

#777



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	0
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

792-795

17094

Please Return to  
City of San Diego Water Dept.  
Room 208 Civic Center  
Telephone Main 5161

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.39	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.891	.981	1.11	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.78	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

ChesterTan Pipeline

Page

1-12

ChesterTan P.h. Profile

15-21

Kearney mesa P.h. Realignment + Profile 23-29

STA 30+00 - 46+92.44

ChesterTan realignment.

29

" "

30-49

X-sections ChesterTan WaterTank 1 d.d. 50

Realignment - Proposed X-sects - ChesterTan P.h. 51-52

Diameter & Measurements - ChesterTan Tank 1 d.d. 52

Const. Notes - ChesterTan P.h. also 54-70

Misc. Elev's ChesterTan Tank also 72-73

Misc. Details " " 74

& Profile & Aligment Prelim Line From Alice 75-77

CHESTERSON TANK Northernly to City Bay

ChesterTan Tank Survey

Alice 78

ChesterTan Pump Plant Site Survey & X-sects.

Alice 79-81

PROPOSED 24" MAIN IN PL 1202 - CHESTERSON 82

PROPOSED 16" MAIN IN PL 1202

CHESTERSON TANK CROSS-SECTION OF PROPOSED NEW TANK SITE 83 COM

CHESTERSON - Proposed Tank Location SHOWING EXISTING 10" C.I. PIPELINES 86

(SHOTS ALL)

Alice

GRADE FOR 21" C.I. 90° BEND ALSO REVISED X-SECTIONS OF PROPOSED TANK SITE 21

PROPERTY CORNERS & 2' OFFSET FOR FENCE - CHESTERSON STAND PIPE 78

June 3, 1949 Shipman  
Rayney West  
Payne



7°01'30" LT.  
12+31.19 BK  
12+30.86 F hd.  
10+96

Gladiolas

8+67

7+65 BOTTOM

7+00 S EDGE DRAW

20+32.6+412'

34.6+12

35'

Gladiolas

Gladiolas

P.L.  
1199

WESTINGTON PIPELINE

Sta. 1450

38°30'

8'

90°00'

Sta. 1471

Pueblo w

Lot Line

3' water ring Sta. 1463

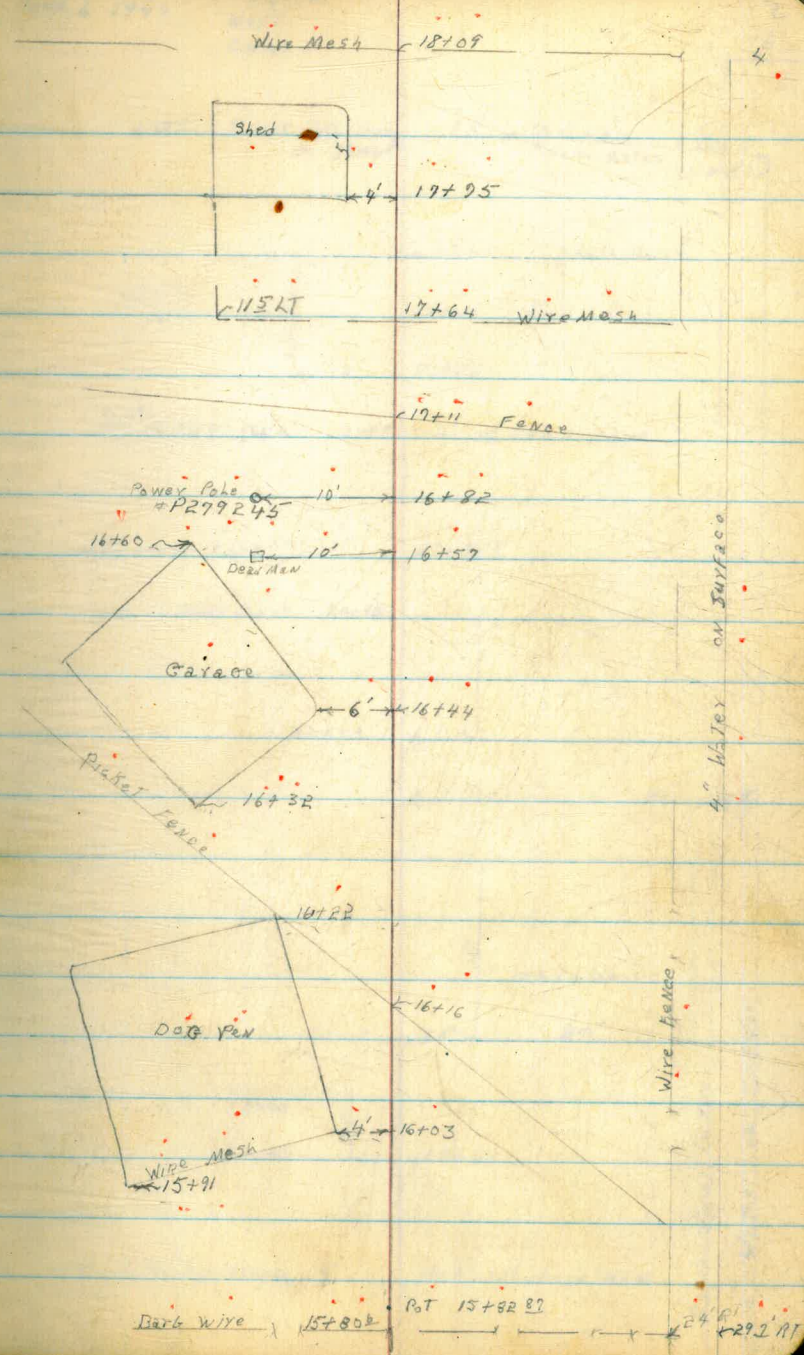
on ground

8°03'

90°00'

Kearny Mesa P.L.

Kearny Mesa Sta. 110+70 = 0+00



5  
June 6 1949

SHIPMAN  
WEST  
CAYVEY

6

← 39.2 4' 1/2" P.P. Fence  
Sta 22+54

7.5' → 2" Water  
Water Meter 33' → 8.5'

← 22+11 10' Bath House

22+02 15.5' → 10'

← 12' 21+88

P.P. # 2722+3 0.14' 21+58 11' → Dead Man

ENG Tree 1' DIA → 19' 20+96.5

Back Fence 20+92

20+79 4.5' →

← 32' → 8.5'

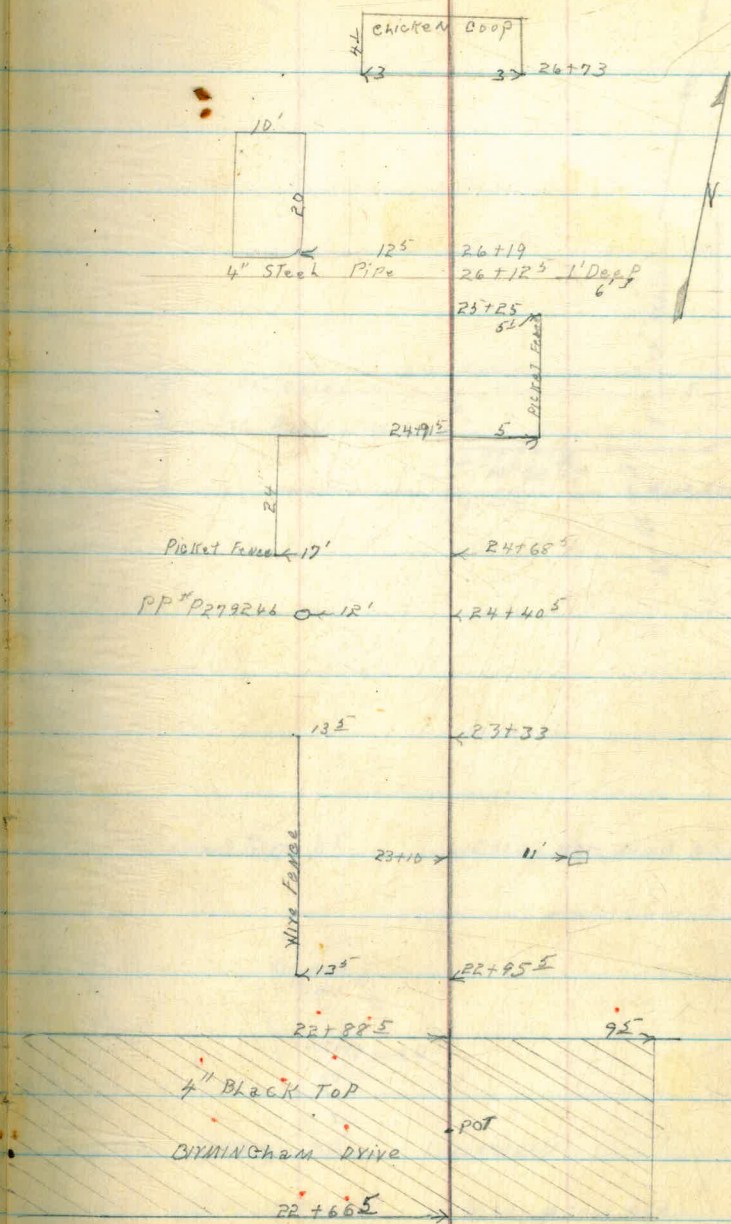
Garage

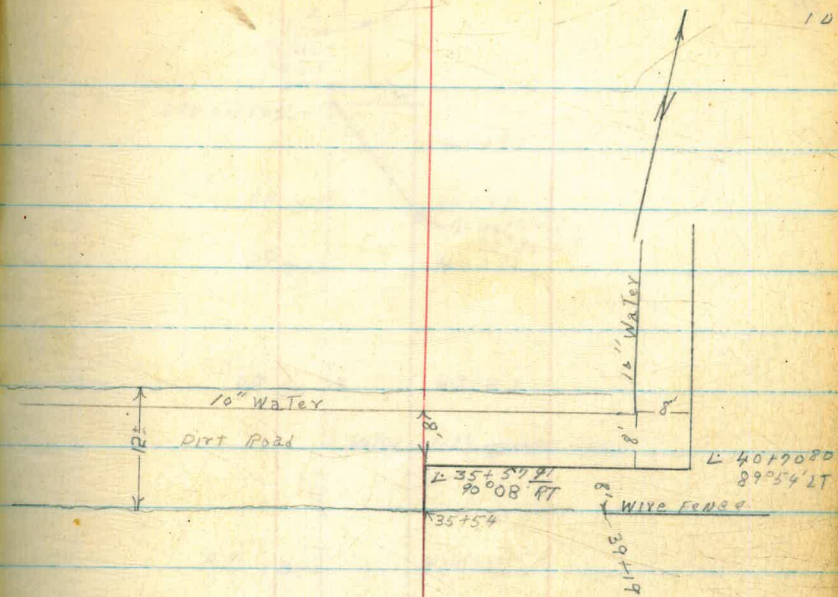
20+18 ← 3.5' → 20'

Shed  
6.4' → 1' → 19+33

P.P. # 2792+40 7' → 1819' 12' → Dead Man

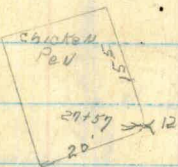
Back Wire Fence  
4" Water on Surface





Telephone Pole 118

← 29101 950 Dead Man



EUC Tree 8" DITCO ← 225

← 291225

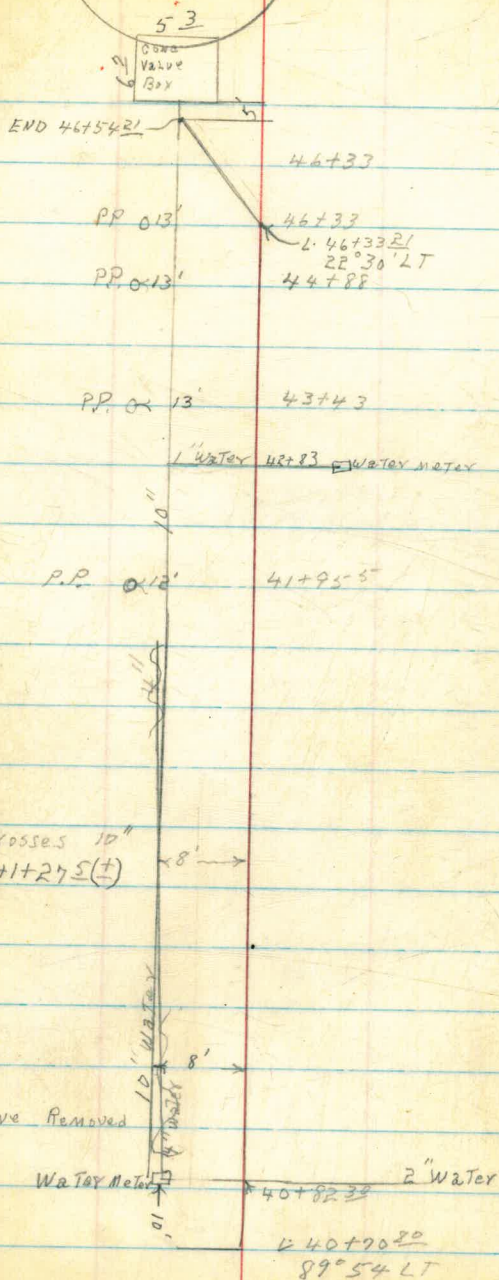
PP# P279247 ← 113

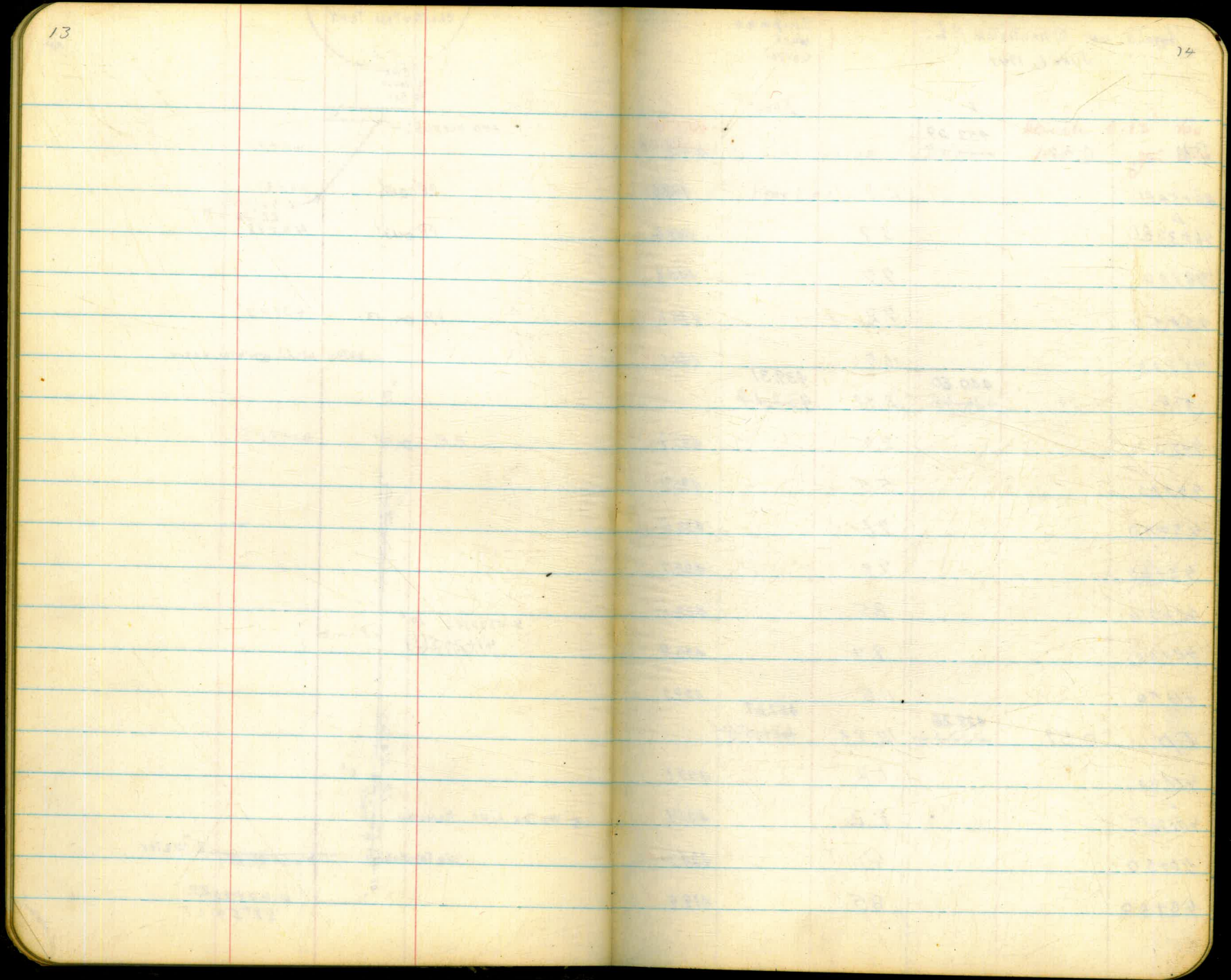
← 29101, B Dead Man  
814



Chasterton Tank

12





Levels on Chesterton P.L.  
June 6, 1949

Shipman  
West  
Carver

15

	I	Σ	-	Height	
BM	0.49	452.29 <del>446.17</del>		<del>451.82</del> <del>445.70</del>	ON Base of Chesterton Tank
4675421			2.7	449.6	END OF Pipeline
↳ 4673321			3.9	448.4	
46700			7.9	444.6	
45750			7.2	445.1	
45700			10.7	441.6	
T.P.	1.29	440.60 <del>434.48</del>	12.98	439.31 <del>433.19</del>	
44750			2.7	437.9	
44700			5.5	435.1	
43750			7.1	433.5	
43700			7.9	432.7	
42750			8.5	432.1	
42700			9.7	430.9	
41750			11.5	429.1	
T.P.	0.59	428.26 <del>422.14</del>	12.93	427.67 <del>421.55</del>	
41700			1.2	427.1	
↳ 4070880			2.2	426.1	
40750			4.1	424.2	
40700			8.5	419.8	

Bench 6.12' too low.  
JK 6.20

		$\bar{A}$		Elev
39+50		<del>422.14</del> 428.26		
T.P.	0.01	417.32 <del>411.20</del>	12.0 -10.95	416.3 417.31 <del>411.19</del>
39+00			5.2	412.1
38+50			9.5	407.8
38+00			13.2	404.1
T.P.	0.92	406.55 <del>400.43</del>	11.69	405.63 <del>399.51</del>
37+50			4.0	402.6
37+00			4.5	402.1
36+50			5.8	400.8
36+00			7.8	398.8
35+57.91			9.9	396.7
35+00			11.0	395.6
34+50			12.3	394.3
T.P.	2.23	395.77 <del>389.65</del>	13.01	393.54 <del>389.42</del>
34+00			2.6	393.2
33+50			5.1	390.7
33+00			5.8	390.0
32+50			7.4	388.4
32+00			7.8	388.0

Gunny at 34+25

	+	+	-	Elev
3 31+50		395.77 <del>389.65</del>	7.4	388.4
7 31+00			9.0	386.8
3 30+50			10.5	385.3
3 T.P.	0.90	387.21 <del>381.09</del>	9.26	386.51 <del>380.39</del>
3 30+00			2.8	384.4
7 29+50			4.4	382.8
29+00			4.5	382.7
T.P.			2.52	378.57
28+50			5.0	382.2
3 28+00			5.5	381.7
3 27+50			6.3	380.9
3 27+00			7.0	380.2
3 26+50			7.7	379.5
26+00			8.0	379.2
25+50			9.7	379.5
25+00			8.6	378.6
T.P.	R.21	381.32 <del>375.20</del>	8.10	379.11 <del>372.99</del>
24+50			R.8	378.5
24+00			3.5	377.8

T.B.M. on SPIKE on P.P. # 448249H Sta 29+00

	T		ELEV
3 23+50			377.1
23+00			376.6
N. Edge Black Top			376.57
S. Edge " "			376.24
22+50			375.8
22+00			374.8
21+50			373.6
21+00			371.3
20+50			368.4
T.P.	1.44	369.80 363.68	368.36 362.24
20+00			365.8
19+50			364.1
19+00			361.5
18+50			359.4
T.P.	3.17	360.98 354.86	357.81 351.69
18+00			357.1
17+50			356.9
17+15			
T.P.	3.52	359.65 353.53	356.13 350.01
17+00			355.9

G.W.V. 20+49

	$\pi$	-	Elev
	<del>353.53</del>		
	359.65		
3 16+50		4.1	355.6
16+00		4.7	355.0
15+50		5.3	354.4
15+00		6.5	353.2
14+80		7.4	352.3
14+60		8.5	351.2
14+37		7.4	352.3
14+00		5.8	353.9
13+50		7.2	352.5
13+00		7.1	352.6
12+50		6.8	352.9
12+00		7.3	352.4
TP	0.93	6.12	353.53
	<del>348.34</del>		<del>347.41</del>
11+50		2.7	351.8
11+00		3.4	351.1
10+50		3.1	351.4
10+00		2.8	351.7
9+50		3.5	351.0
9+00		3.7	350.8

354.46

353.53

GHESTERTON PIPE LINE

6-6-49

20

	+	$\pi$		Elev
		<del>348.34</del> 354.46		
8+50			6.9	347.6
8+00			11.8	342.7
7+65			17.3	337.2
7+00			7.6	346.9
6+41 <sup>2</sup>			5.7	348.8
6+00			5.8	348.7
TP	8.61	357.76 <del>351.64</del>	5.31	349.15 <del>343.03</del>
5+50			9.6	348.2
5+00			9.4	348.4
4+50			8.6	349.2
4+00			7.1	350.7
3+50			6.7	351.1
3+00			5.5	352.3
2+50			5.4	352.4
2+00			4.6	353.2
1+50			4.4	353.4
1+00			4.1	353.7
0+50			5.0	352.8
0+00			6.19	351.57
TP	4.82	356.59 <del>350.47</del>	5.99	345.45 351.77
			3.92	352.65 <del>346.55</del>

Reduced & checked  
8.16.49 RM

352.46 - 6.12 = 346.34

BM on Hy  
395



CHESTERTON  
TANK  
GRADE FOR 24" C.I. 90° BEND  
ALSO REVISED X-SECTIONS  
OF PROPOSED TANK SITE

JUNE 26, 1952 21

BEATTY  
POWELL  
FISH

BM 0.01 451.83 451.82

on Ftg of Existing Tank

2.79 449.04 GRADE  
E PIPE

Spike on pole Mkd C4 = (TO GRADE FOR TANK)

12.81 439.02 - 442.23  
F321

(E of pipe for 90° BEND)

8.01 443.82 C159

⑦ East E pipe

10.03 441.80 F043

⑦ South E pipe

Ceiling  
covered up  
or destroyed

440.23	440.43	442.03	442.33	443.4	446.0	447.0
11.6	11.6	9.8	9.5	8.4	5.7	4.8
100	97	92	79	73	55	40
Loose	Loose	Loose				

438.3	440.43	440.8	441.5	444.7	446.1
13.5	10.9	11.0	10.3	5.1	5.7
100	93	78	70	46	40
Loose	Loose	Loose	Loose		

440.5	440.5	441.9	440.6	445.3	445.7	448.1
11.3	11.0	12.0	11.2	6.5	6.1	6.7
100	97	90	74	54	29	40
Loose	Loose	Loose	Loose			

440.1	440.3	441.4	443.6	445.4	446.1
11.7	11.5	10.4	8.2	6.4	7.7
100	92	77	69	59	40
Loose	Loose	Loose			

0+00 = SW Cor Existing Tank Site

0+20

0+40

0+60

0+80

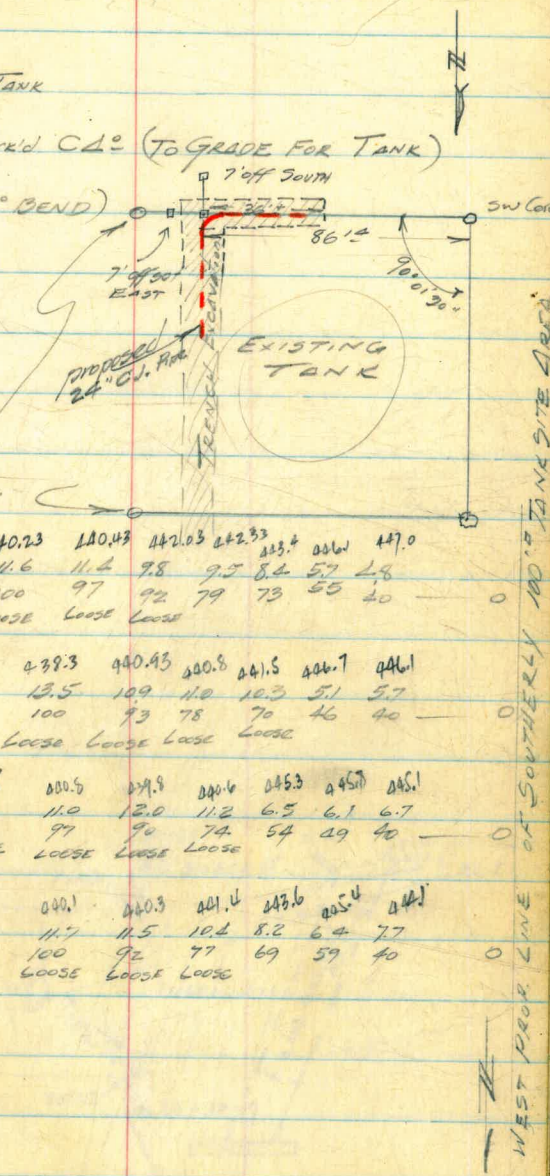
1+00 = 100' So. / SW Cor Existing Tank Site

PROPOSED  
2nd  
TANK SITE

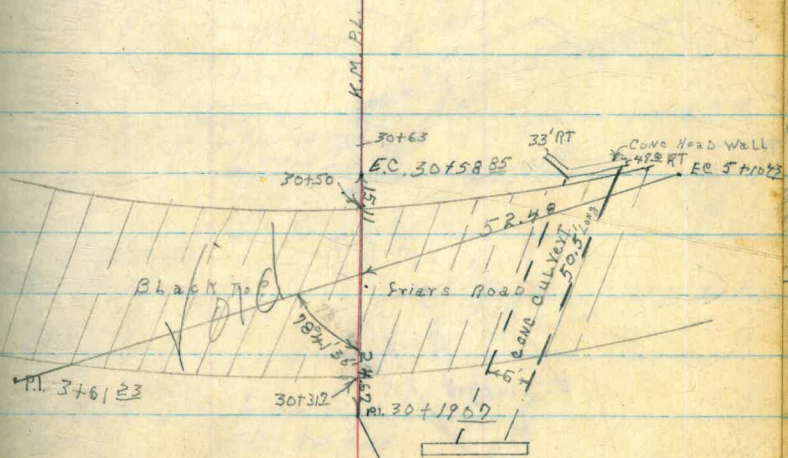
(SEE Pgs 84-86  
THIS BOOK)

CK BM

0.01 451.82



WEST PROP. LINE OF SOUTHERLY 100' TANK SITE AREA



June 13, 1919

(Cont. FB 769 pg. 16)  
2-9-99 RM

46+79.5 Ah =  
46+82.24  
EQUATION AT EXISTING EC.

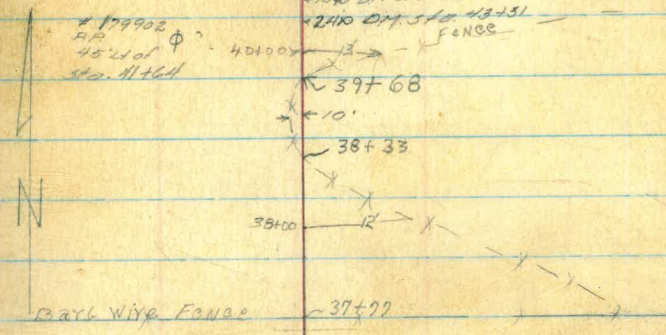
Railway  
Shack  
West  
Fence

#179901  
PP  
45' 21" of  
Sta 44+90

Gravel rd  
strand B wire fence  
1119 Sta. 43+25

#179902  
PP  
45' 21" of  
Sta. 41+61

1500 DM Sta 43+75  
2210 DM Sta 43+31  
FENCE



PP 179903 - 45' -> 36+81  
PP 179904 - 45' -> 31+43  
Dead Man x 42' -> 30+95

Double dead man  
Sta 31+39

134200  
B wire fence  
EC Sta.  
30+59.25  
Sta. 30+31

FRAMES  
Road  
2" cold lay

edge oil  
Sta 30+31  
2" water  
Sta. 30+100

EC Sta. 29+80.23

(Cont. from  
FB 771 pg. 37)



Profile on K.M. Realignement Sta 30+59.25  
 (Cont. from FB 771 p. 45)  
 8-4-49 RM To 46+82.44

July 13, 1949

Shipman  
 West  
 Payne

25

STA	+	π	-		LT	RT
B.M.	7.09	90.13		83.04		
30+59.25			9.3	80.8	90.0	81.9
30+64			6.4	83.7	$\frac{0.1}{25}$	$\frac{8.2}{25}$
Top Culvert			4.1	81.0		
Culvert						
Flow Line			14.1	76.0		
T.P.	10.21	99.88	0.46	89.67		
31+00			6.6	93.3	$\frac{93.9}{25}$	$\frac{91.9}{11}$ $\frac{86.8}{25}$
					$\frac{6.0}{25}$	$\frac{8}{11}$ $\frac{13.1}{25}$
31+50			1.7	98.2	$\frac{98.5}{25}$	$\frac{97.8}{16}$ $\frac{94.5}{25}$
					$\frac{1.4}{25}$	$\frac{2.1}{16}$ $\frac{5.4}{25}$
T.P.	12.22	111.92	0.18	99.90		
32+00			8.4	103.5	$\frac{104.2}{25}$	$\frac{102.9}{9.0}$
32+50			2.8	109.1	$\frac{103.5}{25}$	$\frac{100.0}{3.3}$
					$\frac{110.0}{19}$	$\frac{108.6}{3.3}$
T.P.	13.09		2.10	109.82		
		122.91				
33+00			7.6	115.3	$\frac{115.9}{25}$	$\frac{115.8}{7.1}$
					$\frac{7.0}{25}$	$\frac{7.1}{25}$
33+50			1.0	121.9	$\frac{122.7}{25}$	$\frac{122.0}{0.9}$
					$\frac{0.2}{25}$	$\frac{0.9}{25}$
T.P.	12.94	135.27	0.58	122.33		

BM ON SPIKE IN Friers Road

June 14, 1949

Shipman  
West

26

Sta	+	T	-			
		135.27				
34700			6.8	128.5		
					129.4	128.9
					5.9	6.4
					<u>25</u>	<u>25</u>
T.P.	12.55	147.41	0.41	134.86		
34750			10.0	137.4		
					140.4	136.6
					7.0	10.8
					<u>25</u>	<u>25</u>
T.P.	12.96	160.37	0.0	147.41		
35700			9.8	150.6		
					147.4	153.8
					13.0	6.6
					<u>25</u>	<u>25</u>
T.P.	12.70	172.28	0.29	160.08		
35750			10.6	162.2		
					168.1	156.9
					7.7	15.9
					<u>25</u>	<u>25</u>
					178.2	165.4
36700			0.3	172.5		
					+5.4	7.4
					<u>25</u>	<u>25</u>
T.P.	12.22	185.47	0.03	172.25		
36750			3.5	182.0		
					195.2	171.7
					+9.7	13.8
					<u>25</u>	<u>25</u>
T.P.	5.75	190.73	0.49	184.98		
37700			1.7	189.0		
					180.9	178.7
					9.8	12.0
					<u>25</u>	<u>25</u>

		190.23			
37+50			4.5		186.2

T.P.	3.39	185.77	8.35	182.38	
------	------	--------	------	--------	--

38+00			5.6		180.2
-------	--	--	-----	--	-------

38+43			12.0		173.8
-------	--	--	------	--	-------

38+50			16.2		175.6
-------	--	--	------	--	-------

39+00			8.6		177.2
-------	--	--	-----	--	-------

T.P.	12.99	197.72	10.4	184.73	
------	-------	--------	------	--------	--

39+50			9.7		188.0
-------	--	--	-----	--	-------

40+00			0.2		197.5
-------	--	--	-----	--	-------

T.P.	12.90	210.60	0.02	197.70	
------	-------	--------	------	--------	--

T.P.	11.09	220.76	0.93	209.67	
------	-------	--------	------	--------	--

40+50			6.8		214.0
-------	--	--	-----	--	-------

197.7	175.6
+ 9.0	15.1
<u>25</u>	<u>25</u>

189.5	174.8	171.3	165.6
+ 3.7	11	14.5	RDR
<u>25</u>	<u>12</u>	<u>78</u>	<u>30</u>

183.2	169.1
2.6	16.7
<u>25</u>	<u>22</u>

188.8	174.5	173.9
+ 3.0	11.3	11.9
<u>25</u>	<u>4</u>	<u>23</u>

197.7	182.1	179.3
0.0	15.6	18.4
<u>25</u>	<u>15</u>	<u>78</u>

185.9	186.1	183.1
11.8	11.6	14.6
<u>25</u>	<u>25</u>	<u>33</u>

225.6	198.7
+ 4.8	22.1
<u>25</u>	<u>25</u>

STH.	+	π	-			
		220.76				
T.P	7.96	223.39	5.33	215.43		
41+00			1.5		221.9	215.4 8.0 <u>25</u>
T.P	4.31	214.84	12.86	210.53		
41+50			6.2		208.6	220.1 +5.3 <u>25</u>
T.P.	10.59	223.39	2.04	212.80		
T.P.	12.59	235.98	0.00	223.39		
42+00			6.4		229.6	226.9 9.1 <u>25</u>
T.P	12.76	248.59	0.35	235.63		
42+50			7.2		241.4	
43+00			1.8		246.8	
T.P.			0.39	242.20		
	11.85	260.05				
43+50			6.1		254.0	



260.05

44+00 3.9 256.2

44+50 1.9 258.2

I.P. 0.67 259.38

18.89 272.27

45+00 11.3 261.0

45+50 9.0 263.3

46+00 4.7 267.6

46+50 0.0 272.3

ck to P.I. 5/24/1922 2.47 269.80 269.76 Corr.

Checked & Reduced pg. 25-29  
6-15-49 RM.

(See FB. 769 pg 32)  
8-4-49 RM

10-24-49

# REVISION CHESTERTON PIPELINE

King T  
Shipman  
West

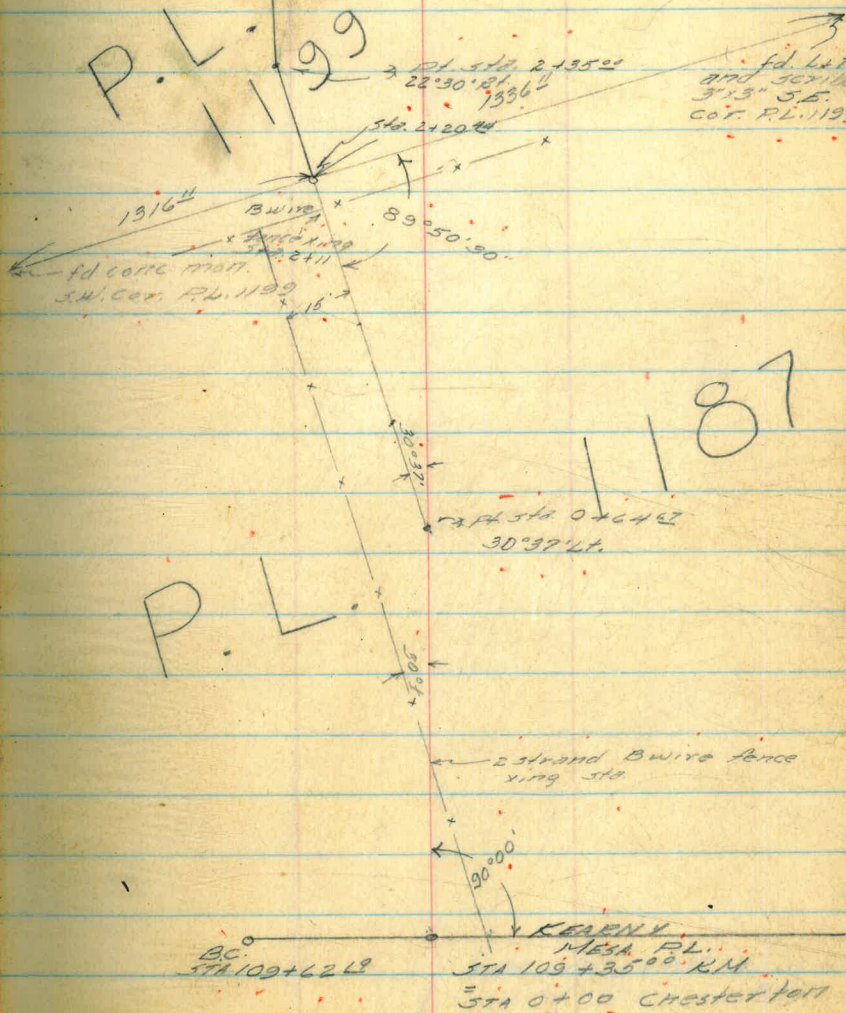
Rainy - Notes

Rainy  
King  
Shipman  
West.

3 Pt. Sta. 2+72.00  
21°58'30" LT

30

P.L. 1199



fd. lat  
370' 50" 00"  
3' 15" S.E.  
Cor. P.L. 1199

P.L.

1187

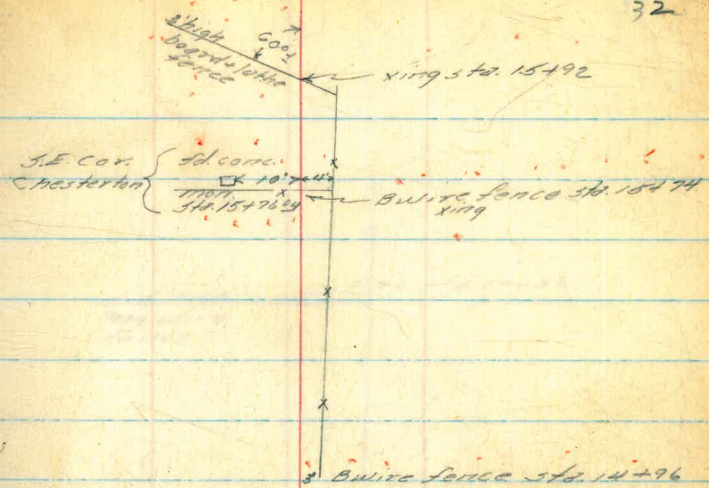
BC  
Sta 109+62.00

KEARNY  
MESA P.L.  
Sta 109+35.00 K.M.  
Sta 0+00 Chesterport

SEE REVISED BEGINNING  
PAGE 51  
EE.

2 Pt. Sta. 2+72<sup>00</sup> 21°58'30"  
 Gladiolos Lt.  
 2+59  
 2 Pt. Sta. 2+35<sup>00</sup>  
 22°30' Lt

3" Water



5' high  
hog wire  
fence

1199 sta. 17+56

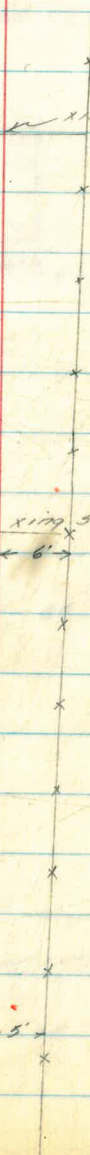
30' high  
rustic board  
rail fence

85' xing sta. 16+99

1700 6'

16+00

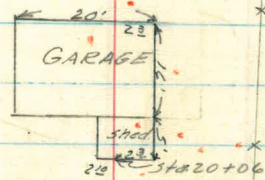
5'



REVISION OF  
CHESTERTON PL.

39

PLAIN  
WIRE FENCE



19+00 ← 82

PPHS  
φ

DM 578  
○

4' high  
WIRE FENCE

X 1179 STA 18+03

18+00 ← 75

22+07  
 10' 11c'  
 HOUSE  
 4' 6'  
 5/16. 21+97

2400 ← 10'

3' 10' 11c' 5/16. 20+54  
 Pick of fence

2' 4' 10' 11c' 5/16. 20+74  
 Wood fence

< 7' 9 1/2' 27+80

27+00

< 15'

26+50

26+31 W.M. Box  
7' R

Top Pipe  
El. 3783

26+07

27+405 Fd Pipe

6" 8' Cotton  
Road  
Tees

25+80

< 22'

1  
+  
0

214'

15 22 1/2  
Fd. Pipe

< 10'

E.C.

23+22.33 H.H. = 23+06.0 BK.

$\Delta S = 41.03715''$   
 $R = 80.06'$   
 $L = 58.16'$

22+48 P.P. = El. 3765

BC Sta. 22+60.47

New Alignment

RF

Fd Pipe 252317

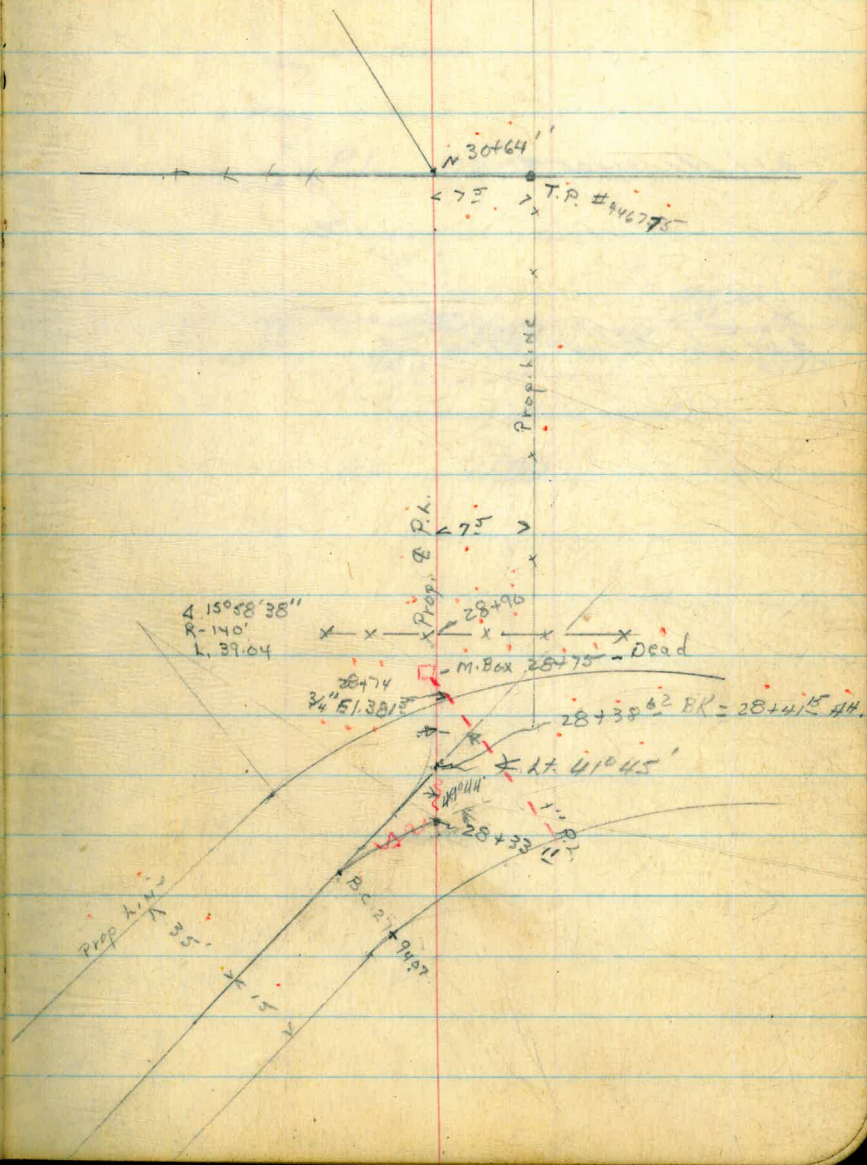
M. Box

Existing Alignment

22+30.24 41' 40" Pt

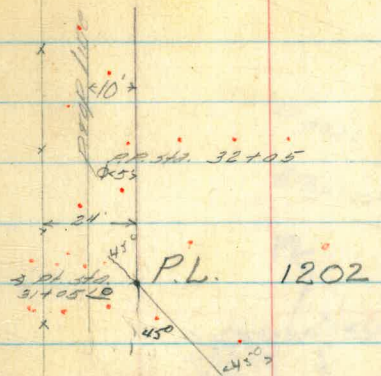
3" Water  
on top ground  
P.L.  
3





3 PL. Sta. 31405<sup>12</sup>

3 PL. Sta. 30264<sup>17</sup> 45°00' Lt.



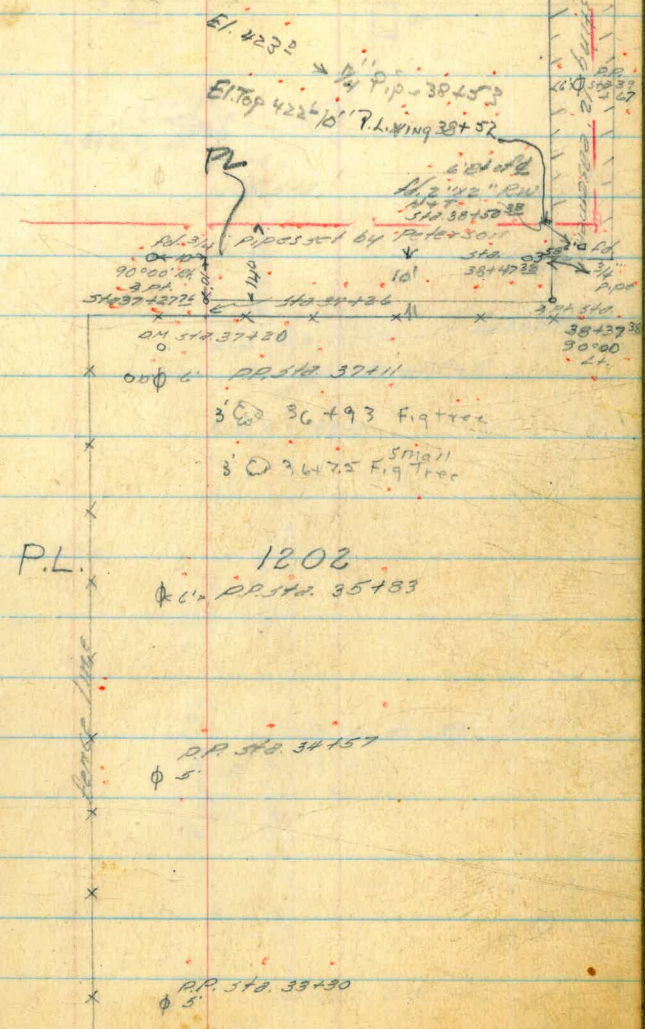
Ad Conc. 213.30  
 NE Cor 21.34  
 CHESTNUT 2317  
 21.212"  
 NE 500 P77 45°00' Lt.  
 18.1741  
 (3.22 West of line ahead)

P.L. 1199



2 Pt. Sta 38+37.38 90°00' Lt.

3 Pt. Sta 37+27.26 90°00' Rt.



El. 423.2  
El. Top 422.10 P.L. Wing 38+52

P.L.  
"The 1/2" Riv  
Sta 38+50.38"

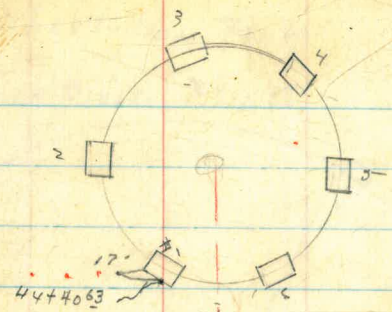
10.34  
90°00' Lt  
54+37+27.26  
ON Sta 37+20  
10' 38+42.28  
3/4" Pip  
38+37.38  
90°00' Lt.

φ 6" P.P. Sta. 37+11  
36+93 Fig Tree  
Small 36+25 Fig Tree

P.L. 1202  
φ 1" P.P. Sta. 35+83

P.P. Sta. 34+57  
φ 5"

P.P. Sta. 33+30  
φ 5"



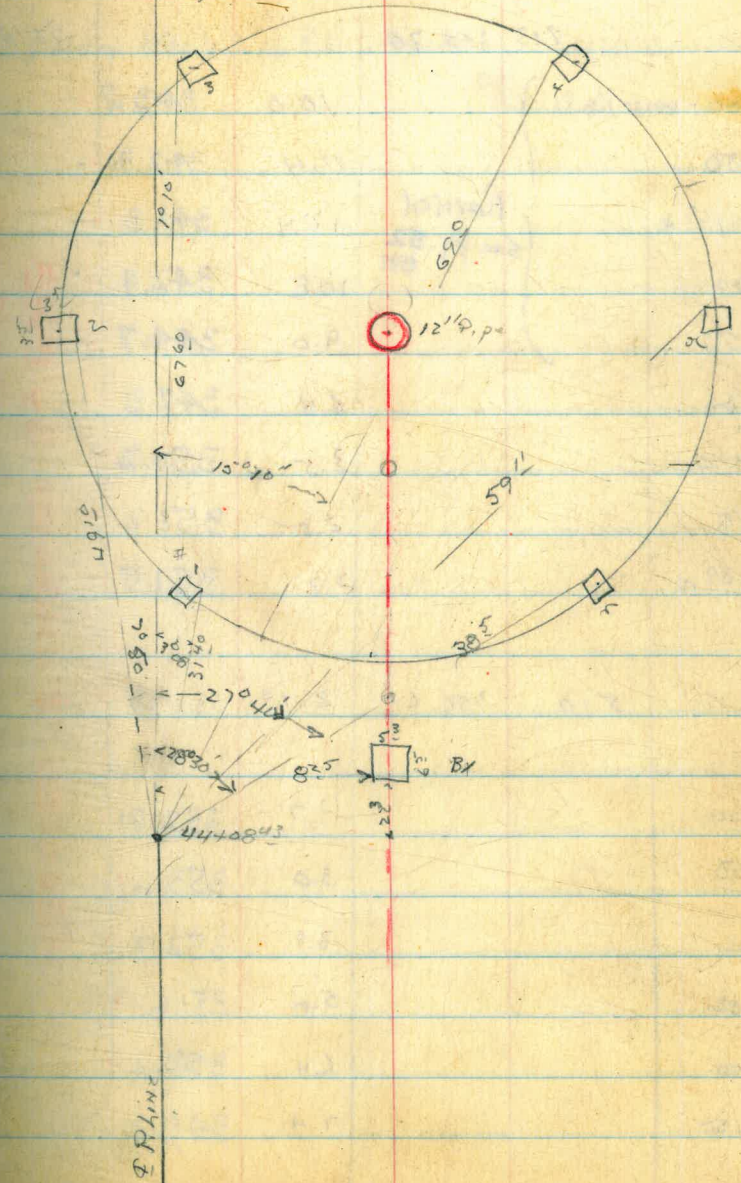
Existing P.L.  
 60' 2' x 2' CW. NAT 4440758  
 RR STA 44+06  
 10' 43+00

Proposed P.L.  
 60' RR STA 42+59  
 10' 42+00  
 Existing P.L.

RR STA 41+13  
 60'  
 10' 41+00  
 10' 39+00

Chesterlow Tank.

Top of Piers - 32 x 32



Profile Chesterton P.H.  
(New line)

11-14-49  
King  
10034  
Shipman

2.13 353.70

351.57

ON 91X Key 110220 K.M. P.H. Page 20

0+00 = 109435 P.H.

10.0 343.7

0+50

11.4 342.3

0+64<sup>67</sup> f

Revised  
See Pg. 52  
BE

12.4 341.3

1+00

10.8 342.9

1+50

9.0 344.7

2+00

6.4 347.3

2+35 f

3.5 350.2

2+50

2.5 351.2

2+72<sup>09</sup> f

2.2 351.5

T.P.

5.10 : 356.61 : 2.19 : 351.51

3+00

3.7 352.91

3+50

3.0 353.6

4+00

3.9 352.7

4+50

5.0 351.6

5+00

6.4 350.2

5+50

7.4 349.2

REDUCED & CHECKED BY LEWE. 12-15-49

356.61

6+00	8.0	348.6
6+50	9.2	47.4
7+00	10.0	46.6
7+50	10.6	46.0
8+00	10.8	45.8
8+50	11.5	45.1
8+75 ditch	12.9	43.7
9+00	9.8	46.8

T.P. 9.62 357.94 8.29 348.32

9+50	8.7	349.2
10+00	8.2	49.7
10+50	7.0	50.9
11+00	7.5	50.4
11+50	6.7	51.2
12+00	5.1	52.8
12+50	4.7	53.2
13+00	5.1	52.8

357.94

13+50	4.9	353.0
14+00	3.6	54.3
14+50	6.0	51.9
14+65	6.5	51.4
15+00	4.9	53.0
15+50	3.6	54.3

T. B. M. 12.65 367.82 2.77 355.17

16+00	12.6	355.2
16+50	11.9	55.9
17+00	11.7	56.1
17+50	11.0	56.8
18+00	10.0	57.8
18+50	8.4	59.4
19+00	5.3	62.5
19+50	2.5	65.3
20+00	1.6	66.2

T. P. 12.10 378.59 1.33 366.49

ON CONC. MON. 16th Sta. 15+74 2 15+76.04 BE.



378.59

20+50	8.8	369.8
20+84	7.0	71.6
20+85	5.9	72.7
21+00	5.7	72.9
21+50	4.1	74.5
22+00	3.0	75.6
22+30 <sup>24</sup>	2.2	76.4
22+50	2.1	76.5

T.B.M. 6.84 384.02 1.41 377.18

23+00	7.9	376.1
23+50	7.1	76.9
24+00	6.8	77.2
24+50	6.0	78.0
25+00	5.9	78.1
25+50	5.5	78.5
26+00	5.2	78.8
26+50	3.8	80.2

on E.C. Propylene Pipe No. Side Pol 2340610

384.02

27700	2.9	381.1
27750	2.9	82.1
28100	1.2	82.8
28+3862 BK 284415	1.5	82.5
28+50	1.5	82.5

T.P. 12.80 395.47 7.35 382.67

29700	11.8	383.7
29750	10.9	84.6
30400	9.7	85.8
30750	7.6	87.9
30964 +	6.6	88.9
31205 <sup>10</sup> +	6.0	89.5
31750	3.7	91.8
32400	1.9	93.6

T.P. 11.50 406.05 0.92 394.55

406.05

32+50	9.4	396.7
33+00	6.6	399.5
33+50	4.6	401.5
34+00	2.7	403.4

T.P	12.57	417.63	0.99	405.06
-----	-------	--------	------	--------

34+50	11.5	406.1
35+00	9.0	08.6
35+50	7.5	10.1
36+00	6.2	11.4
36+50	4.6	13.0
37+00	3.1	14.5
37+27.24	2.2	15.4

T.P	12.92	428.14	2.41	415.22
-----	-------	--------	------	--------

37+50	8.3	419.8
38+00	7.2	20.9

428.14

28+37.38

3.8

424.3

28+50

3.2

24.9

39+00

1.3

26.8

T.P.

10.25

437.04

1.35

426.79

39+50

8.0

429.0

40+00

6.9

30.1

40+50

5.6

31.4

41+00

5.1

31.9

41+50

3.8

33.2

42+00

1.6

35.4

T.P.

10.62

447.00

0.66

436.38

42+50

8.8

438.2

43+00

5.1

41.9

43+50

1.8

45.2

T.P.

7.55

452.40

2.15

444.85

452.40

44700

5.0

4474

4470843

4.9

447.5

B.M

0.51

451.89

451.82

CONC. Pier Water Tank

Cont'd. on p-50

BM

0.11

451.93

451.82

IP

0.95

446.02

6.86

445.07

0.38

433.38

13.02

433.00

0.90

421.52

12.76

420.62

Hub T curb F019

6.56

414.98

415.91

E " " F019

5.47

416.05

416.24

(5) F.H.

5.59

415.93

416.10

Bottom 18"

408.8

IP

0.49

415.36

6.65

412.87

IP

0.33

406.36

9.33

406.03

(3) F.H.

6.23

400.12

400.40

Bottom 18"

391.2

IP

2.34

396.33

12.35

394.01

CK

6.36

389.97

389.99

Nail in pole

REMOVED & CHANGED BY E.W.E. 12-15-49

2 1/2" x 1/2" post

8' LT 37+04.19  
FO2 to E C62 to E11

on 3/2" IP

8' LT 32+52.20  
CO- C82

X-sections & Profile  
 Chesterton P.L.  
 #1 " TANK

King-Notes 1-19-50  
 Shipman  
 West

clear  
 cool

50

#1

RT

B.M. 1.02 • 452.84 • 451.82 •

Top Conc. Pier #2

44+00

5.4 447.2

$\frac{98}{30}$   $\frac{60}{12}$   $\frac{50}{10}$   $\frac{49}{19}$   $\frac{69}{30}$

+25

+25

4.4 448.4

$\frac{67}{30}$   $\frac{52}{12}$   $\frac{32}{9}$   $\frac{38}{30}$

+50

3.3 449.5

$\frac{64}{30}$   $\frac{48}{12}$   $\frac{27}{11}$   $\frac{18}{17}$   $\frac{31}{34}$

+75

3.4 449.4

$\frac{50}{30}$   $\frac{41}{12}$   $\frac{24}{12}$   $\frac{25}{34}$

45+00

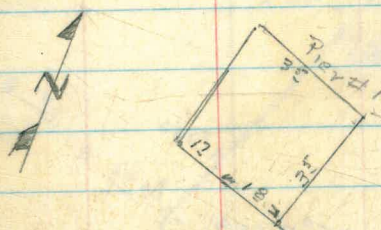
2.1 450.7

$\frac{48}{30}$   $\frac{30}{12}$   $\frac{18}{12}$   $\frac{24}{30}$

B.M.

1.01 451.81

#1 Chesterton P.L.



Chesteron Pk.  
 Realignment - 0+00 - 1+65.80  
 For Pump House

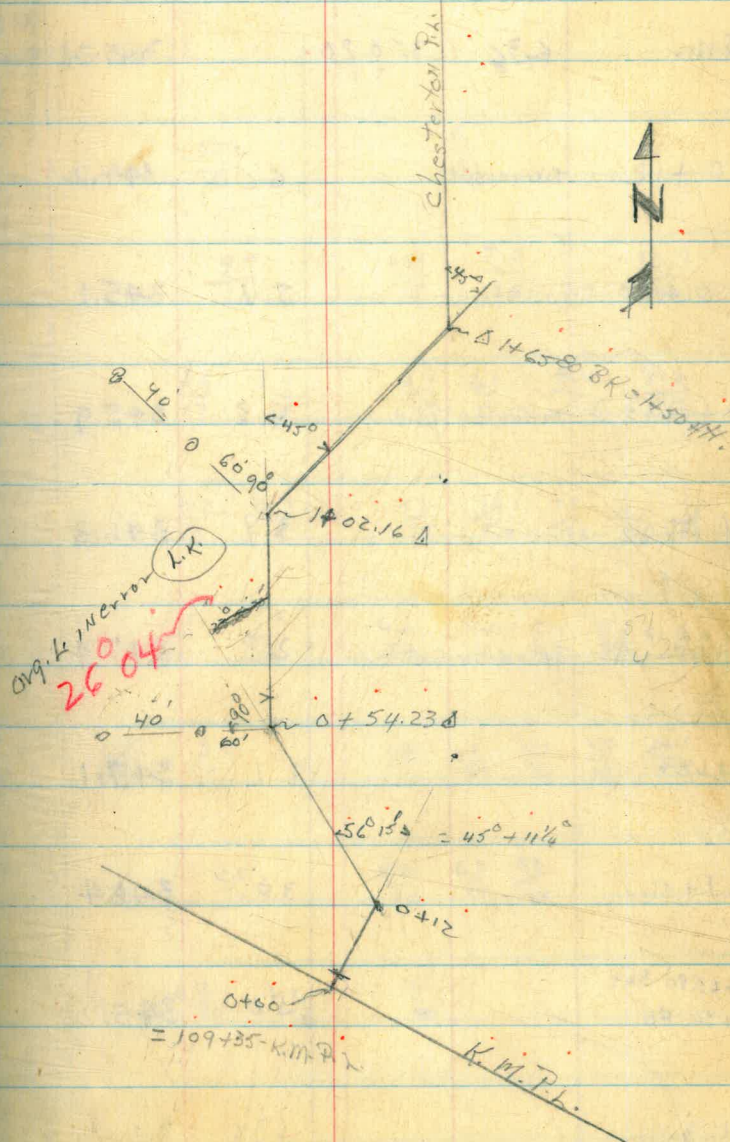
◁	1+50 FH.	45° L.
	1+65.80 BK =	
◁	1+02.16	45° R.
◁	0+54.23	33° 50' 30" R.
◁	0+12	56° 15' LT.
0+00	0+00	

King T  
 Shipman  
 West

1-23-50

Clear - Cool

51



Chesterton P.L.  
Profile & X-sections on  
Relocation for Pump House  
0+00 - 1+65

King-Notes  
Shannon-R  
West-T

1-23-50

clear - Cool

5-2

LT

RT

B.M.	6.36	350.20	343.84	NE Cor 91N x 94	on Box 109435 - K.M.P.H.
0 + 12	Taken on split	6.0	344.2		5.2 10
0 + 25		5.1	345.1		4.5 10
0 + 54.23	Taken on split	4.3	345.9		6.8 13
0 + 75		3.9	346.3		8.0 26
1 + 02.16	Taken on split	2.8	347.4		9.1 29
1 + 25		3.1	347.1		10.9 40
1 + 50		3.8	346.4		4.9 13
1 + 65.80 BK = 1 + 50 FH.		5.0	345.2		6.1 17
ck. 8.71		6.34	343.84		8.4 29

5.6  
10

6.9  
35

2.5  
12

5.2  
10

6.2  
14

8.3  
32

4.1  
10

2.4  
25

3.2  
18

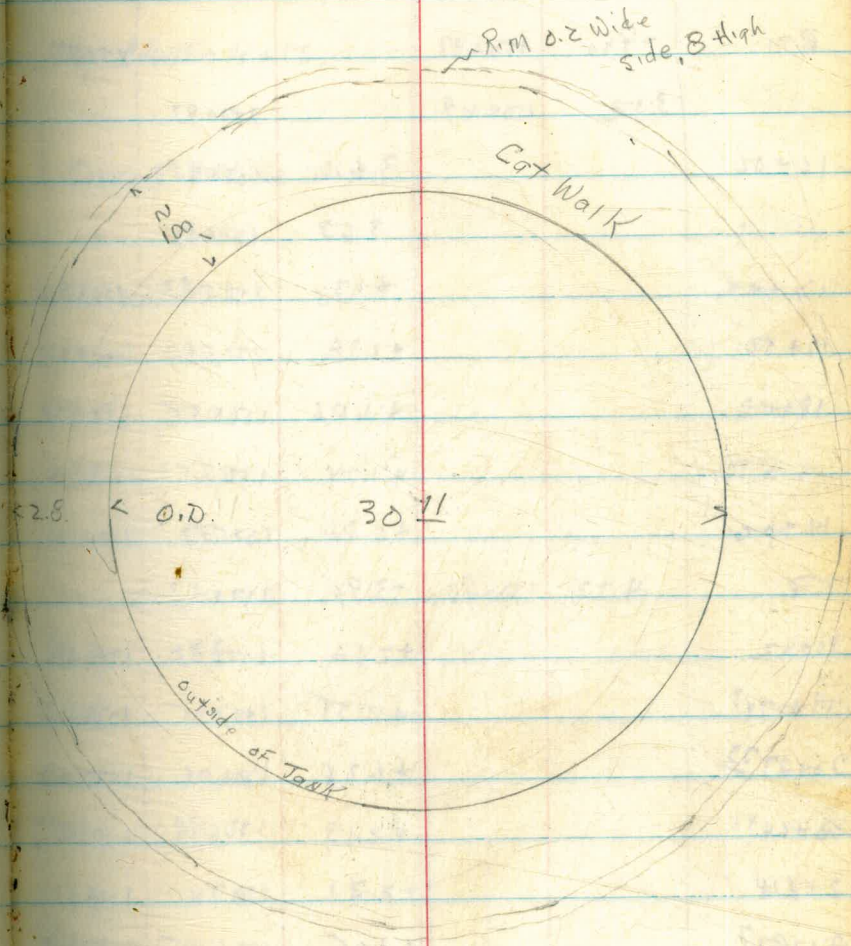
7.1  
20



Chesterton Water Tank

King  
Shipman  
West

1-23-50



Dulzura Conduit  
Flume-S - Flume #7

KING  
Baker  
West

9-11-50

59

B.M.	-9.40	1500.97		1510.37		Top #dwll - 16+56
	3.52	1504.49		1500.97		
16+52			3.60	1500.89		Conc. End Flume #6
11			3.63	1500.86		
17+00			+1.34	1505.83	1500.86	4.97
17+50			+1.38	1505.87	1500.89	5.04
18+00			+1.06	1505.55	1500.80	4.75
+50			+1.04	1505.53	1500.76	4.77
19+00			+0.88	1505.37	1500.72	4.65
T.P.	4.27	1504.80	-3.96	1500.53		
19+42			+2.52	1507.32	1500.69	6.63
19+78 <sup>3</sup>			+2.55	1507.35	1500.67	6.68
20+27 <sup>2</sup>			+1.26	1506.06	1500.63	5.43
20+64 <sup>11</sup>			+2.19	1506.99	1500.61	6.38
21+18			+2.31	1507.11	1500.51	6.54
21+97 <sup>7</sup>			+1.65	1506.45	1500.51	5.94
22+14 <sup>81</sup>			+1.55	1506.35	1500.50	5.85
22+88 <sup>57</sup>			+2.36	1507.16	1500.45	6.71

1504.80

23+19.14			+2.24	1507.08	1500.41	6.67
24+20.39			+2.27	1507.07	1500.35	6.72
24+61.34			+1.72	1506.52	1500.33	6.19
T.P	3.98	1503.79	-4.99	1499.81		
25+12.6			-0.67	1503.12	1500.29	2.83 - Scratch on wall
25+32.4			+0.90	1504.69	1500.27	4.43
26+00			+1.11	1504.90	1500.23	4.67
26+50			-1.02	1502.77	1500.20	2.57 Top Wall in Tunnel
27+00			-1.43	1502.36	1500.16	2.20 - Scratch on wall
27+50			+0.78	1504.59	1500.13	4.44
T.P	4.42	1504.18	-4.03	1499.76		
28+00			+0.33	1501.51	1500.08	4.42
+50			+0.22	1504.40	1500.14	4.34
29+00			+0.15	1504.33	1500.02	4.39 4.31
T.P	4.53	1504.13	-4.50	1499.60		
29+50			-1.22	1502.91	1499.99	2.92 Ox Wall
30+00			+0.19	1504.32	1499.96	4.36
T.P	2.73	1502.36	-4.50	1499.63		
30+50			+1.97	1504.33	1499.33	4.40

		1502.36			
T.P.	+3.90	1503.20	-3.06	1499.30	
31+00			+1.00	1504.20	1499.89
31+09			-4.00	1499.70	
+19			-3.32	1499.84	
31+93			-3.45	1499.75	1499.78

4.31

Step up in Floor

Top Concrete New Floor

Bottom Floor #7 - BK671

## Dutzura Conduit

Tunnel # 6  
Profile & CutsKing  
Baker  
West

9-13-30

57

T.B.M	0.68	1461.72		1461.04	Top Lt Wall 547409-BK.671	
3 547459 <sup>s</sup>			+1.74	1463.46	1456.97	6.49
3 gr			-4.75	1436.97		
548400			+1.78	63.30	52.93	6.57
gr			-4.14			
3 548420 <sup>2</sup>			-5.0			Top Floor in some part of Tunnel
+4.5 <sup>0</sup> gr			-4.52			
+4.5 <sup>0</sup>			+0.93	62.65	52.49	5.76
549400			+3.30	65.02	52.84	8.18
gr			-4.5			
+50			+1.30	63.02	52.79	6.23
gr			-4.1			
550400			+2.01	63.73	52.74	6.99
gr			-4.2			
+50			+2.03	63.75	52.69	7.06
gr			-4.4			
551400			+1.60	63.32	52.64	6.68
gr			-4.5			
T.P	-2.24	1461.08	+1.60	1463.72		

1461.08

551450

+2.65 63.73 58.59 7.14

qr

-3.5

3 552400

+3.13 64.21 58.54 7.67

qr

-3.9

552450

+2.22 63.30 58.49 6.81

qr

3.9

553400

+3.05 64.13 58.44 7.69

qr

-4.1

+50

+2.61 63.69 58.39 7.30

qr

-4.2

554400

+2.45 63.53 58.34 7.19

qr

-3.9

+50

+2.94 64.02 58.29 7.73

qr

-4.6

555400

+2.37 63.45 58.24 7.21

qr

-4.2

+50

+2.85 63.93 58.19 7.74

qr

-4.0

B.P

-2.87 1461.06 +2.85 1463.93

1461.06

556 + 00

+2.01

63.07

56.14

6.93

9r

-4.3

3 + 50

+1.71

62.77

56.09

6.68

9r

-4.2

557

+1.87

62.93

56.04

6.89

9r

-4.4

+33

+4.33

1456.73

1456.00

C.O. 73 - ginnery in 2 Tunnel Portal - Oct 6 1867

+35

-1.47

1459.59

T.B.M. 6' Pt 557 + 35 - on Pt. of Rock - pointed

Chesterton P.L.

King T  
BAKER LEVEL  
WEST CH - etc.

9-14-50

CLEAR WARM

60

351.18

Top CONC. MON - Hgh W 395 - R.M. 7-1-#2

N.W. Cor. K.M. Ph. B.V. chamber 109435 = 0400 Chesterton

c 7 3/4

c 8 1/4

c 6 5/8

c 5 1/4

c 5 7/8

c 5 1/4

c 4 8/8

c 5 9/8

c 5 4/8

B.M.	6.32	357.50		351.18
T.B.M.	8.00	354.94	-10.56	344.94
0+54 <sup>23</sup> (6)			8.6	346.3 339.0
1402 <sup>16</sup> (6)			8.0	346.9 338.2
1450 (6)			9.2	345.7 339.2
1465 <sup>80</sup> BR (6)			10.0	344.9 339.3
1450 <sup>4h</sup> (6)			9.9	345.0 339.3
2+04 <sup>44</sup> (6)			7.4	347.3 341.9
2+41 <sup>53</sup> (6)			5.9	349.0 344.2
2+41 <sup>53</sup> (5)			5.7	349.2 344.2
2+50 (5)			5.0	349.9 344.5



Chesterton Pk.  
5-10-50

Keep  
Elev.  
West

9-14-50

51

354.94

354.94

3400 (3)			2.3	352.8	346.4	<sup>c</sup> 6.2
450 (3)			1.3	353.6	346.7	<sup>c</sup> 6.9
4700 (3)			2.1	352.8	346.3	<sup>c</sup> 6.5
450 (3)			3.4	351.5	346.0	<sup>c</sup> 5.5
5700 (3)			4.6	350.3	345.0	<sup>c</sup> 5.3
5750 (3)			5.7	349.2	344.0	<sup>c</sup> 5.2
6700 (3)			6.5	348.4	343.0	<sup>c</sup> 5.4
T.P.	2.30	350.78	6.46	348.48		911474 @ 640'
6450 (3)			3.3	347.5	342.0	<sup>c</sup> 5.5
7400 (3)			4.1	346.7	341.1	<sup>c</sup> 5.4

Chesteron P.h.  
5' OFF

King  
West  
Baker

9-14-50

62

350.18

7450 ③

4.6

346.2

340.2

c 60

8400 ③

5.4

345.4

339.3

c 61

8450 ③

5.4

345.4

338.5

c 62

8475

6.0

344.8

338.5

c 63

9400 ③

4.1

346.7

339.5

c 72

T.B.M.

11.26

357.95

4.09

346.69

GINNEY - 9400

9425

9.5

9.8

48.5

46.0

7.5

+50

8.9

49.1

42.5

6.6

+75

8.8

49.2

43.5

5.7

10400

8.1

49.9

44.0

5.9

10450

7.2

50.8

44.5

6.3

Chesterton Ph.

King  
Baker  
West

9-14-50

67

357.95

11700	7.3	50.7	45.0	5.7
	<del>6</del>			
11750	6.4	51.6	45.5	6.1
12700	4.9	53.1	46.0	7.1
+50	4.6	53.4	46.0	7.4
13700	5.2	52.8	46.0	6.8
+50	4.3	53.7	46.0	7.7
14700	3.9	54.1	46.0	8.1
+50	5.5	52.5	46.0	6.5
+63	6.2	51.8	46.0	5.8
15700	5.4	52.6	47.0	5.6

Chesterton P.h.

King  
Baker T.  
West.

9-14-50

64

357.95

15+50

3.5

57.5

48.5

6.0

16+00

2.5

55.5

48.9

6.6

+50

1.8

56.2

49.3

6.9

16+75

1.4

56.6

49.5

7.1

T.P.

10.86

367.43

1.38

356.57

2

17+00

11.2

56.2

380.0

6.2

17+50

10.3

57.1

51.0  
~~58.5~~6.1  
~~6.6~~

18+00

9.1

58.3

52.0

6.3

+50

7.5

59.9

54.0

5.9

19+00

4.7

62.7

56.5

6.2

Chesterton Pk.

King  
West  
Baker

9-14-50

65

367.43

19450			1.7	65.7	59.0	6.7
20700			1.0	66.7	61.5	4.9
T.P.	10.58	372.06	0.95	366.48		
20750			7.3	69.8	64.0	5.8
21400			3.9	73.2	66.5	4.7
21450			2.3	74.8	68.7	6.1
22400			0.9	76.2	69.0	7.2
T.P.	5.28	381.44	0.90	376.16		
224024			4.8	76.8	69.2	7.4
B.m			4.17	377.27		

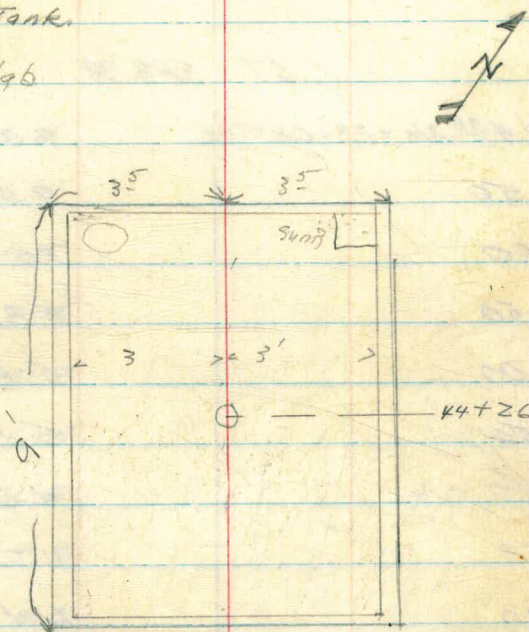
Chesterton P.L.  
 Constr. # H. Snyder G.V. Box 44+26<sup>13</sup>

King  
 West

9-28-52

46

B.M.	0.27	452.09		451.82	Top Conc. Pier Tank.
N.E. Cor (8') off			2.45	449.64	440.90 8.74
S.E. Cor (8')			2.72	449.37	441.22 8.15
S.W. Cor (8')			5.00	447.09	441.40 5.69
N.W. Cor (8')			4.50	447.59	441.15 6.44
	0.27			451.82	



Chesterton Const.

5' OFFsets

Lawrey

67

Sept. 29, 1950

King  
West

377.27 Pipe

6.67 383.94

23+24 <sup>33</sup> AH = 23+08 <sup>95</sup> BK	7.8	376.1	369.7	6.4
23+50	7.5	376.4	370.0	6.4
24+00	7.0	376.9	370.4	6.5
24+50	5.8	378.2 <sup>1</sup>	370.9	7.2 7.5
25+00	5.8	378.1	371.4	6.7
25+50	5.5	378.4	371.9	6.5
26+00	4.8	379.1	372.3	6.8
26+50	3.2	380.7	373.4	7.3
27+00	1.4	381.5	374.5	7.0
T.P.#1	1.70	382.24		
	8.40	390.64		
27+50	8.0	382.6	375.6	7.0
28+00	8.0	382.6	376.5	6.1
28+38.62 BK	8.1	382.5	377.2	5.3
= 28+41.15 AH	8.0	382.6	377.2	5.4
28+50	7.9	382.7	377.4	5.3
29+00	6.7	383.9	378.3	5.6

77.1  
4.5  
77.7  
5.5  
77.0  
7.0

77.1  
77.1  
5.5  
76.6  
5.0

Chesterton P.L.  
5' offsets

Rainey  
King  
West 9-29-50

68

390.64

29+50			6.0	384.6	379.2	5.4
30+00			4.7	385.9	380.0	5.9
30+50			2.6	388.0	382.0	6.0
30+61 <sup>2</sup> BK			1.0	389.5	382.5	7.0
30+61 <sup>2</sup> AH			1.39	389.25	382.5	6.7

31 T.P. 9.70 398.95

31+02.10			9.6	389.4	384.0	5.4
31+50			7.4	391.6	385.9	5.7
32+00			5.0	394.0	388.0	6.0
32+50			2.0	397.0	391.0	6.0

T.P. 13.24 410.91 1.28 397.67

33+00			11.2	399.7	394.0	5.7
+50			9.3	401.6	395.6	6.0
34+00			7.2	403.7	397.5	6.2
+50			4.4	406.5	400.2	6.3
35+00			2.2	408.7	403.0	5.7
+50			0.6	410.3	404.4	5.9

T.P. 10.77 421.06 0.62 410.29

04 91111111



421.06

36+00			9.7	411.4	405.7	5.7		
+50			7.2	413.9	407.1	6.8		
37+00			6.1	415.0	408.6	6.4		
Δ +27.26			5.3	415.8	410.0	5.8		6.5
37+50			4.1	417.0	411.5	5.5	3.40	420.90 417.5
38+00			8.3	420.8	415.2	5.6	36+50	4131 7.8 467.1 405.7 - 7.4
T.P	10.06	430.79	0.33	420.73			36+50	6.6 -14.3-407.1 -7.1
38+37.30 R			6.7	424.1	418.1	6.0	37+27.26	5.4 -15.5-410.0-5.4
RN			6.0	424.8	418.1	6.7		
+50			5.4	425.4	419.0	6.4		
39+00			3.7	427.1	421.0	6.1		
+50 25			2.0	428.8	422.0	6.8		
40+00 394.50			1.3	429.5	422.6	6.9		
T.P	12.12	441.57	1.34	429.45				ON GINNEY
40+00			10.7	309	424.0	6.9		
+50			9.8	318	425.0	6.8		
41+00			9.1	325	426.0	6.5		
+50			7.9	337	427.5	6.2		
42+00			5.8	358	429.5	6.3		

441.57

42450 2.5 39.1 432.5 6.6

T.P. 811.90 453.07 0.40 441.17

43400 10.2 429 435.5 7.7

43150 7.6 45.5 439.5 6.0

B.M. 1.23 453.07 1.23 451.82

43466 6.8 446.3 440.3 6.0

44415 4.00 449.1 442.9 6.2

4.23 451.84 451.81





MISC. ELEV.S  
CHESTERTON TANK

45482

5.2	449.62
4.1	50.7
9.2	45.6
4.9	49.9
3.21	51.61
3.07	51.75
3.01	51.81
3.29	51.33
3.46	51.36
7.11	447.71
2.06	51.76

FEB 26 1951

73

NAT. GED. 10' from Pier #3 outside

" " " " # 4 "

" " " " # 5.

" " " " # 6

Top 4" G.I. Blow-off line (Top all)

" " " " " " End of pipe

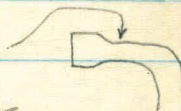
" " " " " " 6' from end of pipe

Top of orig Valve Chamber

Top of NEW " "

Top Conc Foot Pier N°1

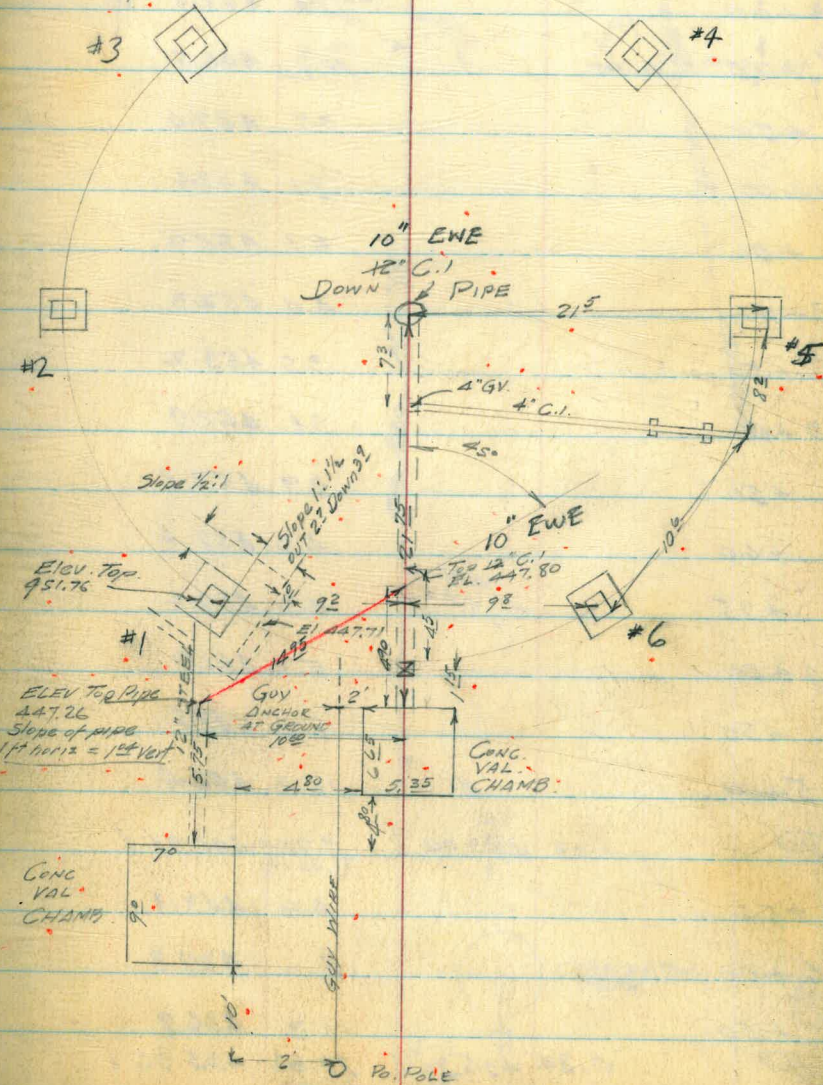
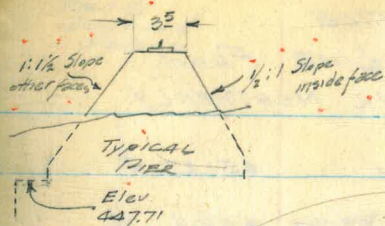
Top of Pier N°1



Feb. 26, 1961

# CHESTERTON TANK

## DETAILS

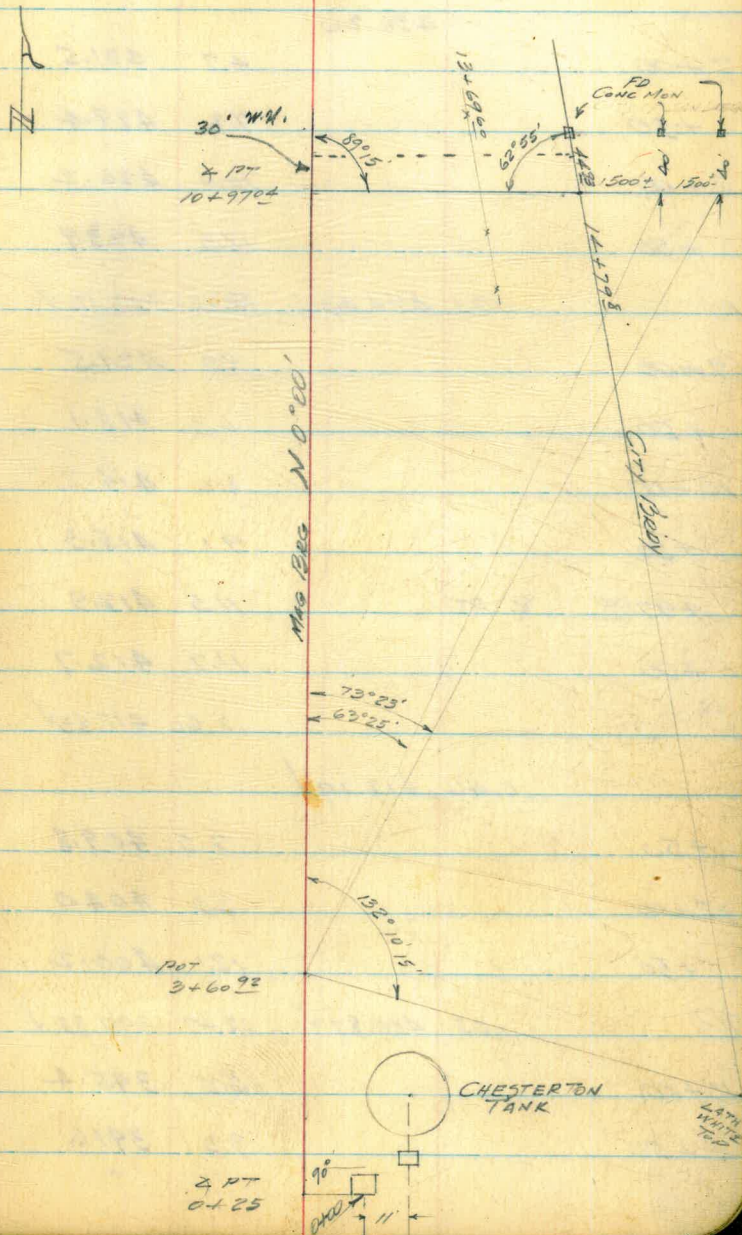


E PROFILE  
 PRELIMINARY LINE FROM  
 CHESTERTON TANK NORTHERLY

BM	4.84	456.66 ✓	451.82
0+00		7.9	448.8
+25	(2 PT)	10.2	446.5
+50		9.7	447.0
1+00		8.1	448.6
+50		6.1	450.6
2+00		4.4	452.3
+50		3.5	453.2
3+00		3.8	452.9
+50		3.9	452.8
+60		4.3	452.4
+75		4.3	452.4
4+00		5.7	451.0
+50		8.2	448.5
5+00		10.3	446.4
TP	1.03	447.99 ✓	9.70 446.96 ✓
+50		4.9	443.1
6+00		8.2	439.8
+50		11.3	436.7
TP	0.84	436.20 ✓	12.63 435.36 ✓

May 8 1951  
 Peaty  
 Leonard  
 Nelson

75.



5/8/51

76

# E PROFILE CHESTERTON TANK NORTH

	436.20		
7+00		4.7	431.5
+50		7.8	428.4
8+00		10.0	426.2
+50		12.3	423.9
P	1.31	13.08	422.43 ✓
9+00		2.9	421.5
+50		6.3	418.1
10+00		8.2	416.2
+50		9.1	415.3
+97 <sup>04</sup>	¥ PT.	11.5	412.9
11+00		11.7	412.7
P		12.60	411.83 ✓
	0.46		412.29 ✓
+50		2.5	409.8
12+00		8.3	404.0
+50		12.1	400.2
TP	1.05	12.47	399.82 ✓
13+00		5.5	395.4
+50		9.3	391.6



5/8/51

77.

2 PROFILE  
CHESTERTON TANK NORTH

	400.87			
7	13+69.6 (at fence)	10.6	390.3	
	W (rock)	0.26	388.57 ✓	12.56 388.31 ✓
8	14+00	2.0	386.6	
	+50	12.2	376.4	
4	SET TOM	1.30	380.57 ✓	9.30 379.27 ✓
				Top Conc Mon 44.3 at 14+79.8
9	+79.8	13.9	366.7	
10				
11				
12				
13				

CHESTERTON TANK  
LOCATION SURVEY

May 25, 1951  
BESSY  
LEONARD

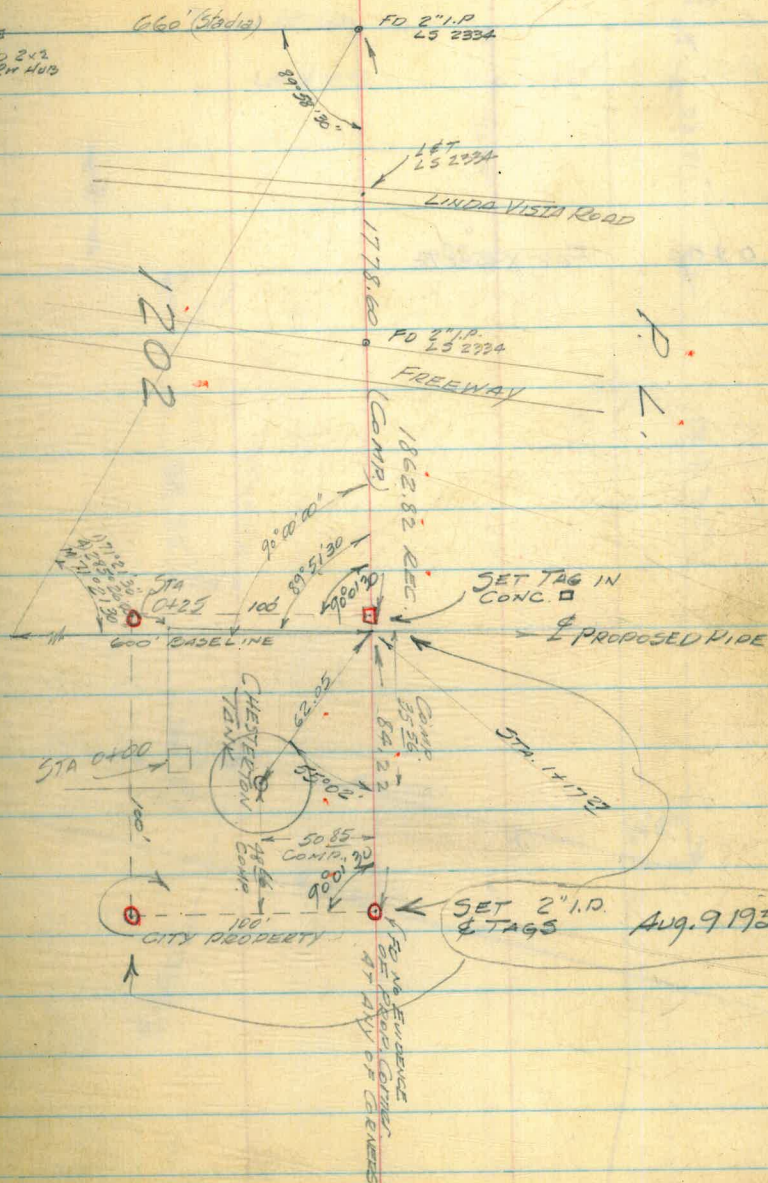
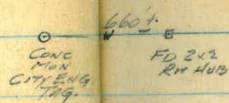
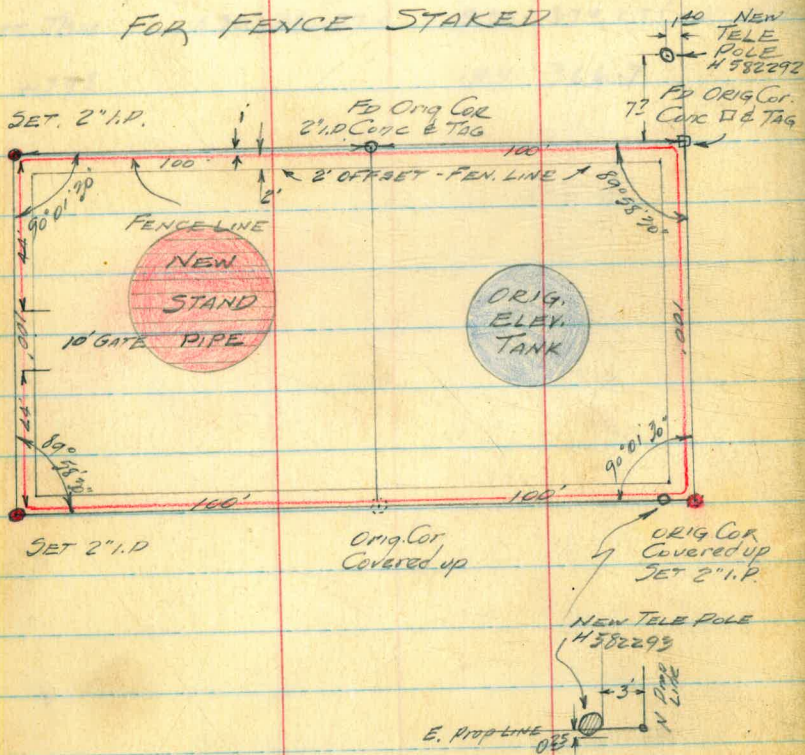
Aug. 9, 1951 78.

JUNE 29 1953

BESSY  
MARTELL  
ALEXANDER

PROPERTY CORNERS & 2' OFFSET

FOR FENCE STAKED



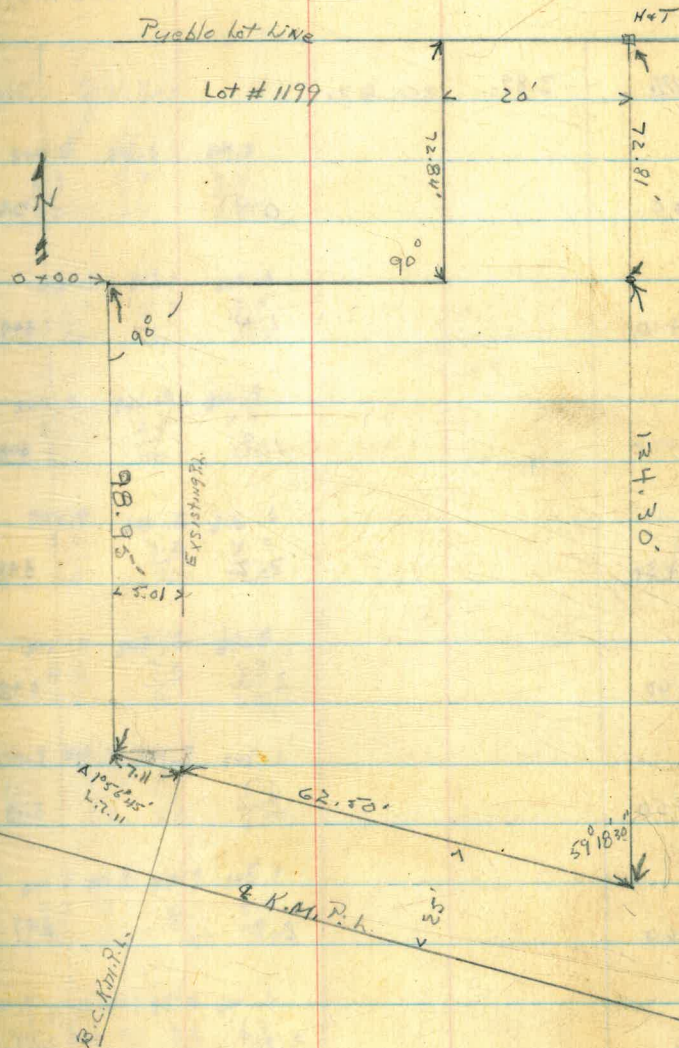
Aug. 9 1951

Chesterton P. Plant Site

King  
West  
Williams

79

0400 For X-Sections



Chesterton P. Plan  
 Site - X-sects  
 Base line West P.L. 0+00 = N.W. Cor.

King  
 West  
 Williams

7-20-57

80

B.M.	3.89	350.830	346.94
0+00		0.9	349.9
0+10		1.4	349.4
0+20		1.9	348.9
0+30		2.2	348.6
0+40		2.3	348.5
0+50		2.6	348.2
0+60		2.9	347.9
0+70		3.2	347.6
0+80		3.3	347.5

N.W. Cor G.V. Box

346.5 348.6 347.8  
 6.3 5.2 3.0  
 60 50 25

343.6 345.1 347.3  
 7.2 5.7 3.5  
 60 50 25

344.7 344.3 346.9  
 8.1 6.5 3.9  
 60 50 25

342.4 343.6 346.6  
 8.4 7.2 4.2  
 60 50 25

342.0 343.6 346.5  
 8.8 7.3 4.3  
 60 50 25

340.7 341.4 342.7 345.6  
 10.1 9.7 8.1 5.2  
 60 53 52 25

340.2 341.1 341.8 342.7 345.1  
 10.6 9.7 9.0 8.1 5.7  
 60 58 44.5 43 25

340.2 341.1 341.8 342.7 346.6  
 10.6 9.4 9.7 8.1 6.2  
 60 53 40 39 25

340.6 341.6 342.7 346.2  
 10.2 9.3 8.6 6.6  
 60 54 38 25

Chasterton P. Plant Site  
X-Sections

KING  
WEST  
WILLIAMS

7-19-51

Hotter "L"

81

350.83

0+90

3.6

347.2

339.5 341.8 344.7 343.6  
 $\frac{11.3}{60}$   $\frac{9.0}{48}$   $\frac{8.1}{31}$   $\frac{7.0}{25}$

1+00

3.7

347.1

338.6 340.6 344.0 342.7 344.0  
 $\frac{12.2}{60}$   $\frac{10.2}{50}$   $\frac{8.8}{42}$   $\frac{8.1}{32}$   $\frac{6.8}{25}$

1+10

3.8

347.0

338.1 340.9 344.0 342.9 344.3  
 $\frac{12.7}{60}$   $\frac{9.9}{47}$   $\frac{8.8}{43}$   $\frac{7.9}{33}$   $\frac{6.5}{25}$

1+20

4.0

346.8

337.3 339.9 342.6 342.9 344.7  
 $\frac{13.5}{60}$   $\frac{10.9}{49}$   $\frac{8.2}{44}$   $\frac{7.9}{33}$   $\frac{6.1}{25}$

CK B.M.

3.89

346.94

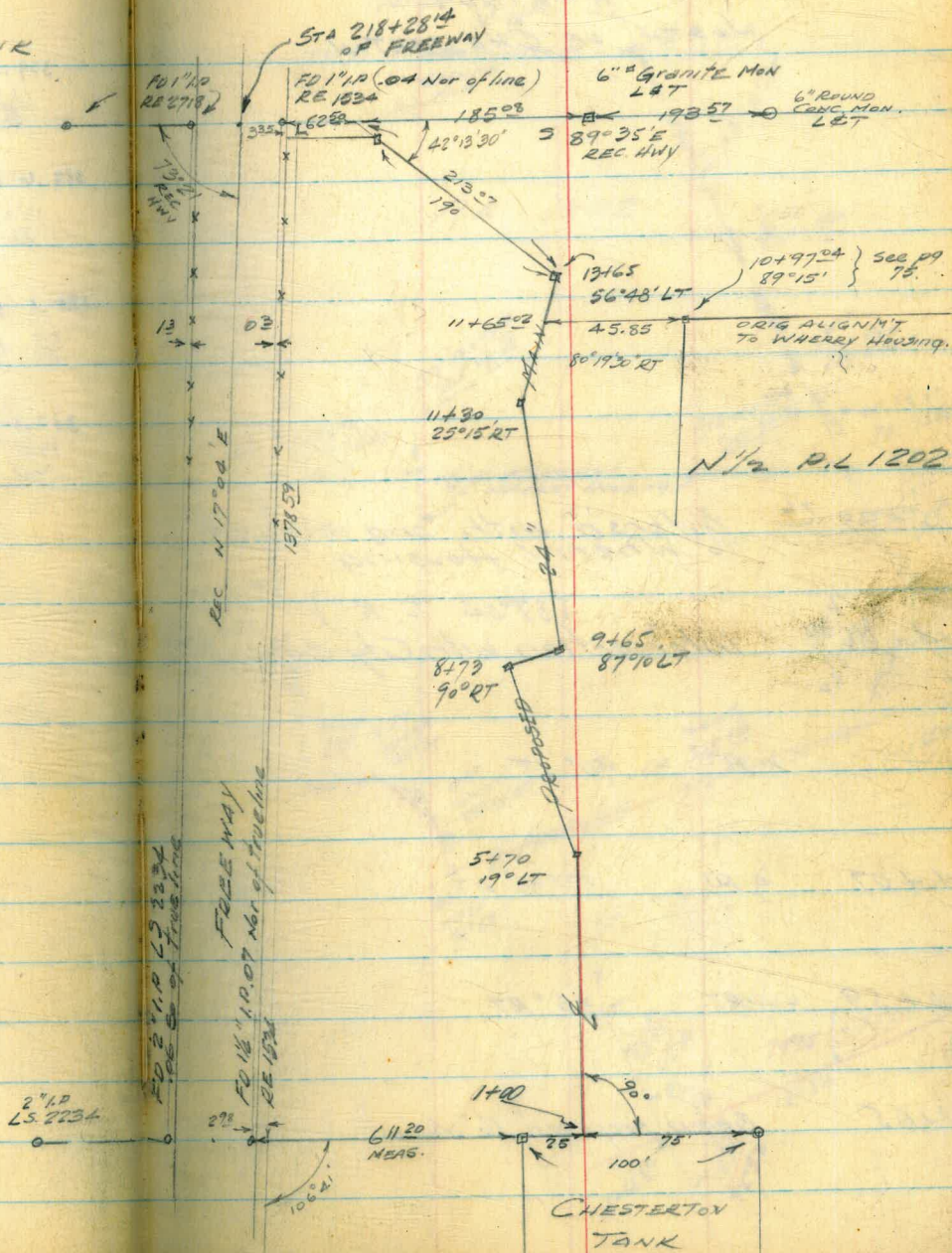
GRS 7/20/57

PROPOSED 24" MAIN  
IN P.L. 1202  
NORTH OF CHESTERTON TANK

JAN. 29 1952

BEATTY  
LEONARD  
POWELL

82.



PROPOSED 16" MAIN  
IN R.L. 1202  
NORTH OF CHESTERTON

15+99 <sup>2L</sup> Intersect with orig. alignment  
to Wherry Housing.

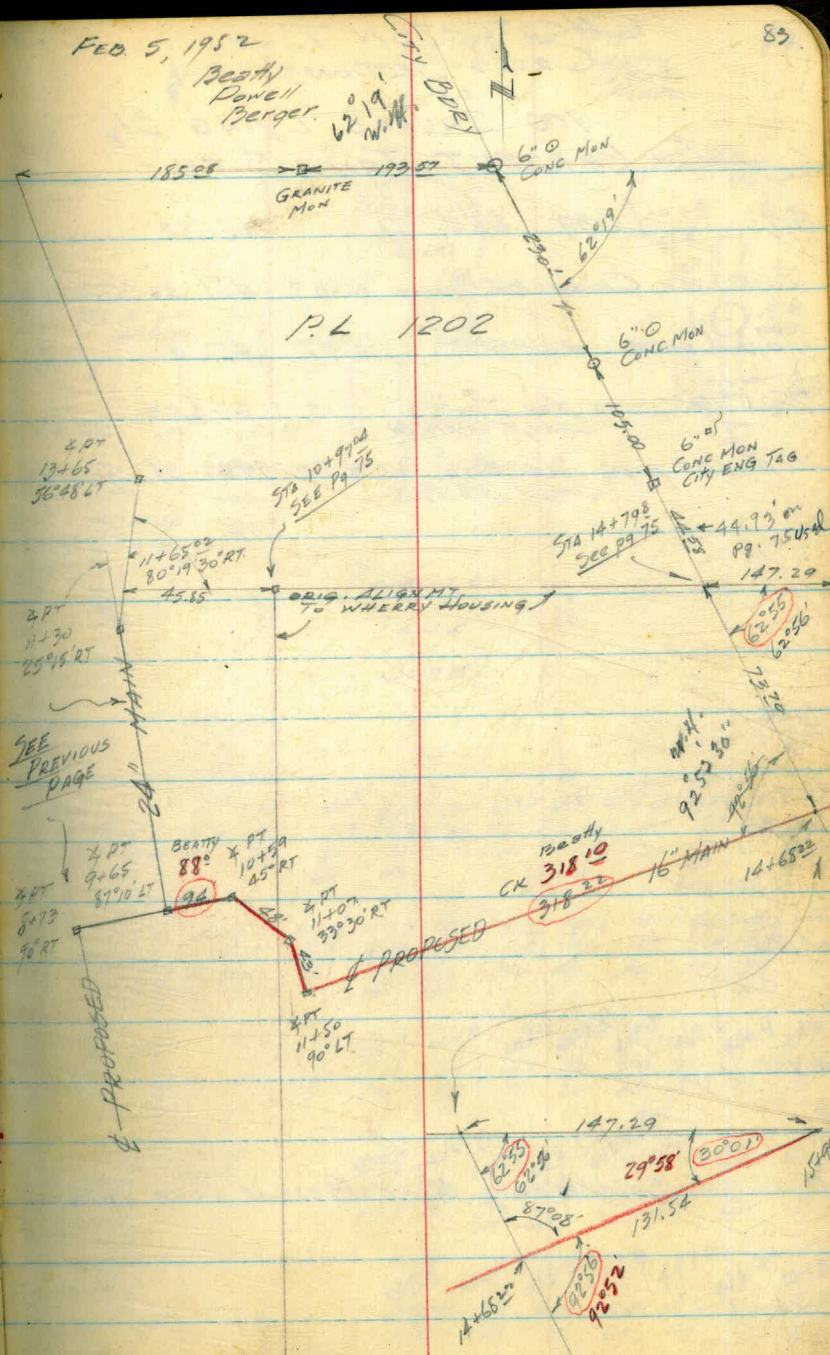
14+68 <sup>2Z</sup> Intersection with City Bdy  
(87°04' to RT)

11+50 <sup>4PT</sup> 90° LT

11+07 <sup>4PT</sup> 33°30' RT

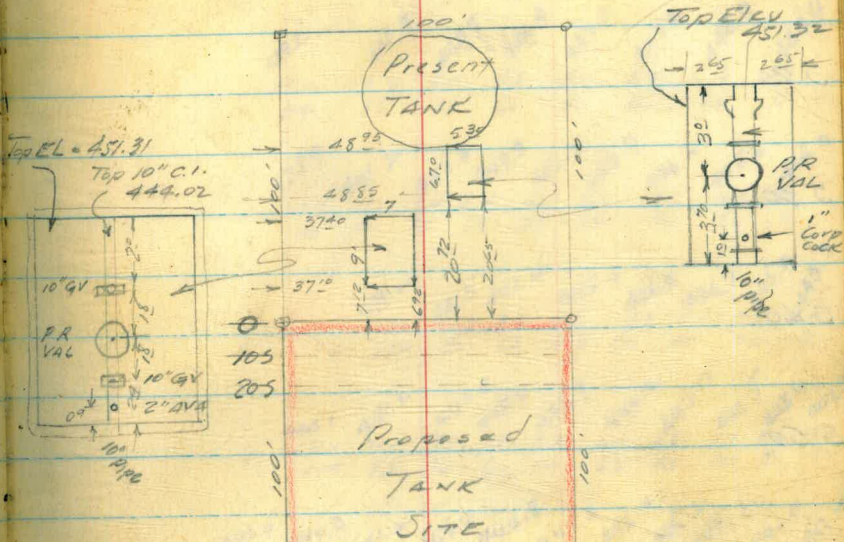
10+59 <sup>4PT</sup> 45° RT

9+65 Begin proposed 16" Main



CHESTERTON TANK  
 CROSS-SECTIONS  
 OF  
 100' SQUARE LYING 3/4  
 OF PRESENT TANK SITE

BM	0.39	452.21	451.82
Top Conc Chamber	0.89	451.32	
Top Conc Chamber	0.90	451.31	
Top 10" pipe Nor End - LARGE CHAMBER	8.19	442.02	
Top 10" pipe Nor End - Small Chamber	4.82	447.39	



EAST LINE	100.50																
	100.0	439.1	440.9	450.0	450.6	449.6	446.0	447.9	447.3	446.5	445.7	443.1					
	12.7	9.1	5.3	2.2	1.6	2.6	4.3	4.9	5.7	6.9	9.1						
	100	90	80	70	59	44	37	30	20	10	0						
			HP	HP				Cor. LEG									
								HP	(HARD PAN)								
	439.8	442.3	447.8	449.8	450.3	449.2	447.9	446.7	445.3	444.0							
	12.2	9.9	4.4	2.4	1.9	3.0	4.3	5.9	6.9	8.2							
	100	90	77	75	60	40	30	10	3.5	0							
			HP	HP													
	439.7	444.4	448.9	449.5	449.3	448.5	446.4	444.8									
	12.5	7.8	3.3	2.9	3.7	5.2	7.2										
	100	85	73	60	45	37.5	28	0									
	439.7	444.9	447.2	448.1	448.9	448.7	447.2	444.8									
	12.5	7.3	5.0	4.1	3.3	3.5	5.0	7.2									
	100	80	72	68	60	45	30	0									
			HP	HP													
	439.5	442.9	445.6	447.6	447.7	446.2	444.8										
	12.7	9.3	6.6	4.6	2.5	6.0	7.2										
	100	85	70	60	20	20	0										

N 30

N 20

N 10

0 = Southwesterly Line Present Tank Site

2 10

April 24 1952

DEATY  
 WEST  
 POWER



CHESTERTON TANK  
Cont'd

4-24-52

85

S 20 452.21

S 30

S 40

S 50

S 60

S 70

S 80

S 90

S 100 Southerly Line Proposed TANK SITE

OK BM

0.39 451.82

459.2 441.9 445.7 446.4 447.2 447.0 445.9 444.4  
13.0 10.3 8.5 5.8 5.0 5.2 6.3 7.8  
100 85 75 60 50 40 20 0

438.9 441.2 442.8 443.8 446.1 446.7 446.6 445.6 444.0  
13.3 11.0 9.4 8.4 6.1 5.5 5.0 6.6 8.2  
100 90 75 63 58 52 40 20 0

439.2 441.5 442.4 445.6 446.4 446.1 445.0 443.3  
13.0 10.7 9.8 6.6 5.8 6.1 7.2 8.9  
100 80 65 58 52 40 20 0

440.1 441.2 442.4 444.4 445.9 446.2 445.7 444.5 443.6 442.7  
12.1 11.0 9.8 7.8 6.3 6.0 6.5 7.7 8.6 9.5  
100 85 70 60 59 55 40 20 8 0

440.0 440.3 441.2 442.4 444.8 445.8 446.0 445.2 444.1 442.4 441.2  
12.2 11.9 11.0 9.8 7.4 6.2 6.2 7.0 8.1 9.8 11.0  
100 90 80 70 60 59 55 40 20 4 0

440.2 442.2 445.7 444.6 443.4 442.4 440.8  
12.2 10.2 6.5 7.6 8.8 9.8 11.4  
100 75 57 40 20 10 0

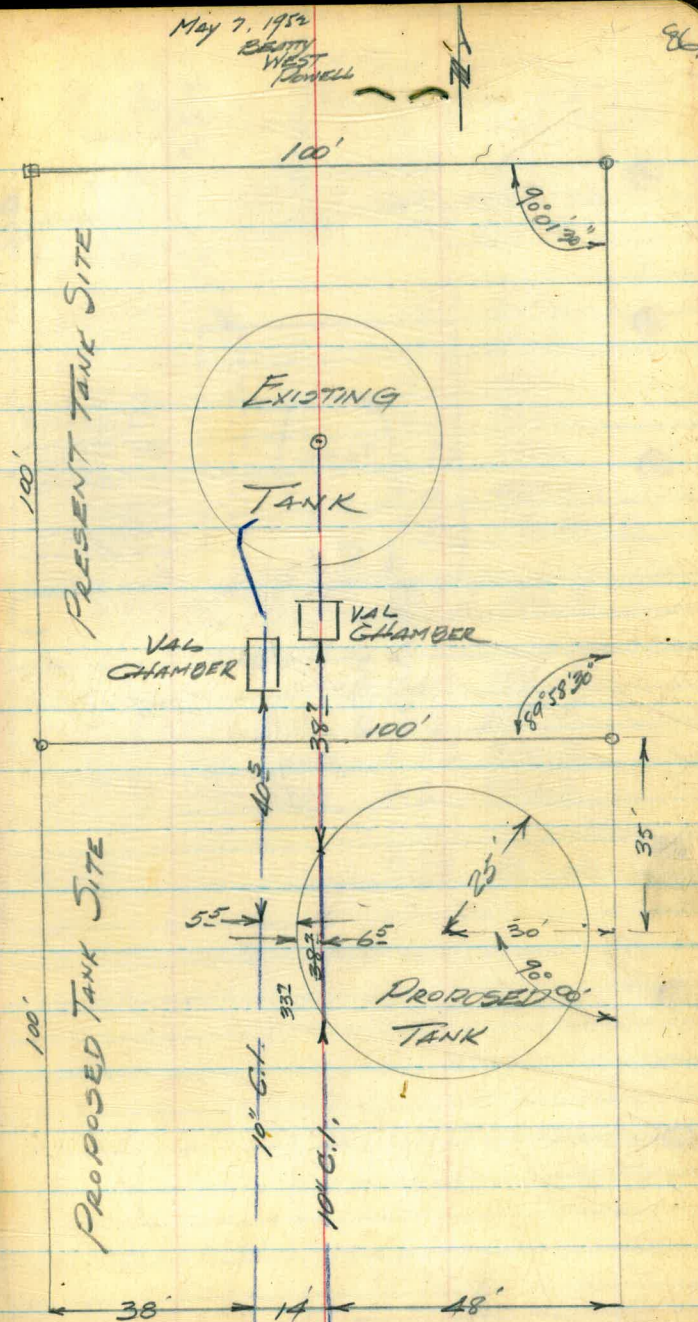
440.4 440.4 445.6 444.0 442.4 441.1 438.9  
11.8 11.8 6.6 8.8 9.8 11.1 13.3  
100 85 59 40 20 10 0

440.3 440.6 442.2 444.4 445.0 443.4 442.4 441.0 438.0  
11.9 11.6 10.0 7.8 7.2 8.8 9.8 11.2 14.2  
100 90 80 70 60 40 30 20 0

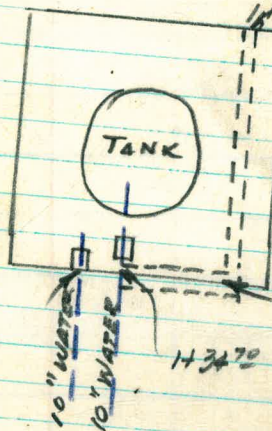
440.6 441.1 444.9 444.6 442.5 441.5 440.1 437.6  
11.6 11.1 7.3 7.6 9.7 10.7 12.1 14.6  
100 90 71 60 40 30 20 0

Pgs 84-85  
Checked & Reduced  
4/25/52 VLL

CHESTERTON  
 PROPOSED TANK LOCATION  
 SHOWING EXISTING 10" C.I.  
 PIPE LINES.



ON TANK FTG.



7-8-52  
BEATTY  
TUNNEY  
KEMP  
VANDERHART  
FISH.

TRENCH  
EXCAV  
24" C

NOTE -  
TRENCH  
BE FILLED  
6" SAND  
HOOD WITH  
HARDENED  
CONCRETE  
6" TO RAISE  
TO GRADE  
1+00

(accord.  
to flood  
formula)

# CHESTERTON TANK

## PROFILE OF TRENCH FOR 24" C.I.

### # TOP OF 10" C.I. 5' OF VOL. BOXES

B.M	+25	452.27	451.82
IP	9.84	448.86	13.25 439.02

0+00	14.3	434.6
+25	14.2	434.7
+50	12.75	436.1
+75	10.67	438.2
1+00	9.85	439.0
+10	9.0	439.5
+25	7.3	441.6

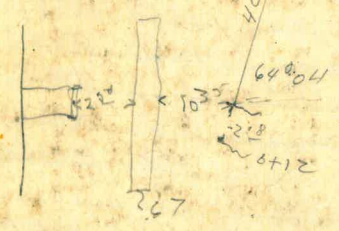
IP	6.48	452.61	2.73 446.13
----	------	--------	-------------

1+34.70 (Top pipe)	6.64	445.97
+36 (Nat Grd.)	3.9	448.7
+45.50 (Top pipe)	8.56	444.05
+45.50 (Nat Grd.)	4.3	448.3

CK BM	0.79	451.82
-------	------	--------

1777  
 42.23  
 218  
 46.05

351.18  
 632  
 357.50

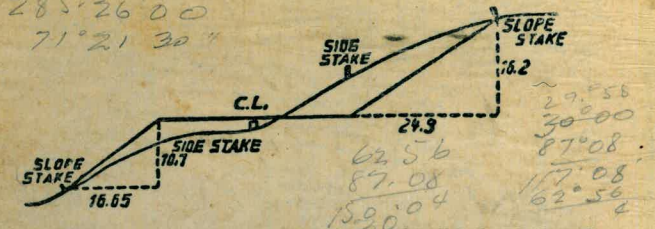


46.45  
 @ 16°40'  
 62°56'

346.9  
 4  
 347.3  
 4.2  
 343.1  
 338.7  
 4.4

100  
 334  
 1126

1) 71-21-30  
 285.2600  
 M 71°21'30"



29.55  
 30.00  
 87°08'  
 117.08  
 62.56  
 87.08  
 139.04  
 59.04

**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50