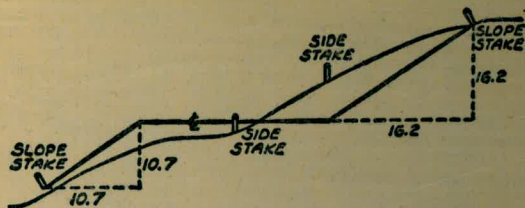


#792



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

JAN 1 1950

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Construction Notes K.M.P.L. #2 1- ✓
 Par. Depth - Umic - Wheatstone - 05 low ✓ 67-71 mod.
 ADDITIONAL X SECTIONS ON K.M.P.L. #2 ✓ 76.

K.M.P.L. #2
8' offset - RT

Level # 5140

King-Notes
Shipman T
West - φ

2-16-58

Clear-cool

①

	4	H1	-		Grade		Cuts
B.M.	0.21	291.48			291.27		Lt. Sta. 231+25
230+79 ⁴⁰			8.1	283.4	279.0		4.4
φ			7.9				
T.P.	0.08	278.64	12.92	278.56			
φ			+1.4				
230+58			0.8	277.8	274.4		3.4
+59 ⁰⁴			+1.2	279.8	275.9		3.9
T.P.	25 0.05	265.96	12.93	265.71			230+44 ⁰⁸ 1.8 φ 1.7 276.8-272.7- 4.1
230+00			1.7	264.3	259.3		5.0
φ			1.8				
T.P.	0.39	253.68	12.67	253.29			
+83 ³⁴			+7.5	260.2	252.4		7.8 φ 47.5
229+65			2.8	250.9	244.6		6.3
φ			2.5				
T.P.	0.24	240.96	12.96	240.72			
+46 ²⁴			+7.3	243.3	236.5		6.8
φ			+2.1				
229+40			0.7	240.8	233.5		7.3
+37 ⁶²			0.9	240.1	232.8		7.3

K.M.P. #2
8 offsets

240.96

229+15

9.3

231.7

~~220.7~~

225.0

♀

9.0

T.P.

0.68

228.69

12.95

228.01

9544

228+15

1.8

226.9

~~224.2~~

221.0

5.9

♀

4.5

7.5

228+50

12.0

216.7

210.7

6.0

♀

12.0

T.P.

0.29

216.09

12.89

215.80

228+30⁵⁰

1.8

214.3

208.7

5.6

♀

1.6

228+60⁶³

7.5

208.6

203.6

5.0

♀

7.2

T.P.

0.85

204²⁴~~34~~

12.70

203.39

227+79⁴⁸

1.7

202.5

198.9

3.6

♀

1.8

227+50

6.5

197.7

194.6

3.1

227+48⁴⁴

6.8

197.4

194.3

3.1

♀ 6.7

King-N.
Shipman X
West

2-16-50

240.96

9.3

8.7

~~8.7~~

231.66

475.4

125.0

57.94

K.M.P.L. #2
8' offsets

King N.
Shipman N
West

2-16-50

3

20424

20424

227+26 12.2 192.0 187.0

5.0 227+390 9.2 195.0 - 191.8 - ^{cut} 3.2

♀ 12.0

T.P. 0.16 192.16 12.24 192.00

♀

227+40 6.9 185.3 180.2

5.1

♀ 7.2

T.P. 0.42 179.65 12.93 179.93

226+73 6.0 173.7 166.6 7.1

♀ 6.3

T.P. 0.24 167.36 12.53 167.12

226+46^{SD} 6.7 160.7 152.7 8.0

♀ 6.4

T.P. 0.31 154.63 13.04 154.32

226+20 7.3 147.3 138.8 8.5

♀ 7.3

T.P. 0.47 142.00 13.06 141.57

K.M.P.L.#2
8.000sets

King N
Shipman
West

2.16.50.

4

142.00

222+80			4.6	137.4	130.1	7.3
♀			4.6			
225+80			12.0	129.2	122.5	6.7
♀			12.6			
T.P.	0.01	129.16	12.85	129.15		
225450			8.3	120.9	114.6	6.3
♀			8.4			
T.P.	0.92	117.28	12.86	116.36		
2257140			2.7	114.6	110.3	4.3
♀			2.3			
224+34 ³⁰			5.5	111.8	106.9	4.9
♀			5.1			
224+34 ⁴⁰			8.3	109.0	104.0	5.0
♀			7.6			
224+25			10.1	107.2	101.0	6.2
♀			10.0			
223+30			15.5	101.8	93.6	8.2
♀			15.3			

N.M.P.L. #2
8' off sets

King
Shipman
West 2-16-50.

11728

223+25 ⁻			13.7	103.6	93.6	10.0
Q			13.9			
223+00			12.7	104.6	98.0	6.6
Q			13.1			
222+00 EC			10.34	106.0	101.2	4.8
T.B.M	6.85 ⁻	119.04	5.15 ⁻	112.13	112.19	50' 14. 221+00
222+73 ³²			13.0	106.0	100.2	5.8 6.2
Q			13.5			
222+53 ⁸⁰			11.7	107.3	101.8	5.5
Q			12.1			
222+33 ⁸⁰			10.3	108.7	103.4	5.3
Q			10.7			
222+14 ⁰⁴			8.4	110.6	105.0	5.6
Q			8.7			
221+94 ²⁷			7.0	112.0	106.4	5.6
Q			7.3			
221+74 ⁰⁰			5.8	113.2	107.9	5.3
			5.7			

K.M.P.L. #2
Profile 8' Offsets

KING
SHIPMAN
WEST

3-2-50

5

119.04

22145976

5.0

114.0

108.8

5.2

♀

5.0

221435

4.6

114.4

109.3

5.1

♀

4.3

T.B.M.

6.85

112.19

K.M.P.L.#2
Profile 5' offsets

King
Shipman
West

3-8-50 clear

7

B.M.	7.91	346.37		338.46	
155+402		1.6	344.8	336.0	8.8
155+445		1.9	344.5	336.0	8.5
155+3455		2.3	344.1	336.0	8.1
155+6447		2.5	343.9	336.0	7.9
155+6892		2.5	343.9	336.0	7.9
155+9849		1.7	344.7	336.0	8.7
156+2891		2.1	344.3	336.0	8.3
+3860		2.5	343.9	336.0	7.9
16849		4.9	341.5	334.5	7.0

Nail in Flood Lite P.P. Next to grate in Ball Park

K.M.P.L. #
Profile 5' off 5 cts

King
West
Shipman

3-8-50

clear

8

74637

156+98 ^{3/4}	7.7	338.7	333.0	5.7
157+58"	8.2	338.2	332.8	5.4
158+17 ^{2/5}	8.1	338.3	332.6	5.7
158+50	8.3	338.1	332.5	5.6
158+85	8.4	338.0	328.1	9.9
159+35	8.5	337.9	328.1	9.8 9.7
159+70	8.4	337.8	322.5	5.3
159+99 ^{1/2}	8.7	337.7	332.5	5.2
160+29 ⁶⁰	8.7	337.7	332.5	5.2 0
160+59 ⁶⁰	8.6	337.8	332.5	5.3

K.M.P.L.#2
Proble 5' offsets

King
Shipman's
West

3-8-50

clear

9

346.37

T.P	12.41	350.16	8.62	337.75		ENGINELEY
160+895 ²			12.2	338.0	332.5	5.5
161+194 ⁴			12.0	338.2	332.5	5.9
161+49 ³⁶			12.2	338.0	332.6	5.4
161+75			11.1	339.1	332.6	6.5
162+04 ⁵⁸			8.1	342.1	337.1	5.0
162+34 ²²			6.3	343.9	339.6	4.3
162+63 ⁹³			3.7	346.5	341.4	5.1
162+93 ⁷³			3.1	347.1	341.8	5.3
163+26 ⁶⁵			2.2	348.0	341.8	$\frac{6.2}{7.2}$

K.M.P. #2
Profile offsets

350.16
346.37

King
Shipman
West

Foggy

10

163+53 ²⁷		1.9	348.3	341.8	6.5
163+83 ⁴⁹		1.6	348.6	341.8	6.8
164+13 ⁰¹		2.3	347.9	341.8	6.1
164+13 ³³		2.5	349.7	341.8	5.9
164+13 ²⁵		2.5	347.7	341.8	5.9
165+03 ¹⁶		2.1	348.1	342.4	5.7
165+16 ⁷⁴		2.2	348.0	342.4	5.6
T.P.	11.86	359.80	2.20	347.94 344.17	
165+23 ⁰⁴		11.9	347.9	342.4	5.5
52 ⁹¹		11.7	348.1	342.4	5.7

K.M.P.L. #2
Profile, 5' offsets

King
West X
Shipman

3-17-58

	359.80			
+82 ⁸⁸	11.7	347.1 347.8	342.4	5.7 2.4
146+12 ⁸⁰	11.7	348.1 349.8	342.4	5.7 2.4
166+42 ⁷²	11.7 11.4	348.1 348.7	342.4	6.3 5.7
166+72 ⁶⁴	11.7	348.7	342.4	1.3 5.7
167+25	10.5 10.5	349.3	342.4	7.2 6.9
+54 ⁹⁰	9.9	349.9	343.5	6.4
+84 ⁸⁶	9.7	350.1	344.7	5.4
168+24 ⁸²	8.8	351.0	346.2	4.8
+54 ⁴³	7.9	351.9	347.0	4.9
84 ³⁷	6.9	352.9	347.9	5.0

K.M.P.L
Profile 5' offsets

359.80

169414³³

6.0

353.8

348.7

5.1

14414

5.1

350.7

349.6

5.1

169474⁰⁴

4.2

353.6

350.4

5.2

170403⁹⁵

3.3

356.5

~~350.8~~
357.0

~~5.7~~
5.5

Changed in field by Rainey - To go over
No 23 - Sewer

170433⁸⁶

2.4

357.4

~~351.6~~
351.6

~~6.2~~
5.8

16378

1.8

358.0

~~351.2~~
352.0

~~6.8~~
6.0

19361

1.6

358.2

~~351.2~~
352.0

~~7.0~~
6.2

171423⁵³

1.6

358.2

~~351.2~~
352.0

~~7.0~~
6.2

171453⁵³

2.1

357.7

~~351.2~~
351.6

~~6.5~~
6.1

TIP

1.82

357.8

358.0

171452¹⁴ - (8)

K.M. P.L. #2
5' offsets

King
West
Shipman

3-21-50

Clear-Cool

13

T.B.M. 0.59 228.63 228.01

Top iron pin

294+74⁵¹ 11.6 217.0 211.5 5.5

T.P. 0.59 216.11 13.11 215.62

294+46⁷⁵ 9.6 206.4
~~6.5~~ 200.8 5.6

T.P. 0.57 207.95 12.73 203.38

294+28⁷⁰ 4.6 199.4 192.5 6.9

T.P. 0.52 191.47 13.00 190.95

294+61² 3.8 187.7 179.6 8.1

293+78 13.8 177.7 167.8 9.9
~~9.8~~

293+44⁵² 17.8 173.7 167.0 6.7

27708

4

191.47

T.P. 12.45 203.76 0.16 191.31

297+09^H 12.9 192.9 187.9 5.0

292+92⁸⁶ 1.3 202.5 198.4 4.1

T.P. 12.72 215.76 0.72 203.04

292+75⁰⁴ 2.3 213.5 208.2 5.3

T.P. 13.09 228.63 0.22 215.54

+57⁰³ 5.1 223.5 217.5 6.0

T.P. 12.79 240.48 0.94 227.69

+40 7.4 233.1 226.8 6.3

+21⁹⁶ 0.5 240.0 234.8 5.2

K.M.P. 2 #2
5' offsets

KING
Shipman
West T

3-21-50

clear-600 15

240.48

T.P 11.77 251.77 0.50 239.98

ON GINNEY

291498³²

3.3 248.5 243.2

5.3

T.P 12.94 264.36 0.35 251.42

291484⁴⁵

12.2 252.2 247.2

5.0

T.P 13.05 277.41 0.00 264.36

T.B.M

0.20 277.21 277.08

ON 280 400

13.25 265.45

252.2

ON GINNEY 291484⁴⁵

291489²⁷

9.7 255.8 250.1

5.7

291462²⁴

9.0 251.5 251.4

5.1

Page 24

K.M. P.L. #2
5' OFFSETS.

King
SHIPMENT
West

3-21-50

clear 1/2

T.B.M.	0.48	358.46		357.98		
171+83 ⁴⁵			1.4	357.1	357.2	5.9
172+13 ³⁰			2.5	356.0	355.8	5.2
+43 ¹⁸			3.9	354.6	349.4	5.2
+75 ⁰⁶			5.6	352.9	348.0	4.9
173+02 ⁹²			7.5	351.0		4.8
			6.5	352.0	346.2	5.8
+32 ⁷⁸			9.2	349.3	344.4	4.9
+62 ⁶⁴			11.1	347.4	342.5	4.9
+92 ⁵⁰			12.9	345.6	340.9	4.7
T.P.	1.25	346.78	12.93	345.53		

K.M.P.L. #2
5' OFFSETS

King
Shipman/W
West

3-21-50

Clear

17

346.78

174+22 ²⁰			3.0	343.8	338.9	4.9 5.0
752 ¹⁴			4.9	341.9	338.0	4.9 5.0
72 ⁰²			6.1	340.8	335.8	4.9 5.0
175461 ⁰⁸			7.9	338.9 339.6	334.0	4.9 5.0
B.M.	0.82	339.63	8.60	338.18	338.21	
175+31 ²⁵			1.8	337.2	332.4	4.8
175461 ⁶⁰			3.1	335.9	331.1	4.8
175745 ⁰⁵			3.2	335.8	330.5	5.3
176140 ⁸²			4.0	335.6	328.1	6.9
176+34 ⁶⁴			7.0	332.6	325.7	6.3

355.8
354.7
351.1

Top F.H. Ultra 9 05/er corrected up

Top Gas El. 331.1

6.3
CONT. 19

K.M.P.L. #2
B.O. - 159430

King
Shipman
West

3-22-50

Clear - Hot.

T.B.M 5.34 343.24 9.11 337.90

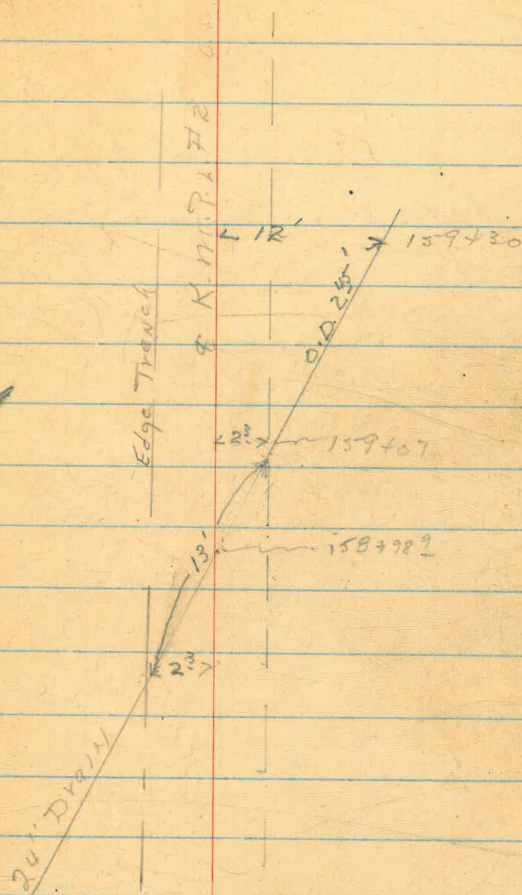
Top 24" Drain East Side Ditch 9.21 334.03

O.D. Pipe 2.45

Top 24" @ K.M.P.L. 9.12 334.12

Top 24" West Side Ditch 9.10 334.14

5.33 337.91



K.M.P.L. #2
5' offsets

339.03

King
West
Shipman

3-22-50

clear

19

174+64⁴⁶

10.3

328.7

323.2

5.5

176+94²³

12.6

326.4

321.3

5.1

T.P.

1.94

328.49

12.48

326.55

177+24¹¹

3.6

324.9

319.9

5.0

45401

4.4

324.1

318.9

5.2

178+00A

5.2

323.3

317.4

5.9

T.P.

0.48

324.02

4.95

323.54

4 Nail Sta. 178

178+28⁹²

1.1

322.9

317.2

5.7

178+31 Top 995 El. 318.3

178+33 7 115' Water El. 318.4

178+70

2.0

322.0

317.0

5.0

178+99⁹⁹

2.5

321.5

316.5

5.0

K.M.P.L. #142

18" Storm Drain Removed
Sta 155+02

~~T.B.M. 1.80 351.70 349.96~~

~~167+61' 4.65 347.05~~

~~167+62' 4.95 346.75~~

~~167+64' 7.93 348.78~~

~~Fl. Pipe
167+62 343.7~~

T.B.M. 5.96 349.8 343.9

Bottom West End Pipe 8.6 341.2

Bottom East End Pipe 8.0 341.8

King
Shipman
West

3-29-58

~~5' offset - 167+57.90~~

~~Top 99'~~

~~Top Water - O.D. 94'~~

~~Top Sewer~~

End Pipe
K.M.P.L.
155+72.5

ON GINNEY 155+64

Past our Ditch

90

18" DRAIN

154+92.5 End Pipe Drain

K.M. P.L. #2
 Grades on Pipes uncovered
 at Clinic + Osler St.

T.B.M.	1.80	351.70	349.90
167+67'		4.65	347.0
167+67'		4.95	346.7
167+64'		7.92	343.78
167+62' Bottom Pipe			343.7

King
 Shipman
 West

3-29-50

5' offset G. N. Hwy 167+54.90

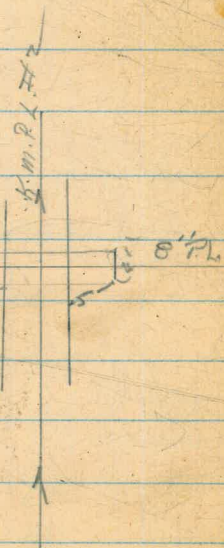
Top 2" Gas. O.D. .28'

Top 10" Water Pipe O.D. .94'

Top 8" Sewer

Co. Plays

Backfilled with sand
 by contractor



K.M.P.L #2

32102

179+29⁰²

2.9

321.1

~~315.8~~
~~315.5~~179+39⁶⁵

3.4

320.6

~~315.8~~
~~315.5~~+89⁵⁶

3.9

320.1

~~315.5~~
~~314.8~~180+19⁴⁷

4.4

319.6

~~314.8~~
~~314.3~~+29³⁸

4.6

319.4

~~314.4~~
~~314.0~~+59²⁶

5.1

318.9

312.6

69¹⁷

5.3

318.7

312.1

+89⁰⁸

5.7

318.3

311.5

98⁹⁷

5.9

318.1

311.3

181+10⁰⁸

6.8

317.2

310.9

King
Shipment
West

3-27-50

22

~~5.2~~
~~5.2~~~~5.1~~ 4.8
~~5.2~~~~4.6~~
~~5.5~~~~4.8~~
~~5.3~~~~5.0~~
~~5.4~~

6.3

6.6

6.8

6.8

6.3

Grade Change IN Field
3-31-50 - Rainy179+82⁵ - 316.1 Top 1" Water

179+83 315.3 " Sewer

179+83⁵ 316.1 - " 3/4" ggs180+77² ggs

E1-316.0

180+79² Water

E1-316.0

K.M.P. L.#2
Profile 5' OFF

King
Shipman
West

3-27-50

23

329.82

181448²⁰

8.6

315.4

309.9

5.5

+7860

10.2

313.8

308.7

5.1

182408⁴⁷

11.5

312.5

307.6

4.9

182440^{38 49}

12.5

311.5

306.4

5.1

T.P.

2.93

~~314.00~~
315.00

12.95

~~311~~
312.07

+68⁷⁹

3.7

310.3

305.2

5.1

+9819

4.9

309.1

304.0

5.1

183428⁸⁸

6.1

307.9

302.7

5.2

L32⁵⁹

7.1

306.9

~~301.4~~
301.8

~~4.9~~
5.1

4-6-50
changed in field to clear 50' or

L38⁸¹

7.2

306.8

~~301.2~~
301.8

~~5.0~~
5.1

+93⁷³

7.5

306.5

~~301.2~~
301.8

~~4.7~~
5.1

K.M.P.L. #2
Profile 5' off

K.M.P.
Shipman
West

3-27-50

24

314.00
~~315.00~~

T.P.

4.56

309.44
~~310.44~~

E.H. Osler & Wheatstone

CONT From P.15

M.H.

265.45

291+72⁵⁷

4.7

260.8

258.0

5.8

40287

1.4

264.1

258.6

5.5

T.P.

12.68

278.02

0.11

265.34

290+73⁷

10.9

267.1

262.2

4.9

T.B.M.

0.78

277.24

277.21

K.M.P.L #2

Profile 5' off

King
Shimney
West

3-31-50

cloudy-cool

25

T.P 4.01 303.45 309.44

Top of H. Asbest. White Stone

18442365 6.4 307.1 301.9
301.25.3
5.9

18422-995

Elev.

302.9 - Top Pipe

302.9 " 6" "

301.6 " Sewer

18445348 5.1 308.4 301.4
301.27.0
7.0184072 Water
184722 Sewer

18449340 4.4 309.1 301.2

7.9

184494⁸⁵ 4.2 309.3 301.2

8.1

Eoaf 8

184453³⁷ 4.2 309.3 301.2

8.1

184 832 5.3 308.2 301.2

7.0



+9305 6.0 307.5 301.2

6.3

185402⁸¹ 6.7 306.8 301.1

5.7

185432⁶³ 9.7 303.8 298.7

6.1

K.M.P. #2
PROF 145' OFF

King
Ship Max
West X

3-31-50

76

313.45

185+12.5

12.5

301.0

296.4

4.6

.04
24
7.00

T.P.

0.54

300.94

13.01

300.44

185+72.3

1.0

299.9

295.6

4.3

185+91.3

2.6

298.3

293.1

5.2

186+06.2

4.6

296.3

290.3

6.0

186+20.6

7.1

293.8

286.5

7.3

+35.2

9.9

291.0

283.7

7.3

+48.4

11.8

289.1

282.5

6.6

28
28.5

T.P.

7.41

296.39

11.96

288.98

186+199.1

9.7

286.7

281.4

5.3

K.M.P.L. #2
Profile 5' OFF

King
West
Shipman

3-31-50

cool-cloudy

27

296.39

186+9980

11.0

285.4

281.4

4.0

6000
186+9980 285.4

+ 6.02

291.42

- 7.46

283.96

+ 7.04

291.00
top chamber

187+1971

10.4

286.0

281.9

4.1

187+4953

8.5

287.9

283.0

4.9

187+7943

7.7

288.7

284.1

4.6

188+0925

7.2

289.2

285.2

4.0

188+3915

6.4

290.0

286.2

3.8

+6905

4.6

291.8

287.3

4.5

188+9898

3.7

292.7

288.4

4.3

189+2878

2.6

293.8

288.5

5.3

+5870

2.3

294.1

288.5

5.6

Blow off chamber
sta 186+96

K.M.P.L.#2
Profile - 5' off

King
West
Shapiro

3-31-50

cool cloudy

28

296.39

189+8862

1.8

294.6

288.5

6.1

T.B.M.

11.62

306.20

1.81

294.58

5' off set + given way 189+8862 on old B.C. offset

1.99

304.31

304.4

OK on old B.C. Order St.

T.B.M.

2.80

297.38

294.58

190+1849

2.8

294.6

288.5

6.1
5.1

+4831

3.0

294.4

288.5

5.9

+7819

3.0

294.4

289.5

4.9

191+0825

2.3

295.1

290.2

4.9

+3725

2.1

295.3

290.2

5.1

+6721

1.4

296.0

290.2

5.8

CONT. P32

Pg 32

K.M.P.A. #2
 X-Sections ON Ditch Cave IN
 East of Ulric St.

Krupp
 West
 Slupman

4-4-50

291.

L.T.

R.L.

4.00

354.10

358.1

ON ground 167184

16549.89 Δ

12.0

$\frac{6^2}{8'}$

$\frac{12^2}{5'}$

$\frac{12^2}{5'}$

$\frac{6^2}{5'}$

165450

12.6

IN Bell
 Hole

$\frac{6^2}{8'}$

$\frac{12^2}{2^2}$

$\frac{12^2}{2'}$

$\frac{6^2}{8'}$

166400

11.6

342.5

Top Sanel

$\frac{6^2}{6'}$

$\frac{11^2}{2^2}$

$\frac{11^2}{2^2}$

$\frac{6^2}{7'}$

166450

11.8

$\frac{5^2}{5'}$

$\frac{11^2}{2^2}$

$\frac{11^2}{2^2}$

$\frac{5^2}{6'}$

166461

11.8

End Cavein

$\frac{6^2}{2^2}$

$\frac{11^2}{2^2}$

$\frac{11^2}{2^2}$

$\frac{5^2}{2^2}$

4.00

358.1

K.M.P.L. #2
Check on 24" Drain
167+25

4-5-50

KING
Shipman
West

20

7.8.17

4.15

354.05

349.90

ON 5' OFFSET - 167+51'

12.0

342.0

Grade
342.4

Top Sand - 167+25

6.85

347.2

Top 24" Drain 347.2 Shows on City Plan

9.05

345.0

Top K.M.P.L. O.D. 2.82

Check on 6" Pipe - Nye St.

Lowered by City

T.B.M.

4.0

324.9

322.9

7.2

315.7

Bottom Hole dug by City

8.5

318.4

Top existing 6" Pipe

9.9

317.0

Bottom K.M.P.L. Ditch as dug

317.2

K.M.P.L.

K.M.P.L. #2
 Proche-Top Pipe
 For Extra Sand

WING
 SHIPMAN
 WEST

4-6-56

clear hat

31

T.B.M.	7.25	357.78		350.10
			9.7	348.01
167+84 ⁸⁰			8.8 9.5	340.6 347.9
169+24 ⁵			8.5 8.8	348.9 348.6
168+54 ⁵³			7.5 8.5	349.9 348.9
167+84 ³³			6.8 7.5	350.6 347.9
167+14 ⁹³			6.8	350.6

167+84⁸⁰ ON 9" X 1" NAY

Top 3" Pipe - raised by City at Ulric St.

K.M.P.k.#2
5' offsets

Kin
West
Shipman

4-7-50

Cold-cloudy

32

297.38

19149725

1.5

295.9

290.2

5.7

19242764

1.8

295.6

289.7

5.9

+5958

2.9

294.5

289.2

5.3

+89

4.0

293.4

288.3

5.1

193+17

4.1

293.3

287.6

5.7

+47.08

3.8

293.6

287.5

6.1

+76.93

3.3

294.1

287.5

6.6

194+06.84

3.3

294.1

287.5

6.6

+36.82

3.8

293.6

287.5

6.1
8.4

66.46

5.0

292.4

287.0

5.4

K.M.P.L.#2
5' offsets

King
West
Shipman

4-7-50

clear-cloudy

33

297.38

1944 962		5.5	291.9	286.0	5.9
1954 26 ¹⁵		8.2	289.2	284.6	4.6
5					
55 ²²		9.5	287.9	283.2	4.7
85 ²³		10.6	286.2	281.9	4.9
1964 15 ⁴⁸		13.0	284.4	279.3	5.1
1964 15 ⁴⁸ T.P.	5.00	289.43	12.95	284.43	
E.C. 1964 35 ²¹		7.8	281.6	278.0	3.6
165 ³²		10.1	279.3	278.0	1.3
+95 ¹⁵		10.5	278.9	278.0	0.9
1971 24 ²⁸		10.3	278.1	278.0	1.1

K.M.P. #2
5' off sets

King
Shipman
West

4-7-50

Cold-cloudy

34

289.43

1974 54 ⁹⁰	9.3	288.1	278.0	2.1 [✓]
	6.3	283.1		
84 ⁸²	6.3	283.1	278.0	5.1 [✓]
1984 14 ⁷⁸	3.3	286.1	278.0	8.1 [✓]
B.C. +29 ⁵⁶	2.4	287.0	278.0	9.0 [✓]
+59 ⁸²	2.1	287.3	278.0	9.3 [✓]
+59 ⁸⁰	2.1	287.3	278.0	9.3 [✓]
1994 15 ⁷⁴	5.6	283.8	277.5	6.3 [✓]
+48 ⁸³	9.0	286.4	275.0	5.4 [✓]
+72 ⁸²	10.2	279.2	275.0	4.0 [✓]
EE 2004 08 ²²	9.8 9.25	288.1	275.0	5.1 [✓]

K.M.P.A. #2
5'0 FFsets

K.M.P.A.
Shannon
West

4-7-50

Cold-

35

289.43

2950	7.0	282.4	275.0	7.4'
2001	7.2	282.2	275.0	7.2'
+50	11.3	278.1	275.0	3.1'
202	12.0	277.4	275.0	2.4'
+50	10.1	279.3	275.0	4.3'
203	8.8	280.4	275.0	5.6'
+50	10.1	279.3	275.0	4.3'
204	11.9	277.5	275.0	2.5'
+50	10.2	279.2	275.0	4.2'
205	8.3	281.1	275.0	6.1'

N. N. P. L. # R
50 Offsets

289.43

205+31^E

7.1

282.3

275.0

7.3

B. N.

1.37

284.62

6.25

283.18

288.25

ON CORN. MAX. 10' RT 205+40⁺

205+46^H

1.2

283.4

275.0

8.4^v

206+00

0.7

283.9

275.0

8.9^v

206+50

1.7

282.9

275.0

9.9^v

206+75⁸⁵

3.5

281.1

275.0

6.1^v

206+90⁵⁴

4.8

279.8

274.1

5.7^v

207+20¹⁸⁰

8.1

276.5

270.0

6.5^v

207+49⁶⁶

13.0

271.6

265.9

5.7^v

T.P.

0.72

271.91

13.03

271.59

King
Shirman
West

4-7-50

cold-cloudy

38

K.M.P.L.#2
5' offsets

King
West
Shipman

4-13-58

Clear

37

271.91

208+60

10.5 241.4 256.0 5.9

T.P. 0.84 259.66 13.09 252.82

208+50 7.6 252.1 246.1 6.0'

T.P. 0.46 252.51 7.61 252.05

208+7657 5.8 246.7 240.3 6.4'

209+04⁴⁴ 8.9 243.6 237.4 6.2'

T.P. 0.27 239.87 12.91 239.60

209+33.84 2.0 237.9 231.7 6.2'

+63'' 7.7 232.2 225.5 6.7'

T.P. 0.65 227.3 12.79 227.08

K.M.P.L. # 2
5' offsets

King
Shipton
West

4-14-50

Clear

78

2273

209+92⁴¹

1.7

226.0

219.7

6.3 ✓

210+217³⁵

7.6

220.1

213.6

6.5 ✓

T.P.

0.01

215.00

12.74

214.99

2104 80⁹⁵

1.4

213.4

207.1

6.3 ✓

210+80³⁸

7.9

207.1

201.7

5.4 ✓

210+99⁸¹

12.1

202.9

198.1

4.8 ✓

T.P.

0.64

203.57

12.07

202.93

211+290⁶

6.7

196.9

191.8

5.1 ✓

211+85³⁵

12.6

191.0

185.7

5.3 ✓

T.P.

0.65

191.59

12.63

190.94

K.M.P.L.H.

King
Shipman
West

4-14-50

Clear 39

191.59

2 211+8793 6.2 185.4 180.1 5.3 ✓

2 212+1710 11.8 179.8 174.4 5.4 ✓

T.P. 1.17 180.07 12.69 178.90

2 212+4644 6.0 174.1 168.5 5.6 ✓

2 212+7599 12.4 167.7 163.8 3.9 ✓

T.B.M. 0.21 172.72 7.47 172.60 172.51 B.M.P.L. 212+72 - corrected E.I.

213+0033 9.4 163.3 160.2 3.1

2 T.P. 0.72 160.65 12.79 159.93

2 213+2991 1.8 158.9 154.6 4.3

213+597 7.3 153.0 149.0 4.4

K.M.P.L #2
5' OFF

King
Shipman
Worst

4-14-52

40

16065

2	21377866		11.5	149.2	145.2	4.0
2	T.P.	0.64	148.29	13.04	147.61	
2	213797 ⁹⁹		13.6	144.7	141.2	3.5
2	21472 ¹		7.9	148.4	136.3	4.1
2	214736 ³⁹		12.0	136.3	131.2	5.1
	T.P.	1.02	136.28	13.03	135.26	
	214755 ⁵⁷		4.2	132.1	126.1	6.0
2	77475		8.5	127.8	121.0	6.8
	T.P.	1.16	124.57	12.93	123.35	
	79393		1.5	123.0	116.0	7.0

K.M.P.L # -
5' offsets

King
Shipman
West

4-14-50

41

12451

215413 ^E	6.5	118.0	111.0	7.0
215432 ^E	11.1	113.4	106.9	6.5
24779	13.1	111.4	104.4	7.0
475 ⁰²	13.6	110.9	104.4	6.5
492 ³⁰	12.3	112.2	105.7	6.5
216412 ⁷	11.1	113.4	107.2	6.2
43193	10.4	114.1	108.2	5.9
457 ⁷¹	10.5	114.0	108.4	5.6
47155	10.5	114.0	108.6	5.4
49139	10.5	114.8	108.7	5.3

R.M.P.H #2
5' offsets

124.51

217+1125

10.2

114.3

108.9

5.4

43107

9.9

114.6

109.1

5.5

T.P.

5.39

120.06

9.84

114.67

51440404EC

7.85

112.21

112.19

Grade Top Box

2154557
+12.19

2.34

116.94

114.60

114.0

9.6

107.34

114.0

F666 Top Box

Grade Top Box

5.15

108.75

103.60

12.15

96.60

105.0

8.40

King
Shipman
West

4-14-50

KL

K.P.L.P.R.
Thickness of Sto. Oil Pav. & Conc. Pav.
Utric - wheatstone -

King
West
Shipman

4-19-50

43

167447 to 168435 8" Oil Pav.

168435 to 178410 6" Oil Pav.

178410 to 178435 8" Oil

178435 to ~~181473~~ 6" Oil

181473 to ~~181483~~ 10" Oil

181483 to ~~183455~~ 6" Oil

183455 to ~~184487~~ 6" Conc.
1" Oil

184487 to 184430 6" Oil

K.M.P.L. #2
5 OF 808

King
West
Shipman

4-20-50

Fog

44

T.B.W.	8.96	300.23		291.27	50' Lt. 230+25	
231409			12.3	287.9	283.9	4.0
231430 ⁶			8.4	291.8	287.3	4.5
231460 ³²			4.4	295.8	291.2	4.6
231499 ⁴⁹			0.5	299.7	295.0	4.7
T.P.	10.00	309.69	0.54	299.69		
232+290 ⁰⁰			8.4	301.3	297.0	4.3
232+87 ¹⁰			7.4	302.3	297.1	5.2
4890 ²			7.0	302.7	297.1	5.6
233+16 ⁹⁴			6.6	303.1	297.2	5.9

K.M.P.L.#2

S'offsets

KING
Shipment
West

Fog:

45

		309.69				
23344 ⁸⁴			6.2	303.5	297.5	6.0
23347 ⁷²			5.0	304.7	299.2	5.5
23470 ⁶⁰			3.3	306.4	300.8	5.6
+3647			1.7	308.0	302.5	5.5
T.P.	12.95	322.40	0.24	309.45		
46632			12.8	309.6	304.5	5.1
+9616			10.2	312.2	306.6	5.6
23542 ⁸			7.9	314.5	308.7	5.8
+55			6.1	316.3	310.7	5.6
+8560			4.6	317.8	312.3	5.5

K.M.P.L #2
5' offsets

King
Shipman
West

4-20-50

Fog.

46

322.40

236+15⁵⁰

3.5

318.9

313.5

5.4

+45⁴⁰

2.7

319.7

314.6

5.1

+75³¹

1.6

320.8

315.3

5.5

T.P.

5.70

327.17

0.93

321.47

237+05²²

5.2

322.0

316.0

6.0

+35¹³

4.9

322.3

316.6

5.7

+65⁰⁴

4.2

323.0

317.0

6.0

+94⁹⁷

4.2

323.0

317.0

6.0

238+24⁵⁰

4.0

323.2

317.0

6.2

+54⁷²

4.0

323.2

317.0

6.2

K.M.P.L.#2
5' offsets

King
Shipman X
West

4-20-50

Fog.

47

32717

+84.6y	4.0	323.2	317.0	6.2
239 ↓ 145y	4.2	323.0	317.0	6.0
+44.7y	4.4	322.8	317.0	5.8
+74.4y	4.5	322.7	317.0	5.7
240 + 250y	5.0	322.2	317.0	5.2
+34.7y	5.5	321.7	316.5	5.2
+64.4y	5.9	321.3	316.0	5.3
+94.2y	6.4	320.8	315.4	5.4
241 + 245y	6.8	320.4	313.7	6.7
+54.7y	7.1	320.1	312.0	8.1

K.M.P.L. #2
5' OFFSETS

King
Shipment
West

4-20-50

Fog.

48

5,72

327.17

+6929	7.5	319.7	312.0	7.7				
+7330	(7.58)	319.6 Valve Box	312.0	7.6				
+8950	7.6	319.6	312.0	7.6		9.84		
242415 ⁵⁰	8.1	319.1	312.0	7.7				
242450	8.7	318.5	312.0	6.5				
+7992	8.9	318.3	311.7	6.6				
243409 ⁸⁴	9.6	317.6	311.4	6.2		2.67	329.89	527.22
+3978	10.1	317.1	311.1	6.0	S.W.		10.57	319.32
+6960	10.5	316.7	310.8	5.9	N.W.		11.10	318.79
					N.E.		10.60	319.29
					S.E.		10.37	319.52
24349960	10.8	316.3 316.8	310.4	5.9		6.38	324.80	12.17
					Top Pipe		9.08	315.02
					Bottom		11.50	312.30

G.V. Box & Side outlet
2414747

14.52

9.05
9.00
9.00
9.19

K.M.P.L.#2
5' OFF

King
West
Shipman

4-21-50

cloudy-mist 49

322.17

T.B.M.	2:20	319.13	10.24	316.33		819.0000 - 24319960
244-2995			3.2	315.9	310.1	5.8
+5914			3.8	315.3	309.7	5.6
2 +8936			4.2	314.9	309.4	5.5
7 245+1928			4.5	314.6	309.1	5.5
+4911			5.0	314.1	308.7	5.4
2 +790			5.3	313.8	308.4	5.4
246+0894			5.5	313.6	308.0	5.6
+3815			5.7	313.4	307.4	6.0
+6876			6.2	312.9	306.8	6.1

K.M.P. #2
5' off

KING
Shipman
West

4-21-50

Cloudy
Mist

50

319.13

24649859	6.7	312.4	306.2	6.2
24711858	7.0	312.1	305.8	6.3
+4850	7.1	312.0	305.7	6.3
+7842	7.4	311.7	305.7	6.0
24848834	7.8	311.3	305.6	5.7
+3877	7.9	311.2	305.6	5.6
+4809	8.0	311.1	305.6	5.5
+78	8.2	310.2	305.1	5.1
24920790	9.1	310.0	304.2	5.8
+3700	9.4	309.7	303.4	6.3

K.M.P.L.#2
5:00FF

King
West T
Shipman

4-21-50

Cloudy
mist 31

319.13

249+67²⁰

9.8

309.3

302.5

6.8

497⁶⁰

11.7

307.4

301.7

5.7

T.P.

3.04

310.51

11.66

307.47

ORIGINALLY = 249+67⁶⁰

250+27⁵⁰

4.2

306.3

301.2

5.1

457⁴⁴

3.2

307.3

300.8

6.5

487

4.0

306.5

300.4

6.1

254+7⁹¹

3.7

306.8

300.2

6.6

447¹¹

3.3

307.2

300.2

7.0

475⁰³

3.3

307.2

300.2

7.0

252+66⁹⁴

4.3

306.2

300.2

6.0

K. W. P. L. #2
5'5FF

King
West T
Shipman

4-21-50

Cloudy
Mist

52

318.51

+186			4.9	305.6	300.1	5.5
+26 ⁷⁷			5.0	305.5	299.8	5.7
+36 ⁶⁷			6.5	304.0	298.6	5.4
+86 ⁵¹			7.7	302.8	297.4	5.4
253+16 ⁴⁷			8.4	302.1	296.3	5.8
+36 ³⁷			8.9	301.6	295.5	6.1
+46 ²⁰			9.1	301.4	295.3	6.1
TBD 11	4.50	305.87	9.14	301.37		
253 ⁶²⁹ 17			5.1	300.8	295.0	5.8
253+92 ⁸ 254+16 ⁴⁷			4.6	301.3	294.8	6.5

OR 91/10/11 253+46²⁰

Kim. P. 2 # 2
5' OFFSET

King West
Shipman

Cold - Rocks 55

305.87

254+17

4.7

301.2

294.7

6.5

+29

4.6

301.3

294.6

6.7

254+52⁵⁷

4.8

301.1

294.5

6.6

254+82⁵⁹

4.6

301.1

294.3

6.8

253+10⁵⁷

5.1

300.8

294.1

6.7

255+42⁴⁸

5.9

300.0

294.0

6.0

T.B.M

5.61

304.45

7.03

298.84

34-N. Nail in psv. 65' fire to 257+22⁷¹

255+72³⁷

4.7

299.8

293.8

6.0

+02²⁷

4.9

299.6

293.6

6.0

132.10

4.8

299.7

293.6

6.1

K.M.P.L.#2
5' offsets

King
West
Shipman X

5-4-50

Cold - cloudy 54

301.45

256 + 6202			4.9	299.6	293.5	6.1
+ 91.94			3.8	300.7	293.4	7.3
T.P.	5.15	303.99	5.1	298.4		
257 + 2186			5.1	298.9 ⁹	293.2	5.7
+ 51.78			4.7	299.3 298.3	293.1	6.2 5.2
+ 81.70			4.8	299.2 298.2	293.0	6.2 5.2
258 + 1162			5.2	298.8	292.8	6.0
258 + 4124			5.6	298.4	292.5	5.9
T.P.	3.75	302.59	5.15	298.84		
258 + 7146			4.4	298.0	292.2	5.8
259 + 01 ³⁸			4.5	298.1	292.0	6.1

K.M.P.L #2
5 offsets

King
Shipman
Wood

5-4-50

cold-cloudy

55

302.59

259437 ¹			4.9	297.7	291.7	6.0
16 ^B			5.5	297.1	291.4	5.7
1910 ⁵			5.6	297.0	291.2	5.8
set T.B.M	8.34	302.00	8.97	293.62		
260420 ⁹⁷			5.0	297.0	291.0	6.0
150 ⁸⁹			4.9	297.1	291.6	6.1
180 ⁸¹			5.1	296.9	290.9	6.0
261410 ²³			5.1	296.9	290.8	6.1
T.B.M			8.37	293.63		

gunney 24 290400 - 130'

R.M.P.L. #2
5' offsets - LT

5-4-50

52

T.B.M	9.67	286.75		277.08	(181) (sub - 50' 14 290.40)
284+82 ⁷⁶			1.9	284.9	279.0 5.9
285+12 ⁶⁸			2.4	284.4	279.0 5.4
+42 ⁵¹			2.7	284.1	278.9 5.2
+72 ⁴³			2.9	283.9	278.9 5.0
286+02 ³⁵			2.7	284.1	278.9 5.2
+32 ²⁷			2.4	284.4	278.9 5.5
+62 ¹⁹			2.0	284.8	278.9 5.9
286+92 ¹¹			1.7	285.1	278.9 6.2
287+22 ⁰³			1.9	284.9	278.9 6.0

K.M.P.L.#2
5' offset

King
Shipman
West

5-4-50

clear

59

286.75

287 + 5795

2.3 284.5 278.9 5.6

+ 74⁸⁰

2.5 284.3 278.9 5.4

288 + 0479

3.0 283.8 278.6 5.2

+ 3470

3.2 283.6 278.0 5.6

+ 6461

3.4 283.4 277.6 5.8

+ 9412

3.7 283.1 277.1 6.0

289 + 2429

5.4 281.4 275.4 6.0

289 + 8416

6.2 280.6 273.8 6.8

+ 8414

9.1 277.7 271.6 6.1

290 + 1380

12.6 274.2 269.0 5.2

K.M.P.L. #2
50 FFsets

King
Shipping
West

5P

7.92

286.75

T.P	1.34	275.46	12.63	274.12		
290 + 435 ⁵			4.7	270.8	265.8	5.0
473 ¹⁷			7.9	267.6	262.2	5.4
291402 ⁸⁷			10.9	264.6	258.5	6.1
291432 ⁵⁷			13.8	261.7	254.9	6.8
T.B.N1			P.5	266.96 267.02		290731 ⁷ R4.

K.M.P. 2J2
5' OFF

59

	7.21	300.84			293.63	
290	261440 ⁵		4.1	296.7	290.7	6.0
	+70 ⁵⁷		4.3	296.5	290.6	5.9
2	262400 ⁴⁹		4.2	296.6	290.5	6.1
2	+30 ⁷²		4.7	296.1	290.5	5.6
	+60 ²⁴		4.4	296.4	290.4	6.0
	+90 ⁶		4.2	296.6	290.4	6.2
	T.P. 263+20 ⁰⁸	5.1 301.84	4.1	296.7	290.4	6.3
	263+50		5.0	296.8	290.4	6.4
	+79 ⁹²		4.9	296.9	290.4	6.5

R.M.P. #2
5' OFF

King
Shipman
West

5-5-50

80

301.84

~~264 + 68^{PM}~~

~~44~~ 297.2 290.4

~~6.8~~

29

~~+3974~~

~~44~~ 297.2 290.4

~~6.8~~

~~+696^{PM}~~

~~45~~ 297.3 290.4

~~6.9~~

T.B.M

8.21 293.63

5.0 302.3

297.3

+68^{PM}

5.3 297.0 290.4

6.6

+3976

5.1 297.2 290.4

6.8

T.B.M

7.26 302.12

294.86

264 + 69^{PM}

5.0 297.1 290.4

6.7

+9960

5.0 297.1 290.4

6.7

265 + 299^{PM}

5.2 296.9 290.4

6.5

K.M.P.L.#2
5 offsets

King
Shipman
West

3-5-50

61

	3.60	30050		296.9		
2 765+598			4.2	296.3	290.3	6.0
765+89 ²⁷			4.2	296.3	290.2	6.1
266+19 ⁹			4.8	295.7	290.1	5.6
T.B.M.	5.48	300.34		294.8		Nail in N.E. corner Airport Oil 266 to 0.1 120 24.
266+49 ¹¹			4.8	295.5	290.0	5.5
+79 ⁰			4.8	295.5	289.9	5.6
267+08 ⁸⁵			4.6	295.7	289.7	6.0
+39 ⁰⁷			4.8	295.5	289.6	5.9
+28 ⁷⁸			4.9	295.4	289.3	6.1

K.M.P.L.#2
5' off

300.34

49864	5.3	295.0	288.9	6.1
268428 ⁵²	5.9	294.4	288.5	5.9
4843	6.5	293.8	288.2	5.6
4834	6.8	293.5	287.8	5.7
269418 ²⁵	7.0	293.3	287.5	5.8
4486	7.5	292.8	287.1	5.7
47804	7.7	292.6	286.9	5.7
270008	7.9	292.4	286.7	5.7
43792	8.2	292.1	286.5	5.6
46784	8.3	292.0	286.3	5.7

King
Supman
West

5-0-50

62

K. W. P. L. #2
5' off

KING
SHIPINGAN
WEST

5-5-65

63

300.74

270+97⁷⁶ 8.3 292.0 286.2 5.8

271+22⁵⁹ 8.3 292.0 286.0 6.0

+57⁵¹ 8.0 291.8 285.8 6.0

+57⁴³ 8.8 291.5 285.6 5.9

272+17³⁵ 8.8 291.5 285.5 6.0

+47²⁷ 8.9 291.4 285.4 6.0

T. P. 4.39 296.43 8.36 292.04

B. m. 9.44 286.99

5/8" Balsa S.E. Cov wind sock 68' Lt 274415

K.M.F.L #2
5' offsets

RANNEY
KING 5-6-50

64

cuts

208	294.07	286.99			
272+77 ¹³	2.7	291.9	285.3	6.1	
273+07 ⁴	2.7	291.4	285.2	6.2	
273+37 ⁰³	3.2	290.9	285.0	5.9	
273+66 ²⁴	3.1	291.0	284.7	6.3	
273+96 ²⁵	3.3	290.8	284.3	6.5	
274+26 ⁶⁸	3.4	290.7	283.9	6.8	
274+56 ³⁹	4.0	290.1	283.6	6.5	
274+86 ⁵⁰	4.5	289.6	283.2	6.4	
275+16 ⁴¹	4.9	289.2	282.8	6.4	
275+46 ³²	5.5	288.6	282.5	6.1	
275+76 ²⁴	5.6	288.5	282.4	6.1	
275+06 ¹⁶	5.4	288.7	282.3	6.4	
276+36 ⁰⁹	5.4	288.7	282.2	6.5	
276+66 ⁰⁰	5.4	288.7	282.1	6.6	
276+95 ⁹²	5.8	288.3	282.0	6.3	
277+25 ⁷⁵	5.7	288.4	281.9	6.5	
277+55 ⁶²	6.0	288.1	281.8	6.3	

5/8" bolt S.E. Cor. Windsock

K.M.P.L #2
5' OFF

Rainway T
King

5-6-50

65

294.07

Cuts

277+85 ⁵⁹	6.2	287.9	281.7	6.2
278+15 ⁵¹	6.6	287.5	281.4	6.1
278+45 ⁴³	7.2	286.9	281.2	5.7
278+75 ³⁵	7.6	286.5	280.9	5.6
279+05 ²⁷	7.6	286.5	280.6	5.9
279+35 ¹⁹	7.9	286.2	280.3	5.9
279+65 ¹¹	8.1	286.0	280.0	6.0
279+95 ⁰³	8.3	285.8	279.7	6.1
280+24 ⁹⁵	8.1	286.0	279.7	6.3
280+54 ²⁰	8.4	285.7	279.7	6.0
280+84 ²⁰	8.4	285.7	279.7	6.0
281+14 ¹²	8.4	285.7	279.7	6.0
281+44 ⁵⁴	8.4	285.7	279.7	6.0
281+74 ⁴⁶	8.3	285.8	279.6	6.2
TR 3.70	28943	8.34	285.73	on 5' offset sta 281+74 ⁴⁶
282+04 ²²	3.7	285.7	279.6	6.1
+29 ⁰⁰	3.9	285.5	279.5	6.0
+53 ⁷⁷	4.1	285.3	279.5	5.8
+78 ⁵⁰	4.5	285.1	279.4	5.7

K.M.P. 2#2
50FF

289.43

28370366

4.6

284.8

279.4

5.4

+2852

4.9

284.5

279.3

5.2

+2836

4.9

284.5

279.3

5.2

+2824

4.9

284.7

279.2

5.5

28470310

4.9

284.5

279.2

5.3

+2876

4.8

284.6

279.1

5.5

+2824

4.9

284.5

279.1

5.4

T. B. M.

3.63

5-8-50
King
Shannon
West
22
4.6
CONC. MON. under Fence 100' No. 204254

Depth O.1 Par.
No. + So. Edge
K.M.P.L.#2

King
Shipman
West

5-10-50

67

167449	8" O.1	
167450	8" "	
168400	6" So. Edge	
168400	6" No. "	
168410	5 1/2" No. "	
168410	8" So. "	
168420	6 1/2" " "	
168420	6" No. "	
168450	6" So. "	
168450	5 1/2" No. "	
169400	5 1/2" " "	
169408	6 1/2" So. "	
169400	5 1/2" No. "	
+50	5 1/2" " "	
+50	70" So. "	
170400	5 1/2" No. "	
170400	6 1/4" So. "	
170450	6" No. "	
170450	6 1/4" So. "	

Depth - 0.1 Pay.
No. 4 So. Edge Trench
Kimi Pt. # 2

KING 5-10-50
Shipman
West

68

171400	5 $\frac{1}{2}$ "	No. Edge
171400	6 $\frac{1}{4}$ "	So. "
1714 50 ⁴⁴	5 $\frac{1}{2}$ "	No. "
1714 50 ⁴⁴	6 $\frac{1}{2}$ "	So. "
171450	5 $\frac{1}{2}$ "	No. "
171450	70	So. "
171456	6 $\frac{1}{2}$ "	No. "
171456	5 $\frac{1}{2}$ "	So. "
172400	5 $\frac{1}{2}$ "	No. "
172400	7 $\frac{1}{2}$ "	So. "
172450	6.0"	No. "
172450	6 $\frac{3}{8}$ "	So. "
173400	6 $\frac{5}{8}$ "	No. "
173400	6 $\frac{1}{2}$ "	So. "
173450	5 $\frac{3}{4}$ "	No. "
173450	6 $\frac{3}{8}$ "	So. "
174400	5 $\frac{1}{2}$ "	No. "
174400	6"	So. "

Depth - 0.1 Pav.
No. 4 So. Edge Trench
K.M.P.L. # 2

King
West
Shipman

5-10-50

65

174+50	5 1/2"	No. Edge
174+50		
174+50	6 3/4"	So. "
175+00	6 1/2"	No. "
175+00	6 3/4"	So. "
175+50	6 0"	No. "
175+50	5 1/4"	So. "
176+00	6 0"	No. "
176+00	6"	So. "
176+50	6 3/4"	No. "
176+50	6 1/2"	So. "
177+00	6 1/4"	No. "
177+00	7 0"	So. "
177+50	6 3/4"	No. "
177+50	6 3/4"	So. "
178+00	7 1/8"	No. "
178+00	7 1/2"	So. "
178+50	6"	No. "
178+50	7"	So. "

Depth - 0.1 Pav.
No. 4 So. Edge Pav.
K.M.P.L.H2

	No
179400	5 $\frac{3}{4}$ " No. Edge
179400	6 $\frac{1}{4}$ " So "
179450	5 $\frac{1}{4}$ " No "
179450	6 $\frac{0}{4}$ " So "
180400	5 $\frac{1}{4}$ " No "
180400	5 $\frac{1}{4}$ " So "
180450	6 $\frac{0}{4}$ " No "
180450	5 $\frac{1}{2}$ " So "
181400	4 $\frac{1}{4}$ " No "
181400	7 $\frac{1}{2}$ " So "
181426	4 $\frac{1}{2}$ " No "
181426	4" So "
181450	4" No "
181450	6" So "
181466	7" No "
181466	5 $\frac{3}{4}$ " So "
181477	7" No "
181477	10" So "

King
Shogun
West

5-10-50

70

Depth 6.1 Pav.

71

181+80		11 ⁶ "	No. Edge
181+80		11"	So "
181+83		6"	No. "
181+83		9"	So "
182+00		5"	No. "
182+00		5"	So "
182+50		5 ⁴ "	No. "
182+50		5 ⁰ "	So "
183+00		4"	No. "
183+00		4 ¹ / ₂ "	So. "
183+47 ⁰	CONC. 6 ¹ / ₂ "	1" oil	No. "
183+47 ⁰	" 6 ¹ / ₂ "	1"	S "
184+00	" 6 ¹ / ₂ "	1"	No. "
184+00	" 6"	1"	So "
184+074 ⁰	End CONC.		
184+30		5 ¹ / ₂ "	No. "
		6"	So "

K.M.P.L. #2
5' offsets

King
West
Shipman

5-15-50

72

B.m	11.23	266.59		255.36	Spike in R.R. tie Fence Post 25' Lt Sta 299	
T.B.m	1.23	257.50	10.32	256.27	Top 2 nd Fence post 305 + 75 [±] Lt.	
306 + 49 ¹⁴			5.9	251.6	246.9	9.7
306 + 78 ⁷⁹			7.0	250.5	241.9	8.6
307 + 08 ⁹¹			7.7	249.8	241.9	7.9
307 + 34 ⁸³			8.5	249.0	241.9	7.1
T.P.	0.75	249.34	8.91	248.59		
307 + 62 ⁷⁵			0.6	248.7	241.9	6.8
307 + 94 ⁰²			1.3	248.0	241.9	6.1
308 + 05 ⁷⁵			1.9	247.4	241.9	5.5

249.34

308423⁵³

2.4

246.9

241.0

5.9

443³⁰

3.6

245.7

239.2

6.5

463⁰⁷

5.0

244.3

237.6

6.7

308402⁰⁴

(7.07)

241.87

7.5

241.8

236.1

5.7

ORIGINAL

T.P.

1.34

243.21

7.47

241.87

ORIGINAL 308402⁰⁴308402³³

4.4

238.8

234.5

4.3

317⁰

8.5

234.7

229.2

5.5

611³

13.2

230.0

224.0

6.0

T.P.

0.19

230.68

12.92

230.49

218.8

490⁵⁵

5.8

224.9

218.8

6.1

310+20¹⁰ 230.68 11.2 219.5 213.5 6.0

T.P 111 219.21 12.58 218.10

+49⁵⁶ 4.0 215.2 208.8 6.4

+79³⁸ 7.7 211.5 206.3 5.2

311+09²⁰ 9.9 209.3 203.9 5.4

+39⁰² 12.0 207.2 201.6 5.6

68²² 13.1 206.1 200.5 5.6

T.P 0.08 206.80 12.49 206.72

+98²² 1.7 205.1 199.4 5.7

312+28⁶³ 2.4 204.4 198.4 6.0

312+48⁴⁸ 206.80 3.7 203.1 197.7 5.4
~~5.7~~

+68³⁶ 4.8 202.0 196.5 5.5

+98¹³ 6.9 199.9 194.8 5.1

313

313+27⁹¹ 9.5 197.3 191.9 5.4

+47⁶⁵ 71.2 195.6 190.0 5.6

T.P 0.57 196.21 11.16 195.64

313+77³¹ 4.4 191.8 186.1 5.7

7.1²
+96⁹⁹ 7.1 189.1 183.5 5.6

K&E. LEVEL 7106346

Aug. 29, 1950

RAINEY
REATTY,
KING
LEONARD
WEST

26

KEARNEY Mesa Pipeline #2. ADDITIONAL X-SECTIONS.

R.M.				283.25	CONC. MON. DATE 203-40
204+50	17' LT.	0.6.	-4.8	280.4	
"	37' RT.	0.6	-16.9	268.3	
204+00	24' RT.	0.6	-14.6	270.6	
"	24' LT.	0.6.	-5.2	280.0	
203+50	10' LT.	0.6.	-5.2	280.0	
"	10' RT.	0.6.	-6.3	278.9	
202+50	16' RT.	0.6.	-8.9	276.3	
"	12' LT.	0.6.	-5.0	280.2	
202+00	22' LT.	0.6.	-5.6	279.6	
"	32' RT.	0.6.	-20.0	265.2	
201+50	27' RT.	0.6.	-14.3	270.9	
"	15' LT.	0.6.	-4.7	280.5	
200+00	5' LT.	0.6.	-6.4	279.8	
"	35' RT.	0.6.	-17.9	267.3	
199+50	37' RT.	0.6.	-14.4	270.8	
"	4' LT.	0.6.	-4.6	280.6	
199+00	20' RT.	0.6.	-1.5	283.7	
"	10' LT.	0.6.	+1.0	286.2	
CHECK R.M.			-1.96	283.26	

NOTE: O.G. = ORIGINAL GROUND SURFACE.

The image shows an open notebook with two pages. The left page is ruled with blue horizontal lines and features two vertical red margin lines, one on the left and one on the right, creating a central column and two side columns. The right page is ruled with blue horizontal lines and has a single vertical red margin line on the left side. The pages are cream-colored and appear to be blank, with some faint smudges and a small handwritten number '78' in the top right corner of the right page.

$$\begin{array}{r} 118.87 \\ 4.94 \\ \hline 113.93 \\ 2.15410 \end{array}$$

$$\begin{array}{r} \text{HYP} \\ 112.19 \\ 6.69 \\ \hline 118.87 \\ 1.55 \\ \hline 117.32 \end{array}$$

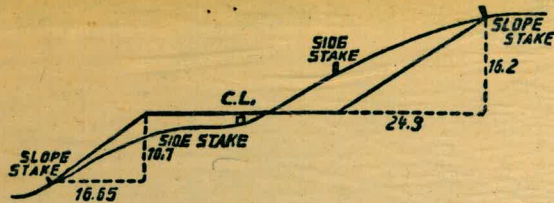
$$\begin{array}{r} 112.19 \\ 2.14 \\ \hline 114.33 \\ 9.17 \\ \hline 105.16 \end{array}$$

$$\begin{array}{r} 27224 \\ 222 \\ \hline 29408 \\ 493 \\ \hline 32455 \\ 493 \end{array}$$

1140

Handwritten calculations and notes on the left page of the notebook, including various numbers and mathematical operations:

- 338.21
- 908 / 272 = 118.8
- 349.3 / 23
- 3470
- 345
- 3424 / 206
- 342.4
- 245.4
- 6.9 / 2.3
- 4.6
- 3105
- 3007
- 349.9
- 56
- 355.5
- 833
- 3474
- 11400
- 8754
- 866
- 2.33
- 30 / 1.04
- 30 / 1.20
- 8.5
- 463.8
- 866
- 30.42
- 11
- 349.9
- 320
- 531.5
- 924
- 391
- 343.70
- 84
- 342.84
- 14
- 342.04
- 6.35
- 2.07
- 84
- 10500
- 9660
- 840
- 32722



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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