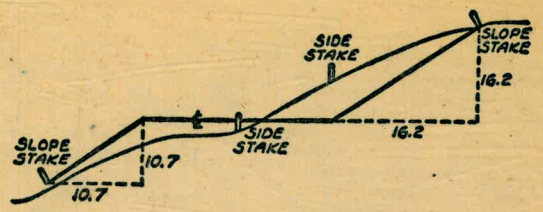
#790



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

54th St. S of Univ

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TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

SEMINOLE DRIVE
8" C.I. WATER MAIN GRADES
W.O. # 2-759-5
PROFILE 3700

JAN. 26, 1950
Beatty
Rogers
Finney

1

B.M	5.15	457.52		452.37		
PI						
0+00	7.68	465.19	0.01	457.51	456.0 451.5	
0+14			7.3	457.9	456.2 451.3	C6
0+56	B.C.		7.4	457.8	456.6 452.1	C5
+75			7.4	457.8	456.8 452.3	C55
1+00			6.9	458.3	457.2 452.7	C56
1+28.13	E.C.		6.1	459.1	457.4 452.9	C63
+50			5.9	459.2	457.6 453.1	C61
2+00			5.2	460.0	458.2 453.7	C63
+50			5.2	460.0	458.6 454.1	C59
3+00			5.2	460.0	458.9 454.4	C56
+50			5.3	459.9	459.0 454.5	C54
+83.45	B.C.		5.0	460.2	459.1 454.6	C56
PI 2"IP	2.29	462.65	4.83	460.36		
2+00			2.4	460.3	459.0 454.5	C58
+50			2.4	460.3	458.9 454.4	C59
5+00			3.2	459.5	458.7 454.2	C53

P.O.B. SW Cor Rolando & El Cajon

T/P 11.6 453.6 P.O.T. 7.31 455.88

Δ - 8°12' RT
T 36.13
R 504.00 = 4' offset
L 72.13

(10'E & ROAD)

F.H.

460.36 PI
3.20
463.56 ℄
5.06
458.50 (5) F.H
458.40
C0.10

Fd 6" Conc Mon 12' West of 4' offset line

SEMINOLE DRIVE
462.65

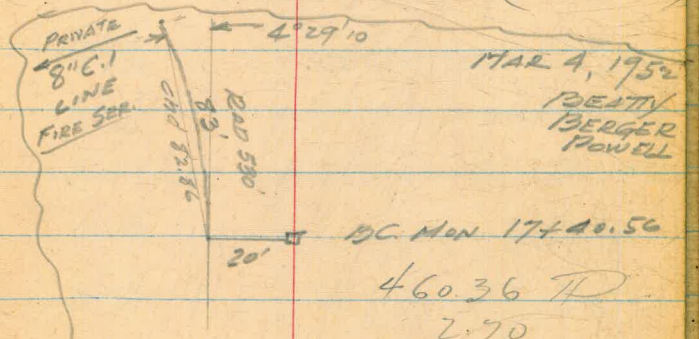
5+50			4.1	458.6	458.4 453.9
6+00			4.6	458.1	458.2 453.7
	FIRE HYDT (5)		4.4	458.3	458.2
+50			5.1	457.6	458.1 453.6
7+00			5.3	457.4	457.9 453.4
+50			5.7	457.0	457.7 453.2
7+96.00	EC.		5.8	456.9	457.6 453.1
(8+08.77	℄ RD E.C)				
+50			5.4	457.3	457.4 452.9
9+00			4.8	457.9	457.2 452.7
+50		9.07 467.55	4.17	458.48	457.0 452.5
10+00			8.5	459.1	456.9 452.3
+50			9.0	458.6	456.6 452.1
11+00			10.1	457.5	456.4 451.9
+50			12.0	455.6	456.3 451.8
12+00			11.0	456.6	456.5 452.0
	FIRE HYDT (3)		13.1	454.5	456.5
+50			10.6	457.0	456.9 452.4
13+00			9.6	458.0	457.5 453.0
+50			8.4	459.2	458.3 453.8
14+00			7.4	460.2	459.0 454.5

C47
C44
CO1
C40
C40
C38
C39

Δ 43°-17'-30" RT
R 546.00
T 216.58
L 412.55

FD CONC MON 9' NW - ℄ offset

(5' EAST ℄ RD)



C44
C52
C6°
C63
C65
C56
C38
C46
FE°
C46
C5°
C51
C57

BC MON 17+40.56
460.36 P
2.70
463.06 ℄
5.85
457.21
458.3 FL
Curb
GRD

SEMINOLE DRIVE

467.55

14+50		6.6	461.0	459.7 455.2	C58
14+81.3		6.0	461.6	460.2 455.7	C59
(15+30.3	P.I.	45° LT on ℄ pipe)			
15+28.68 BACK 15+31.72 AHEAD		4' offset	6.2	461.4	460.6 456.1	C53
2.1.32 (interval)					
15+53.24		6.2	461.4	461.2 456.7	C47
15+90.7 BC					
16+03.24		4.9	462.7	461.8 457.3	C54
16+53.24		4.4	463.2	462.9 458.4	C48
17+03.24		3.6	464.0	463.2 458.7	C52
17+05.3	FIRE HYDT. (5)	3.8	463.8	463.2	COC
+53.24		2.3	465.3	463.5 459.0	C63
	(DITCH	8.4	459.15)		
18+03.24		2.3	465.3	463.8 459.3	C60
+53.24		1.9	465.7	464.0 459.5	C62
19+03.24		2.2	465.4	464.2 459.7	C57
+53.24		1.8	465.8	464.4 459.9	C51
20+03.24		2.0	465.6	464.6 460.1	C55
+53.24		2.0	465.6	464.8 460.3	C53
20+71.74	END OF LINE CONN. TO 2" MAIN	2.2	465.4	464.9 460.4	C51
11	6.25	469.71	4.09	463.46	
CK BM			4.20	465.51	= 465.51

BP. NW Cor 63rd (Catection)

REPLACEMENT
54TH ST. PIPELINE
CHOLLA STATION ROAD TO EUCLID AVE

Mag. S 1°00' E
Orig.

1+14.68 E.C.

0+86.06 P.I. Δ = 8°00' LT
R = 410.67
T = 28.72
L = 57.34

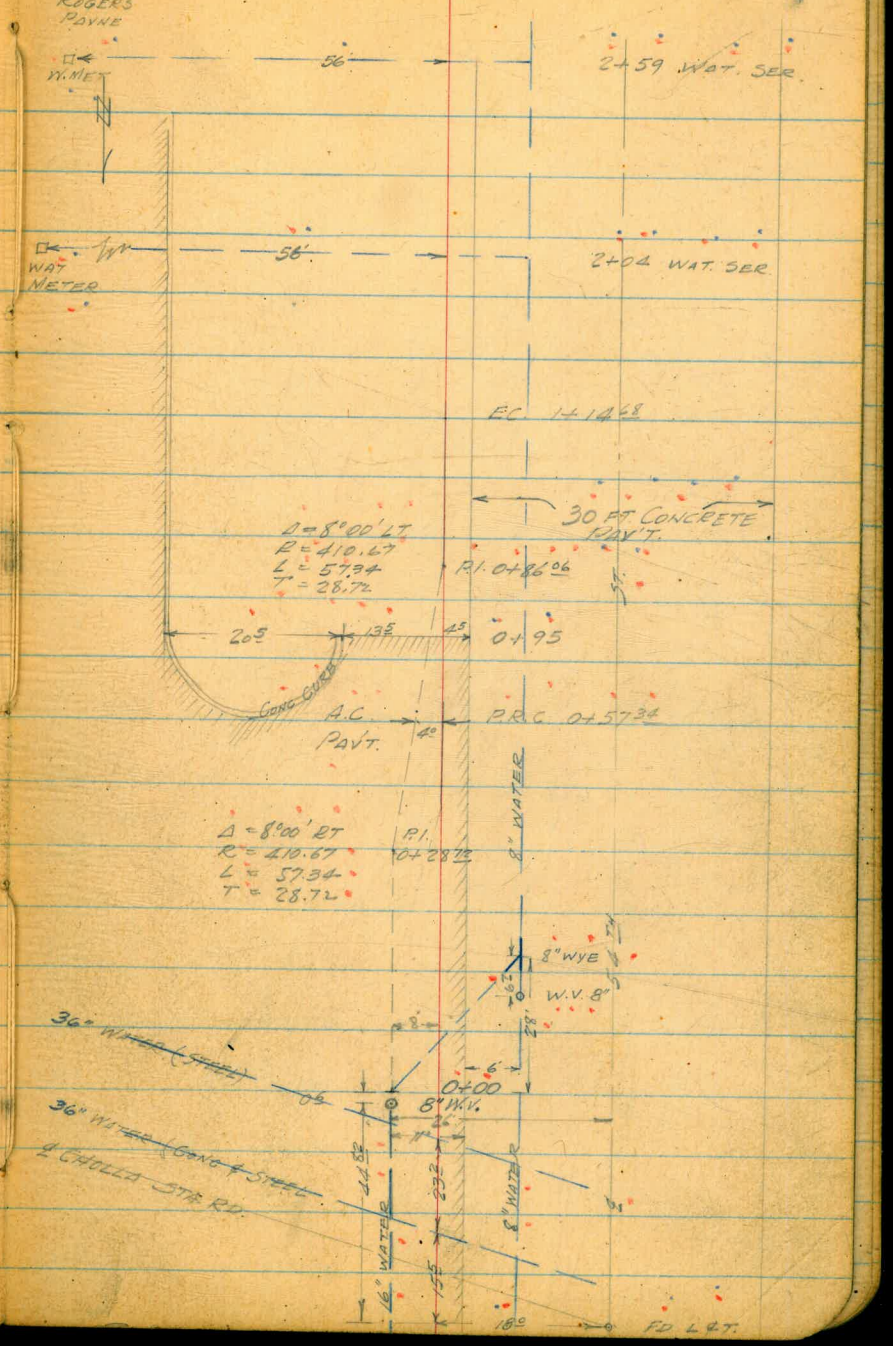
0+57.34 P.R.C.

0+28.72 P.I. Δ 8°00 RT
R 410.67
T 28.72
L 57.34

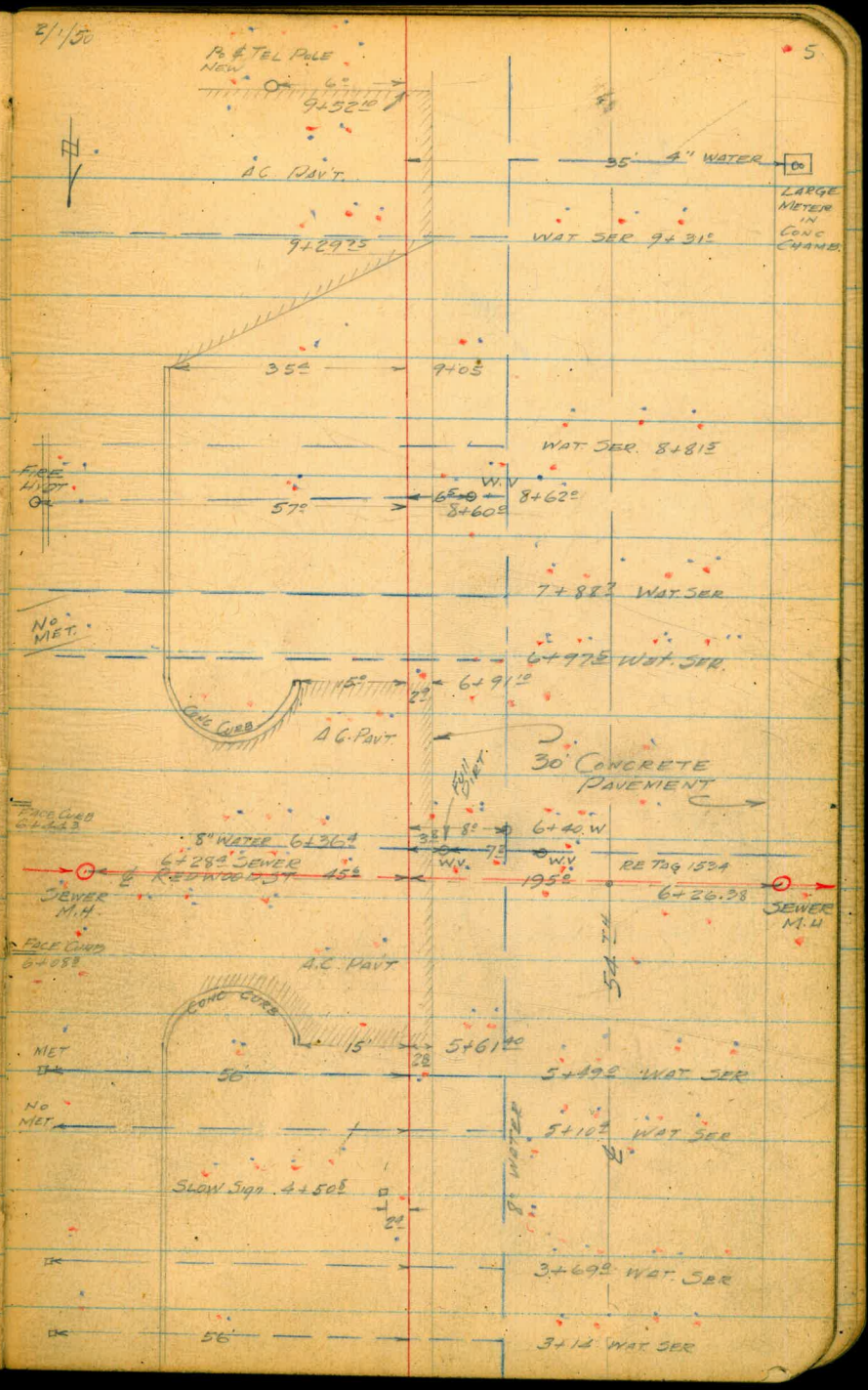
0+00 B.C.

JAN. 31. 1950 - COLD
BEATTY
ROGER'S
PAYNE

4



54TH ST. PIPELINE



54TH ST. PIPELINE

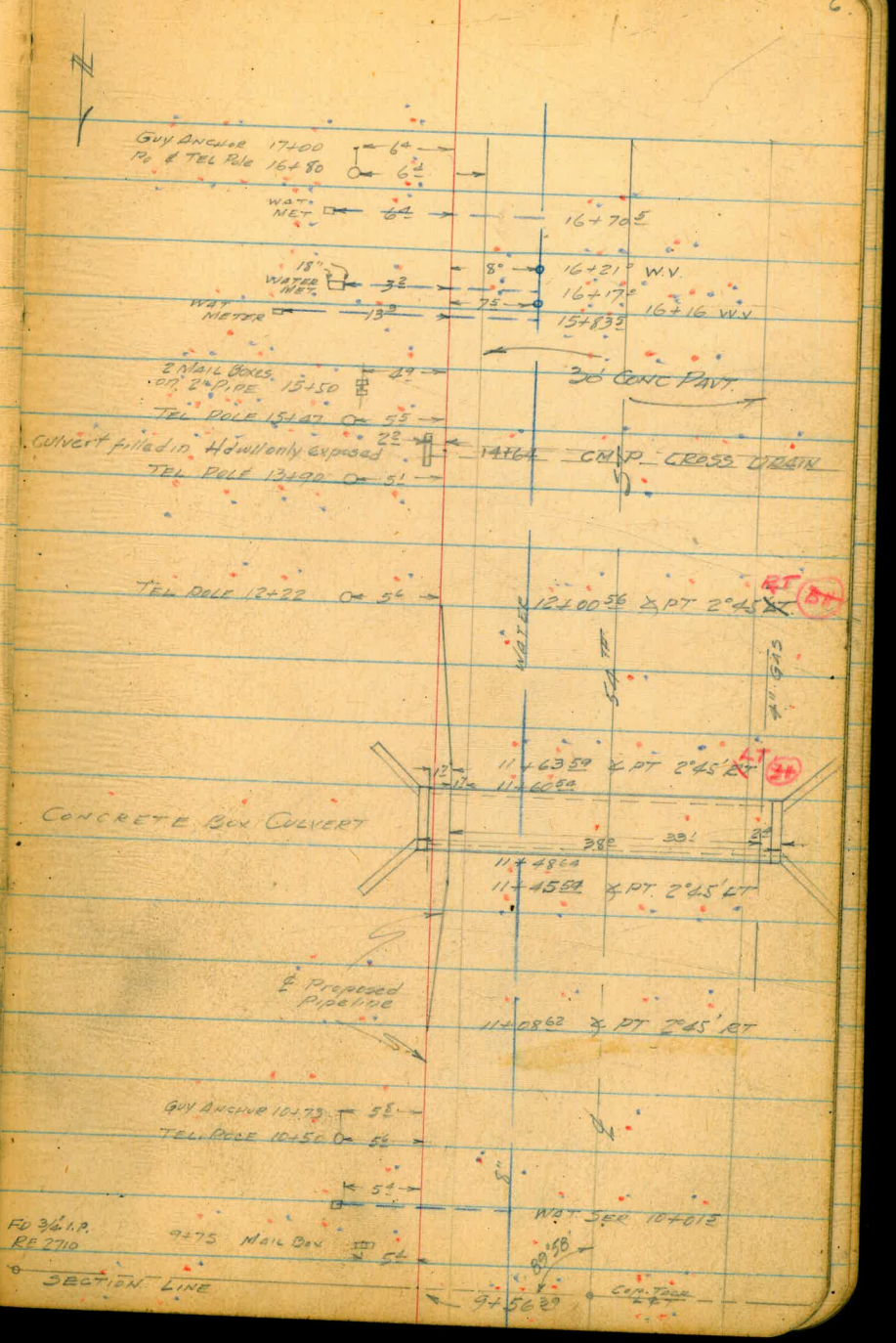
12+00 56 P.I. 2°45' RT

11+63 59 P.I. 2°45' LT

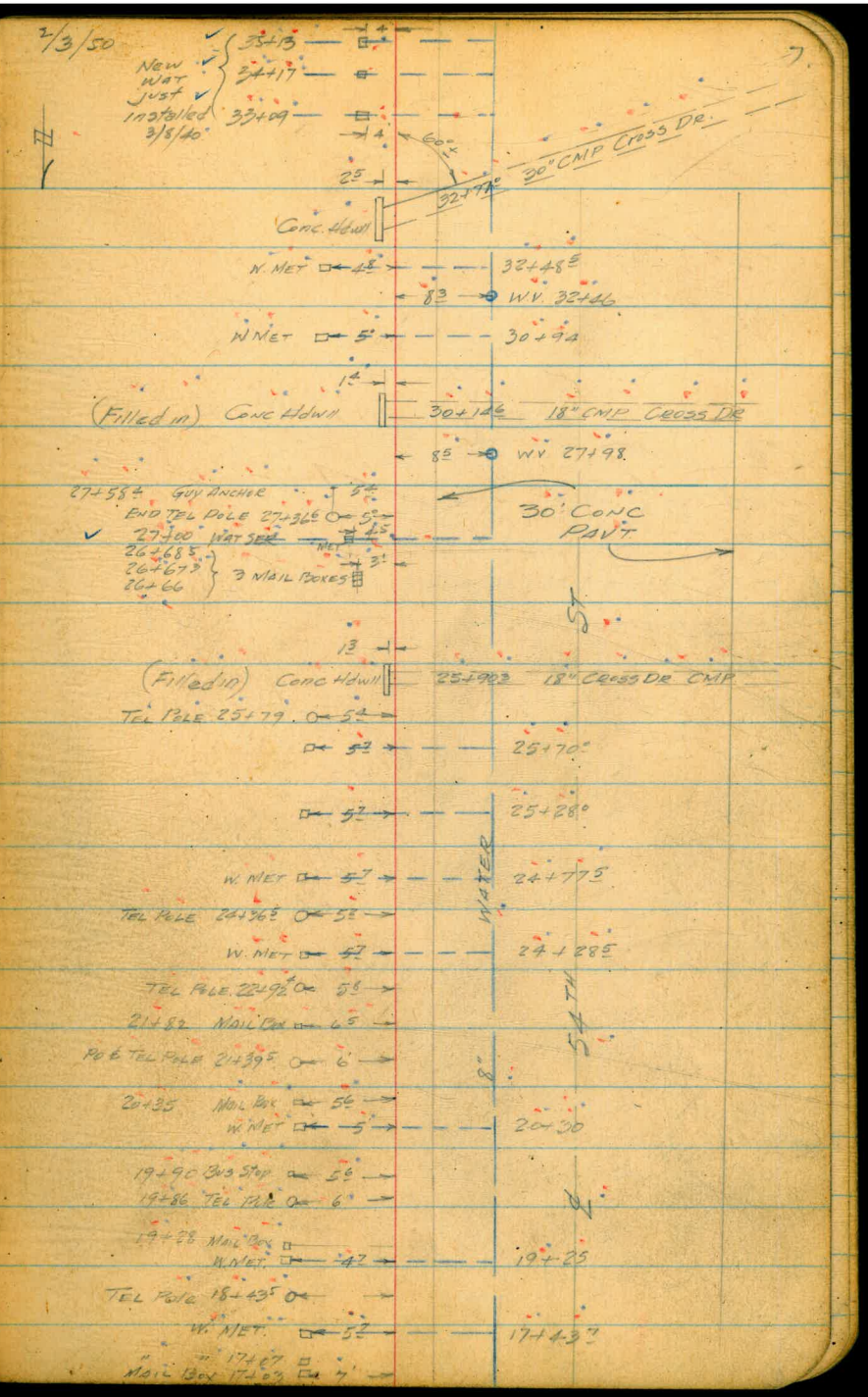
11+45 54 P.I. 2°45' LT

11+08 62 P.I. 2°45' RT

FEB 3 1950 (MILD)



54TH ST. PIPELINE



54TH ST. PIPELINE

MAG BRG S.36°00'W

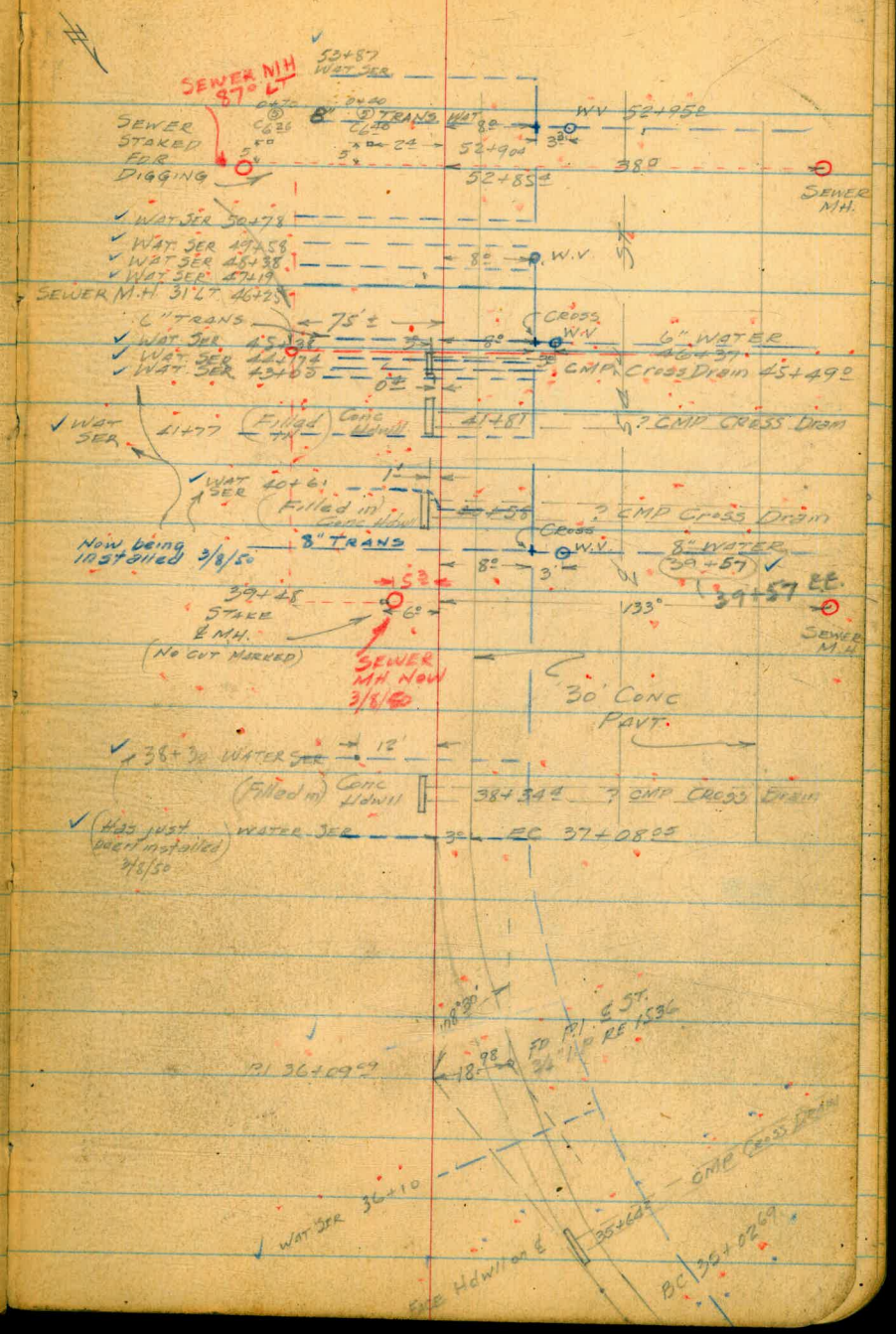
37+08.05 E.C

A = 37°00
R = 318.00
T = 106.40
L = 205.36

36+09.69 P.I.

35+02.69 B.C

MAG BRG S.1°00'E.



54TH ST. PIPELINE

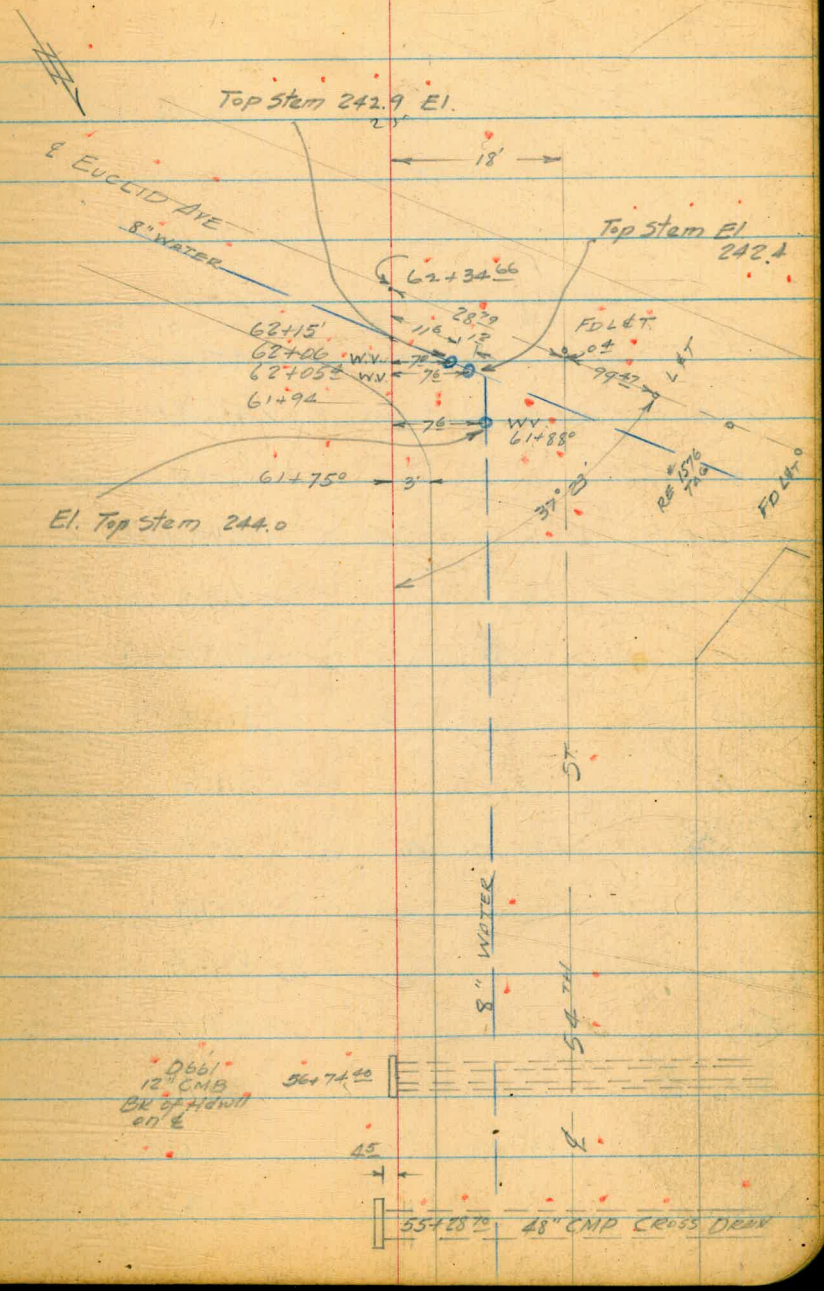
Mag Brg S 1°30' E

(37°23' LT)

62+34.66 Intersection ℄ Proposed Pipeline & ℄ Euclid Ave

62+15 End of Line

Mag Brg S 36°00' W



54TH ST.
CHOLLA STA. ROAD TO EUCLID
& PROFILE

BM.	0.68	314.52		313.84
"	6.57	308.27	12.82	301.70
"	11.44	316.56	3.15	305.12
"	5.10	321.46	0.20	316.36
			0.65	320.81
SET "			0.45	321.01
SET TBM.			5.49	315.97
0+00			1.35	320.1
			4.55	316.9
+57.34			3.59	317.9
+95.0			5.97	315.5
1+14.65			7.3	314.2
1+50			9.9	311.6
"	0.68	309.62	12.52	308.94
2+00			1.7	307.9
+50			5.2	304.4
3+00			8.6	301.0
+50			12.0	297.6
"	0.50	297.54	12.58	297.04
4+00			3.5	294.0

CITY DATUM
~~Book~~ 320 pg. 70

℄ Intersection 54TH ST & Chol STA. ROAD
on Stop sign-marker ℄ Cholla Road

Cor curb return, near Mail Box (U.S.) SE cor of intersection
on A.C. Pav't.

Top stem of G.V. 0-0050 SIZE ?

Edge of A.C. Pav't.

7.18	
9.78	
1.51	
5.10	
8.45	
11.79	
3.37	

54TH ST. Pipeline

℄ PROFILE

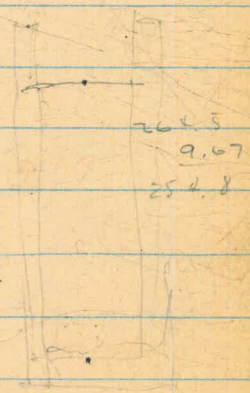
297.54					
4+50		7.2	290.3		
5+00		11.0	286.5		
11	0.20	284.72	13.02	284.52	
+50		1.0	283.7		
+61 40		1.48	283.2		
(4+36± Top W.V. Stem 11° RT)		5.2	~~292.34~~	279.42	
6+00		3.00	281.7		
(+26± Rim Sewer MH 45± LT		3.91	280.81		
INV " " " " "		15.91	268.81		
+50		4.52	280.2		
(+26± Rim Sewer M.H 195° RT		6.21	278.51		
		16.71	268.01		
+91.10		5.39	279.33		
7+00		5.5	279.2		
+50		6.6	278.1		
8+00		8.1	276.6		
+50		10.1	274.6		
9+00		12.5	272.2		
11	0.47	272.82	12.37	272.35	
+29.75		1.9	270.9		
+50		2.70	270.1		
+52.10		2.82	270.0		
10+00		5.0	267.8		

Conc Pavt.	
7.14	
10.75	
0.61	
1.42	Edge A.C Pavt.
2.91	on A.C Pav't
4.53	" " "
5.36	Edge A.C Pav't
5.55	
6.55	
7.98	
10.03	
12.38	
1.90	Begin A.C Pavt.
2.70	on A.C Pav't
2.83	End A.C. Pavt.
4.78	4.0 4.0 4.7 5.0
	10 6 3 4

54TH ST. Pipeline
℄ PROFILE
272.82

10+50		7.2	265.6
11+00		8.7	264.1
11+08.6 BC		9.0	263.8
+44.64		9.4	263.4
+48.64		9.35	263.5
		8.34	264.5
		17.69	255.13
		8.24	264.58
+60.54		9.25	263.5
+64.54		9.4	263.4
12+00.56		9.4	263.4
+50		9.0	263.8
P	10.46	275.17	8.11 264.71
13+00		10.6	264.6
+50		9.3	265.9

6.97	67.8 66.9 66.4 65.6 5.0 5.9 6.4 7.2 10 4 2 C	
6.53	54.2 65.0 64.4 64.1 9.9 7.8 8.4 8.7 6 5 3 C	
8.69	62.5 64.5 63.8 10.3 8.3 9.0 6 3 C	
	on Conc Deck of Culv.	
	Top Hdwll	
	100' ℄ Conc Box Culvert	
	Top Hdwll	
	on Conc. Deck of Culv.	
9.23		
8.87	61.3 64.5 64.5 63.8 63.8 11.5 8.3 8.3 9.0 9.0 10 4 3 2 C	
10.44	10.2 10.6 10.6 4 4	
9.07		



54TH ST. PIPELINE
℄ PROFILE
275.17 EE

14+00	8.0	267.2	
+50	6.1	269.1	
(+64.)	5.48	269.7	
15+00	5.0	270.2	
+50	3.3	271.9	
(Shldr on Left 0.0 15+70)			
16+00	2.1	273.1	
(Shldr on left 0.0 16+20)			
(Shldr " " 0.0 16+47)			
+50	0.3	274.9	
PI (on pavt)	11.12	286.09	0.20 274.97
17+00	9.7	276.4	
(Shldr on left 0.0 +46)			
+50	8.1	278.0	
(" " " 0.0 +53)			
18+00	6.8	279.3	
+50	5.2	280.9	

7.64	0.5 (12)	5.4 (3)	7.8 (3)	8.0 C	
6.27	0.1 (11)	4.7 (3)	5.9 (3)	6.1 C	
Top Hdwll cond Cross Drain filled up.					
270.45 4.72	0.6 (12)	2.6 (9)	3.2 (5)	5.0 (4)	5.0 C
2.29	1.0 (10)	1.3 (7)	2.8 (4)	3.3 C	
1.76	+0.5 (6)	1.5 (4)	2.2 (3)	2.1 C	
0.20	+1.0 (10)	0.3 (5)	0.3 C		
9.65	7.0 (8)	8.8 (3)	9.6 (3)	9.7 C	
8.07	6.5 (7)	7.9 (3)	8.1 C	(OVER. SECTION)	
6.52	4.8 (8)	6.1 (3)	7.1 (3)	6.8 C	
5.18	4.7 (10)	4.7 (3)	5.3 (3)	5.2 C	

54TH ST. PIPELINE

℄ PROFILE

286.09

19+00		4.5	281.6	281.52	
				4.57	3.6 3.9 4.5 (10 5 C)
+50		4.2	281.9	4.28	
20+00		4.2	281.9	4.30	
+50		4.4	281.7	4.54	
21+00		4.7	281.4	4.76	4.1 4.3 4.7 (10 1 C)
SET TBM	1.99	284.18	3.90	282.19	NAIL IN Pole D33059 TT (21+31 LT 6.0)
+50		3.0	281.2	3.20	2.4 2.6 3.0 (10 4 C)
22+00		3.5	280.7	3.49	3.1 2.9 3.5 (10 4 3 C)
+50		3.9	280.3	3.8	3.6 3.3 3.9 3.9 (10 4 3 C)
23+00		4.3	279.9	4.21	4.2 3.5 4.2 4.3 (10 4 3 C)
+50		4.5	279.7	4.46	4.5 4.6 3.7 4.3 4.5 (10 5 4 3 C)

54TH ST. PIPELINE

℄ PROFILE
284.18

24+00	4.9	279.3	4.76
+50	5.1	279.1	5.15
25+00	5.4	278.8	5.37
+50	5.6	278.6	5.56
(+90³ Top of Hdwll)	6.0	278.18	
Top of Pipe	7.2	276.98	
(+90³ Inv. # CMP Cross Drain)	8.7	275.48	
26+00	5.9	278.3	5.86
+50	6.1	278.1	6.19
(Shldr on left 00, +57)			
27+00	6.5	277.7	6.58
℄ (edge pavt) 1.55	279.15	6.58	277.60
+50	1.8	277.4	1.88
28+00	2.2	277.0	2.24

4.76 — 47 (10) 47 (5) 41 (2) 49 (3) 49 (8)

5.15 — 50 (10) 50 (7) 47 (5) 50 (3) 51 (2)

5.37 — 50 (10) 52 (6) 47 (4) 52 (2) 54 (2)

5.56

5.86

6.19

6.58 — 36 (10) 47 (5) 55 (3) 62 (2) 65 (2)

1.88 — +15 (10) +16 (7) 14 (3) 18 (8)

2.24 — +12 (10) 05 (6) 09 (2) 19 (3) c

54TH ST. PIPELINE

℄ PROFILE

279.15

28+50			2.7	276.5	2.64	+0.4 (10)	0.6 (4)	2.6 (3)	2.7 (C)
29+00			3.3	275.9	3.12	1.0 (10)	1.8 (6)	2.6 (4)	3.4 (3) 3.3 (C)
+50			4.3	274.9	4.08	2.3 (10)	3.3 (5)	4.4 (4)	4.3 (C)
30+00			5.6	273.6	5.34	4.4 (10)	5.1 (5)	5.5 (3)	5.6 (C)
	(+14'	Top Hdwll	5.42	273.7					
		Top Pipe	7.24	271.9					
	(+14' 7.24	Inv. # CMP	8.74	270.4					
+50			7.0	272.2	6.80	6.0 (8)	6.1 (4)	6.7 (3)	7.0 (C)
31+00			8.6	270.6	8.34	7.7 (7)	7.7 (4)	8.6 (4)	8.6 (C)
+50			9.8	269.4	9.81	9.2 (8)	9.4 (5)	8.8 (3)	9.8 (C)
32+00			11.5	267.7	11.22	10.9 (8)	11.0 (5)	11.8 (4)	
+50			13.0	266.2	12.79	13.4 (7)	12.5 (2)	13.4 (3)	13.0 (C)
℄ (edge Pvmt)		0.21	266.57	12.79	266.36				

52nd St. Pipeline
& Profile
266.57

(32+77	Top Hdwll	1.25	265.32
	Top CMP	3.15	263.42
(32+77	Inv. ℄	5.65	260.92
33+00		1.8	264.8
+50		3.0	263.6
34+00		3.5	263.1
+50		3.9	262.7
35+00		4.2	262.4
+02.69 B.C.			
(Sta. 104+08 ℄ Pavt.		4.45	262.12 = 262.4
+50		4.5	262.1
(+64.2	Top Hdwll	4.56	262.01
	Top pipe	5.86	260.71
(+64.2	Inv. ℄ CMP	7.86	258.71
36+00		4.8	261.8
+50		5.4	261.2
Set TBM.		5.84	260.73

1.63 — 0.8 C, 1.1 3, 1.8 2, 1.8 C

2.84 — 0.2 10, 1.0 7, 2.0 2, 2.9 3, 3.0 C

3.50 — 0.0 11, 1.7 4, 2.2 3, 3.5 C

3.78 — 0.6 11, 2.2 4, 3.8 3, 3.9 C

4.18 — 1.8 10, 2.8 4, 4.2 3, 4.2 C

262.00
4.54 — 2.2 10, 2.8 6, 4.2 2, 4.5 C

261.55
5.02

261.11
5.46

End of Cuts 46' Rt. 36+20

54TH ST. PIPELINE
& PROFILE

		266.57			
37+00			6.0	260.6	5.90
			6.9	259.7	
37+08.02 (Ec.)		(Bym Red!) ✓	9.9	~~256.7~~	
+50			6.6	260.0	6.54
38+00			7.0	259.6	7.09
(P (Edge Pavt.)	1.92	261.40	7.09	259.48	
+34.2		Top Hdwll Inv. ℄ of CMP	2.07	259.33	
+50			2.4	259.0	2.35
39+00			2.9	258.5	2.83
(+48		Rim Sewer MH 133' RT.	9.6	251.8	
		Inv. " "	16.4	245.0	252.0
+50		Inv. 53 LT. - - ✓ - - - -	9.4-3.3	258.1	3.22
✓(+57		Top 8" Trans WATER)	6.20	255.2	
40+00			3.7	257.7	3.70
+50			4.2	257.2	4.17
		Top Hdwll	4.23	257.17	
(+58		Top PIPE Inv. ℄ of CMP			
41+00			4.7	256.7	4.65
+50			5.3	256.1	5.10
		Top Hdwll	5.42	255.98	
(+81		Top PIPE Inv ℄			
42+00			5.6	255.8	5.58
+50			6.0	255.4	6.07
43+00			6.8	254.6	6.60
+50			7.7	253.7	7.60
(P (Edge Pavt.)	0.64	254.44	7.60	253.80	

54TH ST. PIPELINE

℄ PROFILE

254.44

3	44+00			2.2	252.2
3	+50			3.6	250.8
	45+00			5.3	249.1
3	+50			6.4	248.0
		Top Hdwll		6.37	248.1
4		Top Pipe Inv. ℄ End			
	46+00			7.9	246.5
	+25	31' LT Sewer MH. Inv. ✓		14.27	240.17
	+37	Top 6" Trans. Water ✓		11.27	243.17
3	+50			9.1	245.3
	47+00			10.4	244.0
4	+50			11.8	242.6
	H.	0.69	242.07	13.06	241.38
	48+00			1.0	241.1
4	+50			2.5	239.6
	49+00			3.9	238.2
	+50			5.9	236.2
4	50+00			8.1	234.0
	+50			10.5	231.6
4	51+00			12.9	229.2
4	(edge part)	0.11	229.32	12.86	229.21

	1.98
	3.50
	4.85
	6.35
	7.70
	9.07
	10.49
	11.97
	1.07
	2.34
	3.83
	5.82
	8.10
	10.41
	12.86

54TH ST. PIPELINE
& PROFILE

229.32

51+50		2.5	226.8	2.35
(52+85 87° LT. Inv. Sewer MH)		11.7		
52+00		4.2	225.1	4.19
+50		5.5	223.8	5.51
+85± Rim of Sewer MH. 38' RT		3.64	223.68	
+85± Inv. " " " 38' RT.		12.25	217.07	
(+85± Something to be dug here)				
(+90± 24 LT	(on cut stake)	5.7	223.6	
+95 Top 8" Trans pipe		8.94	Inv 0.38	
53+00		6.0	223.3	5.94
+50		6.3	223.0	6.05
54+00		6.4	222.9	5.93
+50		6.0	223.3	5.72
SET TBM		5.20	224.12	End of curb 40' RT 54+40
55+00		5.7	223.6	5.40
(+28±	Top Hdwll	7.69	221.6	
	Top pipe	10.57	218.8	
	Inv. ± CMP	14.57	214.75	
+50		4.9	224.4	4.87
56+00		3.9	225.4	3.59
+50		1.8	227.5	1.72
TH 11.62	240.19	0.75	228.57	
	Top Hdwll	10.98	229.21	
(+74±	Top pipe	12.44	227.75	
	Inv. ± CMP	13.44	226.75	

42 (10) 44 (1) 55 (8)

CUT STAKE MARKED
= 0+40 - C 6± (?? FUTURE ~~WATER~~ SEWER ??)

69 (10) 38 (5) 38 (3) 49 (2) 49 (8)

38 (10) 36 (7) 26 (4) 34 (3) 39 (8)

00 (10) 09 (2) 18 (1) 18 (8)

2/2/50

2.1

54TH ST. PIPELINE
& PROFILE

		240.19			
57+00		10.2	230.0	10.06	9.6 9.4 9.5 10.5 10.2 10 5 3 2 C
+50		7.4	232.8	7.36	7.4 7.0 7.6 7.4 5 3 3 E
58+00		4.6	235.6	4.40	Lt. Shldr 0.00
+50		1.6	238.6	1.40	
P	8.65	248.68	0.16	240.03	
59+00		7.2	241.5	6.96	
+50		5.6	243.1	5.28	
60+00		5.0	243.7	4.81	
+50		4.7	244.0	4.47	
61+00		4.2	244.5	4.09	
+50		4.2	244.5	3.67	
+94		3.45	245.23		Edge Conc Pav't
62+00		3.44	245.24		on " "
+15	(AT 8" MAIN)	3.5	245.33		on " "
		3.14	245.54		on L & T Intersection ℄ {54TH EUCLID
SET IBM	2.25	248.73	2.20	246.48	NAIL IN POWER POLE #27018

54TH ST. PIPELINE

CHECK LEVELS

		248.73		
P	0.47	238.06	11.14	237.59
CK BM			11.81	226.25 = 226.23
CK BM			12.16	225.90 = 226.10

CHECK LEVELS

BM.	0.25	342.97		342.72
P	0.05	330.53	12.49	330.48
P	1.15	320.55	11.13	319.40
			6.58	313.97 = 313.99

C.T. & FED & EUCLID
CITY DATUM
CHIS ☐ 32'50" LBT. CT. & FEDERAL & EUCLID

on Conc gate valve chamber

BK 320 pg 27, 28
" " pg 70

54TH ST. PIPELINE

(5) OFFSETS FOR EXCAVATION

SEPT '24 1951
BEATY
Leonard
Seavello

TBM	7.03	323.00	315.97		CH13 ⊓ Cor Curb 17'E 0+95
0+20			3.0	320.0	308.0	C 12
+50			4.6	318.4	307.45	C 11
0+75			6.1	316.9	307.0	C 9
1+00			7.7	315.3	306.33	C 9
+50			11.3	311.7	305.00	C 6
TP	1.27	311.31	12.96	310.04		
2+00			3.2	308.1	302.6	C 5
+25			5.0	306.3	301.4	C 4
+50			6.8	304.5	299.7	C 4
3+00			10.1	301.2	296.35	C 4
+50			13.4	297.9	293.0	C 4
TP	0.64	298.97	12.98	298.33		
4+00			4.7	294.3	289.5	C 4
+50			8.5	290.5	286.0	C 4
5+00			12.2	286.8	282.5	C 4
TP	0.27	286.22	13.02	285.95		
+50			2.3	283.9	279.0	C 4
+85			3.9	282.3	277.6	C 4

54TH ST. PIPELINE

(5) offsets for Excavation

286.22

6+25		5.4	280.8	276.0	C4.8			
+35		5.7	280.5	275.80	C4.7			
+85		6.7	279.5	274.65	C4.9			
7+00		7.0	279.2	274.30	C4.9			
+50		8.0	278.2	273.15	C5.1			
8+00		9.4	276.8	272.0	C4.8			
+50		11.5	274.7	269.8	C4.9			
P	0.41	274.03	12.60	273.62				
9+00		1.6	272.4	267.6	C4.8			
+50		3.9	270.1	265.4	C4.7			
10+00		6.0	268.0	263.2	C4.8			
+50		8.1	265.9	261.0	C4.9	✓		
11+00		9.7	264.3	~~257.0~~ ~~258.8~~ ~~260.0~~ 256.3	~~C4.3~~	C7.3 ~~+13~~ C6.2	✓	Revised grade Oct. 8, 1951
+08.62		9.9	264.1	~~254.83~~	~~C4.3~~	C7.8	✓	
+40			263.6	254.8		C8.8	✓	
+45.54		10.5	263.5	~~258.92~~ 254.8	~~C4.6~~	C8.7	✓	
+62.59		10.5	263.5	~~259.0~~	~~C4.5~~	C8.7	✓	
+67			263.5	254.8		C8.7	✓	
12+00.56		10.4	263.6	~~259.0~~ 256.7	~~C4.6~~	C6.9	✓	
+50		10.0	264.0	259.5	C4.5			
13+00		9.3	264.7	260.5	C4.2			
P	8.72	274.28	8.47	265.56				

54TH ST. PIPELINE

(5) OFFSET GRADES FOR EXCAVATION

274.28

13+50		8.1	266.2	261.5	C47
13+75		7.4	266.9	262.0	C49
14+00		6.7	267.6	262.8	C48
+50		5.3	269.0	264.4	C46
15+00		3.8	270.5	266.0	C45
CL Edge Conc. Pavt 15+00		3.79	270.49	= 270.45	.04
SET II	9.73 281.82	2.19	272.09		NAIL IN PO. POLE # 170659
+50		9.9	271.9	267.5	C44
16+00		8.4	273.4	269.0	C44
+30		7.4	274.4	269.9	C45
+50		6.8	275.0	270.5	C45
+75	F.H. TEE	6.1	275.7	271.25	C45
17+00		5.3	276.5	272.0	C45
+50		3.8	278.0	273.5	C45
18+00		2.2	279.6	275.65	C40
+50		0.9	280.9	276.80	C41
19+00		0.3	281.5	277.0	C45
II	3.15 284.68	0.29	281.53		
+50		2.8	281.9	276.9	C50
20+00		2.9	281.9	276.8	C51
+50		3.1	281.6	276.7	C49

(5) F.H. 2.4 - 279.4
EL & ST 6.0 - 275.8

C36 C72
TO FLANG TO BELL PIPE

54TH ST P.L

(5) OFFSET GRADES FOR EXCAVATION

		284.68			
21+00		3.4	281.3	276.6	C47
+03					
+50		3.7	281.0	276.5	C45
22-		4.0	280.7	276.12	C46
+50		4.4	280.3	275.74	C46
23-		4.7	280.0	275.36	C46
+50		5.0	279.7	274.98	C47
24-		5.2	279.5	274.60	C49
+50		5.6	279.1	274.31	C48
25-		5.8	278.9	274.03	C49
+50		6.0	278.7	273.74	C50
26+00		6.3	278.4	273.45	C50
+45		6.6	278.1	273.19	C49
+50		6.7	278.0	273.16	C48
+95	F.H. TEE	7.1	277.6	272.90	C47
27+00		7.1	277.6	272.87	C47
+50		7.4	277.3	272.58	C47
28+00		7.7	277.0	272.29	C47
(H)	0.33	277.26	7.75	276.93	
28+50			0.7	276.6	272.0 C46

(5) F.H. 1.8 - 282.9 C15 To FLANGE
Cl. & ST 3.3 - 281.4 C50 To Bott. PIPE

Note: This F.H. moved from Sta. 21+50 AS NEW TELE POLE Placed on Prop Line prolongation.

(5) F.H. 2.2 - 282.5 C48 To FLANGE
Cl. & ST 7.0 - 277.7 C83 To Bot. Pipe

54TH St P.L.

(5) OFFSET GRADES FOR EXCAVATION

		277.26			
29-			1.2	276.1	271.0
+50			2.1	275.2	270.0
30-			3.5	273.8	269.0
+50			4.9	272.4	267.5
31-			6.4	270.9	266.0
+50			7.9	269.4	264.5
32-			9.3	268.0	263.0
+05			9.5	267.8	262.7
+40	F.H TEE		10.7	266.6	260.3
+45			10.9	266.4	260.0
+50			12.3	265.0	259.60
33-			12.59	264.67	259.17
P		4.12 268.79	5.0	263.8	258.73
+50			5.7	263.1	258.30
34-			5.9	262.9	257.86
+50			6.4	262.4	257.43
35+02.69	2 PT		6.9	261.9	257.0
+50			7.7	261.1	256.5
36-			8.08	260.71	=260.73
CK TBM					

SEE PS REL 32

C5.0			
C5.2			
C4.8			
C4.9			
C4.9			
C4.9			
C5.0			
C5.1			
C6.2	(5) F.H	10.6	266.7 FO 3 TO FLANGE
C6.4	FL. 2 ST	10.4	266.9 C5.3 TO BOTT PIPE
C5.5			
C5.5			
C5.1			
C4.8			
C5.0			
C5.0			
C4.9			
C4.6			
PM.17			

NOTE: F.H. MOVED TO 32+40 TO MISS SEWER M.H.

54TH ST. P.L.

(5) OFFSET GRADES FOR EXCAVATION

	268.79				
36+50		8.0	260.8	256.0	C4.8
37+04.5 BK 37+08.5 AH		8.2	260.6	255.42	C5.2
37+50		8.8	260.0	255.0	C5.0
38-		9.3	259.5	254.5	C5.0
+50		9.7	259.1	254.0	C5.1
39+00		10.2	258.6	253.50	C5.1
39+05		10.3	258.5	253.45	C5.0
+59.6		10.7	258.1	253.0	C5.1
40+05		11.1	257.7	252.64	C5.1
P	0.24	258.27	10.76	258.03	
40+50		1.0	257.3	252.33	C5.0
41-		1.5	256.8	252.0	C4.8
+50		1.9	256.4	251.5	C4.9
42-		2.4	255.9	251.0	C4.9
+50		2.9	255.4	250.5	C4.9
43-		3.4	254.9	250.00	C4.9
+50		4.5	253.8	248.7	C5.1
44-		5.8	252.7	247.4	C5.3
+50		7.2	251.1	246.1	C5.0

Top Curb 40± Nor. side St. S.W. COR.

261.2 C5.2

260.6 C5.2

10-1-15

Beatty
Leonard
Powell

5.4
0.06
5.8
5.4
36.8

45
4.07
31.5
2.70
39.1.5

54th St PIPELINE 10-15-51

(5) OFFSET GRADES FOR EXCAV

		258.27				
45+00			8.6	249.7	244.8	c4 9
+50			10.2	248.1	243.5	c4 6
45+75			10.8	247.5	242.8	c4 7
+85			11.1	247.2	242.5	c4 7
46+39			12.6	245.7	241.0	c4 7
TP	1.10	246.40	12.97	245.30		Top curb
46+85			2.0	244.4	239.7	c4 7
47+00			2.4	244.0	239.3	c4 7
+50			3.9	242.5	237.9	c4 6
48+00			5.4	241.0	236.5	c4 5
+50			6.7	239.7	234.8	c4 9
49+00			8.1	238.3	233.1	c5 2
+50			10.0	236.4	231.5	c4 9
50+00			12.4	234.0	229.2	c4 8
TP	0.02	233.62	12.80	233.60		
+50			1.9	231.7	226.9	c4 8
51-			4.4	229.2	224.7	c4 5
+50			6.6	227.0	222.4	c4 6
52-			8.5	225.1	220.5	c4 6

15
.028
120
30
420

46
028
368
92
1288

028
54
112
140
1512

54TH ST PIPELINE

(5) OFFSET GRADES FOR EXCAV

		233.62			
52+45			9.7	223.9	219.1	C48
52+965			10.3	223.3	218.0	C53
53+45			10.4	223.2	217.8	C54
54+00			10.2	223.4	217.6	C58
+50			10.0	223.6	218.8	C48
55+00			9.7	223.9	219.2	C47
+38			9.5	224.1	219.5	C46
+50			9.2	224.4	219.9	C45
56+00			8.0	225.6	221.0	C46
+50			5.9	227.7	223.3	C44
57+00			3.6	230.0	225.5	C45
H	+10.99	241.84	2.77	230.85		
+50			9.0	232.8	228.3	C45
58+00			6.2	235.6	231.2	C44
+50			3.2	238.6	234.0	C46
59+00			0.2	241.6	237.0	C46
TP	+9.76	251.53	0.07	241.77		
59+50			8.2	243.3	238.5	C48
60+00			7.7	243.8	238.9	C49

025
45
125
10
115

45
004
180

54th St. Pipeline

(5) Offset Grades For Excav.

251.58

60+50		7.4	244.1	239.4
61+00		7.0	244.5	240.0
+50		6.6	244.9	240.3
+90		6.3	245.2	240.3
62+00 End		6.3	245.2	240.2
Ck BM		5.15	246.38	= 246.48

Revised Alinement as of Oct. 16.

T.B.M.	+5.76	266.49		260.73
B.C. 35+55			4.7	261.8 257.6
35+68			4.5	262.0 257.5
35+81			4.6	261.9 257.3
35+94			4.9	261.6 256.7
36+07			5.0	261.5 256.4
36+20			5.1	261.4 256.1
36+33			5.2	261.3 256.1
36+46			5.3	261.2 255.9
E.C. 36+58.96			5.4	261.1 255.7

C&7

C&5

C&7

C&9

C&8

Nail in Po. Pole

End of Curve 40' Rt 36+20 P17.

C

C

C

C

C

C

C

C

C

54th St. Pipeline
Revision Between
Sta 35+02.69 – 36+77.3

Oct. 17 1951
Beatty
Leonard
Powell

TBM		6.98	267.71		260.73	
34+50				4.8	262.9	258.2
35+02.69	Orig. P.I.			5.4	262.3	257.9
+35.2	Rev. B.C.			5.6	262.1	257.8
+48				5.7	262.0	257.7
+61				5.8	261.9	257.5
+74				5.8	261.9	257.3
+87				6.0	261.7	257.1
36+00			Δ = 37°00'	6.1	261.6	256.9
+08.81	P.I		R = 220.			
+13			T = 73.61	6.2	261.5	256.7
+26			L = 142.02	6.3	261.4	256.5
+39				6.5	261.2	256.3
+52				6.6	261.1	256.1
+65				6.6	261.1	255.9
36+77.3	E.C.			6.8	260.9	255.7
37+00				7.0	260.7	255.4

C47	
C48	
C43	
C43	Top-Bell 8" Sewer 257.2
C44	
C46	
C46	
C47	
C48	
C49	
C49	
C50	
C52	
C52	
C53	

Nov. 2 1951

BEATTY
LEONARD
POWELL

ELEVATIONS TOP 16" C.I. PIPE
30TH ST.
POLK TO SUNCREST

			EL Top Pipe	EL Pavt	
BM	2.98	368.94	365.96		BR SE Cor OHIO & POLK
0+00			9.53	359.41	363.34 Top 30" x 16" Cross
0+02			10.15	358.79	Top 16" C.I.
0+05 ?		(?)	8.55	360.39	Top 6" C.I.
0+12			9.73	359.21	Top 16 C.I.
0+49			8.80	360.14	363.54 Top 16 C.I.
0+51 ±	16" Horiz Val.				
0+56			8.89	360.05	" " " point of Wye
0+60 ±			8.95	359.99	" " "
2+49 ±			7.76	361.18	364.58 " " "
2+54			7.65	361.29	" " "
P	6.05	372.30	2.69	366.25	Top Curb
5+48 ?			8.65	363.65	366.45 Top 16" C.I.
5+54			8.57	363.73	" " "
8+33 ±			8.88	363.42	366.22 " " "
8+38			8.87	363.43	" " "
10+66 ±			10.19	362.11	363.91 " " "
10+75 ±			10.23	362.07	" " "
P	5.93	370.22	8.01	364.29	
12+11 ±			9.28	360.94	" " "
12+22 ±			9.22	361.00	" " "

ELEVATIONS Top 16" C.I. PIPE 30TH ST

POLK TO SUNCREST

		370.22			
CK BM			1.03	369.19	BP. NE Cor EL CAJON & 30TH
15+51			7.85	362.37 365.07	Top 16" C.I. PIPE
15+59			7.77	362.45	" " "
18+54	AT WYE			363.03 365.78	
18+87			6.62	363.60	" " "
18+94			6.51	363.71 366.21	" " "
P			2.21	368.01	Top F.H. SE Cor. Meade & 30TH
CK BM				365.68	~~City Engr Tag NE Cor. Meade~~ B.P. SE Cor " " "
B.M.	4.93	372.42		367.49	BP. NW Cor HOWARD & 30TH Nov. 14 1951
7+12			8.27	364.15 367.25	Top 16" C.I.
7+39			8.31	364.11 366.81	" " "
8+33.5			8.97	363.45 ~~366.42~~	" " "
P	8.84	376.85		368.01	Top F.H SE Cor Meade & 30TH
CK BM			11.19	365.66 ~~365.67~~	BP. SE Cor Mead & 30TH
21+89.5			6.98	369.87 372.27	Top 16" C.I.
21+95.2			6.79	370.06	" " "
P	10.25	386.99	0.11	376.74 ✓	
24+94			10.64	376.35 378.65	" " "
25+01			10.58	376.41	" " "

Elevations Top 16" C.I. Pipe 30th St

Polk To Suncrest.

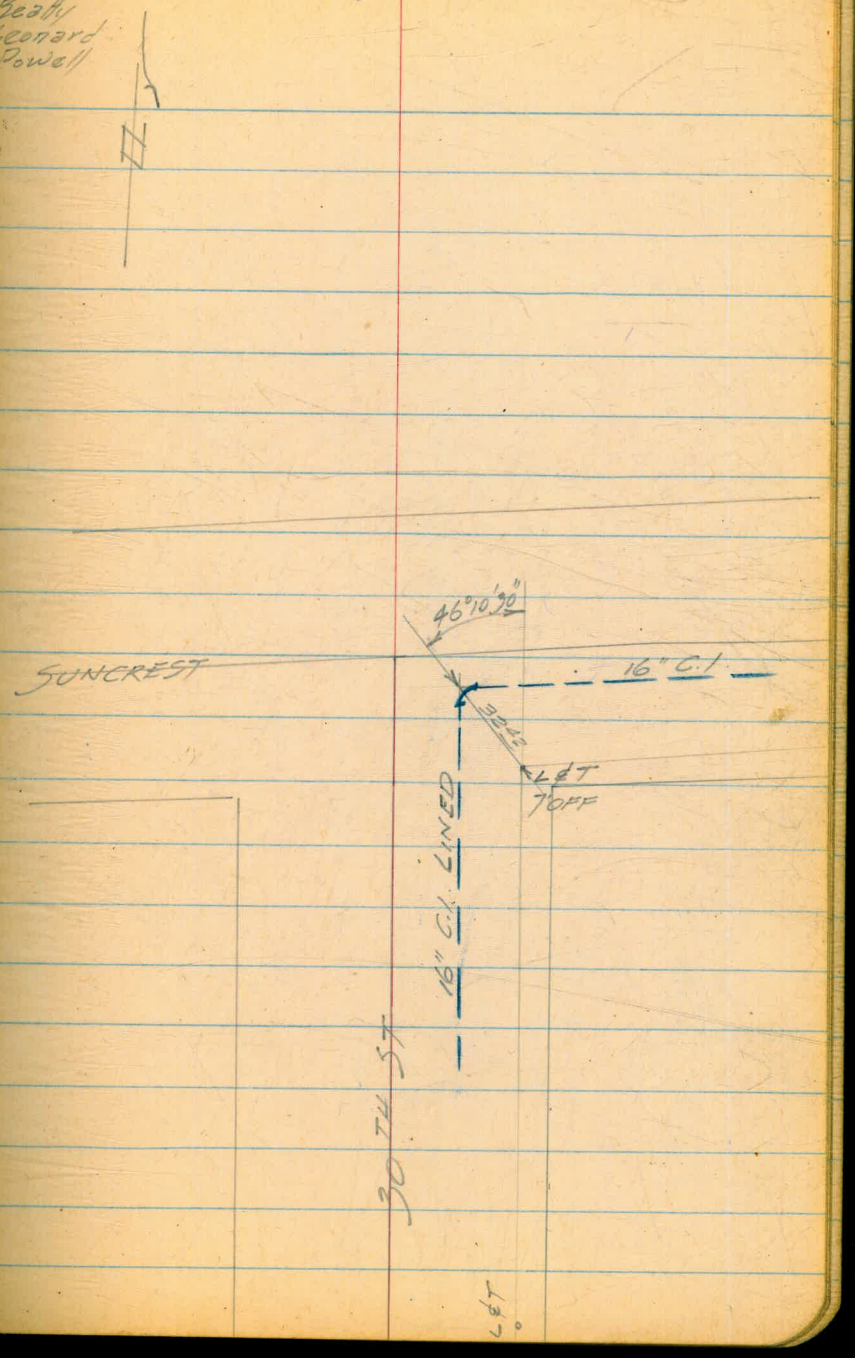
386.99

CK BM			8.05	378.94 = 378.96	SE Cor Monroe & 30th
27+97			7.59	379.40	381.60 Top 16" C.I.
28+03			7.50	379.49	" " "
31+00			4.48	382.51	384.71 " " "
31+05			4.42	382.57 ✓	" " "
TP	6.20	392.36	0.83	386.16	
33+96			8.26	384.10	386.50 " " "
34+00			8.19	384.17	" " "
36+94			6.88	385.48	388.18 " " "
36+99			6.81	385.55	" " "
CK BM	4.90	394.26	3.00	389.36 = 389.04	BP SE Cor Adams & 30th
39+39			8.13	386.13	389.13 Top 16" C.I.
SET TP			4.16	390.10	Top F.H. SE Cor Suncrest & 30th
CK BM	2.89	392.25		389.36	BP. SE Cor Adams & 30th
TP	2.03	388.21	6.07	386.18	
CK BM			9.28	378.93 = 378.96	BP. SE Cor Monroe & 30th
TP	3.06	393.16		390.10	Top F.H.
39+625			6.56	386.60	389.1 Top 16" C.I.
42+27			7.80	385.36	387.41 " " "
42+30	End of Bell (90° Bend)				
CK TP			30.6	390.10	

TIE TO & PT of 16" C.I
30TH & SUNCREST.

Nov. 21 1951

Beath
Leonard
Powell



PROPOSED 12" WATER
WREN ST SCIMITAR - BROADWAY

37°15'30" LT TAN. To Curve

8+45 13 E.C & ∠ PT

Δ 38°50'30" LT
R 590.
L 399.80

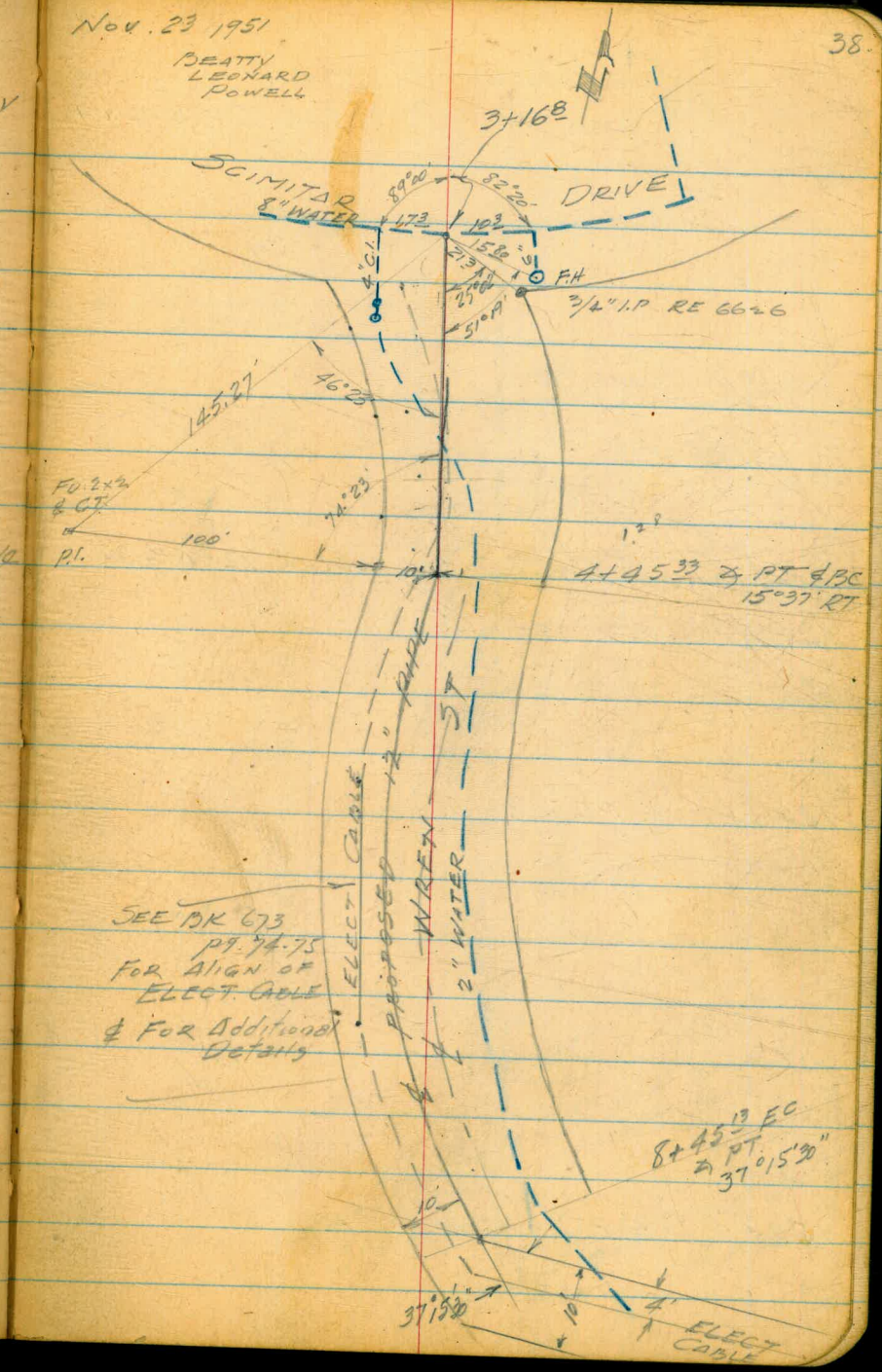
4+45 33 ∠ PT & BC
15°37' RT

3+16 8 Intersn of 8" C.I. MAIN

Nov. 23 1951

BEATTY
LEONARD
POWELL

38



PROPOSED 12" MAIN
WREN ST. SCIMITAR TO BROADWAY

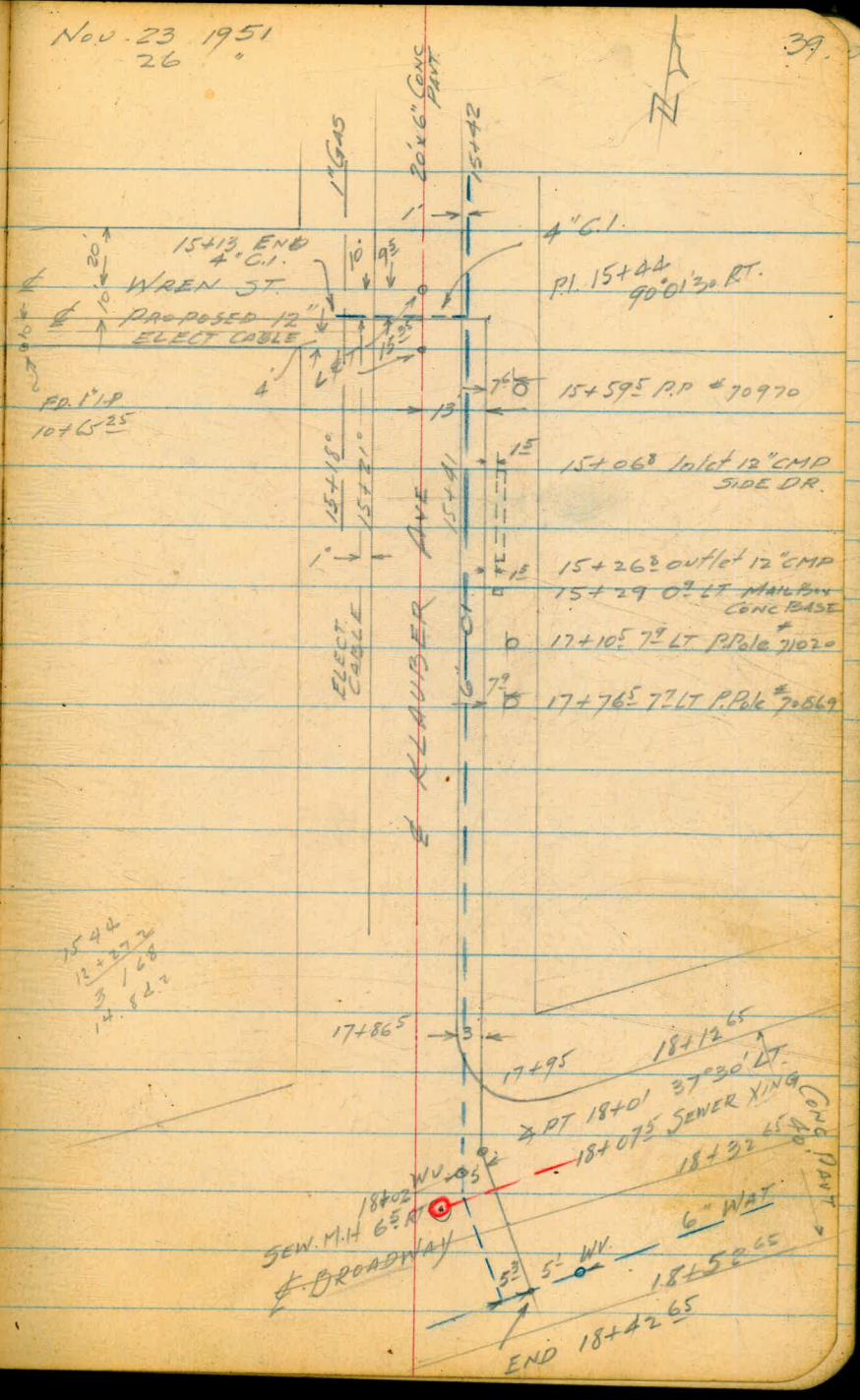
18+42.65 END PROPOSED 12" MAIN

18+01 ℄ PT 37°30' LT

15+44 ℄ PT 90°01'30" RT.

Nov. 23 1951
26 "

39.



WREN ST
SCIMITAR TO BROADWAY
℄ PROFILE → PROPOSED 12" MAIN

	+B.S	H.I	-FS		
T.B.M.	0.26	416.95		416.69	Top FH SE Cor Scimitar ℄ Wren BK 673-pg. 77
3+16.8			3.7	313.3 ✓ 413.3	NAT GRD.
3+16.8			5.3	311.7 ✓ 411.7	Top 8" C.I Pipe
+25			5.6	311.4 ✓ 411.4	
			7.96	309.0 ✓ 409.0	Top 4" G.V. 11' RT 3+39
			8.87	308.13 ✓ 408.13	Top 2" G.V. 10± RT 3+40.5
+50			11.2	405.8 ✓ 405.8	
T.P. (rock)	0.54	406.14	13.35	403.60	
+75			2.7	401.4	
4+00			6.5	397.6	
+45.33	℄ PT ℄ B.C.		13.0	391.1	
T.P. ℄ NAIL	0.64	391.80	12.98	391.16	
5+00			6.0	385.8	
+25			8.6	383.2	
+50			12.9	378.9	
T.P. (rock)	0.40	379.09	13.11	378.69	
6+00			4.7	374.4	
+50			8.9	370.2	
T.P. ROCK	0.67	366.47	13.29	365.80	6+49 (℄) WAT. MET.
CK TP			3.49	362.98 = 363.04	

WREN ST.

℄ PROFILE - 12" PROPOSED MAIN

	366.47		
7+00		1.5	365.0
+50		5.9	360.6
8+00		9.4	357.1
+45.13 ℄ PT.		12.3	354.2
+60		11.2	355.3
9+00		9.6	356.9
+50		9.8	356.7
10+00		11.7	354.8
TP (rock) +2.10	355.30	13.27	353.30
+50		3.9	351.6
SET TP		-6.35	348.95
11+00		-9.1	346.2
T.P. +0.08	342.23	-13.15	342.15
+50		-4.8	337.4
TP 0.92	330.08	13.07	329.16
12+00		3.7	326.4
TP 0.99	318.14	12.93	317.15
+50		4.3	313.8
13+00		13.4	314.7 ✓ 304.7 ✓

PROP. COR. IRON PIPE.

WREN ST.

℄ PROFILE — 12" PROPOSED MAIN

		318.14		
13+00			16.0	302.1
+50			15.1	303.0
+55			12.4	303.7
+75			9.5	308.6
14+00			5.6	312.5
℄	12.32	330.43	0.03	318.11
+50			11.1	319.3
+75			5.0	325.4
℄	6.16	335.80	0.79	329.64
15+00			3.2	332.6
+10			2.0	333.8
+21			1.79	334.0
+21			5.27	330.5
+31			1.79	334.0
+41			1.79	334.0
+44	℄ PT.		2.0	333.8
16+00			6.4	329.4
+50			9.9	325.9
℄	0.75	323.46	13.09	322.71
17+00			1.4	322.1

Edge Conc Pav't
Top 4" C.I.
℄ " "

Edge Conc Pav't

6.0 (3) RT Edge pav't

9.68 " " " "

1.16 " " " "

WREN ST

℄ PROFILE - 12" PROPOSED MAIN

		323.46		
17+50		5.3	318.2	4.50 @ RT. Edge Conc. Pavt
17+95		8.20	315.3	Edge of Conc Pavt
18+01	℄ PT	8.39	315.1	
		8.60	314.9	Rim Sewer M.H. Inv. -8.65 lower.
18+32.65		9.33	314.1	℄ Broadway
18+42.65		9.65	313.8	
CK		11.15	312.31 = 312.37	BP IN PAVT

Nov. 27, 1951

BEATTY N
LEONARD
POWELL

'E' ST

℄ PROFILE – PROPOSED PIPELINE
10' Southerly ℄ ST
28TH ST TO 30TH ST.

	R.R.	H.I.			
BM.	1.24	188.80 ✓	187.56 BM	CITY DATUM	BP NW Cor 30TH ℄ E (also given as 187.63)
12+49	WATER VALVE				
12+48	W. Prop. line 30TH ST.				
12+48			3.3	185.5	on edge conc pavt.
12+00			2.7	186.1	
+50			2.8	186.0	
+25			3.7	185.1	
11+00			5.7	183.1	
+50			11.4	177.4	
		H.I.		TBM	
TP	1.24	176.89 ✓	13.15	175.65 ✓	
+05			5.9	170.99	
10+00			6.1	170.79	
+96			6.6	170.29	
	R			TBM	
TP	1.62	165.24 ✓	13.27	163.62 ✓	
+83			1.6	163.64	
+75			4.3	160.94	
+61			9.2	156.04	
+50			12.3	152.94	
TP	0.31	152.68 ✓	12.87	152.37 ✓	
+35			5.4	147.28	

E –
30 – 37

"E" ST
℄ PROFILE – Proposed Waterline
28TH to 30TH

		152.68		
℄	5.69	145.13 ✓	13.24	139.44 ✓
9+25			6.5	138.63
+19			8.8	136.33
9+00			11.2	133.93
+85			12.0	133.13
+50			10.6	134.53
8+00			4.2	140.93
℄	11.85	156.07 ✓	0.91	144.22 ✓
+87			11.3	144.77
+81			6.9	149.17
+75			6.0	150.07
+59			4.7	151.37
+50			3.1	152.97
+38			1.50	154.57
℄	11.86	167.61 ✓	0.32	155.75 ✓
+25			9.3	158.31
7+00			5.9	161.71
+80			3.0	164.61
6+50			1.6	166.01
℄	12.17	179.14 ✓	0.64	166.97 ✓

Top 2" GAS & NAT GAS 1:1 Slope to left
Level to Right

(2" WATER 1℄ RT) $\frac{0.0}{5} \times \frac{8.0}{3}$ $\times \frac{4.5}{2}$

'E' St.

& Profile - Proposed Pipeline

28TH to 30th

		179.14		
6+39		12.4	166.74	Edge AC Pavt
6+00		10.5	168.64	on AC "
+50		8.4	170.74	" " "
5+00		6.5	172.64	" " "
+50		4.3	174.84	" " "
4+00		1.4	177.74	" " "
H.P	6.70	185.18 ✓	0.66	178.48 ✓
+50			4.2	180.98 " " "
3+00			1.9	183.28 " " "
+75			1.5	183.68 " " "
2+50			2.0	183.18 " " "
2+00			5.0	180.18 " " "
+50			10.4	174.78 " " "
H.P	0.18	172.27 ✓	13.09	172.09 ✓
1+00			4.5	167.77 " " "
+50			11.9	160.37 " " "
H.P	2.90	161.91 ✓	13.26	159.01 ✓
+30			4.0	157.91 " " "
+12	At Wat. Val.		4.43	157.48 " " "
0+00	& 28TH ST.		4.52	157.39
CK BM.			4.15	157.76 = BP. SE Cor 28TH & E

E ST.
31ST to 32nd
℄ Profile - Proposed Waterline
10' Southerly ℄ ST.

BM.	2.18	181.17 ✓	178.99	BP SW. Cor 31ST ℄ E ST.
0+00 = W. Prop 31ST St.		2.4	178.77	
+50		3.1	178.07	
1+00		7.9	173.27	
+50		13.3	167.87	
TP	0.75	168.73 ✓	13.19	167.98 ✓
+86		4.3	164.43	
+90		5.8	162.93	
+94		5.0	163.73	
2+00		7.8	160.93	
+12		13.1	155.63	
TP	0.32	155.93 ✓	13.12	155.61 ✓
+15		0.3	155.63	
+25		3.4	152.03	
+40		9.7	146.23	
TP	0.50	144.07 ✓	12.36	143.57 ✓
+42			0.0	144.07
+50			2.6	141.47
+75			8.7	135.37
TP	0.62	131.68 ✓	13.01	131.06 ✓

2" I.P. WATER Line 1' RT Same elev.

E ST
31st to 32nd
℄ Profile - Proposed Waterline

		131.68		
2+90			0.0	131.68
3+00			3.2	128.48
+15			9.8	121.88
P	0.86	119.44	13.10	118.58
+25			2.1	117.34
+40			7.4	112.04
+50			10.6	108.84
+60			15.0	104.44
+65			15.5	103.94
+78			14.3	105.14
+90			6.3	113.14
4+00			2.6	116.84
P	13.00	132.14	0.30	119.14
+16			12.3	119.84
+25			11.0	121.14
+45			8.3	123.84
+75			3.6	128.54
P	2.29	132.29	2.14	130.00
5+00			4.0	128.29

'E' St
31st To 32nd
& Profile - Proposed Waterline

		132.29	
5+25		5.0	127.29
+50		8.1	124.19
PI	0.29	119.48 ✓	13.10 119.19 ✓
6+00		4.5	~~106.38~~ 117.98
+31		6.2	113.28
+50		8.3	111.18
+55		9.6	109.88
+68		10.8	108.68
+87		12.0	107.48
+88		11.3	108.18
+90		11.7	107.78
PI		12.52	106.96 ✓
+92		13.7	105.78 ✓

on City Eng. 2x2 Hub. SW. Cor

Notes Worked
11-28-51 DEZ

JEFFERSON ST.
ARISTA TO HARNEY
& PROFILE - PROPOSED

APRIL 3 1952
BEATTY
POWELL
BERGER

	+	H.I.	RP. +	Ground Elev
B.M.	1.06	44.81		43.75
TP	0.79	35.37	10.23	34.58
TP	3.16	26.29	12.24	23.13
SET TBM.			3.90	22.39
0+00			1.8	24.49
0+05			4.1	22.19
0+18			4.9	21.39
0+50			4.8	21.49
0+68			5.7	20.59
1+00			8.9	17.39
TP	4.54	18.91	11.92	14.37
+50			7.6	11.31
2+00			9.1	9.81
+50			10.8	8.11
3+00			10.1	8.81
+15			9.5	9.41
+50			5.2	13.71
+68			3.2	15.71
Storm Sew MH	Rim	3.92		14.99
	Inv.	21.05		
				-2.14

Proposed ℄ = 10' NELy ℄ ST ; ℄ of 24" RCP 14' Swly ℄ St.

BP. SE Cor Ampudia & San Diego

NAIL IN Po. POLE SE Cor ARISTA & Jefferson

St. level 4.7 (6) × 0.3 (5)

2-WAT MET 27' LT 0+06

STORM MH. 20' LT 0+41

St. level 6.7 (3) 4.8 (2) ×

3-WAT MET's 27' LT 0+47

8.0 (3.5) 5.7 (3) ×

11.2 (3) ×

8.9 (3) 7.6 (2.5) ×

10.8 (1.5) 9.1 (1) ×

6½ RT 2+83 Tele Pole

3+68 Storm Sew Ling. 24' LT. To NEW STORM M/H

JEFFERSON ST. (CONT'D)

		18.91 Rim	2.21	16.70	
	San Sew	M.H. Inv.	16.71	2.20	
TP	10.43	28.74	0.60	18.31	
4+00			9.3	19.44	
+22			7.3	21.44	
+50			5.6	23.14	
+70			4.9	23.84	
5+00			4.45	24.29	
+50			3.9	24.84	
6+00			3.4	25.34	
+50			3.3	25.44	
7+00			3.4	25.34	
+10			3.55	25.19	
+25			3.35	25.39	
				25.29	
		Rim	3.45		
		Inv.	10.35.	18.39	
TP	3.46	28.98	3.22	25.52	
	12.71	34.~~42~~ 32	7.37	21.61	
				31.95	
CK BM			2.37	~~32.05~~	
TP	9.26	18.57		18.31	
CK TBM			15.26	03.31 = 03.31	

3+75 8" Sewer Xing		10' LT ℄ of M.H.
4+12 4+23	23'	LT 9- Wat. Met.'s
4+00		Westerly Prop. line CONDE ST.
		Begin Conc Curb & 5' RT
		" 1" oiled surfacing
		Edge 5' Sidewalk 75 RT 350' parking
4+31		6' RT Guy Anc
4+48		6' RT WAT. MET
4+49		Gas Ser Xing "
4+51		6' RT Tele Pole J.P. 2458
~~4+88~~		6' RT WAT. MET
4+97		Gas. Ser Xing
5+19		6' RT WAT. MET
5+20		Gas Ser Xing
275' Parking 5+26		24' LT WAT. MET
Begin Curb & Sidewalk 5+78		6' RT WAT. MET
6+00 25' LT 5+83		Gas Ser Xing
6+09 27' LT WAT. MET 6+15		6' RT. Tel Pole # 307967
6+64		27' LT. WATER MET

Gutter line, face curb E'ly side Harney

& Harney St.

7+25 10' LT. ℄ of M.H. Sewer.

7' off LET Se Cor Jefferson & Harney

BP. SW Cor CONDE & San Diego

TBM. NAIL IN Pole & Nor side MOORE & CONDE

JEFFERSON ST
ARISTA TO HARNEY
PROPOSED 6" WATER

7+25 ℄ HARNEY ST.

4+03 18' RT. CITY ENGR TAG IN CONC SW.

3+75 ℄ CONDE ST.

0+00 = Easterly Propline Arista St

April 4 1952
Beatty
Powell
Berger

52

SEWER MH 2" A.C. 7+25
℄ HARNEY ST WATER 7+15
Curb 7+10 LT 7' off ℄ LT
CONC SW
GAS
A.C. SURFACING
CONC SIDEWALK
6+00
25'
WATER 15
CITY ENGR. 7' offset
6+00 Prop. line
GAS 3+85
8" SEWER MH 3+75
℄ CONDE ST
3+68 MH 24" 36" STORM SEWER
24" STORM SEWER
℄ PROPOSED
10'
NEWLY CONSTRUCTED STORM SEWER
℄
℄ ARISTA ST 0+25
0+15 WATER
Closed for School Grounds
0+00

(5) GRD

"E" ST. 29TH to 30TH STRS FOR 6" WATER MAIN

BM	1.97	189.60		189.63	BP NW Cor 30TH & E ST
			Top 6" C.I. - 7.80		12+84 = G VAL.
12+83			Bott 6" C.I. 8.40	181.2	12+83 = PAVT
					12+81 = End Exist. 6" C.I.
12+50			3.7	185.9	181.8 182.6 C41
12+00			3.4	186.2	181.8 C44
+50			5.1	184.5	179.2 C53
11+00			10.2	179.4	174.0 C54
TP (rock)	0.43	176.67	13.36	176.24	166.5
+50			4.4	172.3	167.8 C58
BP +25			8.3	168.4	161.0 C74
10+00	0.23	164.41	12.49	164.18	
			6.3	158.1	155.2 132.2 C39
TP	0.51	152.09	12.83	151.58	
+75			4.0	148.1	145.3 C28
BP	7.61	146.47	13.23	138.86	
+50			8.3	138.2	133.0 C52
+25			13.3	133.2	132.0 C12
9+00			13.3	133.2	132.0 C12
+75			11.5	135.0	132.0 C30
+50			9.0	137.5	134.9 C26
+25			3.2	143.3	138.2 C49
	12.99	159.37	0.09	146.38	
8+00			10.0	149.4	144.2 C52
+50			2.0	157.4	155.6 C18
	12.88	171.92	0.03	159.34	
7+00			8.3	163.6	160.4 C32

E ST.
(Cont'd.)

			171.92			
6+50			4.9	167.0	164.1	C 2.9
+25			2.8	169.1	165.4	C 3.7
~~+15~~	~~G.V.~~		~~2.8~~	~~169.1~~	~~165.8~~	~~C 3.3~~
6+11	F.H. TEE	(corbin)	2.8	169.1	165.9	C 3.2
6+00			2.4	169.5	166.2	C 3.3
TP	13.03	182.24	2.71	169.21		
(6+03 G.V.)						
						LOT (5) 3' BK of P.L SW Cor 29TH & E
						(5-9-52)
5+50			10.6	171.6	168.2	C 3.4
5+00			8.6	173.6	170.6 ~~170.9~~	C 3.0
+50			6.0	176.2	173.2 ~~173.6~~	C 3.0
4+00			2.8	179.4	176.3	C 3.1
TP	2.77	184.48	0.53	181.71	179.0	C 3.5
+50			2.0	182.5		
+25			1.2	183.3	180.2	C 3.1
3+00			0.9	183.6	180.2	C 3.4
+75			1.6	182.9	179.4	C 3.5
+50			2.8	181.7	177.4	C 4.3
2+00			7.4	177.1	173.6	C 3.5
TP	0.00	171.48	13.00	171.48		
+50			0.65	170.8	166.4	C 4.4
1+00			8.0	163.5	159.3	C 4.2
+75			11.8	159.7	~~159.1~~ ~~159.8~~	C 3.6
+70	F.H. TEE		12.4	159.1	155.6	C 3.5
TP	4.20	163.44	12.24	159.24	154.8	C 3.0
+50			5.9	157.5		
0+45			6.0	157.4	154.8	C 3.0
⊄ BH			5.58	157.86		
					157.40	

JUNIPER ST
TULIP to 39TH

④ GRADE FOR REPLACING 10" C.I. MAIN

BM	0.28	254.16		253.88	Top F.H
16+45			2.4	251.8	246.0 C5.8 / Conn. to Exist. Pipe
16+00			5.2	249.0	244.4 C4.6
15+50			8.3	245.9	242.0 C3.9
15+21	1" Tap		9.4	244.8	240.5 C4.3
15+00			10.2	244.0	239.4 C4.6
14+50	2" D.O		11.2	242.8	238.0 C4.8
14+00			12.2	242.0	237.7 C4.3
13+50			11.3	242.9	238.0 C4.9
13+00			10.2	244.0	239.2 C4.8
+50			9.4	244.8	240.4 C4.4
12+16			9.1	245.1	240.4 C4.7
12+00			9.2	245.0	240.4 C4.6
11+50			11.3	242.9	237.4 C5.5
H		1.48 242.41	13.23	240.93	
11+00			2.2	240.2	235.0 C4.8
+69	10x6 Cross		3.3	239.1	233.6 C5.5
+66	G.V.		3.2	239.2	233.3 C5.9
10+50			3.8	238.6	232.6 C6.0

JUNIPER ST. (CONT'D.)

		242.41			
10+00			6.4	236.0	230.5	C5 5
9+50			10.3	232.1	228.8	C3 3
9+25			11.6	230.8	228.5	C2 3
SET TP	3.11	238.63	6.89	235.52		Nail in power pole
9+00			9.3	229.3	228.3	C1 0
8+58			8.9	229.7	228.0	C1 7
8+45			9.0	229.6	227.9	C1 7
8+00			8.5	230.1	227.5	C2 6
7+50			6.9	231.7	227.0	C1 7
7+05			4.7	233.9	226.6	C2 7
7+03			4.6	234.0	226.5	C7 5
6+50			6.5	232.1	226.2	C5 9
6+08	F.H Tee					(5) F.H
6+31						
CK BM			7.45	231.18	= 231.21	Conc. Mon Cor

E ST. - 30TH TO 29TH

② STKS & GRADES SET FOR WATER MET.S

Back of MET. 22.5 From ℄ St.

BM.	4.30	191.93		187.63	BP NW Cor 30th & E
0+00 = W. Prop. line 30TH (METERS to the west)					
0+45 Nor.			5.2	186.7	186.6 CO1
0+68 Nor.			4.9	187.0	186.4 CO6
0+72 So			6.3	185.6	185.5 CO1
1+32 Nor.			6.2	185.7	184.5 C1.2
1+22 So			6.9	185.0	183.5 C1.5
1+71 Nor			10.05	181.9	179.5 C2.4
1+87 So			13.4	177.5	176.9 CO6 ✓
℄	1.21	180.05	13.09	178.84	
2+12 Nor			4.95	175.1	173.8 C1.3
2+15 So.			4.55	175.5	173.5 C2.0
2+54 So.			10.75	169.3	168.5 CO8
0+00 = W Prop line 29TH St (Meters to the EAST)					
1+28 Nor			13.75	166.3	161.3 C5.0
0+89 Nor			11.40	168.7	164.6 C3.1
℄	1.40	168.56	12.89	167.16	
1+48 So			13.5	155.1	159.1 F4.0
ck ⓐ 7+50			11.2	157.36	157.4 ✓
0+00 = West prop. line 32nd.					
0+19 So.				111.9	112.0 CO1

4.95 − 3.15 = 1.8 lower

4.55 − 2.75 = 1.8 low

8.95 − 1.8 = 10.75

107.06 − 4.8 = 111.86

OCT. 16 1952
BEATTY
POWELL
ALEXANDER

RADIO ROAD
& PROFILE - PROPOSED WATER
ATTIX TO 60TH ST.

Sta.	B.S.	H.I.	F.S.	ELEV.	
BM	0.40	345.17		344.77	CITY DATUM
0+00	E Prop. line ATTIX DR.		2.2	342.9	
+30	℄ ATTIX DR		2.8	342.3	
+50			3.7	341.4	
1+00			5.0	340.1	
+50			5.9	339.2	
2+00			6.8	338.3	
+50			7.9	337.2	
3+00			8.7	336.4	
+50			9.6	335.5	
4+00			11.3	333.8	
TP +50	1.30	334.19	12.28	332.89	
5+00			1.9	332.2	
+50			2.0	332.1	
6+00			2.6	331.5	
+50			3.8	330.3	
7+00			4.5	329.6	
+50			5.4	328.7	
8+00			6.6	327.5	

Top. E.H. ATTIX DR & RADIO ROAD SE Cor

Shldr of Road 8.9 7

8.6 15. 6.7 7 Shldr

RADIO Road. (Cont'd.)

Sta.	B.S.	H.I.	F.S.	ELEV.
		332.19		
8+30		℄ PT.	7.8	326.3
+50			8.1	326.0
9+00			10.3	323.8
PT +50	0.31	321.19	13.31	320.88
10+00			3.9	317.2
+50			7.0	314.1
11+00			8.8	312.3
+50			9.4	311.7
12+00			10.0	311.0
+50			11.4	309.7
PT Rock	0.00	308.62	12.57	308.62
13+00			1.4	307.2
+50			3.8	304.8
14+00			4.9	303.7
+50			5.1	303.5
15+00			5.1	303.5
+50			5.5	303.1
16+00			5.9	302.7
+50			6.4	302.2

8.5 9.1 7.4
15 8 2
Shldr

10.0 7.9
12 6
Shldr.

12.7 10.9
12 5

(1-3" Mach) Edge 2 AC.

7.0 5.4
10 5
Shldr. Edge AC.

8.7 6.1
9 3
Shldr. Edge AC.

RADIO ROAD (Cont'd.)

		308.62		
17+00			8.0	300.6
+50			9.6	299.0
+81	℄ RT.		10.00	298.6
SET TBM	044	302.49	6.59	302.03
18+00			4.2	298.2
+50			4.8	297.6
19+00			5.2	297.2
+50	(SOUTH. Edge A.C. pavt.)		5.0	297.4
20+00			8.8	293.6
+50			15.5	286.9
+80			16.9	285.5
21+00			13.8	288.6
+16			11.6	290.8

10.0
Edge A.C 10 ×
COR Conc Wall NWly Cor. WINNET & RADIO

4.8
Edge A.C 4.5 ×

9.9 5.6 5.6
15. 7. 4 Edge A.C.
5. Shldr. 2" Thick

8.5 5.2 3.8
10. 3. 1. — ✓

13.5 13.3 5.4 5.6
15 8 × 6 10 Edge A.C.
5. Shldr

16.4 5.6
6 × 15
5. Shldr

21.9 5.8 ✓
6 × 15
Shldr

19.0 6.0
10 × 13.
Shldr

RADIO ROAD (Cont'd)

30247

21+20			13.4	289.0				
21+29			10.4	292.0				
21+50			11.5	290.9	13.8 / 10	×	7.6 / 8	7.6 / 9 Sa. Shldr Edge AC
22+00			10.9	291.5	14.2 / 10	13.3 / 4	×	9.3 / 4 — 9.5 / 6 Sa. Shldr. Edge AC
+50			10.4	292.0	13.5 / 7	×	10.4 / 2 Edge AC	
23+00			10.5	291.9	14.0 / 8	×	10.6 / 1 Edge AC	
PT +50	4.01	295.57	10.91	291.56	13.7 / 7	10.9 / 1	×	10.9 / 1 Edge AC
24+00			5.45	290.1	8.0 / 10	5.5 / 3		5.45 / 2 Edge AC
24+56.93	PT		7.0	288.5	8.1 / 8	×	7.0 / 2 Edge AC	
+83			7.4	288.1	12.5 / 5	×	7.1 / 3 Edge AC.	
+95			9.6	285.9	294.4 / 11.2 / 1 / E	18" Steel Cross Drains	×	10.4 / 23 / E

RADIO ROAD (Cont'd)

295.57

25+00	9.2	286.3	11.1 / 5	×	7.0 (3 Shldr) 7.1 (5 Edge A.C.)
+11	7.6	287.9	8.5 / 5	×	6.9 (2 Shldr.) 7.0 (5 Edge A.C.)
+50	6.3	289.2	25+43 / 25+55 Conc. Driveway 6.65 / 2.5	×	6.9 (5 Edge A.C.)
26+00	5.1	290.4 ✓	6.4 / 5	×	4.7 (3 Edge A.C.) 4.6 (5)
+50	5.6	289.9	8.2 / 10	×	5.7 (2 Edge A.C.) 5.6 (5)
27+00	8.1	287.4	11.8 / 10	×	8.1 (4 Edge A.C.) 8.1 (5)
+50	10.7	284.8	14.0 / 10	×	10.3 (2 Shldr) 10.3 (4 Edge A.C.) 10.3 (5)
28+00	12.1	283.4	14.4 / 10	×	11.9 (5 Edge A.C.)
+50	11.3	284.2	14.2 / 10	×	10.2 (2 Shld.) 10.2 (4 Edge A.C.) 10.15 (5)
29+00	8.8	286.7	12.5 / 10	×	8.2 (3 Shldr) 8.2 (4 Edge A.C.) 8.2 (5)

RADIO ROAD (Cont'd.)

		295.57		
29+50			9.0	286.5
30+00			11.1	284.4
+50			13.5	282.0
P	0.30	282.65	13.22	28235
31+00			2.7	279.9
+50			3.3	279.3
32+00			3.5	279.1
+50			3.4	279.2
+57.85		⊼ PT	4.0	278.6
		ⓑ Spk	3.23	279.42
SET TBM			5.52	277.13
33+00			6.0	276.6
+42		36" San Diego 2nd Main		
+42			9.1	273.5

Spk in Pole #178289
9' LT 32+57.85

13.4 / 10	9.0 × Shldr	8.9 / 2 Edge AC	8.8 / 5
14.5 / 10	×	10.9 / 2 Edge AC	10.9 / 5
18.9 / 10	×	13.2 / 1.0 Edge AC	13.2 / 5
8.7 / 6.	×	1.8 / 3 Shldr	1.75 / 4 Edge AC / 5
6.7 / 5	×	2.6 / 2 Shldr	2.4 / 5 Edge A.C.
7.7 / 5	×	2.4 / 2 Shldr	2.2 / 5 Edge AC
7.3 / 10	×	3.0 / 2 Shldr	3.0 / 4 Edge A.C (2" Thick) / 3.0 / 5
7.8	×	3.2 / 2 Shldr	3.2 / 4 Edge AC / 5
8.6 / 10	× Shldr	5.7 / 1 Edge A.C	5.7 / 5

RADIO ROAD.
(Cont'd.)

		282.65							
33+50		9.2	273.4						
				11.8		9.3	9.3		
				10		× Shldr	2 Edge AC.	5	
34+00		12.9	269.7						
				15.6	12.8		12.8		
				10	3	×	5 Edge A.C		
℄ ⑤ NAIL	2.79	272.63	12.81	269.84					
+50		5.6	267.0						
				8.1		5.2	5.2		
				5		×	3 Shldr	5 Edge A.C	
+75		7.4	265.2						
				8.4		5.3	5.6		
				5		×	4 Shldr	6 Edge A.C	
35+00		7.6	265.0						
				8.6		5.3	5.9		
				5		×	5 Shldr	7 Edge A.C	
+50		5.9	266.7						
				9.0		5.4	5.3		
				10		×	3 Shldr	6 Edge AC	
36+00		6.2	266.4						
				9.2		6.0	5.9		
				10		×	1 Shld	3 Edge A.C.	
+50		8.8	263.8						
				11.3		8.5	8.5		
				10		×	1 Shldr Edge AC	5 AC.	
37+00		12.1	260.5						
				15.0	12.2		12.0	12.0	
				10	5	×	2 Edge AC	5	
+50		13.9	258.7						
				22.0	18.0	14.2	12.0		
				15	10	3 ×	5 Edge AC		

RADIO ROAD

		272.63		
41	3.08	262.56	13.15	259.48
38+00			5.3	257.2
+50			4.3	258.2
39+00			4.0	258.5
+50			5.6	256.9
40+00			7.3	255.2
+50			9.2	253.3
41+00			9.9	252.6
+52.65	℄	PT.	12.4	250.1
42	0.89	251.07	12.38	250.18
42+00			2.1	248.9

7.6		4.4	4.3
5		1	5
		Shldr	Edge AC
7.5		4.1	4.0
8		3	5
		Shldr	Edge AC
7.5		4.0	3.9
8		2	5
		Shldr	Edge AC
8.3		5.4	5.2
8		1	5
		Shldr	Edge AC
9.9		7.0	6.9
8		2	5
		Shldr	Edge AC
11.7		8.6	8.5 8.6
8		1	3 6
		Shldr	Edge AC
13.0		9.5	9.5
8		4	5
		Shldr	Edge AC
13.0		10.9	10.8
8		5	6
		Shldr	Edge AC
4.7		1.6	1.5 1.5
8		1	3 5
		Shldr	Edge AC

RADIO ROAD (Cont'd.)

			251.07		
42+50			4.2	246.8	
43+00			5.8	245.2	
+50			10.3	240.7	
44+00			12.8	238.2	
+50			13.3	237.7	
TP		2.42	241.56	11.93	239.14
+53			3.9	237.6	
+53			5.2	236.1	
44+96.24			4.1	237.4	
45+10			4.8	236.7	
SET TBM			1.69	239.87	
TP		11.20	252.64	0.12	241.44
TP		13.36	265.87	0.13	252.51
TP		13.32	279.15	0.04	265.83
TP		7.52	286.56	0.11	279.04
CK BM				4.22	282.34 = 282.13 282.04

SISSON
WALKER

7.0 / 8 × 3.6 Shldr, 3.3 Edge AC, 3.3 / 5

7.7 / 8, 7.1 / 3 × 5.7 / 4 Shldr, 5.5 / 5 Edge AC

11.7 / 8 × 9.6 / 5 Shldr, 9.3 / 7 Edge AC

13.5 / 5 × 12.0 / 4 Shldr, 12.0 / 6 Edge AC, 12.5 AC Shldr, Edge AC

23.5 / 15, 18.2 / 8 × 14.6 / 5 Edge AC

on AC
on AC } 2" Thick

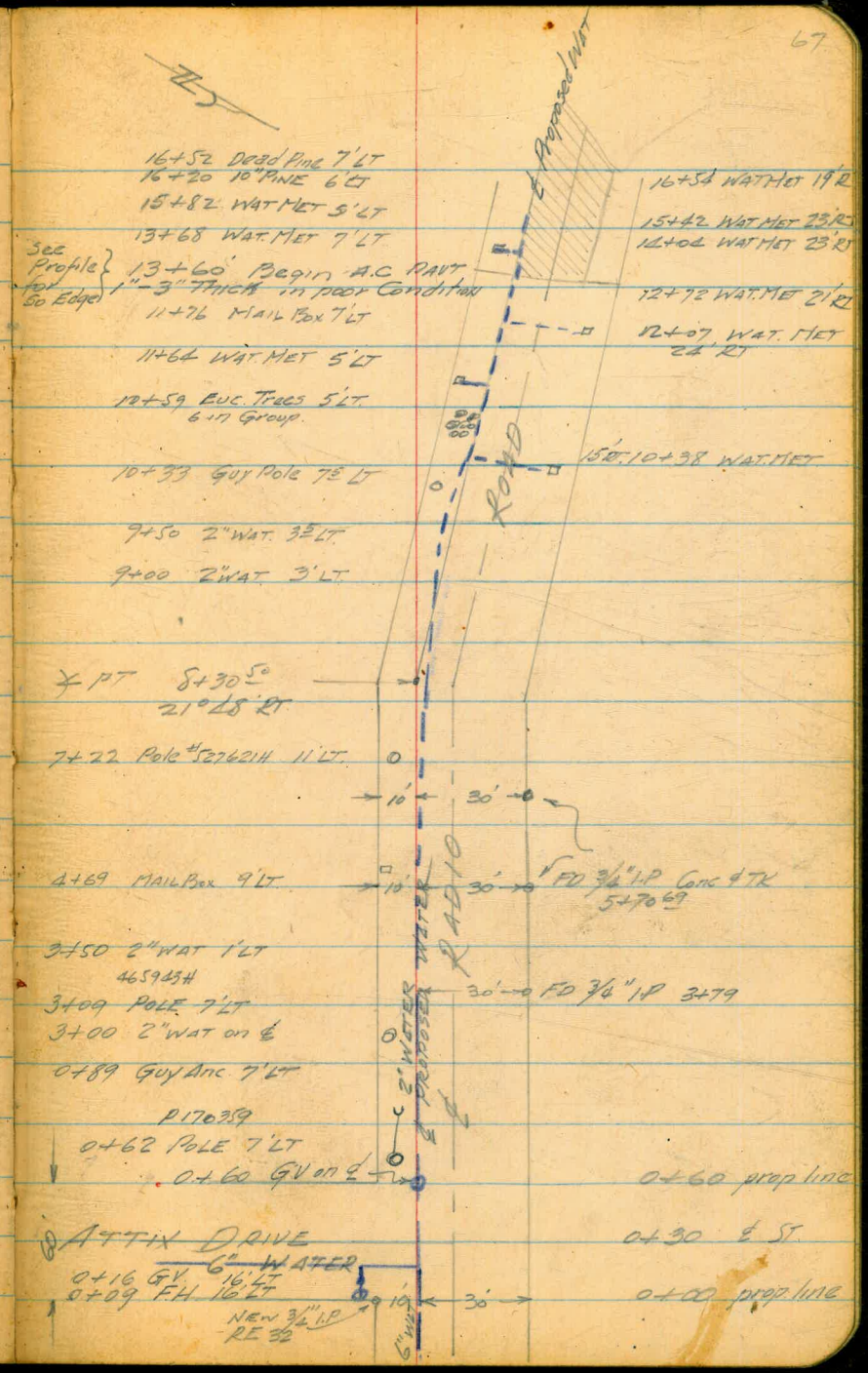
on AC. 1" Thick.

Spk in Tele pole NW Cor 60th & Radio Drive
530382H

RADIO ROAD
ATTIX DR. TO 60TH ST
℄ PROPOSED WATER

8+30 ± ℄ PT. 21°48' RT

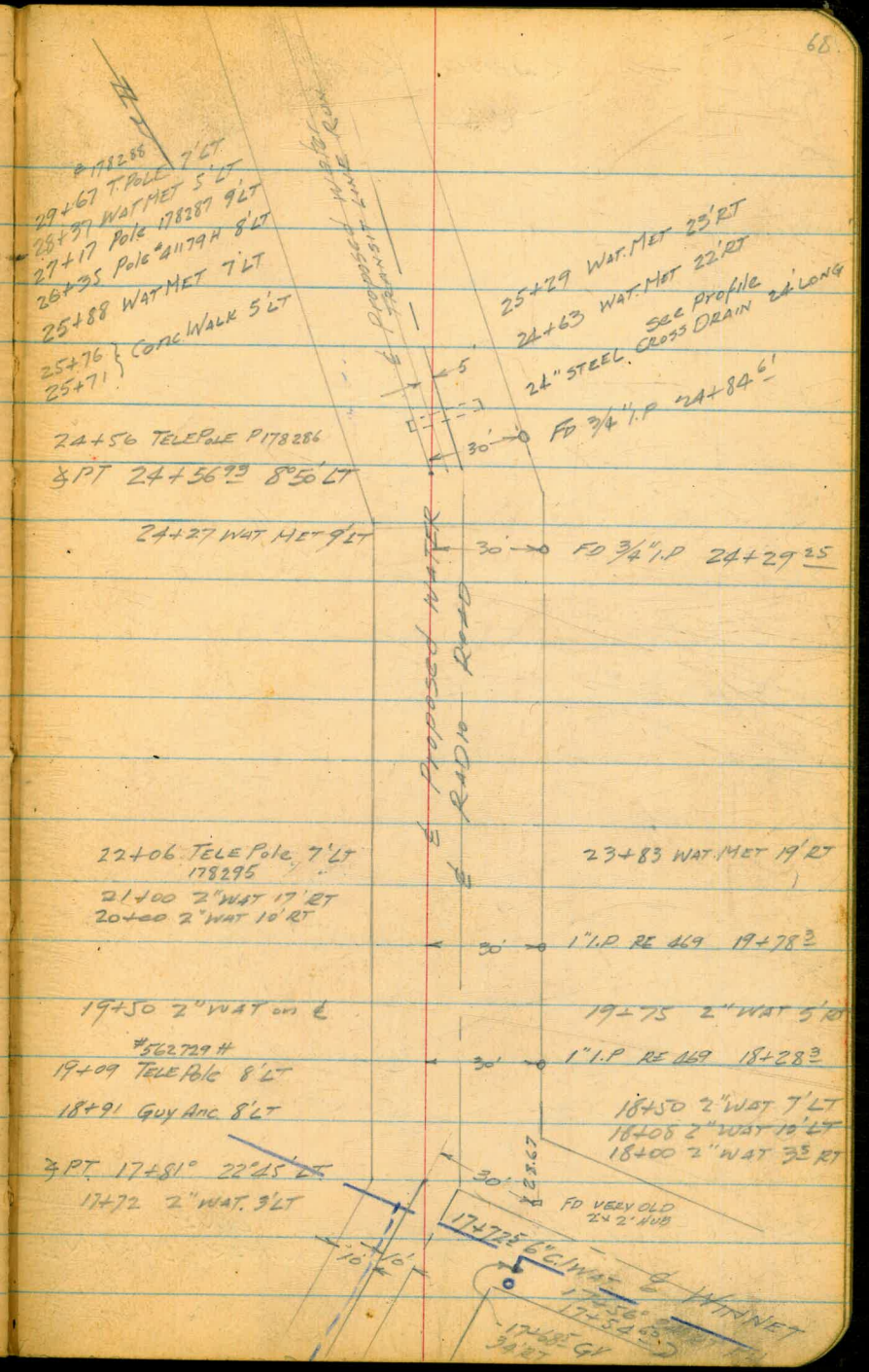
0+00 Est'ly prop line ATTIX DR



RADIO ROAD (Cont'd.)

24+56 93 ℄ PT 8°50' LT

17+81 00 ℄ PT 22°45' LT



RADIO ROAD (Cont'd.)

℄ PT 41+53.65 11°41' RT

32+57.85 ℄ PT 5°30' RT.

32+28.60 Intersn ⑤ TRANSIT LINE WITH ℄ Proposed WATER - BURIAN ST

43+68 T.Pole 1' LT

41+68 T.Pole 9' LT

℄ PT 41+53.65 11°41' RT

39+89 T.Pole 7' LT

38+49 Guy Anc 7' LT

38+20 T.POLE 7' LT

36+76 Guy Anc 7' LT

5627284

36+52 T.Pole 7' LT

34+75 Large Clump Toyon ℄ 6" Line

43+67.0

34+45 T.POLE 8' LT.

36" S.D 2nd MAIN

33+42

Note:- Approx 6' deep to Top of pipe.

℄ PROPOSED WATER TRANSIT LINE RADIO ROAD

34+82 WAT MET 28' RT END ON ℄ 2" WATER

℄ BURIAN ℄ PROPOSED WATER

32+57 2" WAT 3' LT

℄ PT 32+57.85 5°30' RT.

58°30'

FD VERY OLD 2x2 HUB

25'

32+57 T. POLE 8' LT 170-89

32+47 WAT. VAL 4' LT

32+32 Guy Anc 8' LT

31+00 ± WAT 4' LT

0+00

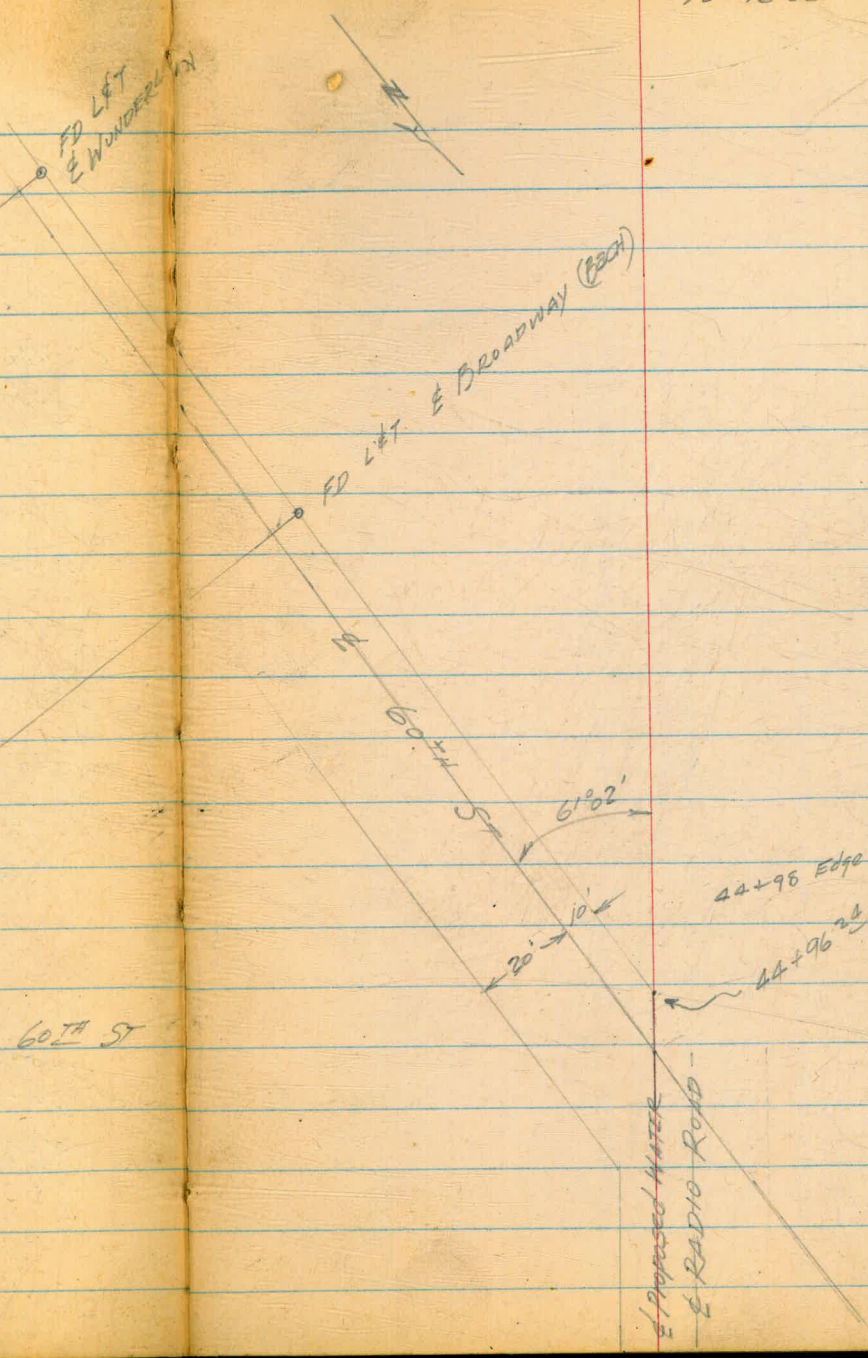
0+17 ± BURIAN

32+28.6 RADIO

5

5

RADIO ROAD
(CONT'D.)



44+96 24 Intsn WITH 10' W ℄ 60TH ST

ALLEY BLOCK 126
NOR of REDWOOD ST.
EAST of 41ST ST.
℄ PROPOSED WATER

7+60 So prop. line Redwood
6+80 Nor prop. line Redwood

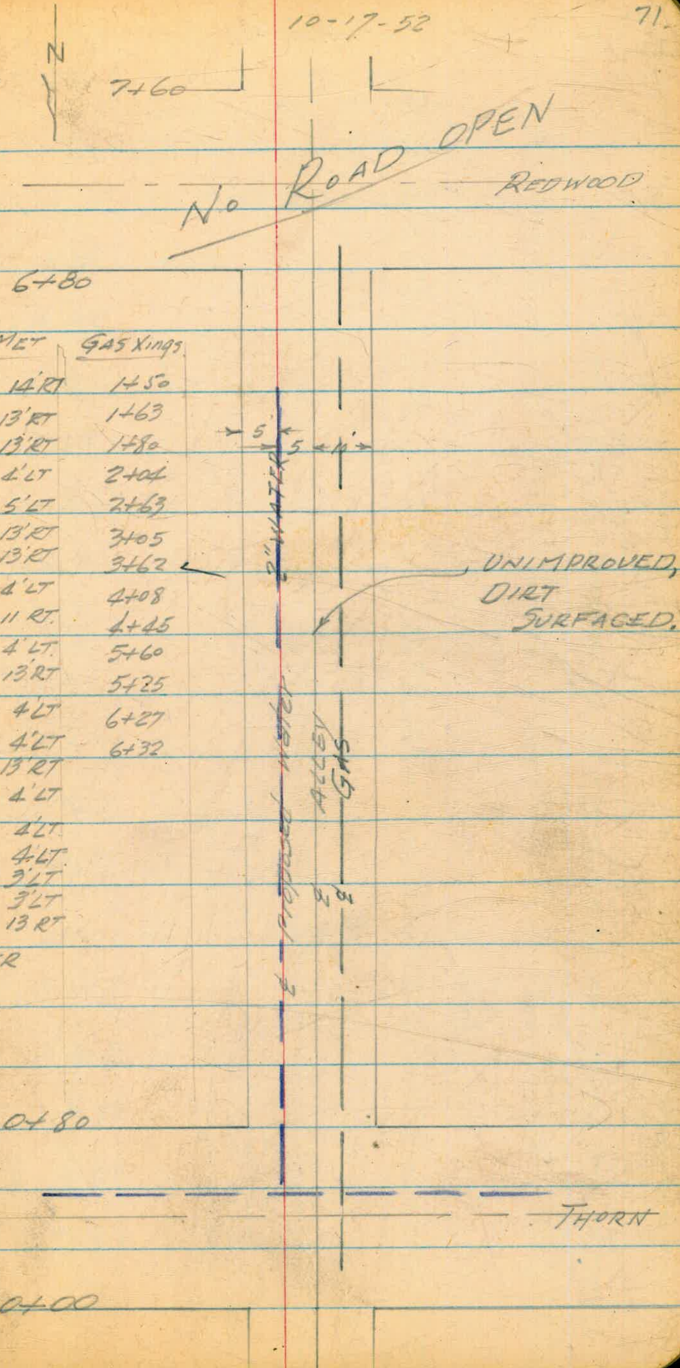
0+80 So prop. line Thorn.

0+00 = Nor prop. line Thorn

BEATTY
POWELL
ALEXANDER

10-17-52

	WAT. MET		GAS Xings
	1+08	14' RT	1+50
2 MET	1+39	13' RT	1+63
	1+79	13' RT	1+80
	1+94	4' LT	2+04
	2+15	5' LT	2+63
	2+42	13' RT	3+05
	2+45	13' RT	3+62
	2+56	4' LT	4+08
	3+02	11 RT.	4+45
	3+07	4' LT.	5+60
	3+41	13' RT	5+25
	3+72	4' LT	6+27
	4+06	4' LT	6+32
	4+06	13' RT	
	4+48	4' LT	
	5+07	4' LT	
	5+54	4' LT.	
	5+67	3' LT	
	5+68	3' LT	
	5+68	13 RT	
	END WATER		



ALLEY BLK 126
Nor. of REDWOOD
EAST of 4 ST.
℄ Profile of Proposed WATER

BM	9.15	310.97	301.82	BP N.W Cor THORN & MADERA
0+00		2.8	306.1	Nor prop line THORN
+14		6.1	304.8	
+40		5.7	305.2	℄ THORN
+66		6.1	304.8	
0+80		5.4	305.5	So. prop line THORN
1+00		4.3	306.6	
+50		2.4	308.5	
2+00		3.0	307.9	
+50		3.3	307.6	
3+00		4.2	306.7	
+50		5.0	305.9	
P 4+00	0.04	304.86	6.15	304.82
+50			0.9	303.9
5+00			2.2	302.6
+50			3.6	301.2
6+00			5.2	299.6
+50			7.1	297.7

ALLEY BLK 126
(Cont'd)

		304.86		
6+80			8.6	296.2
7+00			9.6	295.2
7+60			13.5	291.3
TP.	9.40	302.76	11.50	293.36
CK BM.			0.95	301.81
	18.59		18.00	

Nor prop line Redwood
So prop line Redwood
} NO STREET open.

Alley Blk 126
N of Redwood
E of 41st Stks for 6" AC.

West
Williams ⊼
Varonfakis ϕ
Kump

1-28-54

BP N-W Cor. Thorn & Marlborough

	1170	313.22		301.82			
0+60			8.2	305.0	301.3	C3 7	Begin Work
+70			8.1	305.1	301.5	C3 6	FH Jac
60' FH			8.5	304.7	305.2	FO 5	
1+00			5.3	307.9	303.0	C4 9	
+08			4.0	309.2	307.5	C1 1	WMW
+25			4.8	308.4	304.0	C4 4	
+39			4.4	308.8	308.5	CO 3	WMW
+50			4.8	308.4	304.3	C4 1	
+62			5.0	308.2	308.3	FO 1	WM E
+75			5.1	308.1	304.6	C3 5	
+75			4.4	308.8	308.7	CO 1	WMW
+79			4.8	308.4	308.7	FO 3	WMW
+94			5.2	308.0	308.2	FO 2	WM E
2+00			5.2	308.0	304.2	C3 8	
+15			5.1	307.8	308.0	FO 2	WM E
+42			5.1	308.1	307.9	CO 2	WMW
+46			5.4	307.8	307.8	CO 0	WMW
+50			5.4	307.8	303.3	C4 5	

ALLEY BLK. (CONT) 126

WEST
WILLIAMS
VARONFAKIS
KEMP

1/28/54

75

713.22

2+63		6.0	307.2	307.3	FO 1 WME
3+00		6.4	306.8	302.4	C4 4 -
+01		6.2	307.0	306.9	CO 1 WMW
+06		6.7	306.5	306.6	FO 1 WME
+42		6.9	306.3	306.2	CO 1 WMW
+50		7.0	306.2	301.5	C4 1
+72		7.5	305.7	305.5	CO 2 WME
4+00		8.2	305.0	300.7	C4 3
+05		8.1	304.8	304.8	CO 0 WME
+04		8.2	305.0	305.2	FO 2 WMW
	0.79	304.63	9.38	303.84	M
+47		0.5	304.1	303.8	CO 3 WME
+50		0.5	304.1	299.9	C4 2
+52		0.3	304.3	304.0	CO 3 WMW
5+00		1.8	302.8	299.0	C3 8
+06		2.1	302.5	302.3	CO 2 WME
+33		3.0	301.6	301.7	FO 1 WME
+50		3.2	301.4	297.3	C4 1
+67		3.4	301.2	300.9	CO 3 WMW
+85		4.3	300.3	296.4	C3 9

ALLEY BLK. (CONT.) 126

WEST
WILLIAMS
VARONFAKIS
KEMP

1/28/54

	304.63				
6+00		4.8	299.8	295.0	C4 8
+12		5.3	299.3	298.5	C0 8
+50		6.9	297.7	291.0	C6 7
+61		7.5	297.1	294.1	C3 0
+90		8.7	295.9	288.0	C7 9
7+00		9.4	295.2	288.0	C7 2
+25		10.9	293.7	288.0	C5 7
+50		12.8	291.8	288.0	C3 8
+55		13.3	291.3	288.0	C3 3
(5') FH		12.9	291.7	291.4	C0 3
+61		13.8	290.8	291.1	F.O 3
T.P	8.73	313.34	.002	304.61	
			11.54	301.80=301.82	

WATER

6" G.V.

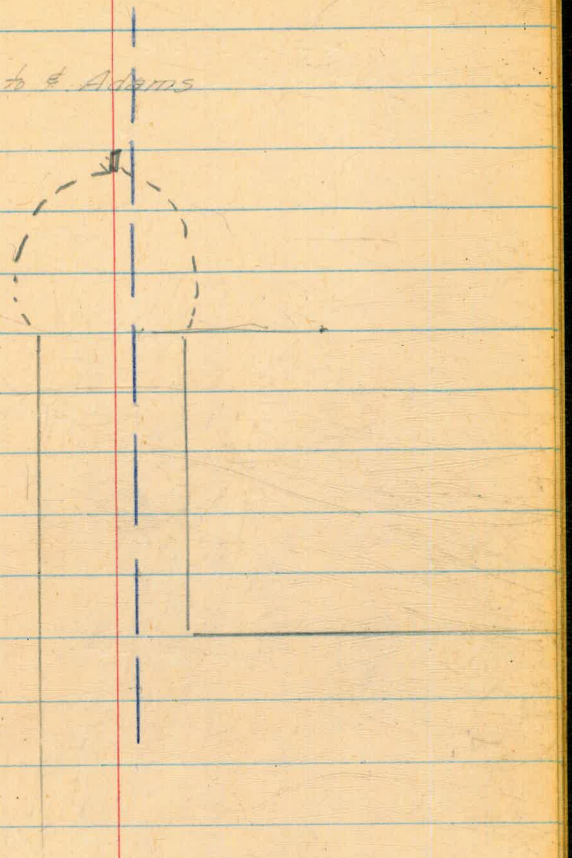
FH TOO

WATER

ADAMS AVE
EL CERRITO TO ASHBY.
ELEV. TOP 6" C.I WATER

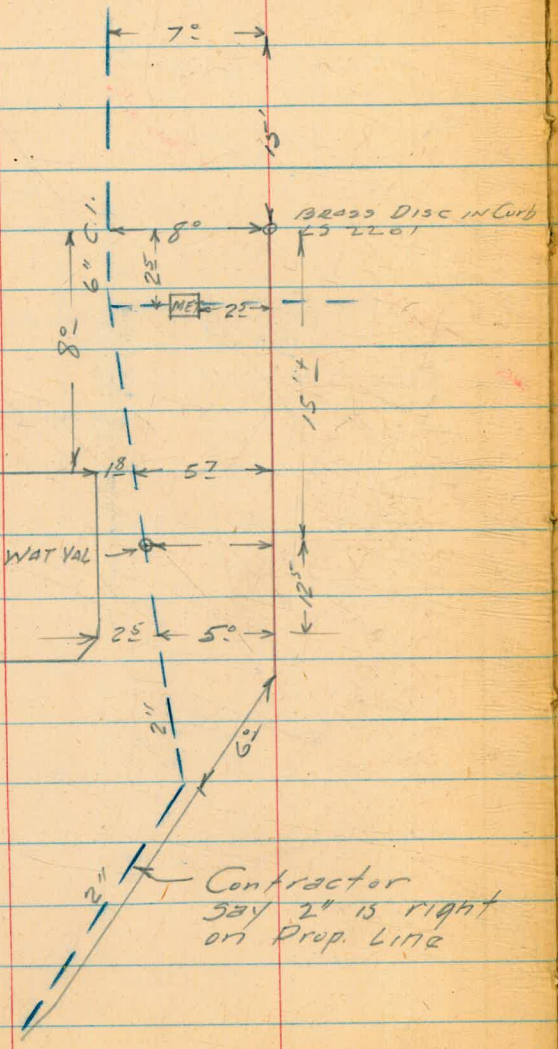
BM		1.89	458.29	456.40
0+00	= W. Prop. line EL CERRITO			
0+49²	Conc. Pavt	2.70	455.59	
	Top Val. Stem	4.20	454.09	
1+10	Nat. Grd.	2.8	455.49	
	Top. Pipe	5.00	453.29	
1+57	Nat. Grd	4.00	454.29	
	Top pipe	5.85	452.44	
1+81	Nat. Grd	5.2	453.09	
	Top Pipe	6.40	451.89	
2+21	Nat. Grd	8.0	450.29	
	Top Pipe	9.32	448.97	
2+38	LATH MK'D E Edge Banjo			
CK BM		1.89	456.40	

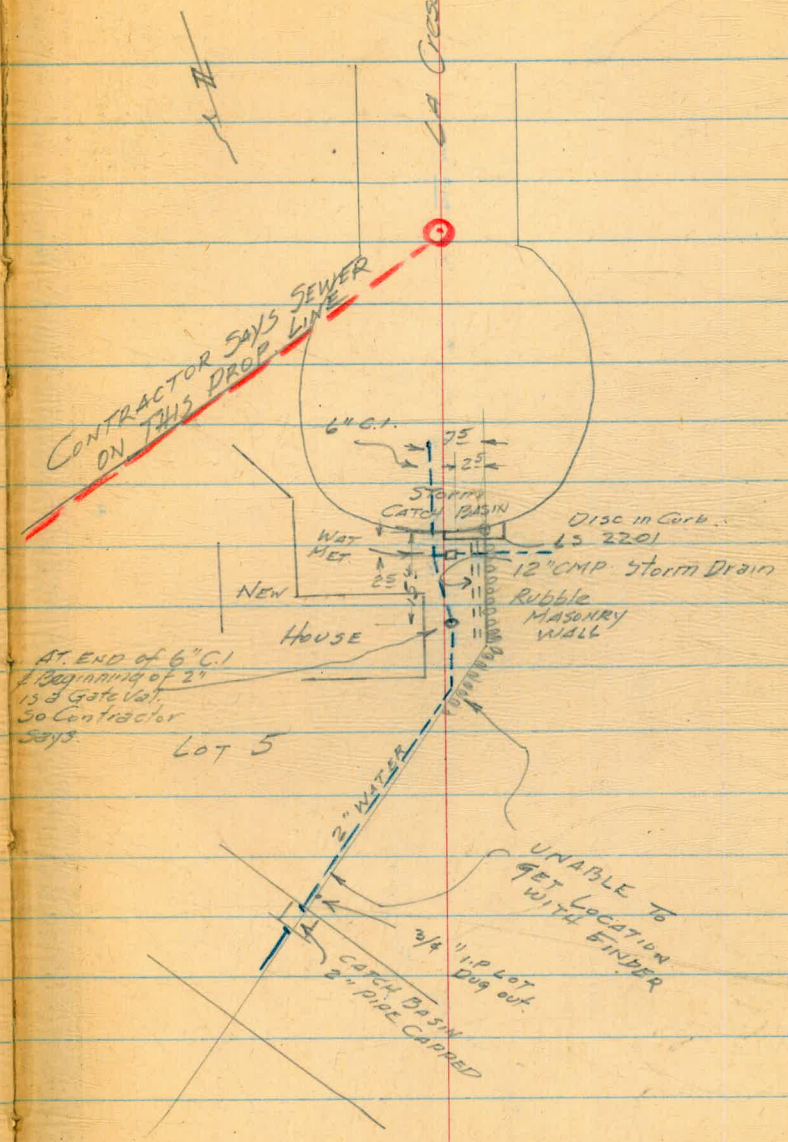
BP. SE Cor El Cerrito & Adams

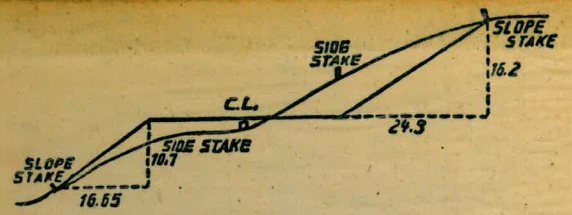


NOV. 16 1951

LOCATION of WATER
LOT 5 ON
LA CRESCENTA DRIVE
RAY CLARK DICKSON.
OWNER. @ EL CORTEZ PONTIAC MOTOR CO







DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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