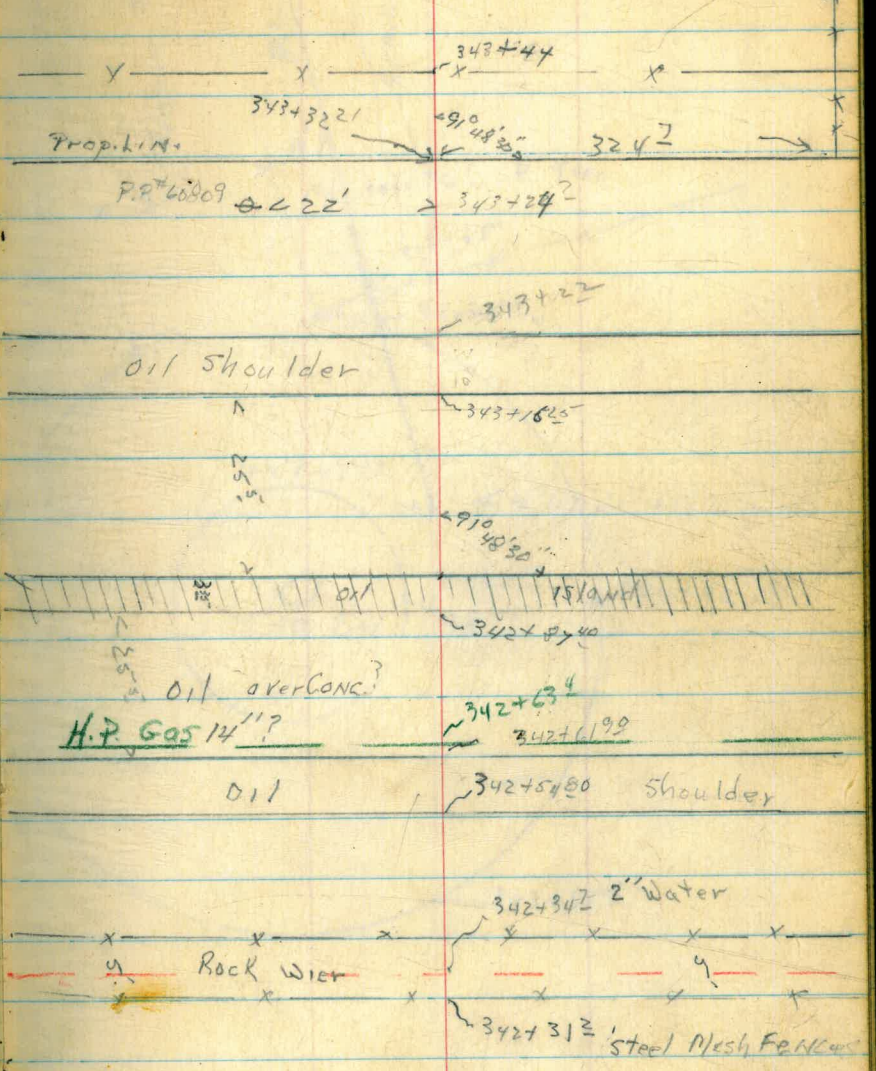
55° 50'

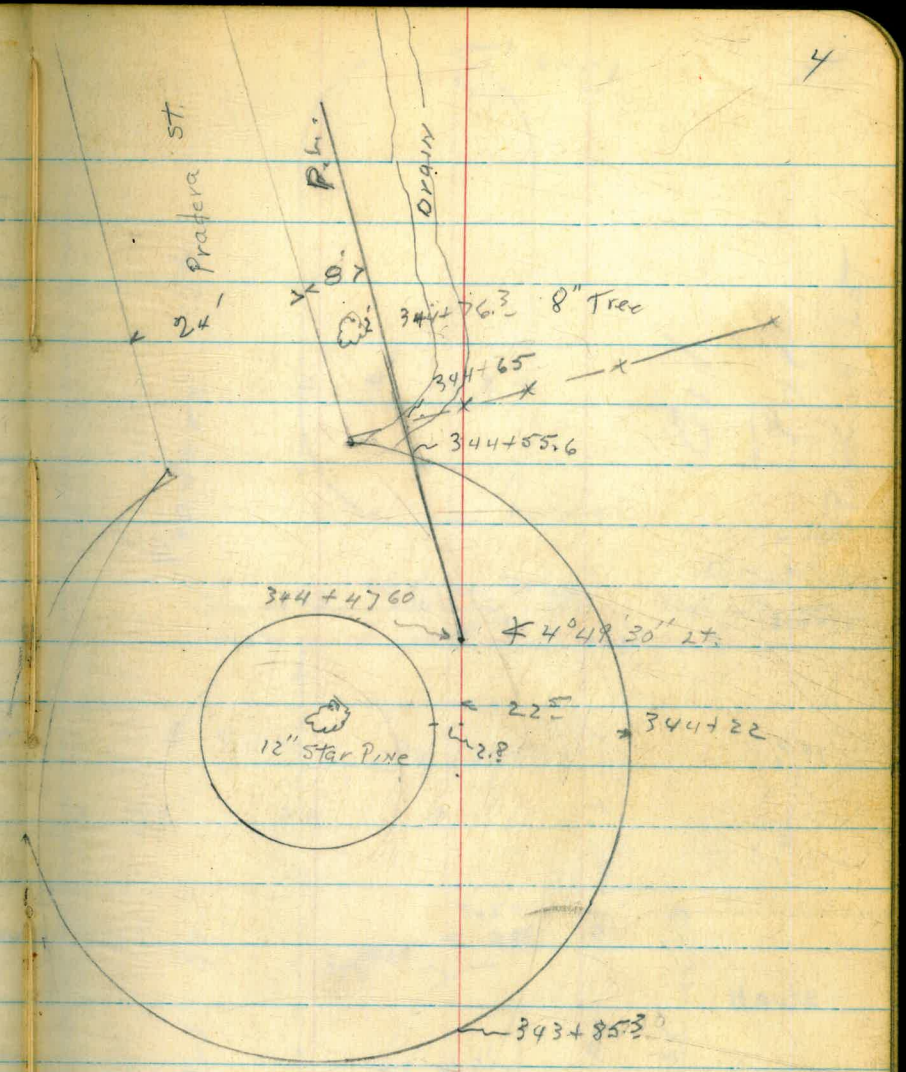
(See opposite page)

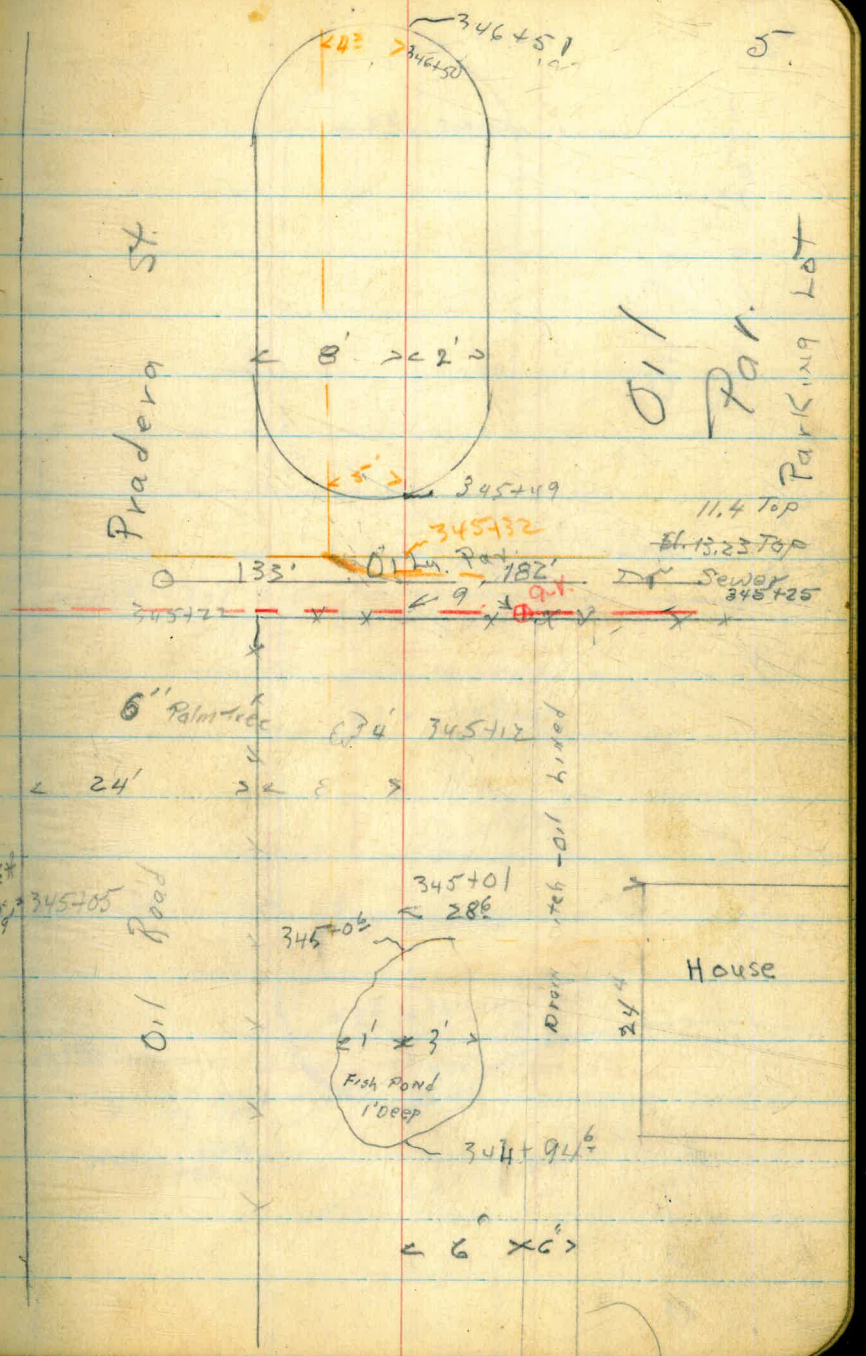
332+13.5'



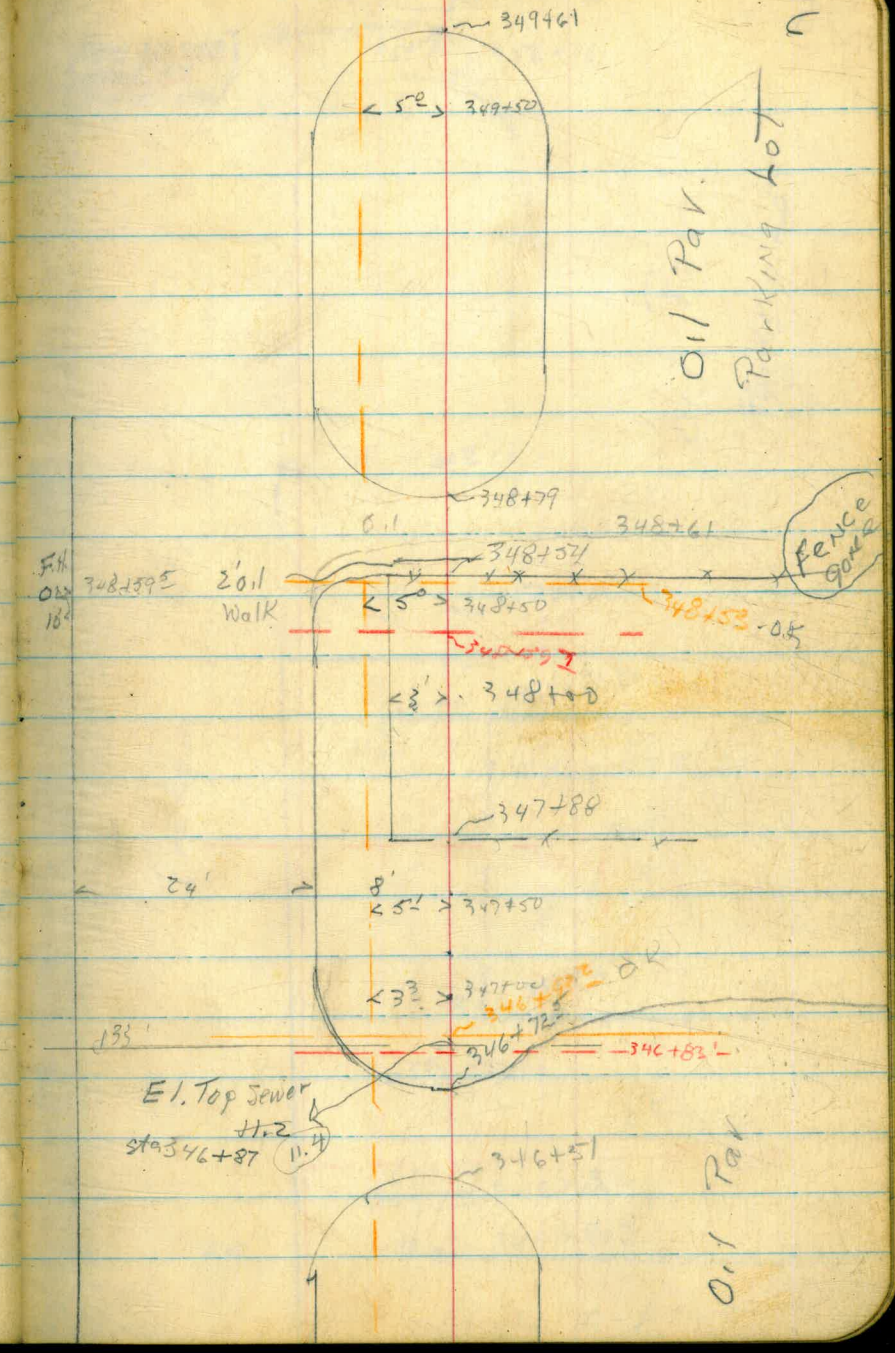

341+76
Creek
~ E.C. 341+26 16
Δ 16° Lt.
T. 28 11
L.C. 55 00
R=200'
B.C. 340+70 31
Creek
~ 339+90
Profile sta. 339+60
10.25.49 RM
338+33 42 P.O.T.
337+90
Void
332+13 ± 55° 50' Lt


343+44
343+32.21
Prop. Line
91° 48' 30"
324.7
P.P. 6+809
343+24?
343+22
Oil Shoulder
343+18.25
91° 48' 30"
Oil
15" CMP
342+40
Oil over Conc.?
H.P. Gas 14"?
342+63.4
342+61.99
Oil
342+54.80
Shoulder
342+34.7
2" Water
Rock Wier
342+31.2
Steel Mesh Fence

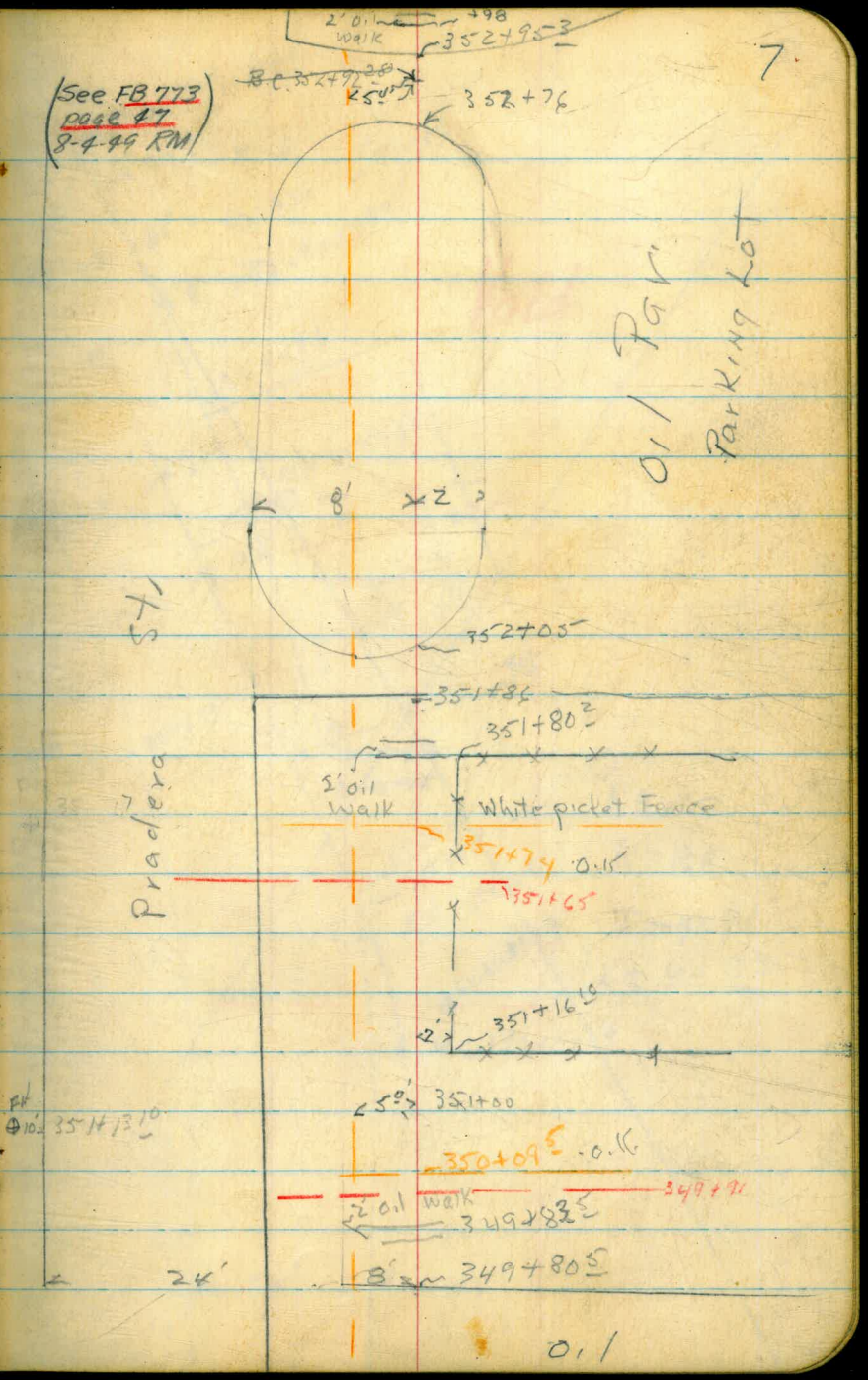

Prattera St.
Rd.
Drain
24'
8'
344+76.3
8" Tree
344+65
344+55.6
344+47.60
4°48'30" Lt.
22
344+22
12" Star Pine
2.8
343+85.3

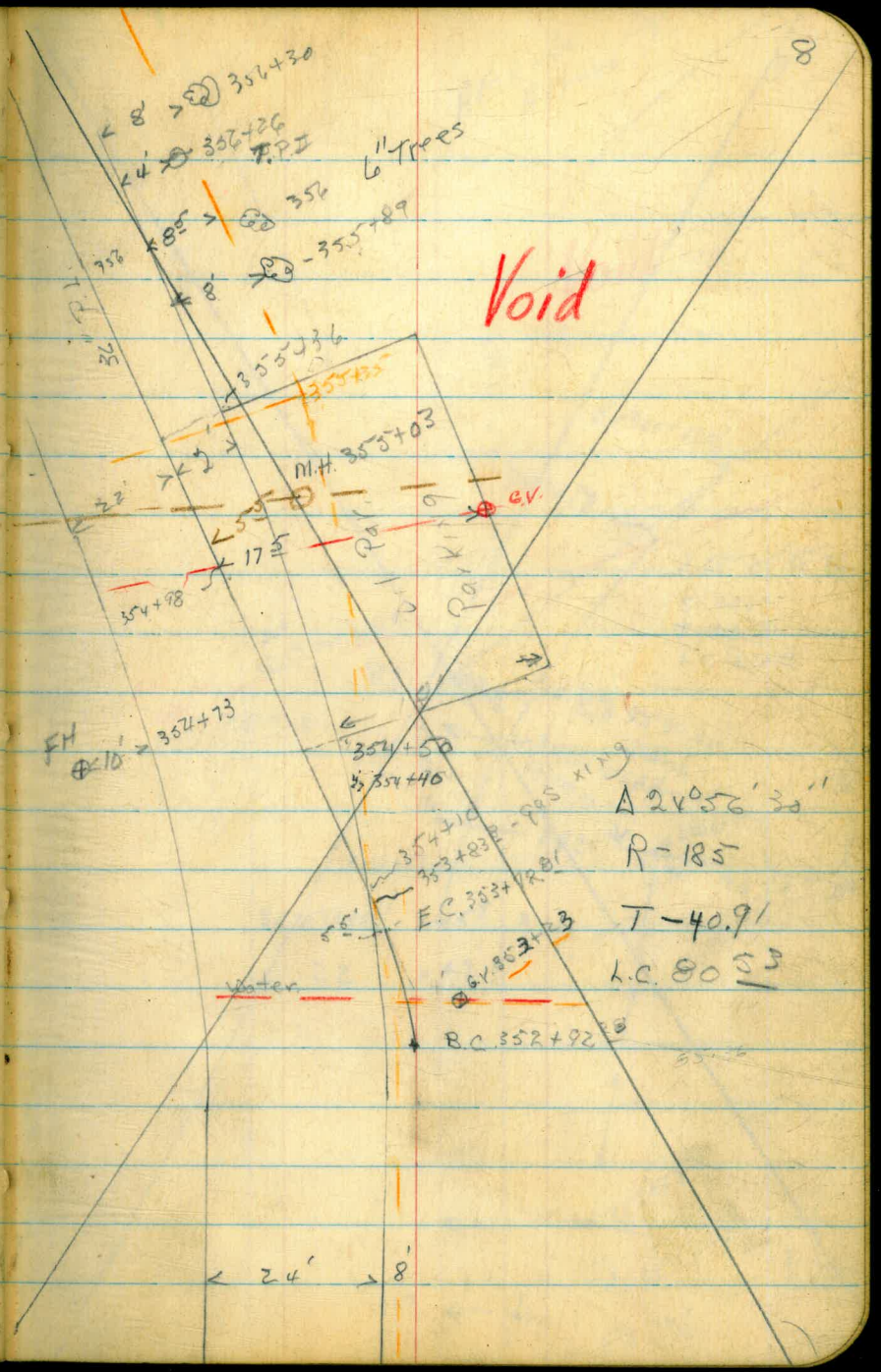


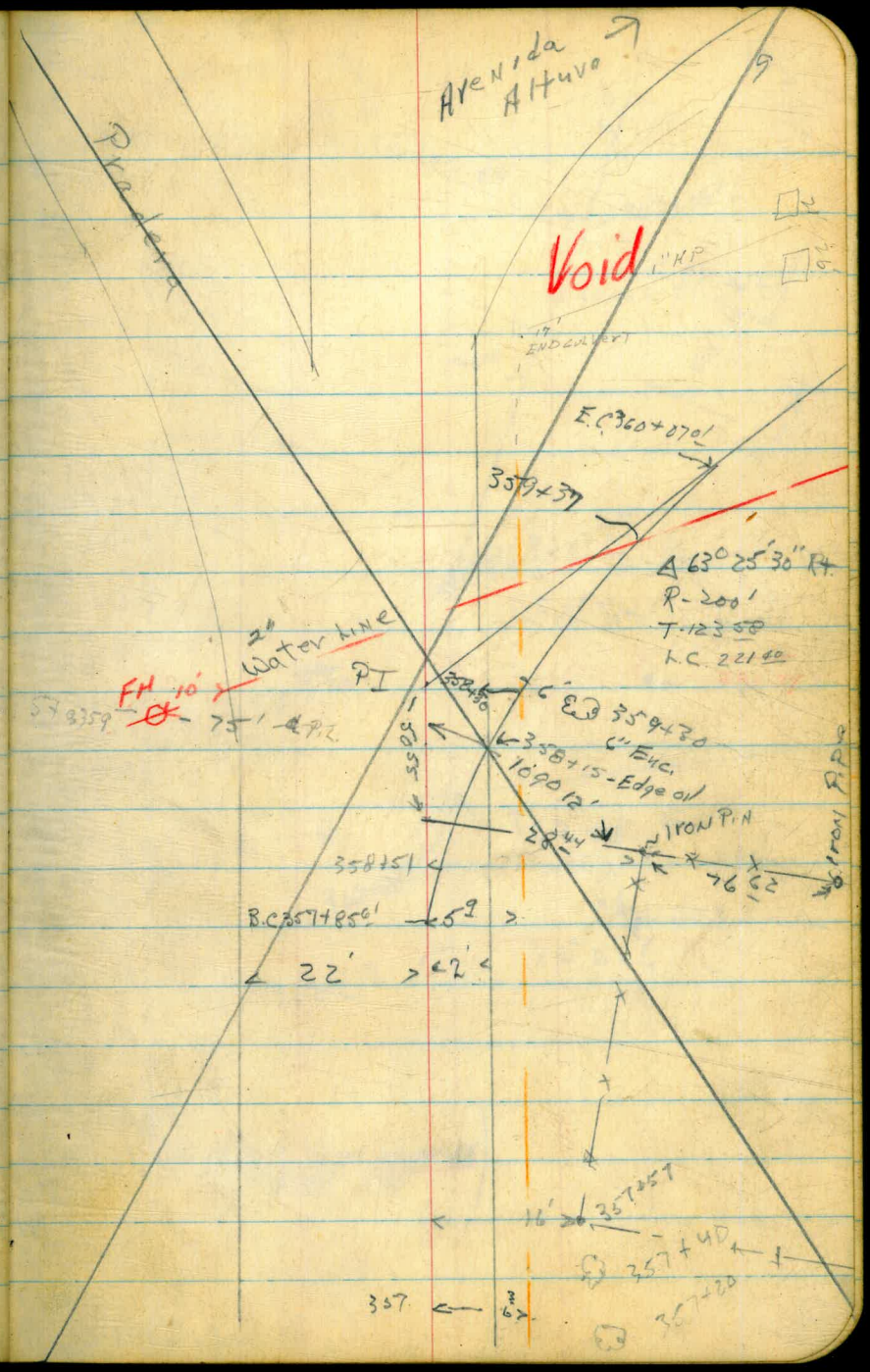
15.2
3.0
18.2
6.8
11.4

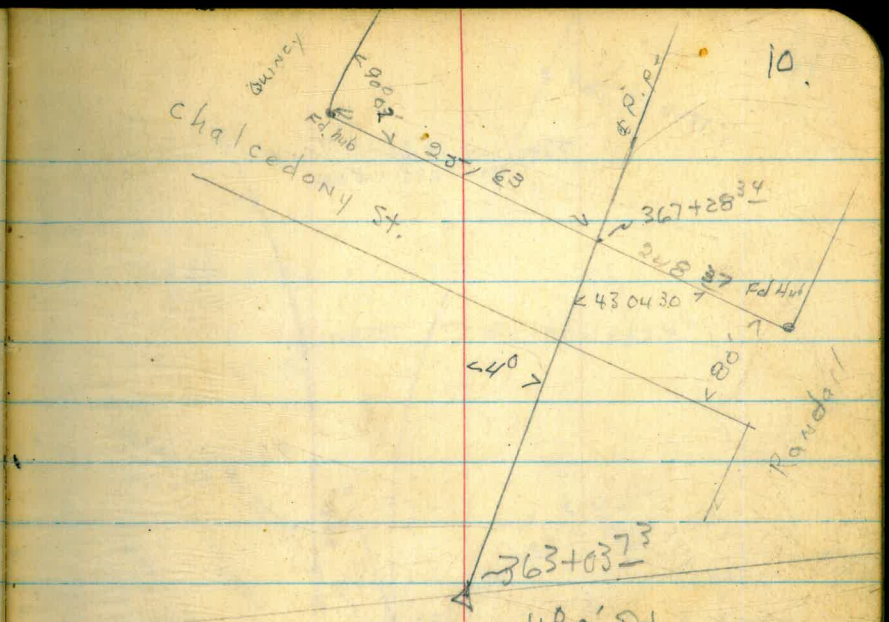

349+61
5%
349+50
Oil Rd.
Parking Lot
348+79
6:1
348+61
348+54
Fence
Gate
F.H.
Oil
18"
348+59
2'0:1
Walk
5%
348+50
348+53
-0.5%
3%
348+00
347+88
24'
8'
5%
347+50
3%
347+00
346+83
-0.5%
346+72
346+83
13%
346+87
El. Top Sewer
Ht. 2
sta 346+87
11.4
346+51
Rd
0:1

(See FB 773 page 87 8-4-99 RM)




Void
6" Trees
M.H. 355+03
G.V.
FH @ 10' → 354+73
Water
Δ 21°56'30"
R - 185
T - 40.91
L.C. 80.53
B.C. 352+92
24'
8'


Avenida Altuvo
Void
E.C. 360+07.01
359+37
Δ 63° 25' 30" Rt.
R- 200'
T. 123.58
L.C. 221.40
2" Water Line
FH 10'
75' ± P.I.
P.I.
359+30
6" E.C.
358+15 - Edge of
1090 ft.
IRON PIN
B.C. 357+85.01
22'
42'
16'
357+57
357+40
357+20
357



Corte Cresta ?
Oil Pav.

362+92 ? 6" Water

Dead End

362+81.5

362+88 ±

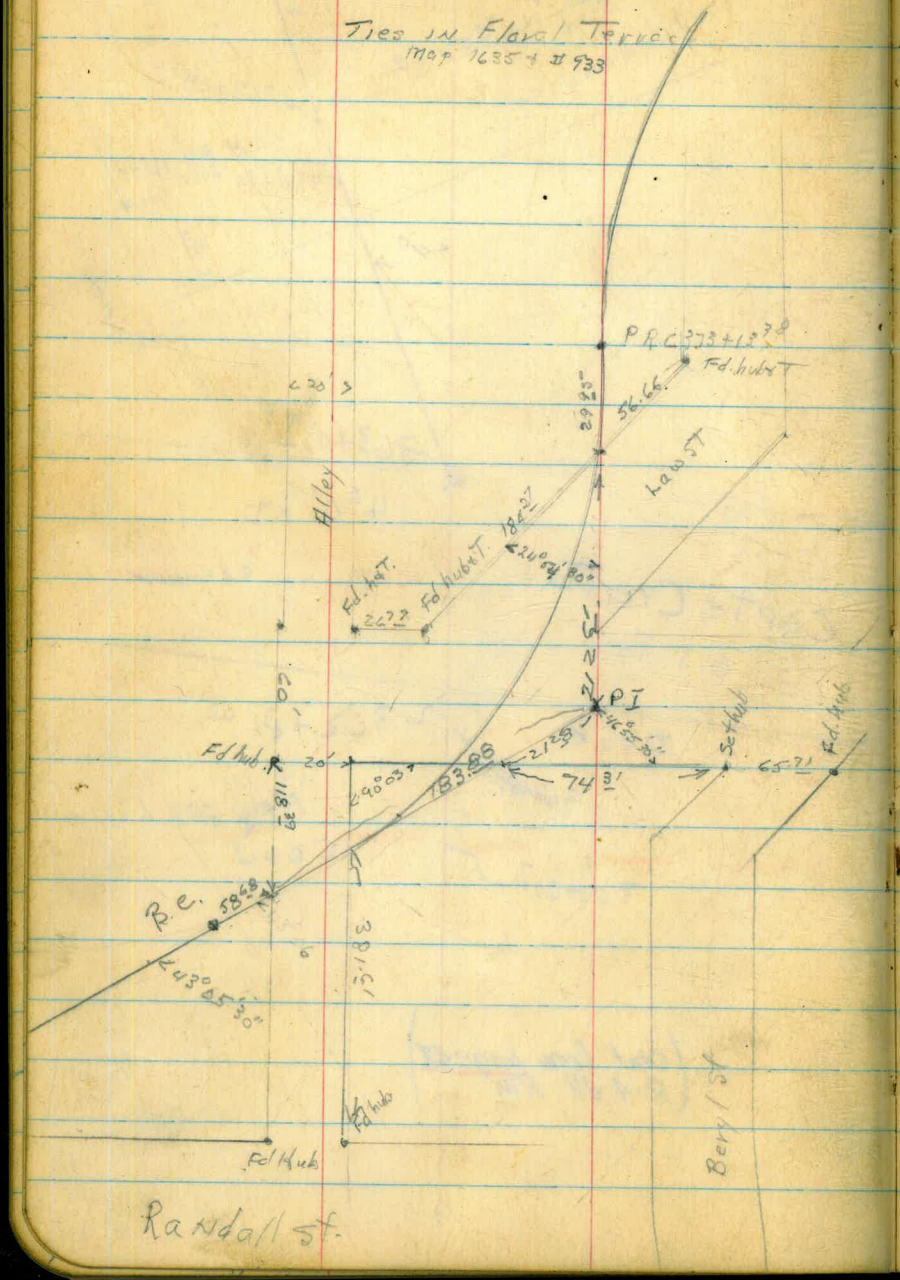
New gas Line

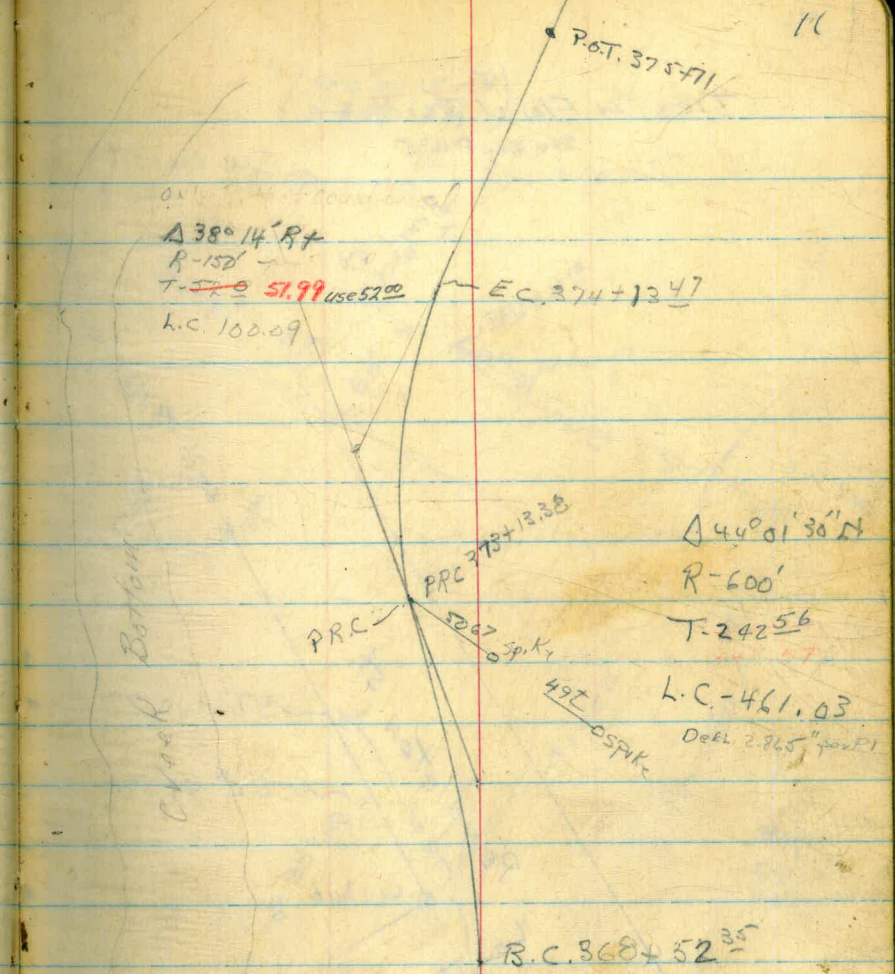
362+60.7

7 ± Down

(cont. from page 48
8-4-49 RM)

Ties in Floral Terrace
Map 1635 + # 933

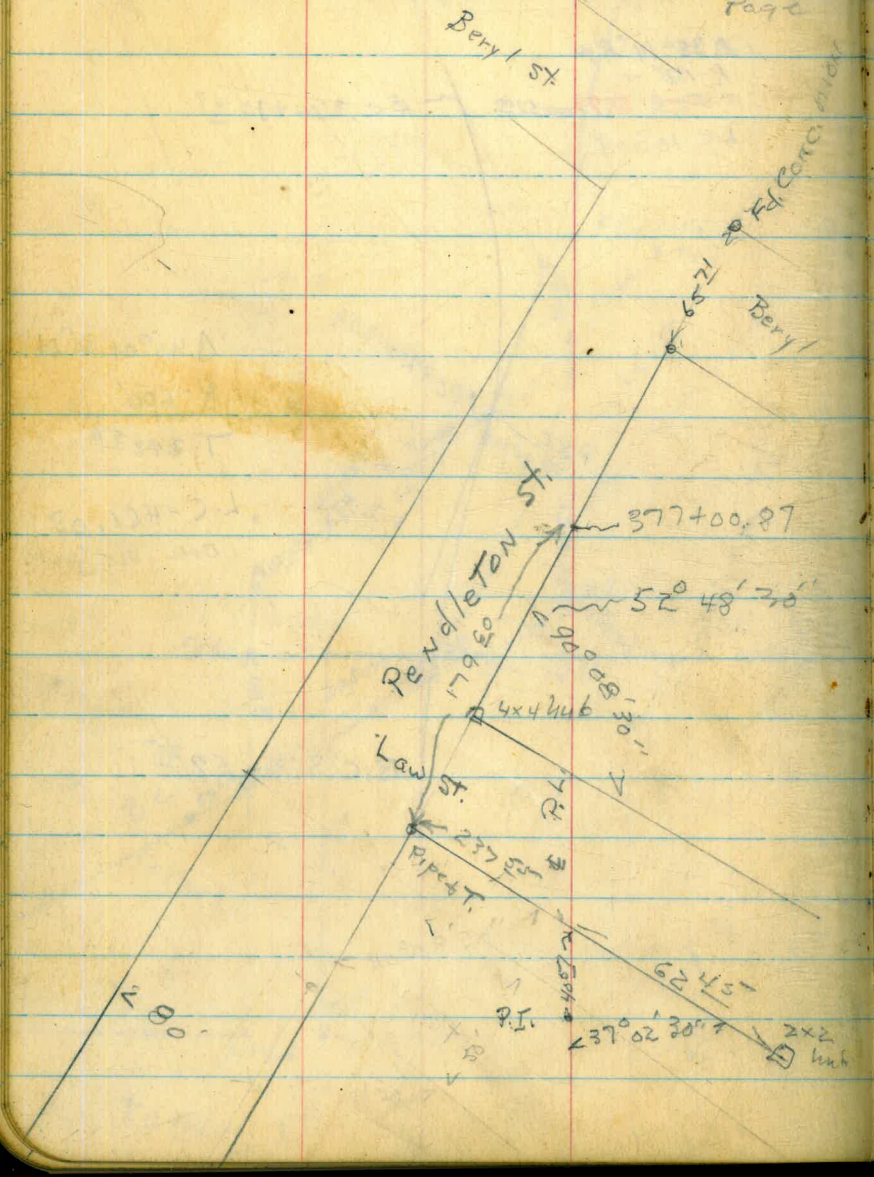




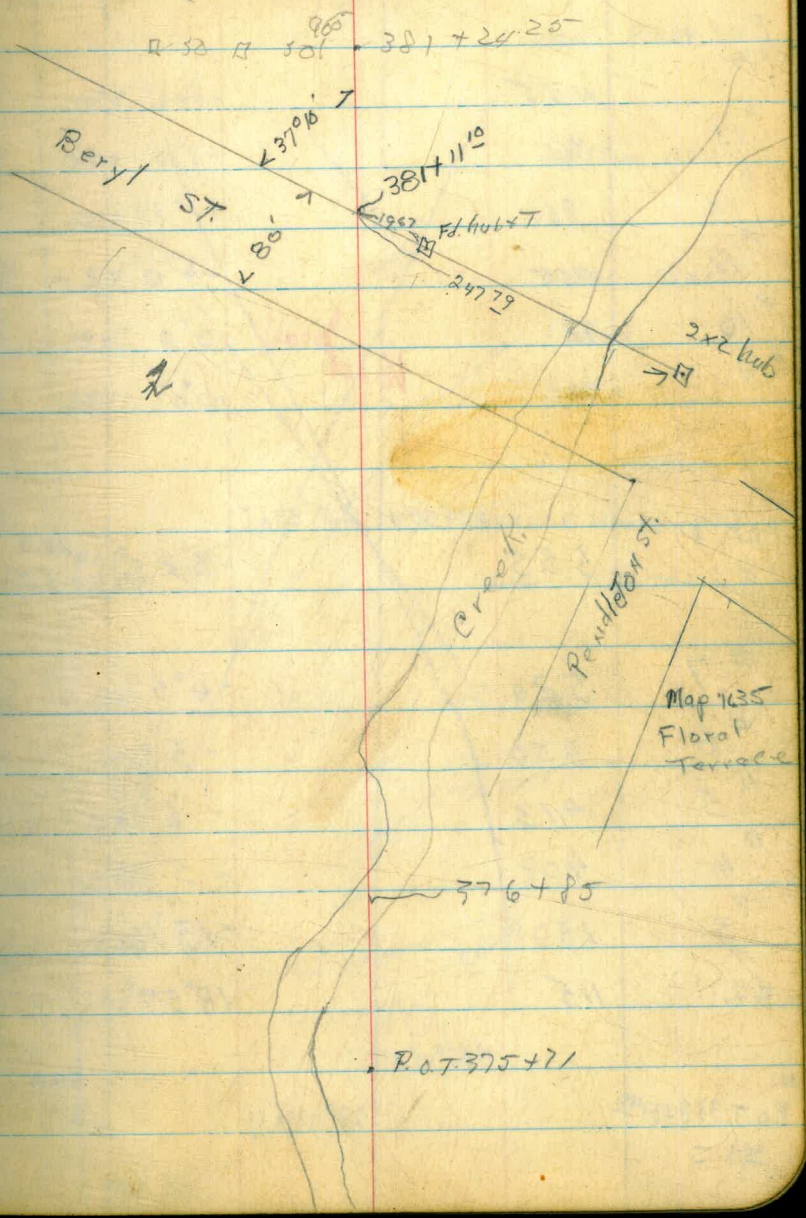
Ties in Floral Terrace

See Map #1635

See opposite Page

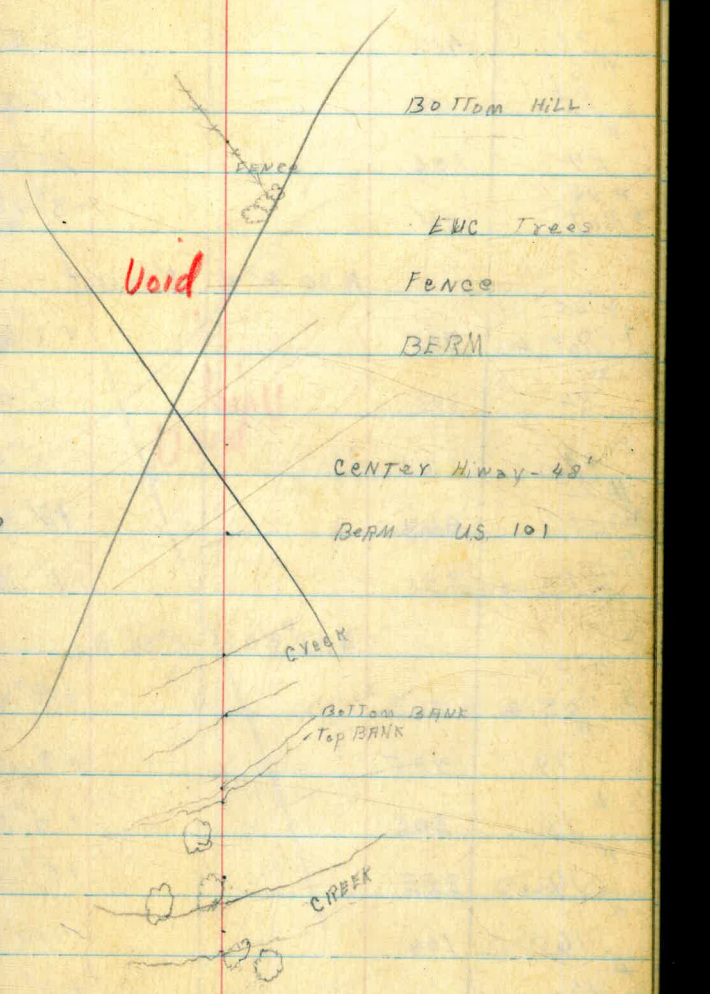


(See page 28 8-4-99 RM)



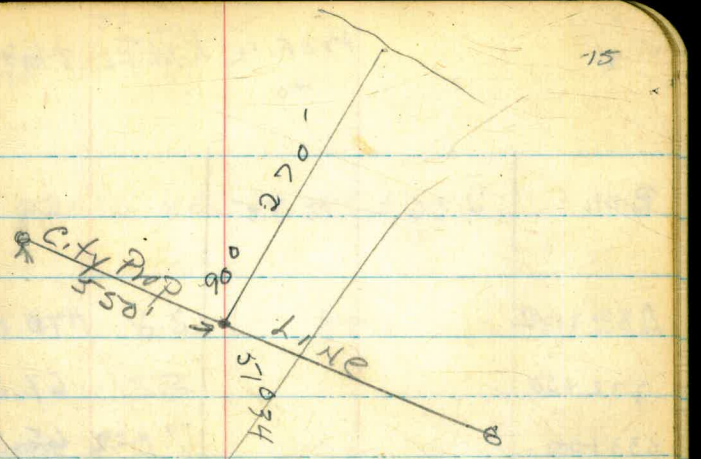
Sta. #	Dist.	Bearing Hor. L	Vert.	Elv.
POT *				
#14	1155		+4°46'	
#13	960		+2°10'	
#12	760		+1°30'	
#11	405		-4°0'	
#10	92'		0°0'	
#9	82'	Void	00°0'	
		S80°30'W	85°33'T	
POT *				28.0
#8	555		-3°25'	5.2
#7	520		-4°59'	
#6	450		-5°31'	
#5	413		-6°00'	
#4	409		-5°33'	
#3	150		-13°16'	
#2	115		-18°57'	
		N55°45'W		
* P.O.T. 338+33.47		28°47'30" Rt		60.0
#1 =				5.2

Rod	Elev.
5.2	118.4
5.2	59.0
5.2	42.7
5.2	-5.4
8.5	19.5
4.9	23.1
5.2	21.8
5.2	22.80
5.2	9.8
5.2	11.7
5.2	11.9
5.2	15.5
8.0	18.5
15.0	9.7
	54.80



STA	Dist	BEARING	HOR ∠	VERT ∠	HI	Rod	ELEV	
# 30	635			- 2°46'		5.2	257.0	
# 29	410			- 3°29'		5.2	262.8	
# 28	182			- 13°12'		5.2	247.2	
# 27	106			- 23°0'		5.2	249.5	
# 26 * P.O.T.	170			- 3°43'	292.8 5.2 303.8	5.2	287.6	
		N 70 45 W	18°54'30" RT		5.2			
# 25 * P.O.T. ∠	365			+ 1°03'		5.2	298.6	
# 24	295	Void		0° 0		11.4	285.7	
# 23	210			0° 0	5.2	5.5	291.6	Void
# 22 * P.O.T.	643			+ 2°12'	297.1 ?	5.1	291.9	
# 21	231			+ 1°52'		5.1	274.8	FENCE
		N 52°30'W	12°34' RT		272.4 5.1			
# 20 * P.O.T. ∠	663			+ 9°31'		5.4	267.3	TOP HILL
# 19	495			+ 9°55'		5.1	243.2	
# 18	306			+ 6°55'		5.1	195.9	
# 17	222			+ 6°01'		5.1	182.4	BANK CANYON
# 16	104			- 10°49'	5.1	5.1	140.1	BOTTOM CANYON
# 15 * P.O.T.	548			+ 4°17'	164.4 123.6		159.3	BANK OF CANYON
# 14 * P.O.T. ∠		N 65° W	15°56'30" RT		5.2	5.2	118.4	

STA	DIST	BEARING	HOR ∠	VERT ∠	H.I	ROD		
# 42 ∠	1082	Void		+4° 57'				
# 41	810			+2° 37'		5.6	434.4	435.85 ON South Prop' Line
# 40	390			-10° 45'		5.0	385.2	
# 39	225'			-22° 16'	5.0	5.0	276.7	
* # 38 POT	113			-1° 59'	353.2 5.1	5.0	269.3	EAST Edge BANK 40' BACK
* # 37 POT	226			+2° 31'	364.2	12.1	348.2	
		N 58° 30' W	13° 32' 35" ST		359.0 5.1	12.0	359.1	
* # 36 POT ∠	215			+ 6° 58'		5.1	353.9	Checked & Reduced pages 13-15 incl. 5-11-49 RAM
* # POT 35	1328			+1° 40'	331.3 5.1	5.2	326.2	
# 34 ½	1176			+ 0° 20'		5.2	294.4	
# 33 ½	1040			-2° 52'		5.2	235.7	
# 32	1003 (776)			-3° 59'		5.2	218.2 223.7	
# 31	785'			-5° 28	5.1	5.1	213.3 219.1	
		N 70 45 W			5.2			



Profile K.M. P.L. Sta 332+13.5 ℄
to

B.M.	2.06	72.75 ✓			70.69
A 332+13.5 ℄			2.8	70.0	
332+50			5.3	67.5	
333+00			7.6	65.2	
333+50			8.4	64.4	
334+00		Void	~~8.5~~ 8.3	~~63.3~~ 64.3	
334+50			9.1	63.7	
335+00			13.2	59.6	
335+50			14.9	57.9	
336+00			15.2	57.6	
336+06			15.0	57.8	
336+24			5.3	67.5	
336+50			5.1	67.7	
337+00			6.6	66.2	
337+50 ✓			8.8	64.0	
T.P.	0.30	61.77	11.28	61.47	

King
Shipman
West-

5-16-49
Rain

16

Top Conc. Mon 76+27+332+10.6 ℄ B.K 770 P.68

Lt. Rt.

See page 32
9.16.49 RM

0.0 / 20

+1.0 / 14 +10.4 / 28 +11.0 / 30

Bottom bank

Top bank +10 / 20' 0.0 / 6'

0.0 / 30'

00 / 10'

+1.0 / 20'

61.77

338+00	Void		3.8	58.0
338+33			7.3	54.5
338+50			13.0	48.8
T.P	0.65	50.22	12.20	49.57
338+82			10.6	39.6
T.P	0.18	39.59	12.81	39.41
339+00			11.2	26.4
T.P.	1.12	28.67	10.04	27.55
T.P	5.58	22.08	12.17	16.50
339+54			14.7	7.4
339+67			14.7	7.4
339+73			11.6	10.5
339+81			11.8	10,3

Top of BANK

(Cont. from page 32
8-4-49 RM)

Bottom creek
" "

		22.08		
339+94			6.1	16.0
340+00			4.9	17.2
340+50			6.3	15.8
BC340+70 31			7.4	14.7
341+00			7.7	14.4
EC341+26 16			9.2	12.9
341+36			10.0	12.1
341+44			12.3	9.8
341+50			12.5	9.6
+63			12.6	9.5
+72			13.7	8.4
+80			13.7	8.4
+82			12.7	9.4
342+00			11.8	10.3
T.P.	1.40	22.18	1.30	20.78
342+31			6.9	15.3
342+33			3.6	18.6
342+43			1.5	20.7

Creek

		22.18			
	342+54		1.3	20.9	Edge o.l
	342+87.40		0.80	21.4	
	342+87.60		0.40	21.8	Top ℄ Isle 21.78
B	342+90.75		0.49	21.67	℄ Isle
	342+90.95		0.91	21.27	
E	343+27		1.50	20.68	Edge o.l
	343+31		5.7	16.5	
	343+44		7.2	15.0	
	343+50		7.2	15.0	
	343+85.3		6.8	15.4	Edge o.l
	344+00		7.3	14.9	
	344+47.60		7.8	14.4	
	T.B.M.	2.71	19.80	5.09	17.09	Extreme Top F.H. 344+05
	344+55.4			5.0	14.8	
	344+64			5.0	14.8	
	+65			6.0	13.8	bottom gutter
	344+70			4.6	15.2	

57
47
1.6

19.80

345+01	6' Rt	4.7	15.1
		6.3	13.5
345+22		4.9	14.9
345+49		5.0	14.8
345+49	6' Rt	6.0	13.8
346+00		4.5	15.3
346+00	-10 Rt	5.6	14.2
346+51		5.0	14.8
346+51	6' Rt	5.6	14.2
346+72.5		5.0	14.8
347+00		5.1	14.7
347+50		5.2	14.6
348+00		5.2	14.6
348+50		5.2	14.6
348+61		5.3	14.5
348+79		5.5	14.3
349+00		5.5	14.3
349+50		5.8	14.0
349+61		5.8	14.0
349+80.5		5.7	14.1
350+00		5.6	14.2

Gutter
Edge 0.1
" "
gutter

Gutter
0.1
gutter
Edge 0.1

Edge 0.1
" "

Edge 0.1
Edge 0.1

19.80

350+50			5.6	14.2
351+00			5.8	14.0
T.B.M.	9.15	25.33	3.62	16.18
351+50			11.0	14.3
351+86			11.1	14.2
352+05			11.0	14.3
352+50			10.1	15.2
350+76			8.9	16.4
B.C. 352+92.28			8.0	17.3
+95.3		Void	7.8	17.5
353+00			7.4	17.9
353+50			3.6	21.7
E.C. 353+72.81			2.5	22.8
354+00			1.0	24.3
T.P.	10.81	35.75	0.39	24.94

Extreme top F.H. 351+13 1+

Edge 0.1

Edge 0.1

(See page 49
8-4-49 RM)

	35.75		
354+10		11.2	24.5
354+50		9.5	26.2
355+00		7.5	28.2
355+50	Void	5.0	30.7
356+00		3.2	32.5
356+50		1.9	33.8
357+00		0.9	34.8
357+50		0.4	35.3
BC 357+85.4		0.3	35.4
T.P.	8.63	43.16 1.22	34.53
358+00		7.5	35.7
358+15		7.2	36.0
358+50		5.4	37.8
359+00		5.3	37.9
359+50		4.2	39.0
360+00		2.6	40.6
EC 360+67.01		2.5	40.7

Edge 0.1

(cont. from page 50)
8-4-49 RM

43.16

B.M.	12.20	55.48	4.88	38.28		Extreme Top F.H. 4 3 5 9 4 0 W
360+50			7.8	43.5		
361+00			3.6	46.9		
361+50			0.4	50.1		
T.P.	13.01	60.86	2.63	47.85		
363+00			7.7	53.16	53.2	
362+50			4.0	56.86	56.9	
362+81.5			2.7	58.16	58.2	Edge of
363+03.73			1.5	59.36	59.4	
363+06			1.7	59.16	59.2	
363+20			6.8	54.06	54.1	
363+50			8.1	52.76	52.8	
364+00			9.0	51.86	51.9	
364+50			9.7	51.16	51.2	
365+00			5.3	55.56	55.6	
T.P.	12.75	68.50	5.11	55.75		

	+		-	
365+50		68.50	13.0	55.5
366+00			10.7	57.8
366+16			9.4	59.1
366+50			5.8	62.7
367+00			6.0	62.5
+16			6.4	62.1
+50			1.9	66.6
T.P.	12.91	79.02	2.39	66.71
368+00			4.2	74.8
BC 368+52.33			6.7	72.3
T.P.	6.27	83.71	1.58	77.44
369+00			8.6	75.1
369+50			0.3	83.4
370			+2.8	86.5
370+50			4.5	79.2
370+60			0.5	83.2
T.P.	12.85	95.83	0.73	82.98

Lt

Creek

80.7
-3.0
25

77.7
-6.0
25

75.6
-8.1
25

88.3
+4.6
25

Rt

88.4
+4.7
25

91.7
+8.0
25

89.1
+9.4
25

90.7
+7.0
25

95.83

371+00			10.6	85.2
371+50			12.4	83.4
372+00			10.6	85.2
372+50			6.3	89.5
373+00			2.0	93.8
P.R.C. 373+13.39			1.1	94.7
T.P.	6.03	100.76	1.10	94.73
373+25			4.6	96.2
373+50			4.5	96.3
373+75			5.2	95.6
374+00			7.2	93.6
E.C. 374 +13.47			8.0	92.8
374+50			7.6	93.2
T.P.	8.21	106.32	2.65	98.11
375			7.1	99.2

Lt

86.2 −7.6 = 25'

88.8 −7.0 = 25'

88.2 −7.6 = 25'

85.4 −10.4 = 25'

88.7 −7.6 = 25'

93.8 −7.0 = 25'

86.8 −14.0 = 25'

87.4 −13.4 = 18' creek

94.8 −6 = 25'

95.8 −5.0 = 30'

99.8 −6.5 = 25'

Rt

107.9 +12.1 = 25'

106.5 +10.7 = 25'

106.2 10.4 = 25'

108.0 +12.2 = 25'

82.8 13.0 = 25'

+6

107.4 +6.6 = 25'

107.6 +6.8 = 25'

108.0 +7.2 = 25'

100.3 −6.0 = 25'

106.32

375+50			6.3	100.0	
376+00			8.7	97.6	
376+50			6.7	99.6	
376+79			8.7	97.6	
376+94			10.4	95.9	
377+00			8.2	98.1	
377+27			7.2	99.1	
377+31			9.3	97.0	
377+47			8.3	98.0	
377+50			6.7	99.6	
377+57			6.1	100.2	
+79			7.3	99.0	
378+00			0.00	106.3	
T.P.	12.98	118.14	0.96	105.36	
378+50			5.0	113.1	
T.P.	12.32	130.04	0.42	117.72	

Lt
98.9
-7.6
25'

102.9 -3.4 25
100.3 -6.0 22
103.2 -3.1 18
103.8 -5.0 25
101.8 -4.8 18
Creek
100.8 -5.5 13
103.5 -2.8 7

Creek
115.0 +8.7 25'

Creek
116.0 +9.7 25'
108.8 +2.5 11
104.3 -2.0 7
104.3 -2.0 2'

Creek
110.7 +4.1 25'

122.7 +4.6 25'

Rt
113.0 +6.7 25'
113.1 +6.8 25'
108.1 +1.9 12
113.0 +6.7 25'

112.7 +6.4 25'

108.5 +2.2 14
114.0 +7.7 25'

105.5 -0.8 10
101.0 -5.0 18
102.7 -3.6 22
103.1 -3.2 25'

114.6 -3.5 25'

		130.04		
379+04			12.3	117.7
379+50			4.5	125.5
T.P.	12.73	142.14	0.63	129.41
380+00			8.1	134.0
T.P.	12.51	154.14	0.51	141.63
380+50			11.9	142.2
381+00			3.4	150.7
T.P.	12.08	165.85	0.39	153.75
Pot. gutter 381+24.21			10.39	155.44
381+50			8.0	157.8
382+00			3.8	162.0
T.B.M.			3.76	162.07

Contd. Page 33

Lt

133.6
+3.6
25'

133.4
+3.4
25'

146.4
+4.3
25'

157.1
+3.0
25'

157.0
+2.9
25'

Rt

126.5
-3.5
25'

124.0
-6.0
25'

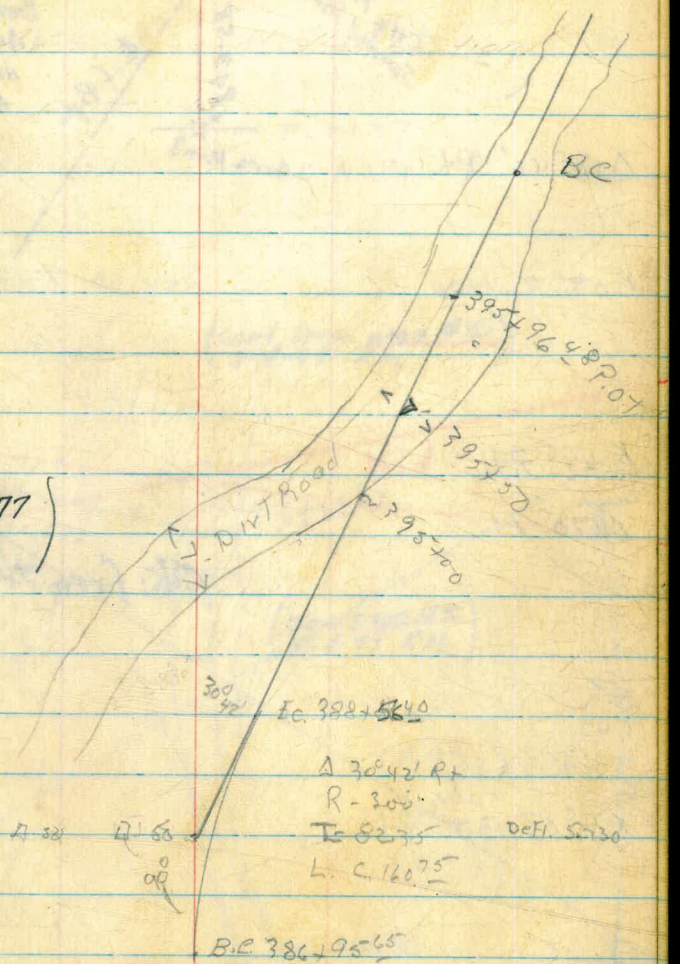
136.5
-5.6
25'

150.0
-4.1
25'

150.5
-3.8
25'

Top gutter Sta. 382+00
(See page 33
8-4-49 RM)

Checked & Reduced
pg. 16-27 7-15-49 RAM

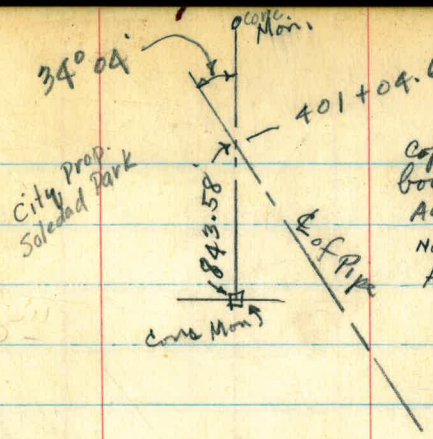


(See page 77 for ties 8-5-49 RM)

(Cont from page 12 8-4-49 RM)

Δ 30° 42' Rt. Ft.

82.35
386+95.65
381+24.25
1.40
82.35
385+75



Copied in this book by W.H. Aug. 3, 1949
Notes by King Aug 1, 1949

Δ 13°40' Rt

P.O.T. 401+00

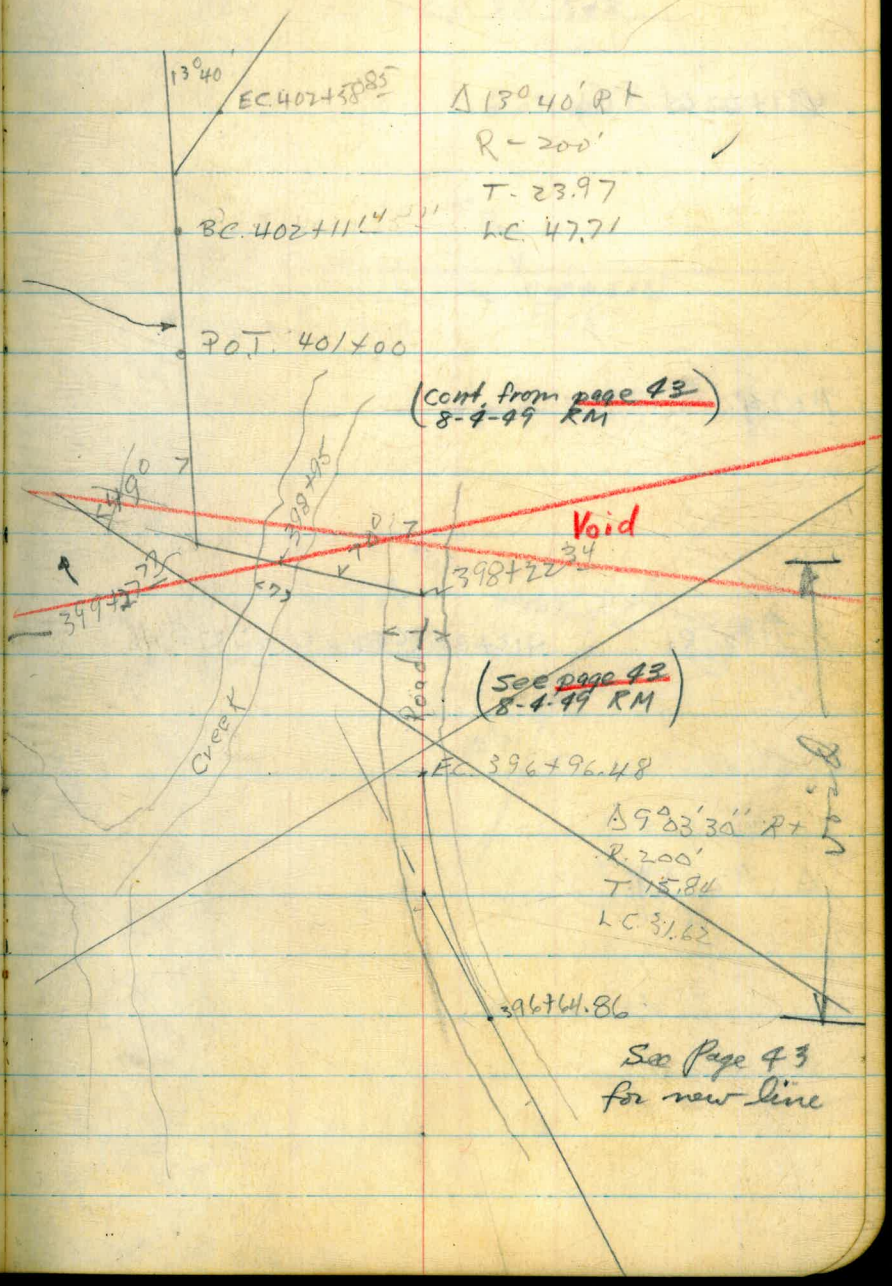
Δ 49° Rt.

Δ 70° Lt.

O.K. from this Sta. ahead

Δ 9°03'30" Rt.

401+04.63



Δ 13°40' Rt
R = 200'
T. 23.97
L.C. 47.71

(See page 78 for Res. Prop. Lines 8-5-99 RM

421+62.61 P.O.T.

P.O.T 415+29.46

Δ 7°52' Rt

412+36.96 BK = 412+37.56 Ahd.

Δ 12°21 Rt.

Kearny Mesa Rd. to tie into 30" Spigot at Sta. 422+56.74 (25.55' North of South Prop Line) (offset on Bayview Res = S 392.45')
R.A.M. 7-15-99
Inv. El. of 30" spigot = 431.5

City Prop Line N ON Res

422+31.19

30

P.O.T. 421+62.61

City Prop Line

Soledad Terrace

Park

P.O.T 415+29.46

P.O.T.

Δ 7°52' R.
R = 200
L.C. 27.46
T = 13.75

7°52' Rt

412+37.56 Ahd
412+36.96 BK =

412+09.52 P.C.

12°21

EC 408+79.83

Δ 12°21 Rt.
R = 200'
T = 21.6'
L.C. 43.11'

BC 408+36.72

Profile Realignment K.M.P.L.

Sta 332+135 – 339+18

(Cont. from F.B. 770 pg. 68
8-4-49 KM)

	253	73.22	70.69	
332+50			4.3	68.9
333+00			5.3	67.9
△ 333+40.65			5.7	67.5
333+50			6.1	67.1
334+00			8.7	64.5
334+50			10.6	62.6
335+00			10.0	63.2
335+50			8.5	64.7
335+83	Top Bank		5.8	67.4
336+00			8.8	64.4
336+16			4.8	68.4
336+58			3.6	69.6
337+00			4.2	69.0
337+50			5.0	68.2
338+06			6.8	66.4
338+50			12.3	60.9
T.P.	1.41	12.27	12.36	60.86

King
Shipman
West

6-27-49

(13)
57
11.

31

L.T.

74.3
+1.1
50
63.2

69.1
-4.1
35

69.9
-3.5
24'

73.4
+0.2
20'
64.7

65.2
-8.0
55'

65.3
-7.9
14'
67.4

75.8
+2.6
3

76.2
+3.0
10'

69.0
-6.2
20'

67.2
-6.0
10'
64.4

61.5
-11.7
30'

61.6
-11.6
24'

73.2
+0.1
10'
69.6

62.0
-11.2
57'

71.9
-1.3
42'
69.0

61.2
-12.0
60'

71.9
-1.3
50'
68.2

62.27

B.C 338+86.33	5.5		56.8
339+00	7.8		54.5
E.C. 339+18.29 BK	14.3		48.0
= 338+52.39 AH			
T.B. M1	7.59	54.68	54.73 Page K

(See pg. 17
8-4-49 KM)

Profile Contd From Page 27

(Cont. from page 27 8-4-49 RM)

T.B.M.	10.52	172.59		162.07	
382+50			8.4		164.2
383+00			9.0		163.6
383+50			9.9		162.7
384+00			10.0		162.6
384+50			9.7		162.9
385+00			9.0		163.6
385+50			7.1		165.5
386+00			5.0		167.6
386+50			3.3		169.3
B.C 386+95 65			0.0		172.6
T.B.M.	11.15	182.28	1.46	171.13	
387+00			8.9		173.4
387+50			6.2		176.1
388+00			9.5		172.8
388+50			10.2		172.1

King Shipman West. 6-30-49

33

Lt Rt

Set Ginney 30' Rt. 386+75 14' West of C Rd.

180.3 -2°/30 178.3 -4°/25 167.1 15.2/50

174.3 -8°/45

183.3 +10/25 184.9 +26/55 189.5 +72/23

		182.28			
388+58 40			11.0		171.3
389+00			10.5		171.8
389+30			8.8		173.5
389+50			10.1		172.2
390+00			11.1		171.2
390+50			10.4		171.9
391+00			6.4		175.9
391+23			3.2		179.1
T.B.M.	8.80	187.09	3.99	178.29	
391+50			5.5		181.6
392+00			4.1		183.0
392+50			3.3		183.8
393+00			7.8		179.3
393+50			9.2		177.9
394+00			11.6		175.5
394+12			14.2		172.9
T.B.M.	12.45	198.94	0.80	186.29	

LK

-14⁴/50'

-15⁷/40' -13³/25 -5⁸/73'

-7⁰/40' -5⁴/25'

-5⁴/40' -8⁰/25

-8⁰/40' -5⁴/25'

175.0 -11²/40'

176.8 -10³/40'

180.7 -6⁴/48'

173.1 -14⁰/45

181.5 -5⁶/40

176.9 -11¹/25'

179.0 -8'/25'

182.1 -5⁰/20'

173.9 -13²/28'

179.5 -7⁶/30'

PK

+8⁰/25'

+9¹/25'

+9³/25'

+7⁸/25'

+8¹/25'

197.9 +10⁸/25

194.7 +7.6/25

192.8 +5⁷/25

194.7 +7.6/25

193.6 +6⁵/25

Minimum Ly. 394+50 = 40'

4' West RR

		198.94			
394+50			14.3		184.6
394+75			8.1		190.8
394+83			7.1		191.8
395+00			3.7	195.2	195.2
T.P.	9.72	208.45	0.21	198.73	
395+50			6.8	201.7	201.7
396+00			4.9		203.6
396+50			7.2		201.8
BC 396+64.86			7.5		201.0
EC 396+96.48		Void	7.0		201.5
397+00			7.0		201.5
397+50			4.6		203.9
398+00			3.1		205.4
398+22.54			2.5		206.0
T.P.	1.23	207.37	2.31	206.14	

Lt.

188.9	193.9	200.9	201.2	
+10	-5	+20	+23	
80	67	40	20	
180.9	185.9	190.9	198.9	
-18	-13	-8	0.0	
84	67	50	16	
186.6	190.5	208.0	208.5	210.2	211.6
-21.9	-18	-05	00	+17	+31
45	45	9	7	10	35
169.5	186.6	208.0	209.1	214.4	217.5
-39.0	-21.9	-05	+06	+59	+90
95	52	C'L Rd >3		22	44

(See page 44 8-2-49 RM)

See Page 44 Relocation & X-Sects

Rt.

189.7	194.9	193.8
-93	-40	-52
20'	36	40
198.9	193.9	
0.0	-50	
7'	35'	

Void

		207.37			
398+27			1.2		206.2
398+50			8.2		199.2
T.P	0.88	195.54	12.71	194.66	
398+91			17.5		178.0
398+95			22.7	172.8	172.8
399+00			19.2		176.3
399+06			14.4		181.1
T.B.M.	12.90	207.68	0.75	194.79	
399+27			8.2	199.5	199.5
399+50			3.0		204.7
T.P.	13.06	220.04	0.71	206.98	
400+00			1.9		218.1
T.P.	13.00	232.30	0.74	219.30	

(cont. from page 45
8-4-49 RM)

Bottom Creek

Gilliam & Sta 399+16

		232.30 Void				
T.P.	12.07	244.18	0.19	232.11		
400+50			9.2		235.0	
T.P.	13.08	256.84	0.42	243.76		
401+00			4.9		251.9	
T.P.	12.35	268.83	0.36	256.48		Rock - 6' Rt 401+20
401+50			5.9		262.9	
401+70			0.4		268.4	
T.P.	12.63	281.14	0.32	268.51		Rock 401+70 Lt
402+00			0.5		280.6	
T.P.	12.09	292.64	0.59	280.55		Rock 2' Lt 401+98

		292.64			
BC 402+11.4			8.6		284.0
402+50			4.5		288.1
402+58.8			3.8		288.8
T.P.	12.87	304.53	0.98	291.66	
403+00			11.3		293.2
403+50			6.7		297.8
404+00			2.2		302.3
T.P.	12.80	316.81	0.52	304.01	
404+50			9.4		307.4
405+00			6.4		310.4
405+50			3.3		313.5
T.P.	12.95	329.22	0.54	316.27	
406+00			11.2		318.0

Rock 404+10 - 10' Rt.

		329.22				
406+50			4.0		325.2	
407+00			1.5		327.7	
T.P	12.96	341.78	0.40	328.82		Rock - 10' Rt Sta 406+90
407+50			12.7		329.1	
408+00			7.8		334.0	
B.C 408+36.72			1.7		340.1	
408+50			0.2		341.6	
T.B.M.	12.20	353.15	0.83	340.95		Ginney 30' Lt P.I
E.C. 408+79.83			8.8		344.4	
409+00			7.1		346.1	
409+50			2.6		350.6	
T.P.	12.24	365.09	0.30	352.85		
410+00			10.6		354.5	

43055

		365.09			
410+50			4.2		360.9
T.P.	12.86	377.73	0.22	364.87	
411+00			11.0		366.7
411+50			6.7		371.0
412+00			1.8		375.9
B.C. 412+09.50			0.8		376.9
T.P.	13.00	390.47	0.26	377.47	
E.C. 412+37.56			10.7		379.8
412+50			9.6		380.9
413			4.7		385.8
T.P.	12.80	402.72	0.55	389.92	
413+50			10.8		391.9
414+00			6.6		396.1
414+50			3.3		399.4

Rock E 410+77

		402.72				
T.P	12.36	414.90	0.18	402.54		
415+00			9.7		405.2	
415+50			3.1		411.8	
T.P.	12.75	427.33 ~~427.33~~	0.32	414 58		
416+00			11.7		415.6	
416+50			11.3		416.0	
417+00			10.4		416.9	
417+50			9.0		418.3	
418+00			2.9		424.4	
T.P.	9.03	435.66	0.70	426.63		
418+50			6.9		428.8	
419+00			4.1		431.6	
419+50			0.8		434.9	
B.M.			12.45	423.21	423.65	Nail in F. Post 200' So. on City Prop. Line

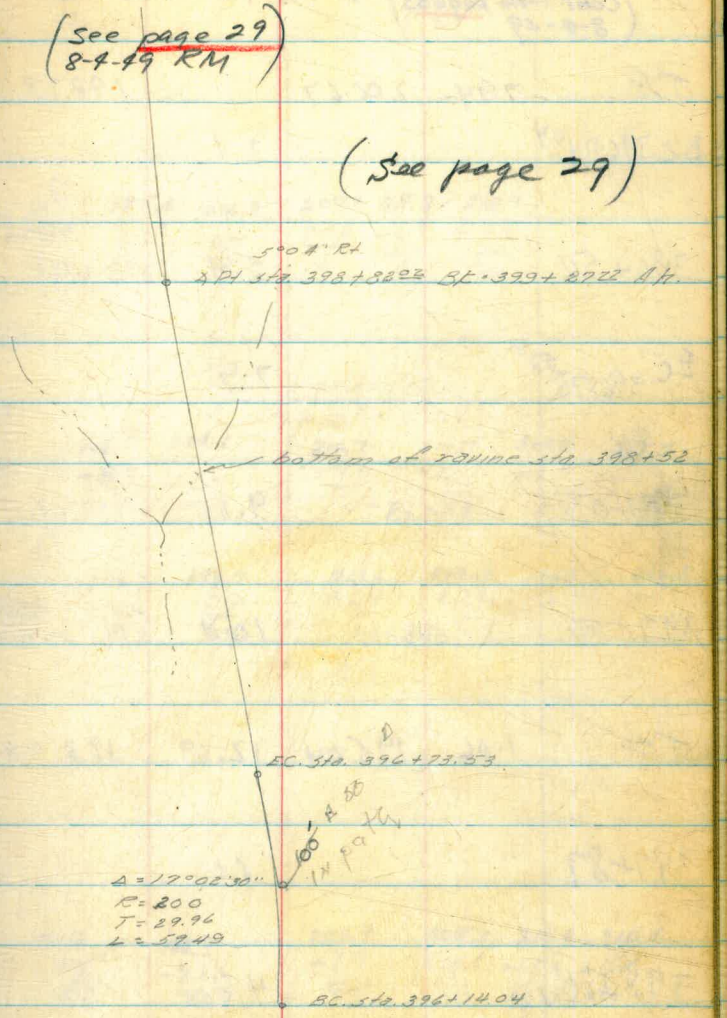
		435.66			
T.P.	12.35	447.59	0.42	435.24	
420+00			9.5		438.1
420+50			4.9		442.7
T.P.	9.22	454.55	2.26	445.33	
421+00			7.1		447.5
421+50			4.4		450.2
422+00			5.1		449.5
422+50			8.3		446.3
423+00			9.1		445.5
423+50			9.4		445.2
T.P.	1.19	442.76	12.98	441.57	
T.P	0.12	435.33	7.55	435.21	
B.M.			12.12	423.21	423.65

End

Realignment - K.M. P.L.
Sta. 396+00 to 399+27.72

(See page 29
8-4-99 RM)

(See page 29)



(Cont. from page 29
8-4-99 RM)

Profile Realignment

(cont. from page 35 8-4-49)

396+14.04 - 398+80.02 = 399+22.27 Ahd.

T.P.	7.94	20467		198.73	
B.C. 396+14.04			3.1		203.6
396+50			5.4	201.3	201.3
EC 396+73.55			7.9		198.8
397+00			9.1	197.6	197.6
397+50			10.9	195.8	195.8
T.P.	1.06	19504	12.69	193.98	
397+87			1.0		194.0
398+00			4.8		190.2
398+48			19.5		175.5
398+52	Bottom Creek		25.5	169.6	169.5

7-5-49

Shipman

IN			R+		
	185.4	206.3	207.1	211.8	213.7
-36.0 (16.5)	-20.3	-0.4	+0.4	+4.9	+7.0
90	55	5	4	6	20
	196.7	204.1	210.7	210.7	213.0	213.7
-31.5 (16.1)	-8.0	-2.6	+4.0	+4.0	+6.3	+7.0
76	29	20	16 - Rd - 23		30	35
	196.1	198.7	213.6	213.9	215.5	216.3
-30.5 (16.3)	-10.6	8.0	+6.9	+7.2	+8.8	+9.6
62	37	29	40 - Rd - 47		50	60
	171.0	186.9	202.9	205.1	210.1	210.4
	-24'	-8.1	+7.9	+10.1	+15	+15+1=81
	52'	23'	35'	50	72+9=81	
198.9	200.7	194.5	199.0	208.3		
+3.9	+5.7	-0.5	+4.0	+13.3		
44'	18	16	8'	26		

195.04

398+58			18.1		177.9
T.P.	8 24/7	201.96	1.74	193.70	
BK 398+82 92			2.35	199.61	199.6
399+27 77					

Profile Cont. Page 36

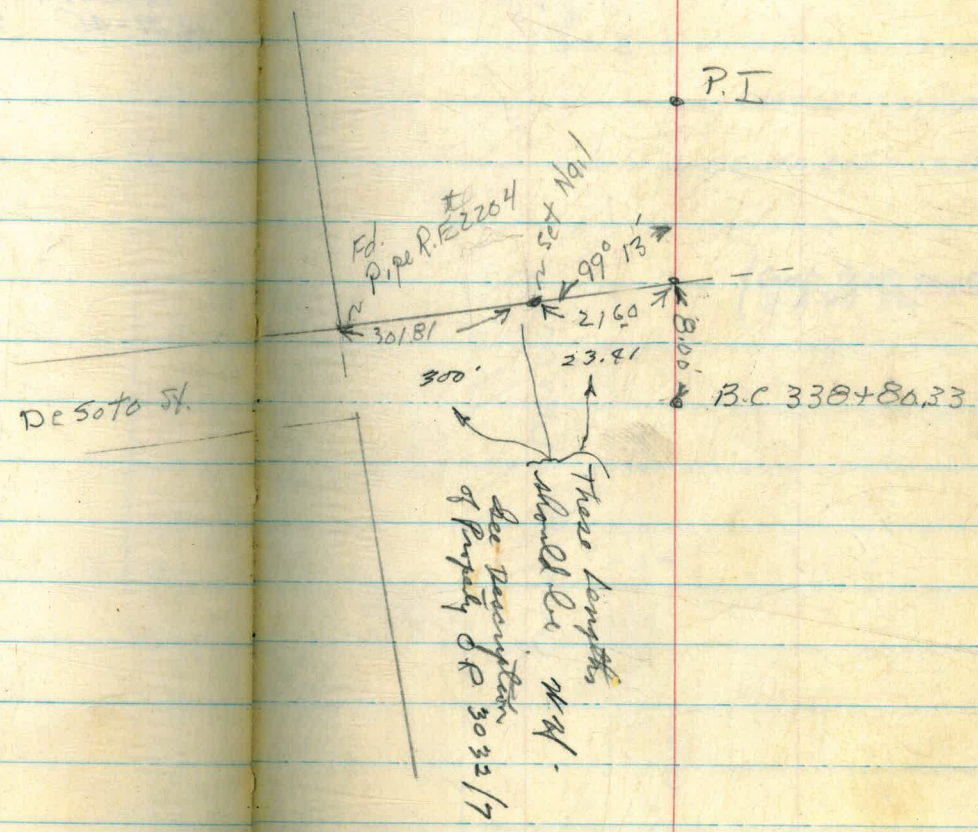
(See page 36 8-2-49 RM)

Lt		Rt		
199.0	195.8	189.5	190.0	195.0
+4.0	+0.8	-5.5	-5.0	0.0
30	8	10	16	19'
201.8	198.5	193.0		
-0.2	-3.5	-9.0		
25'	15'	20'		

Checked & Reduced
pg 31-45 7-15-49 RAM

King Shipman 7-20-49

Ties to Allied Synthetics Co. (Archibauld)
Pueblo Lot 1788 & Homelands Villa

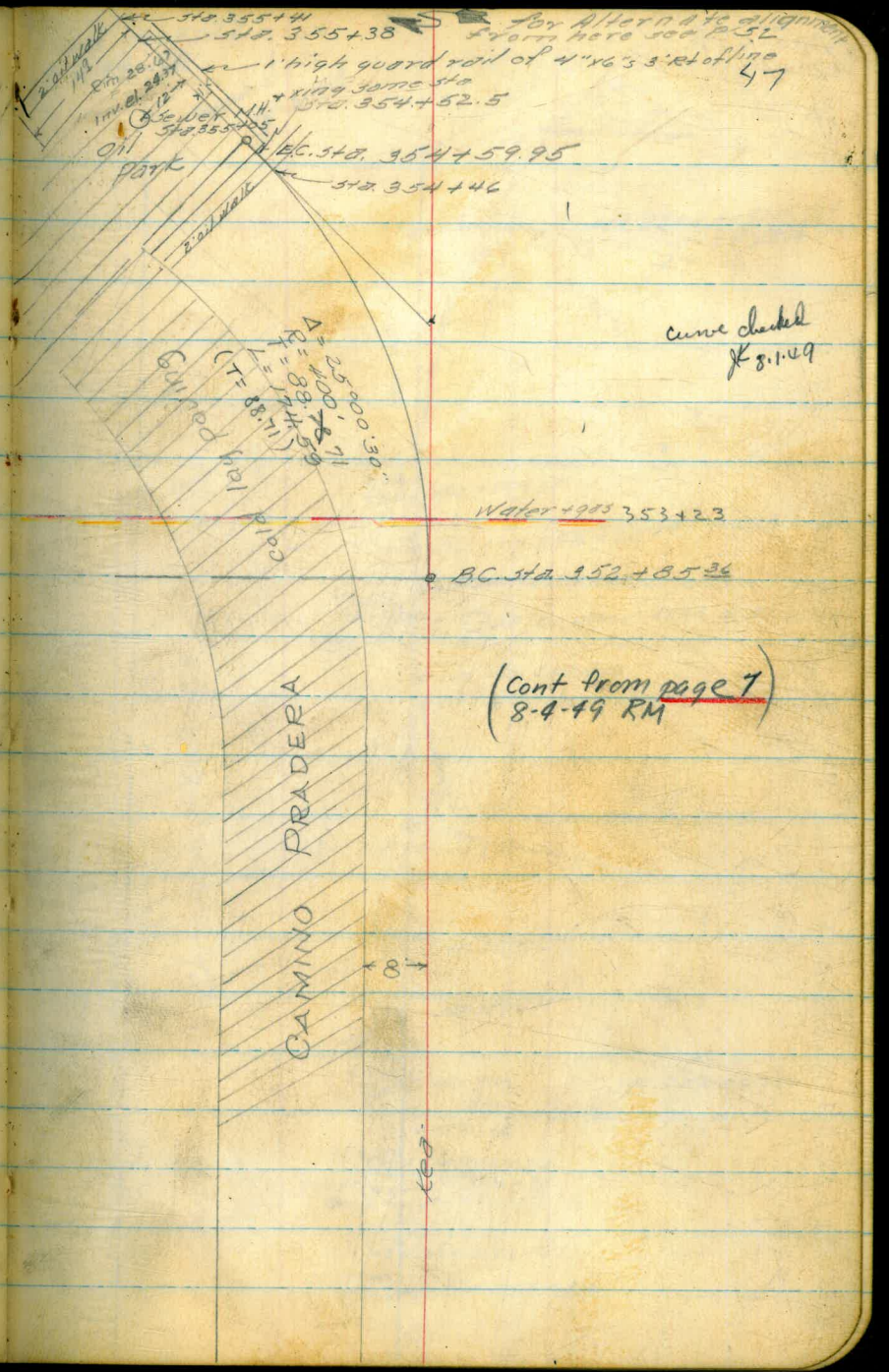


K.M.P.L. Realignment & Profile

From 352+85.36 To 360+10.37 BK = 360+16.77 Ah.

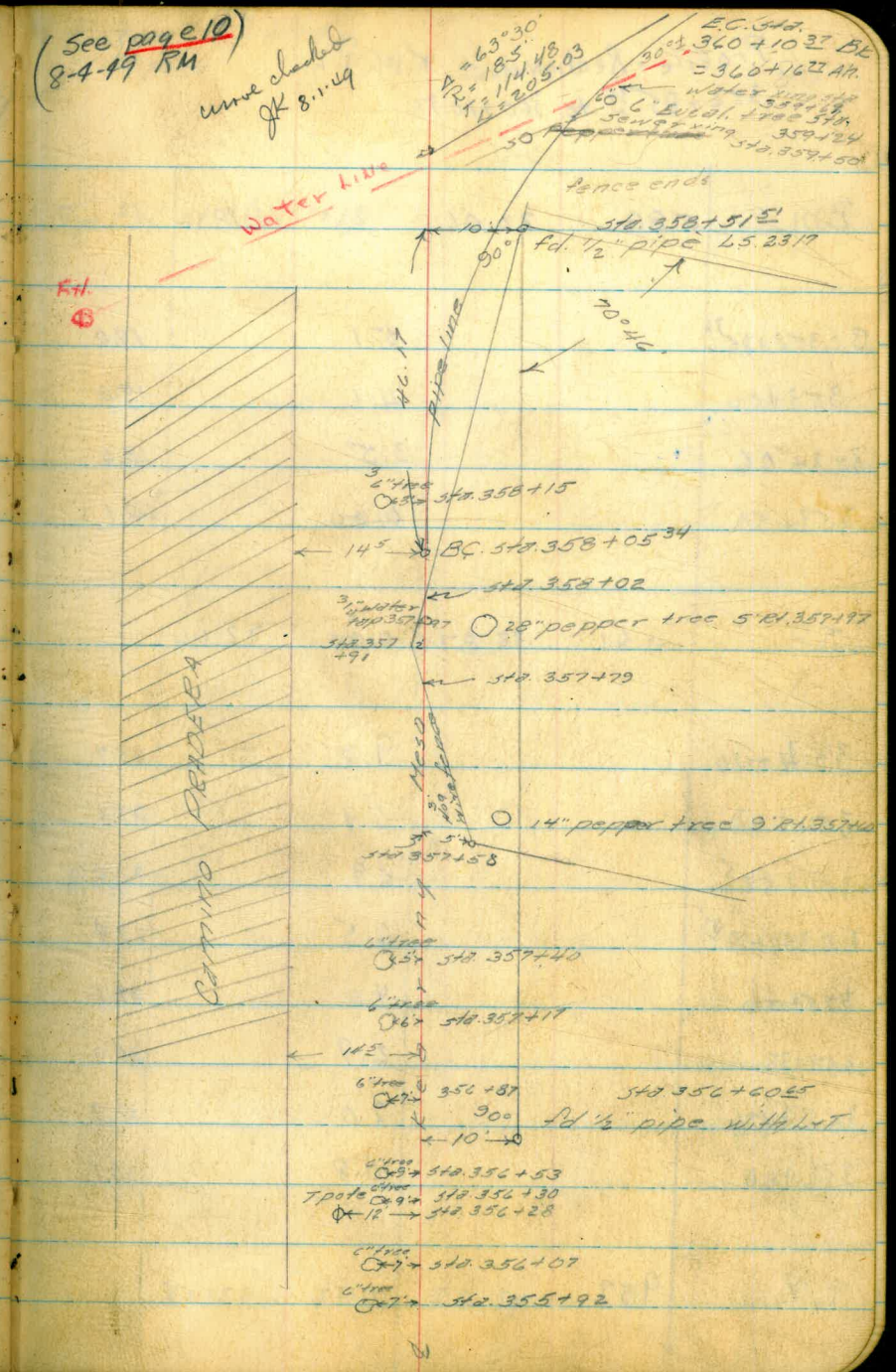
7-28-49

King Stylman Rainey



(See page 10)
8-4-49 RM

curve checked
JK 8.1.49



Profile - Realignment K.M. P.h.
352+85.36 to 360+10.37

B.M.	5.88	22.06		16.18	
B.C. 352+85.36			5.1		17.0
353+00			4.1		18.0
353+06			3.5		18.6
353+50			0.00		22.1
T.P.	11.81	33.87	0.00	22.06	
354+00			9.2		24.7
354+50			6.9		27.0
354+52.5			6.9		27.0
E.C. 354+59.95			6.5		27.4
355+00			4.8		29.1
355+38			2.9		31.0
355+56			2.0		31.9
357+00			0.8		33.1
T.P.	9.57	42.72	0.72	33.15	

King 7-29-49
Shipman

49

Top F.H. 24. Sta. 351+13

Edge of

ON. Rock 356+01

		42.72			
356+50			7.3		35.4
357+00			5.9		36.8
357+50			4.9		37.8
358+00			4.3		38.4
BC 358+05[34]			4.5		38.2
358+50			4.5		38.2
359+00			4.5		38.2
T.P.	5.23	43.26	4.69	38.03	
359+50			3.9		39.4
360+00			2.5		40.8
EC. 360+10[37] BK.			2.3		41.0
= 360+16[77] Ah.					
T.B.M.			4.98	38.28	38.28

Five. Hyd 41.357

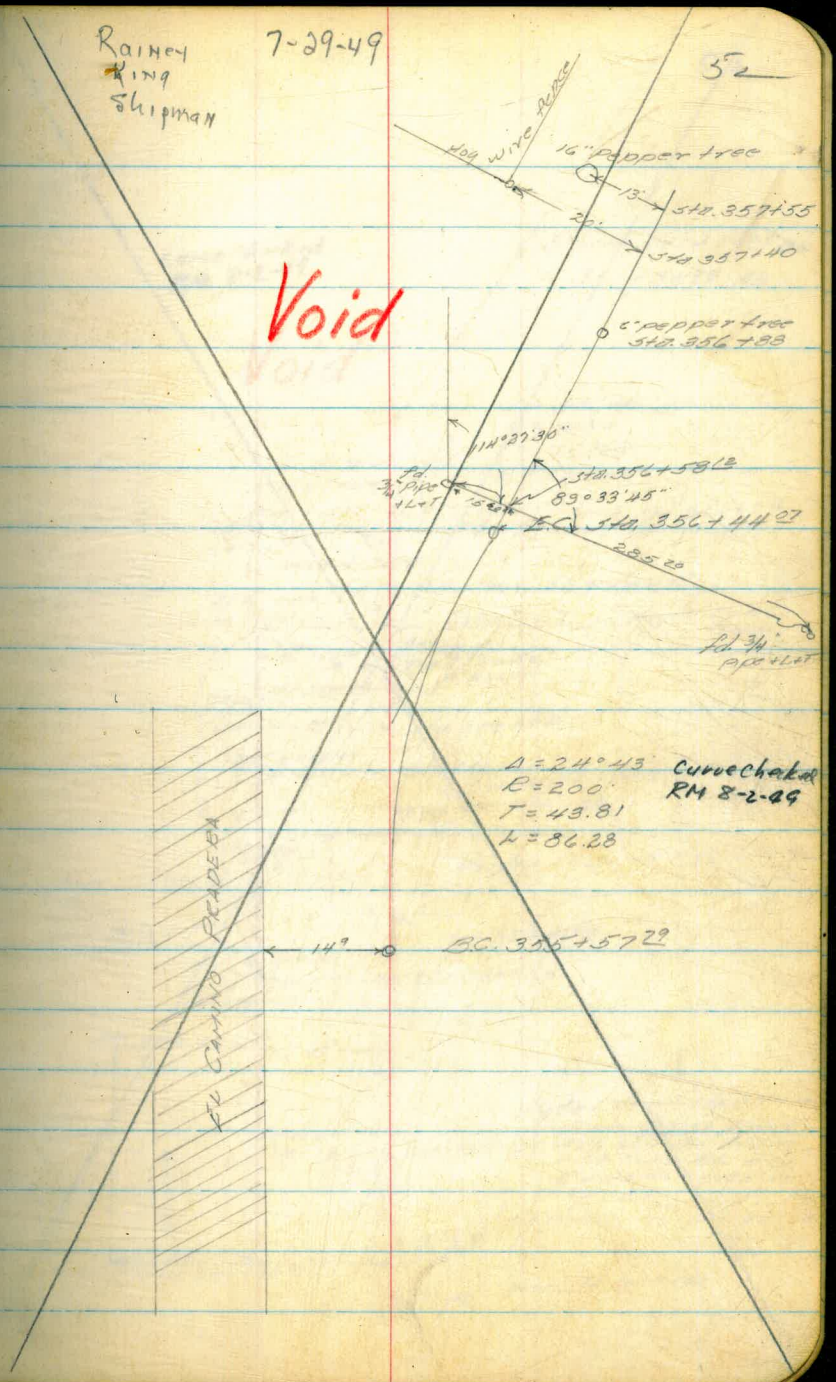
(See page 23
8-4-49 RM)

Alternate
Realignment Kearny Mesa
Pipeline from Sta 355+57.29
361+19.75

Rainey
King
Shipman

7-29-49

52



Curve Checked
R.M. 8-2-99

Void

EC. Sta. 361+19.75 BK
= 361+84.85 Ah.

Δ = 39°46'30"
R = 200'
T = 70.38
L = 138.35

Inv. el. 39.85
Rim el 45.45
Sewer MH.
Sta. 360+02
21' Lt.
Sta. 359+72.40

Water xing sta 360+25
Sewer xing sta 360+33

P.C. Sta. 359+84.75

fd. 3/4" pipe
45.24
21'
(350° rec)
fd. conc. mon.
89°44'30"
Sta. 359+36
4" Eucal
8" Eucal
14'
Sta. 359+50
#500,289
T pole
28'
Sta. 359+04
24" pepper
30'
Sta. 358+80
24" pepper tree
+6'
Sta. 358+63
6" pine
12'
6'
10'
Sta. 359+12
Wooden coop of 1"x6" Vertical
6'
10'
Sta. 358+53
fd. 3/4" pipe
45.23.17
8" pine
19'
Sta. 359+50
end fence
Sta. 358+53
Sta. 358+26.48
20'
Note: from sta. 357+76 to sta. 358+23 there are shrubs from line to 10' Rt. Also 6' from house to house
6" tree
19'
Sta. 358+06
House
24" pepper tree Sta. 357+91
9'
24'
Sta. 357+84.49
20'
9'
6" tree Sta. 357+81

Realignment detailed on pages 52-53

	9.72	42.87	33.15
355+57.29		10.9	
		Void	
356+00		9.7	
356+44.97		6.9	
357+00		4.1	
357+50		1.7	
T.P.		1.12	41.75
	7.20	48.95	
358+00		6.4	
358+50		5.5	
358+92		3.9	

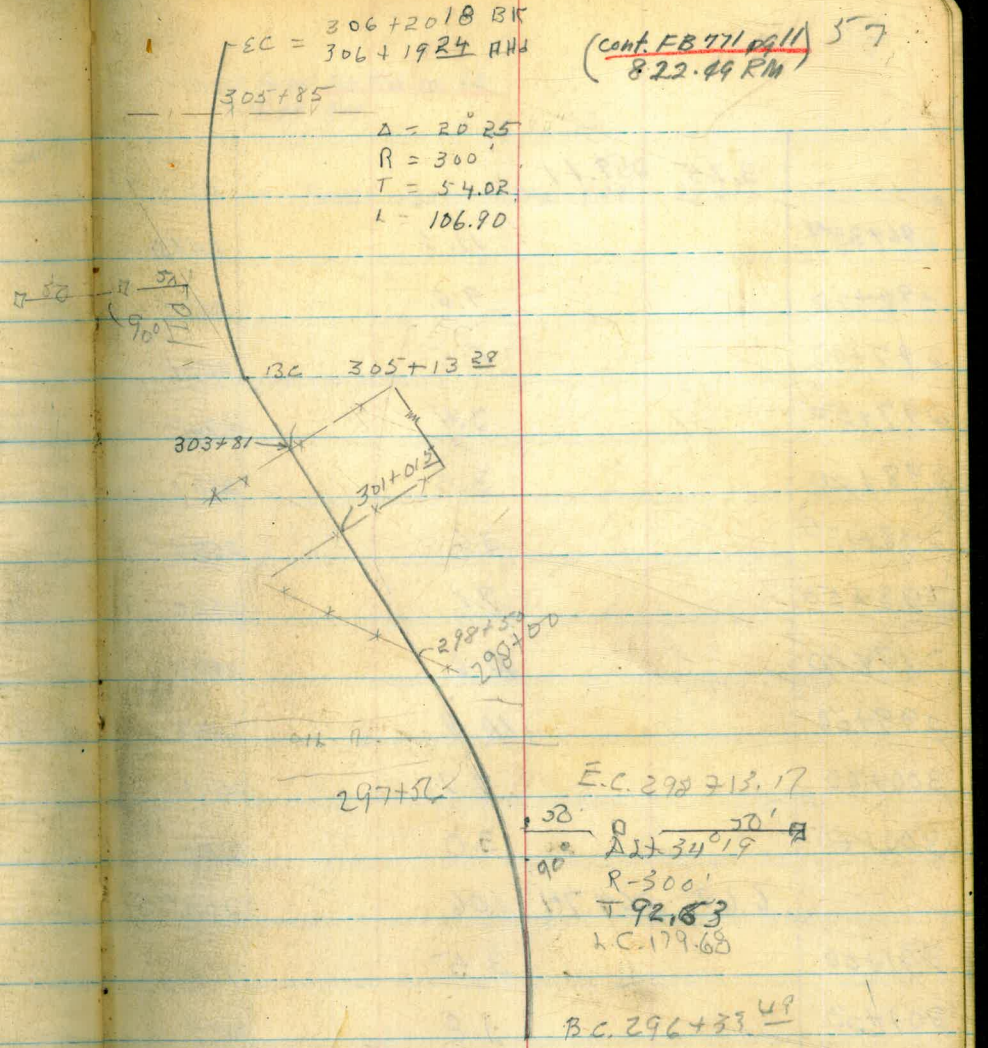
		46.95		Lt.	Rt.
359+99.5			5.5		
	Void				
359+04			5.2		
359+12			3.5		
359+50			2.3	3.7 / 15	0.8 / 15
T.P.			2.74		
	11.89	58.10	46.21		
359+84.82	B.C.		9.8	12.5 / 15	5.3 / 15
360+00			8.6	12.1 / 15	3.7 / 15
360+50			7.0	10.8 / 15	2.6 / 15
361+00			6.8	10.1 / 15	1.9 / 15

		358.10			
= 361+84.85 AH 361+19.25 BC		EC.	5.9		
			Void		
T.P.			12.63	45.47	
	1.17	46.64			
CL 10 EH	P.23		8.35	38.29	Corr 38.28

Lt	Rt
10.1 15	1.1 15

KING
Shipman
West - 8-15-49

Relocation K.M.P.L.



(cont. FB 771 pg 11)
8-22-49 RM

57

305+13 28
54 02
305 67.30
301 70 90
3 96 40

296+33 49
92 63
293 26 13

B.C 296+33 49

(cont From FB 771 pg. 9)
8-22-49 RM

Cont. from EB 770 pg. 60
9-16-49 RM

	3.75	259.11		255.36
BC 296+33.29			11.1	248.0
296+50			9.6	249.5
297+00			5.5	253.6
297+50			2.4	256.7
298+00			3.0	256.1
EC 298+13.47			3.6	255.5
298+50			7.1	252.0
299+00			10.6	248.5
299+50			10.4	248.7
300+00			7.7	251.4
300+50			3.0	256.1
	6.69	264.74	1.06	258.05
301+00			3.5	261.2
301+50			1.8	262.9
302+00			3.5	261.2
302+50			12.0	252.7
	7.36	259.05	13.05	251.69
303+00			11.9	247.2

Spike in Fence Post Sta 299 25' LT

	+	⊼	−		
		259.05			
303+50			14.0		245.1
304+00			11.5		247.6
304+50			8.0		251.1
305+00			5.1		254.0
BC 305+13.28			5.0		254.1
305+50			4.6		254.5
306+00			6.3		252.8
EC 306+20 HP BK / 306+18 93 AH			6.7		252.4
	See Alignment pg. 57		6.30	252.75	252.80

Sta 306+00 ON old alignment

See FB 770 pg 62

9.16.49 RM

				255.36	T.B.M. Page 58
	6.15	266.51			
296+29.23			12.60	248.91	242.4 6.5
	1.42	250.33			
296+00.00			4.4	245.9	239.7 6.2
295+80.52			6.7	243.6	236.6 7.0
295+51.44			11.4	238.9	232.0 6.9
T.P.			11.41	238.92	
	1.39	240.31			
295+22.			8.7	231.6	225.7 5.9
T.P.			12.27	228.04	on steel stake Sta 295+02.00
295+02.00			14.4	225.9	220.4 5.5

P.M.P.L. #2
5' OFFSETS

King
West
Shipman

4-17-50

Clear-Hot

67

	7.40	119.59			112.19	
~~220+13~~			~~4.6~~	~~115.0~~		
221+05	15		4.6 ~~4.4~~	115.0	109.4	5.6
220+86	61		~~4.4~~ 4.4	115.2	109.4	5.8
220+58	29		4.1	115.5	109.5	6.0
220+23	29		4.1 ~~3.8~~	115.5	109.5	6.0
219+93	35		3.8	115.8	110.0	5.8
+63	43		3.9	115.7	110.4	5.3
+33	51		3.9	115.7	110.3	5.4
219+03	59		3.9	115.7	110.1	5.6
218+78	3		4.1	115.5	110.0	5.5

K. M. P. L. #2
5' offsets

119.59

2.8+43.75			4.1	115.5	109.7	5.8
218+13.83			4.5	115.1	109.4	5.7
			5.40	112.19		

King
West
Shipmon

4-17-52

6 2

AUG 30 1950
BEATTY
KING
LEONARD
WEST

KEARNY MESA #2 PIPELINE

FINAL X-SECTIONS OF FILLED AREAS

BM	1.13	256.49 ✓	255.36
298+50	0.0	Area	
298+75			
299+00			
299+50 (CL 11)	1.13		255.36 ✓
300+00	0.0	Area	
BM	0.38	263.94 ✓	263.56
302+50	0.0	Area	
303+00			
303+50			
+75	0.0	Area	

Spike in FEN. POST 25' LT Sta 299

51.9	51.9	50.9	45.5
4.6	4.6	5.6	11.0
13	12	C	23
(NATURAL GROUND) N G			N G

51.7	50.4	44.6
4.8	6.1	11.9
18	C	16
NG		NG

52.3	50.9	50.8	45.6
4.2	5.6	5.7	10.9
20	11	C	20
NG			NG

Cor of Val. Chamber

54.4
9.5
C

52.6	48.9	40.9
11.3	15.0	23.0
15	C	30
NG		NG

51.3	47.9	41.0
12.6	16.0	22.9
15	C	19
NG		NG

48.5
15.4
C

Kearny Mesa #2 — Jan 23, 51 — West Williams

64

Profile on Box's

	+	Hi		
BM on Pipe (50') SW. Cor. Box	1.59	451.76		450.17
			2.80	448.96
			12.31	439.45
			1.60	450.16 BM on Pipe
	1.52	68.69		67.17
			4.02	64.67
			1.08	67.61
			6.49	62.20

NW Cor B.V. Box — Sta 422+39 ±

NW Cor A.V.A — Sta 419+90 ±

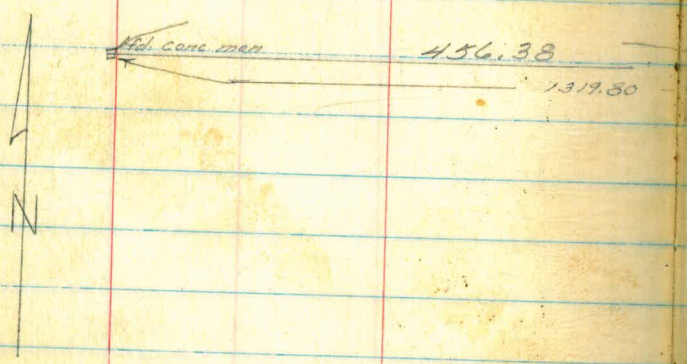
329+05 ±0 Top RR rail

Sta 327+80 ± B.V. Chamber

Sta 324+95 ± 2" A.V.A

Sta 321+85 ± 4" B.O.

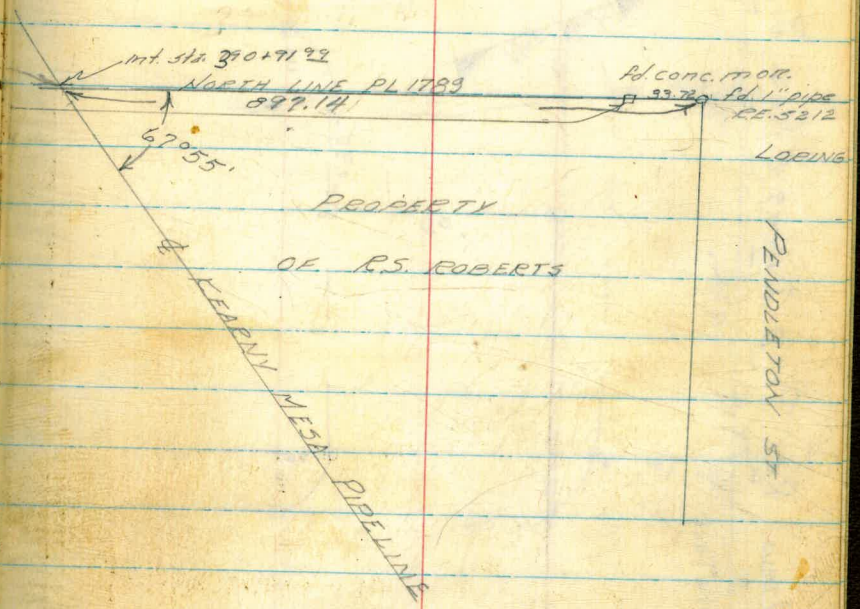
Ties To P.L. 1789
1787



456.38
897.14
37
1353.52
33.72
1319.80

868.45 to nail

July 14, 1949 Reiney
King
Shipman

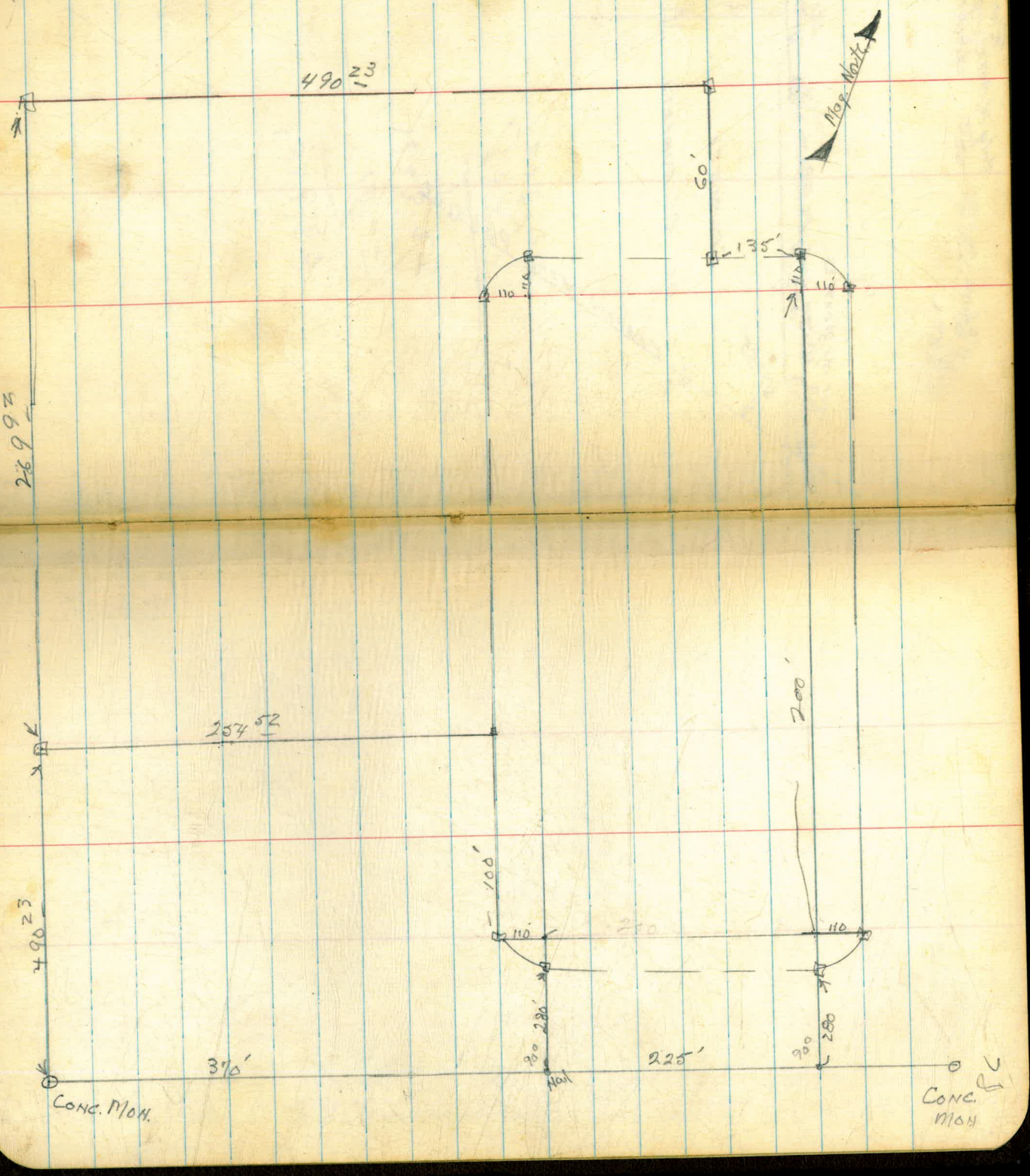


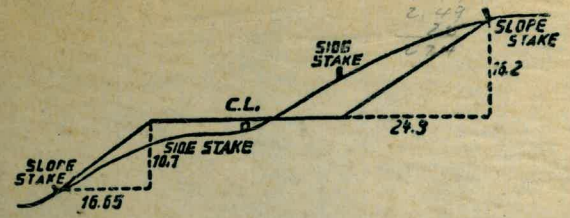
King
West
Shipman

4-12-49

Bay View Res. Prop Lines & Res. Site

⊡ = Hub & Tack





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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