

66

TRANSIT

397

W79

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.14	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.71	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.

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11986

Crocker Quality

TRANSIT BOOK



No. 397

Rneeshaw

MANUFACTURED BY

H. S. CROCKER CO.

SAN FRANCISCO AND SACRAMENTO CALIFORNIA

MICROFILMED

JAN 20 1965

$$\begin{array}{r} 40 \\ 8 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 30 \\ 8 \\ \hline 240 \end{array}$$

$$\begin{array}{r} 32 \\ 180 \end{array}$$

$$32 \overline{)260}$$

- 1 10x10 - 5.50 Rvw
- 2 10x10 - 8 OP
- 1 6x12 - 14.2 OP with stringer
- 3 10x10 - 7 OP with gains
- 1 10x10 - 6.5 OP
- 1 10x10 - 8 OP with gains

TRAVEL BOOK

HICKORY
 281 BY 114

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Grades for End walls & Ditches
on slab at Saluzu Farm Wash

535		10000
10535	778	9757 ✓
	500	10035
10145	505	10030 =
9575	115	9385 ✓
<u>560</u>	597	9938
	97	9865
	39	10145
	70	9835
		9785

Wm. S. Kelley
7-26-16

- = assumed elev of wall at sink end
- = bottom of east wash on south side ditch
- = ground on north side road
- = ground at edge cut north side ditch
- = bottom of east wash on north side road
- = Elev wall at west end
- = bot of west wash South side ditch
- = edge cut north side ditch
- = north side road.

Notes:

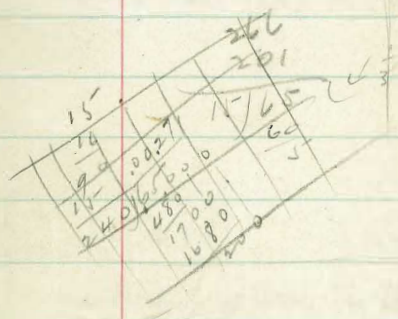
- cut 2.5 at edge of cut east wash
- cut 3.0 at north side road east wash
- cut 3.0 at north side road west wash
- cut 5.5 at edge of cut west wash.

Grades for Flume 3 Conduit ext.
 on final Runway Curve Location

Wrights
 Dilling 7-27-16 2

	grad Rod	Pin Rods.	Fill	
Be	266			
3C	2.01			
Burr #1	262			
#2	257			
#3	253			
#4	249	1176	9.27	9' 3 3/4"
#5	244	939	7.35	7' 2 1/2"
#6	240	969	7.29	7' 3 1/2"
#7	236	1377	11.41	11' 5"
#8	231			
#9	227			
#10	223			
#11	218			
#12	214			
#13	210			
#14	205			
#15	2.01 = 3C			

32/65
 64/100



Inspection Trip Dulzuna Conduit
 R. W. West - R. B. Dillen 7-27-16

Slabbing:

Sta	to Sta	necessary to prevent disintegration
✓ 315 + 39.3	316 + 20.1	80.8
✓ (Wall at west end contains:		2.31 cu yds)
✓ 227 + 89.5	227 + 63.65	
✓ (Wall at west end contains:		0.93 cu yds)
✓ (Wall at east end contains:		0.90 cu yds)
✓ 208 + 56.5	213 + 48.9	492.4
✓ (Wall at west end contains:		2.07 cu yds)
✓ (Wall at east end contains:		1.65 cu yds)

and Dulzuna Conduit Extension

necessary to prevent
 loose material and
 no sand from entering

In place this date
 original corr. H.O.B.

			80.8
			25.85
			25.85
			492.4
✓ 169 + 0.5	169 + 34.6	29.6	
✓ (Wall at west end contains		0.13 cu yds)	
✓ (Wall at east end contains		0.13 cu yds)	
✓ 148 + 50.2	148 + 94,	438	

* Road crossing.

memo for

HOB.

fix fencing.

85+363 plug original hole

connect lids on bridge cover & sections.

backing up on pylon^s,

patch culvert from settling basin.

memo for

work

4

quasi over on gate of upper diverting
dam

daily gaging at dam

clean screen from upper flow dam

clean up cut brush & carp waste

at piers.

can for 3 lengths 2" pipe at flow 12

can for steel gate at flow 12

4' bridge gate out to end

gate in fence.

Salvage steel 3' lumber cut from below

low diverting dam.

memo for Kirkwood.

Install gage at upper diverting dam
6x6 frame to hold grizzly in position
runing boards on flume.

Ladder or cleated runing boards at drop
fix deflector gate on turn 6 South side
broken cap for flume 5.

bridge to weir at settling basin
gage at weir at settling basin

5
misc.

Series of water samples from
morua to SD same day.

number plate for flume conduit end.
Runing gate stick to pierce

Morua weir for bay in present
(electrical indicator to tower - stilling
basin for for bay)
gauge soil for morua
water stage. Register for end conduit.

$$\checkmark 147 + 05 \quad 147 + 709 \quad 659$$

✓ (wall at west end contains: 1.12 m yds)

$$\checkmark 129 + 91.1 \quad 130 + 432 \quad 52.1$$

$$\checkmark 128 + 18.8 \quad 127 + 11.9 \quad 106.9$$

$$\checkmark 125 + 41.4 \quad 125 + 55.2 \quad 138$$

✓ (wall at west end contains: 0.50 m yds)

$$\checkmark 180 + 43.9 \quad 180 + 77.1 \quad 332$$

✓ wall at east end contains: 0.92 m yds

✓ wall at west end contains: 0.92 m yds

$$\checkmark 114 + 7.9 \quad 114 + 64.6 \quad 14.4$$

✓ wall at east end contains: 0.33 m yds

$$\checkmark 114 + 14.2 \quad 114 + 30.3 \quad 11.1$$

✓ wall at west end contains: 0.60 m yds

$$\checkmark 91 + 9.0 \quad 93 + 34 \quad 139.0$$

✓ (wall at west end contains: 0.72 m yds)

✓ (wall at east end contains: 0.55 m yds)

$$\begin{array}{r} 159 \\ 52 \\ \hline 659 \end{array}$$

$$\begin{array}{r} 89 \quad 27 \overline{) 160} \\ 432 \quad 32 \\ \hline 521 \quad 27 \overline{) 145} \end{array}$$

$$\begin{array}{r} 55 \quad 189 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 27 \overline{) 15.0} \\ 135 \\ \hline 15.0 \end{array}$$

= Pond crossing

✓ 76 + 60 77 + 223 623

✓ wall at east end contains 1 over yd

✓ wall at west end contains 210 cu yd

Dulzina conduct Cottonwood Branch

✓ Break in high 121' west 121

Wall at ditto location

(wall at west end contains 136 cu yd)

✓ 19 + 03 ± 19 + 191 ± 161

Wall at west end contains 0243 cu yd

Wall at east end contains 050 cu yd

Dulzina conduct

✓ B 13 + 358 B 9 + 72 3638

✓ ~~B 9 + 41~~ 8 + 78 ~~33~~ 63

✓ 10 + 07 11 + 50 143

✓ 16 + 78 16 + 57 21

✓ wall at east end contains 15 cu ft

✓ 16 + 98 19 + 80 282

(beside road below flume 6

735

27) 36.75 (.76

27
97
81
165

slabs 7' wide 6" thick

15.5

1.5
77.5

= Road crossing slabs 6" thick 8.7' wide

23.25
5.43

17) 116.25
108
82

8-1-16 Dilly-wrights

ditch 6.75' wide

ditch 5.75' wide

Road crossing

ditch 5.50' wide

ditch 6.00' wide

Beideman

clean up man & bridge (flume #1)

clean up at Wilson Creek

Earth in contact with timber

etc of flume #7

clean up blocking etc at flume 6

clean up around flume 8

Earth in contact with flume 9

Sauterbach

clean up at flume #12

Lane

flume # 348

Earth around flume 12 1/2

ore on screens

debris from flume posts

✓ 25+37	25+765	395
✓ 27+44	28+00	56
✓ wall w north end contain		5 mph
✓ wall w south end contain		5 mph
✓ 28+40	29+00	60
✓ 30+00	31+15	115
✓ 48+75	49+10	35
✓ 62+50	63+00	
✓ 64+12	64+85	73
✓ 66+85	67+25	
✓ 70+00	70+75	
✓ 75+00	75+60	
✓ 81+85	81+46	
✓ 82+12	82+33	
✓ 83+59	83+38	21
✓ 85+30	86+18	88
✓ 88+18	89+00	82
✓ 94+43	97+00	
✓ 100+18	100+48	

50
40
75
60
39
21
257
30

9

ditch 57' wide
ditch 56' wide

56
56
56
56
65
65
65
65
65
65
65
65
65
65
65

✓ 110+21	110+91	70
✓ Tunnel N		54 1/2 sq ft
✓ 131+06	131+45	60
✓ Open open but 2 nd & 3 rd slabs and of Roubidoux		15
✓ hole in slab #3		70
✓ 167+05	167+75	18 m ft
✓ wall at north end contains		20 m ft
✓ wall at south end contains		66
✓ 174+33	173+67	38
✓ 177+27	177+65	69
✓ 186+85	187+54	45
✓ 189+55	190+00	

Dulzina border 8-2-16

✓ 397+55	397+25	20
✓ between 2 slabs at 397		39
✓ 387+94	388+33	11 m ft
✓ wall at east end contains		25
✓ 372+90	373+15	15 m ft *
✓ wall at east end contains		

39

69

30

65

565

65

65

25' 86 45' 65

65

65

65

68

65

65

65

65

✓ 365+58	364+94	62
✓ wall of west end contains		162 m ²
✓ wall of east end contains		14 m ²
✓ 364+00	361+70	230
✓ 353+67	354	33
✓ 351+00	350+45	
✓ 318+88	318+52	36
✓ 313+10	313+28	18
✓ 310+00	309+54	46
✓ 304+65	306+00	+
✓ 299+00	300+00	100
✓ 292+18	291+90	38
✓ north end found 4		25
✓ wall of north end contains		10 m ²
✓ 265+27	265+97	70
✓ 264+73	264+37	36
✓ 263+25	261+45	180
✓ 259+10	258+68	42
✓ 256+10	255+25	85

230

55

135

65

65 Jap. end.

65 Shaker's house

65

65

65

65

65

65

65

65

65

65

65

65

✓ 254+95 254+59 36

✓ 253+90 253+40 30

✓ 248+00 248+60 60

Dulzina conduct amp³

✓ South end Tunnel 5 1/2 100

✓ North end Tunnel 6 150

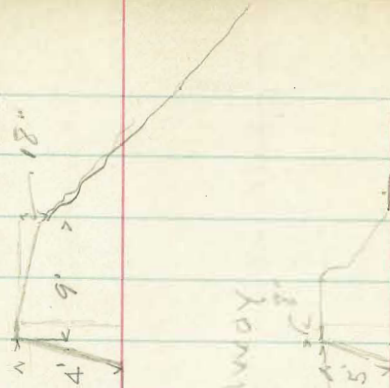
R. V. V. V.

Gage Readings W. S. Cook

Date	Hr	Upper Dam	Lower Dam
6-28	7 am	7"	10 1/2"
7-5	7 am	8 1/2"	9 1/2"
7-14	7 am	10"	9 1/2"
7-24	7 am	5 1/2"	7 1/2"
7-29	7 am	7 1/2"	11 3/4"
8-7	7 am	7 1/2"	11 1/2"
8-14	7 am	12"	11 3/4"
(wrest)	10:55 am		0.88'
(wrest)	11:15 am	0.87'	
		Settling Basin	
8-14	12:45 pm	1.17	wrest

Moreno Spillway

11-14-16
Wheeler Carrell
Swenson.



x-section Upper End Spillway



Drain to grade
toward west
quarry before

X sect Lower End

56'

3'±

x-section

64'

80'

35'

187'

Upper Scot.

10'

Lower Scot.

Laguna Trip 11-14-16

Monna	61.5
Warren's	69.0
Benton Junct	71.7
1 st Summit	73.9
Benton	77.2
Thing Ranch Hse	85.1
Joe Morris Ranch Hse	91.4
Joe Morris Ranch Hse	92.75
Joe Morris Ranch Hse	94.1
Little Laguna Lake	97.75
Pango station	98.15
Big Laguna Lake	99.25
Laguna Ranch	100.2
Big Laguna Lake	101.0
Little Laguna Lake	101.8
Joe Morris Ranch Hse	105.35
Joe Morris " "	106.7
Junction Morris Road	108.0
End Olive pipe Canyon	112.45

15

Thing Ranch Hse	114.0
Lower Thing Ranch Hse	115.25
Monna	137.65
Hatfield Junct.	139.3
Culver induction oaks	139.85
Zicklers Junct	140.55
Summit	140.85
Harvey Road Junct	?
Red Camp Road Junct	144.65
Julian Agency	152.2
Monna Junct	159.65
Camp	161.15
Monna Junct	162.6
Harvey Junct.	165.45
Pearson Ranch Junct	165.85
South end new road	166.15
Summit	166.4
Monna	169.6
Petro	188.2
Smith	195.3
Summit Junct	195.9

Oulzena 2022

Supervisors annual Report.

2 men for 1917 on day - Sunday
Paper Lin.

Gate & blowoffs in wood bridge

Patches in place and record

Stems in others.

107 actual count water stems in #1

Excavate open into N 95 #1

Drainage of Tunnels

Corr net lining beneath.

(20" x 20 spikes to green Monday)
5 velvet tubes for V. munda.

Tunnel #3 19 bad places attention

in gutter good shape.

Tunnel 4 19 bad places - lagging

of timber work needs attention

a 16' and a 20' section of square sets.

16
drain at north end of #4
needs opening up on outside.

3 and 4" air valves.

Dam at Woma

Finish slabbing

control

Winn & Ryzden

#1 & 2 tunnels conduct.

Upper Harrow Dam

Carbon paper for Cook.

Settlement and Recession
Morena Dam. 12-18-16.

condition OK - calm, cool, bright.
Wweste-Swenson-Symons.

R.P. No.	Normal	Reverse	Mean	Feet	Inc.	Dec.
1						
2	$8\frac{13}{16}$	$8\frac{3}{4}$	$8\frac{25}{32}$	7318	—	—
3	$8\frac{14}{16}$	$8\frac{25}{16}$	$8\frac{27}{32}$	7396	$\frac{1}{32}$ 0.0026	
4	$9\frac{1}{2}$	$9\frac{1}{2}$	$9\frac{1}{2}$	7917	$\frac{5}{64}$ 0.0065	
5	$11\frac{3}{16}$	$11\frac{3}{16}$	$11\frac{3}{16}$	9323		$\frac{1}{32}$ (?)
6	13	13	13	10833	$\frac{1}{4}$ 0.0208	
7	$13\frac{5}{16}$	$13\frac{5}{16}$	$13\frac{5}{16}$	11094	$\frac{2}{32}$ 0.0182	
8	$13\frac{3}{4}$	$13\frac{15}{16}$	$13\frac{27}{32}$	11536	$\frac{5}{32}$ 0.0130	
9	$13\frac{3}{4}$	$13\frac{7}{8}$	$13\frac{13}{16}$	11510	$\frac{2}{16}$ 0.0104	
10	$13\frac{13}{16}$	$13\frac{15}{16}$	$13\frac{7}{8}$	11563	$\frac{1}{16}$ 0.0052	
11	$14\frac{1}{4}$	$14\frac{5}{16}$	$14\frac{9}{32}$	11901	$\frac{1}{32}$ 0.0026	
12	$14\frac{1}{4}$	$14\frac{1}{4}$	$14\frac{1}{4}$	11875		$\frac{3}{32}$ (?)
13	$13\frac{3}{4}$	$13\frac{7}{8}$	$13\frac{13}{16}$	11510	$\frac{3}{16}$ 0.0156	
14	$12\frac{13}{16}$	$12\frac{3}{4}$	$12\frac{25}{32}$	10651	$\frac{3}{32}$ 0.0078	
15	$11\frac{1}{4}$	$11\frac{7}{16}$	$11\frac{11}{32}$	9453	—	—
16	11	11	11	9167	$\frac{3}{8}$ 0.0313	
17	$9\frac{7}{8}$	$9\frac{11}{16}$	$9\frac{25}{32}$	8157	$\frac{1}{32}$ 0.0026	
18	$9\frac{5}{16}$	$9\frac{5}{16}$	$9\frac{5}{16}$	8760	$\frac{1}{16}$ 0.0052	
19	$8\frac{7}{16}$	$8\frac{7}{16}$	$8\frac{7}{16}$	8031		$\frac{1}{16}$ (?)
20	$7\frac{7}{8}$	$7\frac{5}{8}$	$7\frac{3}{4}$	6458	—	—

R.P.			Elev	Elev 10-31-16		Fill to grade by new pins Dec Elev 157.16	
Bm	255½	157.75½	15520		Jan		
#1			540	152.36½	152.36½	0.01	4.80½
#2	257	154.89½	543	152.32½	152.33½	0.01	4.83½
#3			256½	152.33	152.34	0.01	4.83
#4			260	152.29½	152.30½	0.01	4.86½
#5			264½	152.25	152.26	0.01	4.91
#6	215½	154.33	272	152.17½	152.18	0.00½	4.98½
#7			275½	152.07½	152.09	0.01½	5.08½
#8			277	152.06	152.07½	0.01½	5.10
#9	207	154.14	226	152.07	152.08½	0.01½	5.09
#10			215	151.99	152.00	0.01	5.17
#11			216½	151.97½	151.99	0.01½	5.18½
#12	241½	154.40½	215	151.99	152.00	0.01	5.17
#13			239	152.01½	152.02	0.00½	5.14½
#14			236	152.04½	152.05	0.00½	5.11½
#15	3.14½	155.21½	233½	152.07	152.07½	0.00½	5.09
#16			308½	152.13	152.13	—	5.03
#17			303½	152.18	152.18	—	4.98
#18			290½	152.31	152.31	—	4.85
#19	276	155.07	269	152.38	152.38½	0.00½	4.78
#20			272	152.35	152.35	—	4.81
#21			277½	152.29½			4.86½
#22			279	152.28			4.88
#23			276	152.31			4.85
#24			269½	152.37½			4.78½
#25			265½	152.41½			4.74½
Bm			108	153.99			3.17
Bm			699	148.09			

2 to 0+00 & spillway wall

check

levels for Top Wall along Spillway

12-18-16

19

		15507	Elw.	Grade	Fill To Top New Wall
0	042	148.76	6.73	148.34	
#1 - sta	0+16.03	0.59	148.17	153.30	5.13
#2	0+41.1	1.59	147.17	152.22	5.05
3	0+66.1	2.64	146.12	151.25	5.13
4	0+90.95	3.70 $\frac{1}{2}$	145.05 $\frac{1}{2}$	150.08	5.02 $\frac{1}{2}$
5	1+15.95	4.69	144.07	149.00	4.93
6	1+40.05	5.70 $\frac{1}{2}$	143.05 $\frac{1}{2}$	147.97	4.91 $\frac{1}{2}$
7	1+64.25	6.75	142.01	146.93	4.92
8	1+91.15 = grade less 5 feet at lower end.	7.99	140.77	145.77	5.00
Bm		0.66	148.10	Bm = 148.08 ✓	
Sta	0+00 = grade upper end		153.91	153.99	0.00

	279½	157.99½	1550
107		563½	152.36
Cap south with dan		269½	
" 1		566½	152.33
" 3		566	152.33½
" 4		570	152.29½
" 5		574	152.5½

104 = 20-21

106 = 21-22

104 = 22-23

105 = 23-24

108 = 24-25

52.7
 481.27
 533.97

Sizes of Horse & mule shoes.

Bobby * 1 horse Maudie * 5

Dolly * 2 horse Queen * 7

L.O. 4 up mule * 4 mule Joe *

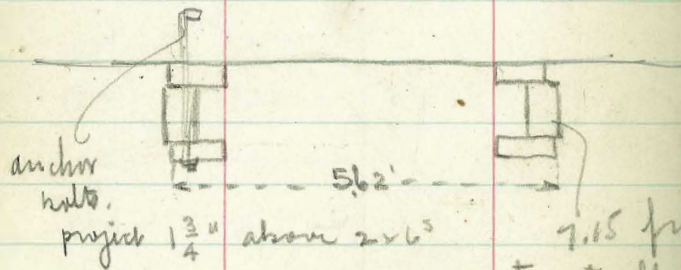
Gabe * 3 horse Buddy *

Notes for design of screen

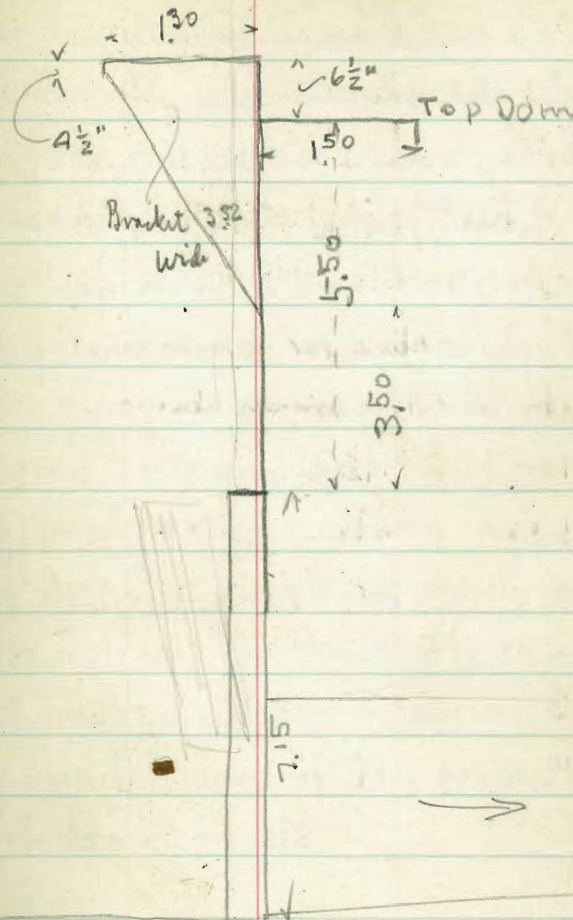
for Harry Dam. Intake chamber

outside to outside of 4x6^s 5.73 17'

outside to outside of 2x6^s 5.62 7 1/2'



7.15 from top to floor of intake and stand $6\frac{1}{2}$ inches above water with dam full



Send carbon copy of So dicata
report to City atty.

Refrain beginning of second report.

Get list of instruments for Mr. Ironwell.

Get measurements of screen for water
wall at Harvey Dam.

Mona gate combinations:

#1	195
# 1 2	377
# 1 2 3	480 483 ²⁸⁸
# 2	483 182
# 3	182 148
# 4	148 116
# 5	87

1-28-17 Wueste - Rimbey
22

Mona Spillway Sill

Axial length reconstructed sill 118.48

Top width sill 2'0"

Up-stream side plumb (117.99' long)

Down-stream side $\frac{1}{2}$ to 1 batter.

Sill has crest clew above cross-section
of spillway channel at this point
varying bet one and two feet.

Behavior of water running nine
feet deep at south-westerly end
problematical. Southwesterly ten
feet might discharge a diminished
flow due to curve of dam projecting
out in front of sill.

Elevations for Effective
Spillway cross-section during
period between destruction of
old sill and construction of
sack dam and subsequent
construction of new sill.

Sta.	BM	15146	Elev.
0	546	151.46	146.00
+5		73	✓ 144.15
+10		73.5	✓ 44.10
+15		75	✓ 43.90
+20		74	✓ 44.05
+25		75	✓ 43.95
+30		72.5	✓ 44.20
+35		72	✓ 44.25
+40		75	✓ 44.70
+45		63.5	45.10
+50		670	44.75
+55		71	44.35
+60		69	44.55
		68.5	44.60

15146	Elev.	23
+65	69	144.55
+70	71	44.35
+75	70	44.45
+80	68.5	44.60
+85	68.5	44.60
+90	69	44.55
+95	68	44.65
	67	44.75
+05	66	44.85
+10	61	45.35
+18		46.50

Notes on Carduit 1-31-17

Telephone after measures.

Saw 3 birds around flower feeding

Repair on Salazar Pouch - filling after

Salazar trees - now bristled.

About a dozen flower feeding near station.

Notes on Settlement of Moravia Dam

(First notes on new R.P.s on 5 foot crest altitude)

R.P. No.	488	160.08	155.20
*1			285½ 157.22½
	269	159.91½	
*3			264½ 157.21
	229	159.56	
*5			235 157.21
	260½	159.81½	157.30½
*7		159.96	251 157.29½
	265½	159.95½	
*9			159.26 157.25½
	254½	159.80½	
*11		159.90	261 157.19½
	270½	159.89½	
*13			157.16 157.15½
	264½	159.80½	
*15		159.86	250½ 157.29½
	256	159.85½	
*17			157.19 157.18½
	255½		267 157.58½

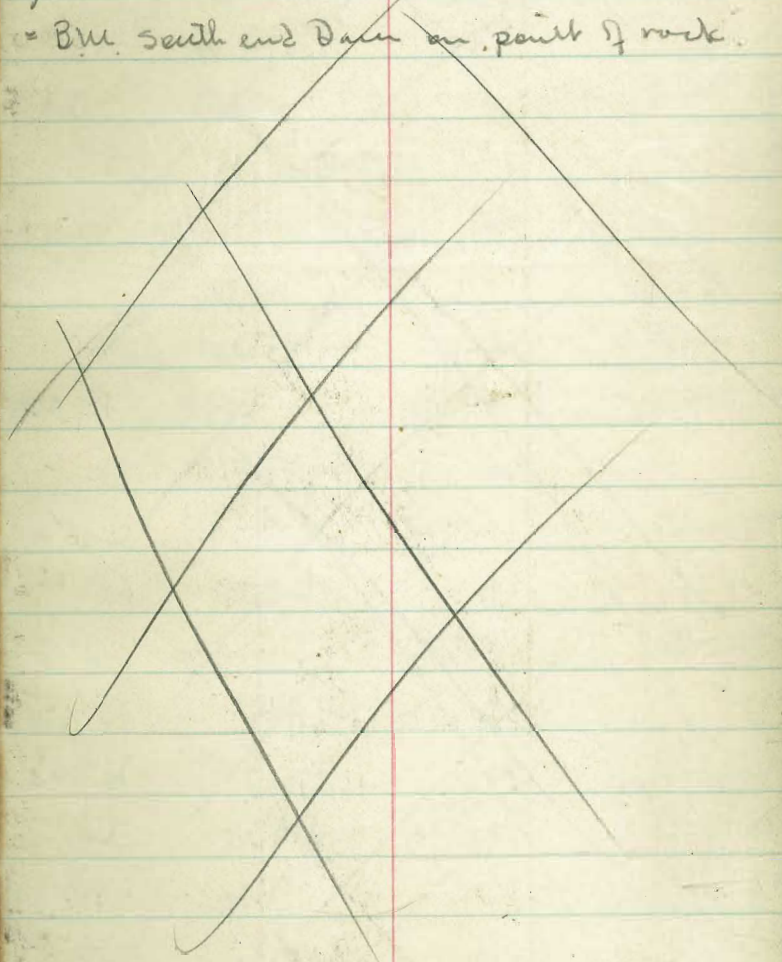
March 4th 1917

Wm. R. R. R. R.

25

Moderate east wind

= B.M. south end Dam on point of rock



5

#19 307 ~~160.26~~ ~~160.25 1/2~~ 157.19
~~291 1/2~~ ~~292 1/2~~ ~~157.33 1/2~~
~~22 1/2~~ ~~159.59 1/2~~
 #20 298 160.20 1/2 237 157.22 1/2
 #18 290 160.23 290 157.30 1/2
~~292 1/2~~ ~~160.22 1/2~~
 #16 285 160.07 1/2 300 157.22 1/2 # 4
 #14 296 160.10 1/2 292 157.15
~~291 1/2~~ ~~157.14 1/2~~ # v
 #12 280 159.99 1/2 291 157.19 1/2
 #10 292 160.16 278 157.24
~~160.18 1/2~~ ~~157.23 1/2~~
 #8 284 160.07 1/2 292 157.23 1/2
 #6 286 157.21
~~157.20 1/2~~
 2560 1/2 ✓ 2558 1/2 ✓

1149 148 10 1/2 = Bu N end epillwoysill (148.08)
 160.13 157.21
~~292~~ ~~160.12 1/2~~ ~~157.20 1/2~~
~~157.27~~
~~157.26 1/2~~
 # 4 286
 272 159.99 157.27
~~157.26 1/2~~
 272
 294 160.21 155.25
~~155.24 1/2~~
 8.59 ✓ 496 1/2
 10.55 ✓
~~157.21~~
~~146~~
~~157.25~~
~~157.20 1/2~~
~~196~~
~~157.24 1/2~~

Notes on Settlements of Niagara Dam
 First notes on new R.P.s on 5 foot crest addition

March 4, 1917. ^{Windy} ~~moderate~~ ^{moderate} west wind 27
 15998½

Bm. south end dam	496½	160.16½	155.20	*16	278½	157.20
*1		294	157.22½	*17	281	157.17½
	300	160.22½		292½	160.10	
*4		300	157.22½	*18	282	157.28
	296½	160.19	157.19½	19	278	157.32
*6		302½	94	20	290	157.20
	285	160.02		Bm north end spillway.	1202	(14808) 148.08
*8		281½	157.20½			
	290	160.10½		*8	300½	160.21
*9		285½	157.25	*7	291	157.30
*10		290	157.20½	*6	304	157.17
*11		292	157.18½	*5	300	157.21
	295	160.13½		302½	160.23½	
*12		297	157.16½	*4	300½	157.23
*13		298½	157.15	*3	296½	157.27
*14		301	157.12½	*2	300½	157.23
	286	159.98½		306	160.29	
*15		270	157.28½	*1	306½	157.22½
		20.41		Bm	508½	155.20½
	22.49					(15520)

Seems to determine location of chlorine
house at 8.0. so that a gravitic feed

	257	7252		6995
0			203	7049
	1266	8315		
0			072	8243
	1251	9494		
0			010	9484
	1226	10710		
0			143	10567
	1238	11805		
0			102	11703
	1210	12913		
0			400	12513

6995
5518
12513

64.48 ✓

9.30 ✓

3-23-17

29

can be used. Wants, Carroll

= elev to 2 gauge on testing stand
in Filter House

= Top upper band on 1st collar exposed
on 24" machine banded W.S. pipe
below road.

Note: Distance from filter test water
tap on 24" C.S. west of building to ground
elev 124.7 along 24" W.S. pipe below road
= 420' ±

Notes on Settlement of Morana Dam

Opriadeh 21 str

1917 Wm
Sumner

30

Bm	4.92	160.12	155.20	284½	160.17½	condition good	30
2			2.90	157.22	20	157.20½	20
	2.76	159.98		313	160.33½		
4			2.75	157.23	19	157.32½	32
	2.82	160.05		285½	160.18		
6			2.88	157.17	17	157.18	17½
	2.88	160.05		2.82	160.00		
8			2.85	157.20	15	157.29	28½
	2.84½	160.04½		2.57	159.86		
10			2.84½	157.20	13	157.15	15
	2.76½	159.96½		2.85½	160.00½		
12			2.81	157.15½	11	157.18½	18½
	2.78	159.93½		2.82	160.00½		
14			2.82	157.11½	9	157.25	25
	2.84	159.95½		2.83	160.08		
16			2.76	157.19½	7	157.30	20
	2.92½	160.12		2.77	160.07		
18			2.84	157.28	5	157.21	21
	2.53½ ✓		2.545½ ✓		2.54½ ✓	2.561½ ✓	

	2.95	160.16	157.21	
3			288½	157.27½

	2.92	160.19½		
1			296	157.23½

	3.10½	160.34		
Bur			513	155.21 ✓ (155.20) ✓

27.53½	25.45½
25.54½	25.61½
8.97½	10.97½
<u>62.05½</u>	<u>62.04½</u>

~~8.97½~~

10.97½

Notes on Revision of Monera Dam

April 20th 1917

32

Wrest, Swenson Pennington.
condition fair

R.P.No	normal	Mean	Revised	inches	R.P.No	normal	Revised	inches	inches
1	12 $\frac{1}{2}$ "	1.0208	12 $\frac{1}{2}$ "	12 $\frac{1}{2}$ ✓	18	12 $\frac{3}{8}$	12 $\frac{3}{8}$	12 $\frac{5}{16}$	16
2	13	1.0833	13	13 ✓	19	(1.0313)	11	11 $\frac{1}{8}$	X
3	13 $\frac{5}{8}$	1.1354	13 $\frac{5}{8}$	13 $\frac{11}{16}$ X	20	(.9167)	10 $\frac{1}{4}$	10 $\frac{3}{8}$	X
4	14 $\frac{1}{2}$	1.2083	14 $\frac{1}{2}$	14 $\frac{1}{2}$ ✓		(.8542)			
5	16 $\frac{1}{4}$	1.3542	16 $\frac{1}{4}$	16 $\frac{1}{16}$ $\frac{3}{16}$					
6	17 $\frac{5}{8}$	1.4688	17 $\frac{5}{8}$	17 $\frac{11}{16}$ $\frac{1}{4}$					
7	18 $\frac{1}{4}$	1.5208	18 $\frac{1}{4}$	18 $\frac{1}{16}$ $\frac{3}{16}$					
8	18 $\frac{3}{8}$	1.5313	18 $\frac{3}{8}$	18 $\frac{1}{8}$ $\frac{5}{8}$					
9	18 $\frac{1}{2}$	1.5208	18 $\frac{1}{2}$	18 $\frac{1}{16}$ $\frac{3}{16}$					
10	19 $\frac{5}{8}$	1.6354	19 $\frac{5}{8}$	19 $\frac{1}{8}$ $\frac{1}{8}$					
11	20	1.6667	20	19 $\frac{3}{4}$ $\frac{1}{4}$					
12	19 $\frac{1}{2}$	1.6250	19 $\frac{1}{2}$	19 $\frac{1}{2}$ ✓					
13	19 $\frac{1}{4}$	1.6042	19 $\frac{1}{4}$	19 $\frac{1}{16}$ $\frac{3}{16}$					
14	19	1.5833	19	18 $\frac{3}{8}$ $\frac{1}{8}$					
15	17 $\frac{1}{4}$	1.4375	17 $\frac{1}{4}$	17 $\frac{1}{4}$					
16	15 $\frac{1}{2}$	1.2917	15 $\frac{1}{2}$	15 $\frac{3}{16}$ $\frac{1}{16}$					
17	13 $\frac{5}{8}$	1.1354	13 $\frac{5}{8}$	13 $\frac{1}{2}$ $\frac{1}{8}$					

- Copy -
 notes on settlement of Monroe Jan 3

August 28, 1907 Wash, D.C. near Allie.
 clear, brisk west wind.

33

Bill	5.01	160.21		155.20		3.16	160.34		157.18
" 1			298 $\frac{1}{2}$	157.22 $\frac{1}{2}$	23 $\frac{1}{2}$	" 19		3.01	157.33 32 $\frac{1}{2}$
	2.91	160.13 $\frac{1}{2}$				3.16	160.19		
" 3			2.87	157.26 $\frac{1}{2}$	27 $\frac{1}{2}$	" 20		3.27 $\frac{1}{2}$	157.21 $\frac{1}{2}$ 20 $\frac{1}{2}$
	2.84	160.10 $\frac{1}{2}$				2.95	160.16 $\frac{1}{2}$		
" 5			2.90 $\frac{1}{2}$	157.20	21	" 18		2.87 $\frac{1}{2}$	157.29 28
	2.91	160.11				2.93 $\frac{1}{2}$	160.22 $\frac{1}{2}$		
" 7			2.82	157.29	30	" 16		3.02	157.20 $\frac{1}{2}$ 14 $\frac{1}{2}$
	2.91	160.20				2.76 $\frac{1}{2}$	159.97		
" 9	Under SE in Fort		2.96	157.24	25	" 14		2.84 $\frac{1}{2}$	157.12 $\frac{1}{2}$ 11 $\frac{1}{2}$
	2.90 $\frac{1}{2}$	160.14 $\frac{1}{2}$				2.85	159.97 $\frac{1}{2}$		
" 11			2.97	157.17 $\frac{1}{2}$	18 $\frac{1}{2}$	" 12		2.81	157.16 $\frac{1}{2}$ 15 $\frac{1}{2}$
	2.87 $\frac{1}{2}$	160.05				2.81	159.97 $\frac{1}{2}$		
" 13			2.91	157.14	18	" 10		2.77	157.20 $\frac{1}{2}$ 20
	2.86 $\frac{1}{2}$	160.00 $\frac{1}{2}$				1.53 $\frac{1}{2}$	158.74		
" 15			2.72	157.28 $\frac{1}{2}$	29	" 8		1.53 $\frac{1}{2}$	157.20 $\frac{1}{2}$ 20
	2.76 $\frac{1}{2}$	160.05				3.06 $\frac{1}{2}$	160.27		
" 17			2.87	157.18	18	" 6		3.09	157.18 17
	27.99 ✓		26.01 ✓			25.23 ✓		25.23 ✓	

- Copy -

Notes on Mission of Monna Jan
8-29-17 United Mission, Pat. Dillon³⁴

				Drive	Run	Man
#1	294 ^{1/2}	160.22 ^{1/2}	157.18	12 ^{3/16}	12 ^{3/16}	1.0156
	288 ^{1/2}	157.24	23	12 ^{15/16}	12 ^{7/8}	1.0755-12 ^{29/32}
#2	298 ^{1/2}	160.22 ^{1/2}		13 ^{9/16}	13 ^{9/16}	1.1302
	298 ^{1/2}	157.24	22	14 ^{7/16}	14 ^{7/16}	1.2031
	313	160.37		16 ^{1/16}	16 ^{1/16}	1.3385
B.M.	5/6	155.21	(20)	17 ^{4/16}	17 ^{4/16}	1.4335
	9.06 ✓	11.03 ✓		18 ^{5/16}	18 ^{3/16}	1.5208-18 ^{1/2}
				18 ^{5/16}	18 ^{5/16}	1.5260
				18 ^{1/2}	18 ^{7/16}	1.5182-18 ^{7/32}
				19 ^{7/16}	19 ^{7/16}	1.6198
				19 ^{7/8}	19 ^{7/8}	1.6563
				19 ^{7/16}	19 ^{7/16}	1.6198
				19 ^{5/8}	19 ^{5/8}	1.5938
				19 ^{1/16}	19 ^{1/16}	1.5985
				17	17	1.4167
				15 ^{5/16}	15 ^{5/16}	1.2760
				13 ^{1/2}	13 ^{1/2}	1.1250
				12	12	1.0000
				11	11	.9167
				9 ^{13/16}	9 ^{13/16}	.7177

Levels at Flume 17
Duzina contour.

on Packing near 525
on Platform in Flume 17 547

Levels for contours east of
No. 1 Filtration Plant.

BM	1.18	71.13		6995
o	2.40	63.31	1022	6091
			890	54.41
			390	59.41
o	11.27	73.22	136	61.95
			881	64.41
			381	69.41
o	11.51	83.20	153	71.69
			879	74.41

12-11-17
Went to Sam

35

34
136
22
52
12

Went to - Roben

1-22-18

= dr. gage on testing stand.

= ground level at S.E. cor Filtration Plant

= first 5 ft contour

= second 5 ft contour

= third 5 ft contour

34
15
22
52
12
879

Transit and Stadia Positions

Stadia Dist. ht

Rt

of CP's east of Filtration Plant

20 cont

65

91° 50' ✓

(Instrument Position on axis of building)

41

34° 59' ✓

33 feet east of east line of garage

✓

62

94° 51' Top cor int ✓

Stadia Dist

angles left

angles right

113

120° 43'

✓

0 station

51

116° 47'

✓

25 cont

75

33° 00' ✓

52

118° 10' ✓

151

116° 12' ✓

5 cont.

52

115° 04' ✓

30 cont

159

107° 00' ✓

31

21

164° 32' ✓

✓

63

26° 51' ✓

0

51

111° 30'

✓

81

8° 21' ✓

10 cont

134

155° 30' ✓

✓

137

102° 08'

✓

54

106° 00' ✓

25 cont

109

107° 16'

✓

0

54

107° 09'

✓

Drum

109

144° 30' ✓

✓

100

144° 06'

edge int ✓

✓

66

91° 05' ✓

✓ 15 cont

80

129° 04'

edge int ✓

✓

51

102° 45' ✓

0

57

99° 26'

cor int ✓

✓

67

54° 50'

✓

56

cor int

97° 40' ✓

✓

70

87° ±

69

edge int

118° 39' ✓

✓

76

116° 30' ±

121

141° 25' ✓

✓

✓ 20 cont

121

126° 24' ✓

✓

Levels for Cross-section
Water-side Samul Ranch Weir

B.M.	450	104.50	100.0	= Assumed elev.
0+94 ✓			1.1	103.9
0+97 ✓			28	101.7
1+05 ✓			32	101.3
1+12.5 ✓			5.0	99.5 = Transit station
1+19 ✓			4.8	99.7
1+22 ✓			6.5	98.0
1+33.5 ✓			7.3	97.2
1+40 ✓			7.1	97.4
1+50 ✓			6.0	98.5
1+50 ✓			8.2	96.3
1+56 ✓			9.0	95.5
1+59 ✓			7.0	97.5
1+67 ✓			7.4	97.1
1+66 ✓			6.4	98.1
1+70 ✓			7.1	97.4
1+75 ✓			5.0	99.5
1+79 ✓			5.5	99.0
1+79 ✓			6.6	97.9

104.50

101.2
4.3
96.9

1+83.5 ✓ 79 96.6

1+88 ✓ 10.4 92.1

1+92 ✓ 79 96.6

1+93 ✓ 48 99.7

1+95 ✓ 33 101.2

1+99.5 ✓ 52 99.3

1+99.5 ✓ 40 100.5

2+04 ✓ 5.0 99.5

2+04 ✓ 6.5 98.0

2+05 ✓ 6.6 97.9

2+05 ✓ 7.7 96.8

2+10.5 ✓ 8.0 96.5

= intersection of bed rock with earth bank.

2+10.5 ✓ 4.6 99.9

2+17 ✓ 3.5 101.0

0 8.61 112.85 0.26 100.24

0+60 ✓ 7.5 105.35

0+08 1.8 111.05

2+33 ✓ 5.0 107.85

Levels for Pipe and Ditch
Cottonwood Diverting Dam

Floor-line
Grade

39

3-1-19

Wueste - Watts

Stream-bed Ctr of Dam site.

	1123	11123		100.0
St 0+00			41	107.1
+25			45	106.7
+50			50	106.2
+75			47	106.5
1+00			45	106.7
+25			42	107.0
+50			39	107.3
+75			40	107.2
2+00			44	106.8
o +25	072	106.98	4.97	106.26
+50			3.9	103.1
+75			4.9	102.1
3+00			4.9	102.1
+25			5.0	102.0
+50			4.3	102.7
+75			4.4	102.6

102.92

Intake

1/5 ft



9° Lt.

102.47

End 24" W.S. Pipe =
beginning of ditch bed

11.95 ✓

4.97 ✓

Flow-line
Grade

.40

525	300
.01	.08
<u>.0525</u>	<u>.2400</u>
24	825
<u>.765</u>	<u>.15</u>
101.68	4125
<u>102.545</u>	<u>825</u>
	12375
	<u>101.68</u>
	1029.175

10698

4+00			54	101.6
+25			54	101.6
+50			53	101.7
+75			55	101.5
5+00			58	101.2
0+25	6.13	106.58	6.53	100.45
+50			55	101.1
+75			61	100.5
6+00			5.9	100.7
+25			63	100.3
+50			66	100.0
+75			63	100.3
7+00			5.5	101.1
+25			52	101.4
+50			4.9	101.7
+75			4.8	101.8
8+00			4.9	101.7
8+29			4.90	101.68
8+25	6.13		1.64	104.94

11° Lt

Bottom of concrete box at Wye
Top outside concrete rd at Wye =
End ditch sect

B.M.	101	105.95		104.94	
	523	106.44	4.74	101.21	
	914	112.18	3.40	103.04	
Sta 2+25	15.38	6.48	185.70	103.28	2.72
2+00		5.56	106.62	103.30	3.32
1+75		5.02	107.16	103.32	3.84
1+50		4.81	107.37	103.34	4.03
1+25		5.25	106.93	103.36	3.57
1+00		6.20	105.98	103.38	2.60
0+75		5.70	106.48	103.40	3.08
0+50		6.08	106.10	103.42	2.68
0+25		7.56	104.62	103.44	1.18
0+00		5.45	106.73	103.46	3.27

$$\begin{array}{r} 101.68 \\ + 1.00 \\ \hline 102.68 \\ + 6 \\ \hline 103.28 \end{array}$$

$$\begin{array}{r} 8.129 \\ + 2.625 \\ \hline 10.754 \\ + 0.04 \\ \hline 10.794 \end{array}$$

Lower Stay Levels

41.

Presently Diller's notes found on camp of
 paper & copies into this book by R. Wash 9-8-17

031	486.879		486.569
184	481.369	735	479.529
114	475.679	688	474.489
		445	471.229

Bottom of Spillway

049	487.059		486.569
12.45	498.739	077	486.289
		386	494.879

Bye on Run via.

connection bet Pump Discharge Line

and U.O. - P.O. Line

42

Went, Bellamy Canal

3-15-17

Point on U.O. - P.O. Line about 65' upstream
from 24x24x12 tee

Note: 558' of 24" WS. machine banded
pipe available from joint
assumed as sta 0+00 to C.I.

Pipe at Pump House.

Note: Point assumed as sta 0+00
also equals P.C. of curve of
40'40" deflection in 20 feet to
right in pump line.

Sta	Deflection angle left	BS
+41		
4	23°20'	
+75	23°20'	
+50	23°20'	
+25	23°20'	
3	23°20'	Sta 1+75
+75	56°00'	
+50	51°20'	
+25	46°40'	
2	42°00'	
1	37°20'	Sta 0+00
+75	32°40'	
+50	28°00'	
+25	23°20'	
1	18°40'	
+75	14°00'	
+50	9°20'	
0+00 = B.C.	4°40'	Tangent of 24" WS line from Tunnel

Monera.

Bms

Monera south end 155.20 = Point of Pt

Monera Spillway 148.08 = Top axle

grades.

Top new pipe 157.16

44

15'± west of main plate about 1' from ^{Rock wall} ~~Point~~
North end Spillway cill.

Outlet Discharges at Monona
Passage water to Swan Lake.

Date	Hour	min (h)	corrected to		Remarks	
			H.L.	R.R. Elev.		
June 28	2:10 P.M.	8"	7.24	7.50	.74	opened as shown
29	12:30 P.M.					closed altogether
July 7	✓ 8:15 P.M.	4 $\frac{1}{2}$ "		7.79	.45	opened as shown
8	✓ 6:30 P.M.	5 $\frac{1}{4}$ "		7.71	.53	opened as shown
12	✓ 5:00 am	6 $\frac{5}{8}$ "		7.63	.61	opened as shown
17	✓ 9:30 P.M.	6 $\frac{5}{8}$ "		7.59	.65	opened as shown
21	✓ 12:30 P.M.	5 $\frac{9}{16}$ "		7.695	.545	closed as shown
24	✓ 3:05 P.M.	4 $\frac{9}{16}$ "		7.79	.45	" " "
27	✓ 11:30 am	5		7.74	.50	opened " "
29	✓ 12:00 M	6 $\frac{1}{2}$ "		7.595	.535	opened " "

Road-crossings of conduit extension.

Upper Salazar 8'3" wide

walls 6" thick

30° ± skew

2'0" top ditch to top wall

6" slab.

Lower Salazar 12'5" wide

walls 6" thick

45° ± skew

1'0" top ditch to top wall

6" slab

Manholes in extension leading

36" x 18" in diam

4" walls (6" above slab)

213+489 to 208+565

492'

165 cu yds in 3rd wall of Salazar for slab.

manhole at 212+479.5

" " 211+484.5

" " 210+463.5

" " 209+461.5

22.20
6.16
16.04
32.08
160.20

46
51.1
48.9

22.2 x 27" x 6"

2'4"

222

258

1776

1110

444

5727.5

286380

1604

27)44,678 (165

27

176

123

147

209 46.15
894
208 567.5

100.95

213+489

1 0.95

212+479.5

99.5

211+484.5

1 21

210+463.5

1 22

209+461.5

Station Supply & Tool Equipments.

July 26 1916

Monica
concrete powder
 Pipe tools
 cap
 road tools
 rock
 earth
 telephone
 blk. south
 horse spring
 concrete
 misc
 brush
 rusty
 rolling stock
 stock
 painter
 boot repair

House
concrete powder
 Pipe tools
 cap
 Road
 rock
 earth
 brush
 steel
 telephone
 blacksmith
 concrete
 rolling stock
 stock

Barnett
concrete powder
 pipe tools
 cap
 Road
 Rock
 earth
 telephone
 blacksmith
 horse spring
 concrete
 floor
 misc
 brush
 rolling stock
 stock

Lester back
concrete powder
 cap tool
 Rock
 earth
 telephone
 concrete
 floor
 brush

Dalyan Summit
concrete powder
 pipe tools
 cap
 Rock
 earth
 telephone
 concrete
 floor
 brush

Loren stay
concrete powder
 pipe tools
 cap
 Road
 Rock
 earth
 telephone
 blk. south
 horse spring
 concrete
 w.s. pipe
 misc
 brush
 painting
 m. h. u
 rolling stock
 surveying
 draughting
 gaging
 stock

Telegraph house

47
 earth
 brush
 blacksmith
 concrete
 w.s. pipe

Charles Deight
 pipe tools
 cap
 garden
 earth
 brush
 w.s. pipe
 rolling stock
 stock

Feltin Plant

SO. pump plant

5" hand pump

Systematization of Impounding System.

July 26 1916

Transfer slips	Boarding Camp test sheets
Meal sheets	Coagulant Records
Pump Records	
Water supply Records	
Slabbing Records	

0400 = Ctr Road
026. +8 = edge road
+14 fence
+60 breaks
+94 edge bank
2+33

Clean Settling Basins
Brush along roads
Install Cippolatti weirs.
Telephone repairs
Mule for Moreno
Hunting Licenses
Paper around toilets
Yard for toilet
New Swenson toilet
Pipe for Hauser

161	250	375	161
2	17	213	62
<u>805</u>	213	<u>162</u>	<u>9.9</u>
213			
4805	tant poles 12x19		
1610	3 mats		
1746	roofing paper		
4019	93 1" lumber		
<u>25165</u>			

520	178	330	200
3	103	103	37
<u>181</u>	<u>534</u>	<u>167</u>	<u>163</u>
	1067		177
	673		62
	<u>22010</u>		116
	5		167
	<u>165070</u>		812
	9686		606
	<u>1710193</u>		116
	26		<u>19372</u>
	254		<u>96860</u>
	243		
	<u>163</u>		

1745	197
17	
<u>170</u>	
18	
5	
<u>40</u>	
118	
132	
<u>250</u>	
444	
118	
<u>22066</u>	
11033	

802	17000	24
	802	85
	<u>169105</u>	<u>19.7</u>
	143	5.2
	147	<u>14.7</u>
	<u>1691050</u>	
	296	
	<u>169346</u>	

147	148140	1255
5	438	139
<u>735</u>	<u>104502</u>	<u>5440</u>
2736		381
277		395
22		<u>18605</u>
		166
		<u>18639</u>
		33.2
		<u>18077</u>

47 h	3100
18	147
<u>159</u>	
295	
181	
<u>1475</u>	
2368	
295	
<u>24595</u>	
27285	
112	
<u>31405</u>	