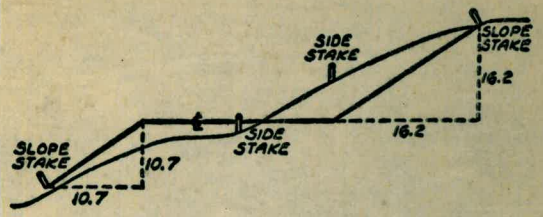

Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

729

727.81

480 NOR
2.44 SO
2.36

3.515 NOR
147.5
2.34

6.28 NOR
3.92
2.36

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1 83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.758	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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JULY 22 1949
BEATTY
ROGERS
WEST

4.75
4.05

& PROFILE & CROSS-SECTIONS

PROPOSED PIPELINE MIDWAY DR to PT LOMA

RESERVOIR

B.M	7.66	10.66		02.997	Be P.N Culvert Hdwl
			4.15	6.51	
			3.51	7.15	
			3.45	7.21	
			4.17	649	
			4.07	6.59	
			3.87	06.79	
0+00			3.67	6.99	
+50			3.28	7.38	
1+00			3.52	7.14	
	Rim of clean out	Storm Sew	5.36	05.30	
	Rim of Cleanout	" "	4.57	06.09	
+50			3.94	6.72	
2+00			4.28	6.38	
			5.15	5.51	
+50	Edge AC Pav.		~~5.05~~	~~5.61~~	
+59			4.8	5.86	
~~+56~~	~~Edge of Cut~~		~~5.11~~	~~5.55~~	
+63			4.7	6.0	
3+00	(on oil sidewalk)		4.82	5.84	
+50	" " "		4.62	6.04	
4+00	" " "		4.74	5.92	
+50	" " "		4.65	6.01	
5+00	" " "		4.76	5.90	
H +50	2.70	09.29	5.07	05.59	
6+00			3.83	5.46	

8-3-49

REDUCTIONS CHECKED BY E.E.

(1) Rim of M.H A.V. East & RT (-2.5 Top 24") Bott. 24" Pipe El. 2.01
(2) " " Val. West & RT (& Val. 4.10 lower) Bott. 24" Pipe El. 2.05
(3) " " A.V. West & RT. Air Val Box (full of dirt.)
(4) " " East & LT & Val. 3.75 lower) Bott. Pipe El. 2.07
(5) " " East & LT (& Val 4.35 lower) Bott Pipe El. 1.57
(6) " " San Sew 24" Trunk (Flow East) Inv.: 14.8 lower = El. -08.0

Invert Elev: -04.95 54" Conc. Pipe (w Cleanout 27.25 LT 1+49.00
" " -05.51 " " " " " " 91.00 RT 1+82.50

		09.29		
6+50			4.25	5.04
7+00	on Oil Sidewalk		4.71	4.58
+50			4.8	4.5
8+00			5.1	4.2
+50			5.4	3.9
9+00			5.7	3.6
+50			5.8	3.5
10+00	4.34	07.59	6.04	03.25
+50			4.5	3.1
11+00			4.4	3.2
+50			4.7	2.9
12+00			5.0	2.6
+50			5.1	2.5
13+00			5.1	2.5
+33.5	Inv. 12" RCP Side DR		8.88	(71) -1.29 5' RT Sta 13+33.5
+34.2	Top Curb		5.30	2.29
+34.2	Gutter		6.36	1.23
+50			5.88	1.71
+51.7	℄ St.		5.86	1.73
+69.2	Gutter		6.39	1.20
+69.2	Inv. 18" RCP DRAIN		9.98	-2.39 Intersect ⊄ & PIPE.
+69.2	Inv. 12" " Side Dr.		10.88	-3.29 5' RT Sta 13+69.2
+69.2	Inv. 18" Cross DR		10.90	-3.31 8' RT Sta 13+69.2

8.88
7.59
1.29

						L.	R.
		07.59					
13+69 2	Top of curb		5.36	2.23	✓		
+78 2	Begin Bus Oil Paint platform		5.40	2.19	✓		
14+00			5.21	2.38	✓	5.3 6.2 6.5 6.3 5.2 5.29	
SET TBM	5.33	07.66 ✓	5.26	02.33 ✓	SW Cor. West End Curb Chapman St.	23 16 13 10 7. 1.8 Return	
+08	End Bus Oil Paint platform		5.27	2.39	✓		
+50			5.3	2.4	✓	5.1 6.3 6.8 6.3 5.1	
						22 16 12 9 5.5	
15+00			5.1	2.6	✓	5.0 6.1 7.0 6.2 4.9 5.8	
						24 17 13 9 5 11 Edge of oil	
+50			5.0	2.7	✓	4.7 5.5 7.3 5.6 4.7	
						25 19 12 8 5	
16+00			4.9	2.8	✓	4.9 5.3 7.1 5.4 4.6	
						26 20 15 10 6	
+50			5.0	2.7	✓	4.9 5.7 7.3 4.6	
						26.7 21 15 5	
17+00			5.2	2.5	✓	4.9 6.0 7.4 6.5 5.1	
						27.2 22 15 12 5.5	
+50			4.4	3.3	✓	4.9 6.4 4.1	
						28 14 5.	

7/22/69

		07.66			
18+00			4.3	3.4	NE Cor Hdwll 15' ~~RT.~~ LT.
SET TBM	6.99	09.02 ✓	5.63	02.03 ✓	17+97
℄ 24" Conc. Cross Culvert 15' LT. Sta 18+05			9.70	−0.68	
+50			5.8	3.2	
19+00			5.2	3.8	
+50			5.1	3.9	
20+00			4.9	4.1	
+50			4.4	4.6	
21+00			4.1	4.9	
+50			3.8	5.2	
+77.8	Top Curb		3.35	5.67	
+77.8	Gutter		4.04	4.98	
22+00			3.93	5.09	

6.1 5.6 7.6 7.5 5.6 6.3 4.3 4.6
28.6 26 20 15 10 4.5 & 11 edge of 0.1
Top Hdwll

(Fall in Culv. 0.5%)

6.5 7.3 8.5 5.7
30 20 14.5 4.5 C

6.6 8.0 4.8
30.5 12.5 4 C

6.5 7.0 7.8 4.7
30 18 12.5 4 C

6.7 6.9 7.8 6.3 4.5 4.4
29.5 19 13 9.5 3.3 C 9.5 edge of 0.1

6.6 6.9 7.5 6.5 4.0
31 20.5 15 13 4 C

6.8 7.2 6.5 3.6 4.7
31 18 11 4.4 C 9.6 edge of 0.1

2.9
3.8 (6.1) 4.6
31 21.6 21.6 C
INV. Top Hdwll
12" Conc.
Cross Drain

		09.02			
22+11.80	Gutter		3.89	5.13	SW Cor. West Side Curb Ret Adrian St.
22+11.80	Top of Curb		3.30	5.72	
Set TBM	4.27	09.97 ✓	3.32	05.70 ✓	
+43	on oil Paint Bus Plat		4.12	~~5.85~~ O.K. EE.	
22+50			4.3	5.7	
23+00			4.9	5.1	
+50			4.8	5.2	
24+00			5.3	4.7	
+50			5.6	4.4	
25+00			5.2	04.8	
+50			5.8	04.2	Top. 2" pipe
TP	0.06	07.45 ✓	2.58	07.39 ✓	

4.7				4.4	5.1			
30		C		5	9	Edge Oil		
5.2	4.5			4.6	5.1			
30	17	C		6	9	"	"	
8.6	5.4			4.6	5.3			
31	24	C		7	9	"	"	
11.8	5.5	4.9	3.3					
28	13	5	4	C				
	11.3	5.2						
	19	6	C					
11.3	4.3	4.4						
17.5	7.5	4.5	C					
— 01.2	04.5	04.9						
11.2	5.5	5.1		3.2	3.7			
19	10	4	E	6.6	9.3	E O.	(Edge Oil)	

		07.45		
26+00	Rim of NH		3.6	03.9
	Bottom of 12" C.I.		3.12	4.33
			6.80	0.65
+50			3.8	3.7
+60			4.0	3.5
27+00			4.2	3.1
+50			4.7	2.8
28+00			5.1	2.4
+50			5.3	2.2
29+00			5.6	1.9
+50			5.5	2.0
30+00			5.5	2.0
℄ N&E N311	3.28	05.37	5.36	02.09

8.8 2.9
22 10.3 C

9.0 3.9
28 18 C

9.7 8.6 4.1
21 15.6 5 C

9.8 8.2 4.4
21 13 6 C

9.8 8.6 4.7 5.0
20 13 6 C 9. E.O (Edge 0.1)

10.4 9.1 5.0
20 12 6 C

10.6 9.2 4.9
19 12 5 C

10.3 9.4 5.3
20 12 6 C

9.4 9.0 5.3
20 11 6. C

10.1 9.1 5.6
21 12 5.3

05.37

30+50 — 3.3 — 2.1 ✓

31+00 (℄ PT.) — 3.4 — 2.0 ✓

NOTE. For Revised Profile See page 27 this Book.

~~+50~~ — 3.5 — 1.9

VOID

2.5 EE.

32+00 (℄ PT.) — 2.9 — ~~2.7~~

(Double) 4"-Conc DRAIN 14.5 RT. 32+00 — East 11.16 — −5.79 — West 11.06 — −5.69

Inlet Inv.

+20 — 3.1 — 2.3

+32 — 4.2 — 1.2

Outlet Inv. 4" Conc Drain (Double) West 12.18 — −6.81 — East 12.15 — −6.78

+60 40 (℄ PT.) — 4.0 — 1.4

INVERT Sewer MH (Orig Align) { 1° RT. 32+50 } — 8.20 (4.0 Rim) — 4.7 — 0.7

33+00

+50 — 4.1 — 1.3

VOID

34+00 — 3.5 — 1.9

+50 — 2.8 — 2.6

8.2 / 21 — 7.0 / 15 — 2.6 / 4 — C

8.3 / 23 — 6.5 / 11.5 — 3.5 / 5 — C — 4.2 / 10.6 E.O.

Edge Water — 9.9 / 16 — 8.9 / 11 — 4.8 / 5 — C

6.74 / 14.5 — 6.7 / 8.5 — Top Conc PIPE

7.2 / 39 — 3.3 / 18 — C — 2.8 / 8 — 4.3 / 13 E.O.

C — 3.8 / 4 — 2.2 / 11

C — 3.2 / 4 — +1.0 / 5

C — 2.7 / 5 — +2.0 / 8

		05.37		
35+00			1.3	4.1
℄ E NAIL	10.58	14.68 ✓	1.27	04.10 ✓
+50			8.8	5.9
36+00			6.6	8.1
Rim of M.H 36+08 (10' LT.)			6.97	7.71
+50			5.7	9.5
INV. 8" Sewer (From Rialto Street)			13.07	
INV. 12" TRUNK Sewer			16.47	
				10.8 E.E.
37+00			3.9	H.T.
+50			1.0	13.7
+65			0.0	14.7
+71			2.6	+2.1
38+00			2.9	11.8
+10 (℄ PT)			3.2	11.5
(℄ NAIL)	5.37	16.88 ✓	3.17	11.51 ✓
+50			6.9	10.0

Lt.	Rt.
	1.1 / 7 +3.0 / 10
	8.4 / 7.5 4.7 / 11 7.2 / 17 (Street cut Begins 35+77 Ends 36+29)
	5.0 / 3 1.8 / 6
4.0 / 10 4.2 / 1	0.7 / 4 0.6 / 10
3.2 / 4	+0.2 / 1.5 +0.5 / 10
3.0 / 12 3.0 / 5 2.4 / 3	+0.5 / 2 +0.5 / 10
2.7 / 13	1.6 / 10
2.7 / 10	2.4 / 3 1.3 / 9
(RT & To Rx Temp.) 2.5 / 10	3.4 / 10 +0.6 / 16

			16.88		
35	39+00			8.7	8.2
	+50			8.5	8.4
		Rim of MH	27' RT 39+45	8.50	8.38
		Invert		15.3	1.58
	40+00			7.3	9.6
		Rim of MH	92± LT 39+62	11.7	5.18
		Invert		17.1	- 0.22
	+50			4.7	12.2
	TP Rock	12.38	28.99	0.27	16.61
	41+00			11.5	17.5
	+50			6.0	23.0
	42+00			1.7	27.3
	TP (Rock)	12.00	40.91	0.08	28.91
	+50			8.6	32.3
	+90	Rim Sewer MH		3.51	37.40
		Invert		16.80	24.11
	43+00			3.5	37.4
	TP	12.23	52.90	0.20	40.67
	+50			10.7	42.2
	44+00			6.2	46.7
3	+50			2.9	50.0
	SET TBM	12.45	63.64	1.71	51.19
	45+00			10.7	52.9
	+50			7.7	55.9
	46+00			4.6	59.0
	+44±	Rim Sew. MH	222° LT	+ 0.01	63.65
		INV. EL.		6.89	56.75
		Rim Sew. MH	179± RT	16.84	46.80
		INV. EL.		28.44	~~38.20~~ 35.20 EE

Nail in Pole 20' LT 44+60

3.91
26.00

6.91
30.00

		63.64		
46+50			2.0	61.6
IP	11.92	74.82	0.74	62.90
				1.42
47+00			10.6	64.2
				66.7 EE.
+50			8.1	68.7
+71.48	℄ PT.		7.1	67.7
48+00			6.0	68.8
+50			4.4	70.4
49+00			3.3	71.5
+15			3.1	71.7
+20			2.4	72.4
+50			1.0	73.8
+63			0.6	74.2
+65			+1.0	75.8
+67			+1.0	75.8
IP (ROCK)	4.22	72.19	6.85	67.97
				4.22
+83			4.7	67.5
50+00			5.4	66.8
+50			5.7	66.5
51+00			7.0	65.2

× ON NE COR of WALK 19' RT STA 46+65

		72.19		
51+50			6.6	65.6
52+00			5.3	66.9
+23			4.2	68.0
+50			7.4	64.8
53+00			11.0	61.2
+35			12.0	60.2
				56.9 EE.
+42			15.3	~~57.9~~
P	3.62	63.06	12.75	59.44
+50			5.0	58.1
+55			5.0	58.1
+65			8.0	55.1
P	0.69	52.67	11.08	51.98
54+00			9.8	42.9
P	0.11	40.43	12.35	40.32
+50			6.6	33.8
P	0.98	28.67	12.74	27.69
55+00			3.2	35.5

62.3 61.2 60.8 50.1 50.9
9.9 11.4 21.1 21.3
15 C 8 22 30

60.9 60.2 60.1 44.2 44.2
11.3 12.1 28.0 28.0
8 8 2 28 35

60.4 56.9 44.2
11.8 28.0
12 C 23

60.0 59.5 58.1 44.0
3.0 3.5 19.0
12 3 C 23

60.2 59.4 43.7
2.8 3.4 19.3
27 6 C 24

60.5 59.6 40.0
2.5 3.4 23.0
15 9 C 23

52.4 37.2 36.5
+6.0 0.3 15.5 16.2
28 14 C 16 25

0.0 4.0 10.2
30 13 C 30

		28.67		
55+11			4.7	24.0 ✓
+22			7.2	21.5 ✓
+50			9.9	18.8 ✓
+80			13.1	15.6 ✓
56+00			13.2	15.5 EE. ✓ ~~15.7~~
TP	1.21	17.71 ✓	12.17	16.50 ✓
+30			4.4	13.3 ✓
+42			4.4	13.3 ✓
+45			3.9	13.8 ✓
+50			5.2	12.5 ✓
57+00			7.4	10.3 ✓
+50			9.1	8.6 ✓
+75			9.4	8.3 ✓
+84			9.5	8.2 ✓
58+00			8.5	9.2 ✓
+08			8.4	9.3 ✓
+12			6.3	11.4 ✓
TP	11.97	29.26 ✓	0.42	17.29 ✓ 11.97
+50			11.1	18.2 ✓

3.3 / 26 — 4.3 / 13 — ℄ — 9.0 / 25

4.3 / 26 — ℄ — 17.6 / 33

		29.26		
58+85			6.6	22.7
59+00			5.3	24.0
+10			4.2	25.1
+20			4.4	24.9
+50			4.6	24.7
+70			7.7	21.6
60+00			8.1	21.2
+13			8.0	21.3
+42			5.9	23.4
+50			4.3	25.0
+59			3.5	25.8
+75			00	29.3
II Rock	12.50	41.76	0.00	29.26
61+00			8.6	33.2
+10 54	(2 PT)		7.4	34.4
+50			2.3	39.5
II Rock	13.04	54.64	0.16	41.60
62+00			9.0	45.6
+13			7.4	47.2

+20 26 1.6 13 c 15.1 39

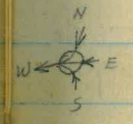
+1.2 26 c 11.3 30

+1.0 26 c 9.8 13 9.7 26

8.7 12 c 8.5 3 9.3 5 8.3 9 8.2 20

		54.64		
62+15			8.0	46.6
+50			6.4	48.2
+66			6.1	48.5
+67			5.5	49.1
63+00			3.6	51.0
SET TBM			4.68	49.96
+50			0.1	54.5
℄ NAIL		5.05 59.60	0.09	54.55
64+00			2.2	57.4
+50			1.7	57.9
65+00			3.2	56.4
+50			7.0	52.6
66+00			11.4	48.2
+34	Top CURB		12.44	47.16
+35	GUTTER		13.17	46.43
+50			13.58	46.02
+55±	RIM OF M.H. (SEW) 20.5 RT		15.1	44.50
	INV. EL		20.2	39.40
+75	GUTTER		13.80	45.80
+77	Top CURB		12.54	47.06
67+00			12.1	47.5

NAIL IN POLE 25 RT 62+20±



11.6 12.3 12.3 13.7
10 ℄ 4.5 5.1 7.4
Conc Curb

		59.60			
67+50			9.8	49.8	✓
68+00			6.2	53.4	✓
II		11.66	67.38 ✓	3.88	55.72 ✓
+50				9.4	58.0 ✓
+87 63	Begin Side			6.18	61.20 ✓
+90 13	& PT			6.10	61.28 ✓
+92 33	Top Curb			6.05	61.33 ✓
+92 33	Gutter			6.65	60.73 ✓
Rim of M.H.				6.75	60.63 ✓ E.E.
INV. E 20' RT	68+94 5			18.05	+9.33
69+00				6.27	61.11 ✓
+21	& Voltaire			5.58	61.80 ✓
Rim of M.H.	7 LT	69+32 3		5.52	61.86 ✓
Top 10 WATER PIPE				10.50	56.88 ✓
+50				5.72	61.66 ✓
+60 24	& PT			5.67	61.71 ✓
70+00				4.48	62.90 ✓
SET TBM				2.89	64.49 ✓ Top F.H.
+50				2.78	64.60 ✓
71+00				1.03	66.35 ✓
II		10.55	77.31 ✓	0.62	66.76 ✓

9.0 / 10	C	10.0 / 4.5	10.0 / 5.1 — 11.4 / 7.4 (Conc Curb)
5.6 / 13	C	6.4 / 5	7.4 / 6 (Conc Curb)
9.1 / 13	C	9.5 / 5	10.3 / 5
	C	6.37 / 4.0	7.00 / 4.0 (Curb)
	C	6.22 / 2.3	6.76 / 2.5 (Curb)

7-26-68
8/10/48
Beatty
Rogers
Finney

℄ Profile Midway Drive - Pt Loma Pl.

		77.31			
71+50			9.11	68.20	
72+00			7.37	69.94	
+50			5.54	71.77	
73+00			3.77	73.54	
CK BM			2.54	74.77	BR. IN SE. COR UDALL ST
+50			1.68	75.63	
11		11.92 89.15	0.08	77.23	
74+00			11.32	77.83	
+32.5	Rim of M.H. 16' RT. Invert El.		10.06	79.09	
+42.83	B.C		13.36	75.79	
			9.35	79.80	
+50			9.06	80.09	
75+00			6.83	82.32	
+78.0	Rim TELE MH 15' LT Top of Duct.		2.08	87.07	
+50			14.25	74.90	
+96	Rim of Sew MH 19' RT Invert. El.		4.74	84.41	
76+00			5.34	83.81	
			10.14	79.01	
			2.48	86.67	
12		12.62 101.23	0.50	88.61	
+50			12.44	88.79	
CK BM			11.34	89.89	BR. SE COR TENNYSON
77+00			10.16	91.07	
+50			7.95	93.28	
78+00			5.76	95.47	
+15.09	P.R.C.		5.08	96.15	
+50			3.50	97.73	
+78.3	Rim of MH. 13' RT Inv.		6.76	94.47	
	Rim of MH 23' LT. Inv.		12.96	88.27	
			+13.50	114.73	
			+ 7.70	108.53	

REDUCTION SURVEY CHECKED BY E.E. 8-3-49

Rim of M.H. 82' LT. Invert El.	74+32.5	+4.50 14.3	93.65 74.85	
		19.3 5.8 13.5		

℄ PROFILE Midway Drive - Pt Loma P.L

		101.23		
79+00			1.36	99.87
P		11.64	112.74	0.13 / 1.64	101.10 — Cor Side Walk 79+10 12' East
+50				10.56	102.18
+83⅜	NOR Rim MH			9.83	102.91
	Invert			15.93	96.81
80+00				8.37	104.37
CK B.M				6.00	106.74 = 107.01 — Be. R.n SE Cor Alicia Dr
+50				6.50	106.24
81+00				4.75	107.99
+50				2.97	109.77
+62⅝	Rim Sewer M.H 14' RT			3.07	109.67
	Invert			9.10	103.64
82+00				1.23	111.51
P		10.57	122.55	0.76	111.98
+50				9.54	113.01
83+00				8.07	114.48
	+37 ± NOR Rim M.H			7.73	114.82
+50				7.15	115.40
84+00				6.27	116.28
CK BM				5.68	116.87 = 116.85 — SE Cor Atascadero Dr
+50				5.00	117.15
85+00				4.42	118.13
+08⅝	INSERT NOR Rim MH			4.55	118.00
	INVERT Sewer			11.60	110.95
	322± LT Rim MH			+25.10	147.65
	INVERT			+15.10	137.65

79 +83⅜
1½ below Sta 6± down Invert

℄ PROFILE Midway Dr - Pt Loma P.L.

	122.55		
85+50		3.66	118.89
86+00		2.72	119.83
+50		1.88	120.67
87+00		0.87	121.68
86+97	14° RT Nor Rim M.H.	1.10	121.45
	Invert Sewer	8.60	113.95
	84± LT Rim M.H.	+1.30	123.85
	Invert of Sewer	7.30	115.25
P	11.02 133.27	0.30	122.25
+50		10.74	122.53
88+00		9.62	123.65
			BRP. SE Cor
CK BM		8.69	124.58 = 128.63
+54.72	(B.C)	8.63	124.64
89+00		7.51	125.76
+22	13° RT Sew MH Rim	7.20	126.07
	Invert	16.50	116.77
+50		6.08	127.19
90+00		4.72	128.55
+50		3.30	129.97
+80.19	(E.C)	2.42	130.85
91+00		1.92	131.35
+14	16° RT Nor Rim M.H	1.79	131.48
	Invert Sewer	9.20	124.07
D ↘ ℄ Nail			
+50	12.73 145.51	0.49	132.78
92+00		10.97	134.54
+49°	16° RT Rim Sew MH	9.23	136.28
	Invert Sewer	16.20	129.31

℄ PROFILE MIDWAY DRIVE – Ft. Loma P.L.

		145.51			
89	92+50			9.03	136.48 ✓
8	93+00			7.08	138.43 ✓
	+50			5.18	140.33 ✓
8	94+00			3.20	142.27 ✓
	+50			1.36	144.15 ✓
					B.P. Nu. Cor. NIAGARA
	CK B.M.			2.15	143.36 ✓ 143.42
	+64.5	16° RT Nor Rim M.H.		1.02	144.49
		Invert Sewer		6.72	138.79
8		11.06	156.06 ✓	0.51	145.00 ✓
c	95+00			10.46	145.60 ✓
	+50			9.07	146.89 ✓
8	96+00			7.65	148.41 ✓
	+50			6.19	149.87 ✓
	+56	16° RT. Sewer M.H. Rim		6.30	149.76
		Invert		11.70	144.36
9	97+00			4.89	151.17 ✓
	+50			3.38	152.68 ✓
	98+00			2.15	153.91 ✓
	+48	SEWER M.H. 17° LT. Rim		+15.6	171.66
		Invert		+8.3	164.36
	+50			1.31	154.75 ✓
	+48	SEW. M.H. 16° Nor Rim M.H.		6.41	154.65
	99+00	RT Invert		0.48	155.58 ✓
		8.08	163.56 ✓	0.58	155.48 ✓
	CK BM			6.02	157.54 ✓ =
					B.R.P. NE Cor. NARRAGANSETT

15 7.54 15 7.50

5 c

℄ PROFILE – MIDWAY DRIVE – Pt LOMA PL.

163.56

99+50			7.49	156.07
100+00			7.02	156.54
+40	SEW. MH. 16° RT.	Rim	6.70	156.86
		Invert	12.40	149.16
+50			6.46	157.10
101+00			5.89	157.67
+50			5.39	158.17
102+00			4.88	158.68
+05	SEW MH. 16° RT.	Rim	5.20	158.36
		Invert	12.50	151.06
+50			4.30	159.26
103+00			3.63	159.93
+50			3.45	160.11
104+00			2.57	160.99
+325	SEW. M.H	16° RT Rim	2.40	161.16
		Invert	9.70	153.86
+50	9.11	170.57	2.10	161.46
105+00			8.56	162.01
+50			8.07	162.54
106+00			7.44	163.13
+22	16° RT.	Sewer M H Rim	7.51	163.06
		Invert	13.10	157.47
+22	266 LT	Rim Sewer MH.	+10.8	181.37
		Invert	+4.8	175.37
+50			7.00	163.57
107+00			6.42	164.15
+50			5.89	164.68
108+00			5.11	165.46

℄ PROFILE MIDWAY DRIVE – PT LOMA PL

		170.57		
108+50		4.19	166.38	✓
109+00		2.77	167.80	✓
		1.41	169.16	✓
+50		~~1.41~~	~~156.5~~	X
TP				
110+00	12.39	182.55 ✓	10.41	170.16 ✓
+02.5	15± RT	RIM SEW. M.H	9.70	169.87 ✓
		INVERT	5.10	165.47 ✓
+50			11.44	171.11 ✓
+02.5	14± LT	RIM. SEW. M.H	+7.80	178.37
		INVERT	2.80	167.77 ✓
111+00			9.97	172.58 ✓
+50			8.33	174.22 ✓
+92.8	15 RT	RIM SEWER M.H	7.12	175.43
		INVERT	12.50	170.05 ✓
112+00			6.52	176.03 ✓
+50			3.92	178.63 ✓
113+00			1.29	181.26 ✓
TP	12.51	194.93 ✓	0.13	182.42 ✓
+82.5	22.9± LT	RIM MH	7.60	187.33
		INVERT	13.20	181.73 ✓
+50			11.89	183.04 ✓
+82.5	15± RT	RIM M.H. SEWER	11.01	183.92
			17.31	177.62 ✓
114+00			10.41	184.52 ✓
CK BM			7.37	187.56 ✓ ✓
				BR P.N. SW. COR Del Mar = 187.53
+50			8.58	186.35 ✓
115+00			6.56	188.37 ✓
+50			4.47	190.46 ✓
+73.5	15± RT	RIM of SEWER MH	3.87	191.06
		INVERT	10.87	184.06 ✓
116+00			2.95	191.98 ✓
+50			2.01	192.92 ✓

℄ PROFILE MIDWAY DRIVE – PT. LOMA P.L

194.93

116+87.90	B.C.		1.36	193.57
117+00			1.13	193.80
P	7.98	202.82	0.09	194.84
+50			7.88	194.94
+59.7	18° RT	Nor Dim M.H. Sewer	7.52	195.30
+59.7	25.64 LT	Invert	17.0	185.82
		Rim	7.30	195.52
		Invert	14.8	188.02
CK BM			6.29	196.53 = 196.50
				BP. SW Cor Orchard
118+00			7.14	195.68
+13.68	(E C)		7.01	195.81
+50			6.77	196.05
119+00			6.33	196.49
+50			5.89	196.93
+55	16° RT. Rim	SEWER MH	6.0	196.82
		Invert	12.0	190.82
120+00			5.37	197.45
+50			4.96	197.86
121+00			4.48	198.34
+50			4.00	198.82
+94	RT. Rim	SEWER MH	3.70	199.12
		Invert	9.60	193.22
122+00			3.52	199.30
P on curb	6.35	206.60	2.57	200.25
+50			6.85	199.75
123+00			6.32	200.28

℄ Profile Midway Drive - Pt Loma Pl.

206.60.

8	123+50		5.93	200.67
	+88.5 16°RT Rim Sewer MH.		5.50	201.10
		Invert	11.50	195.10
8	124+00		5.43	201.07 201.17 EE
	+34.3 16°RT Rim Sewer MH		4.88	201.72
		Invert	10.88	195.72
	+50		4.66	201.94
	+79.5 12½ LT Rim of AVA } FULL of		4.22	202.38
	TOP Pipe } WATER		8.22	198.38
	125+00		3.92	202.68
	+50		2.92	203.68
	~~+26+00~~ DELETED		~~2.31~~	~~204.29~~
	CK BM		4.98	201.62 BR R NE Cor CHATSWORTH 201.61
	P		2.32	204.28
	BM	5.40 207.02		201.62
	125+55.72 ℄ PT		3.23	203.79
	+78± Edge AC Pavt.		4.03	202.99
	126+00		3.5	203.5
	+50		5.8	201.2
	+80		9.1	197.9
	127+00		10.2	196.8
	+25		10.9	196.1
	P & Nail 127+50	0.21 194.26	12.97	194.05 193.7 EE
	+52.70 ℄ PT.		0.6	(194.20)
	+75		2.4	191.9

Rim 03 lower
4.3 low top pipe

August 23 1949

8/23/49

℄ Profile Midway Drive Pt. Loma P.L.

194.26

128+00		6.4	187.9
+33		11.2	183.0
+75.07 B.C.		13.5	180.7
129+00		14.4	179.8
Top of Nut 8" GV. B.O.	129+06.2 2.5 RT.	17.85	176.41
Bottom of B.O. Pipe		19.5	174.7
+25		14.4	179.8
+50		12.9	181.3
+75		11.0	183.2
130+00		8.1	186.1
+50		3.8	190.4
131+00		0.0	194.2
P.	9.61 203.70	0.17	194.09
+50		6.9	196.8
132+00		5.5	198.2
+34.80 E.C.		4.5	199.2
Top 18" Conc. Pipe (5' RT. E.C.)		8.85	194.85
SET TBM (RP Hub 45' LT.)		6.21	197.49
+50		3.8	199.9
133+00		2.7	201.0

10.3
3.9
3.65
17.85

14.2
5.3

4.35
3.5
8.85

8/23/49

℄ PROFILE MIDWAY DRIVE – Pt LOMA P.L.

		203.70	
133+50		1.8	201.9
134+00		1.0	202.7
P	8.61	212.31	0.00	203.70
+50			8.2	204.1
135+00			7.3	205.0
+50			6.5	205.8
136+00			5.9	206.4
+50			4.7	207.6
137+00			5.3	207.0
+50			3.2	209.1
P	7.27	219.51	0.07	212.24
138+00			7.2	212.3
+10			6.5	213.0
+50			7.1	212.4
139+00			6.6	212.9
+50			7.0	212.5
140+00			7.1	212.4
+25			7.6	211.9
+50			6.5	213.0

8.8 18 | 8.6 12 | 5.6 5 | ℄ | 5.1 7 | 5.0 9 | 5.4 11 | 5.0 17 | 4.0 24

3.5 6 | 4.2 1 | ℄ | 2.8 5

℄ PROFILE MIDWAY DRIVE POINTLOMA R.C.

	219.51		
141+00		4.0	215.5 ✓
+50		2.6	216.9 ✓
142+00		2.4	217.1 ✓
+50		1.0	218.5 ✓
P	11.13	230.09 ✓	0.55 218.96 ✓
+72.60			11.30 218.79 ✓
Top 18" Conc. Pipe 5' RT.			15.50 214.59 ✓
143+00			11.0 219.1 ✓
+50			10.5 219.6 ✓
+72.17 ℄ PT.			9.65 220.44 ✓
+90			9.0 221.1 ✓
144+00			7.3 222.8 ✓
+05.2 Top 16" C.I. Pipe.			8.64 221.45 ✓
+24			2.6 227.5 ✓
+26			3.4 226.7 ✓
+27			2.2 227.9 ✓
+31.42 ℄ PT.			1.9 228.2 ✓
P (Top PL Hub)	12.30	241.35 ✓	1.04 229.05 ✓
144+47.50 END OF PROPOSED R.C. AT ℄ 16" C.I. Pipeline			10.4 230.9 ✓ Ground
Top 16" C.I. 8' RT			14.46 226.89
Top 16" C.I. 7.3' LT.			13.61 227.74

9.06
5.80

10.37
3.29

8/23/49

℄ PROFILE MIDWAY DRIVE PT LOMA RL

241.35

SET TBM	NE Cor Valve Chbr	Right	9.05	232.30 ✓
℄		11.50 25277 ✓	0.08	241.27 ✓
CK BM. Br. P. S.W Cor Varona & Catalina.			1.98	250.79 ✓ = 250.82

Revised Profile (see page 7.)
Continued from page 7

℄	3.63 05.72		02.09
31+50		2.8	2.9 ✓
+68		4.0	1.7 ✓
+74		5.3	0.4 ✓
+79		4.5	1.2 ✓
32+00		3.6	2.1 ✓
+04		3.3	2.4 ✓
+20		3.5	2.2 ✓
+30		4.6	1.1 ✓

CONTINUED ON PAGE 28

+50		4.4	01.3
32+60.98 BK & PT ~~32+64.90~~ AH		4.5	
33+00		5.1	09.6 = 00.7

V.O.I.D

Sept. 8 1949

Midway Dr — Pt Loma Pt

Profile & X-Sections — Revised Alignment

Continued from page 27.

#	4.28	06.37	02.09	LEFT	Right
32+35 68	℄ pt.	5.2	1.2	WE = Waters edge	
+40		5.3	1.1	10.0 6.8 4.0 4.3 C 5.0 4' 33 20 9 20 WE	
+50		5.6	0.8		
+54		5.6	0.8	10.0 4.9 5.1 4.0 5.2 C 5.2 30 22 15 10 5 20 WE	
SET TBM		7.74	-01.37		
33+00		5.6	0.8	10.0 6.9 5.9 3.4 6.1 5.5 33 17 9 4 C 4 20 WE	
+15		4.8	1.6		
+18		5.8	-0.6		
+22		6.4	0.0		
+26		6.1	0.3		
+33		4.5	1.9		
+40		3.9	2.5		
+45		4.9	1.5		
+50		4.3	2.1	9.4 9.3 8.0 6.1 3.7 5.5 5.0 30 22 18 11 3 C 5 20	
+53		3.4	3.0		
+63		3.7	2.7		
+71		5.4	1.0		
34+00		3.8	2.6	9.4 9.4 1.9 4.7 5.0 4.3 30 18 5 C 1 5 20	

8/8/49

Midway Drive — Pt. Long P.C.

Profile & X-Sections — Revised Alignment

06.37

					LEFT					RIGHT		
34 +13			4.5	1.9 ✓								
+21			3.0	3.4 ✓								
+50			3.0	3.4 ✓								
					9.6 / 30	9.4 / 15	2.3 / 4	C	3.9 / 6	3.3 / 20		
35+00			1.3	5.1 ✓								
					9.5 / 30	9.3 / 15	1.3 / 5	C	0.8 / 1	2.3 / 8	1.6 / 20	
PT (Rock)	7.73	13.44	0.66	05.71								
+50			6.4	7.0 ✓								
					16.1 / 30	15.8 / 18	5.4 / 4.5	C	6.8 / 6	7.8 / 7	6.8 / 20	
36+00			5.0	8.4 ✓								
					16.1 / 30	15.7 / 18	4.5 / 2.4	C	5.5 / 1		4.8 / 20	
+50			3.8	9.6 ✓								
					16.5 / 40	12.2 / 23	2.7 / 4		3.8 / 1.5	C	3.5 / 20	
37+00			2.2	11.2 ✓								
					11.8 / 44	7.3 / 23	2.5 / 13	1.6 / 7	2.3 / 4	C	2.7 / 20	
+50			1.0	12.4 ✓								
~~37+53 45 ~~ ~~37+70 21 ~~	4.55	17.06	0.93	12.51 ✓	10.2 / 43	5.8 / 30	+10 / 18		0.2 / 8	1.0 / 5	C	1.4 / 20
38 +00			5.0	12.06								
+14.10	RIM SEW. M.H. 4' LT 38+03 INV. 12" Sewer		5.00	12.10								
			18.60	−01.50								
CK			5.6	11.5 ✓								
			5.56	11.50 ✓ = 11.51								

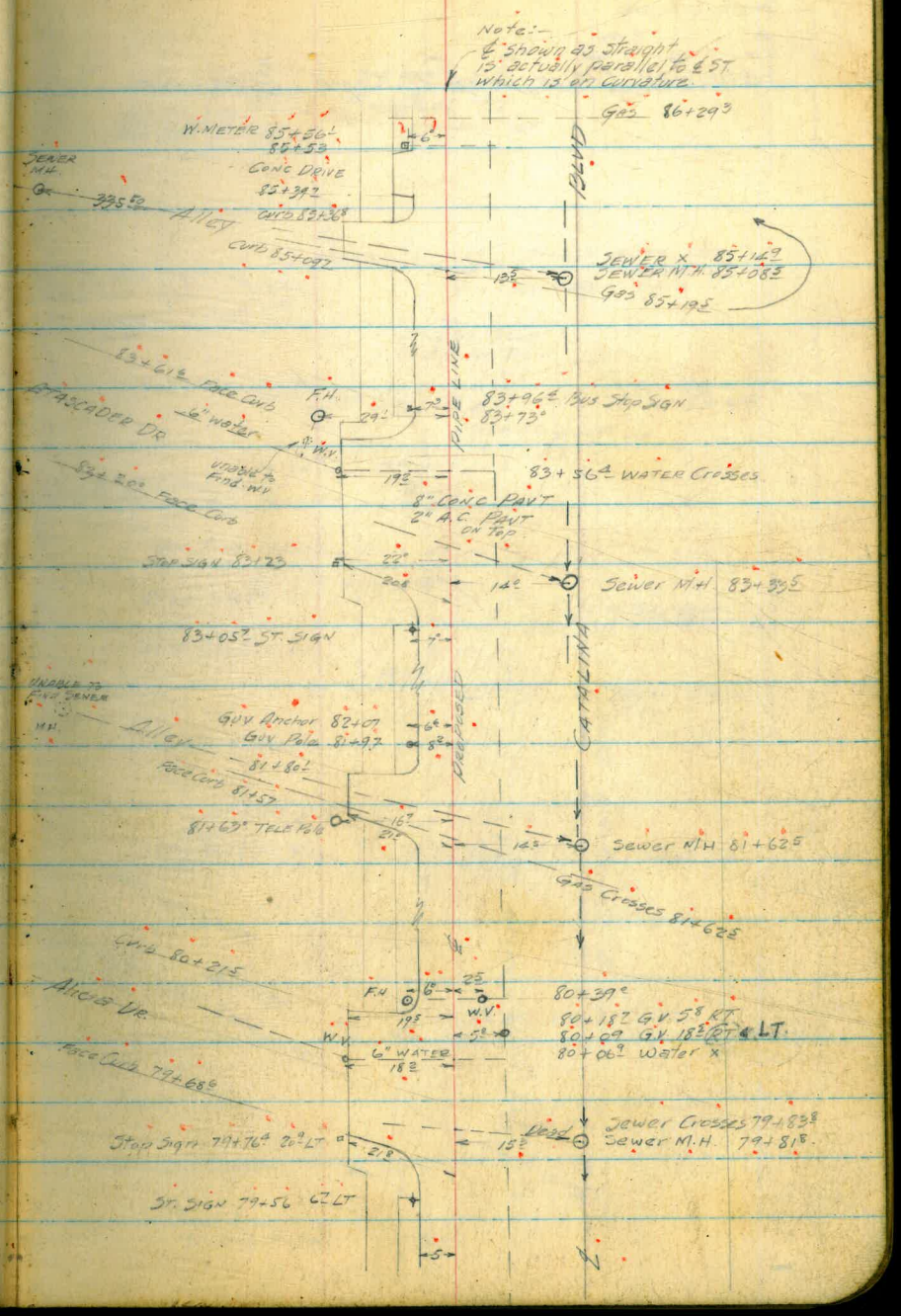
Continued on page 8

pg. 8

SEPT. 20 1949
BRATTY
ROGERS
FINNEY

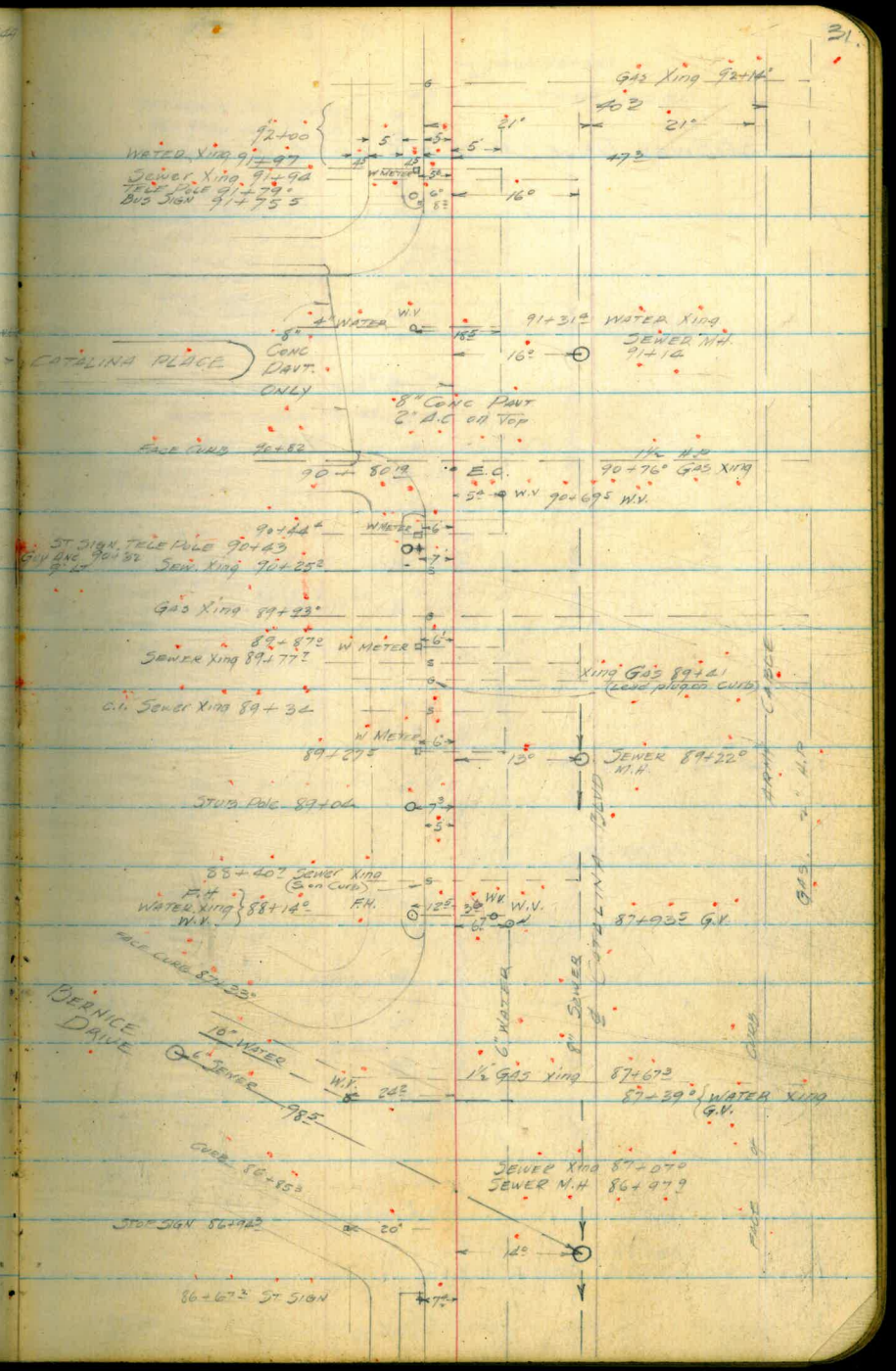
MIDWAY DRIVE → PT. LOMA PIPELINE

(CONTINUED FROM BOOK 776 PAGE 14)



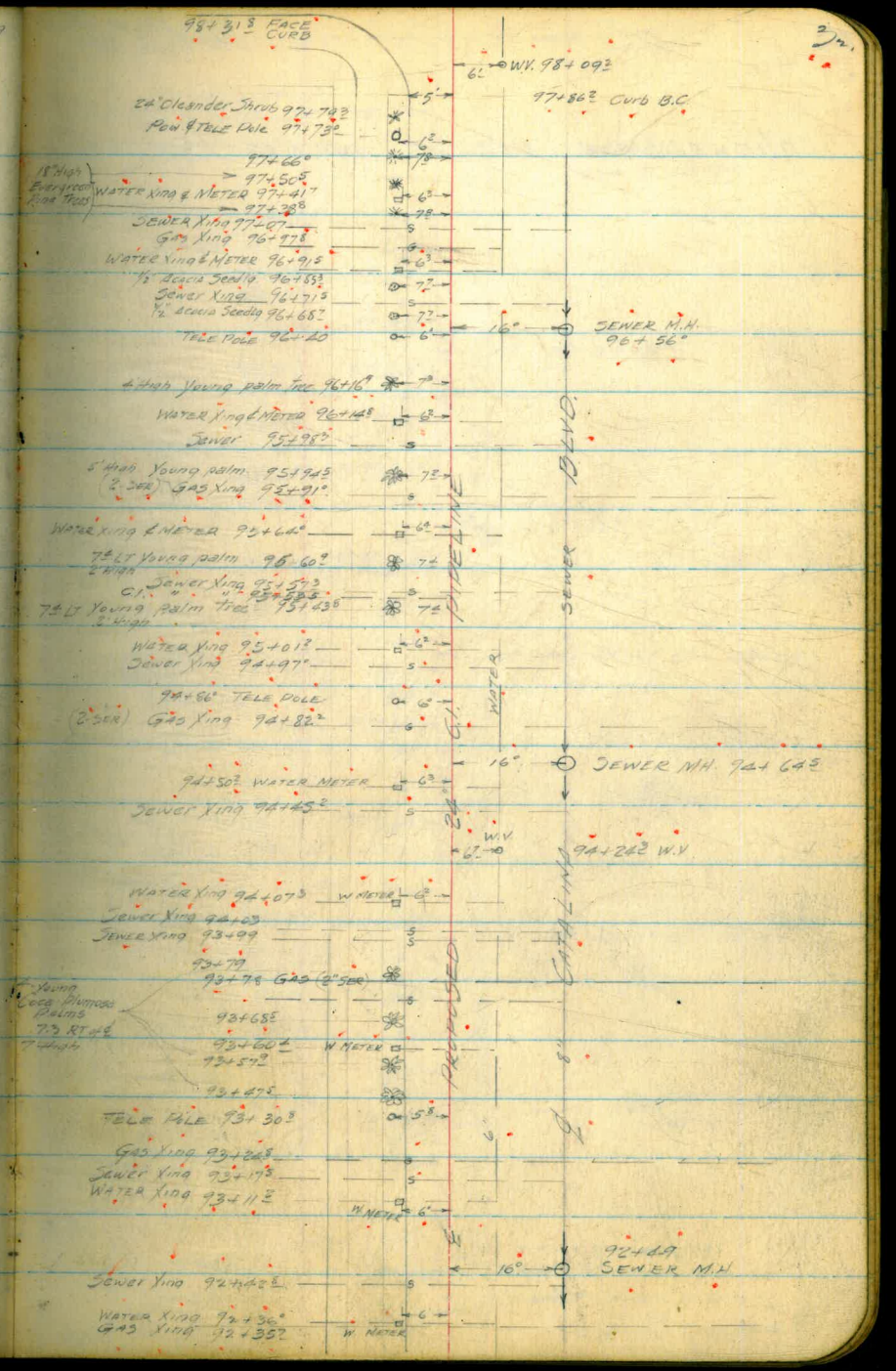
SEPT 20 1962

MIDWAY DRIVE & PT. LOMA PIPELINE



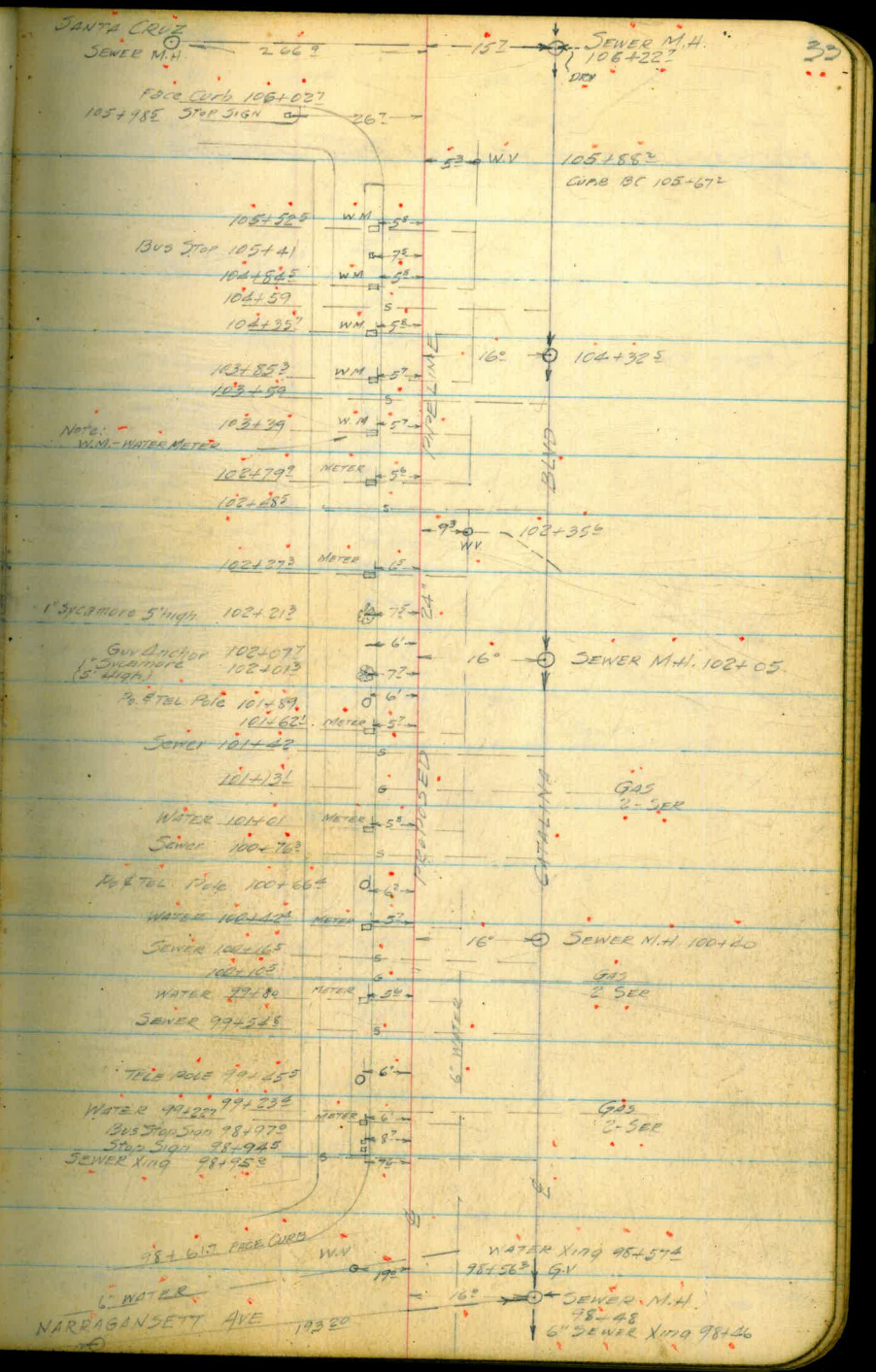
SEPT 20 1949

Midway Drive C/L Pt Loma Pipeline



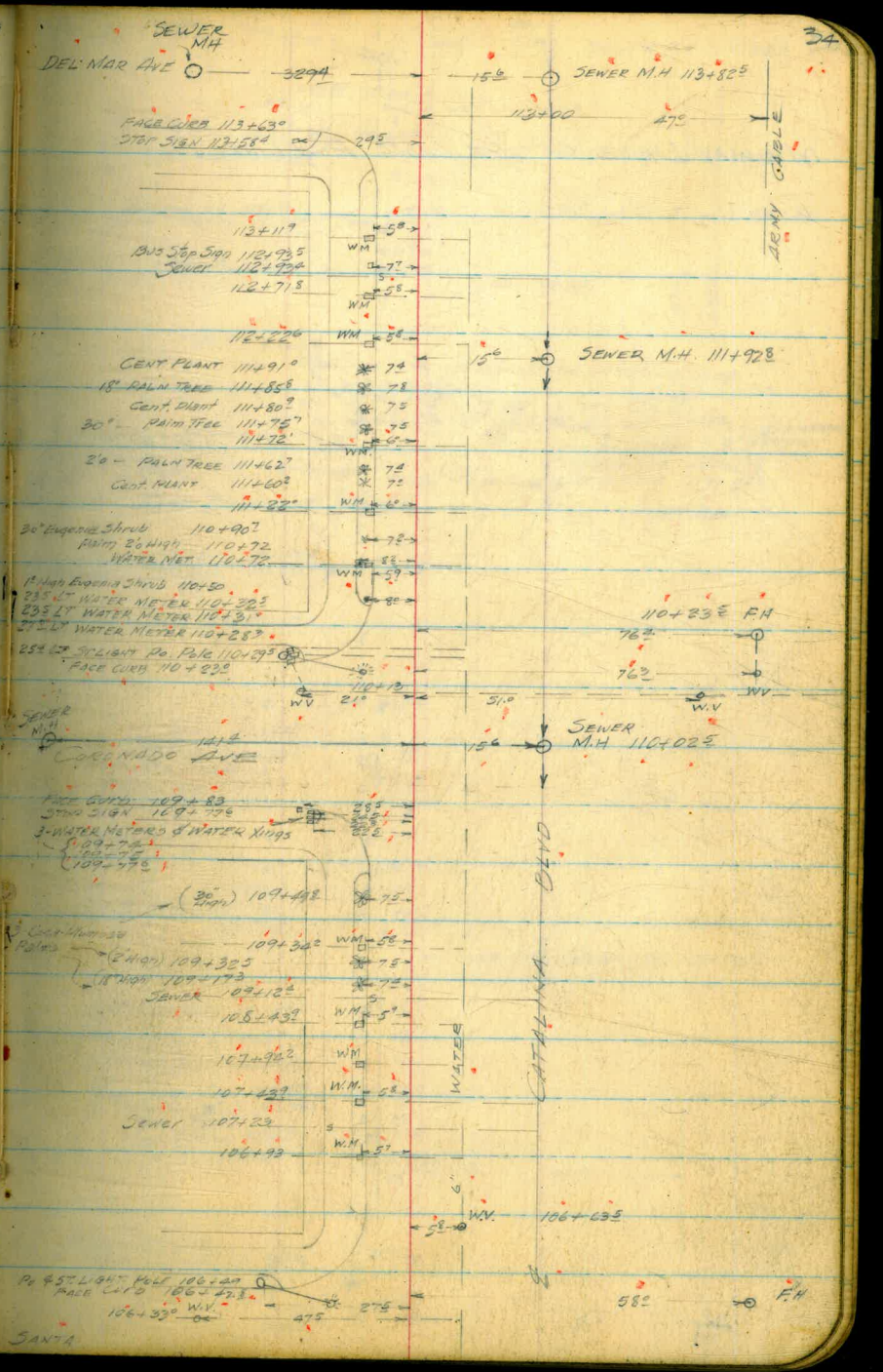
SEPT 22 1949

MIDWAY DRIVE ⊂ PT. LOMA RES. PIPELINE



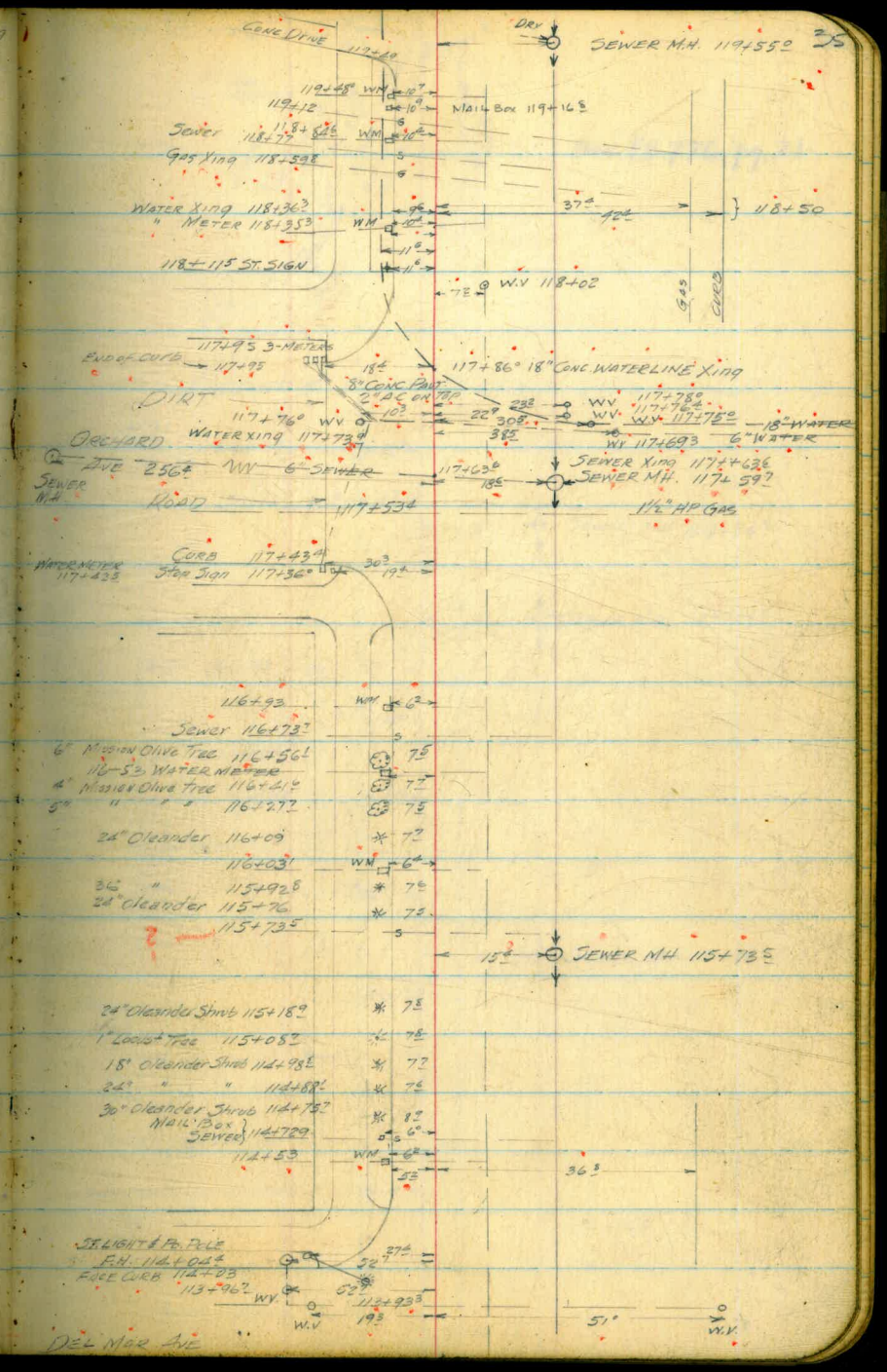
SEPT. 22 1949

MIDWAY DRIVE — PT LOMA RES. PIPELINE

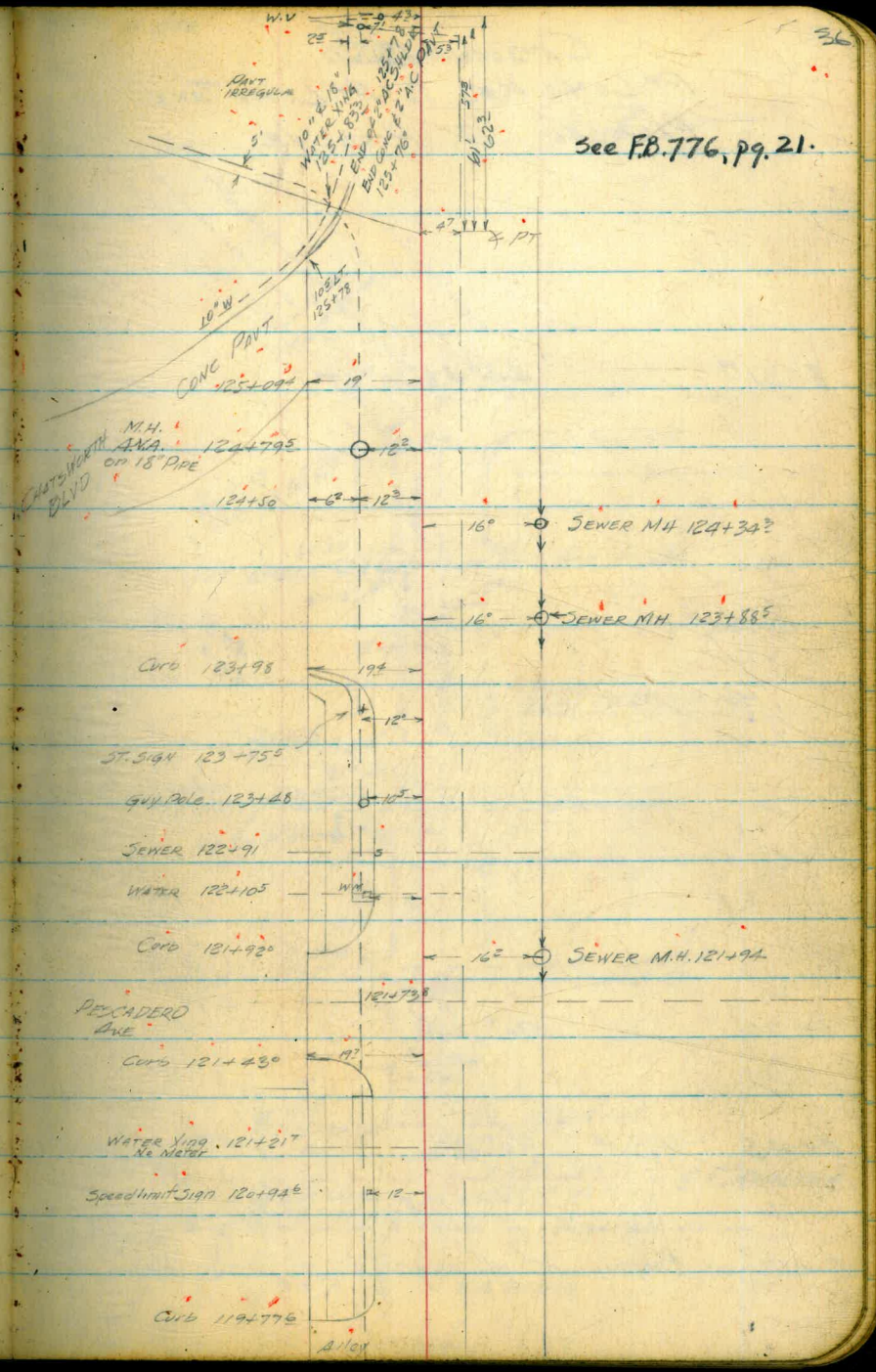


SEPT 24 1949

MIDWAY DRIVE — PT. LOMA PIPELINE



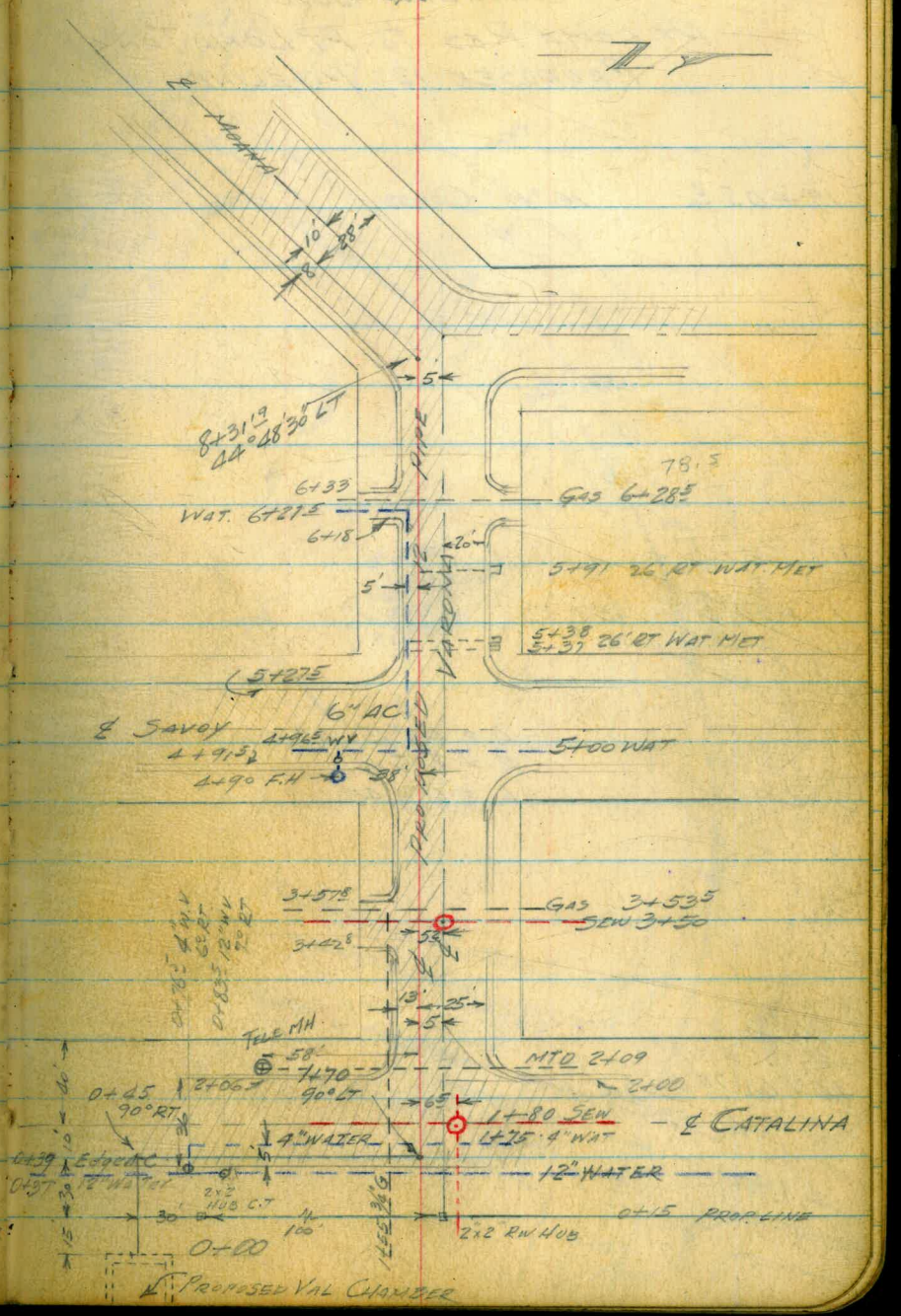
SEPT. 26 1949



See F.B. 776, pg. 21.

CATALINA BLVD
PT. LOMA RES TO PT. LOMA TANK
PROPOSED 12" PIPELINE

8+31.19	44° 48' 30" LT
1+70	90° LT
0+45	90° RT
0+00	Begin at N. edge of proposed Val Chamber



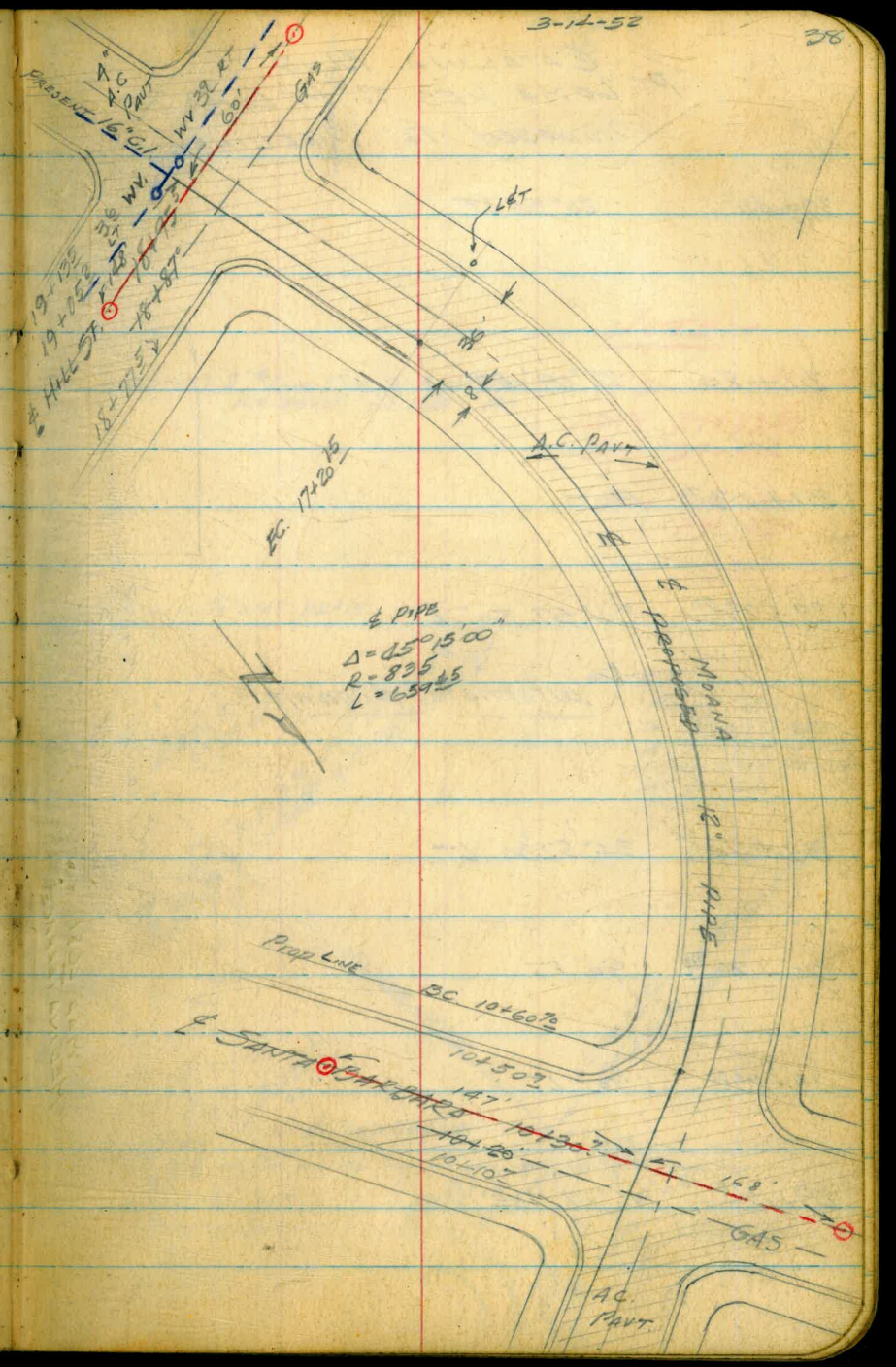
CATALINA BLVD
PT. LOMA RES to PT. LOMA TANK
PROPOSED 12" PIPELINE

19+05.2 16"x8" Cross.

17+20.15 E.C

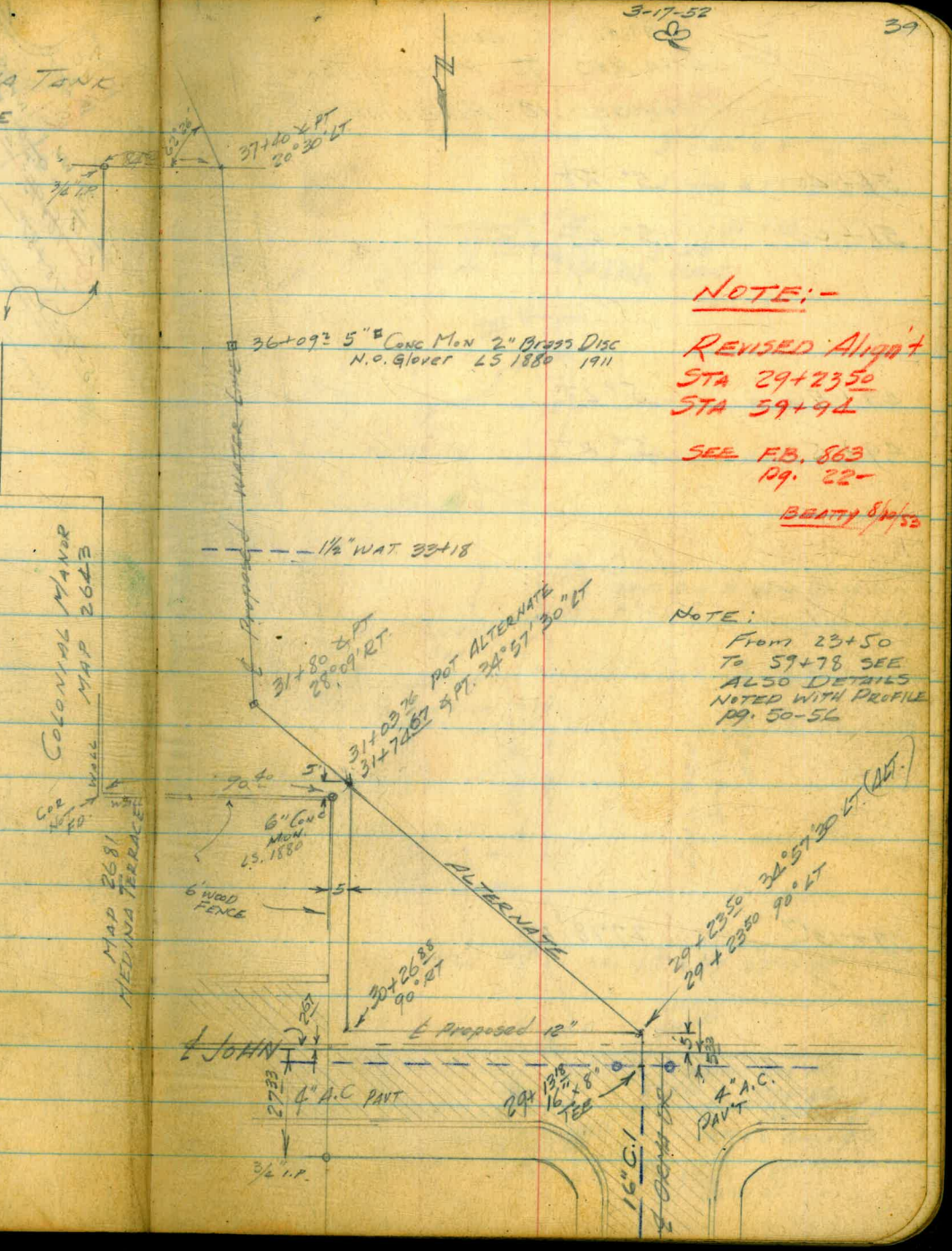
Δ = 45°15' LT
R = 835.00
L = 659.45

10+60.70 B.C



CATALINA BLVD.
PT. LOMA RES TO PT. LOMA TANK
Proposed 12" PIPELINE

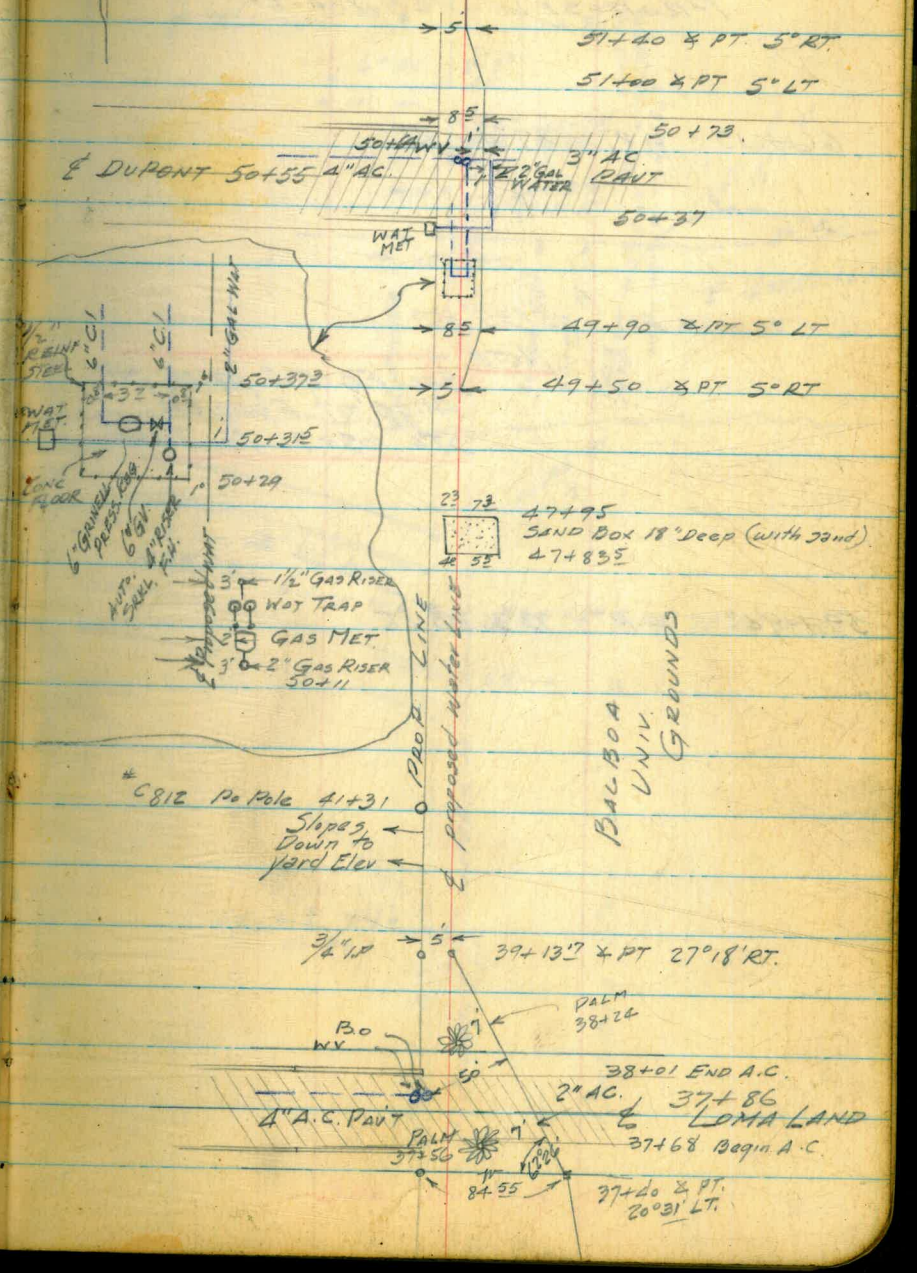
37+40	20°30' LT
31+80	28°09' RT
31+03.76	POT
29+23.50	34°57'30" LT
	Alternate Alignment
31+74.67	34°57'30" LT
30+26.88	90° RT
29+23.50	90° LT
29+13.18	16"x8" TEE



CATALINA BLVD
PT LOMA RES TO PT. LOMA TANK
PROPOSED 12" PIPE LINE

51+40	5° RT
51+00	5° LT
49+90	5° LT
49+50	5° RT
39+13.7	27°18' RT

SEE NOTE Pg. 39



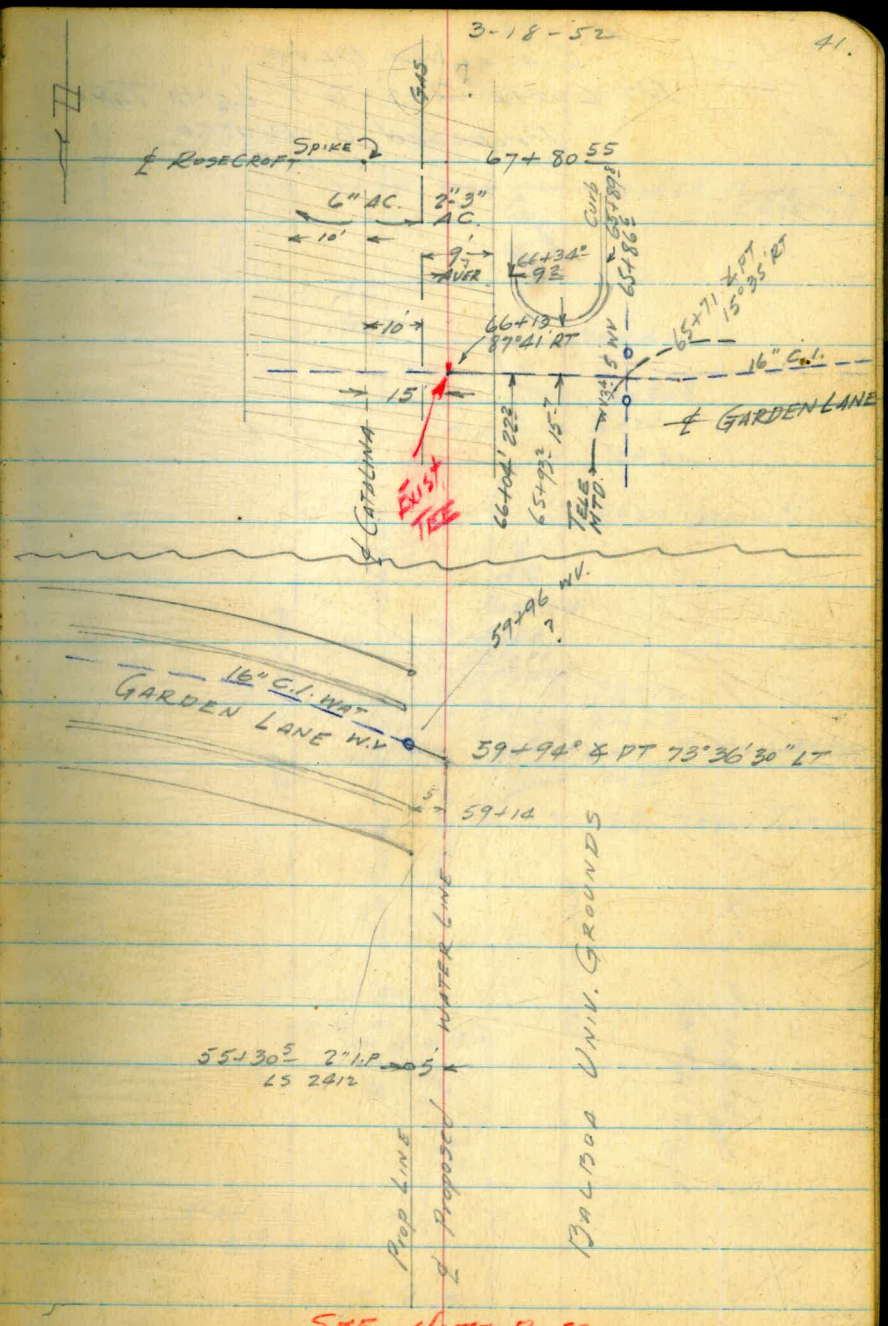
CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
PROPOSED 12" WATER

66+13 ℄ PT 87°41' RT.

65+71 ℄ PT 15°35' RT

NOTE:
See FB 865 pg. 14 for
Alignment Revision
STA 65+71 to TANK

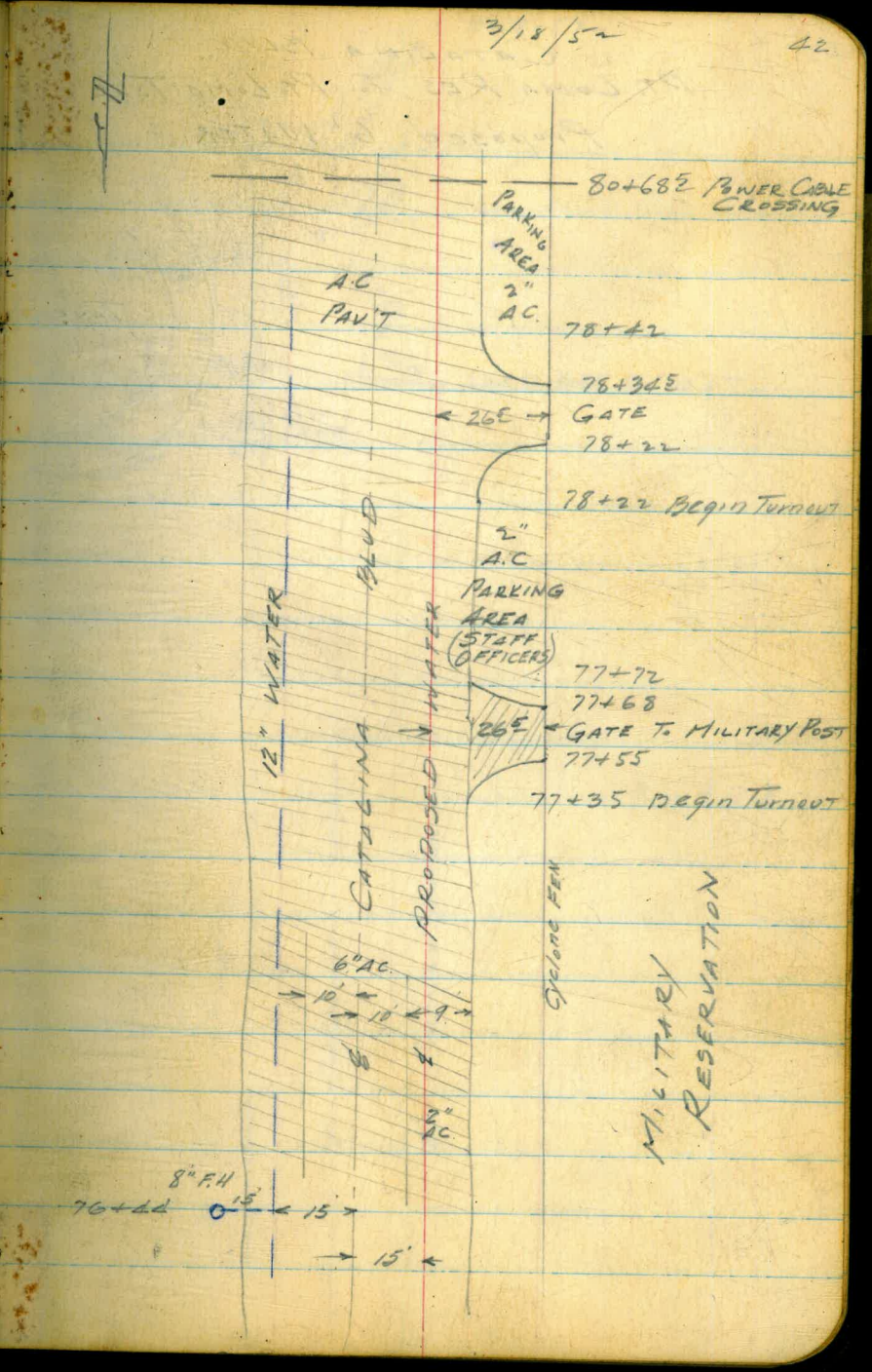
59+94± ℄ PT 73°36'30" LT.



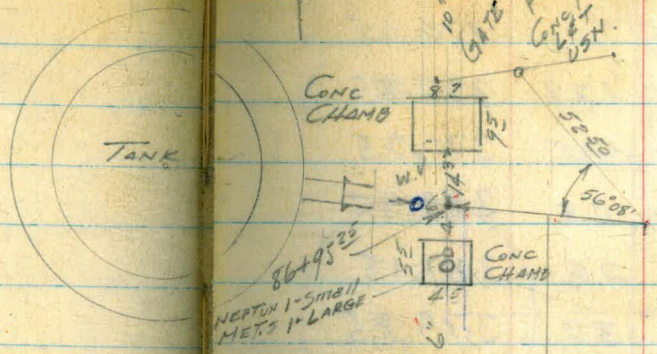
SEE NOTE Pg. 39

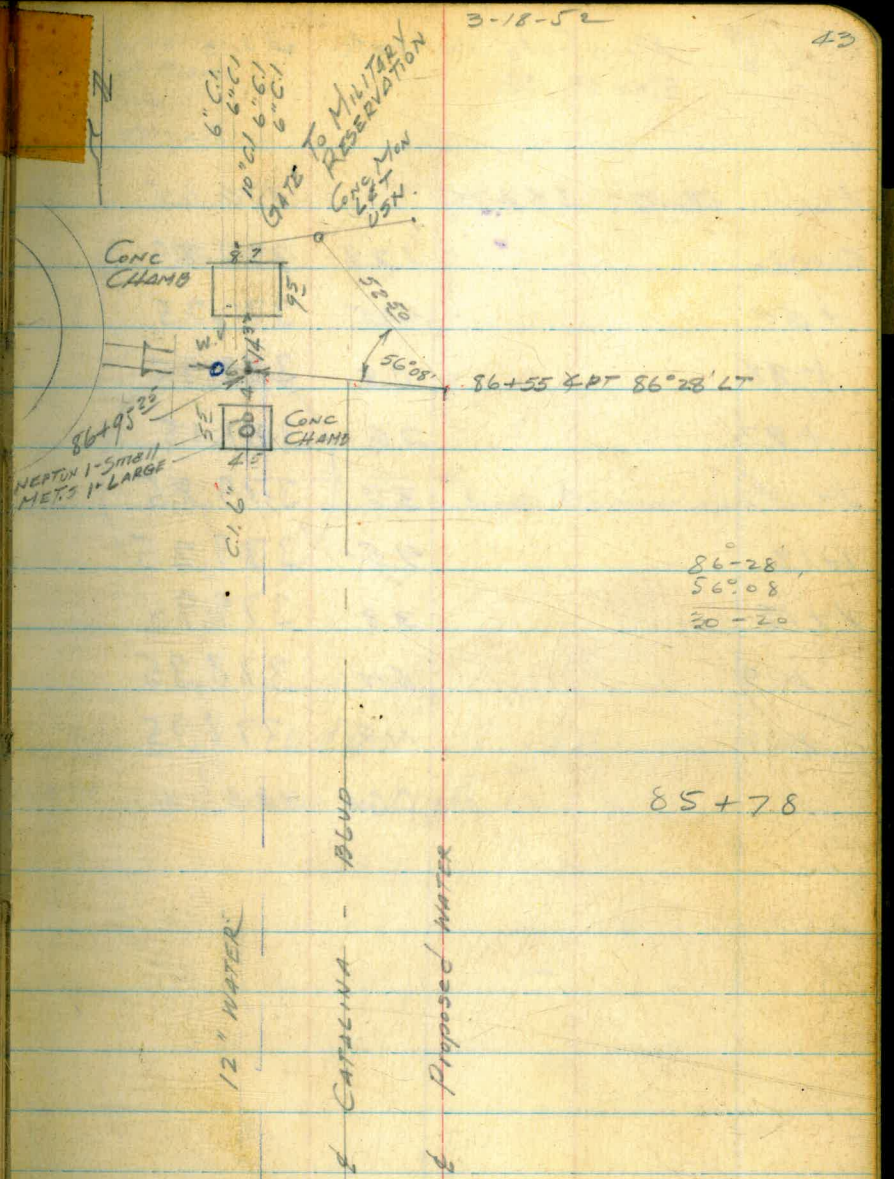
CATALINA BLVD
PT. LOMA RES TO PT. LOMA TANK
Proposed 6" WATER

3/18/52 42



CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
Proposed 6" WATER





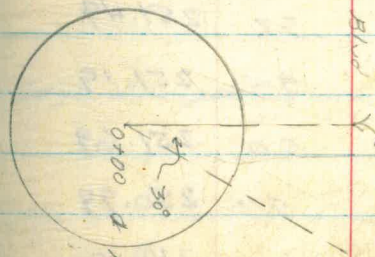
℄ Profile Waste Line

West
Williams
Kemp
Varontakis

7-30-53

1	13.10	383.75		370.65
0+00			12.9	370.85
+54			12.5	371.25
+88			0.8	382.95
+97			2.6	381.15
1+01.5			3.9	379.85
1+13			4.5	379.25
1+17			3.8	379.95
+19			5.4	378.35
+26			4.8	378.95
			0.61	383.14 = 373.14

℄ Tank



edge of Catalina
Cone Mon on navy gate

worked up p87
3/31/52

CATALINA BLVD
PT. LOMA RES. TO PT. LOMA TANK
& PROFILE

MAR 19, 1952
BEATTY
POWELL
BERGER

B.M.	5.87	256.69		250.82
0+00			7.45	249.24
+15			6.30	250.39
+34			5.2	251.49
+39			5.5	251.19
+45		℄ PT. 90°RT	5.0	251.69
+76.5			5.7	250.99
			7.50	249.19
			6.37	250.32
1+00			6.3	250.39
+50			7.95	248.74
+70			8.55	248.14
+80		℄ Catalina	7.80	248.89
		Rim	7.94	248.75
		Inv	15.74	240.95
2+00			7.25	249.44
		Rim	5.26	251.43
		Top MTD	9.86	246.83
		Bot MTD	11.76	244.93
2+09			6.45	250.24

BP SW Cor Varona & Catalina

E. prop. line Catalina BLVD

Edge A.C. pav't

4" G.V. 6°RT Top of val. stem 0+76.5

12" G.V. 7°RT Top of Val. Stem 0+83.5

1+12.5 39' LT TELE MH

(Edge A.C. pav't 3'RT)

(" " " 3.5 RT.)

1+55.5 3/4" GAS SER X-ING

SEW MH 6.5 RT 1+80

2+00 Face Curb Nor.
2+06 " " South
2+09.5 M.T.D. ⊞ Crossing

TELE MH 38' LT. 2+09.5

CATALINA BLVD
PT LOMA RES. TO PT. LOMA TANK
& PROFILE

		256.69		
℄ 2+50			2.65	254.04
TP	13.35	269.89 ✓	0.15	256.54 ✓
3+00			10.9	258.99
+50			5.7	264.19
		Rim	5.60	264.29
		Inv.	12.13	257.76
TP & NAIL				
4+00	12.75	282.17 ✓	0.47	269.42 ✓
+50			7.55	274.62
5+00			4.25	277.92
CH in □ SW Cor SET T&M			2.75	279.42 ✓
+50			2.80	279.37
6+00			0.70	281.47
TP	10.62	292.71 ✓	0.08	282.09 ✓
+50			9.15	283.56
7+00			6.90	285.81
+50			5.25	287.46
8+00			4.70	288.01
8+31.9 ℄ PT			4.90	287.81
+50			5.25	287.46
9+00			7.05	285.66

6" SEW. MH 5 ℄ RT 3+50

3+42.8
3+53.2 Gas } curb line Alley LT
3+57.8

Savoy 4+91.5 Face Curb
5+27.5 Face curb

4+90 38' LT Fire Hydt
4+96.5 38' LT W.V
5+00 WAT Crossing

5+37 26' RT WAT MET
5+38 26' RT " "
5+91 26' RT " "

7

ALLEY So 6+68 Curb line
6+83 Curb line
6+78.5 Gas Xing

6+61 26' RT WAT MET
6+62 " " "
6+79.5 WAT Crossing

6+82 WAT MET 26' RT
6+86 " " "
6+88 " " "
6+90 " " "
6+91 " " "

CATALINA BLVD
PT. LOMA RES. TO PT. LOMA TANK
℄ PROFILE (ET. AL)

		292.71		
9+50			8.55	284.16
10+00			10.00	282.71
CK BM	9.12	293.39 ✓	8.44	284.27 = 284.24
+10 Z			11.00	282.39
+30 Z			10.4	282.99
+50 Z			10.73	282.66
+60 Z (P.C. Prop Line)				
11+00			7.15	286.24
+50			3.25	290.14
IP on curb			0.30	293.09 ✓
BM	3.95	288.22 ✓		284.27
		RM 0.76		287.46
		Inv. 10.26		277.96
		RIM 11.90		276.32
		Inv. 21.55		266.67
CK BM			3.95	284.27 ✓
IP	11.98	305.07 ✓		293.09
12+00			10.85	294.22
+50			6.90	298.17
13+00			2.95	302.12
IP	3.36	308.26 ✓	0.17	304.90 ✓

BP NE Cor Santa Barbara & Moana

Face Curb Line

10+20 Gas Xing

℄ Santa B ℄ Sewer Xing

Face Curb line

8" Sew. MH. 147' LT.

Sew M.H. 168' RT.

CATALINA BLVD.
PT. LOMA RES. TO PT. LOMA TANK
℄ PROFILE

	308.26		
13+50		2.65	305.61
14+00		1.15	307.11
+50		0.70	307.56
15+00		0.95	307.31
+50		2.30	305.96
16+00		4.15	304.11
+50		6.00	302.26
17+00		7.75	300.51
17+20.13 EC		8.45	299.81
+50		9.50	298.76
18+00		11.20	297.06
(1) ℄ Nail +50'	5.65	300.88	13.03 295.23
+77.5			6.50 294.38
87°			6.45 294.43
+95.5			6.35 294.53
19+00			6.30 294.58
+05.2 16"x6" Cross,	Top Stem		7.43 293.45
"	"		7.81 293.07
+05.2			6.35 294.52
+13.5			

Face Curb line

18+87.2° Gas Xing.

℄ Hill St

W.V. 3.5 LT

W.V. 3.9 RT

Face of Curb line

CATALINA BLVD.

PT. LOMA RES. TO PT. LOMA TANK & PROFILE

300.88	Rim 8.74		292.14
	Inv. 13.55		287.33
	Rim 0.14		300.74
	Inv. 5.19		295.69
P	6.11	303.16 ✓ 3.83	297.05 ✓
P	5.55	301.16 ✓ 7.55	295.61 ✓
			295.61 ~~296.3~~
29+13.8 16"x8" Cross		5.55	~~300.61~~
	Top Stem	6.75	294.41
	Top Stem	6.90	294.26
29+18		5.50	295.66
29+23.50 ℄ PT 90° LT		5.3	295.86
+50		6.6	294.56
30+00		9.7	291.46
30+26.88 ℄ PT 90° RT		12.2	288.96
+40		12.6	288.56
+37.4		11.1	290.06
+50		9.5	291.66
31+00		9.9	291.26
+50		10.3	290.86
31+74.67 ℄ PT 34°57'30" LT		11.7	289.46
=31+03.76 P.O.T. on Alternate line			

6" SEW, M.H 60'-RT 18+95.5

"6" SEW, M.H 14.8'-LT 18+95.5 Inv 5.05

W.V. 3.8 RT

W.V. 3.8 LT

Edge A.C. paut

NOTE:—

REVISED Alignm't & Profile.

STA. 29+23.3 TO STA 30+94

SEE F.B. 863 pg 26-31

ERRATA 5/12/53

Top Curb 13.10/5 3.5 LT Begin small Eugenia Hedge

yard elev. 13.10/5

" 13.4/5

" 12.3/3

CATALINA BLVD
DT LOMA RES. to DT LOMA TANK
& PROFILE

Alternate Line		301.16		
29+23.5	(℄PT 32°58'LT)		5.3	295.86
+30			5.7	295.46
+42			1.2	299.96
+50			1.7	299.46
30+00			4.0	297.16
+50			7.6	293.56
31+00			11.2	289.96
PI		1.26	290.46	11.96	289.20
+50				4.7	285.76
+80	(℄ PT 28°9'RT)			6.5	283.96
32+00				7.3	283.16
+50				8.6	281.86
33+00				10.3	280.16
+18				10.4	280.06
+50				10.1	280.36
PI (Top 34)		7.69	288.73	9.42	281.04
34+00				9.0	279.73
+50				8.4	280.33
35+00				7.4	281.33

3/19/52 50

29+74 5' LT Acacia Clump
29+96 5' LT " "
30+12 16' LT " "
30+70 4' LT " "

6" Conc Mon LS 1880

31+35 2' LT 3" Acacia
31+50 2' RT " Clump

NOTE: Avacado's as shown appear to have been abandoned and is mostly regrowth.

32+75 9° RT " "

33+00 8" Avacado 12' LT. Half dead
33+18 1½" Wat x'ng
33+56 6' LT 8" Avacado

on ℄ 34+09 12" Avacado Dead Stump
34+38 { 2° LT Acacia Clump / 2° RT 10" Avacado
34+91 { 3' LT 6" Avacado / 8' RT 10" "

CATALINA BLVD
PT. LOMA RES. TO PT. LOMA TANK & PROFILE

288.73

35+39		6.1	282.63
+45		5.5	283.23
+50		5.4	283.33
36+00		4.2	284.33
TBM		3.76	284.97 ✓
+50		1.45	287.28
PT	11.90 300.21 ✓	0.42	288.31 ✓
37+00		9.3	290.91
+22		7.6	292.61
+40 ℄ PT		6.7	293.51
+50		6.5	293.71
+68		7.25	292.96
+70		7.45	292.76
+86		6.80	293.41
38+00		7.55	292.66
+01		7.40	292.81
+11		5.9	294.31
+50		4.9	295.31

35 +49 12' LT Acacia Clump
35 +45 8' LT 7" Avacado

35 +73 6° LT 8" dead Avacado

36+02 4° LT 6" Avacado

on ℄ 36+09.20 5" Conc Mon LS 1880 N.O Glover 1911
2" Brass Disc

36+24 9° RT 3" WY Pine (western yellow)

36+49 10' LT 3" Acacia

36+70 11' LT 3" PINE

37+56 7' LT, 3' Palm

Edge A C Pavt

℄ LOMALAND ST.

Edge of A.C

38+23.5 50' LT W.V & B.O

38+24 7° LT 24" Palm

CATALINA BLVD.
PT. LOMA RES. TO PT. LOMA TANK
℄ PROFILE

		300.21		
39+00			3.45	296.76
39+13.17 ℄PT 27°20' RT			3.15	297.06
SET TBM	12.20	309.21 ✓	3.20	297.01 ✓
+50			10.3	298.91
40+00			7.0	302.21
+50			5.3	303.91
41+00			4.6	304.61
+50			4.6	304.61
+67			4.8	304.41
42+00			5.7	303.51
+30			5.7	303.51
+35			8.2	301.01

on 3/4" I.P. Prop. Cor. 5' LT 39+13.17

Shldr. 7' LT	18.0	10.5	39+49 1" ornamental shrub ?
yard elev →	19.	7	
			39+85 1" RT 10" Euc Tree
"	14.0 / 10	7.3 / 4	
"	13.1 / 14	5.9 / 2	
"	11.6 / 10	4.8 / 1	
			41+31 5° LT #C-812 Po Pole
"	11.8 / 20	5.5 / 11	41+50 9° LT 12" W/ Pine
"	11.6 / 15	5.5 / 4	
			41+69 5° RT 3-12" Dead Euc.
"	11.6 / 21	6.3 / 11	41+90 11' LT 12" W/ Pine
			42+14 clump of pine

CATALINA BLVD
PT LOMA RES. TO PT. LOMA TANK
& PROFILE

309.2'

42+50			8.2	301.01
+72			8.8	300.41
+85			10.4	298.81
43+00			10.6	298.61
TP	5.75	305.59 ✓	9.37	299.82 ✓
+62			6.5	299.09
+64			4.5	301.09
+50			4.6	300.99
44+00			5.3	300.29
+50			5.6	299.99
45+00			4.9	300.69
+23			4.3	301.29
+50			4.2	301.39
46+00			3.0	302.59
+69			2.3	303.29
+50			1.8	303.79
+52			1.0	304.59
TP	11.17	316.74 ✓	0.02	305.57 ✓
47+00			10.4	306.34

	14.1 (15)	9.8 (11)	9.2 (5)	8.4 (4.5)
	13.6 (16)		10.7 (13)	
yard elev	9.9 (19)		5.4 (11)	
yard elev	14.1 (11)		10.8 (4)	

42+55 6' LT Euc. Tree

43+46 12 RT 24" Wy Pine

43+72 2° LT Small palm 4' high

44+08 4° LT Euc. Stump

44+18 1° RT 5" Euc

44+26 3° RT Euc Stump

44+26 Begin Rustic picket FEN 5° LT

44+37 6" Euc 0° RT

44+59 4° RT 6" Euc

44+77 1° RT 3" Euc

45+02 End Rustic picket FEN 5° LT

45+23 1° LT 14" Dead Euc

45+38 3° RT 12" " "

45+75 { Rustic picket FEN 5° LT; 8° 14" Dead Euc

46+24 E Edge 18" Pine ℄

46+56 End rustic picket FEN. 5° LT.

46+56 8° RT. 18" Pine

47+31 5° LT 12" Pine

47+46 0° LT 12" Pine

CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
& PROFILE
316.72

47+50		8.7	308.04
48+00		5.9	310.84
+50		2.0	314.74
P	9.55	326.29 ✓ 0.0	316.74 ✓
49+00		8.4	317.89
+50 ℄ PT 5° RT		6.0	320.29
+90 ℄ PT 5° LT		4.6	321.69
50+00		4.3	321.99
+25		4.4	321.89
+27		9.4	316.89
		11.0	315.29
Top of westerly 6" CI.		9.43	316.86
Top. 2" Galv. Pipe		6.63	319.66
50+37		9.6	316.89
+38		6.0	320.29
+50		6.3	319.99
+56		6.3	319.99

RT

N 4 W 18 — 9.2 10

47+83 5 RT — 4° LT } 18" Deep Sand PLAY Box
47+95 7.3 RT — 2.3 LT

7.2 18. — 2.9 10

Conc floor of Val Chamber under construction

LT.

47+64 3.5 RT 12" PINE
47+82 0.5 LT 16" PINE
48+02 0.5 LT 10" PINE
+27 W. Edge 10" PINE on ℄
+41 4' RT 10" PINE
48+37 0.7 LT 10" PINE
48+73 5° LT Begin 5' high FEN
49+00 4° RT 11" PINE
49+36 1° RT 10" W.V. PINE
49+68.5 END FEN 5° LT
49+73 4° RT 10" W.V. Pine
49+87 7.5 RT " " "
50+11 3° RT 2" Riser GAS } 2" To MET & WAT TRAP
50+18.5 3° RT 1½ Riser GAS
50+25 7° LT 10" Pepper

50+29 LT, 1.5 Reinf steel for Box
50+31.5 2" Galv. Pipe 9.0 E to 1° RT
50+30.5 6" Riser Auto FH SPKL
50+37 8.5 LT End Conc Curb
50+73 8.5 LT End " "
50+64.5 1° LT & 2° LT W.V.s

CATALINA BLVD
PT LOMA RES. TO PT LOMA TANK
& PROFILE

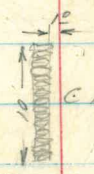
32629

50+69		6.4	319.89
+76		3.9	322.39
51+00 4PT 5° LT.		3.0	323.29
+20 4PT 5° RT.		2.8	323.49
+50		2.8	323.49
PP (Tapstk)	7.15 331.28 ✓	2.16	324.13 ✓
52+00		6.4	324.88
+50		5.0	326.28
53+00		3.6	327.68
		329.28	2
+50		2.0	320.3 ?
PP	13.33 341.14 ✓	3.47	327.81 ✓
+53		11.4	329.74
+60		9.8	331.34
54+00		8.1	333.04
+50		6.4	~~333.74~~ 334.74
55+00		3.0	~~333.14~~ 338.14
+50		1.3	339.84
PP	7.65 347.00 ✓	1.79	339.35 ✓
+85		6.3	340.70

51+14 3E RT 20" W.Y PINE
+18E on & Acacia Clump.
+28 4° RT 16" Pine

51+63 5E LT 4° Conc BLK WALL
+72 & Clump 1"@ 2° Trees

52+03 24" W.Y PINE E. Edge on &
52+39 11' RT 28" PINE
52+42 End Conc BLK WALL 3E LT



C 10' RICK of Fire Wood 1°LT

3/4" prop Cor 5'LT 53+20

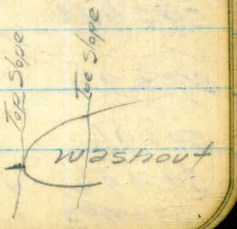
+60 Euc Stump 4' Left
53+96 2E LT Acacia 2"

yard clw 13.2 / 15 — 9.1 / 5 ×
" " 12.0 / 18 — 7.2 / 5 ×
" " 10.2 / 15 — 8.2 / 15 — 3.2 / 3 ×
" " 9.3 / 16 — 7.0 / 16 — 2.1 / 5 ×

54+31 10" Euc 4° RT

3/4" I.P 5'LT 55+53

11.5 / 5 — 7.0 / 4 ×



CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
& PROFILE

		347.00		
56+00			5.9	341.10
+50			4.5	342.50
57+00			4.3	342.70
+50			4.3	342.70
58+00			4.8	342.20
+50			4.8	342.20
59+00			6.1	340.90
PI Top str	0.66	342.25 ✓	5.41	341.59 ✓
+14			2.3	339.95
5+8 2°		End of curb	2.6	339.65
59+92±			3.9	338.35
59+96		Rim	4.48	337.77
59+96		Top Val Stem	6.75	335.50
59+96	NAT GRD		4.0	338.25
59+99±	Edge 4" A.C. Pad		4.25	338.00

yard elev. 13.1/18 6.8/5

12.6/14 9.0/13 4.9/2

12.0/19 7.8/17 5.1/8

12.3/18 8.6/18 vert Rock Wall 8.6/13 5.1/6 wall

SEE NOTE pg. 49

55+92 W. edge 12" 12' high Spanish bayonet plant on ℄

55+30± 5' LT 2" I.P. Prop Cor LS 2412

56+32 7' RT Acacia Clump

56+56 1° LT 12" Euc

57+09 8' LT W/ Pine 12"

57+15 2' RT W/ Pine 10" Dia.

57+10 7± LT Begin Rock Rubble wall 1° High.

57+56 1° RT acacia Clump

57+84 8° RT 10" W/ pine

57+97 5° LT End Rock Wall

57+97± 5± LT Begin RW FENCE 4° High

58+43 - 2° RT 18" Euc

58+63 - East Edge 12" Euc on ℄

59+00 4° RT 12" Euc 6° High

59+27 5± LT End RW FEN

59+35± 4° LT 12" Euc

59+38 6° LT 2' High Wood Rail Fen

59+49 2± RT 8" Euc

59+63 5± LT End Rail Fenc

Face of curb 5' LT 59+14

59+78 5± RT 16" Dead Pine

Catalina Blvd & Profile (Cont'd)

		342.25		
Set TBM		3.78	338.47 ✓	Nail in Pow Pole End of Curb South Side, Garden Lane
P	0.23	329.35 ✓	13.13	329.12 ✓
P	0.07	316.06 ✓	13.36	315.99 ✓
P	6.25	309.90 ✓	12.41	303.65 ✓
65+86.6			7.10	302.80	Top A.C. Pavt	65+89.8 Face of curb Lma
" "		Top of Stem W.V.	9.30	300.60	W.V. 3½ Lt	65+93.2 15.2 Rt to curb
" "		Top of Stem W.V.	9.40	300.50	W.V. 5° Rt	
66+00			6.95	302.95		
66+13.00 (℄ PT 87°41' Rt.)			6.90	303.00		66+04.1 End curb rt 22.2 Rt
Set T3/4	9.07	312.80 ✓	6.17	303.73 ✓	Chis □ End of curb	66+32 9.2 Rt End curb RET
+50			9.35	303.45	Edge AC 6° Rt	
67+00			8.55	304.25	Edge AC 4° Rt	
+50			7.4	305.40	" " 4° Rt	
68+00			6.0	306.80	" " 4° Rt	
+50			4.55	308.25	" " 4° Rt	
69+00			2.70	310.10	" " 4.5 Rt	
+50			0.7	312.10	" 3° "	
P	13.22	325.84 ✓	0.18	312.62 ✓		
70+00			11.55	314.29	" 4° Rt	

CATALINA BLVD.
PT. LOMA RES. TO PT. LOMA TANK
& PROFILE

325.84

70+50		9.20	316.64	Edge AC 4° RT
71+00		6.55	319.29	" " 4° RT
+50		3.75	322.09	" " 3° RT
72+00		0.85	324.99	" " 4° RT
PI	13.23	339.04 ✓	325.81 ✓	
+50		11.05	327.99	" " 5° RT
73+00		8.05	330.99	" " 3° RT
+50		5.05	333.99	" " 4° RT
74+00		2.15	336.89	" " 3° RT
PI	13.10	352.00 ✓	338.90 ✓	
+50		12.0	340.00	" " 3° RT
75+00		9.10	342.90	" " 3° RT
+50		6.15	345.85	" " 3° RT
76+00		3.15	348.85	" " 4° RT
+50		0.35	351.65	4° RT
PI	11.44	363.16 ✓	351.72 ✓	76+44 30' LT 12" TEE
				" 43' LT 8" F.H. (Large)
77+00		8.80	354.36	" " 3° RT
+50		6.40	356.76	77+35 Begin Driveway Turnout
				77+55 26± RT Gate Post
78+00		3.90	359.26	" " 3° RT 77+68 26± RT
				77+72 End Driveway Turnout

CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
& PROFILE

		363.16		
	78+50		1.8	361.36
TP		10.00 373.12 ✓	0.04	363.12 ✓
	79+00		9.80	363.32
	+50		7.95	365.17
	80+00		6.30	366.82
	+50		4.35	368.77
	+68.5		3.85	369.27
	81+00		3.50	369.62
	+50		2.85	370.27
	82+00		1.60	371.52
	+50		0.45	372.67
TP		10.54 383.56 ✓	0.10	373.02 ✓
	83+00		9.85	373.71
	+50		8.75	374.81
	84+00		7.60	375.96
	+50		6.35	377.21
	85+00		5.15	378.41
	+50		4.05	379.51
	86+00		3.00	380.56

Parking Area RT

78+19 Begin Dewy Turnout
+22 Gate Post 26.5 RT
+34.5 " " 26.5
+42 End Driveway Turnout

80+68.5 Power Cable Xing

80+83 22.5 RT
81+13.5 22.5 RT
} Main Gate & Guard House US Naval CIC. Trng Center

81+19 Water Xing

81+48 5' RT Edge Storm Inlet

82+00 3.5 RT Stub Pole

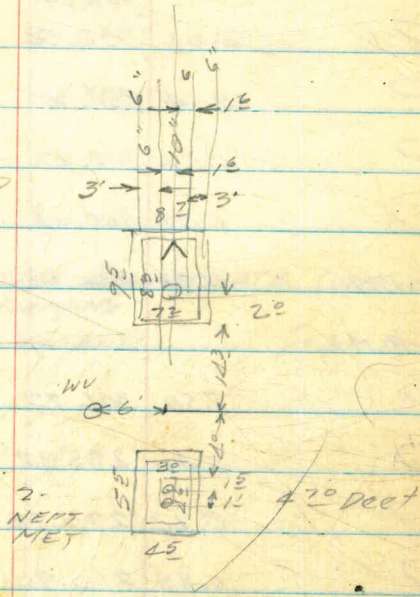
82+94 20' RT
83+15 20' RT
} Gate

Catalina Blvd & Profile (Cont'd)

		383.56		
86+50			1.90	381.66
+55 & PT			1.76	381.80
+71			0.73	382.83
+90 3			1.32	382.24
86+95 25			1.50	382.06
+99 2 · Edge A.C			1.67	381.89
		Rim	1.58	381.98
		Top 6"C.I	5.15	378.41
		Rim	1.28	382.28
		Top 10"C.I	4.64	378.92
SET TBM.			0.20	383.16 ✓
TBM.	1.22	384.38 ✓		383.16
P	0.93	373.60 ✓	11.71	372.67 ✓
P	1.30	361.60 ✓	13.30	360.30 ✓
P	0.53	349.59 ✓	12.54	349.06 ✓
P	8.80	348.46 ✓	9.93	339.66 ✓
CK BM	3.36	348.09 ✓	3.73	344.73 = 358.42

3/21/52

Thicker A.C ?



on L & T, Conc Mon center of Gate into Military Reservation

Mar. 24, 1952

Mon So End of Silvergate & Military Res
(MUST BE ANOTHER MON)

CATALINA BLVD
PT. LOMA RES TO PT LOMA TANK
& PROFILE & CHECK LEVELS

		348.09			
P	0.33	336.54	11.88	336.21	
P	0.14	324.30	12.38	324.16	
P	0.04	310.97	13.37	310.93	
P	0.58	300.68	10.87	300.10	
CK BM	7.33	300.78	7.23	293.45	=293.60
CK B.M			8.34	292.44	= 292.70
P	7.50	301.77	6.51	294.27	
P	0.46	288.92	13.31	288.46	
P	0.12	275.72	13.32	275.60	
P	0.88	265.90	10.70	265.02	
P	0.47	253.66	12.71	253.19	
P	9.10	262.44	0.32	253.34	
P	2.76	261.73	3.47	258.97	
CK BM			10.85	250.88	= 250.82

BP 85' S of SL. DUDLEY & SILVERGATE (0.15 low)
on East Curb of Silvergate

BP SE Cor Charles & Silvergate (0.26 low)

Lillian St
Gertrude to Viola

West
Powell
Kemp

Sta	+	Hi	−	
	12.53	90.40		77.87
	4.69	94.93	0.16	90.24
	1.95	83.78	13.10	81.83
			4.08	+8.2 invert
0+00			7.6	76.2
+50			9.8	74.0
			8.87	+6.80
1+00			8.3	75.5
+50			4.9	78.9
2+00			2.3	81.5
+50			2.2	81.6
3+00			5.6	78.2
			5.00	+6.90 invert
+50			9.8	74.0
	1.81	73.36	12.23	71.55
4+00			4.0	69.4
+50			7.6	65.8
5+00			13.7	60.0
+25			14.4	59.0
5+23			14.15	+8.60 invert 59.2
	12.94	85.97	0.33	73.03
	9.25	94.97	0.25	85.72
	4.21	89.77	9.41	85.56
			11.94	77.83 = 77.87

Bm NE BP Douglas + Hilda

West rim MH 0 - 50

West rim MH 0+71

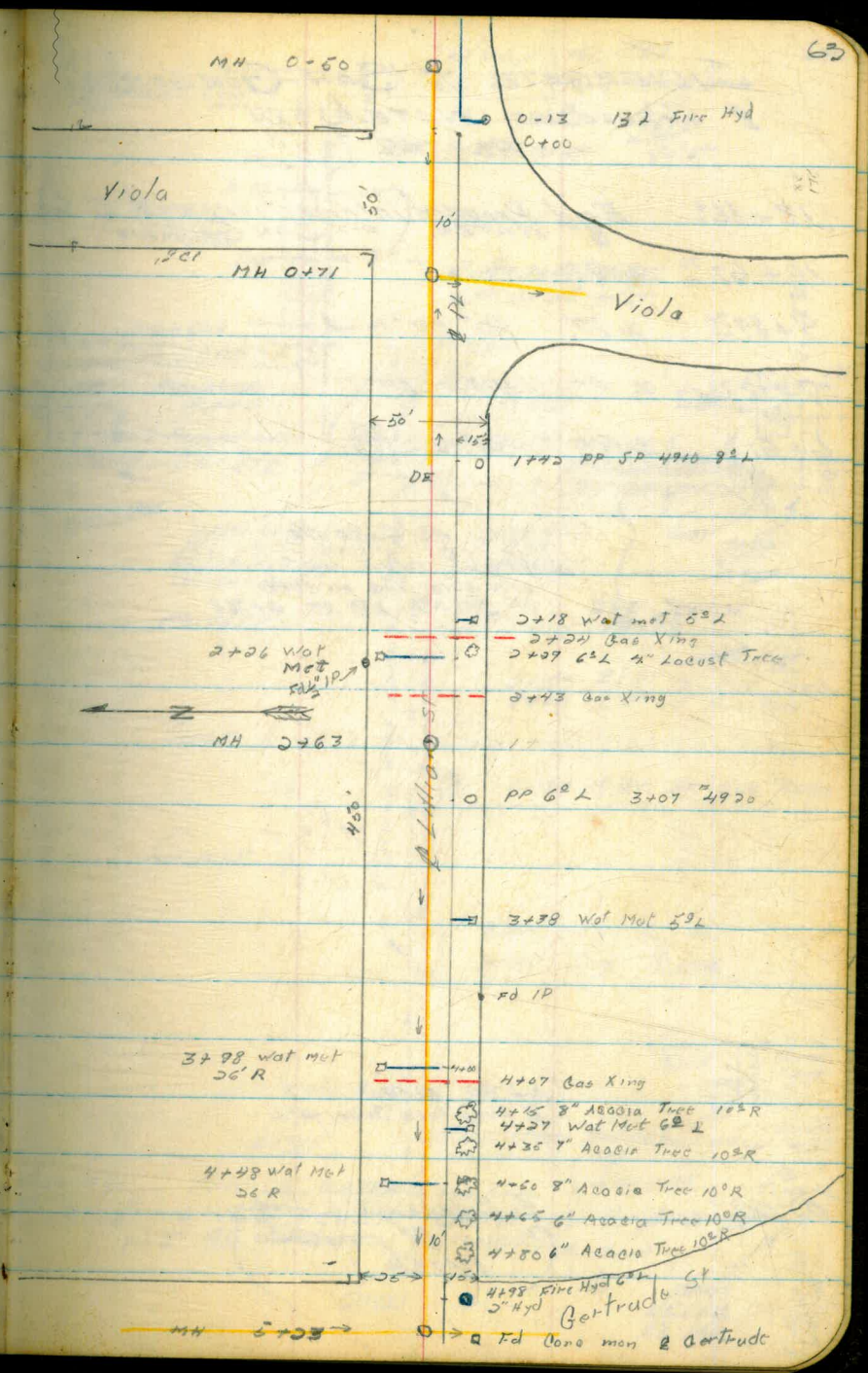
MH Dead end towards Gertrude

MH 5+23

Lillian St (Dirt Street)
Viola to Gertrude St

0+00 East Prop Line Viola

5+25 ℄ Gertrude St



SILVERGATE TO SAN GORGONIA & PROPOSED WATER IN P.L 142 ?

12+86± End Proposed 8" WATER (Intersection with 6" C.I. on SAN Gorgonio)

10+67.7± ℄ PT 90° LT

9+89.7± ℄ PT. 90° RT.

7+12.7± ℄ PT. 90°12' RT

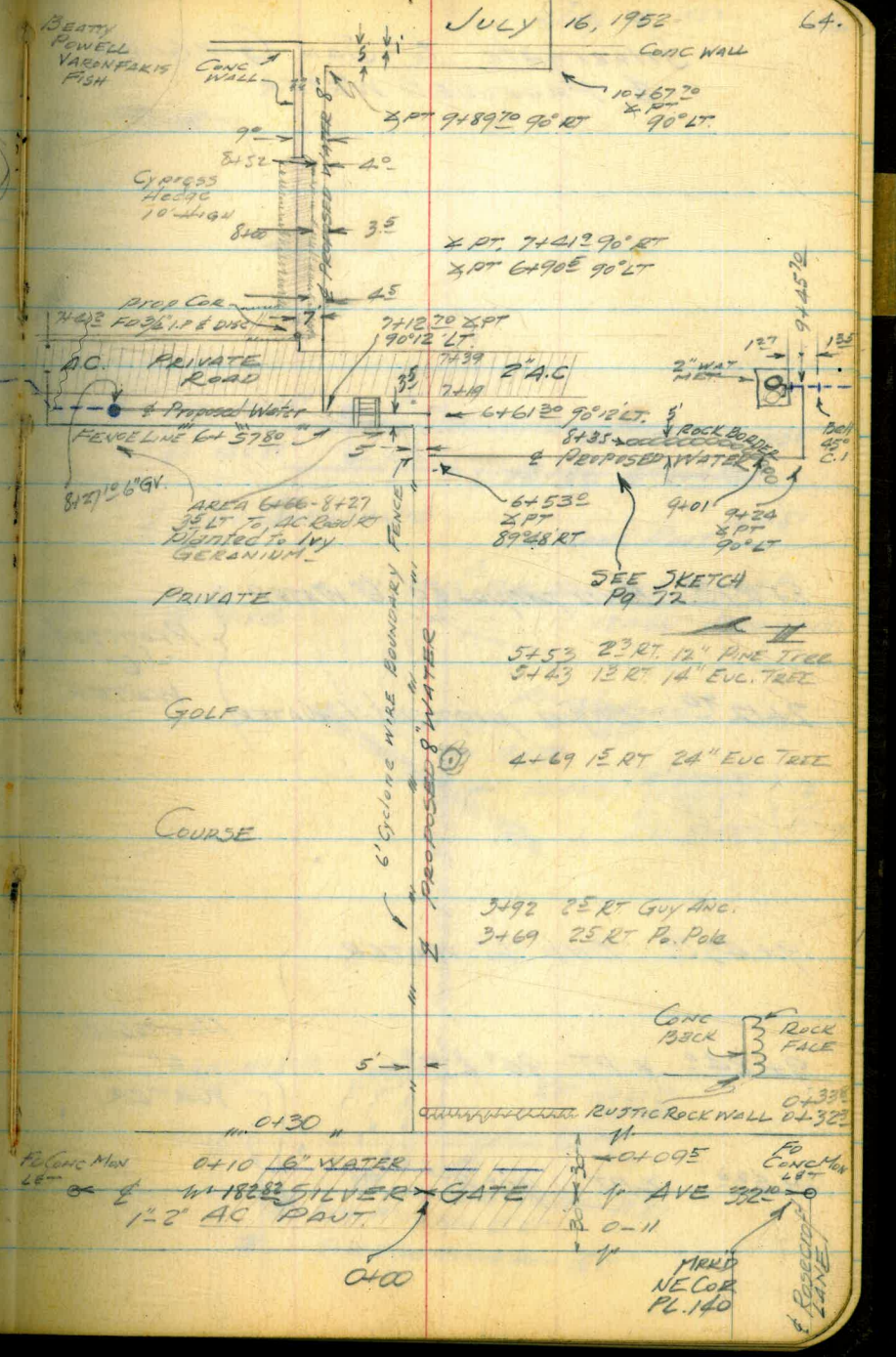
6+61.3± ℄ PT 90°12'LT

(W/y RL. GAGE DR (6+66± prop. line.) City Engr. Tag on Curb OF STEPS, 6.5± RT. 6+76±

(0+30 prop. line E. Prop. line Silvergate)

0+00 ℄ Silvergate Ave. (Begin. 8" proposed WATER)

JULY 16, 1952 64.



Silvergate to San Gorgonia & Proposed Water

8+27.10 End proposed 6" water

7+12.70 Begin proposed 6" water

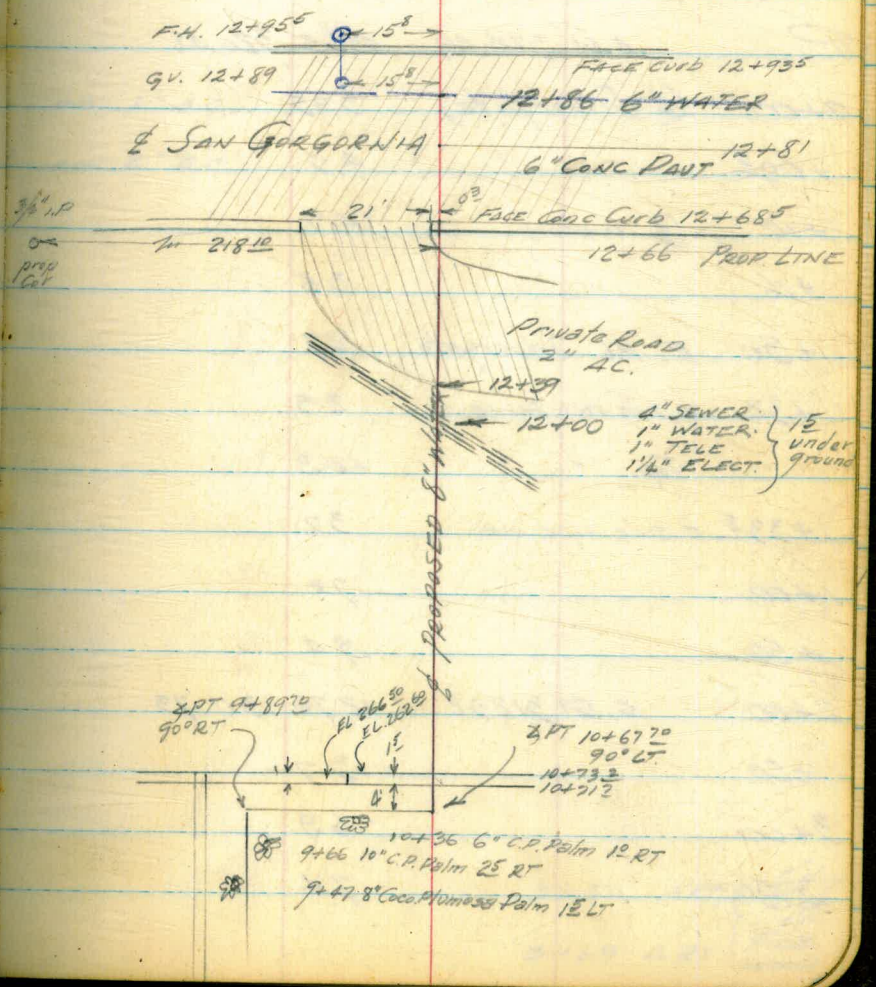
Proposed 6" water

9+45.30 End 6" water

9+24 ℄ PT 90° LT

6+53 ℄ PT 90° RT

Proposed 6" water



℄ Profile Proposed Water Silvergate To San Gorgonio

BM.	1.07	294.67		293.60
TP	13.39	307.82	0.24	294.43
TP	13.12	320.53	0.41	307.41
Set TBM			9.52	311.01
TP	4.01	324.49	0.05	320.48
0+00	(℄ Silvergate)		3.95	
+09.5			4.5	
+10	(℄ water)		4.7	
+16			3.5	
+30	E. P.L Silvergate		2.7	
+32	W side rock fence		2.5	
	Top " "		+0.3	
+33.8	E side rock wall		3.2	
1+00			7.0	
+50			9.4	
TP 2+00	0.59	312.32	12.76	311.73
+50			3.7	
3+00			6.9	
+50			9.4	

B.P. 85' So. P.L Dudley & Silvergate on curb

on Conc mon. Nor 0+00

on 1" A.C.

on 2" A.C.

3+50 4'RT } 5' high Rick of Fire Wood
3+69 4'RT }

℄ PROFILE
SILVER GATE – SAN GORGONIO

		312.32		
4+00			12.3	
P	1.85	301.88 ✓	12.29	300.03
+50			3.2	
5+00			4.9	
+50			6.7	
6+00			8.8	
6+53° ℄ PT 90° RT			9.6	292.3
SET TBM			11.65	290.23
7+00			8.8	293.1
+50			8.5	293.4
P	1.02	295.15 ✓	7.75	292.13
+80			2.5	292.7
8+00			1.0	294.2
+23			3.6	291.6
+50			4.5	290.7
+81			5.6	289.6
9+00			6.2	288.95
+02			6.9	288.3
+05			7.2	288.0

293.0
285.1 285.5 89 293.3 C
16.8 16.4 8.6
16 14 10 C

292.65
284.9 291.9 292.2 2.5
10.3 3.3 3.0 10 C
12 9 5

291.1
284.6 289.9 290.5 4.1
10.6 5.3 4.7 10 C
13 10 5

285.0 288.5 289.5
10.2 6.7 5.7 C
14 10 4

285.1 288.1
10.1 7.1 CROSS
10 6 287.7 C Rock Border 9+01
285.0
10.2 7.5
8 5 C

℄ PROFILE
SILVER GATE - SAN GORGONIO

295.15 ✓

9+10		8.3	286.9
+15		8.4	286.8
+20		7.8	287.4
+24 ⅋ PT 90° LT		8.2	287.0
+27		10.6	284.6
+35		11.3	283.9
9+45.70		11.40	283.8
T3M	0.86	291.09	4.92 290.23
6+61.3 ⅋ PT 90° LT.		+0.7	
+66.		0.0	
+75.9		0.89	
+79.9		0.86	
7+00		1.9	
+50		3.2	
8+00		4.6	
+27.10 ⅋ G.V.		5.6	
7+12.70 ⅋ PT 90° RT		2.2	
+17		3.1	

285.7 288.7

9.5 c 7.0
5 5

280.1

9.1
4 c

Top 6" C.I. pipe (END of 6" C.I. on TAVARA DRIVE place)

c 0.1 4.5 4.7
4 8 9 on AC

on Conc curb of steps c 4.7
8 on AC.

on " " " " c 4.7
8 on A.C

c 2.7 4.7
4 7 on A.C

c 4.8 5.2
5 7 on AC

c 5.0 5.9
3 5 " "

(END of 6" C.I. on GAGE DRIVE) c 5.7 6.3 " "
3. 6.

SPKLR WAT Line 35'-L RT 6+66 8+27

℄ Profile
SILVER GATE – SAN GORGONIO

		291.09		
7+19			4.70	
+39			5.1	
+50			5.5	
8+00			6.6	
+25			7.5	
+50			9.8	
P		0.00	278.26	12.83 278.26
9+00			3.7	
+50			11.2	
+63			12.7	
+66			13.0	
P		1.50	267.99	11.77 266.49
9+89.70	℄ PT	90° RT		4.2
10+00				4.3
+36				4.4
10+67.70	℄ PT	90° LT		4.9
+71.2				5.35 262.64
+73.2				5.45
+73.2				9.6

Edge 3" AC private road
Edge " AC " "

9+47 8" C.P. Palm 15 LT.
9+66 10" " " " 23 RT.

NE Cor End of Wall

10+36 6" CP Palm 1° RT.

on W. edge Conc. Wall
on E. " " "

℄ Profile
SILVER GATE – SAN GORGONIO

		267.99		
10+78			10.4	
+82			12.7	
P	0.23	255.32	12.90	255.09
+83			3.0	
11+00			10.5	
P	0.39	243.54	12.17	243.15
+25			6.4	
P	0.10	231.04	12.60	230.94
11+50			2.8	
+56			3.3	
P	0.84	218.56	13.32	217.72
+92			9.3	
P				
12+00	0.05	206.31	12.30	206.26
+24			7.2	
P	0.42	194.69	12.02	194.27
+35			6.8	
+39			12.65	on A.C.
+50			13.4	on A.C
P	2.53	184.87	12.35	182.34

0.0 4 — 3.0 3 — C — 4.1 6

8.0 6 — C — 11.2 8

18" high punctree 11+05 4' RT

C — 7.1 8 — 10.3 10

4.4 8 — 2.8 3 — C — 3.2 4 — 4.2 6 — 3.5 10

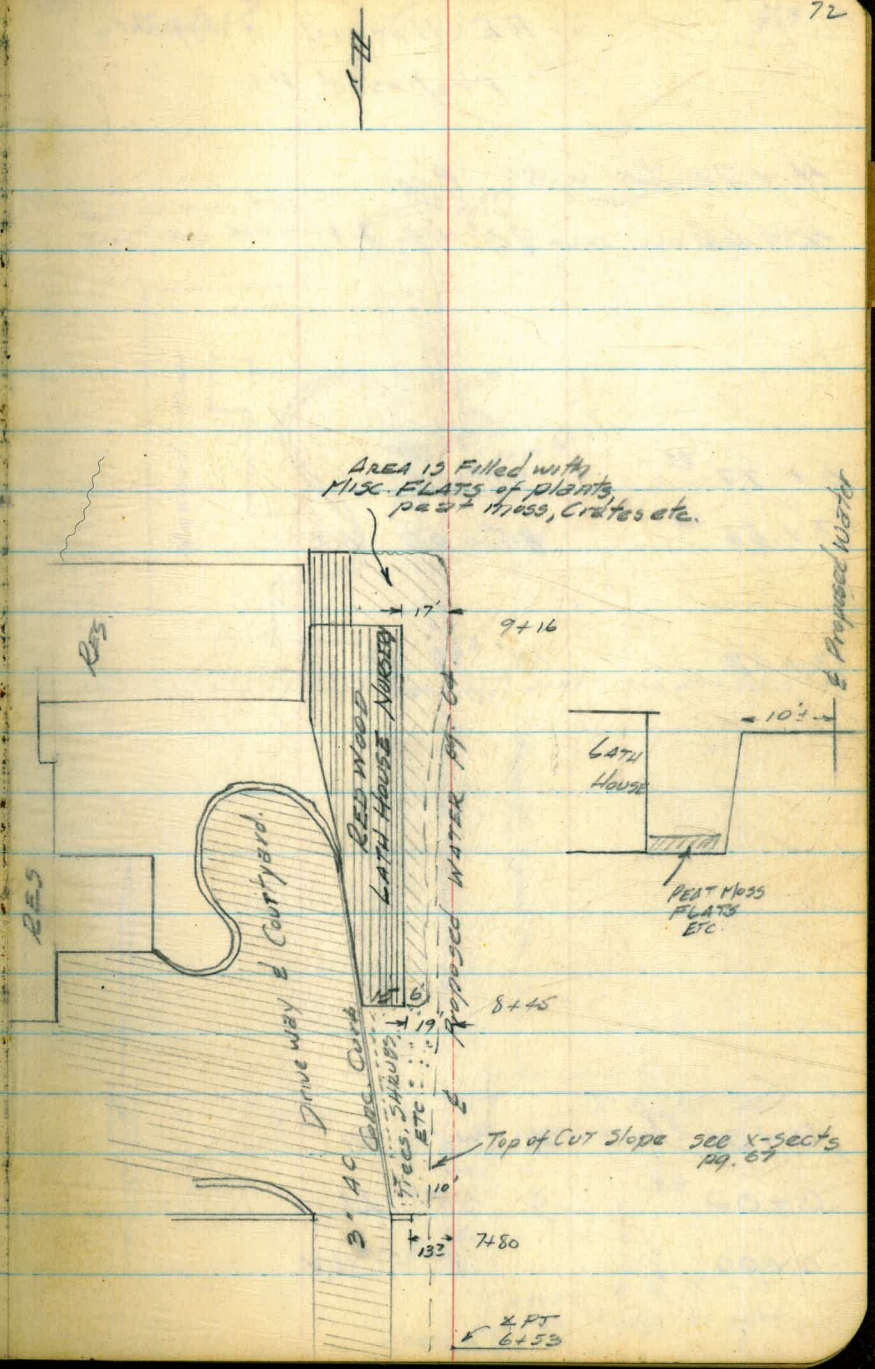
4" SEW, 1" WAT, 1" TEL, 1½ Elect } 15' under Ground
Crosses @ 45° to LT.

& Profile Cont'd.

SILVERGATE — SAN GORGONIO

		184.87			
12+12			5.1	on Edge A.C.	
+68			6.05	Top. curb	
+68			6.65	Gutter (Conc.)	15 RT 12+66 ℄ Mail Box
+86	End proposed 8" water.		6.45	on 6" Conc pavt.	
P.	0.65	172.66	12.86	172.01	
P.	0.03	159.94	12.75	159.91	
P.	1.50	148.35	13.09	146.85	
P.	0.18	140.71	7.82	140.53 ✓	
P	12.75	153.31	0.15	140.56	on SEW DE Cap.
P	13.42	166.26	0.47	152.84	Unable to find B.M. B.P. SW Cor San Gorgonia & La Crescentia Elev. 136.59.
P	13.32	179.55	0.03	166.23	
	13.25	192.75	0.05	179.50	
	12.74	205.44	0.05	192.70	
	9.86	214.78	0.52	204.92	
			2.52	212.26 = 212.21	B.P. NW Cor La Crescentia & Tavara Place

SKETCH OF
HAZARD Property



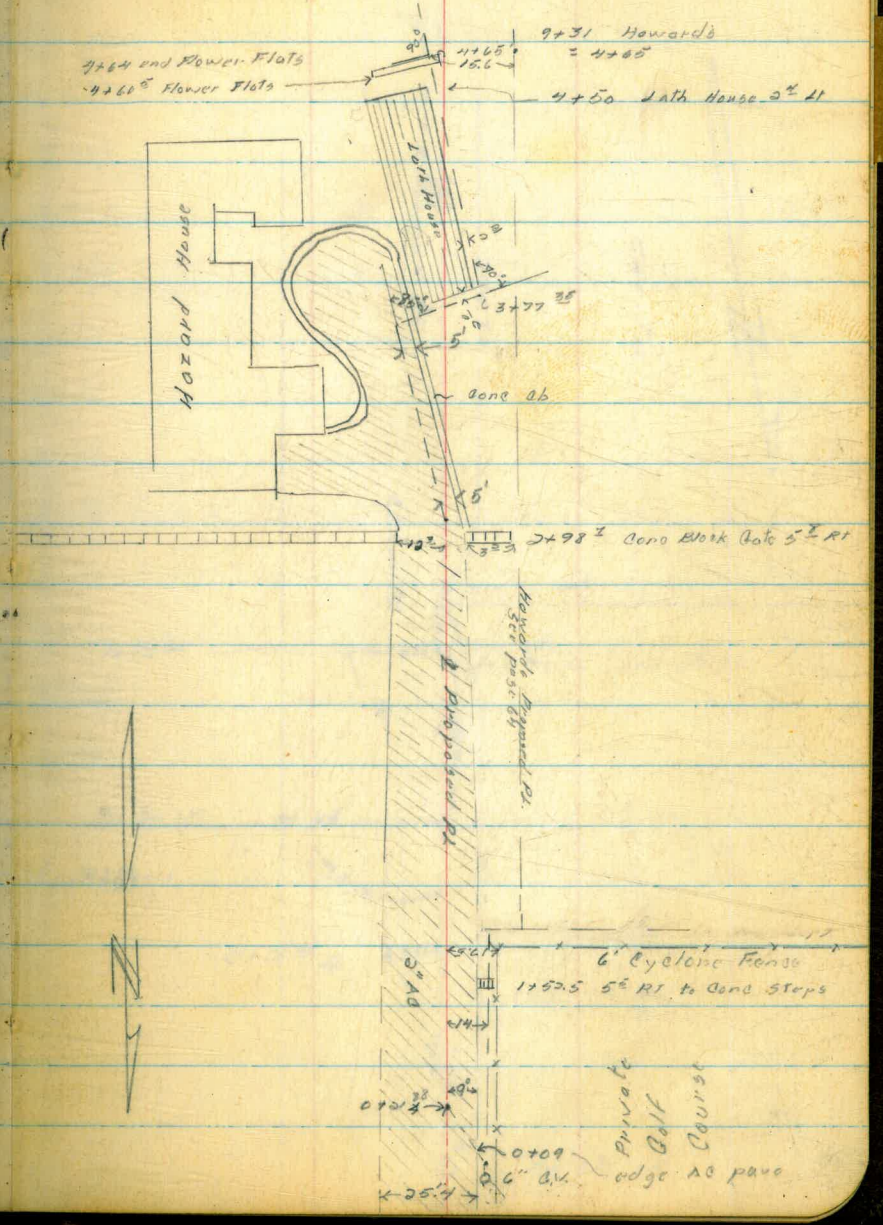
R.E. Hazard Property

Proposed P.I.

Date?

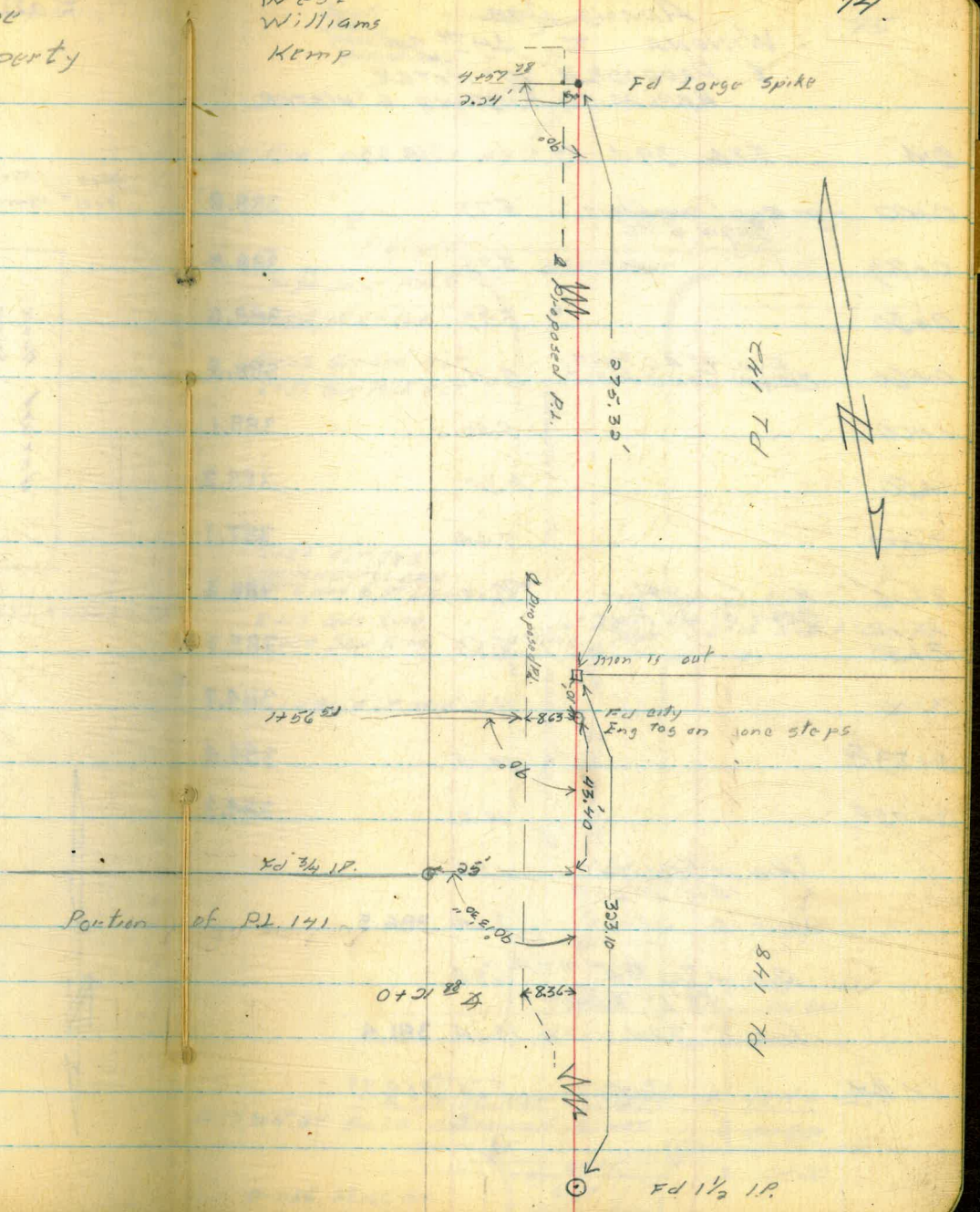
73.

4+71 ±	4" Pipe
4+65	90° 00 Lt
3+77 35	70° 00' Lt
3+56 29	85° 00' Rt
3+03	14° 41 Lt
0+21 98	Δ 45° Rt
0+02 20	Δ 45° Lt
0+00	℄ A.V.



Ties to Pipe Line Thru Hazard Property

West
Williams
Kemp



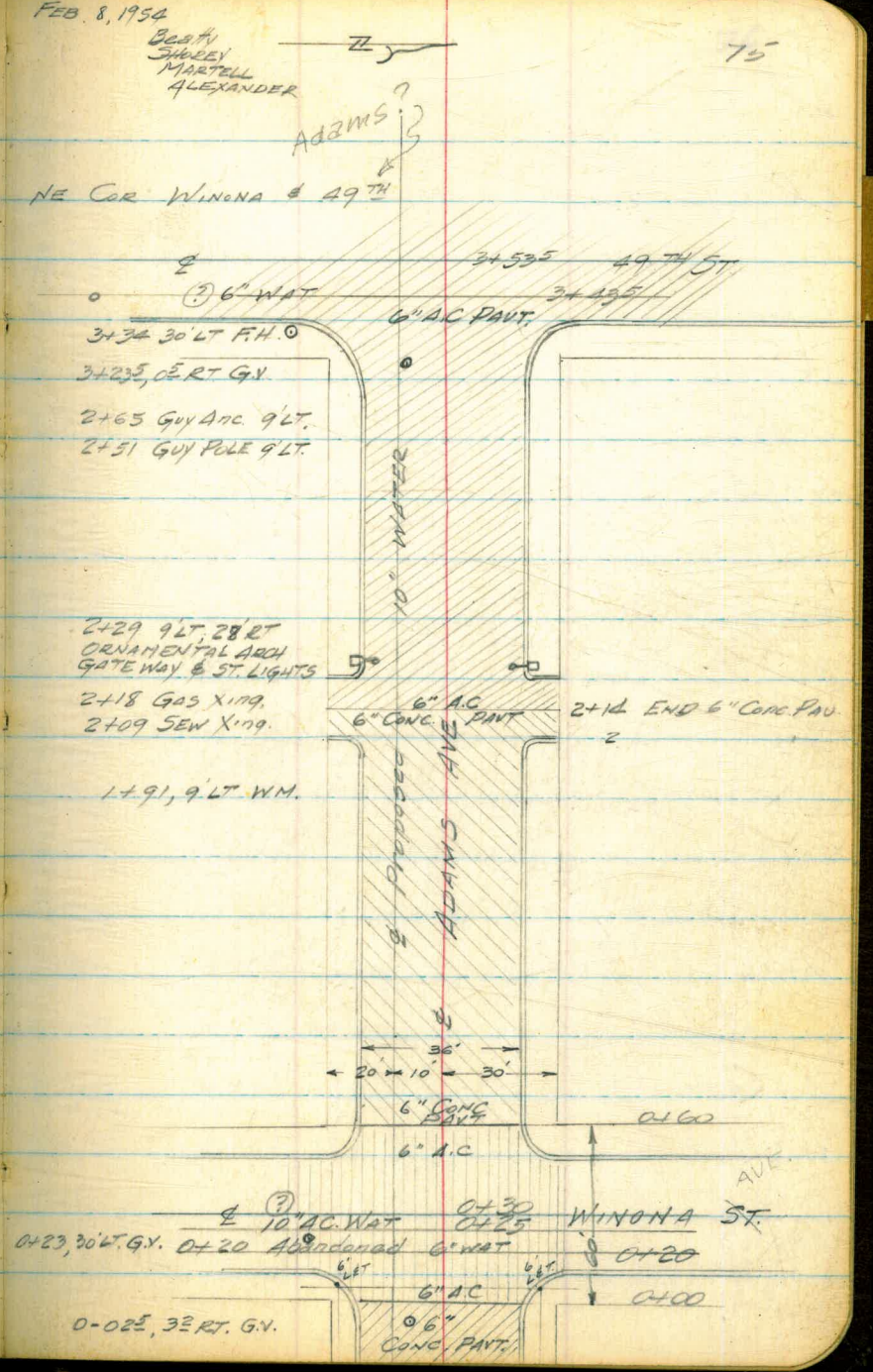
ADAMS AVE
WINONA TO 49TH ST
& PROPOSED 10" WATER
REPLACING EXISTING 6" WATER

BM.	5.24	394.57	389.33
0+00	END CONC PAVT BEGIN 6" AC."	5.73	388.8
0+23		5.75	388.8
0+50		5.93	388.6
0+60	END 6" A.C PAVT, BEGIN CONC. PAVT.	5.71	388.9
1+00		5.50	389.1
1+50		6.39	388.2
2+00		7.44	387.1
2+16	END CONC PAVT BEGIN 6" AC PAVT.	8.01	386.6
2+50		8.85	385.7
3+00		9.91	384.7
3+23.50		10.45	384.4
3+43.5		10.25	384.3
	Rim of SEW MH 278' RT 2+09	1.84	
	INV 6" SEW.	8.04	386.5
	Rim of SEW M.H. 152' LT. 2+09	6.94	
	INV. 6" SEW.	13.14	381.4
CK BM.		5.24	389.33

FEB. 8, 1954

BOATH, SHOREY, MARTELL, ALEXANDER

75



BEATTY
POWELL
BERGER 3/20/52

WATER METERS IN ALLEY BETWEEN FAIRMOUNT & 43rd FROM WIGHTMAN TO LANDIS.

	10.21	351.10		340.89		NW BP Fairmount & DWIGHT		
BM	6.56	355.36	2.30	348.80	~~349.15~~	NW BP Fairmount & LANDIS Gone		
5+97 - Nor Prop line LANDIS								
5+62 E			4.55	350.81	349.7	C/1	0	
5+62 W			4.60	350.76	349.7	C/0		
5+22 E			4.0	351.4	350.4	C/0	0	
TP	6.20	357.38	4.18	351.18				
5+11 W			6.47	350.91	~~350.5~~ ~~350.4~~	C05	1	C04
4+87 W			5.86	351.52	~~350.6~~ ~~350.4~~	C4	2	C09
4+73 E			5.85	351.53	~~350.4~~ ~~350.5~~	C4	1	C09
4+43 W			6.31	351.07	~~350.7~~ ~~350.6~~	C05	1	C04
4+23 E			5.61	351.77	~~350.8~~ ~~350.6~~	C42	2	C/0
3+97 W			5.07	352.31	~~350.8~~ ~~350.7~~	C46	1	C/5
3+52 E			4.25	353.13	~~351.1~~ ~~350.9~~	C02	2	C20
3+51 W			4.51	352.87	~~350.9~~ ~~351.1~~	C02	2	C20
3+17 W			4.75	352.63	~~351.0~~ ~~351.1~~	C46	1	C/5
3+12 E			4.61	352.77	~~351.1~~ ~~351.2~~	C47	1	C/6
2+61 W			4.71	352.67	~~351.5~~ ~~351.6~~	C42	1	C/1
2+47 E			4.25	353.13	~~351.7~~ ~~351.8~~	C44	1	C/3
2+14 W			4.20	353.18	~~352.0~~ ~~352.2~~	C42	2	C/0
1+84 W			3.82	353.56	~~352.0~~ ~~352.6~~	C42	2	C/0
1+59 E			3.54	353.84	~~352.7~~ ~~352.8~~	C41	1	C/0
1+39 E			3.40	354.0	~~353.1~~ ~~352.9~~	C41	2	C09
1+36 W			3.67	353.71	353.2 ~~353.0~~	C07	2	C05
1+32 W			3.60	353.78	~~353.1~~ ~~353.3~~	C07	2	C05

357.38

0+92 E	2.33	355.05	353.7 ~~353.5~~
0+85 W	3.05	354.33	3538 ~~353.6~~
0+51 W	3.16	354.22	3541 ~~3540~~
0+00 = Sa. Proposed Wightman.			
P	2.08	355.30	

C6 2 C14

C07 2 C05

C02 1 C01

(A) 6+40

6)24)53

Profile Proposed PL. Thru Hazard Prop

See page 68

T.B.M. Top North Side conc Steps

℄ A.V.

6.6
5° Lt edge oil

edge oil

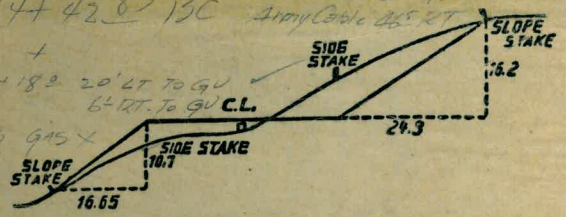
1.1	1.17	291.40	290.23
0+00		5.90	285.5
+02 20 A		5.6	285.8
+09		6.6	284.8
+21 88 B		6.1	285.3
+50		5.8	285.6
1+00		5.2	286.2
+50		5.1	286.3
2+00		5.2	286.2
+50		5.3	286.1
3+03 C		6.0	285.4
+50		7.3	284.1

			291.40			
0+9	3+56 24	6.15	290.13	7.42	283.98	
0+85	3+61 19			6.05	284.08	Bott of Ob
0+5	+61 24			5.55	284.6	Top of Ob
0+00	3+77 35			4.9	285.2	0.0 / 5° RT Top Bank
P	4+00			5.8	284.3	1.3 / 4° Rt Top Bank
	+50			6.4	283.7	5.1 / 8° RT
	+65	11.93	295.12	6.94	283.19	6.8 / 10° RT
	+71			11.8	283.3	180 / 10 Rt 11.6 / 10 Lt
				4.93	290.19	290.25 TBM
0+0						
+0						
+0						
+2						
+5						
1+00						
+5						
2+00						
+5						
3+03						
+50						

9.23
9.07
1.6

90.24
4.57
94.81
9.23
85.58

San Joaq. & Cross
SWBP 136.59
Travis
NW BP 212.21



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.16	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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