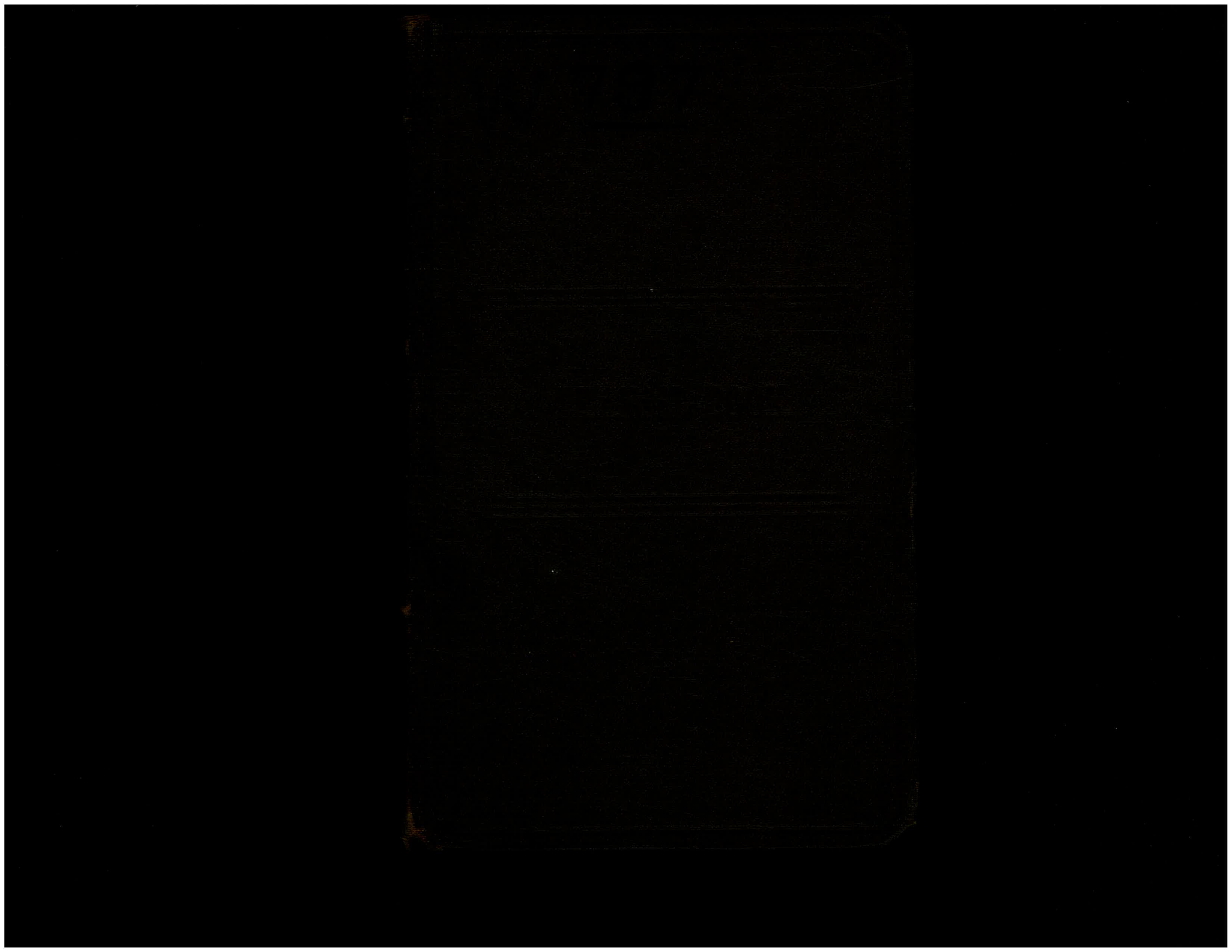
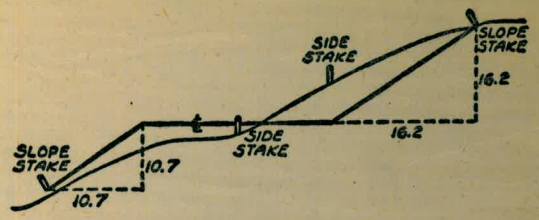




Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Gensler

275 175 to 275 (5) 20 → 11

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX alice

INDEX (Continued)

JULY 13 1950
BEATTY
LEONARD
BAKER

Proposed Distribution Main
& PROFILE - GESNER & BALTIMORE STS.

BM.	7.69	19.20 ✓		11.51	USGS TBM CONC. MON SW COR JELLET
TP	12.06	31.06 ✓	0.20	19.00 ✓	
TBM	8.66	37.64 ✓	2.08	28.98 ✓	L & T. CONC MON.
0+00			12.2	25.4	
0+01 75	ON A.C. PAV'T.		12.05	25.59	
0+23 35	ON A.C. PAV'T.		11.80	25.84	
0+43			11.2	26.4	
+50			10.0	27.6	
1+00			2.9	~~24.9~~ 34.7 EE	
TP ROCK	12.86	50.45 ✓	0.05	37.59 ✓	
+50			10.4	40.0	
2+00			7.2	43.2	
+50			3.4	47.0	
3+00			0.3	50.1	
TP ROCK	12.19	62.53 ✓	0.11	50.34 ✓	
3+42 28			10.6	51.9	
SET TBM			10.63	51.90	
4+00			6.9	55.6	

(City Datum) BH.

Edge Oil

9.6
6

3.7
7

11.5
10

7.5
11

2.1
10.5

10
9

ON L & T. CONC MON.

6.8
6

℄ Profile - Proposed Pipeline Gesner & Baltimore					Edge of pav't.
		62.53			
4+50			2.5	60.0	2.8 / 5
PI (Rock)	12.61	74.87 ✓	0.27	62.26 ✓	
5+00			10.8	64.1	11.5 / 2
+50			7.7	67.2	8.0 / 2
6+00			3.6	71.3	3.7 / 2
PI Rock	8.45	82.94 ✓	0.38	74.49 ✓	
+50			6.2	76.7	6.2 / 1.5
+82.16			2.9	80.0	1.6 / 21.
SET PI on Rock			1.90	81.04	
TBM	12.87	64.77 ✓		51.90	on Lft Conc Mon.
3+42.28			12.8	52.0	
+50 Edge of Paut.			12.9	51.9 EE	
+66 " " "			12.1	52.67 EE	
4+00 " " "			9.1	55.67 EE	
+50 " " "			5.6	59.17 EE	
5+00 " " "			2.6	62.17 EE	
PI Rock	12.95	77.22 ✓	0.50	64.27 ✓	

℄ Profile Prop. PIPELINE - GESNER & Baltimore

	77.22			
5+50		11.9	65.3	
6+00		8.7	68.5	
+09	End oil port 2.0 RT	8.2	69.0	
+30	End of Road.			
+50		4.8	72.4	
7+00		2.1	75.1	
+50		0.5	76.7	
8+00		2.5	74.7	
+20		1.5	75.7	
P Rock	13.18	90.31 ✓	0.09	77.13 ✓
+50			8.8	81.5
P	12.85	103.05 ✓	0.11	90.20 ✓
9+00			11.2	91.9
+50			1.0	102.05 EE 92.1
P (Top of Stk)	12.58	115.36 ✓	0.23	102.82 ✓
10+00			4.8	110.6
+30			0.0	115.4
P Rock	12.85	127.60 ✓	0.61	114.75 ✓
+50			7.7	119.9

Edge oil

12.1 / 1.0 × 11.1 / 1.5

9.1 / 1.0 × 8.2 / 2

8.6 / 2.0 × 7.6 / 2.0

Bottom of gully 45° ± RT)

Bottom of gully 45° ± RT)

℄ Profile Prop. Pipeline GESNER & Baltimore

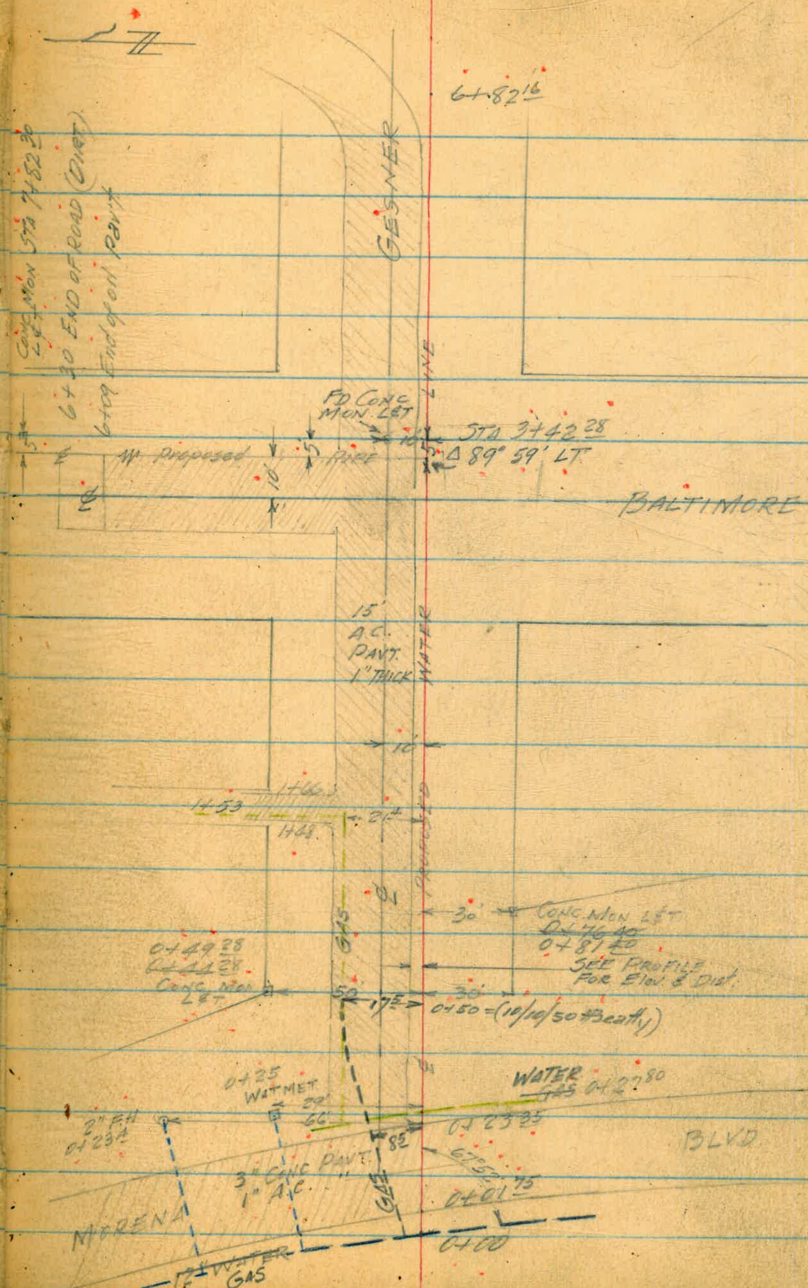
		127.60'		
11+00		0.2	127.4'	
P Rock	12.62'	140.20' ✓	0.02	127.58' ✓
+50			5.8	134.4'
11+72.28			3.9	136.3'
Set. TBM.			3.18	137.02'
				Left Conc Nion 5' Rt. 11+72.28
12+36.50			+2.5	142.7'
				Bottom 4" steel pipe laying on top of ground

JULY 13, 1950
BEATTY
LEONARD
BAKER

Mr. Huntington
sta of the Pacific
Beach pipeline
is 0+265
Bob Rainey

ST.S
11+72.28 Conc Mon LFT
Conc Mon Sta 7+82.20 LFT
6+30 End of Road (Dirt)
6+09 End of oil Pav't

0+00



13, 1950
BEATTY
LEONARD
BAKER

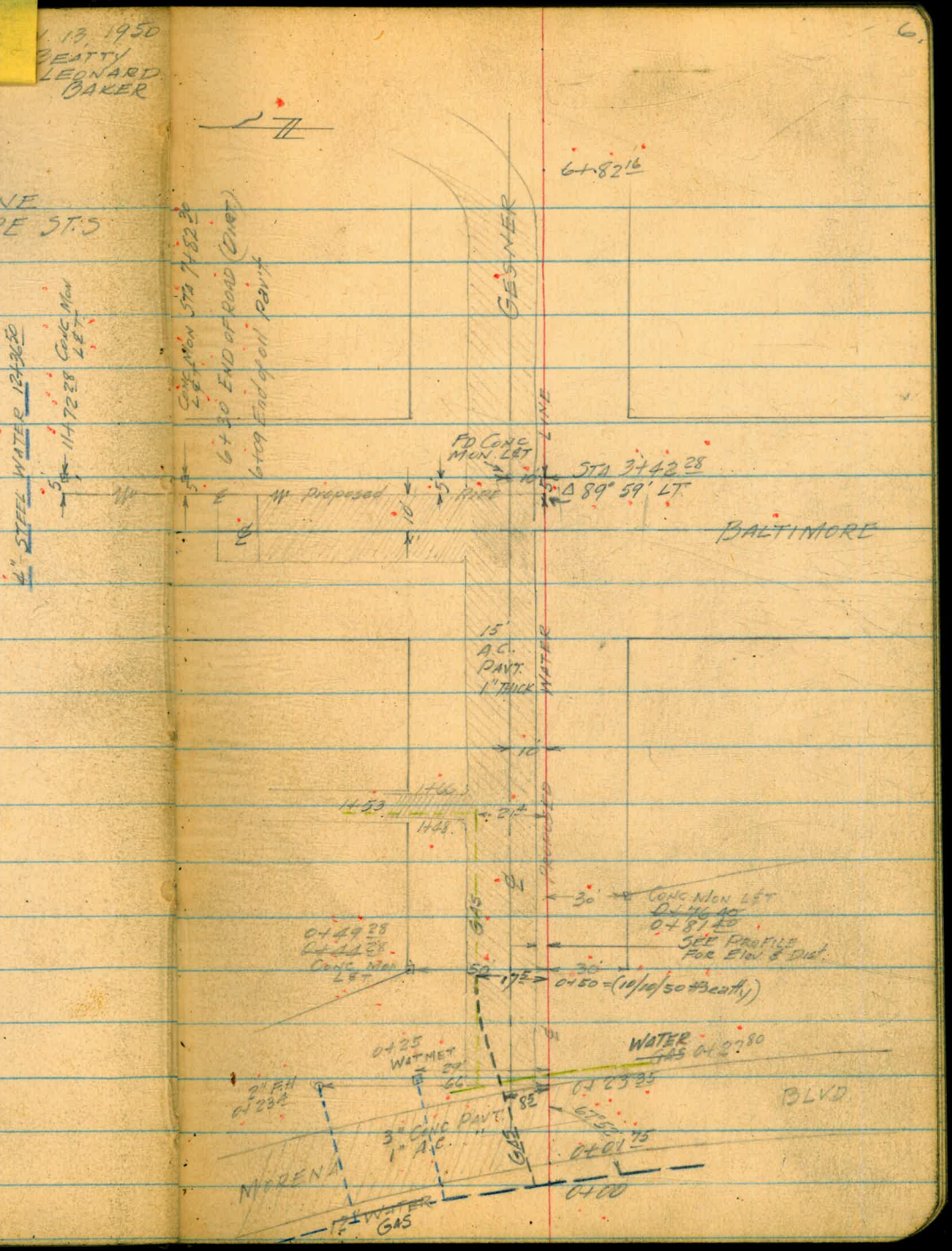
ALIGN'T FOR PROPOSED PIPELINE
GESNER & BALTIMORE ST.S

11+72.28 END of LINE NORTH.

6+82.16 END OF LINE EAST

3+42.28 TEE

0+00



SAN ELIJO ST.

(5) STAKES FOR 6" AC WATER

FEB. 21, 1952

BEATTY
POWELL
BERGER

BM	3.41	45.04 ✓		41.63 ✓		BR NE COR ROSECRANS & NICHOLS
HP	12.59	57.63 ✓	0.00	45.04		
TP	10.98	68.61 ✓	0.00	57.63 ✓		
SET TBM			5.56	63.05 ✓		
SET TBM	3.25	63.75 ✓	8.11	60.50 ✓		
		64.65				
0+30			6.8	57.3	53.7	C36
+50			6.8	57.3	53.7	C36
+55	6" TEE FH.					
1+00			6.8	57.3	53.9	C34
+50			6.4	57.7	54.2	1.5% C35
2+00			6.0	58.1	54.4	C37
+50			5.8	58.3	54.7	C36
3+00			5.6	58.5	54.9	C36
+50			5.2	58.9	55.2	C34
+61	6" TEE					0.6%
+70	6" GV					INV. 54.21 EL Top pipe - 54.9
						Rim 4.54 INV. 9.82
4+00			4.9	59.2	55.5	C37
+50			4.7	59.4	55.8	C36
5+00			5.5	58.6	56.1	C35 C30
+50			5.9	58.2	56.4	C48 C32
6+00			5.4	58.7	56.7	C27 C39

		~~63.75~~ 64.05					
6+50			4.2	59.9	57.0	C 3.0	
+95	6" TEE F.H.						
7+00			3.3	60.8	57.2	C 3.6	
TP	0.23	50.76	13.22	50.53			
TP	2.00	39.83	12.93	37.83			
CK BM.			6.32	33.51	=	NE BR. Kellogg St. ℄	
TP	13.14	~~63.39~~ 63.69		50.53		*BR. SW Cor. Kellogg St. & San Elijo	
CK BM			4.09	59.60 ~~59.30~~	= 59.58	0.30 Low	

6" RL
Sq N E/150

2-25-52
King
West
Williams

7+00 T.B.M.	7.66	68.46		60.8		
7+50			7.2	61.3	57.6	3.7
8+00			8.2	60.3	57.9	2.4
8+50			7.5	61.0	58.3	2.7
9+00			6.9	61.6	58.7	2.9
9+50			6.2	62.3	59.0	3.3
10+00			4.6	63.9	59.4	4.5
10+50			5.0	63.5	59.7	3.8
11+00			4.0	64.5	60.7	3.8
11+50			1.6	66.9	61.9 ~~62.1~~	4.8 ℄ 5 9
12+00			1.6	66.9	62.0 ~~63.5~~	3.4 ℄ 4 9
12+50			0.8	67.7	63.0 ~~63.9~~	2.7 ℄ 4 7
~~T.P.~~	10.45	78.09	0.82	67.64		
13+00			9.0	69.1	64.6 ~~66.4~~	2.7 ℄ 4 5
~~13+50~~			~~6.8~~	~~71.3~~	67.8	~~3.5~~
~~14+00~~			~~4.2~~			
			2.25	75.84	75.71	

Top F.H. Nichols 5/8

6" P.L.
San Elijo

Relocated to 14+77.55

T.BM	7.35	83.16			75.81
13+37.84 BC			12.4		
℄			12.2		
13+52.64			11.9		
℄			11.5		
+67.64			11.1		
℄			10.7		
EC. +86.68			9.9		
℄			9.5	73.7	
BC. 14+14.64			8.1		
℄			7.8	75.4	
14 +30			7.1		
℄			6.7		
+45			6.4		
℄			5.9	77.3	
+60			5.6		
℄			5.6	77.6	

2-26-52
Kins

6" P.L.
San Elijo

2-25-52
Kins

12

83.16

~~EC 14+50~~		~~5.0~~		
~~℄~~		~~5.0~~	~~78.2~~	
BC 14+77.45		5.0	78.2	72.2
℄		5.0	78.2	
+92.45		4.6	78.2	72.9
℄		4.4	78.8	
15+07.45		4.2	79.0	73.4
℄		4.1	79.0	
+22.45		3.9	79.3	74.0
℄		3.9	79.3	
EC 15+37.82		3.7	79.5	74.8
℄		3.7	79.5	
BC 15+49.82		3.6	79.6	75.5
℄		3.6	79.6	
+64		3.5	79.7	76.2
℄		3.6	79.6	
+79		3.3	79.9	76.8
		3.4	79.8	

6.0 O.K.

5.7

5.6

5.3

4.7

4.1

3.5

3.1

		83.16				
4 9+			3.1	80.1	77.6	2.5
℄			3.2	80.0		
16+09			2.4	80.8	78.2	2.6
℄			2.4	80.8		
T.P	12.52	93.28	2.40	80.76		
16+24			11.4	81.9	79.1	2.8
℄			11.5	81.8		
16+39			10.3	83.0	80.1	2.9
℄			10.1	83.2		
EC. 16+56 81			9.2	84.1	80.7	3.4
℄			9.3	84.0		
16+69 ℄			9.2	84.1	81.3	
16+77 ℄			2.3	91.0		
16+79 21 BC.			1.6	91.7	81.8	9.9 begin 10' OFFSETS
℄			1.5	91.8		
T.P.	11.09	102.76	1.61	91.67		
17+00			7.8	95.0	82.8	12.2
℄			7.1	95.7		

		.76 ~~102.67~~					
EC 17+26			3.5	99.3	84.7	15.2	
℄			3.1	99.7			
17+41 ℄			1.1	101.7			
17+45			1.7	101.1	85.0	16.1	
R			3.1	99.7			
T.P.	3.50	.61 ~~93.52~~	12.65	90.11 ~~90.02~~			
17+64 ℄			5.0	88.61 ~~89.52~~			on Pav. return
17+70 ℄			5.2	88.4			End - Top concrete on 8" P.L.
CK			5.4	88.2 ~~89.1~~	89.2		in gutter So. side
TBM			1.24				Top F.H. Owens & E150

6" P.I.

San E1.52

Relocation 13+16.3 to 17+26.10

2-26-52
KINS

T.B.M.	4.75	80.56			75.81	Top F.H. Nichols & San El. 52
BC 13+16.3			9.9	70.7	65.1 ~~66.8~~	5.6 ~~3.9~~
℄			10.4	70.2		
13+31			10.1	70.5	65.8 ~~67.4~~	4.7 ~~3.1~~
℄			5.8	70.8		
13+46			9.4	71.2	66.6 ~~67.8~~	4.6 ~~3.4~~
℄			9.1	71.5		
EC 13+60.96			8.3	72.3	67.8	~~3.9~~ 4.5
℄			5.8	72.8		
BC 13+93.37			6.6	74.0	69.4 ~~69.2~~	4.6 ~~4.8~~
℄			6.4	74.2		
14+08.37			5.7	74.9	70.4 ~~69.4~~	4.5 ~~5.5~~
℄			5.5	75.1		
14+23.37			4.6	76.0	71.0 ~~70.4~~	5.0 ~~5.6~~
℄			4.3	76.3		
14+38.37			3.9	76.7	71.4 ~~70.6~~	5.3 ~~4.1~~
℄			3.4	77.2		
EC 14+52.46			3.3	77.3	71.6 ~~71.0~~	5.7 ~~6.3~~
℄			3.1	77.5		
BK		4.75		75.81		

Relocation

Alignment – San Elijo

6" P.L.

E.C. 17+26.16

Δ 6°43 R
R-400
T-23.47
L 46.89

B.C. 16+79.21

E.C. 16+56.81

Δ 20°26'
R-300
T 54.07
L-106.99

B.C. 15+49.82

E.C. 15+37.84

Δ 11°32' R
R-300
T-30.34
L. 60.39

B.C. 14+77.45

E.C. 14+56.46

Δ 12°03' R
R-300
T-31.67
L 63.09

B.C. 13+93.37

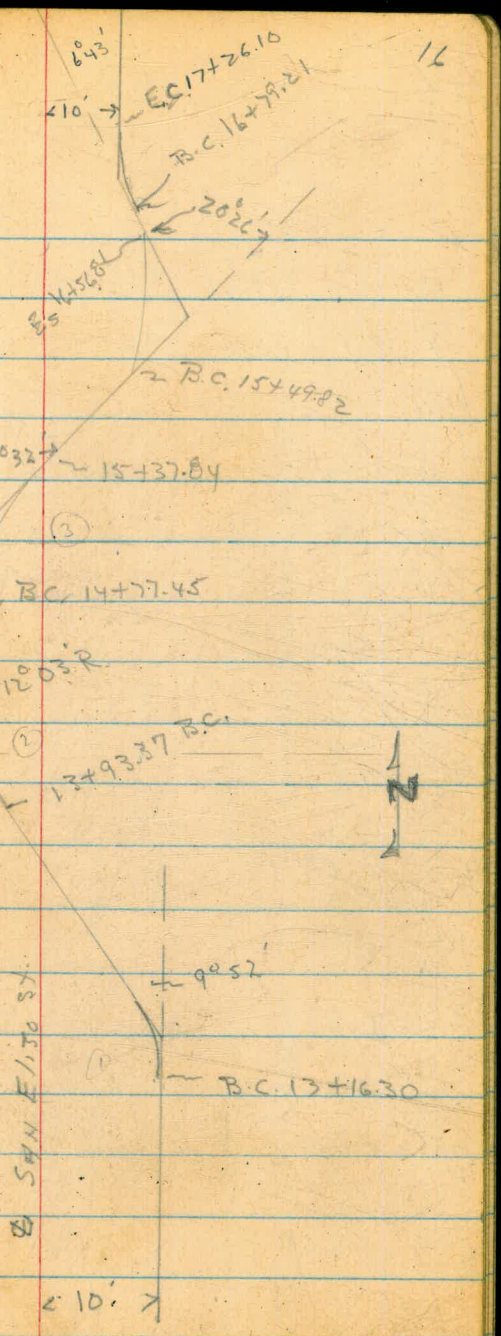
E.C. 13+67.96

Δ 9°52' Lt.
R-300
T 25.91
L-51.66

B.C. 13+16.30

2-26-52
King
West
Williams

1C



Meter Bovos
Alley # BK 183
Mission Beach

King
West
William

B.M.L.	2.57	09.60			7.03	
T.P.	1.77	08.65	2.72	06.88		
0+22 S.			3.0	05.7	5.4	C O 3
0+28 N.			3.3	05.4	4.8	C O 4
0+38 N			3.9	04.8	4.7	C O 1
0+68 S			5.8	02.9	2.5	C O 4
0+89 N			6.7	02.0	1.7	C O 3
1+36 N			8.6	00.1	-0.3	C O 4
1+44 S			8.9	-0.2	-0.7	C O 5
1+73 N			9.3	-0.6	-0.8	C O 2
2+10 N			9.9	-1.2	-1.3	C O 1
2+69 N			9.7	-1.0	-1.0	C O 0
2+83 S			9.8	-1.1	-0.8	F O 3
+ B.M.			9.16	-0.51		

9.7
8.65
51

West Edge 5 on Hi

Meter Boxes
Mission Beach
Alley - 97

King
West
Williams

TBm.	3.55	3.04		-0.51		
2+81S			4.6	-1.6	-1.6	C 0°
2+71N			4.7	-1.7	-1.7	C 0°
2+69S			4.3	-1.3	-1.8	C 0⁵
2+42N			4.7	-1.7	-1.9	C 0²
2+26N			5.0	-2.0	-2.1	C 0¹
2+09N			5.1	-2.1	-2.1	C 0°
2+02S			4.8	-1.8	-2.1	C 0³
1+73S			4.8	-1.8	-1.6	C 0²
1+27N			3.0	00	-0.4	C 0⁴
T.P.	9.66	+9.68	3.02	+00.02		
1+18S			8.8	+0.9	0.7	C 0²
0+92N			7.4	2.3	1.8	C 0⁵
0+74S			6.1	3.6	3.1	C 0⁵
0+42N			5.5	4.2	3.6	C 0⁶
0+59S			5.0	4.7	3.9	C 0⁷
0+44N			4.3	5.4	4.8	C 0⁶
TBM			3.46	6.22		

Meter Boxes
Tourmaline
Cass to Mission Blvd

3-4-52
Rain

Rain

19

13.3
1.4
11.9

B.M.	3.86	114.26			110.40	B.P.S.E. Tourmaline - Cass
2+68 N			- 4.4	109.9	107.8	C 2 1 00 = E. Prop. Bayard
1+72 S			- 8.5	105.7 ~~105.8~~	104.0	C 1 8
1+08 S			- 10.6	103.7	102.2	C 1 5
0+58			11.7	102.6	101.0	C 1.6
0+11			- 13.3	101.0	99.7	C 1 3
~~0+00~~						
T.P.	0.50	101.83	12.93	101.33		Top F.H. Tourmaline Bayard
0+27 S			- 2.8	99.0	98.4	C 0 6 00 = W.P.L. Bayard St.
0+73 S			- 4.0	97.8	97.3	C 0 6
1+20 S			- 4.9	96.9	96.0	C 0 9
1+71 S			- 5.7	96.1	95.0	C 1 1
2+21 S			- 6.6	95.2	94.3	C 0 9
2+70 S			- 7.3	94.5	93.7	C 0 8
3+19 S			- 7.7	94.1	92.8	C 1 3
3+71 S			- 8.2	93.6	91.9	C 1 7
4+22 S			- 8.9	92.9	91.0	C 1 9
4+72 S			- 9.8	92.0	90.4	C 1 6
5+19 S			- 10.6	91.2	89.6	~~C 0 6~~ C 1 9
5+70 S			- 11.5	90.3 ~~89.3~~	88.8	C 1 5
6+48 S			- 12.5	~~88.3~~	87.8	C 0 5 C 1 3

Meter Boxes
Tourmaline
Cass – Mission Blvds

161.83

5+25 N		9.1	92.7	90.5
4+72 N		8.4	93.4	91.3
4+33 N		8.1	93.7	91.8
3+85 N		7.3	94.5	92.6
3+30 N		7.0	94.8	93.4
2+83 N		6.4	95.4	94.0
2+18 N		5.4	96.4	95.0
1+65 N		4.7	97.1	95.7
1+32 N		4.6	97.2	96.4
0+65 N		3.2	98.63	98.0
0+42 N		2.5	99.33	99.30

3-4-52
KINL

RAIN

20

C 0 2
C 0 1
C 1 9
C 1 9
C 1 4
C 1 4
C 1 4
C 1 4
C 0 8
C 0 6
98.5 C 0 8

Meter Boxes
Alley - between Ventura Place & Island

3-4-52
King
West
Williams

RAIN

T.B.M. 3.68	09.90		11.04	06.22	
0+20 S		5.2	04.7	05.0	F 0.3
0+45 S		6.1	03.8	04.2	F 0.4
0+63 N		7.0	02.9	03.8	F 0.9
0+74 S		7.1	02.8	03.2	F 0.4
0+92 N		7.6	02.3	02.6	F 0.3
1+21 N		8.1	01.8	01.7	C 0.1
1+52 S		9.3	00.6	00.7	F 0.1
1+51 N		8.9	01.0	0.8	C 0.2
2+09 N		10.3	-0.4	-0.7	C 0.3
2+20 N		10.4	-0.5	-0.9	C 0.4
2+10 S		10.0	-0.1	-0.7	C 0.6
2+69 N		10.7	-0.8	-1.4	C 0.6
2+99 N		11.0	-1.1	-1.6	C 0.5
3+15 N		10.7	-0.8	-1.6	C 0.8
2+97 N		11.0	-1.1	-1.6	C 0.5
3+27 S		11.0	-1.1	-1.6	C 0.5
3+38 N		10.8	-0.9	-1.5	C 0.6
TBM		4.45	5.25	5.25	

3+54 S - C 0.2

97

Alley - Bayside - Mission Blvd
between Ventura Place
& Island
Grados Meter Boxes

3-7-52
King
West
Williams

22

170

T.B.M.	5.20	+3.65			-1.70
0+46 S			4.8	-1.1	-1.6
0+58 N			5.8	-2.1	-1.6
1+04 N			5.4	-1.7	-1.9
1+04 N			5.4	-1.7	-1.9
1+36 N			5.3	-1.6	-2.0
2+17 N			4.6	-0.9	-1.7
2+19 S			4.3	-0.6	-1.7
2+53 N			4.6	-0.9	-1.5
2+79 S			4.2	-0.5	-1.5
2+89 N			4.5	-0.8	-1.4
3+02 S			4.2	-0.5	-1.4
3+18 N			4.6	-0.9	-1.4
3+37 S			4.5	-0.8	-1.4
			5.40	-1.75	-1.77

C 0.5
F 0.5
C 0.2
C 0.2
C 0.4
C 0.6
C 0.9
C 0.6
C 1.0
C 0.6
C 0.9
C 0.5
C 0.6

Meter Boxes
On Opal from Bayard
to Cass

	+12.63	Hi 102.90	−	90.27	
	0.44	101.59	1.75	101.15	
2+65 N			0.8	100.8	99.8
2+20 N			1.3	100.3	99.0
1+14 N			2.9	98.7	97.0
0+59 N			3.9	97.7	95.9
0+33 N			4.8	96.8	95.5
0+13 S			6.1	95.5	94.5
0+70 S			4.5	97.1	95.6
1+23 S			4.1	97.5	96.5
2+13 S			2.5	99.1	98.2
			-0.60	100.99	101.35
	1.75	102.90	-0.44	101.15	Turn on
			12.63	90.27	90.27
	101.15 9.99	111.14	1.12	110.02	

King
West
Williams

98 SW

Sapphire to mission

23

BM BP SE Cor Loring & Cass

C 1 0
C 1 3
C 1 7
C 1 8
C 1 3
C 1 0
C 1 5
C 1 0
C 0 9

0 400 E Linv Bayard

Fire Hyd

rock

101.15 Turn on rock

100.99
1.9
99.09
97.9
1.21

+ 0.33
101 48
-10.44
91.04
+.21
91.25
-7.96
83.29 H.
+8.84
92.13

92.13
+.30
91.83
+9.33
101.16 Hi
2.65
98 51 L
98 54

Alley Block 99
Mission Beach

3-11-52
King
West
Williams

	4.96	3.19		-1.77	
3+63 N		4.5	-1.3	-2.0	CO 7
3+41 S		4.7	-1.5	-1.6	CO 1
3+10 N		4.2	-1.0	-1.4	CO 4
2+91 S		4.2	-1.0	-1.6	CO 6
2+65 N		4.4	-1.2	-1.5	CO 3
2+49 N		4.3	-1.1	-1.7	CO 6
2+24 S		4.7	-1.5	-2.0	CO 5
2+14 N		4.6	-1.4	-1.8	CO 4
1+84 N		4.4	-1.2	-1.8	CO 6
1+75 S		4.7	-1.5	-2.0	CO 5
1+64 N		4.5	-1.3	-1.8	CO 5
1+55 S		4.8	-1.6	-1.9	CO 3
1+25 S		4.6	-1.4	-1.9	CO 5
1+01 N		4.8	-1.6	-1.6	CO 0
0+98 S		4.7	-1.5	-1.8	CO 3
0+70 S		4.8	-1.6	-1.5	FO 1
0+41 N		4.7	-1.5	-1.3	FO 2
		4.38	-1.19	-1.23	

Alley between Isthmus & Jamaca
Mission Beach

King
West
Williams.

T.B.M.	5.48	4.23		-1.23	
0+26 N		4.9	-0.7	-0.6	Fo.1
0+28 N		4.8	-0.6	-0.6	Co.0
0+88 N		5.0	-0.8	-0.7	Fo.1
1+39 N		5.1	-0.9	-0.8	Fo.1
1+65 N		5.0	-0.8	-0.9	Co.1
1+80 N		4.8	-0.6	-0.9	Co.3
2+23 N		5.1	-0.9	-1.0	Co.1
2+40 N		4.9	-0.7	-1.0	Co.3
2+82 N		4.9	-0.7	-0.8	Fo.1
3+53 N		5.2	-1.0	-1.40	Co.4
3+34 S		5.1	-0.9	-0.8	Fo.1
2+93 S		4.9	-0.7	-0.8	Co.1
2+65 S		5.1	-0.9	-0.8	Fo.1
2+00 S		4.8	-0.6	-1.0	Co.4
1+34 S		4.9	-0.7	-0.8	Co.1
1+15		5.7	-1.0	-0.8	Fo.2
0+46		5.3	-1.1	-0.7	Fo.4
		6.03	-1.80	-1.79	

Alley 107
Santa Barbara
Mission Beach

3-11-52
King
West
William

28

T.B.m.	4.95	4.22			-0.73
0+885			5.0	-0.8	-0.5
1+515			5.0	-0.8	-1.0
1+735			5.1	-0.9	-1.1
2+00 N			5.0	-0.8	-1.3
2+11 S			4.8	-0.4	-1.3
2+175			4.9	-0.7	-1.3
2+18 N			4.8	-0.6 ~~-0.8~~	-1.3
2+39 N			4.9	-0.7	-1.3
2+775			5.2	-1.0	-1.2
2+955			5.2	-1.0	-1.0
			5.51	-1.29	-1.35

MAR. 24, 1932
BEATTY
POWELL
BERGER

51ST ST.
ORANGE TO EL CAJON
(5) STAKES & GRADES SET FOR 6" WATER MAIN

T.B.M.	0.99	335.81		334.82		Top EH SE Cor Orange & 51ST
0+35			5.0	330.8	326.0	C18
+50			5.6	330.2	325.5 ~~326.0~~	~~C58~~ C47
+80			7.3	328.5	323.8 ~~324.1~~	C47
1+00			9.4	326.4	321.5	C49
TP	0.40	323.58	12.63	323.18		
+50			2.3	321.3	314.2	C71
2+00			10.38	313.2	307.0	C62
+25			10.1	313.5	307.0	C65
+50			10.8	312.8	308.1	C47
3+00			10.1	313.5	310.3	C32
+50			8.7	314.9	312.6	C23
4+00			5.3	318.3	314.8	C35
+12			4.6	319.0	315.4	C36
TP	13.25	336.78	0.05	323.53		
+50			12.7	324.1	317.6	C65
5+00			10.1	326.7	320.4	C63
+50			10.1	326.7	323.6 ~~323.2~~	C31
6+00			6.0	330.8	328.6 ~~328.2~~	C22
+12			3.9	332.9	330.2 ~~329.4~~	C27
TP	12.95	349.68	0.05	336.73		

51 ST. ST. (Cont'd.)

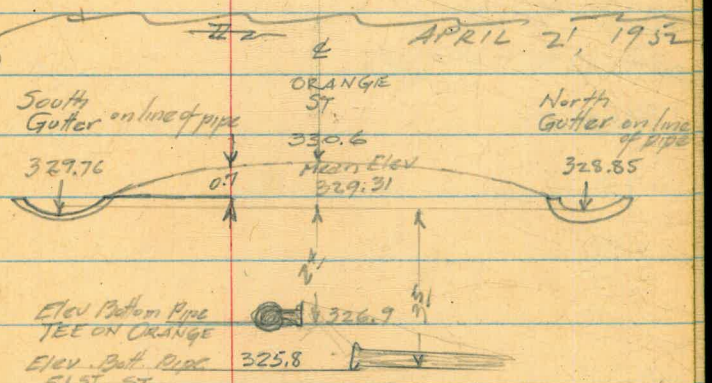
		349.68					
6+50			9.1	340.6	337.0	C36	
				345.3	341.4		
+72				346.6	342.8	C38 C37	F.H. FLANGE 345.8 (5) HUB F 2.8
PI	13.23	362.64	0.27	349.41			
+95			12.9	349.7	346.0	C37	
7+40			7.9	354.7	350.6	C41	
PT+80			2.6	360.0	357.4	C26 C30	
8+00	12.54	375.12	0.06	362.58	361.1	C24 C30	
8+20			11.6	363.5			
			4.4	370.7	368.6	C21 C30	
PT	12.62	387.64	0.10	375.02			
+80			10.3	377.3	374.6	C27 C30	
9+20			6.4	381.2	378.1	C31	
+60			3.5	384.1	380.8	C33	
10+00			2.1	385.5	382.4	C31	
+40			1.1	386.5	383.2	C33	
+50			0.9	386.7	383.3	C34	
PI							
11+00	5.86	393.34	0.16	387.48	383.5	C40	
+50			5.7	387.6	383.7	C39	
12+00			5.7	387.6	383.9	C37	
+50			5.6	387.7	384.1	C36	
+80			5.8	387.5	384.2	C33	
13+00			5.6	387.7	384.1	C36	

51
57
483 15.8

51ST ST. (Cont'd.)

		393.34			
13+50.			5.7	387.6 ✓	384.0
+60			5.9	387.4 ✓	384.0
14+00			6.8	386.5 ✓	382.3
+50			7.2	386.1 ✓	382.4
14+57.3 = F.H. TEE (IN PLACE)					
CK BM			6.63	386.71 ✓ = 386.82	
TP		6.73	325.03	318.3 @ 4+00	
2+05 W (2) WAT MET			10.72	314.3	313.5
2+07 E			10.03	315.0	314.6
2+71.5 W " " "			11.11	313.9	314.4
3+00 W. " " "			10.33	314.7	314.7
4+61 E			0.96	324.1	325.6
at TP @ 1+50			3.82	321.21 = 321.3	
TP		5.30	338.2	332.9	
6+15 W (2) WAT MET			1.0	337.2	337.5
5+09 W " " "			9.30	328.9	325.9
7+40 W (2) WAT MET				355.1	354.6
8+75 E (2) WAT MET				377.5	377.7
TBM		0.46	335.28	334.82	
Top 6" Flange on G.V			8.76	326.52	
Top 6" Bell on TEE Orange			7.64	327.64	
Conc. GUTTER South on ℄ Pipe			5.52	329.76	
" " North on ℄ Pipe			6.43	328.85	

C36
C34
C32
C37
C08
C04
F05
C00
F15
F03
C30
C05
F02



Dia = 0.87 Bottom of pipe 325.8
" " " " 326.9

REX ST.
54TH TO 52nd
(5) STK'S & GRADES SET FOR 6" WATER MAIN

BEATTY
POWELL
BERGER

MAR 27, 1952

BM	13.35	324.01		310.66			BP NW COR UNIV. & 54TH ST.
0+00 = {East Prop. Line 54TH ST							
0+50			7.4	316.6	309.1	C 7.5	
+60			4.2	319.8	309.1	C 10.7	
+75			2.0	322.0	309.1	C 12.9	
TP BOB	11.94	335.91	0.04	323.97			
+87			11.7	324.2	319.3	C 4.9	
1+00			9.0	326.9	322.2	C 4.7	
TP	11.86	347.46	0.31	335.60			
+50			10.5	337.0	332.8 ~~333.5~~	C 4.2	
2+00	10.20	357.43	0.23	347.23	339.0	C 8.2	
+50			5.9	351.5	343.2	C 8.3	
+75							
3+00			3.2	354.2	347.0 ~~347.3~~	C 7.2	
+50			3.0	354.4	348.7	C 5.7	
4+00			3.6	353.8	348.4	C 5.4	
+50			4.5	352.9	346.7	C 6.2	
5+00			6.0	351.4	345.1	C 6.3	
+50			7.3	350.1	342.55	C 7.5	
6+00			9.2	348.2	340.0	C 8.2	
TBM	0.00	347.18	10.25	347.18			Nail in Po. Pole SE Cor Shilo & Rex

NOTE:

ALL CUTS changed or less than shown due to check made on Elev see pg. 32
This applies also to Wightman St.

—Beatty

(5) F.H. Elev. Hub 353.5
Curb 349.8
3.7

Elev. & Ditch

349.4
ROD 8.0 ℄

347.0
ROD 10.4 ℄

REX ST. (Cont'd.)

			347.18				
6+35	F.H. TEE		0.7	346.5	338.9	C76	345.2 2.0 C
					338.7		
6+40	G.V.		1.4	345.8	338.6	C72	344.6 2.6 C
6+50			3.4	343.8	338.5	C53	343.3 3.9 C
7+00			5.8	341.4	336.5	C49	339.9 1.3 C
+50			7.3	339.9	334.6	C53	339.2 8.0 C
8+00			7.8	339.4	331.9	C75	337.9 7.3
+50			11.5	335.7	329.2	C65	334.9 12.3 C
PI		0.34	334.28	13.24	333.94		
9+00				3.0	331.3	326.4	C49
+50				7.0	327.3	323.3	C40
10+00				12.3	322.0	319.0 320.2	C48 C30
+25				14.0	320.3	316.9 318.0	C23 C34
+50				14.2	320.1	315.8 317.4	C27 C43
+75				11.7	322.6	318.0 316.5	C46
11+00				7.7	326.6	321.4	C52
+50				1.9	332.4	324.6	C78
12+00				1.4	332.9	327.1	C58
+50				1.2	333.1	328.6	C45
PI		5.44	338.47	1.25	333.03		

346.6
345.9
338.9
7.0

(10+41 18" RCP Cross Drain
EL TOP: 318.8
EL BOTT: 316.8)

321.9 12.4 C

325.9 8.4 C

332.0 2.3 C

		338.47			
12+75			5.4	333.1	328.9
12+90			5.4	333.1	329.3
TP		(Hi Cont'd to pg. 34)			
BM	12.20	328.27		315.57	
TP rock			0.04	328.23	
TP curb	2.78	330.92	0.13	328.14	
TP	2.19	320.02	13.09	317.83	
CK BM.			9.93	310.09	= 310.66
TP	11.64	339.87		328.23	
TP	8.23	347.45	0.65	339.22	
CK TBM			0.86	346.59	= 347.18

C42

C38

BP. NW Cor 52nd & Univ. (used for 9058-L)

(City Engr Elev.
BP NW Cor 54th & Univ

BEATTY
POWELL
BERGER

MAR. 27, 1952

WIGHTMAN ST.
54TH TO 52ND

(5) STK'S. & GRADES SET FOR 6" WATER MAIN

TBM		10.47	357.65 ✓		347.18
TBM				2.29	~~355.36~~ 354.77
6+50				3.4	354.3 347.3
6+40	6" GV.				347.4
6+35	F.H. TEE			2.9	354.8 347.5
6+25				2.9	354.8 347.6
6+00				2.6	355.1 348.2
5+50				2.3	355.4 349.6
5+00				1.9	355.8 350.3
4+50				1.5	356.2 350.65
4+00				1.3	356.4 351.0
3+50		2.19	358.54	1.30	356.35 ✓ 351.3
3+00				2.6	355.9 ✓ 351.6
2+50				3.0	355.5 351.9
2+25				2.7	355.8 351.3
2+00				3.6	354.9 350.4
1+75				4.8	353.7 348.4
1+50				8.2	350.1 ✓ ~~344.6~~ 345.0
PI		0.38	345.93	12.99	345.55
0+96				7.4	338.5 334.2

Nail in Po. Pole SE Cor Shilo & Rex
Nail in Po. Pole SE Cor Shilo & Wightman

C 7°

C 7 3

C 7 2

C 6 9

C 5 8

C 5 5

C 5 6

C 5 4

C 5 1

C 4 3

C 3 6

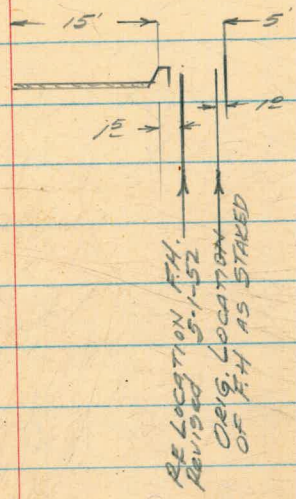
C 3 5

C 1 5

C 5 3

(V.C.) C 5 5

C 4 3



cut to here

WIGHTMAN ST. (Cont'd)

		345.93				
0+76	0.88	334.02	12.79	333.14	315.2	C 79
+60			4.6	329.4	315.2	C 142
+50			13.8	320.2	315.2	C 5 ℄
0+00 = ℄ 54TH ST.						
TP	1.38	322.40	13.00	321.02		
TP	2.42	314.44	10.38	312.02		
CK BM			3.77	310.67 = 310.66		BP NW Cor UNIV. ℄ 54TH

(Hi Cont'd from pg. 32)

		338.47				
12+88			2.7	335.8	329.9	C 59
TP	10.59	348.83	0.23	338.24		Top F.H SE Cor 52nd ℄ Wightman
12+50			7.2	341.6	333.4	C 92 — 340.9 / 7.9 C
12+00			3.4	345.4	338.0	C 66 — 344.8 / 4.0 C
11+50			0.6	348.2	341.2	C 70 — 347.0 / 1.8 C
TP	7.71	356.36	0.18	348.65		
11+00			6.4	350.0	342.6	C 74 — 349.4 / 7.0 C
10+50			6.9	349.5	342.7	C 68 — 349.9 / 6.5 C
10+00			6.0	350.4	342.9	C 75 — 349.8 / 6.6 C
9+50			6.0	350.4	343.0	C 71 — 347.6 / 8.8 C
9+00			8.0	348.4	343.2	C 52

WIGHTMAN ST.
(Cont'd.)

	356.36					
8+50	6.9	349.5	3442	C53	348.7 7.7 C	
8+00	4.8	351.6	345.1	C65	351.3 5.1 C	
7+50	4.0	352.4	345.9	C65		
7+00	3.0	353.4	346.7	C67		
6+40	1.8	354.6	347.6	C70		
CK TBM	1.0	355.36 ✓	= 355.36 50 354 77		Nail in pole SE Cor Shiloh & Wightman	

REX ST.

② STKS FOR WATER METERS
54TH TO 52nd

BEATTY
POWELL
BERGER

(Back of Met. Stk'd 17' From ℄ St.)

BM	11.37	357.96		346.59		NAIL IN POLE SE COR SHILO & REX
1						
1+85 So			12.88	345.1	341.2	c39
2+48				349.9	347.1	c28
~~2+14~~ Nor			~~11.00~~	~~347.0~~	~~343.8~~	~~c32~~
2+60 So			6.20	351.8	348.8	c30
2+67 Nor			6.7	351.3	348.7	c26
3+02 Nor			5.48	352.5	351.1	c14
3+39 So			3.50	354.5	352.7	c18
3+91 So			4.25	353.7	352.7	c10
4+22 So			4.85	353.1	352.1	c10
4+78 Nor			7.67	350.3	349.8	c05
5+18 So			7.49	350.5	348.4	c21
5+38 Nor			10.33	347.6	346.9	c07
6+28 So			11.16	346.8	343.4	c34
6+34/35 } Nor				342.7 / 342.3	342.1	c06 / c02
6+35 F.H.			10.04	347.92	343.1	c48 To Flange
6+40 E Prop line SHILO / 6+90 N Prop line						
① 7+04 So	0.23	346.82	11.37	346.59	341.6	
~~6+98~~ So			5.33	~~341.5~~ 340.9	~~341.9~~	~~F04~~ F07
7+09 Nor			8.75	338.1	340.7	F26

346.82
4.15
342.67

346.82
4.55
342.27

REX ST.

WATER METERS CONT'D

		346.82			
7+56 So			7.40	339.42	339.1
8+00 So.			7.74	339.1	336.8
8+67 NoR			13.42	333.4	332.9
H	1.31	334.79	13.34	333.48	
8+99 So.			3.76	331.0	331.1
9+09 NoR			3.49	331.3	330.3
9+26 NoR			5.98	328.8	328.1
10+13 So.			14.26	320.5	323.8
10+16 Nor			13.49	321.3	324.1
11+35 NoR			5.58	329.2	327.3
11+51 So			2.79	332.0	327.7
11+77 NoR			1.89	332.9	329.7
11+98 So			2.26	332.53	330.2
~~12+41 So~~					~~331.7~~
12+75 F.H.			2.30	332.29	332.9
H	5.55	338.19	2.15	332.64	
			0.50	337.69	Corr. Elev. = 337.64
TBM	3.15	357.92		35477	
6+35 F.H			3.48	354.44	351.80

C03 C23 C05 F04 C01 C07 F33 F08 C19 C43 C32 C25 F04 C31

13.49 77 14.26

12.87 68 51 13

338.24 59 337.65 Top of FH. SE 52 & Wightman

NAIL IN Pole SE Stilo & Wightman

C264 C614 6+35 SE Cor Wightman

April 17 1952
Beatty
Powell

E ST.

⑤ STK's & GRADES SET FOR 6" WATER

30TH ST. to 31ST ST

					℄ of PIPE 10' So ℄ ST.
BM	2.28	189.91 ✓	187.63		NW Cor BP 30TH ℄ E
13+40		5.9	184.0 ✓	181.1 ~~180.4~~	E Prop line 30TH Bottom Exist 6"C.I 181.13 Elev 8.78
+50		5.8	184.1 ✓	180.3	C38
14+00		5.4	184.5 ✓	180.7 ~~181.7~~	~~C28~~ C38
+50		4.9	185.0 ✓	181.2 ~~182.2~~	~~C28~~ C38
15+00		4.4	185.5 ✓	181.7 ~~182.7~~	~~C28~~ C38
+50		4.1	185.8 ✓	182.0 ~~183.2~~	~~C26~~ C38
16+00		4.1	185.8 ✓	182.0 ~~183.2~~	~~C26~~ C38
+50		4.7	185.2 ✓	181.4 ~~182.7~~	~~C25~~ C38
17+00		5.7	184.2 ✓	180.4 ~~181.6~~	C26 C38
PI +50	2.08	184.53 ✓	7.46 182.45 ✓	178.7 ~~179.6~~	~~C29~~ C38
18+00		3.4	181.1 ✓	176.5 ~~177.3~~	~~C38~~ C46
+50		4.55	180.0 ✓	175.6 ~~175.0~~	~~C50~~ C44
19+00		5.41	179.1 ✓	173.3 ~~176.1~~	C30 C38
+40 6" G.V.		6.04	178.5 ✓	174.7 ~~175.9~~	C46 C38 W. Prop line 31ST ST.
CK BM		5.59	178.97 = 178.99		BP SW Cor 31ST ℄ E

(Cont'd to pg. 45)

Pynchon St.

(2) Stks & Grades Set For Water Meters Logan To "T." St.

BM	1.85	120.62		118.77	BP NW Cor 47TH & Logan
0+00 = So Prop Line Logan					
0+30 W	5.72	117.04	9.30	111.32	110.0 C1 3
0+50 W			5.5	111.5	110.2 C1 3
1+07 W			4.7	112.3	110.3 C2 0
1+09.5 E			5.5	111.5	110.8 C0 7
1+38 E			6.0	111.0	110.7 C0 3
1+68 W (New House)			7.2	109.8	109.7 C0 1
1+99 E			8.0	109.0	109.4 F0 4
2+23 W			9.2	107.8	108.6 F0 8
2+47 E			9.4	107.6	108.7 F1 1
2+73 W			9.8	107.2	107.8 F0 6
3+23 W			9.6	107.4	107.5 F0 1
3+42 E			8.5	108.5	108.2 C0 3
3+74 W			8.2	108.8	108.2 C0 6
4+74 W			4.0	113.0	110.8 C2 2
4+83 E			3.4	114.6	111.7 C2 9 ✓
5+25 E			2.3	114.7	112.0 C2 7
5+27 W			1.6	115.4	111.6 C3 8
5+75 W			1.6	115.4	111.9 C3 5

109.72
7.32

PYNCHON ST
(CONT'D)

	117.04		
		2.4	114.6
SET TBM		2.00	115.04

Cont'd to pg 41

Cross MAIN on T. 112.2 FIN GRD
5S down to main. = 109.1
3 1/
Cor. Conc Driveway 100' S. SE Cor T ST & Pynchon

April 18, 1952
Beatty
King
Powell

ELEVS Top EXISTING 6" C.I WATER WEST ST. OCEAN VIEW TO LOGAN

B.M.	12.03	97.47	85.44	C.T. ℄ To West 45TH ℄ Ocean View
0+00 = So. Propline Ocean View				
0+10			7.01	90.46
0+47			7.15	90.32
1+00			7.72	89.75
1+70			8.35	89.12
2+22			8.70	88.77
2+53			9.32	88.15
3+28			9.55	87.92
3+81			9.63	87.84
4+31			9.91	87.56
4+81			10.81	86.66
℄	3.98	94.37	7.08	90.39
5+30			7.40	86.97
0+00 = So Propline T St.				
0+51			7.50	86.87
1+11			7.57	86.80
1+72			8.07	86.30

(Compare with 9375-L)

Elevs Top of Existing 6" C.I. Water
West St.
(Cont'd)

		92.37		
2+48			7.78	86.59
3+15			7.69	86.68
3+72			7.90	86.47
4+66			7.84	86.53
TP	13.35	105.28	2.44	91.93
TP	9.80	114.63	0.45	104.83
CK TP			3.21	111.42 = 111.32

APRIL 21, 1952

BEATTY
WEST
POWELL

WIGHTMAN ST.

(2) STKS & GRDS SET FOR WATER METERS
SHILO TO 52nd

(BACK of Meter 175 From ℄ St.)

			Elev.		
TBM	0.0	354.77	354.77	Curb Grd	NAIL IN POLE SE COR SHILO & WIGHTMAN
6+40 = E PROP. LINE SHILO					
6+87 (SOUTH 4 METERS		1.7	353.1	350.6	C25
7+14.5 Nor.		3.6	351.2	350.3	C09
7+18 So		2.1	352.7	350.7	C20
7+88 Nor		4.1	350.7	349.5	C13 ✓
8+66 Nor		9.0	345.8	348.7	F29
8+80 So		5.9	348.9	349.0	F01
9+19 Nor		9.5	345.3	348.1	F28
9+52 So		4.6	350.2	348.2	C20
10+16 So		5.1	349.7	347.6	C21
10+57.5 Nor		7.6	347.2	346.6	C06
10+78 So		5.2	349.6	346.9	C27
11+61 So.		6.9	347.9	344.8	C31
11+91 So		8.0	346.8	342.8	C40
11+14 Nor		8.9	345.9	345.9	C00

WIGHTMAN ST.
WAT. METERS
(Cont'd.)
SHICO to 54th

TBM 6.10	360.87		354.77		NAIL IN POLE SHICO & Wightman
6+40 - E Prop SHICO					
6+35.5 Nor. ✓		8.2	352.7	351.4	C13
6+04.5 So. ✓		6.4	354.5	352.5	C20
5+35 So ✓		6.0	354.9	354.1	C08
4+82 So ✓		5.4	355.5	354.8	C07
4+83 Nor. ✓		5.8	355.1	354.3	C08
4+17 Nor. ✓		5.6	355.3	354.7	C06
3+70 Nor ✓		5.0	355.9	354.8	C11
3+23 Nor ✓		5.2	355.7	354.9	C09
2+86 Nor ✓		5.3	355.6	355.0	C06
2+06 Nor. ✓		6.2	354.7	355.0	F03
CK (5) 2+00		6.5	354.4		
CK (5) 2+25		5.6	355.3		

April 22, 1952
Beatty
West
Powell

E St.

(5) Stk's & Grades Set For 6" Water

31st To 32nd

~~Cont'd from pg 38~~

BM	1.63	180.62		178.99		BP SW Cor 31st & E	
19+50			1.8	178.8	174.5 ~~175.3~~	C4.3	Top Curb
20+00			~~2.7~~	177.9	172.6 ~~175.6~~	~~C5.3~~ C5' (Replaced 4-25-52)	178.0 2.6 5
+10	F.H. Tee						
+25			5.5	175.1	171.0 ~~171.4~~	C4.1	175.2 3.4 5
+50			8.7	171.9	168.1 ~~168.6~~	C3.8	172.3 8.3 5
TP	1.60	169.02	13.20	167.42			
21+00			2.6	166.4	162.4 ~~162.9~~	C4.0	166.6 2.4 5
+25			4.6	164.4	158.7 ~~160.1~~	C5.7	163.7 5.3 5
+50			11.5	157.5	152.5	C5.0	
TP	0.44	156.17	13.29	155.73			
+75			7.2	149.0	144.0 ~~145.0~~	C5.0	
+87			11.3	144.9	140.2 ~~138.9~~	C4.7	
TP	0.13	143.10	13.20	142.97			
22+00			2.6	140.5	135.5	C5.0	
+25			11.2 ~~7.2~~	131.9 ~~135.9~~	128.5 ~~129.3~~	C3.4	
TP	0.15	130.51	12.74	130.36			
+50			7.3	123.2	119.9	C3.3	
TP	1.11	118.37	13.25	117.26			
+75			4.9	113.5	110.6	C2.9	
23+00			13.2	105.2	100.2	C5.0	
TP Hub +25	3.10	113.66	7.81	110.56	100.2	~~10.6~~ C10.4	8.16 / 6.15 / 14.31 FL Sew @ MH
Inv of MH			14.31	99.35			
Top 8" Sewer			11.90	101.76			

Elev. 175.00

Elev. 173.30

19+96 MTD Tele

178.99
178.99

Cont'd pg 47

BROADWAY
33rd to 34th

(4) STKS & GRADES SET FOR 6" WATER MAIN

NOTE:- ℄ of pipe staked 10' So & St. 4/29/52
Revised by Distribution Div. to 5' So ℄ of St.

BM	5.70	112.25		106.55	Conc Mon BP. NW Cor 33rd & Broadway
7+20			6.0	106.3	101.6 C47
7+00			6.2	106.1	101.8 C43
6+60			5.9	106.4	102.1 C43
6+00			6.0	106.3	101.3 C50
+50			7.8	104.5	100.6 C39
5+00			8.1	104.2	99.9 C43
+50			9.0	103.3	99.2 C41
4+00			10.4	101.9	98.5 C34
+60			11.0	101.3	98.2 C33
3+00	26'	103.26	11.60	100.65	96.6 C41
+50			31	100.2	95.4 C48
2+00			3.6	99.9	92.2 C57
+50			4.3	99.0	93.0 C60
1+00			5.3	98.0	92.2 89.4 C56 C58
+60			6.2	97.1	92.2 89.4 C57 C45
0+20					
			0.69	102.57	
CK BM.					

0+70 F.H. 22' So ℄ of St.
96.4 Elev. (5)
94.5
C 19 To Flange C54

92.2 Elev. Both. 8" on 34th

"E" ST

(5) STKS & GRADES SET FOR 6" WATER MAIN

Cont'd from pg. 45

TP	12.01	122.57		110.56	(5) Hub 23+25
23+37			8.9	113.7 ✓	110.3 / 112.3 — C14 C34
23+50			5.3	117.3 ✓	114.2 / 115.2 — C01 C31
TP	6.72	128.87	0.42	122.15 ✓	
24+00			3.2	125.7 ✓	122.6 — C31
24+25			0.6	128.3 ✓	123.3 — C50
24+50			0.6	128.3 ✓	122.4 — C59
25+00			5.3	123.6 ✓	116.8 — C68
TP					
25+50	0.08	116.55 ✓	12.40	116.47 ✓	111.2 — C53
25+90 FH. Tee			5.5	111.1 ✓	106.7 — C44
26+00			6.7	109.9 ✓	105.2 — C13
26+30			9.4	107.15 ✓	102.8 / 105.1 — C44
26+60			13.4	103.2 ✓	100.0 / 102.6 — C32
CK TP	13.31	120.37 ✓	9.49	107.06 ✓ =	7' offset Hub
TP	0.43	112.07 ✓	6.73	113.64 ✓	
CK BM.			7.49	106.58 ✓ = 106.55	NW Cor 33rd & Broadway.

(5) 110.48 / 6.07 — C05 To Flange, C40 To Bell Ell

Pynchon St

(2) STKS & GRDS FOR WAT. MET.S "T" ST. TO OCEAN VIEW

Cont'd from pg. 40

TBM.	2.45	117.69		115.04	Conc Driveway
0+00 = Nor Prop. Line T. St.					
0+18 ± W.		4.4	113.1	111.2	C 1 9
0+75 W		8.1	109.4	109.1	C O 3
0+86 E		8.4	109.1	109.3	F O 2
1+23 E		9.0	108.5	107.2	C 1 3
1+43 W		10.9	106.6	106.7	F O 1
1+84 W		11.7	105.8	105.3	C O 5
P	+3.02	107.39	13.12	104.37	
2+73 W			3.9	103.5	103.2	C O 3
2+86 E			3.4	104.0	103.6	C O 4
3+33 W			4.7	102.7	102.6	C O 1
4+07 E			4.6	102.8	102.6	C O 2
4+39 E			4.7	102.7	102.4	C O 3
4+77 W			5.3	102.1	101.6	C O 5
4+97 E			4.8	102.6	101.9	C O 7
5+22 E			4.7	102.7	101.8	C O 9
5+23 W			5.4	102.0	101.3	C O 7
5+63 W			6.0	101.4	101.0	C O 4
5+64 E			5.0	102.4	101.5	C O 9
℄ Pavt.			6.70	100.69	= 100.23	

(2)

Broadway 33rd to 34th
Wat. Meters.

Bk of Met = 29' from ℄ St.

BM	4.13	110.68		106.55	
0+66 Nor			11.6	99.1	95.0
1+34 Nor			11.6	99.1	96.7
2+50 So			10.4	100.3	99.1
2+90 So.			9.8	100.9	100.1
3+~~58~~ 48 So.			9.5	101.2	101.4
3+92 So			8.4	102.3	102.0
3+98 Nor			8.1	102.6	102.6
5+34 So			6.8	103.9	103.9
6+60 Nor			2.7	108.0	105.9
ck BM			4.13	106.55	

C39
C24
C12
C08
F02
C03
C00
C00
@21

REED AVE
CASS TO MISSION
(2) STK'S FOR WAT. METERS

BM		2.72	09.10	06.38	BP NE Cor - Thomas & Bayard
0+00 = E. Prop line Bayard					
2+13 Nor	Bayard Easterly	2.1	07.0	07.0	CO^{2}
2+91 Nor.		0.9	08.2	07.6	CO^{6}
3+38 Nor.		0.6	08.5	07.8	CO^{7}
3+68 Nor.		1.1	08.1	08.7	FO^{1}
4+61 Nor		0.4	087	08.7	CO^{2}
0+00 W. Prop line Bayard					
2+30 Nor.		8.70	00.4	0.80	FO^{4}
2+57 Nor.		9.0	00.1	0.70	FO^{6}
CK BM			2.72	06.38	

WRELTON DRIVE
TURQUOISE TO ELECTIC AVE
(4) STKS FOR 6" WATER

BM	0.98	104.27		103.29		BP NW Cor La Jolla Mesa Dr & Tourquroise
4+75	G.V.		6.8	97.5	93.4	C4!
4+43			7.2	97.1	93.2	C3⁹ → $C3^9$
4+35	F.H. TEE		7.3	97.0	92.8	$C4^2$ curb 97.47 / 6.80 (5) FH 97.7 / 6.6 $C0^2$ to Flange, $C3^2$ to Ell
4+00			8.0	96.3	92.0	$C4^3$
+50			9.3	95.0	90.8	$C4^2$
3+35	45° Bend		9.7	94.6	90.8	$C3^8$
2+85	45° Bend		10.7	93.6	90.4	$C3^2$
+50			11.7	92.6	89.1	$C3^5$
TP	3.29	95.48	12.08	92.19		
2+00			4.4	91.1	87.6	$C3^5$
+50			5.9	89.6	86.1	$C3^5$
1+00			7.4	88.1	84.5	$C3^6$
+50			8.9	86.6	83.0	$C3^6$
0+15			9.9	85.6	82.0	$C3^6$
TP	10.92	105.05	1.35	94.13		
ck BM			1.76	103.29		

KENDALL ST.

LA PLAYA TO PACIFIC BEACH DR.

(5) STKS & GRADES FOR 6" WATER

B.M.	2.55	36.23 ✓		33.68 ✓	
H.P.	5.23	28.50 ✓	12.96	23.27 ✓	
H.P.	5.79	30.72 ✓	3.57	24.93 ✓	GRADE
		Both 8"	9.92	20.80	
		Top 8"	9.25		
0+325			7.0	23.7 ✓	20.8
0+75			6.6	24.1 ✓	21.0 21.4
1+00			6.3	24.4 ✓	21.5
+50			6.0	24.7 ✓	21.6
2+00			5.6	25.1 ✓	21.7
+50			5.5	25.2 ✓	21.8
3+00			5.4	25.3 ✓	21.9
+50			5.2	25.5 ✓	22.0
4+00			5.0	25.7 ✓	22.1
+50			4.9	25.8 ✓	22.2
5+00			4.8	25.9 ✓	22.4
+50			4.7	26.0 ✓	22.5
6+00			4.4	26.3 ✓	22.6
+50			4.6	26.1 ✓	22.6
+70	F.H.	TEE	4.6	26.1 ✓	22.5
	(5) F.H. - 4" EE EST.		3.6		

NW Cor Ingram & Moorland (the only one available)

1' LEFT NE. Cor Kendall & La Playa.

C29
C30
C30
C31
C34
C34
C34
C35
C36
C36
C35
C35
C37
C35
C36

KENDALL ST
(Cont'd.)

℄ 6+97.5	7.46 G.V.	30.72	4.40	26.32	22.5	C38
		33.78				
7+50			7.6	26.2	22.4	C38
8+00			7.4	26.4	22.8	C36
+50			7.2	26.6	23.3	C33
9+00			6.9	26.9	23.8	C31 = 24.4 A.R.
+50			6.4	27.4	27.4 / 24.5	C30
10+00			5.7	28.1	25.1 / 25.2	C30
+50			5.1	28.7	25.7 / 25.9	C30
11+00			4.2	29.4	26.4 / 26.6	C30
+50			3.7	30.1	27.1 / 27.3	C30
12+00			3.1	30.7	27.7 / 28.0	C30
+50			2.4	31.4	28.4 / 28.6	C30
13+00			1.7	32.1	29.1 / 29.3	C30
+45	F.H. TEE		1.1	32.7	29.7 / 29.8	C30
	(5) F.H.		0.0	33.8	32.90	C09 T. flange 4± to bottom C.I.
13+72.5	13.25 (G.V.)	46.32	0.71	33.07	29.9	C32
℄	0.63	46.32 / 46.72	0.63	45.69		
℄ BM.			11.27	35.45 / 35.05 =	35.28 =	L℄T NE Cor LAMONT & Pac. Beach Dr

KENDALL ST.
Cont'd.

P.	13.20	46.27 ✓		33.07 ✓	
14+25			12.8	33.5 ✓	29.9 C36
+50			12.3	34.0 ✓	30.6 C34
15+00			11.1	35.2 ✓	31.9 C33
+50			9.9	36.4 ✓	33.3 C31
16+00			8.8	37.5 ✓	34.5 ~~34.7~~ C30
+25			8.3	38.0 ✓	35.0 ~~35.4~~ C30
+47½	GV.		7.5	38.8 ✓	35.4 C34
+95			7.1	39.2 ✓	35.4 C38
17+50			6.0	40.3 ✓	36.6 C37
18+00			5.0	41.3 ✓	37.8 C35
+50			2.8	42.5 ✓	39.0 C35
19+00			2.7	43.6 ✓	40.2 C34
+46	F.H. TEE		1.6	44.7 ✓	41.3 C34
"	(5) F.H.				
+50	END OF WORK		1.5	44.8 ✓	41.4 C34
		Top 6" C.I.	4.2		
			4.8	41.3 ✓	
CKP			0.59	45.68 =	

.024
6
.144

May 5 1952
Beatty
West
Powell

KENDALL ST.

(2) STKS & GRDS. FOR WATER MET. S.
LA PLAYA TO ROOSEVELT.

BACK SIDE OF MET. { 23' RT. East.
225 LT. West.

P	6.22	31.24	25.02		LFT NE Cor La Playa & Kendall.
0+00 = Nor. PL LA PLAYA					
0+68 E		6.0	25.2	25.2	CO$^{0}_{0}$
0+84 W		6.1	25.1	✓ 25.9	FO$^{8}_{8}$
1+06 W		6.3	24.9	✓ 26.0	FI$^{1}_{1}$
1+41 E		5.7	25.5	25.4	CO$^{1}_{1}$
1+64 W		5.5	25.7	26.2	FO$^{5}_{5}$ ✓
1+99 E		5.2	26.0	25.8	CO$^{2}_{2}$
2+31 W		5.0	26.2	26.5	FO$^{3}_{3}$ ✓
3+28 E		4.6	26.6	26.4	CO$^{2}_{2}$
3+84 E		4.5	26.7	26.7	CO$^{0}_{0}$
4+21 W		4.9	26.3	27.3	FI$^{0}_{0}$
4+39 E		4.3	26.9	26.9	CO$^{0}_{0}$
4+57 W		4.4	26.8	27.5	FO$^{7}_{7}$
4+86 E		4.5	26.7	27.1	FO$^{4}_{4}$
4+90 W		4.4	26.8	27.6	FO$^{8}_{8}$
5+18 E		4.6	26.6	27.1	FO$^{5}_{5}$
5+37 W		4.4	26.8	27.5	FO$^{7}_{7}$
5+79 E		4.2	27.0	26.7	FO$^{3}_{3}$
(5) FH.		4.01	27.23	26.60	CO$^{63}_{63}$ to flange CO$^{4}_{4}$ to bottom

25.02 BM
4.69

29.71 29.71 N.
27 3.66
26.2 26.15

4.57
25.14

27
25.4
43

KENDALL ST.

(2) STKS & GRDS FOR WAT. METS
ROOSEVELT to FORTUNA.

BACK SIDE of MET. 22.5 RT & LT
31.24

0+00 = Nor prop line Roosevelt					
0+16 W			4.2	27.0	27.1 FO 1
0+19 E			4.4	26.8	26.6 CO 2
0+69 E			4.2	27.0	27.1 FO 1
0+83 W			4.1	27.1	27.5 FO 4
1+19 E			3.6	27.6	27.5 CO 1
1+39 E			3.5	27.7	27.7 CO 0
1+60 E			3.6	27.6	27.9 FO 3
1+68 W.			3.5	27.7	28.0 FO 3
2+35 E			2.8	28.4	28.8 FO 4
2+93 E			2.1	29.1	29.5 FO 4
3+40 E			0.9	30.3	30.0 CO 3
(1) 3+65	8.17	38.71	0.70	30.54	
3+90 E			7.4	31.3	30.6 CO 7
4+08 E W			8.2	30.5	31.0, 30.8 FO 5
4+41 E			7.1	31.6	31.7 CO 4
4+65 W			7.5	31.2	31.8 FO 6
4+91 E			6.4	32.3	31.7 CO 6
5+17 E			6.2	32.5	32.1 CO 4

KENDALL ST.

(2) STKS & GRDS for Wat MET.

Roosevelt to Fortuna

		38.71			
5+25 W			6.4	32.3	32.6	F_0^3
5+76 E			5.0	33.7	32.8	C_0^9
		Fortuna to CHICO			
0+00 = Nor. P.C. Fortuna					
0+19 E			4.4	34.3	34.0	C_0^3
0+20 W			4.6	34.1	34.4	F_0^3
0+48 W			3.6	35.1	35.1	C_0^0
0+79 E			3.0	35.7	35.7	C_0^0
0+83 W			3.6	35.1	36.0	F_0^9
1+23 W			2.4	36.3	37.0	F_0^7
1+44 E			1.4	37.3	37.3	C_0^0
1+72 W			0.2	38.3	38.2	C_0^1
1+87 E			0.0	38.7	37.6	C_1^1
	8.20	47.07	0.04	38.67		
		CHICO To Pac. Beach Dr			
0+00 = Nor P.C.		CHICO			
0+41 E			6.1	41.0	39.9	C_1^1
0+66 W			6.0	41.1	40.8	C_0^3
0+80 E			5.8	41.3	40.8	C_0^5
1+23 W			4.8	42.3	42.2	C_0^1
1+41 E			4.7	42.4	42.3	C_0^1
1+85 W			3.1	44.0	43.6	C_0^4
1+94 E			3.2	43.9	43.9	C_0^0
ck BM.			1.65	45.42 = 45.59		L & T SW Cor Pac. Beach Dr & Kendall

May 16, 1952
BEATTY
WEST
Dowell
Kemp

ALLEY - BLOCK 20

POLK TO UNIVERSITY
Between 47th & EUCLID
④ STK'S & GRDS FOR 6" A.C. WATER
& PIPE = 5' EAST & Alley

BM	5.08	345.76		340.68	BP NW. Cor UNIV & EUCLID
6+00 = Nor Prop. line UNIV			4.8	341.0	337.0 C4.0
+50			1.5	344.3	340.8 C4.3
TP	5.21	350.07	0.90	344.86	
5+00			3.6	346.5	342.1 C4.4
+50			3.2	346.9	342.5 C4.4
4+00			3.1	347.0	342.5 C4.5
+50			4.0	346.1	341.8 C4.3
3+00			5.3	344.8	340.6 C4.2
+50			8.6	341.5	338.0 C3.5
2+00			13.0	337.1	332.1 ~~335.7~~ C3.2
+50			12.0	338.1	334.7 ~~335.7~~ C3.0
1+00			9.6	340.5	336.2 C4.3
+55			8.0	342.1	338.0 C4.1
0+00 = South Prop. line Polk			7.3	342.8	338.6 C4.2
TP	2.92	345.55	7.44	342.63	
OK BM.			4.86	340.69 = 340.68	

ALLEY – BLK 6
LANDIS TO WIGHTMAN
BETWEEN MENLO & 47TH
(4) STKS & GRDS FOR 6" WATER & PIPE = 5' East & Alley

BM.	9.50	352.26		342.76	T'LT NW COR MENLO & WIGHTMAN
6+49 = So Prop line Wightman		5.8	346.5	342.0	C42
6+00		4.4	347.9	342.0 ~~342.5~~	C59
+50		4.95	347.3	341.5 ~~341.9~~	C58
5+00		6.4	345.9	340.6 ~~341.0~~	C53
+50		7.5	344.8	339.6 ~~340.2~~	C52
4+00		8.0	344.3	339.0 ~~339.4~~	C53
+45		8.0	344.3	338.6 ~~339.0~~	C57
3+00		8.8	343.5	338.1 ~~338.5~~	C54
+50		9.2	342.9	337.7 ~~338.1~~	C48
2+00		10.3	342.0	337.3 ~~337.7~~	C53
+50		10.3	342.0	336.8 ~~337.0~~	C52
1+00		11.3	341.0	335.2	C58
+64		13.3	339.0	333.9	C51

REED AVE

(2) STKS & GRDS FOR WAT. METS

INGRAM – JEWELL

BACK of METER 27' from ℄ ST.

BM.	~~7.84~~ ~~11.79~~	~~51.99~~ ~~56.94~~		44.15	℄ LET REED & INGRAM
3+58 Nor			10.6	41.4	41.3	CO 1
3+47 Nor			10.7	41.3	41.3	CO 0
3+17 Nor			9.9	42.1	41.8	CO 3
2+84 Nor			8.9	43.1	42.9	CO 2
2+44 Nor			6.9	45.1	45.0	CO 1
2+13 So			1.7	50.3	47.6	C2 7
1+86 Nor			2.2	49.8	49.1	CO 7
TP	8.43	60.33	0.09	51.90		
1+77 So.			7.7	52.6	50.1	C2 5
1+69 So			7.2	53.1	50.6	C2 5
1+43 Nor			6.9	53.4	52.1	C1 3
0+92 Nor			4.4	55.9	55.6	CO 3
0+27 So			2.75	57.6	57.8	FO 2
0+03 Nor			2.0	58.3	57.9	CO 4
0+00 = W. Prop line JEWEL						
TP	2.04	51.59	10.78	49.55		
CK BM			7.44	44.15 = 44.15		

Beatty
West
Powell
Kemp
Varonfakis

Shasta St.

La Playa To Pacific Beach Drive

(5) Stks. & Grades For 6" Water

BM.	8.56	33.58 ✓	25.02		7' L.&T. NE Cor. Kendall & La Playa
0+325			5.7	27.9 ✓	24.9 C30
0+50			5.6	28.0 ✓	24.9 C31
0+75			5.5	28.1 ✓	24.9 C32
1+00			5.7	27.9 ✓	24.8 C31
+50			5.8	27.8 ✓	24.5 C33
2+00			5.7	27.9 ✓	24.3 C36
+50			6.3	27.3 ✓	24.0 C33
3+00			6.4	27.2 ✓	23.8 C34
+50			6.4	27.2 ✓	23.5 C37
PI 4+00	5.28	32.13 ✓	6.73	26.85 ✓	23.3 C36
+50			5.3	26.8 ✓	23.1 C37
5+00			4.9	27.2 ✓	22.9 C43
+50			5.0	27.1 ✓	22.6 C45
6+00			5.2	26.9 ✓	22.4 C45
+50					22.3
+61			5.4	26.7 ✓	22.3 C44
~~+55~~		F.H. Tee			
+61		(5) for F.H. = 24' from ℄ Street	4.7	27.4 ✓	Curb – 27.1 C03 to flange
6+75			5.5	26.6 ✓	22.2 C44

SHASTA ST. (Cont'd)

		32.13				
6+97 ~~6+92.5~~	G. VAL	5.6	26.5 ✓	22.7	C3 8	
7+01.5 ~~7+02.5~~	6"x6" Cross	5.3	26.8 ✓	23.0	C3 8	02.6 02.6 47.5 1.9 8.5 2.6 23.4 13.0 28.5 2.6 20.8 9.5 4.4 21.1 13.5
7+50		5.0	27.1 ✓	~~23.8~~ 24.2	C2 9 C3 3	
8+00		3.8	28.3 ✓	~~25.0~~ 25.3	C3 0 C3 3	
+50		2.64	29.5 ✓	~~26.2~~ 26.4	C3 1 C3 3	
9+00		1.54	30.6 ✓	~~27.2~~ 27.5	C3 1 C3 3	
PI +50	10.65 42.35 ✓	0.43	31.70 ✓	~~28.4~~ 28.6	C3 1 C3 3	
10+00		9.53	32.8 ✓	~~29.5~~ 29.7	C3 1 C3 3	
+50		8.35	34.0 ✓	~~30.7~~ 30.8	C3 2 C3 3	
11+00		7.25	35.1 ✓	31.8	C3 3	
+50		6.15	36.2 ✓	32.9	C3 3	
12+00		5.0	37.4 ✓	33.9	C3 5	
+50		3.83	38.5 ✓	35.0	C3 5	
13+00		2.65	39.7 ✓	36.0	C3 7	Elev Curb 40.6 @ Hob 41.0 CO 2
~~+35~~ +50	F.H. TEE	2.05	40.3 ✓	36.6	C3 7	F.H. 24' from ℄ St. 2' back Sidewlk
+50		1.55	40.8 ✓	37.0	C3 8	
13+~~75~~ +73	G. VAL	1.2	41.0 ✓	37.0	C4 0	
13+77.5	6"x6" Cross	1.1	41.0 ✓	37.0	C4 0	
14+00		1.05	41.3 ✓	37.0	C4 0	

Shasta St (Cont'd)

			42.35			
PI	14+25	10.67	52.93	0.09	42.26	37.0	C53
	+50			10.4	42.5	37.7	C48
	15+00			9.0	43.9	39.1	C48
	+50			7.9	45.0	40.6	C44
	16+00			6.7	46.2	42.0	C42
	+25			6.1	46.8	42.8	C40
	~~+42~~ +45	G.V.&L.		5.5	47.4	43.0	C44
	+50	6"x6" Tee		5.3	47.6	43.2	C44
	17+00			4.7	48.2	43.8	C44
	+50			4.1	48.8	44.3	C45
	18+00			3.6	49.3	44.8	C45
	+50			3.1	49.8	45.3	C45
	19+00			2.6	50.3	45.8	C45
	~~+30~~ +43	F.H. Tee		2.1	50.8	46.1	C47
	+50			1.9	51.0	46.2	C48
	20+00			1.4	51.5	46.2	C53
	+05	End of Work		0.9	52.0	46.2	C58
PI	~~CK BM.~~		2.46	54.49	0.90	52.03	
	CK BM.				9.01	45.48	=45.59

Conc pavt begins 19+47

(5) FH 2' back curb

May 20, 1952
Beatty
West
Powell
Kemp
Varonfaris

Alley - Block 20.

Polk to University
47th & Euclid

(2) Stks & Grds for Water Meters

BM	4.95	345.63		340.68		7' Lt NW Cor Euclid & Univ.
5+86 E			4.1	341.53	341.5	C0.0
5+69 W			3.2	342.4	342.5	F0.1
5+34 E			0.4	345.2	345.0	C0.2
TP	5.16	350.53	0.26	345.37		
4+66 W			3.5	347.0	346.5	C0.5
4+28 E			3.2	347.3	346.7	C0.6
4+15 W			3.5	347.0	346.7	C0.3
3+78.5 W			3.7	346.8	346.5	C0.3
3+28 E			5.1	345.4	345.5	~~C0.1~~ F0.1
3+27 W			4.7	345.8	345.5	C0.3
3+21 W			4.8	345.7	345.4	C0.3
2+63.5 E			8.3	342.2	343.4	F1.2
2+55 W			6.9	343.6	343.3	C0.3
2+21.5 W			9.5	341.0	341.9	~~C0.9~~ F0.9
1+83 E			13.3	337.2	340.8	F3.6
1+82 W			12.2	338.3	340.6	F2.3
1+58 W			12.1	338.4	340.2	F1.8
1+21 W			9.5	341.0	340.3	C0.7
0+84.5 E			8.4	342.1	341.0	C1.1
0+75 E			8.8	341.7	341.5	C0.2
0+69 W			9.0	341.5	341.7	F0.2
0+16 W			8.0	342.5	342.7	F0.2
0+05 E			7.2	343.3	342.8	C0.5
0+00 = So. Prop Line Polk						
TP	1.38	345.54	6.34	344.16		
CK BM			4.87	340.67 = 340.68		

May 22 1952
Beatty
Powell
Voronfakis

ALLEY - BLOCK 6.
LANDIS to WIGHTMAN
BETWEEN 47TH & MENLO
(2) STKS & GRDS FOR WAT. METERS.

BM.	9.16	351.92		342.76	7' Lt. NW Cor WIGHTMAN & MENLO
0+00 = So Prop line WIGHTMAN					
0+25 E.			4.3	347.6	346.3 C/3
0+41 W.			4.4	347.5	346.2 C/3
0+87 E.			4.2	347.7	346.1 C/6
0+91 W.			5.2	346.7	345.7 C/0
1+18 W.			5.7	346.2	345.1 C/1
1+20 E.			5.5	346.4	345.3 C/1
1+47 W.			6.5	345.4	344.4 C/0
1+75 W.			7.0	344.9	343.9 C/0
2+14 E			7.1	344.8	343.6 C/2
2+31 W			7.7	344.2	343.2 C/0
2+35 W			7.6	344.3	343.1 C/2
2+78 W.			7.8	344.1	342.7 C/4
2+83 E			7.6	344.3	343.0 C/3
3+10 E			7.9	344.0	342.8 C/2
(1P)	5.32	347.99	9.25	342.67	
3+22 W			4.6	343.4	342.3 C/1
3+46 E			4.1	343.6	342.4 C/2
3+52 W			4.9	343.1	342.1 C/0

ALLEY - BLOCK 6.
(Cont'd.)
WAT. MET. S.

		347.99			
4+08 E			5.3	342.7	341.9	C08
4+16 W.			5.5	342.5	341.5	C10
4+25 E			5.4	342.6	341.8	C08
4+45 W.			5.9	342.1	341.2	C09
4+74 W			6.7	341.3	341.0	C03
5+09 E			5.8	342.2	340.8	C14
5+27 W			6.7	341.3	340.2	C11
5+39 W			7.2	340.8	339.6	C12
5+61 E			6.9	341.1	339.1	C20
P	5.43	350.92	2.50	345.49		
CK B.M.			8.14	342.78	342.76	

SHASTA ST.

(3) STKS & GRDS. FOR WAT. MET.S

Back of Met Bx 22.5 from ℄ ST.

BM.	8.92	33.94 ~~32.07~~	25.02 ~~24.15~~		L℄T NE Cor KENDALL & LA PLAYA
0+00 = Nor Prop line La Playa.					
0+26 E.			5.5	28.4	28.6	$F0^2$
0+97 W			5.3	28.6	28.4	$C0^2$
1+18 E.			5.1	28.8	28.4	$C0^4$
1+74 W.			5.8	28.1	28.2	$F0^1$
2+17 W.			6.0	27.9	28.1	$F0^2$
TP	12.38	39.09	7.23	26.71		
0+00 = Nor Prop line Roosevelt.					
0+37 W			10.5	28.6	28.6	Edge SW Lin Rd 28.4 10.7 $C0^2$
0+94 W.			9.27	29.8	30.0	29.6 9.5 $C0^2$
TP	10.40	49.42	0.07	39.02		
0+00 = Nor Prop line Fortuna.					
0+34 E			6.2	43.2	42.4	$C0^8$
0+64 W			5.1	44.3	43.5	$C0^8$
1+11 E			4.2	45.2	44.1	$C1^1$
1+15 W			3.8	45.6	45.8	$C0^2$
1+67 W			2.9	46.5	46.1	$C0^4$
1+74 E			2.8	46.6	46.2	$C0^4$
2+44 W			1.1	48.3	47.4	$C0^9$
3+39 W			0.30	49.1	48.4	$C0^7$
TP	7.66	56.83	0.26	49.17		

SHASTA ST
(Cont'd)
WAT. MET.

	56.83				
3+85 W		7.0	49.8	49.1	CO 7
4+34 E		6.7	50.1	49.8	CO 8
4+58 W		6.1	50.7	50.2	CO 5
CK BM		11.35	45.48 =	45.59	
BM	9.98	55.57		45.59	
WATER MET 0+64 E W. So. SW Cor Pac. B Dr & Shasta		4.73	50.84	50.2	CO 6
P	2.20	53.04		50.84	
P	6.30	47.50	11.84	41.20	
WAT NW Cor Fortune & Shasta		2.97	44.53	42.00	CO 5
P	4.48	31.71		27.23	
WATER METER NW Cor KENDALL & ROOSEVELT		3.81	27.90	27.0	CO 9
P	3.9	32.5		28.6	
	4.65	32.55		27.9	
WAT. MET 2+63 W Shasta		4.50	28.0	27.9	CO 1

May 26, 1952
West
Line Powell
Varonfakis

Mason St.
San Diego Ave to Jefferson
(5) Stks & Grades For 6" Main
℄ of Main 10' So. & St

BM	155	24.62 ✓			23.07 ✓	SE 7' Left SE Cor Mason & San Diego Ave
			2.34	22.28 ✓		BP SW Cor. Mason & SD Ave
0+55			1.9	22.7 ✓	18.8	C41
1+00			3.0	21.6 ✓	17.9	C37
+50			3.7	20.9 ✓	16.8	C41
+75			4.0	20.6 ✓	16.3	C43
2+00			4.1	20.5 ✓	16.0	C45
2+25			4.6	20.0 ✓	15.8	C42
+50			5.1	19.5 ✓	15.6	C39
3+00			5.4	19.2 ✓	15.4	C38
+50			5.5	19.1 ✓	15.1	C40
4+01	6" G.V		5.9	18.7 ✓	14.8	C39
+06			6.0	18.6 ✓	14.8	C38
+10			6.3	18.3 ✓	14.8	C35
+45			4.9	19.7 ✓	15.0	C47
5+00			4.5	20.1 ✓	15.3	C48
+50			4.2	20.4 ✓	15.5	C49
6+00			3.8	20.8 ✓	15.8	C50
+50			3.7	20.9 ✓	16.0	C49
7+00			4.1	20.2 ✓	16.2	C40
+15	F.H.					
7+40			5.4	19.2 ✓	16.0	C32

MASON ST.

(3) STKS & GRADES FOR WAT MET

BACK of METER 17.5 from ℄ ST.

18.52

BM			
	24.62		
2+51 S		4.9	19.7 ✓
2+25 N		5.0	19.6 ✓
5+38 N		4.6	20.0 ✓
5+72.5 S.		3.6	21.0 ✓
5+39.5 N			
5+68 N		4.5	20.1 ✓
5+95.5 N		4.4	20.2 ✓
6+43.5 N.		3.8	20.8 ✓
7+15 F.H.			

Twiggs St
San Diego Ave
to 25' from E line Jefferson
6" Main
℄ of Main 10' South ℄ Twiggs

West
Kemp
Wilson

June 6, 52

BM	0.16	29.11 ✓	28.95		7"CI SW Cor Twiggs & San Diego Ave.
0+55		0.2	28.9 ✓	25.0	C39
1+00		1.0	28.1 ✓	24.1	C40
1+50		2.7	26.4 ✓	22.9	C35
2+00		3.1	26.0 ✓	21.7	C43
2+50		4.9	24.2 ✓	20.5	C37
3+00		6.0	23.1 ✓	19.4	C37
+50		7.2	21.9 ✓	18.2	C37
+75		7.8	21.3 ✓	17.4 15.6	C39
+80	G.V	8.2	20.9 ✓	17.4	C35
+85	TEE	8.3	20.8 ✓	17.4	C34
+95	G.V	7.9	21.2 ✓	17.4	C38
4+00				17.4	
+25		7.9	21.2 ✓	17.4 17.6	C38
+50		7.1	22.0 ✓	17.8	C42
5+00		6.6	22.5 ✓	18.2	C43
+50		6.1	23.0 ✓	18.6	C44
6+00		5.6	23.5 ✓	19.2	C43
+50		5.3	23.8 ✓	19.6	C42
6+85		5.4	23.7 ✓	19.8	C39
CK BM		0.16	28.95		

19.0 Elev 10"CI Top
10.1 Bot 18.1
.7
17.4

TWIGGS ST

③ WAT. MET.

29.11

2+43 So	4.3	24.8	24.8	CO^{0}
2+56 Nor	5.2	23.9	24.2	FO^{3}
2+95 Nor	6.3	22.8	23.2	FO^{4}
~~5+33~~ ~~4+33~~ So.	6.1	23.0	No Profile 22.5	CO^{5}
5+64 Nor	6.3	22.8	23.0	CO^{2}
6+10 So	5.3	23.8	23.3	CO^{5}
6+44 So	5.1	24.0	23.5	CO^{5}

EMERALD ST.
INGRAHAM TO JEWELL
④ STK'S & GRDS FOR 6" WATER

B.M.	13.38	73.73		60.35		SW 7' LET Hombland & JEWELL
TP	11.96	85.06	0.60	73.10		
TP	4.65	86.23	3.48	81.58		
CK BM	6.75	84.86 corr. Hi.		78.31	= 78.11	Cor/Porch of school - Ingraham & Emerald NW. Cor
0+85			10.21	74.65 ~~74.85~~	71.3 ~~71.7~~	C3 4
1+00			9.63	75.33 ~~75.42~~	71.6 ~~71.9~~	C3 6
+50			9.0	75.9 ~~76.1~~	72.4	C3 5
2+00			8.5	76.4 ~~76.6~~	73.0	C3 4
+50			7.75	77.1 ~~77.3~~	73.6	C3 5
3+00			7.4	77.5 ~~77.7~~	74.2	C3 3
+40			7.0	77.9 ~~78.1~~	74.7	C3 2
+50			6.94	77.9 ~~78.1~~	74.8	C3 1
4+00			6.6	78.3 ~~78.5~~	75.2	C3 1
+50			6.16	78.7 ~~78.9~~	75.4 ~~75.6~~	C3 3
5+00			6.0	78.9 ~~79.1~~	75.6 ~~76.0~~	C3 3
+50			5.64	79.2 ~~79.4~~	75.9 ~~76.4~~	C3 3
5+90	F.H. TE		5.3	79.4 ~~79.6~~	75.9	C3 5
	⑤ F.H.			80.3	79.8	CO 5 TO HANGE CO 6 TO ELL
6+00			5.4	79.5 ~~79.7~~	75.9 ~~76.7~~	C3 6
6+50	90° ELL		5.96	78.9 ~~79.1~~	75.9 ~~76.7~~	C3 0 ← 74.35 ~~74.55~~ TOP 6" V.C. SEW.
TBM			5.01	79.85 ~~80.05~~	(-5.5 TO)	← RIM SEW M.H @ JEWEL & EMERALD

JEWEL ST.
EMERALD to DIAMOND
④ STKS & GRDS FOR 6" WATER

		~~85.06~~ 84.86				
6+50			5.76	~~79.1~~ ~~77.3~~	~~75.9~~ ~~76.7~~	C3 2
7+00			4.05	~~80.8~~ ~~81.0~~	~~77.8~~ ~~78.7~~	C3 0
+50			2.0	~~82.9~~ ~~83.1~~	~~79.6~~ ~~80.6~~	C3 3
④ 8+00	10.31	~~95.05~~ ~~95.25~~	0.12	~~84.74~~ ~~84.94~~	~~81.5~~ ~~82.6~~	C3 2
+50			7.7	~~87.4~~ ~~87.6~~	~~82.6~~ ~~83.5~~	C4 8
9+00			5.65	~~89.4~~ ~~89.6~~	~~85.6~~ ~~86.5~~	C3 8
+50			4.2	~~90.9~~ ~~91.1~~	~~87.7~~ ~~88.4~~	C3 2
+60	F.H. TEE		3.8	~~91.3~~		88.1 C3 2
+70			3.25	~~91.8~~ ~~92.0~~	~~88.5~~ ~~89.2~~	C3 3
10+00			2.2	~~92.9~~ ~~93.1~~	~~89.1~~ ~~89.6~~	C3 8
④ +50	0.38	93.98	1.45	~~93.60~~ ~~93.80~~	90.2	C3 4
ck BM			10.44	83.52 = 83.59		℄ P.T. ℄ Diamond at E. Pl. Ingraham

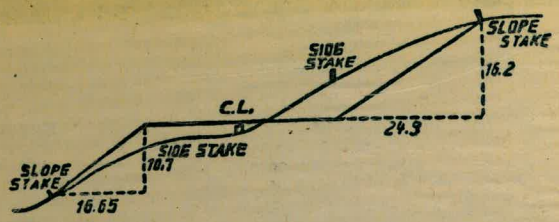
⑤ FH 9+60 92.2 92.4 FO 2 C3 3
2.9

Emerald & Jewel Water Meters

7-22-52

P	13.37	88.02	74.65		Ex 0+85 ②	
1+48 N		on Emerald	10.6	77.4	77.3	CO 1
1+98 S			11.0	77.0	76.7	CO 3
1+98 N			10.2	77.8	77.6	CO 2
2+02 N			10.0	78.0	77.7	CO 3
2+56 N			9.7	78.3	78.2	CO 1
3+38 N			9.3	78.7	78.8	FO 1
3+85 N			9.0	79.0	79.1	FO 1
4+60 N			8.1	79.9	79.8	CO 1
5+~~75~~ S.			8.0	80.0	79.6	CO 4
5+51 N.			7.6	80.4	80.6	FO 2 ck this ✓
7+32 E		on Jewel	4.8	83.2	84.0	FO 8 ✓
7+36 W			4.5	83.5	84.0	FO 5 ✓
P	9.45	96.61	0.86	87.16		
8+86 E			5.8	90.8	89.6	C 1 2 ✓
9+46 W			6.5	90.1	92.1	FZ 2 ✓
9+51 E		3 Mets	5.0	91.6	92.4	FO 8 ✓
9+71 W			4.7	91.9	92.4	FO 5 ✓
ck P @ (10+50)			3.01	93.60	= 93.60	

88.02 / 7.72 / 80.3 — 84.0 / 3.6 / 7.4



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
HOLYOKE MASSACHUSETTS
NEW YORK CHICAGO BOSTON SAN FRANCISCO