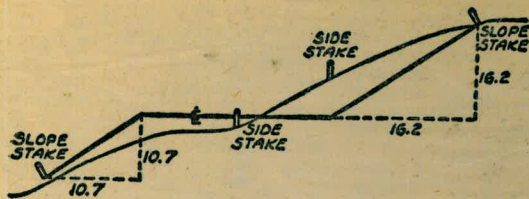




810



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

1007 Amen City Hts
1532 City Open Add

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center
Telephone F-7511 Ext. 313

MICROFILMED

JAN 16 1965

$$\begin{array}{r} 6.88 \\ \underline{11} \\ 6.88 \\ \underline{7.56} \\ 10.1530 \end{array}$$

MICROFILMED

JAN 15 1958

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide degree of curve and add correction found in column of correction. Degree of curve with negative sign is found by dividing tangent (or external) opposite by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

$$T = R \sin \frac{C}{2}$$

$$E = R (1 - \cos \frac{C}{2})$$

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	1.94	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.66	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.103	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.777	.877	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Wightman St 52nd St West ✓
Stks for 6" AC 3/4

Page
80 ✓

INDEX

ENCANTO
LOT 2 ROSEMONT ADDITION, SCIMITAR DRIVE ✓ 1. *alice*

STKS FOR WAT METERS MANZANITA DRIVE ✓ 2.
" " " " OLIVER AVE ✓ 3-4
" " " " POPLAR ST ✓ 5.
" " " " HANOVER ST ✓ 6.
" " " " 6" WAT MAIN JEWELL ST. ✓ 7.

ALIGNMENT & DETAILS - 12" PROPOSED PIPE ✓ 9-15
ON WIGHTMAN ST *alice*

PROFILE - WIGHTMAN ST ✓ 16-24

Profile Proposed WATER LINE - WINSTON ST ✓ 25-27

Stakes for WAT MET TURROSE MANZANITA ✓ 28.

" " " " VIOLET ST ✓ 29.

⑤ of sets for 12" C.I. Wightman St. ✓ 30-34

④ " " " 6" C.I. Briant St - Washington Nbr ✓ 35

② " " " 6" C.I. Brooklyn Ave - 59th / Merlin ✓ 36.

Elev & Location 606 Beacon - Jamaica & Union ✓ 37. *alice*

DENVER ST. Inquit to Milton, Profile for 6" WATER ✓ 44-48 ✓

Alley El Cajon to Orange betw 33rd & Fulton ✓ 49-50 *alice*

Bangor St. Harbor View - Talbot proposed water ✓ 51-53

Talbot St. - 400' W Bangor to Akron. ✓ 54-56 *alice*

Aiken St. 67th City View & proposed water ✓ 57-58

Bancroft St. Oceanview - Webster " " ✓ 59

Arlins St. & profile proposed water ✓ 60-63

Bancroft St. " " " " ✓ 64

" " & Profile " " *alice* ✓ 65-66

Sterne St. " " " " ✓ 68-70

Motena P.L. New Alignment 16" C.I. ✓ 38-40

Moore St. - Ampudia to Conde ✓ 41-43

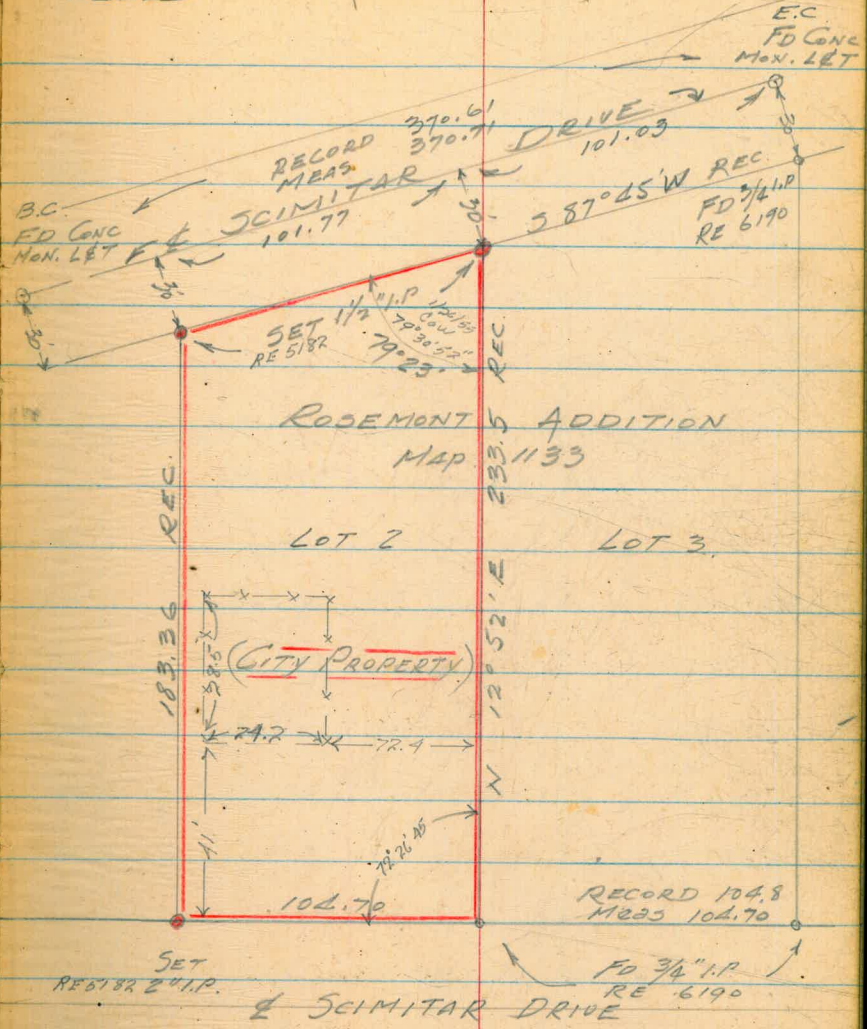
Montalain St. Kalma to Juniper ✓ 71-73

Vancouver St. Kalma to Juniper ✓ 74-77

EL CAJON BLVD - 58TH to SEMINOLE
LOCATION 16" C.I. WATER ✓ 78-79 *alice*

Cor's ESTABLISHED & FLAGGED
 LOT 2 ROSEMONT ADDITION
 SCIMITAR DRIVE - ENCANTO

Aug 28, 1951
 BEATY
 LEONARD
 SEAVELLO



87.45
 12.37
 100.79

STAKES SET FOR WATER METERS
MANZANITA DRIVE
SNOWDROP TO TUBEROSE

IP	5.36	294.75	289.39		3/4" IP Prop. Co
0+00 = BC MANZAN.					
0+88 Nor	= 88' W-BC	5.93	288.8	288.8	C02
0+445 So	= 445' W-BC	4.97	289.8	289.10	C02
IP	5.26	296.97	3.04	291.71	
0+00 = EC MANZAN.					
0+81 So	= 81' E-EC	5.03	291.9	289.90	C22
CK IP		7.58			

WATER METER - TUBEROSE; POPLAR - MANZAN

IP	7.83	297.22	289.39		
0+00 = Nor Line of Alley					
0+085 E		6.62	290.6	289.0	C16
0+202 W		5.08	292.1	289.4	C27
0+60 W		4.6	292.6	289.7	C29
0+952 W		4.75	292.5	290.0	C25
1+55 W		3.95	293.3	290.5	C21
2+195 W		2.0	294.2	290.8	C34
CK IP		7.83	289.39		

WATER METER Nor SIDE MANZANITA

IP	5.58	294.97	289.39		
0+00 = EC Nor MANZANITA					
0+24 Nor		2.97	292.00	290.1	C12

SEPT. 4, 1951

BEATTY
LEONARD
SEAVELLO

3.

STAKES SET FOR WATER METERS
OLIVER AVE
DAWES TO FANUEL

BM.	13.35	16.33	2.98		7' offset Hub. NW Cor. Dawes & Oliver
0+00 = E. Prop. line Dawes.					
0+02 Nor		11.8	04.5	03.3	C13
0+50 So.		12.6	03.7	02.9	C08
0+97.5 Nor		11.3	05.0	04.2	C08
1+08 So.		12.4	03.9	03.4	C05
1+72 So.		11.6	04.7	04.2	C05
1+73 Nor		10.8	05.5	05.0	C05
2+02 So.		11.0	05.3	04.6	C07
2+24 Nor		10.1	06.2	06.1	C01
2+69 Nor.		8.7	07.6	07.1	C05
2+74 So.		9.3	07.0	06.2	C08
3+25 Nor.		7.3 7.9	07.0 08.4	08.4	C06
3+28 So.		7.9 7.3	08.4 09.0	07.5	C02
3+71 Nor		6.3	10.0	09.5	C05
3+73.5 So.		6.5	09.8	08.6	C13
3+96 So.		5.9	10.4	09.2	C13
4+20 So.		5.3	11.0	09.7	C13
4+81 So.		4.3	12.0	11.2	C08
4+87 Nor		3.6	12.7	12.2	C05

9-1-51

4

WATER METERS Cont'd
 Oliver Ave
 Dawes to Fandel
 16.33

0+00 = E. Prop. line Everts

0+02 So.	1.9	14.4	13.4	C/P
0+08 No	1.2	15.1	14.2	C/P
TP 9.73 24.06	2.00	14.33		NE Cor Sidewalk 0+05 South
0+24 So	9.5	14.6	13.7	C/P
0+24 Nor	8.9	15.2	14.5	C/P
1+11 So.	7.8	16.3	14.8	C/P
1+51 So	7.1	17.0	15.4	C/P
1+69 Nor	6.4	17.7	16.3	C/P
2+23 So.	6.4	17.7	16.2	C/P
2+30 Nor	5.3	18.8	17.1	C/P
2+51 So.	6.1	18.0	16.6	C/P
2+91 Nor	5.0	19.1	17.9	C/P
3+00 So	5.2	18.9	17.2	C/P
3+375 Nor	4.5	19.6	18.5	C/P
3+71 Nor.	3.8	20.7	19.0	C/P
4+00 So.	4.4	19.7	18.5	C/P
4+26 Nor.	3.4	20.7	19.7	C/P
4+66 ^E Nor	2.8	21.3	20.3	C/P
ck BM	3.26	20.84		NW Cor Oliver & FANDEL
4+73 So	3.5	20.6	19.5	C/P
ck curb	4.26	19.84	19.80	
	0.64	23.46		TOP FH SE Cor Oliver & FANDEL

8-6-51
Beatty
Leonard
Seavello

STAKES SET FOR WATER METERS
POPLAR ST
DAHLIA - TUBEROSE

BM	5.17	293.06	287.89	Top FH Hollywood Park & Poplar
0+00 = NE Cor 7' offset Marlborough & Poplar				
0+11.5 Nor		6.5	286.6	285.7 C02
0+89 Nor		7.1	286.0	285.5 C05
1+26 Nor		6.9	286.2	285.9 C03
1+92 Nor		5.9	287.2	286.3 C09
2+43 Nor		4.6	288.5	288.3 C02
0+00 = NW Cor 7' offset Marlborough & Poplar				
1+73 Nor		3.05	290.0	289.4 C06
2+24 Nor		2.9	290.2	289.6 C06
TP 3.59				
3+63 Nor	293.41	3.24	289.82	289.2 C06
0+00 = NW Cor 7' offset Snowdrop & Poplar				
2+55.5 Nor		5.7	287.7	287.6 C01
2+01.2 Nor		5.7	287.7	287.4 C03
1+52 Nor		5.9	287.5	287.30 C02
ck BM		3.95	289.46	289.50 Conc Men 92' w NW Cor Tuberosa & Poplar
TP	6.07	298.26	1.22	292.19
SE 1/4 EC Curb Ret		5.44	292.8	290.4 C24
SW 1/4 Cor. Snowdrop & Poplar		8.9	289.4	288.4 C10

Sept. 7 1951

STAKES SET FOR WATER METERS
HANOVER ST
ROSWELL TO GENEVA

P	4.00	258.95		254.95		on sidewalk BX 802 pp 76
0+00 =	4' OFFSET Nor Line Rozwell St.					
2+015 W			5.6	253.4	253.1	C03
2+075 E			3.7	255.3	253.4	C19
2+56 W			6.7	252.3	251.5	C08
3+08 E			6.4	252.6	250.8	C18
3+63 E			8.4	250.6	249.4	C12
4+26 W			12.7	246.3	247.3	F10
P	4.50	255.24	8.21	250.74		
6+293 E			3.4	251.8	248.5	C33
6+73 F			4.4	250.8	248.7	C21

6+91' Prop Line to Side Geneva

P	5.34	260.49	0.09	255.15		
CK P			5.52	254.97		

1+10 = 1+50

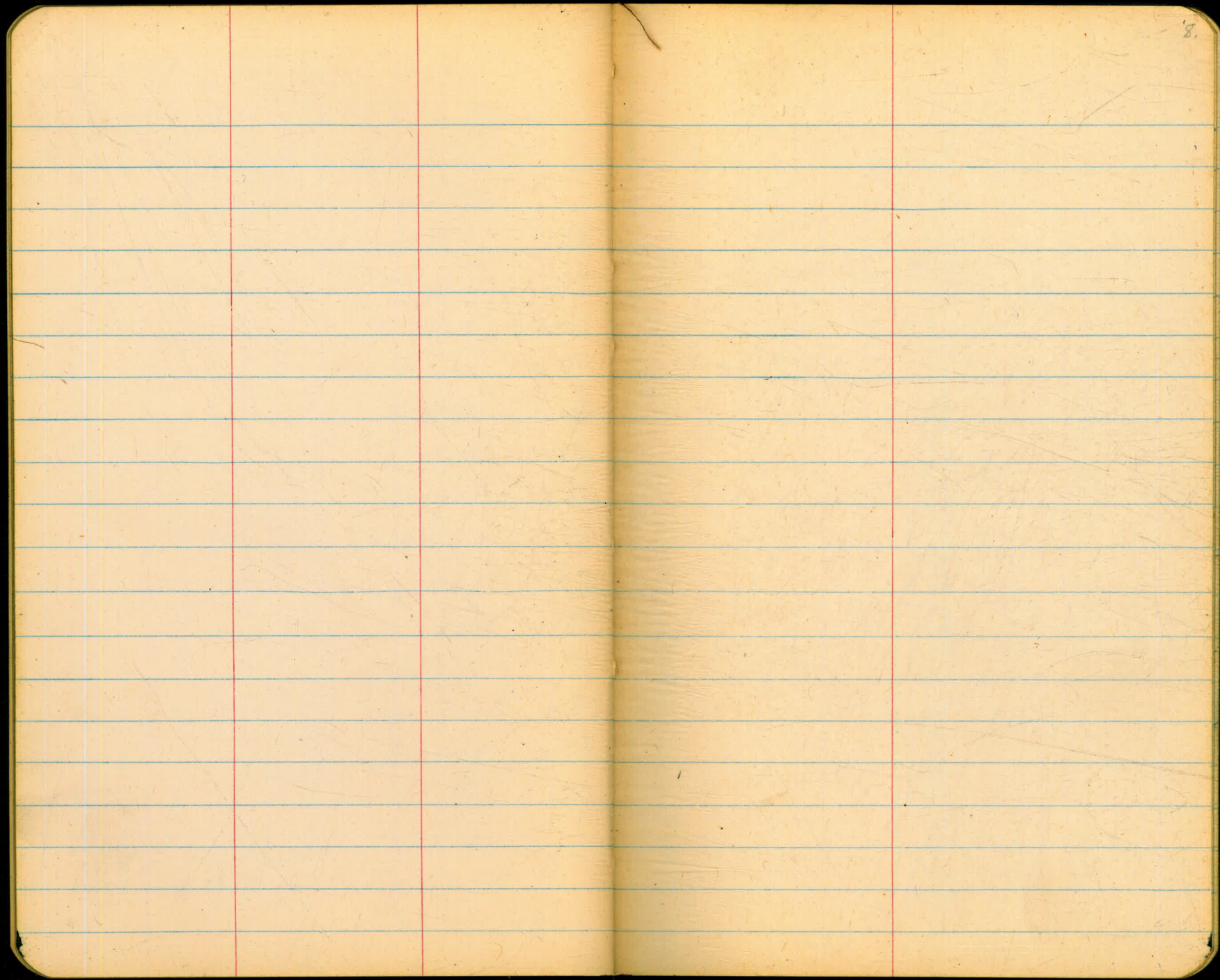
SEPT. 7 1951

7.

④ STAKES SET FOR 6" MAIN ON
JEWELL ST.

Moerland To La Playa

B.M.	2.03	35.71	33.68	BR NW Cor Ingraham & Moerland
ID	6.84	29.54		
0+00	10'50 & Moerland	13.01	22.70	
0+50		6.7	22.8	23.2 19.4 C34
1+00		6.7	22.8	23.4 19.6 C32
1+50		6.1	23.4	23.7 19.9 C35
2+00		5.4	24.1	23.9 20.1 C40
2+50		5.3	24.2	24.2 20.4 C38
3+00		5.1	24.4	24.5 20.7 C37
3+50		5.0	24.5	24.8 21.0 C35
4+00		5.0	24.5	25.1 21.3 C32
4+50		4.9	24.6	25.2 21.4 C32
5+00		4.7	24.8	25.2 21.4 C34
5+50		4.4	25.1	25.0 21.2 C39
6+00		4.6	24.9	24.7 20.9 C40
6+50		4.9	24.6	24.1 20.3 C43
7+00		6.6	22.9	22.8 19.0 C39
7+33	CONN To Cross 10'50 & La Playa.	6.7	22.8	
ID	10.66	35.60	4.60	24.94
ck BM.		1.90	33.70	= 33.68



ALIGNMENT & DETAILS
 PROPOSED 12" PIPE LINE
 ON WIGHTMAN ST

9-5-51
 BEATTY
 LEONARD
 SEAYELLO

9

4+52.92

PT

0°01'30" LT

70' WM
 18T

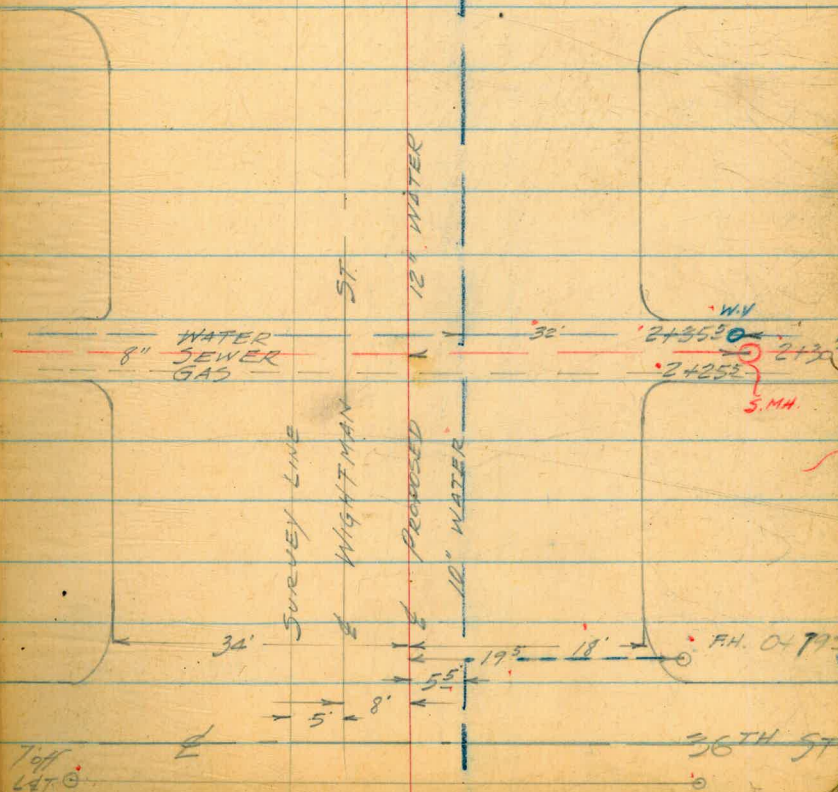
4+61

195

F.H. 4+65.5

CHEROKEE ST

ST



0+00

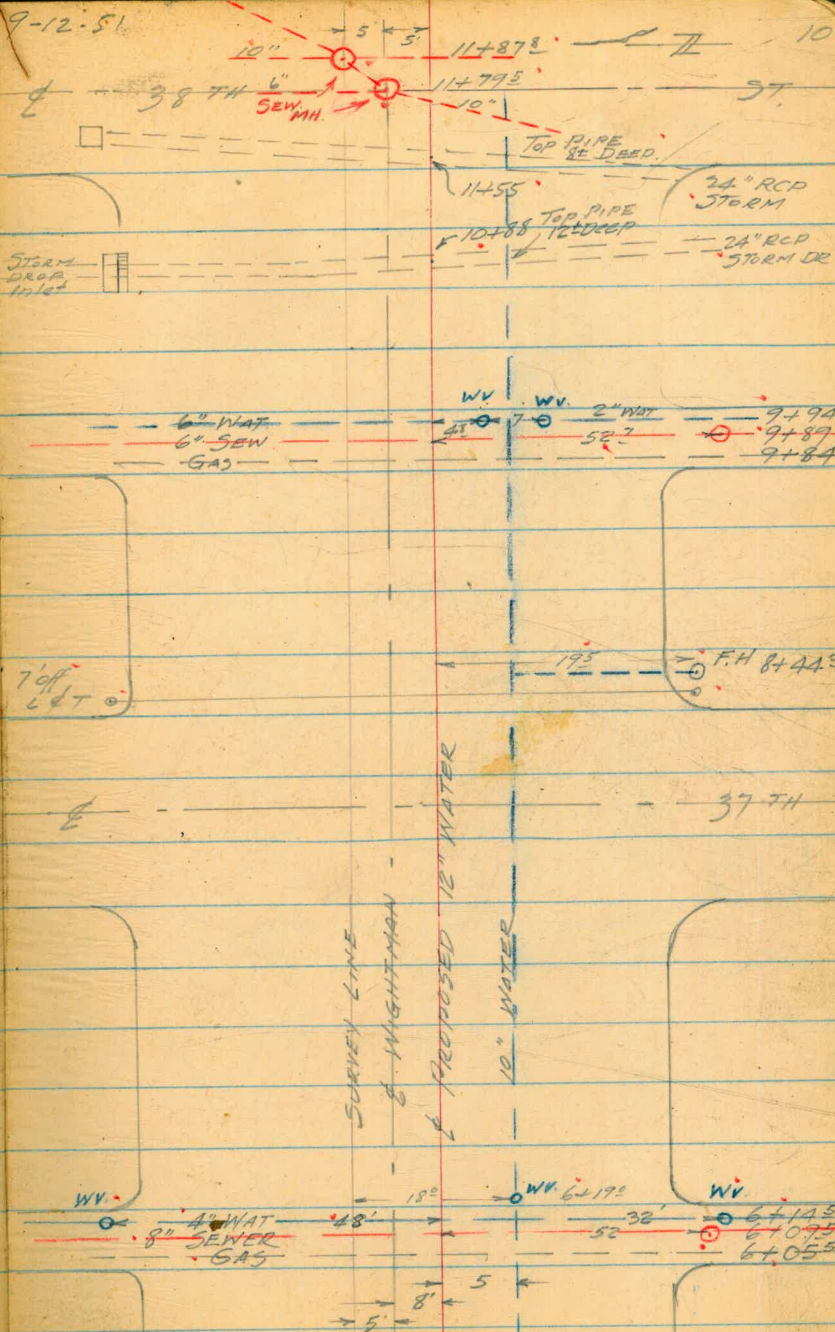
7' OFFSET WEST Prop. LINE 36TH ST

70' WM
 18T

F.H. 0+77.5

36TH ST

12" Proposed Pipeline
Wightman St



8+32.82 POT.

Proposed 12" Pipeline
Wightman St.

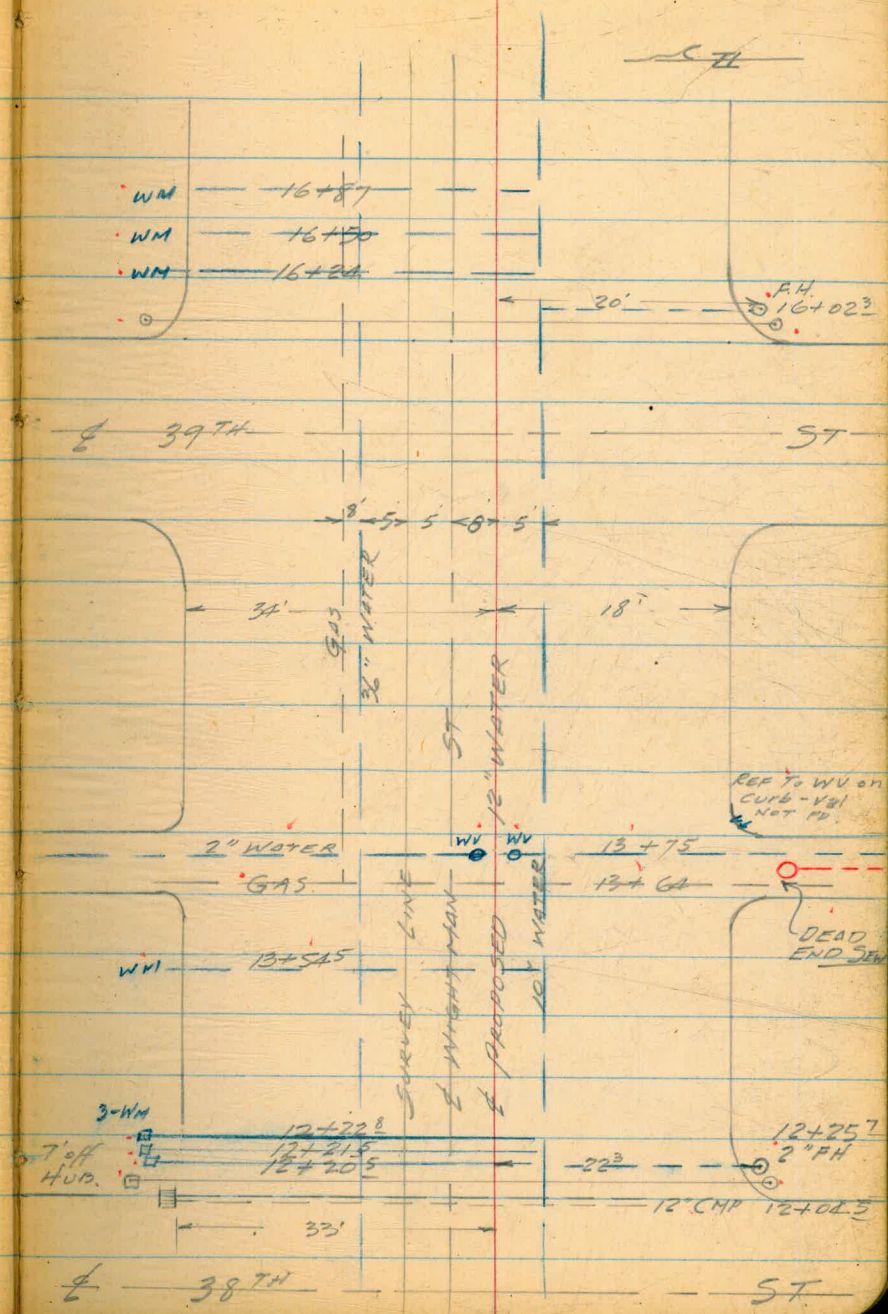
15+92.26 POT.

12+12.63 X PT 0°00'45" RT

248
5.78

9-12-51

11

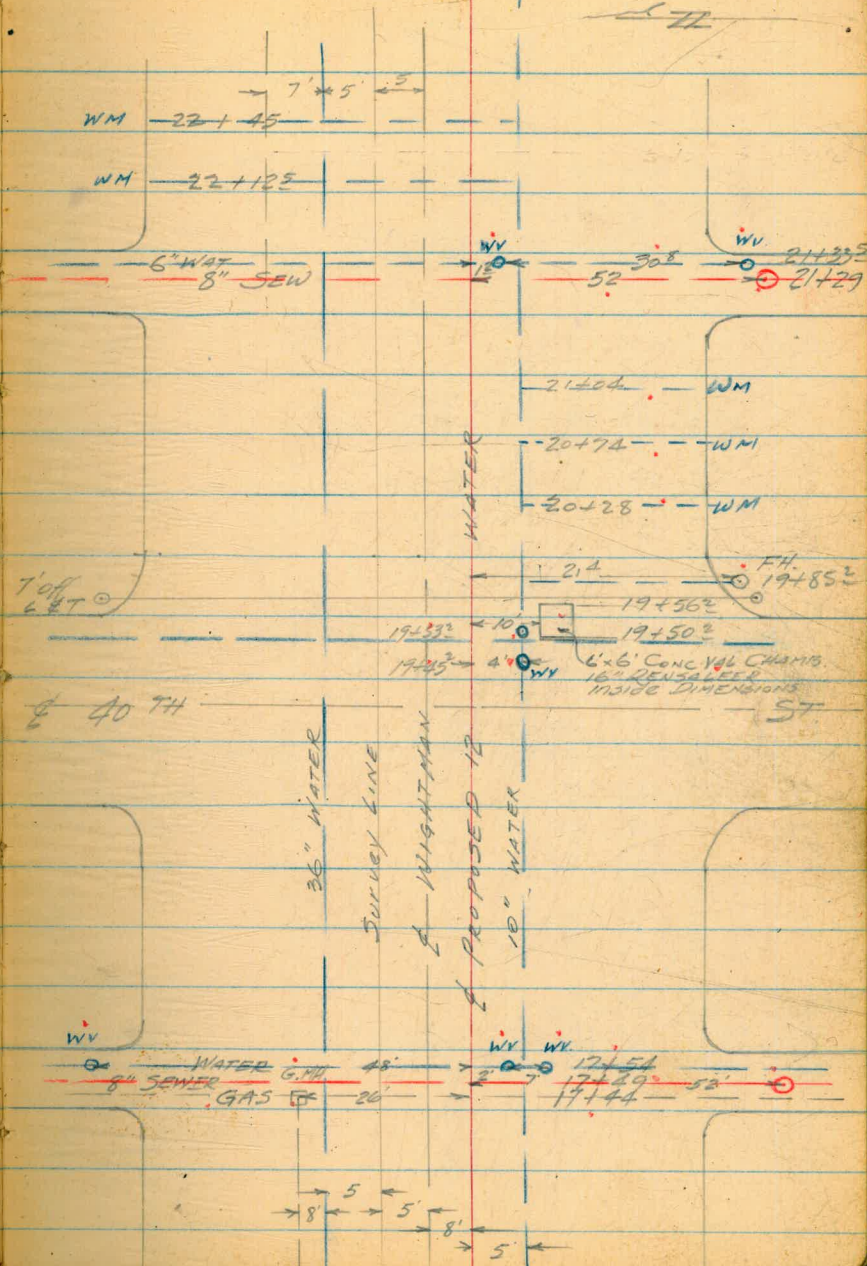


Proposed 12" Pipeline
WIGHTMAN ST.

9-12-51

12

19+79.16 X PT 0°08'15" LT.

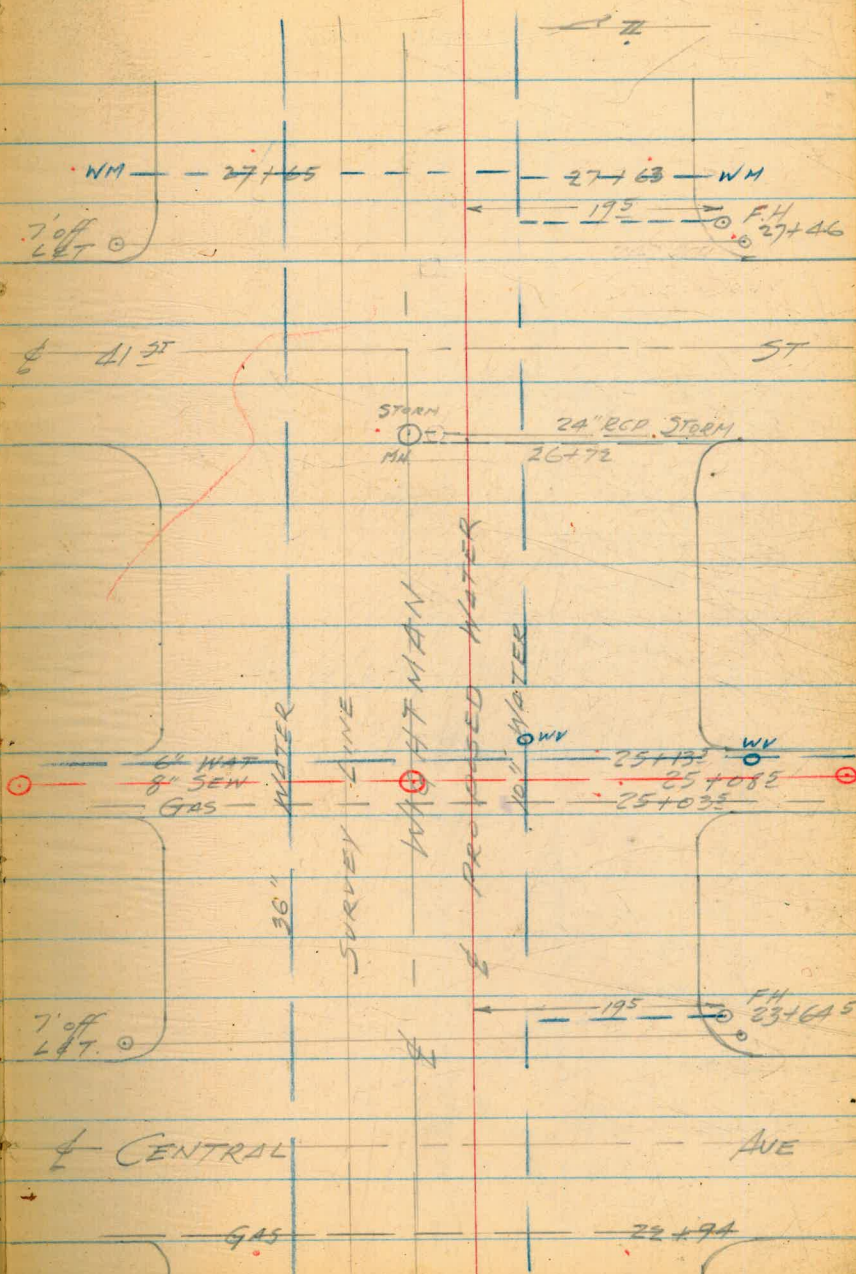


PROPOSED 12" PIPELINE
WIGHTMAN ST.

7-12-51

13

27+31⁵³ XPT 0°00'15" LT



23+51⁷³ XPT 0°02'30" RT

7' off
LPT

CENTRAL

AVE

PROPOSED 12" PIPELINE
WIGHTMAN ST.

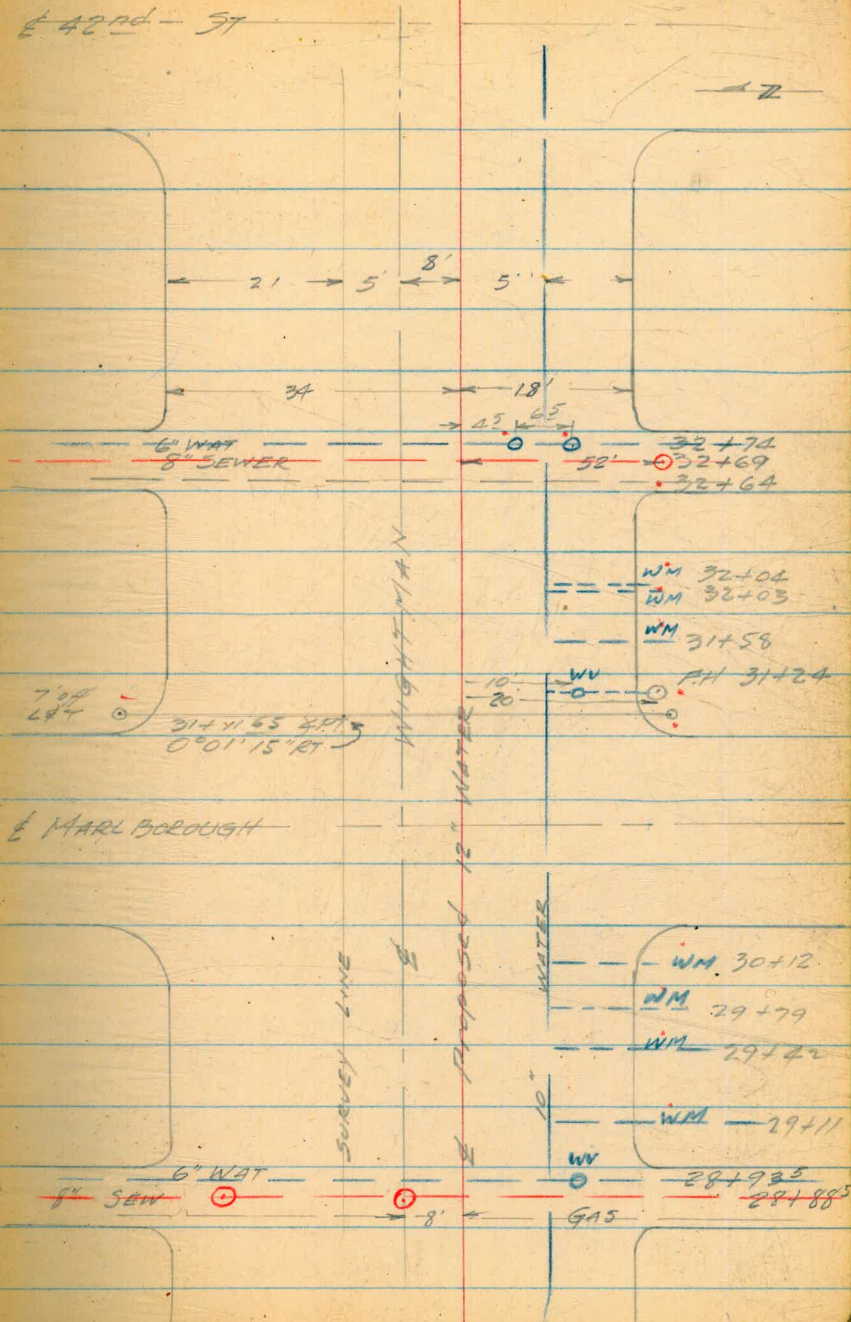
9-11-51

E 42nd - 37

14.

31+1165 X PT 0°01'15" LT

E MARLBOROUGH



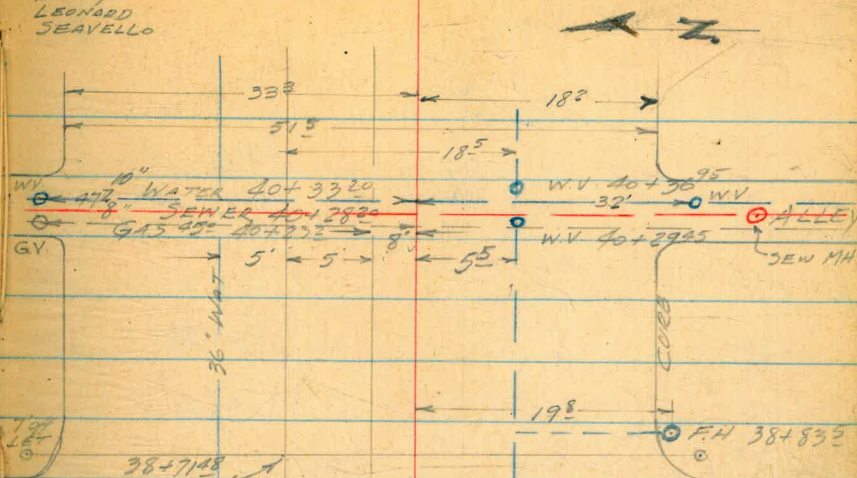
PROPOSED 12" PIPELINE
WIGHTMAN ST

9-11-15
BETTY
LEONARD
SEAVELLO

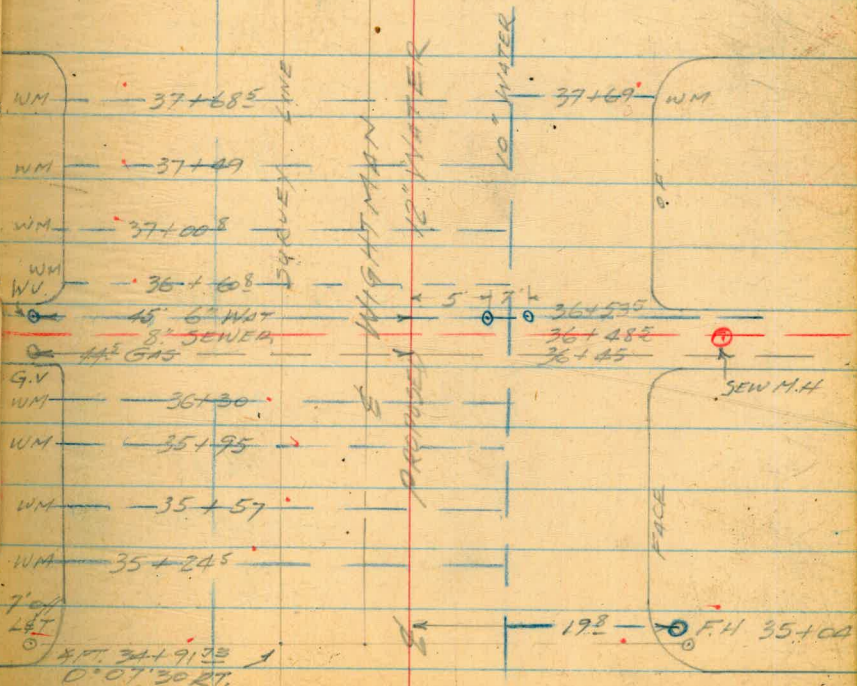
15

40+3320 Intersection of Water Line in
Alley between Van Dyke & 43rd

38+71.48 POT



VAN DYKE



34+91.73 RT

0°07'30" RT

RT 34+91.73
0°07'30" RT

12th St.

SEPT. 7 1951

BEATTY,
LEONARD,
SEAVELLO

16

2 PROFILE PROPOSED
PIPELINE ON
WIGHTMAN ST.
36th ST TO ALLEY/VAN DYKE & 43rd

B.M.	4.09	351.77	347.68	B.P. NW. Cor 36 th & Wightman
0+00	4.9	346.87		Prop. line Topsoil line west side 36 th St on A.C. Pavt.
0+07	5.1	346.67		on A.C.
0+33	4.0	347.77		" "
0+59	4.6	347.17		" "
0+80	4.1	347.67		End of A.C. (4" A.C.)
1+00	4.0	347.77		STREET SURFACE EXCEPT Where otherwise noted is covered with a light palliative coating of Asphalt to settle dust.
1+50	4.3	347.47		
2+00	4.5	347.27		
2+50	4.8	346.97		
3+00	5.0	346.77		
3+50	5.1	346.67		
3+81.5	5.6	346.17		Begin AC (5" A.C.)
3+95	5.9	345.87		on A.C.
4+00	5.7	346.07		" "
+21	5.3	346.47		" "
+61	5.8	345.97		End A.C. (5" A.C.)
5+00	6.3	345.47		" "
+50	7.4	344.37		" "

9-7-51

17.

E PROFILE PROPOSED PIPELINE
WIGHTMAN ST.

351.77

6+00		8.5	343.27	
+50		9.7	342.07	
7+00		11.1	340.67	
7+50		12.8	338.97	
HP	0.66	340.47	11.96	339.81 ✓
CK B.M.		1.60	338.87 ✓	OP NW Cor 37 th & Wightman S
7+60 ³		1.8	338.67	Begin A.C. (5" A.C.)
7+60 ²		1.7	338.77	on dirt
8+00		1.9	338.57	on A.C.
+40		2.4	338.07	End A.C. (5" A.C.)
+50		3.0	337.47	
9+00		6.0	334.47	
+50		9.1	331.37	
10+00		12.1	328.37	✓
HP	1.78	330.36 ✓	11.89	328.58 ✓
+50		5.4	324.96	SE Cor. End Alley part 45' LT 94' 95'
11+00		8.7	321.66	
+50		11.9	318.46	
+83		10.9	319.46	

Sept. 11, 1951
Beatty
Leonard
Seaville

18.

Profile Proposed PIPELINE
WIGHTMAN ST.

	330.36				
12+00		11.0	319.36 .		
+04		11.1	319.24 .		
+50		9.0	321.36 .		
CK BM		10.66	319.70 = 319.72	DR NW Cor 38th & Wightman	
13+00		5.8	324.56 .		
+50		2.5	327.86 .		
(P)	12.15	342.15 ✓	0.36	330.00 ✓	on CURBNE Curb ret of Alley
14+00		11.0	331.15 .		
+50		7.8	334.35 .		
15+00		4.8	337.35 .		
+20		3.8	338.35 .	Begin A.C. Pav't (5" A.C)	
+60		3.0	339.15 .	on " "	
16+00		2.8	339.35 .	End A.C. Pav't (5" A.C)	
+50		1.9	340.25 .		
17+00		1.5	340.65 .		
+50		1.0	341.15 .		
18+00		0.6	341.55 .		
+50		0.1	342.05 .		
(P)	5.59	347.43 ✓	0.91	341.84 ✓	Top Curb LT 18+00

Profile Proposed PIPELINE
WIGHTMAN ST

4/1/51

19.

	347.43			
18+99.3		5.1	342.33	Begin A.C. part (9 1/2" A.C.)
19+39.3		4.8	342.63	on " "
+83		5.7	341.73	on " "
+88.3		5.6	341.83	End A.C. part (9 1/2" A.C.)
20+00		5.2	342.23	
+50		5.1	342.33	
21+00		4.8	342.63	
+50		4.5	342.93	
22+00		4.4	343.03	
+50		4.4	343.03	
+79.4		4.4	343.03	Begin A.C. part (6" Conc. + 1/2" A.C.)
+94		4.8	342.63	on " "
23+00		4.6	342.83	" " "
+34		4.3	343.13	" " "
+45		5.3	342.13	" " "
+59		4.9	342.53	End A.C. part (6" Conc + 1/2" A.C.)
24+00		5.4	342.03	
+50		6.8	340.63	
25+00		7.9	339.53	
24	10.59 349.34 ✓	8.68	338.75 ✓	End Conc. Curb SE Cor. of Alley

2 PROFILE, PROPOSED PIPELINE
WIGHTMAN ST

	+19.5	349.34	-FS	
1	25+50		11.0	338.34.
1	26+00		12.1	337.24.
			13.4	335.94.
	+60		13.6	335.74.
2	27+00		13.4	335.94.
	+382		13.5	335.84.
2	+50		13.4	335.94.
	28+00		11.7	337.64.
2	+50		9.5	339.84.
	29+00		7.6	341.74.
			8.04	341.30.
			7.87	341.47.
	+50		5.7	343.64.
2	30+00		3.8	345.54.
	+39		2.3	347.04.
	+78.5		1.9	347.44.
	31+00		2.3	347.04.
2	+05		2.5	346.84.
	+50		1.7	347.64.
2	ck BM	10.42	357.55	2.21 347.13 = 347.09

Begin A.C. part (7" A.C.)
(4" A.C. 26+98.5)
End A.C. part (4" A.C.)

Hor edge rim MH 28' LT 28+91
" " " " 8' LT 28+88.5 / nu. 11.6 lower

Begin A.C. part (4" A.C.)

00 " "

" " "

" " "

" " "

(8" A.C. 31+12)

B.P. NW MARLBOROUGH & Wightman

E PROFILE, PROPOSED PIPELINE
 WIGHTMAN ST.

9-11-51

21.

Station	Grade	Elevation
32+00	9.1	348.45
+50	8.3	349.25
33+00	7.4	350.15
+50	6.6	350.95
34+00	5.7	351.85
+19	5.5	352.05
+32	5.9	351.65
+59	5.0	352.55
+84	5.5	352.05
35+00	5.1	352.45
+50	4.8	352.75
36+00	4.5	353.05
+50	4.1	353.45
37+00	3.9	353.65
+50	3.7	353.85
38+00	3.4	354.15
+125	3.7	353.85
+38	2.9	354.65
+50	3.0	354.55
OK BM	2.85	354.70

on AC part

B.P.
 NW. Cor VAN DYKE & Wightman

E Profile, Proposed 12" PIPELINE
WIGHTMAN ST

	357.55		
38+66		3.6	353.95
+79		3.2	354.35
39+00		3.3	354.25
+50		3.5	354.05
40+00		3.6	353.95
+33.20		3.7	353.85
SET TBM	4.45 358.53	3.47	354.08
		3.55	354.98
		^{9.2}	
		12.95	345.58
		^{9.6}	
		1.53	357.00
		^{9.6}	
		11.13	347.40
BM	3.58 358.28		354.70
		10.64	347.64
		12.00	346.28
BM	6.86 353.99		347.13
		9.98	344.01
2 BM			347.13

End conc curb SE Cor of Alley

Rim Sew M.H. }
 Inv. 8" Sew. at M.H. } 51' RT 40+28.20

Rim Sew M.H. }
 Inv. Sew M.H. } 278.7 LT. 40+28.20

BR. NW Cor Van Dyke & Wightman

Inv. 8" Sew 28.8' LT }
 Inv. 8" Sew 52' RT } 56+48.5

BR. NW Cor Marlborough & Wightman

Inv. 8" Sew. M.H. 52' RT 32+74
 Inv. 8" Sew M.H. 28.8' LT (Paved over Top)

WIGHTMAN ST

BM 3.30 350.98 ✓ 347.68
 8.87 342.11
 4.47 346.51

PP NW Cor 36th & Wightman

Inv. 8" Sew MH 52' RT }
 Inv. 8" Sew M.H. 287.5 LT. } 2+30.5

BM 10.24 350.05 339.81
 12.65 337.40 ✓
 7.14 342.91 ✓

OO NW Cor 37th & Wightman

52' RT }
 Inv. 8" Sew M.H. 288.2 LT. } 6+09.5

HP 3.37 331.95 ✓ 328.58
 11.10 320.85
 9.90 322.05

Inv. 6" Sew M.H. 52' RT }
 " " " " 128' LT } 9+89

CKP 3.37 328.58

DM 4.22 323.92 319.70
 13.55 310.37
 13.96 309.96
 5.46 318.46

PP NW Cor 38th

Inv. Sew MH Junct 10" & 6" Sew
 Inv. 10" Sew @ M.H. 13' LT 11+87.8
 Inv. 12" Corr. Cross Drain } 33' LT 12+04.5 other
 (unable to locate end)

HP 6.07 347.91 ✓ 341.84
 12.10 335.81
 9.42 338.49

Top curb Nor 18+00

Inv. 8" Sew M.H. 52' RT } 17+49
 Inv. 8" " " 288' LT }

HP 5.37 347.21 ✓ 341.84
 5.06 342.15
 8.86 338.35
 10.31 336.90
 HP 7.02 352.84 ✓ 1.39 345.82 ✓

Rim of M.H. to Conc Val Chamber 15' RT 19+55
 C of 16" Horiz RENSELEAR VAL.

Inv. 8" Sew MH 52' RT 21+29

9/12/51

WIGHTMAN ST

		352.84 ✓				
			12.58	340.26	Inv. 8" SEW M.H. 288' LT Sta 21+29	
TP	10.50	349.25 ✓		338.75	End of Curb SE Cor Alley	
			6.25	343.00	Inv. 8" SEW M.H. 248' LT	
TP	0.97	339.72 ✓		338.75	} 254.085	
			14.72	325.00		Inv. 8" SEW M.H. 153' RT
TP	3.30	342.05 ✓		338.75		
			13.97	328.08	Inv. 8" SEW M.H. 8' LT	
TP	2.10	340.85 ✓		338.75	Inv. 24" RCP Storm Drain at M.H. 26+73 5' LT	
			13.16	327.69		
			12.27	328.58	Inv. 24" RCP Storm Drain 21' RT 26+70	
P						

9/28/51

25.

Profile - Proposed Waterline
10' East of WINSTON
ROSWELL TO HILLTOP

BM	12.46	116.91 [✓]	104.45
	12.02	128.87 [✓]	0.06 116.85 [✓]
	13.15	141.42 [✓]	0.60 128.27 [✓]
	12.89	154.17 [✓]	0.14 141.28 [✓]
	13.37	166.94 [✓]	0.56 153.61 [✓]
	9.65	176.40 [✓]	0.19 166.75 [✓]

BR. NW Cor Bridge MARKET & Euclid

3rd TBM 5.98 170.42[✓]

Nail in Pole NW Cor Winston & Roswell

0+00 = 10.50' E ROSWELL
10' E WINSTON 7.6 168.80[✓]+19' E ST (E Jewer) 6.6 169.8[✓]+50 4.8 171.6[✓]+73' Near Prop. line.
Roswell ST. 3.8 172.6[✓]1+00 2.9 173.5[✓]+50 1.6 174.8[✓]+75 1.4 175.0[✓]2+00 1.9 174.5[✓]+50 3.7 172.7[✓]3+00 5.1 171.3[✓]+50 6.8 169.6[✓]+67 7.6 168.8[✓]

3/4" I.P. Prop. Cor 20' RT

2" WATER 135 RT

4+00 10.8 165.6[✓]9D 5.08 168.19[✓] 13.29 163.11[✓]+50 7.7 160.49[✓]

9/28/51

26

± PROFILE - PROPOSED WATER LINE
 10' E ± WINSTON ST.
 ROSWELL TO HILLTOP
 168.19

4+70	8.8	159.39 ✓
5+00	9.3	158.89 ✓
+50	7.0	161.19 ✓
6+00	3.6	164.59 ✓
+15	3.7	164.49 ✓
+50	6.7	161.49 ✓
7+00	9.9	158.29 ✓
+34	11.9	156.29 ✓
+50	11.4	156.79 ✓
+80	8.5	159.69 ✓
8+00	5.7	162.49 ✓
+24	2.4	165.79 ✓
+50	0.2	167.99 ✓
+69	1.0	167.19 ✓
9+00	5.2	162.99 ✓
+27	9.0	159.19 ✓
+40	9.5	158.69 ✓
+68	7.2	160.99 ✓
+74	7.9	160.29 ✓

10.9 ← Edge of road
 7.1

11.5
7

3/4" I.P. prop. Cor 20' RT 2" water 33 RT

{ AT BARRICADE (END OF GRADED STREET)
 2" WATER 35 RT.

9/28/51

27

± PROFILE - PROPOSED WATER LINE
10' East of WINSTON ST.
ROSWELL to HILLTOP
168.19

9+90		5.2	162.99 ✓
+94		2.5	166.69 ✓
10+00	11.93	0.80	179.32 ✓ 167.39 ✓
+15		12.8	166.52 ✓
+26		9.9	169.42 ✓
+27		9.4	169.92 ✓
+32		10.5	168.82 ✓
+34		10.2	169.12 ✓
+43		9.6	169.72 ✓
+50		4.7	174.62 ✓
		2.9	176.42 ✓
11+00	13.08	2.26	190.14 ✓ 177.06 ✓
+66		8.6	181.54 ✓
+85		4.6	185.54 ✓
11+00		2.3	187.84 ✓
+21	(2" water in Hilltop)	0.4	189.74 ✓
+27±			
SET TBM		5.32	184.82 ✓

9+60 on STR 10' LT 10+26 our sta

= 10+00 on STR 10' LT 10+66 our sta

10+92± 50 Prop line Hilltop (- fence line)

Approx. of Hilltop

Po Pole SW. Cor Hilltop & Winston

10-9-51

28

STAKES FOR WATER METERS
TUBEROSE, MANZANITA
& Violet

BM	7.98	294.38	286.40	Top FH Poplar & Violet		
East Side						
23' Nor	NE Cor	Poplar & Tuberoze	5.75	288.6	288.1	C05
39' So	West Side	93.9	299.05	4.72	289.66	
	SW Cor	MANZ & Tuberoze	5.08	293.97	290.6	C3A
South Side						
78.5	East BC	on MANZ	4.96	294.1	291.2	C29
North Side						
71.0	East of BC	on MANZ	6.4	292.65	290.71	C19
44.0	North Side	E. of BC	6.3	292.75	290.8	C20
63.0	North Side	West of BC	7.55	291.50	290.1	C1A
TP	5.02	297.07	7.00	292.05		
North						
81.0	E of EC		6.86	290.21	289.8	C04
South						
15.0	W of BC		4.01	293.06	291.2	C19
North						
18.0	W of EC		7.46	289.61	288.2	C12
North						
40.0	W of EC		7.30	289.77	288.0	C18
South						
72.0	W of EC		6.44	290.63	288.1	C25
North						
89.0	W of EC		8.51	288.56	287.4	C12
P			10.62	286.45		Don prop Cor

Violet^d WAT. MET.
Next page

10-9-51

29

Stakes For WATER METERS
VIOLET ST
MANZANITA TO POPLAR.

P	6.20	292.65	286.45	
0+00 = Prop line		MANZ & Violet		
1+69 East	5.8	286.9	285.5	C1 ^d
1+87 W	8.4	284.3	282.5	F0 ²
2+13 E	6.2	286.5	285.2	C1 ³
2+43 W	7.5	285.2	284.1	C1 ^L
2+98 W	8.7	284.0	283.7	C0 ²
3+49 W	10.0	282.7	283.2	C0 ⁵
P	6.84	286.41 = 286.4		Top FH. Poplar & Violet

WATER METERS on Poplar

BM	5.02	294.31	289.29	Top FH
0+00 = Prop line		Tuberose		
0+68 Nor	5.3	289.0	288.3	C0 ²
1+26 Nor	6.0	288.3	288.10	C0 ²
CK BM	7.97	286.34	286.38	

⑤ STAKES SET FOR 12" MAIN
WIGHTMAN ST

OCT. 11 1951
Beatty
Leonard
Beavello

30

1 BM	3.01	350.69		347.68		
CP	5.54	344.38	11.85	338.84		
6+00			1.8	342.6	338.1	C45
+50			3.0	341.4	336.9	C45
7+00			4.3	340.1	335.7	C44
+50			5.8	338.6	334.5	C44
8+00			5.9	338.5	333.8	C47
+50			7.3	337.1	333.1	C42
9+00			10.6	333.8	329.9	C39
TD	0.34	331.73	12.99	331.39		
+50			0.9	330.8	326.7	C41
10+00			4.0	327.7	323.5	C42
+50			7.4	324.3	320.3	C40
11+00			10.7	321.0	317.1	C39
+37			13.0	318.7	314.8	C39
+62			13.1	318.6	314.2	C44
12+12			12.6	319.1	314.9	C42
+50			11.0	320.7	317.2	C35
13+00			7.7	324.0	320.3	C37
+50			4.4	327.3	323.4	C39
14+00			1.0	330.7	326.5	C42
TD	13.31	343.30	1.74	329.99		

10-11-51

31.

⑤ OFFSET STAKES SET
FOR 12" C.I. MAIN
WIGHTMAN ST.

343.30

14+50 2.6 333.7 329.6 C41

15+00 6.5 336.8 332.7 C41

IP Top Ft. 4.53 345.94 1.89 341.41

OCT 25, 1951

Betty
Leonard
Powell

+50 7.2 338.7 334.3 C41

16+00 6.9 339.0 334.9 C41

+50 6.4 339.5 335.4 C41

17+00 5.9 340.0 336.0 C40

+50 5.2 340.7 336.5 C42

18+00 4.7 341.2 337.1 C41

+50 4.3 341.6 337.6 C40

18+99 PLUG 3.8 342.1 338.1 C40

19+86 TFF 4.1 341.8 337.8 C40

3.22 347.95 1.21 344.73

1.4
.009
1.26

20+00 5.85 342.1 337.9 C42

+50 5.85 342.1 338.0 C41

21+00 5.6 342.4 338.2 C42

+50 5.35 342.6 338.3 C42

22+00 5.25 342.7 338.5 C42

+50 5.3 342.7 338.6 C41

WIGHTMAN ST.

10-25-51

32.

⑤ OFFSET STAKES FOR 12" C.I.

STATION	+BS	H.I.	-FS	ELEV	GRADE	CUT or FILL
23+00		347.95	5.25	342.70	338.6	c4 ¹
CE H			9.20	338.75 = 338.75		Top Curb
SET II	0.00	344.79	3.16	344.79		Top FH. SE. Cor Central
+50			2.6	342.2	337.9	c4 ³
+75			2.77	342.0	337.7	c4 ³
24+00			3.27	341.5	337.1	c4 ⁴ ✓
+50			4.47	340.3	336.0	c4 ³
25+00			5.8	339.0	334.8	c4 ²
+50			7.0	337.8	333.9	c4 ¹
26+00			8.0	336.8	332.5	c4 ³
+50			9.1	335.7	331.9	c4 ³
+75			9.07	335.7	330.9	c4 ⁸
27+00			8.85	335.9	331.2	c4 ⁷
+50			9.2	335.6	331.9	c3 ⁷
28+00			7.2	337.6	333.7	c3 ⁹
P +50	12.57	351.92	5.44	339.35	335.5	c3 ⁹
29+00			10.5	341.4	337.3	c4 ¹
+50			8.4	343.5	339.1	c4 ⁴
30+00			6.6	345.3	340.9	c4 ⁴
+25			5.7	346.2	341.9	c4 ³

10/29/51

WIGHTMAN ST.

10/29/51

33

⑤ OFFSET STAKES FOR 12" C.I

	351.92				
30+50		5.1	346.8	342.1	C47
31+00		4.9	347.0	342.4	C46
+25		4.9	347.0	342.5	C45
+50		4.4	347.5	342.9	C46
CK BM		4.75	347.17 = 347.13		BP NW Cor Marlborough & Wightman
32+00		3.6	348.3	343.8	C45
+50		2.7	349.2	344.7	C45
33+00		1.9	350.0	345.5	C45
+50		1.2	350.7	346.4	C43
33+75	7.73 358.86	0.79	351.13	346.8	C43
34+00		7.3	351.6	346.9	C47 ✓
+50		6.6	352.3	347.2	C51
35+00		6.5	352.4	347.5	C49
+50		6.2	352.7	348.0	C47
36+00		5.9	353.0	348.2	C48
+50		5.7	353.2	348.5	C47
37+00		5.4	353.5	348.7	C48
+50		5.1	353.8	349.0	C48
38+00		4.8	354.1	349.2	C49

WIGHTMAN ST
⑤ OFFSET STAKES, FOR 12" C.I

10/29/51

34

358.86

CK BM	4.13	354.73	354.70	BP. NW Cor Van Dyke & Wightman
38+50	4.4	354.5	349.8	C4.7
39+00	4.9	354.0	349.8	C4.2
+25	4.9	354.0	349.9	C4.1
+50	5.0	353.9	349.8	C4.1
40+00	5.2	353.7	349.6	C4.1
+33 ² END	5.3	353.6	349.5	C4.1
CK BM	4.13	354.73	= 354.70	PR as above

④ STAKES FOR 6" WATER MAIN
BRANT ST.
WASHINGTON NORTHERLY

Nov. 5 1951
Beatty
Leonard
Powell

35.

6214-L ~ W.O. # 2-1223-5

BM.	1.69	278.68		276.99		ALBATROSS SP. NW Cor WASHINGTON Cor. CURB
TP.	0.13	266.31	12.50	266.18		
0+00			6.5	259.8		Corner to 24" MAIN
0+40	Northernly prop. line Washington.		7.1	259.2	259.10 255.3	C39
0+90			11.97	273.57	4.71	261.60
1+40			9.9	263.7	263.6 259.8	C39
1+90			7.9	265.7	265.6 261.8	C39
2+40			6.1	267.5	267.6 263.8	C37
2+90			4.4	269.2	269.7 265.9	C33
3+40			3.4	270.2	270.7 266.9	C33
3+90			3.6	270.0	270.2 266.4	C36
4+40			5.0	269.6	269.9 265.1	C35
4+90			4.8	268.8	267.5 263.7	C51
5+12			4.0	269.6	266.7 262.9	C62
TP	12.04	277.91	7.70	265.87		
CK BM			0.92	276.99		

STAKES SET FOR 6" MAIN
BROOKLYN AVE
59TH TO MERLIN DR.

OCTOBER 17 1951

BEATTY
LEONARD
POWELL

30

BM	13.22	247.75		234.53		L&T 60 th & Brooklyn
P	13.25	260.89	0.11	247.64		
P	0.67	258.41	3.15	257.74		Top F.H. SE Cor Brooklyn & 59 th
0+00	= E. Prop line 59 th		0.9	257.5	257.5 253.7	C38
+50			2.6	255.8	256.1 252.3	C35
1+00			4.1	254.3	254.4 250.6	C32
+50			6.4	252.0	252.4 248.6	C34
+87			8.2	250.2	250.6 246.8	C34
1+91	TEE-on Merlin		8.2	250.2	250.5 246.7	C35
P	0.04	248.10	10.35	248.06		Top City Eng Tegin Curb
P	0.33	235.40	13.03	235.07		SW Cor. Merlin & Brooklyn
P	0.07	222.18	13.29	222.11		
OK BM			12.88	209.30 = 209.24		L&T Merlin & Kenwood

ELEVATIONS & DISTANCES
JAMACHA & LISBON TO
606 BEACON ST.

Oct. 22, 1951

Beatty,
Leonard,
Powell.

37

TBM.	13.35	284.66		271.31
P.	12.00	296.56	0.10	284.56
P.	11.62	307.04	1.14	295.42
P.	13.14	319.72	0.46	306.58
P.	5.25	323.34	1.63	318.09

2nd 1st Prop. Cor. Bk 673 pg. 70.

3.08 320.26

Top FH SE Cor. LISBON & JAMACHA RDS

7.82 315.52

Top WAT. VAL

6.41 316.93

Top of METER

P. 13.05 334.69 1.70 321.64

P. 12.89 347.56 0.02 334.67

P. 10.41 357.91 0.06 347.50

3.69 354.22

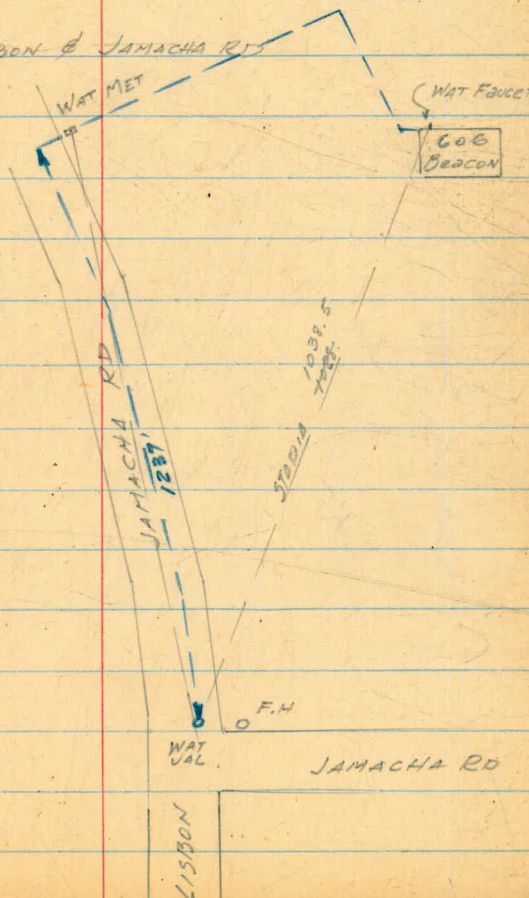
Top Faucet

P. 4.38 350.23 12.06 345.85

P. 0.11 337.22 13.12 337.11

P. 0.58 324.76 13.04 324.18

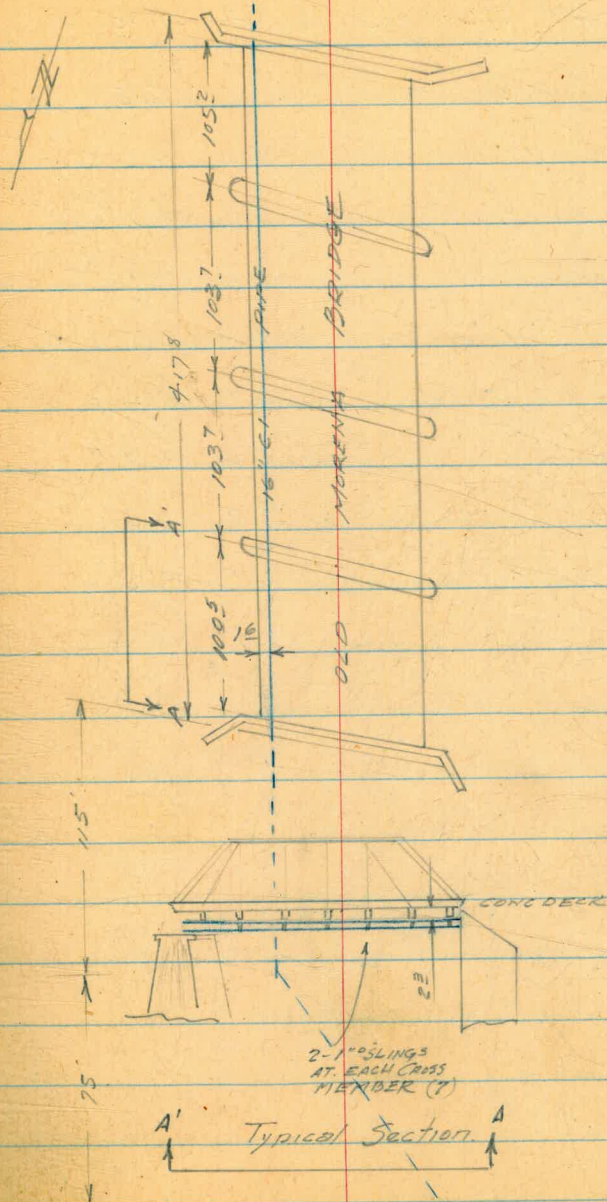
7.80 316.96 = 316.73 Top WAT. MET



16" C.I. PIPELINE
OLD MORENA BRIDGE

Nov. 14 1951

39



ELEV. ON A.C. PAVT Top of 10 C.I
LINDA VISTA ROAD
AT STATIONS ON "A" LINE

Nov. 14

20.

P	4.03	19.88	15.85
3+50		5.2	14.7
4+00		5.6	14.3
+50		6.0	13.9
5+00		6.4	13.5
+50		6.7	13.2
6+00		7.0	12.9
+50		6.9	13.0
7+00		6.7	13.2
+53		6.5	13.4
8+00		6.3	13.6

MOORE ST.
AMPUDIA TO CONDE
PROPOSED 6" WATER LINE

7+25 & CONDE ST.

3+93.12 7' off line w/estly - Arista

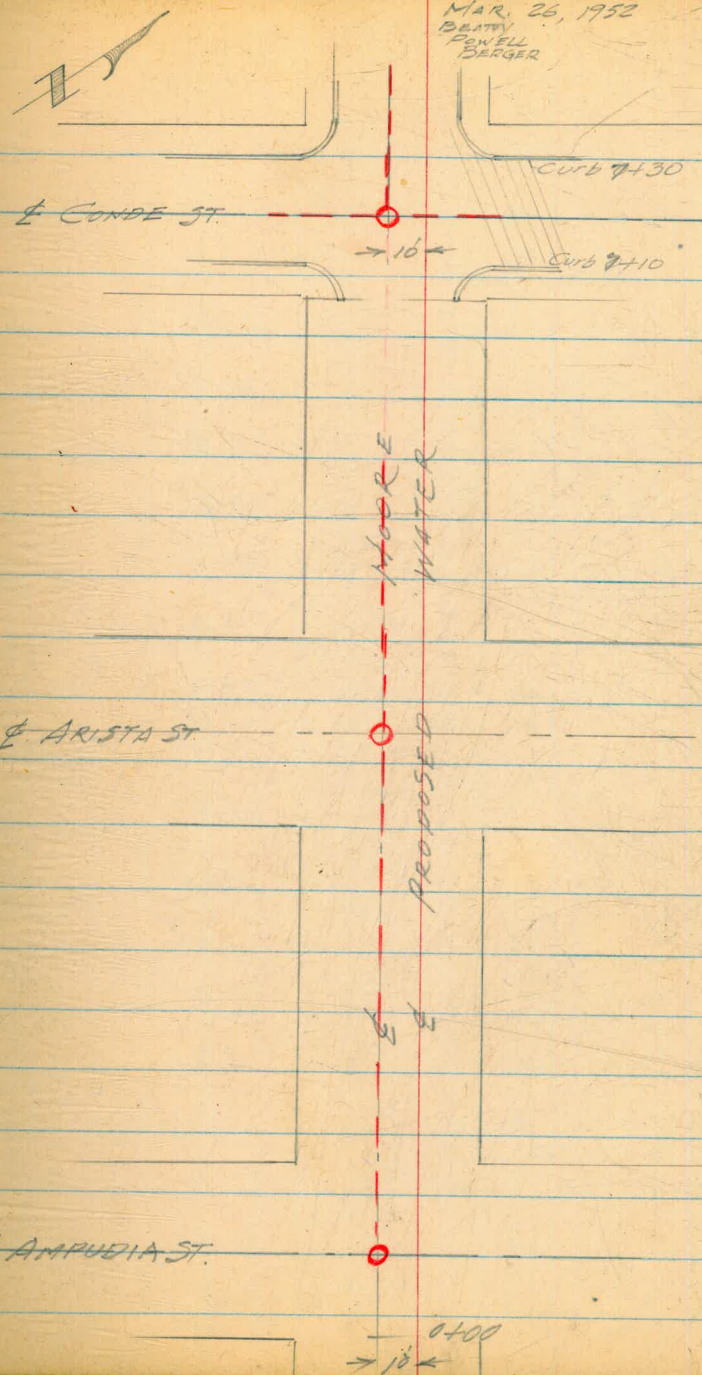
3+75.12 & ARISTA

7+25

0+00 Easteclly Prop. Line AMPUDIA

MAR. 26, 1952
BEATTY
POWELL
BERGER

41.



MOORE ST
(CONT'D)

± PROFILE
PROPOSED 6" WATER LINE

BM	027	44.02	43.75
IP	0.00	34.53	9.49 34.53
SET TBM.		3.08	31.45
0+00		6.12	28.4.
+10		6.17	28.4.
+25		5.95	28.6.
+31.5		6.02	28.5.
+40		6.25	28.3.
+50		6.15	28.4.
	Inv.	10.27	24.06
	Rim	6.15	28.4.
1+00		6.6	27.9.
+50		6.6	27.9.
2+00		6.9	27.6.
+50		7.1	27.4.
3+00		7.3	27.2.
IP	1.39	28.38	7.54 26.99
+50		1.4	27.0.
+75.		1.0	27.4.
	Rim	0.57	27.8.
	Inv.	6.92	21.46

MAR. 26, 1952

42.

9-31
2-99
7-32

BP S.E. COR AMPUDIA & SAN DIEGO

Top F.H. SE Cor Ampudia & Moore

ON AC.

CURB 5'-RT

0+08.5 20' RT F.H.

0+12.5 20' RT W.V.

0+18 Water Xing

0+18 W.V. 20' LT

10' LT 0+25 SEW. M.H.

5' LT Gas MH

+50 END CURB 5'-RT

+51 6' RT Po. & ST LIGHT POLE #2352

} SEW MH 10' LT 0+25

1+03 30' LT WAT MET

1+20 Gas Ser Xing 1+39 Gas Ser Xing

1+57 Gas Ser Xing 1+29 6' RT Po. Pole #2370

1+58 31' LT WAT MET 1+72 6' RT WAT MET

2+26 6' RT WAT MET

2+38 33' LT WAT MET

2+52 6' RT Po. Pole #2380

2+74 33' LT WAT MET

3+34 27' LT WAT MET

3+49 5' RT Po. Pole #2398

& ARISTA

} SEW M.H. 10' LT

MOORE ST.
(Cont'd)
E PROFILE
PROPOSED 6" WATER
28.38

4+00		1.3	27.1.	
+50		4.4	24.0.	
5+00		8.5	19.9.	
+50		13.1	15.3.	
IP	0.18	15.52	13.04	15.34
6+00		7.2	08.3.	
+15		9.5	06.0.	
+50		11.5	04.0.	
+80		12.4	03.1.	
7+00		12.4	03.1.	
+25		13.1	02.4.	
		Rim 13.47		
		TOP 15.77		
SET TBM	12.72	16.04	12.21	03.31
IP	13.15	28.63.	0.56	15.48
IP	6.02	33.36	1.29	27.34
CK TBM	12.58	44.03	1.91	31.45
CK BM.		0.25	43.78	-43.75

3/26/52

43

3+99 11" RT WOT. MET
4+05 " " "
4+41 27' LT " "
4+72 95 RT. " "
5+04 } 26' LT " "
+06 }
5+07 Gas Ser Xing
5+26 } 7' RT. " "
+27 }
+28 }
5+27 } 25' LT " "
+28 }
+29 }
5+49 6" RT. Pole 2422
5+61 Gas Ser. Xing
5+76 6" RT 2-Gov Anc
6+08 Gas Ser Xing

E Conde St

SEW M.H. 10' LT 7+25

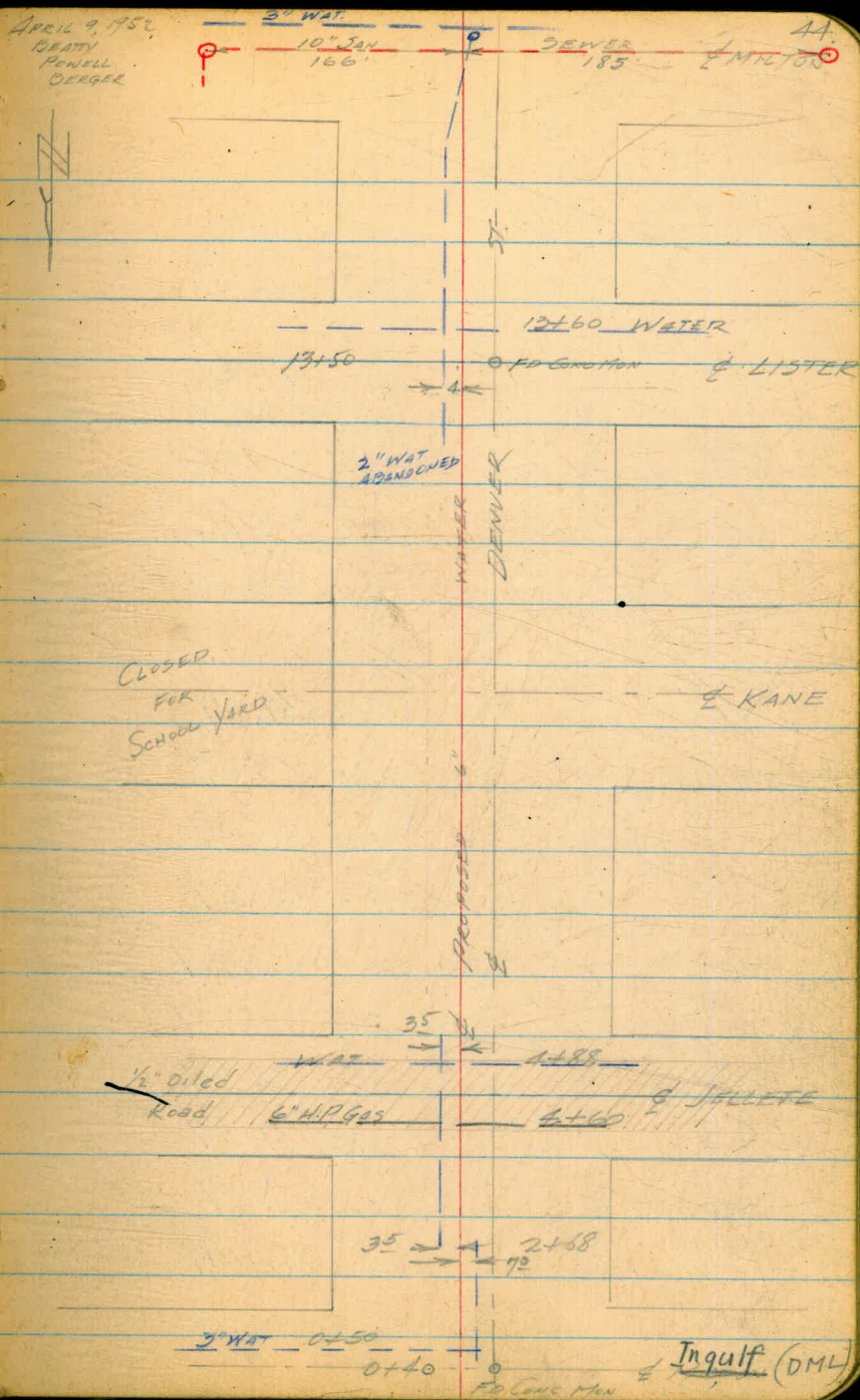
SET NAIL IN Pole Pole E of Moore & Nor Pl. Conde

Top E.H. Ampudia & Moore

BP SE Cor Ampudia & SAN DIEGO

DENVER ST.
INGULF To MILTON
PROPOSED 6" WATER

APRIL 9, 1952
DEATH
PENELL
DEEGEL



DENVER ST.
INGULF TO MILTON
& PROFILE
PROPOSED 6" WATER

April 9

45

BM	1.51	42.54	42.03
			37.83
		Rim 5.71	28.58
		Inv. 14.96	
TP	4.02	37.07	10.51 33.03
			Rim 9.53 27.54
			Inv. 16.43 20.64
17+89		4.7	32.37
+70		3.6	33.47
+64		3.2	33.87
		4.70	32.37
		6.00	31.07
17+50		3.4	33.67
17+00		4.0	33.07
+50		4.5	32.57
16+00		4.8	32.27
+50		5.2	31.87
15+00		5.5	31.57
+50		5.5	31.57
14+00		5.2	31.87
+50		1.6	32.47
TP	10.49	42.62	4.94 32.13

BP SW COR MILTON & FRIS

SEW M.H. 166' LT 17+80

SEW M.H. 185' RT 17+80

17+89 8" C.I.
3" W.I. WATER
17+88 E W.V. 0.2 RT

17+64 24" CMP Cross Drain

Inlet 10' LT

Outlet 31' RT

17+36 2' LT WAT MET
16+52 29' RT " "
16+13 25' RT " "
15+94 14' LT " "
15+76 25' RT " "
15+65 10' LT " "
15+27 27' RT " "
15+06 8' LT " "
14+52 29' RT " "
14+22 9' LT " "
14+15 13' LT " "

Top Conc Man & Lister & DENVER

DENVER ST.
INGULF TO MILTON
& PROFILE
PROPOSED 6" WATER
42.62

4/8/52

46

13+40		10.0	32.62
+37		10.5	32.12
13+00		9.7	32.92
+50		8.5	34.12
12+00		7.7	34.92
+50		6.6	36.02
11+00		5.3	37.32
+50		4.4	38.22
10+00		3.5	39.12
+50		2.1	40.52
9+00		1.0	41.62
RD	9.90	50.54	1.98
			40.64
+50		7.5	43.04
8+00		6.3	44.24
+50		5.4	45.14
7+00		4.7	45.84
+50		3.9	46.64
6+00		3.1	47.44
+50		3.9	46.64

2" WAT. 4' LT. & 11 1/2'

12+77 29' RT WAT. MET
12+32 32' RT " "

12+26 } 30' RT 2-WAT MET'S
12+27 }

NAIL IN ST. LIGHT POLE SW COR KANE & DENVER

7+50 }
7+36E } Conc STEPS UP TO
 } Conc SIDEWALK TO
 } SCHOOL BLDG 5' LT

7+03 7' LT WAT MET
6+99 GAS SER King to School

6+18 5' LT End 8" Conc Tile Drain
 From School yard

5+97 } 5' LT Conc Steps up to
5+91 } School yard

DENVER ST.
INGULF To MILTON
& PROFILE

4/8/52

47

50.54

5+00		5.4	45.14
4+87		5.45	45.09
473		5.40	45.14
459		5.63	44.91
450		6.0	44.54
4+00		5.0	45.54
P	10.02	57.20	3.36 47.18
+50		10.9	46.30
3+00		8.8	48.40
+50		7.6	49.60
2+00		6.3	50.90
+50		5.2	52.00
1+00		4.3	52.90
0+53		3.6	53.60
0+51		3.1	54.10
0+40		3.1	54.10
0+26		3.3	53.90
0+00		6.3	50.90
SET TOM	12.84	66.01	4.03 53.17

5+64	8' LT	End 8" ^{STEEL} Conc Drive from School yard
4+88	WAT	Xing
+ &	JELLYTE	1/2" Palliative oil surfacing
Edge oiled road		4+60 GAS Xing
4+13	11' LT	WAT MET
3+56	9' LT	" "
3+51		} 6' LT Conc DRIVE
3+43		
3+14	8' LT	WAT MET
2+93		} 7' LT Conc DRIVEWAY
2+85		
2+68	7' LT	3' RT WAT MET
2+70	7' LT	WAT MET
2+31		} 4" Conc curb 10" high
1+80		
2+50	2" WAT	6' RT.
2+00	2" WAT	8' RT.
2+20		LT WAT MET
1+95	3' RT	" "
1+66	8' LT	" "
1+42		} 7' LT Conc DRIVEWAY
1+33		
1+06	8' LT	WAT MET
0+50	3" W.I.	WATER Xing
0+50	8' RT.	
Conc Mon & DENVER & Ingulf		

DENVER ST.
INGOLF TO MILTON
& PROFILE

4/8/52

48

66.01

CK BM

8.38 57.63 = 57.55

Elev MARK'D on pole.
NAIL IN stub pole 150' E NE Cor. Ingulf & DENVER

CK ID

0.67 65.34 = 65.35

Sx on Rim of M.H. FRIE & INGOLF

{ SK. 817
79. 34

Alley betwn 33rd + Felton
 from El Cajon to Orange
 (2) STK'S & GRADES FOR
 WATER METERS

West
Temp

27 May 52

	7.81	374.47	366.66	BM	BP	MW	Cor 33 rd + Orange
5+69W			370.8 370.3	0	0 ¹		
5+66E			371.2 370.5	0	0 ¹		
5+66W			370.9 370.4	0	0 ¹		
5+33W			371.9 371.1	0	0 ²		
4+81W			372.8 372.2	0	0 ¹		373.4
			373.1				373.7
4+76E			373.5 372.2	0	X ³	0 ²	375.5
4+59W			373.0 372.5	0	0 ¹		375.5
4+36W			373.1 372.7	0	0 ¹		375.8
							376.0
	5.28	378.30	1.45 373.02				378.8
							379.1
4+32E			373.7 372.7	0	1 ¹		
3+83E			374.3 372.8	0	1 ¹		
3+62W			373.4 372.9	0	0 ¹		
3+29			373.6 373.1	0	0 ¹		
3+23E			374.2 273.1	0	1 ¹		
3+01W			373.5 373.0	0	0 ¹		
3+04E			373.5 373.1	0	0 ¹		
2+25E			373.9 373.3	0	0 ¹		
2+09W			373.9 373.4	0	0 ¹		
			372.3				
2+05W			373.8 373.4	0	0 ¹		
1+86E			374.0 373.4	0	0 ¹		
1+72W			374.0 373.5	0	0 ¹		

Alley -
Cont'd

5/27/52

50

1+32 W	378.30	4.2	374.1	373.7	0 0 ⁴	
2+13 E		3.8	374.5	373.7	0 0 ⁸	
3+05 E		3.9	374.4	373.8	0 0 ⁶	
50+68 W		3.8	374.5	374.2	0 0 ³	
40+47 E		3.4	374.9	374.4	0 0 ⁵	0+00 South line of El Cajon Ave
4	1.03	373.87	5.46	372.94		
4			7.20	366.67 =	366.66	

Bangor St
Harbor View to Tolbot
Profile of Proposed WATER

West
Kemp

28 May 52 51

	T	Hi				
	0.45	257.86	257.41	BM SE Top Hyd Bangor + Harbor View		
0+00			4.70	253.24	0+00 AT North Prop Line Harbor View Dr of 8" BV	
0+09			5.38	252.54	End of curb 29' L Edge of Pavement End of curb Return 10' R	
0+50			9.4	248.54	0+33 Gas Xing	
	0.15	245.51	12.50	246.36		
1+00			1.1	244.44		
1+50			3.7	241.84		
1+94			10.3	235.24	1+66 Road barrosade	$\frac{11.2}{10} L$ $\frac{10.9}{10} R$
	0.71	233.68	12.54	232.97		
2+14			4.8	228.94		$\frac{5.4}{10} L$ $\frac{4.5}{10} R$
	0.79	221.83	12.64	221.04		$\frac{10.3}{10} L$ $\frac{10.6}{10} R$
	0.07	209.75	12.15	209.68		
2+50			10.2	199.64		
	0.05	197.22	12.58	197.17		
	0.59	185.19	12.62	184.60		
2+94			11.3	173.94	Top of Bank Road Out	$\frac{10.6}{10} L$ $\frac{11.5}{10} R$
	0.73	173.29	12.63	172.56		
	2.64	163.97	11.96	161.33		

BANGOR ST
(Contd.)

5/28/52

52

	+	H.	-	
	3.74	155.06 ✓	12.65	151.32 ✓
3+16.3	3.74	155.06	0.3	154.8 ✓
3+19			4.5	150.6 ✓
3+53.3			4.3	150.8 ✓
3+60			8.2	146.9 ✓
3+75			17.1	138.0
3+85			17.5	137.6
	12.87	158.52	9.41	145.65 ✓
	11.94	169.93	0.53	157.99
	12.65	182.04	0.54	169.39
	12.72	194.59	0.17	181.87
	12.39	206.50	0.49	194.11
	11.95	218.89	0.07	206.43
			2.35	216.03 = 216.09

Boat of Out.

edge Road

edge oil Talbot

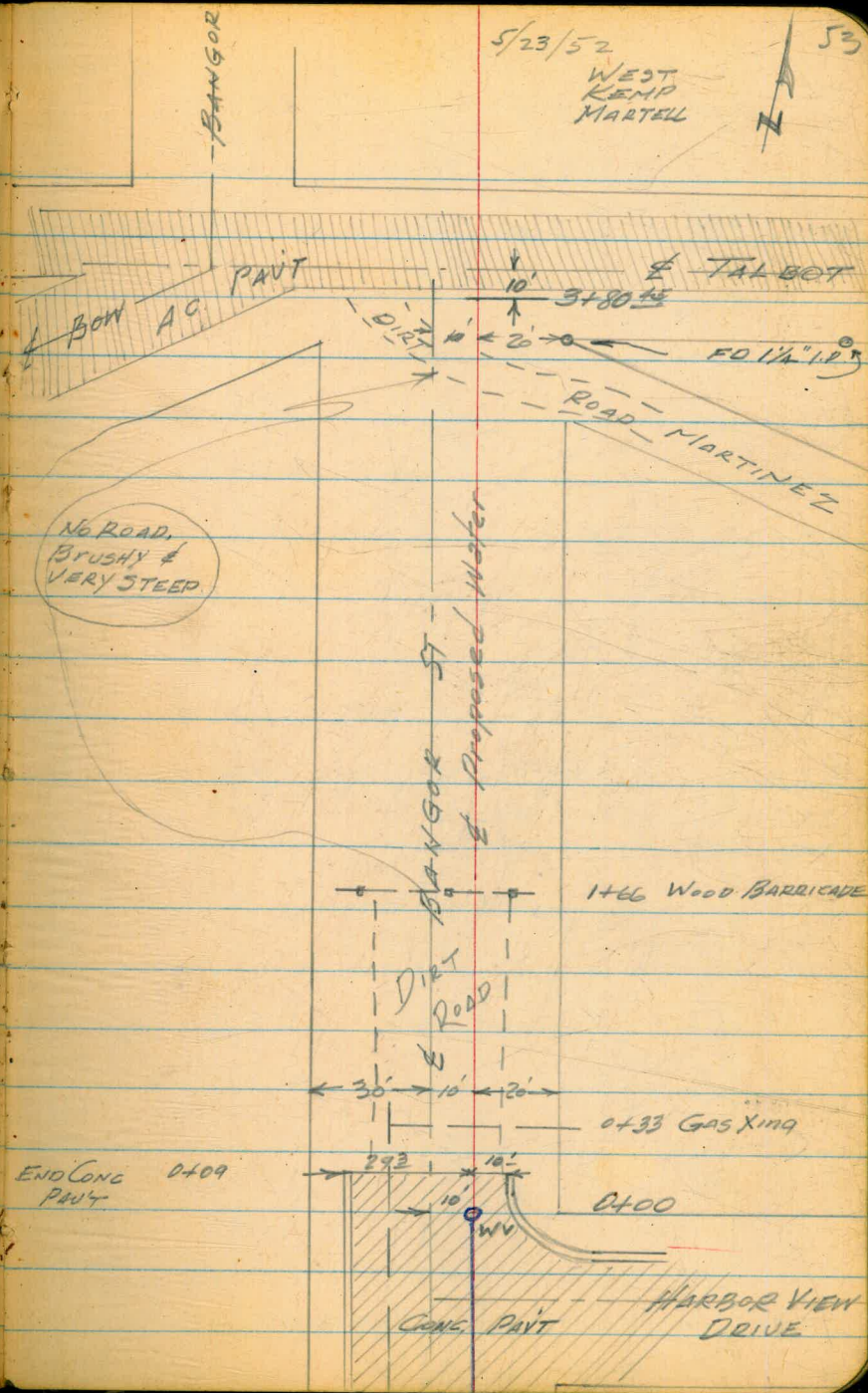
Turn on Pipe
5' IP over Talbot-Bangor
+ Hair

to NW cor
Talbot + Concord

BANGOR ST.
& PROPOSED WATER

3+8045 = 10' So. E TALBOT

0+00 = Nor. Prop Line Harbor View Dr

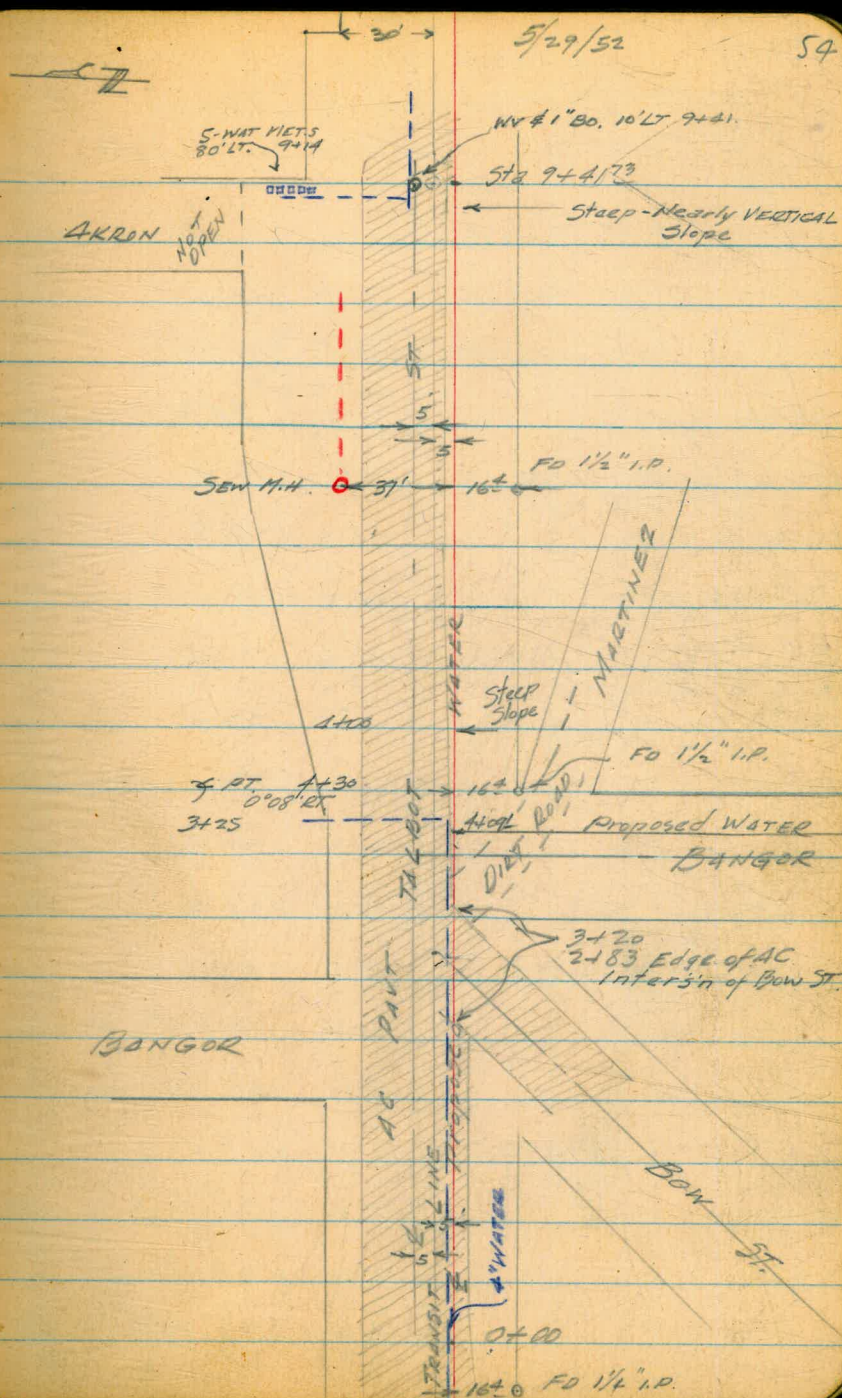


TALBOT ST.
E PROPOSED WATER

9+13.73 = E Line AKRON ST

4+30. = PT 0°08' RT

0+00 = 100' W E BANGOR ST.



TALBOT ST.

May 28, 1952

55

BEATTY
POWELL
VARONFAKIS

200' WEST OF BANGOR TO AKRON
& PROFILE PROPOSED WATER

BM	0.28	216.37		216.09
P	0.31	203.95	12.73	203.64
P	0.15	191.42	12.68	191.27
0+00			11.9	179.5
P	0.27	178.38	13.31	178.11
0+50			4.9	173.5
1+00			10.4	168.0
P	0.15	165.99	12.54	165.84
1+50			2.0	162.0
2+00			9.2	156.8
P	0.61	153.47	13.13	152.86
+50			2.1	151.4
3+00			6.3	147.2
+50			10.6	142.9
CK P			7.78	145.69 = 145.65
P	0.31	141.05	12.73	140.74
4+00			2.4	138.1
+30			3.2	137.9
+50			4.6	136.5

BP NW Cor TALBOT & CONCORD

ON AC PART
5' LT & PROPOSED WATER
TRANSIT. LINE

Edge AC 23' LT 11.4
5

Edge AC Part 3' RT

0+29 WAT MET 11' RT
0+31 GAS XING
Edge AC 4' RT

Edge AC 2' LT
HOB GAS XING
1+11 PATCH ON AC
MAYBE SEWER
1+20 WAT MET 20' RT
1+33 " " 21' RT
Exposed 4" WAT 2' RT
1+50 Edge AC on E

Edge of AC 1' & 32' LT 9.1
5

Edge of AC 1' LT 1.8
5

3' RT 4' WATER

Edge AC 3' RT
3+25 WAT XING &

on 1/2" HP. SE Cor Bangor

Edge AC 2' LT 2.6
5

2.9 5.1
5 3

Edge AC 2' LT 6.2 6.2
5 2.5

TALBOT ST
(Cont'd)

5/28/52

56

	141.05				
5+00		6.9	134.2	Edge AC. 2' LT	9.5 9.6 5 2
+50		9.0	132.1	" " 2.5' LT	12.8 12.5 5 3.5
P	0.52	128.77	12.80	128.25	
6+00		+1.5	130.3	Edge AC. 4' LT	3.2 3.2 5 1
+50		+0.4	129.2	6+28-37' LT SEWER MH.	6.7 6.2 5 2.5
7+00		3.7	125.1	Edge AC. 4' LT	9.1 9.2 5 2.5
+50		7.5	121.3		12.0 8.5 5 2.5
P	1.02	117.54	12.25	116.52	
8+00		0.9	116.6	Edge AC. 3.5' LT	3.5 0.9 5 1
+50		3.9	113.6		6.9 5
9+00		3.9	113.6	Edge AC. 4' LT	9.9 7.6 5 2
+41.73 +50					12.4 8.3 5 1
		13.4	104.1	Tap Corp Cock	
P	10.42	110.44	12.52	105.02	SW Cor sidewalk
	10.92	126.08	0.28	115.16	
	11.85	136.63	1.30	124.78	Turn on Sewer MH Cover
	11.91	148.04	0.50	136.13	
		2.35	145.69 = 145.65	Turn on 5" I.P.	

AKINS ST
67th ST TO CITY BDRY
& Proposed WATER

27+80⁵⁰

28+25

Intersection with City Bdry

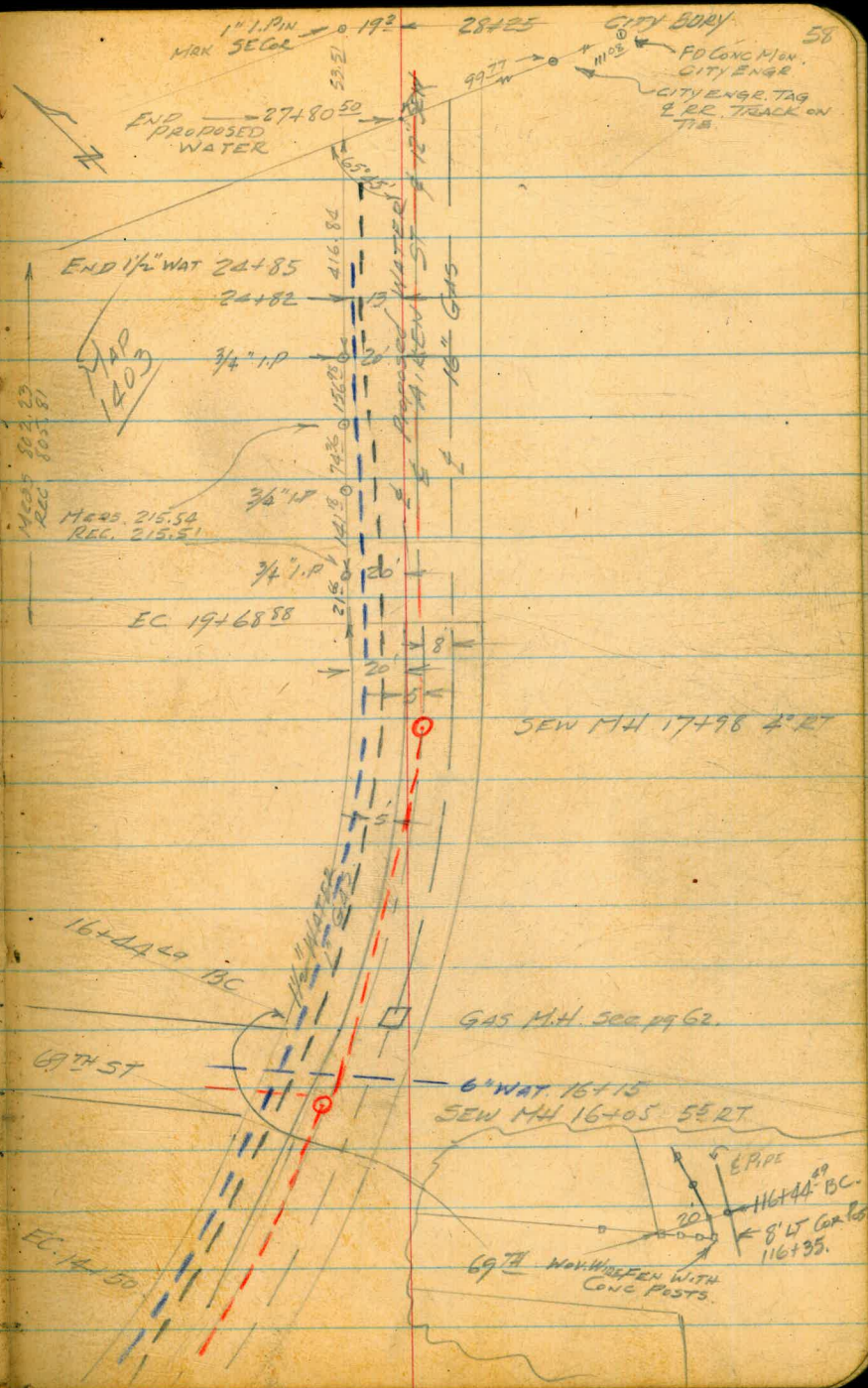
EC 19+68⁸⁸ EC

Δ 13°46'40" LT
R 1349.00
L 324.39

16+44⁴⁹ B.C.

(16+32⁴⁹ BC DEWILSON)

14+50 E.C. & X PT 2°17' LT



50 BANCROFT
 OCEAN VIEW TO WEBSTER
 & PROPOSED WATER

JUNE 24 1952 59
 WEST
 POWELL
 KEMP

(Cont'd on page 64)

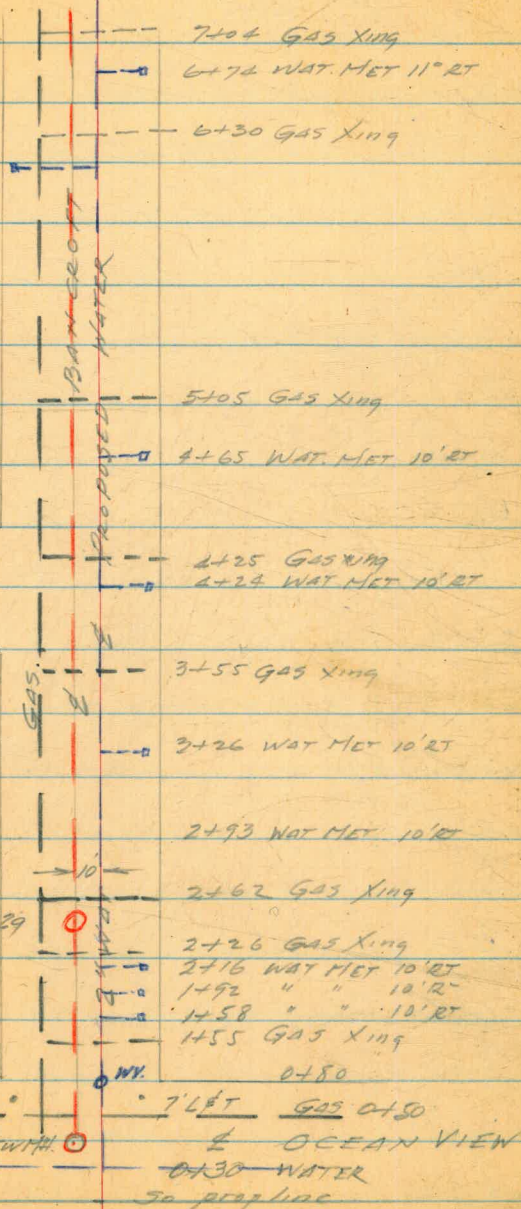
WAT MET 5+25 31' LT

FRANKLIN

curb to curb
 40

SEW M.H. 2429

0+00



0+00 50 Prop Line

AKINS ST.
67th ST. Easterly to City Bdry.
& PROFILE - PROPOSED WATER

JUNE 23, 1952 60.
BEATTY
FISH

BM.	3.12	233.61 230.61	230.49
P	12.41	240. Top 12.64 237.68 Rem 5.34	228. 225.27
0+00		14.1	226.6 ✓
+32		12.6	228.1 ✓
+50		12.6	228.1 ✓
1+00		12.4	228.3 ✓
+50		10.8	229.9 ✓
2+00		9.3	231.4 ✓
+50		8.1	232.6 ✓
3+00		6.9	233.8 ✓
+50		5.4	235.3 ✓
4+00		3.9	236.8 ✓
+50		2.8	237.9 ✓
5+00		1.6	239.1 ✓
+50	10.14	250. 247.57	0.25 240. 237.43
6+00		9.0	241.6 ✓
+50		7.7	242.9 ✓
7+00		6.2	244.4 ✓
+50		4.6	246.0 ✓

L&T. 7' offset line SW. Cor Imperial & Woodman
2" WAT X'S 0+08 G.V. 20' LT.
SEW M.H. 3' RT 0+32
NOTE: Top of 12" V.C. Sew
13 given instead of
14 vert.

13' LT to Drain Inlet 0+55
inlet & outlet filled up

13.0 17.1 18.0 20.2 21
15 20 24 28 35 & Ditch.

WAT. MET 13' LT 2+52

WAT. MET 12' LT 3+35

WAT. MET 14' LT 3+77

2" WAT. (exposed) 8' LT 5+80
WAT MET. 11' LT 6+39

WAT. MET. 11' LT 7+28

AKINS ST
E Profile Cont'd

6-23-52 61.

	250. 847.57		
8+00		29	247.7 ✓
+50		14	249.2 ✓
8+79		0.55	250.0 ✓
+95		0.20	250.4 ✓
P 11.18	261. 258.39	Top pipe 13.86 Rim 0.36	250. 247.21
9+00		10.9	250.5 ✓
+50		9.8	251.6 ✓
10+00		8.8	252.6 ✓
+50		6.8	254.6 ✓
11+00		5.5	255.9 ✓
+50	Rim 5.00 Top pipe 22.00	5.0	256.4 ✓
12+00		4.1	257.3 ✓
+50		3.8	257.6 ✓
13+00		3.9	257.5 ✓
+50		4.1	257.3 ✓
14+00		4.9	256.5 ✓
+50		6.2	255.2 ✓
15+00		7.4	254.0 ✓
+50		8.3	253.1 ✓
TD 5.30	258. 255.41	8.28	253. 250.11

WAT MET 12' LT. 8+19

8+705 22" Storm Dr. Xing.
Inlet 175 Top pipe 22 c. 27 outlet Top pipe

3" A.C. 8+72 2" GAS Xing

SEW M.H. 8+885 5' RT

6" WAT. Xing. 9+00

Top Pipe Inlet 10.5 12.8 outlet 22 25

9+045 22" STORM DRAIN Xing

9+78 35 LT MAIL BOX 98 98 6 2

WAT MET 9' LT 10+19 3.8 6.0 7.1 7.1

Mail Box 2' LT 10+32 6 2 1 8

WAT MET 8' LT 10+42 2.3 5.5

WAT MET 8' LT 11+06 6 1

SEW M.H. 10' RT 10+87

1.5 1.8 5.0
10 5 1

WAT MET 8' LT 11+95 11 3.8 7 2

12+19- 4' LT c/d'd Driveway 1.3 3.1

12+26 2' LT " 1.3 3.1

WAT MET 16' LT 12+55

" " 18' LT 13+26

" " 16' LT 13+72

" " 16' LT 14+41

STORM PIPE 45' LT 14+71

GUYANE 3' LT 14+96

MAIL BOX 2' LT 14+93

WAT MET 11' LT 14+98

LT. 14+50 & DRIVEWAY 10'

AKINS ST.
E Profile Cont'd

16+00	258. 255.41	4.9	253.5 ✓
	Rim 4.71 Top pipe 16.11		250.76 253.70
16+50		4.5	253.6 ✓
17+00		4.5	253.9 ✓
+50		4.3	254.1
18+00		4.3	254.1
	Rim 2.30 Top pipe 9.30		254.1
+50		3.9	254.5
19+00		3.1	255.3
+50		2.3	256.1
+66.14 EC		2.2	256.2
20+00		1.6	256.8
TP	9.03 260. 263.31	1.13	257. 254.28
+50		8.6	257.7
21+00		7.9	258.4
+50		7.0	259.3
22+00		5.9	260.4
+50		5.4	260.9
23+00		4.5	261.8

16+50 Begin AC 6' RT 15' RT
2"
SEW. M.H. 55 RT 16+05
16+15 6" WAT Xing
16+50²⁰ 19+62 10' RT FENCE
16+73 20" PEPPER TREE 55 RT
16+80 18" " " 6 RT
16+85 3' RT WAT MET
16+27-10 RT
9.50
4.82 Top Conc }
10 " } GAS
4.81 Top Conc }
10 " } M.H.
16+35 25
16" GAS
10.80 RT

WAT MET 12' LT 18+02
SEW. M.H. 4' RT 17+98
17+96 10' LT }
17+96 20' LT }

WAT MET 11.5' LT 21+07 3' LT Edge 21+89
21+83 3' RT Edge AC } 1 1/2" AC
22+19 - 3' RT Edge D.C.
22+16 3' LT Edge AC

WAT MET 19' LT 22+23
23+30 35 RT 12' RT
3' LT AC 23+35 - 155 RT.

WAT MET 18.5' LT 23+41 3' LT A.C. 23+46 155 RT AC
" " 19' LT 23+91

AKINS ST.
& Profile Cont'd

6-23-52

63

23+50	263.31 266.	3.4	262.9
24+00		2.6	263.7
+50		2.1	264.2
25+00		1.9	264.4
+50		1.4	264.9
HP	6.37 270. 267.46	2.22	264. 261.09
26+00		5.3	265.2
+50		4.1	266.4
27+00		4.7	265.8
+25		4.8	265.7
28+00		3.8	266.7
28+25		2.7	267.8
(Depth - Fin) (6-24-52)		Top Pipe 8.95 Rim 2.43	268.03
SET T.O.M.	2.80 271. 268.88	1.44	269.02 266.02
HP	0.30 262. 259.77	9.41	262.47 259.47
HP ex HP	8.43 262. 259.08	9.12	253.65 253. 250.65 = 250.70
HP ex HP	1.73 251. 248.89	11.92	250.16 250.21 247.16 = 247.21
HP	0.15 240.54 237.54	11.50	240.39 237.39
HP	5.73 233.99 231.99	12.28	228.26 228.27 225.26 = 225.27
OK BM		3.51	230.48 = 230.49

3-WAT MET 14.5 LT $\left\{ \begin{array}{l} 24+09 \\ 24+11 \\ 24+13 \end{array} \right.$
1 1/2" WAT 13' LT 24+05
2-WAT MET 13' LT 24+82
WAT MET 10' LT 24+85

24+00 1/2" AC
24+35 2" 6" AC
25+00 6' RT AC

	2.0	1.3	2.4
	10	6	2
MAIL BOX 7' LT 26+50	0.2	1.2	1.0
	10	2	2
MAIL BOX 1' LT 26+04	2.4		4.8
	10		2
MAIL BOX 3.5' LT 26+86	4.1		2.8
	10		5
	3.2		
	10		

1" AC
27+10 5' RT Edge AC
END AC

5' - 14.3' LT 28+31.5
SEW. Gauge House
14.3' LT 28+35.5
SEW. M.H. 6' RT 28+41
2750 beginning of Conc. Venturi-flowline of Sew.
1" I.P. IN 19' LT 28+25 - M.H. 5' Pop. Cor

SEW. M.H. Rim 16+05 67th ST
SEW. M.H. Rim 8+88.5 68th ST

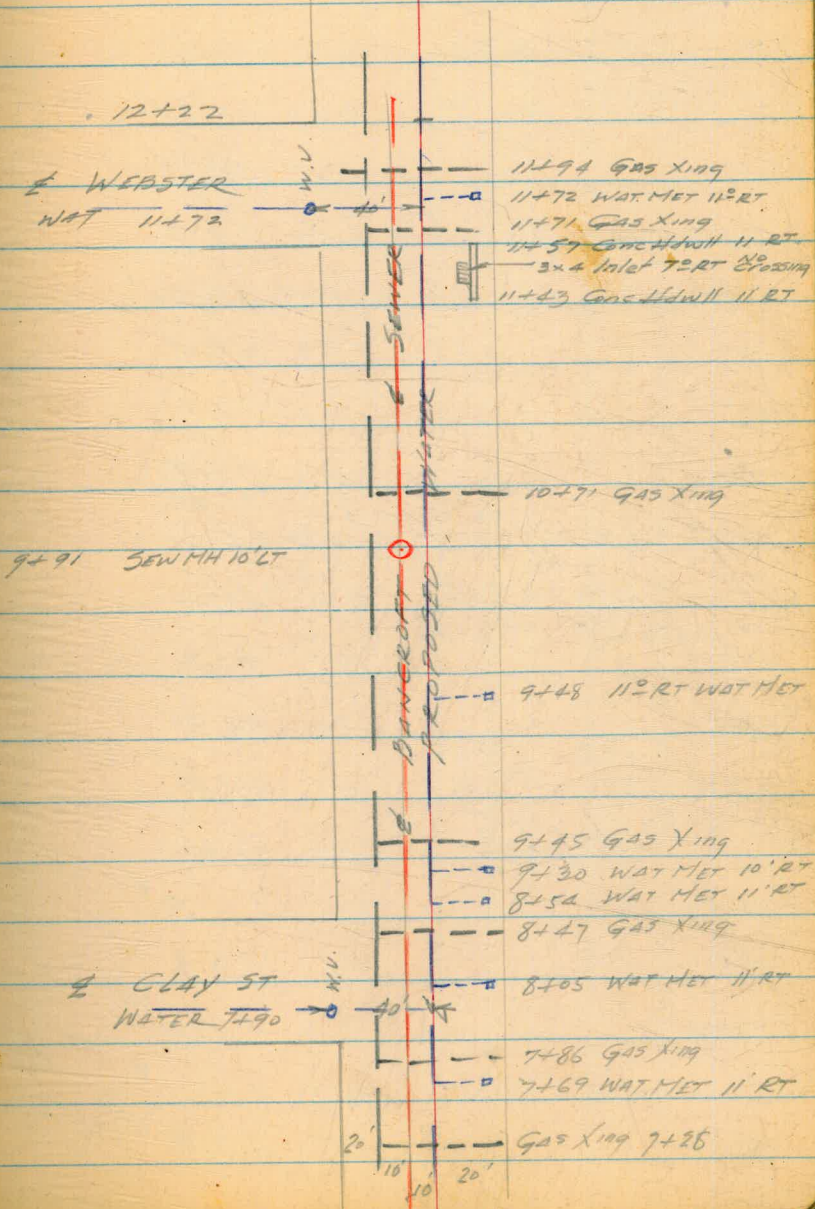
SEW. M.H. Rim 0+32. 67th ST

7' LT SW Cor. Woodson & Imperial

JUNE 24 '52 64

BANCROFT ST
OCEANVIEW TO WEBSTER
& Proposed WATER

12+22 Not prop line Webster



50 BANCROFT ST
 E Profile - Proposed Water
 Oceanview to Webster

JUNE 26 1952 65
 WEST
 Powell
 Kemp

B.M.	13.04	30.26		17.22 ✓
P	13.03	42.67	0.62	29.64 ✓
0+30			10.7	32.0 ✓
+40	SEW Mt.	Inu. 17.80		24.81 ✓
		Rim 10.36		32.3 ✓
+80			10.17	32.50 ✓
1+00			9.7	33.4 ✓
+50			6.0	36.7 ✓
2+00			3.0	39.7 ✓
		Inu. 8.80		33.81 ✓
+29	SEW Mt.	Rim 0.19		42.5 ✓
P	12.83	55.49	0.01	42.66 ✓
+50			12.5	43.0 ✓
3+00			9.0	46.5 ✓
+50			4.1	51.4 ✓
P	13.02	68.09	0.44	55.05 ✓
4+00			11.6	56.5 ✓
+50			9.1	59.0 ✓
5+00			4.9	63.2 ✓
P	10.29	78.26	0.12	67.97 ✓
+50			9.5	68.8 ✓

Top Ft. 33rd & Oceanview SE. Cor

Edge Conc Pavt (north prop line Oceanview)

0+80	32.50	
	5.85	
	38.35	
	2.12	
	36.23	Top Hydt
31.93-32.0		
	38.35	38.35
	6.11	606
	32.24	37.29 W

6400	78.26		5.0	73.3 [✓]
+50			2.6	75.7 [✓]
7400			3.1	75.2 [✓]
+50			6.1	72.2 [✓]
8400			8.6	69.7 [✓]
+50			10.8	67.5 [✓]
TP	3.36	68.68	12.94	65.32
9400			4.3	64.4 [✓]
+50			6.6	62.1 [✓]
+91 SEW M+H			Inu 12.41	56.29
			Rm 6.31	62.4
10400			7.4	61.3 [✓]
+50			8.2	60.5 [✓]
11400			9.2	59.5 [✓]
+50			10.1	58.6 [✓]
12400			9.0	59.7
+22			8.3	60.4
TP	12.02	80.64	0.06	68.62
TP	0.32	77.09	3.87	76.77
TP	0.19	65.12	12.16	64.93
TP	2.39	57.14	10.37	54.75
ck. BM			847	48.67 = 48.61

Not prop line Webster

(31 ST. E. P. ?
Oceanview ?)

7-7-52

67.

CK LEVELS

P (0+80)	5.85	38.35	32.50
CK BM		2.12	36.23 = 36.23
CK W-Rim Sew Mt		6.06	32.29 = 32.31

Top Hydt ~~Pancroft~~ & Oceanview

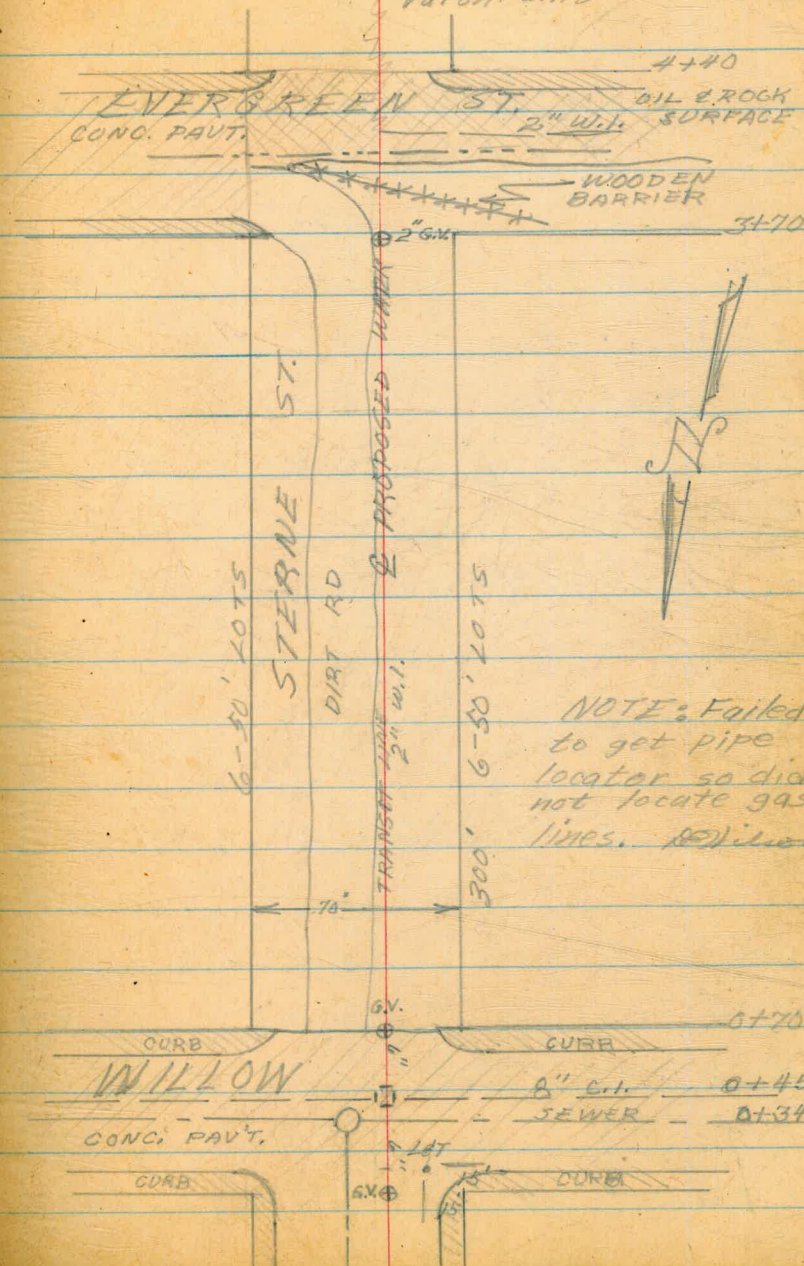
Sterne St.
Willow to Evergreen
& Proposed Water

- 4+40 South Prop. Line Evergreen
- 4+31 S. edge of AC
- 4+15 Existing TP of 2" w.l.
- 4+04 N. edge of AC
- 3+97 1 1/4" Gas
- 3+80 Wooden Barrier
- 3+78 2" a.v.

- 0+70 South Prop. Line Willow
- 0+45 8" WATER
- 0+34 SEWER
- 0+00 North Prop. Line Willow

Aug. 26th 68.

Wilson
Martel
Varonfakis



STERNE ST.
 Q PROFILE - PROPOSED WATER
 WILLOW TO EVERGREEN

	+	HI	-	ELEV.
	0.24	194.14		193.902
TP	1.68	184.10	11.723	182.42
0+00			12.60	171.5
			RIM 11.40	172.7
0+34	Sewer MH		INVERT 16.60	167.5
0+50			11.30	172.8
0+70	Top of GV		12.40	171.7
0+78			11.00	173.1
1+00			7.10	177.0
TP	12.36	188.39	8.07	176.03
1+25			7.40	180.99
1+50			3.50	184.9
1+75			.50	187.9
TP	7.36	195.58	.17	188.22
2+00			5.50	190.1
2+50			4.60	190.98
3+00			8.40	187.2
TP	.42	183.69	12.31	183.27
3+50			4.10	179.6
3+78	Top of GV		8.40	175.29

Wilson
 Martell
 Varonakis

Aug. 27, 1952

69.

L.B.T.
 B.M. N.W. Curb Tennyson & Willow
 N. curb on Willow

6" GV

6" GV

Rock in Sterne

Rock in Sterne

Rock in Sterne

3" GV

Continued

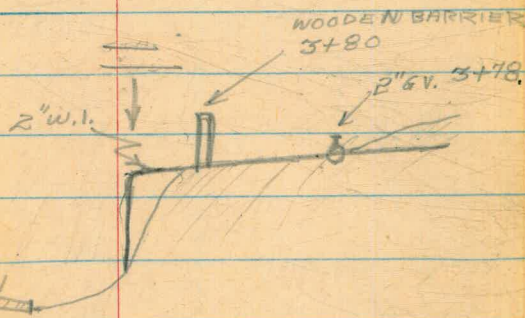
STERNE
E Profile of Proposed Water
Willow to Evergreen

Wilson
Martell
Varoufakis

Aug. 27, 1952

70.

	+	183.69	-		
3+90			10.40	173.3	
TP	6.21	177.96	11.94	171.75	Top of 2" WATER Riser
4+00			11.10	166.9	
4+04			12.00	165.96	N. edge of Paving
4+31			11.70	166.3	S. edge of Paving
4+40			13.30	164.7	
TP	10.90	187.48	1.38	176.58	SW Curb
TP	12.52	198.34	1.06	186.42	NE Curb
CK BM			5.06	193.88 =	193.902
					NW Curb Tennyson & Willow



Montclair St
Kalmia to Juniper
Profile

West
Martell
Varonfakis

16 Oct 52

11.

	1.29	296.41		295.12	BM BP. SE cor. Boundary + Maple
	0.59	286.15	10.85	285.56	
	1.18	275.06	12.27	273.88	
			5.56	269.50	BP NE curb Kalmia + Montclair
0+00			6.3	268.8	North prop line Kalmia
+28				267.8 & 262.0	
			7.21	+5.9 To Flow Line	Top east edge sewer manhole 10°R
+50			8.06	267.0	
			12.7	262.4 Flow Line	23° RT to storm drain Grate 10°
0+51			12.2	262.9 Flow Line	9° Lt to storm drain Grate 10°
+59°					edge of oil
+672			8.43	266.6	Top 8" av. cover
1+00			9.1	266.0	
+50			11.6	263.5	on curb Drive
2+00			12.5	262.6	
	2.65	264.70	12.99	262.07	
+50			2.6	262.1	
3+00			4.1	260.6	
+50			6.0	258.5	
				259.1 & 247.2	
+50			5.59	+11.8 To Flow	Top east edge sewer MH 10° RT
4+00			8.5	256.2	

54.6
77
070

7.2
102R
10°
102R
10°
102R

4750	264.72	11.6	253.1
149	253.56	12.65	252.07
5700		8.4	245.2
6.21	247.27	12.50	241.06
+50		10.4	236.9
+65		11.81	235.58
+76 ¹⁶		16.2	232.1
11.36	258.19	0.44	246.83
10.70	268.60	0.29	257.90
11.40	279.80	0.20	268.40
12.49	292.01	0.28	279.52
8.91	299.72	1.20	290.81
		4.63	295.09 = 295.10 = -0.03 OK

Top east edge Sewer MH
Juniper st. Pl

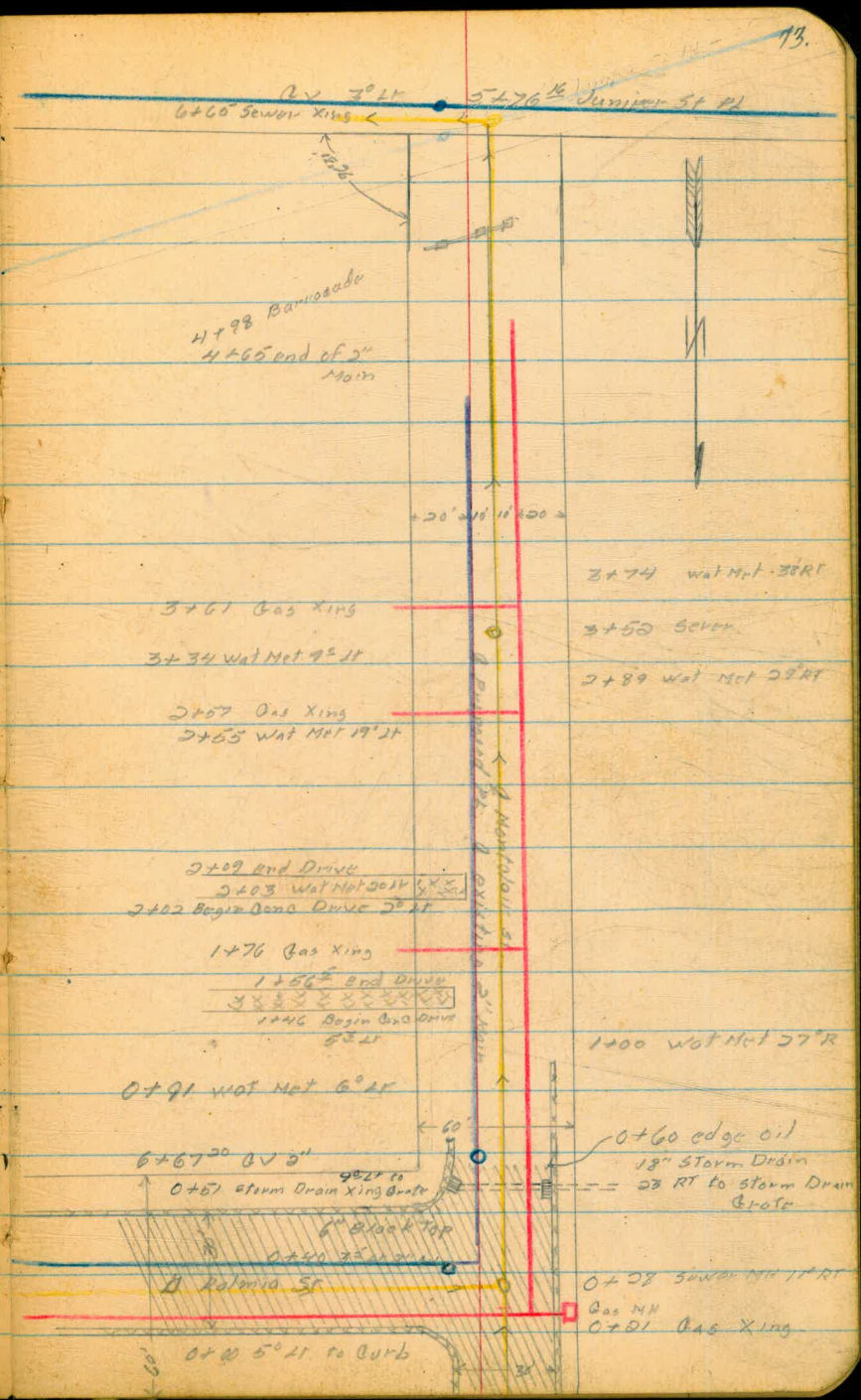
14960
3329
9631

5+63 ¹⁶/₁₆

North Prop Line Juniper

0+00

North Prop Line Kalmia



Vancouver St
 & Proposed Pl.

From End 6" AC at B.C. To Juniper

West
 martell
 Varonakis

Oct 17 52

74

	8.42	277.92		269.50	BP NE cor Kalmia & Montclair
TD	3.67	371.02	10.57	267.35	Top Fire Hyd
0+00 BC			6.2	264.8	
+50			6.4	264.6	
1+00			5.6	265.4	
+34			4.90	266.1 @ 259.0 +7.1 To Flow Line	Top west edge sewer MH 2 ³ 11
+50			5.3	265.7	
2+00			5.9	265.1	
2+11 ⁴ EC			6.0	265.0	267.35 - 2.35 ----- 265.00
+50			6.0	265.0	3.30 ----- 266.14
3+00			5.3	265.7	
3+01 ⁴ BC			5.3	265.7	
+25			5.0	266.0	
+75 ⁴			4.6	266.4	
4+07	1.79	368.10	4.71	266.3 @ 258.1 366.31	Top west edge sewer MH 2 ³ 11
4+25			1.7	266.4	
+72 ⁴ EC			2.8	265.3	
5+00			3.9	264.2	
+50			5.1	263.0	

6+00	368.10	5.9	262.2
+50		6.2	261.9
7+00		6.0	262.1
			262.6 @ 254.7
7+01		5.51	+7.9 To Flow line
		5.9	around elev
			262.2
+27		10.26	257.8
4.25	370.76	1.59	366.51
11.21	378.07	3.90	366.86
		8.55	369.52 = 369.50

Top east edge sewer MH 10° RT

Top stem 6" GV

Top stem 6" GV

0400

Bo curve Vancouver

H 245 by eng. 100. 00.

 Δ 48 23' chords 0750

0750 00

R 250' 1100

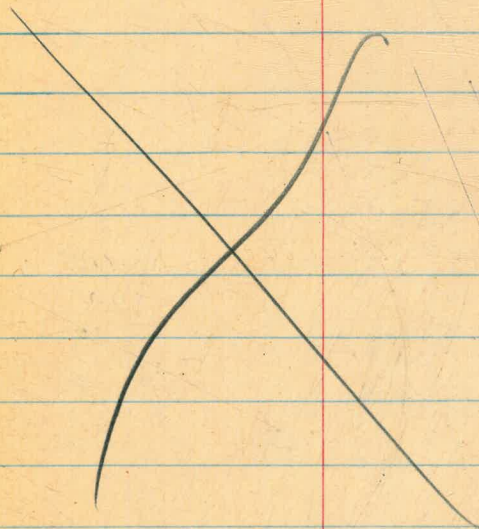
T = 110.30 1100

L = 211.11 2100

1134 chord 700 11

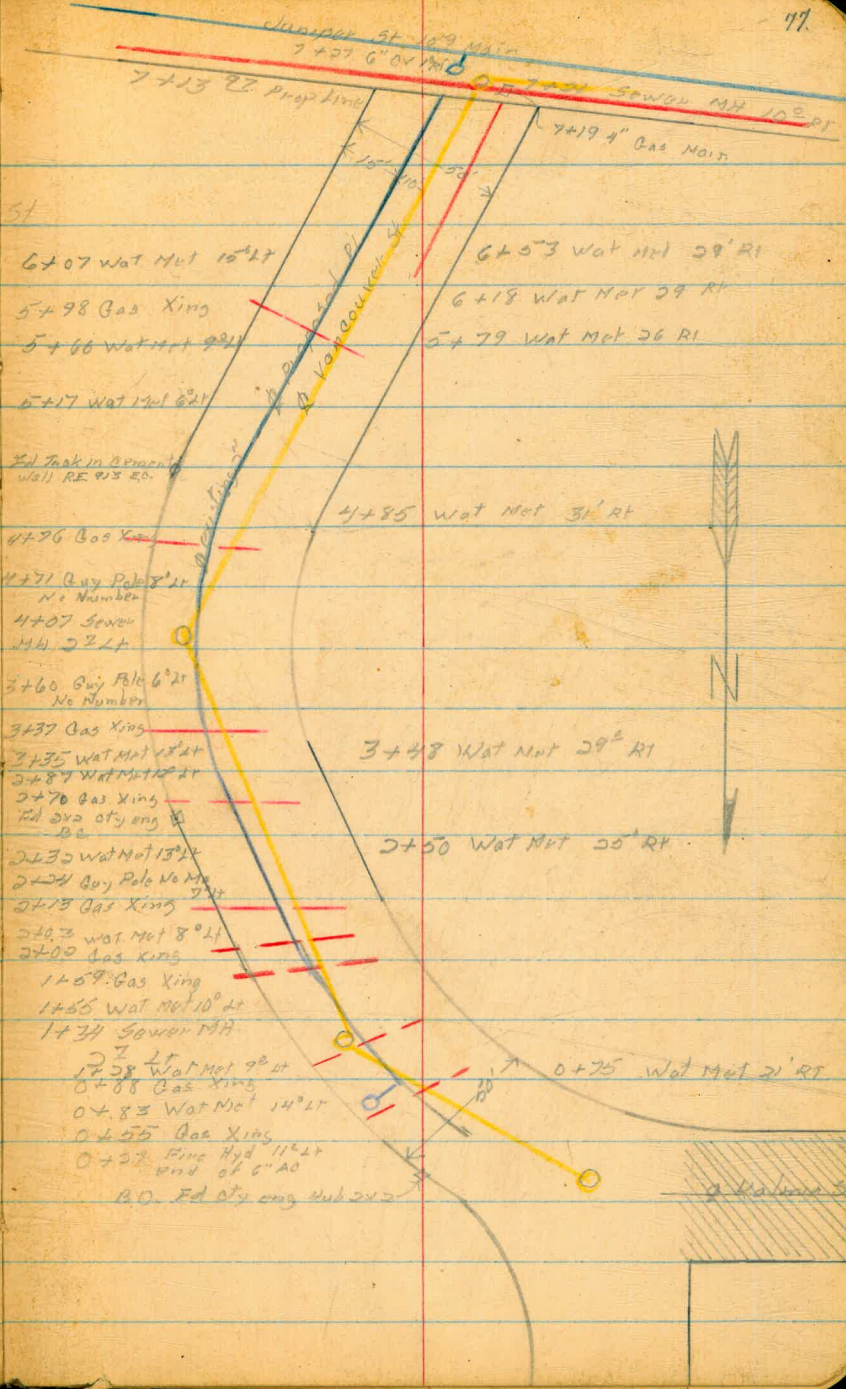
2111" EC

Voicd
See Page 77



H 245 by eng. 100. 00.

7+13 92 North Prop Line Juniper St



4+72 44 EC

$\Delta = 50^{\circ} 24'$
 $R = 195'$
 $L = 171.53$
7.7147

Chords
3+35
3+36
4+25
4+72 44

3+01 44 BC

2+11 44 EC

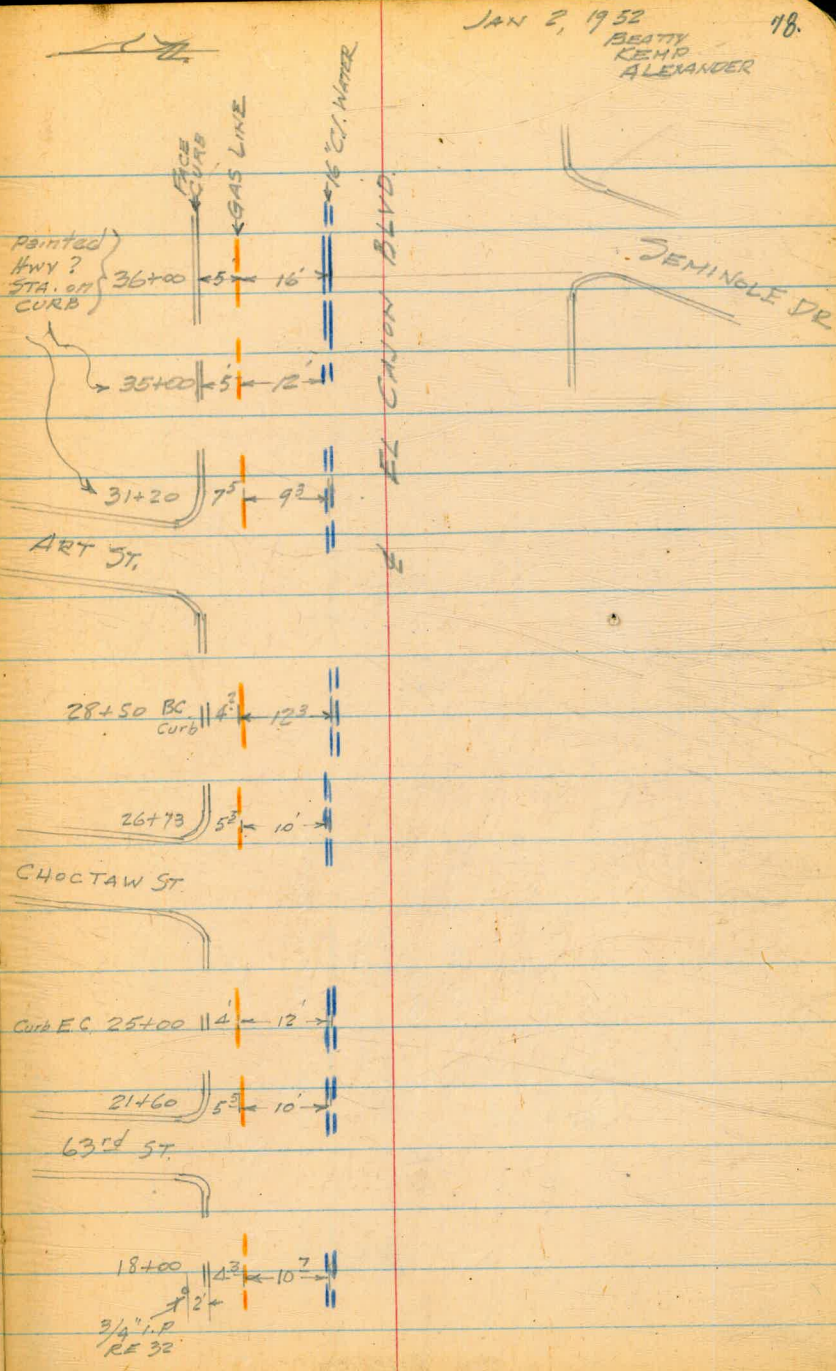
$\Delta 48^{\circ} 23'$
 $R = 250'$
T 112.30
L = 91.11

chords
0+56
1+00
1+50
2+00

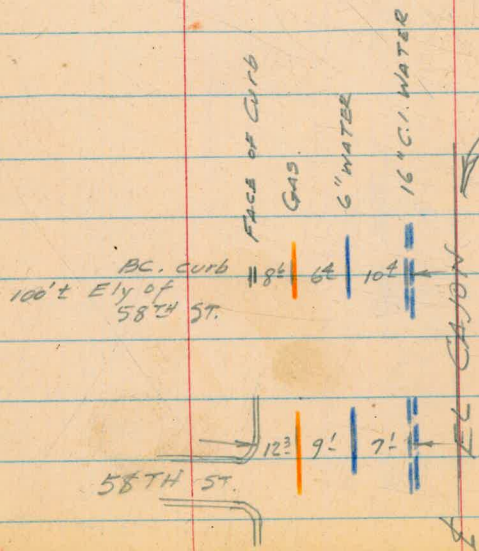
0+00

BC of Curve Vancouver

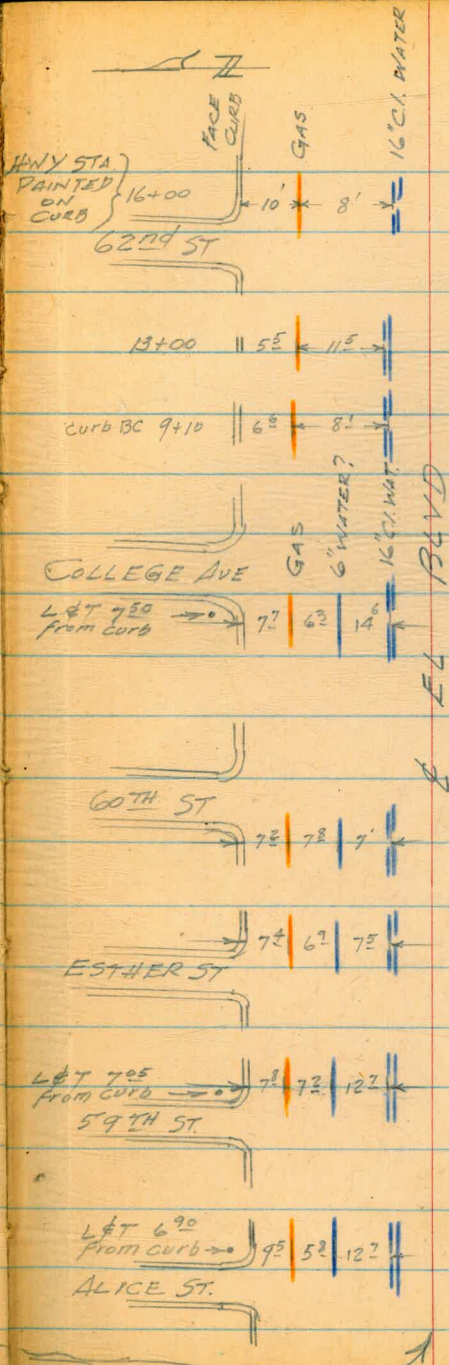
LOCATION OF 16" C.I. WATER
 EL CAJON BLVD
 58TH TO SEMINOLE
 (PIPE FINDER LOCATION)



EL CAJON BLVD
(CONT'D)



HWY STA
PAINTED
ON CURB } 16+00
62ND ST



WIGHTMAN ST
52nd St West
stks for 6" AC slab

12.47	327.79		315.32
10.32	338.03	0.08	327.71
0+00		5.6	332.4 328.4
0+37.2		7.1	330.9 328.5
0.02	327.58	10.47	327.56
		12.26	315.32 =

West
Williams
Varonakis
Kellhofer

2/9/56

80.

B11 NWBP 52nd + University

0.10

3139.0

0.12

132

0.34

4459

West Prop Line 52nd St

315.32

1580-64

28.06
Top curb

29.07
Top curb

757

808

676

626

66.94
94.44
202.56

2+97.0
0.5

2+96.5
25.0

2+71.50
68.94

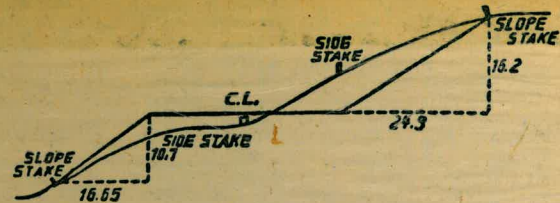
2+02.56
52.56

1.9488
1718.87
882
5368
7938
3387
3528
7990
1050
2390

526
1.95
2630
4734
526
102.570
19488
50
974400

1+50 - 1° 42' 35"
1° 37' 26"
1+00 - 3° 20' 01"
3° 37' 26"
+50 - 4° 37' 26"
4° 37' 26"
0+00 - 6° 34' 53"

1225
3625
60250



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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