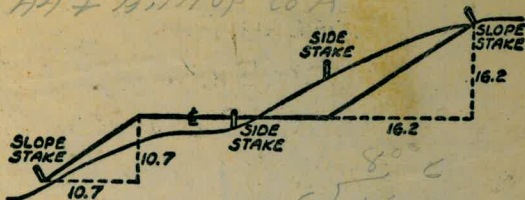


W 812 B

H4 + Hilltop Co A



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

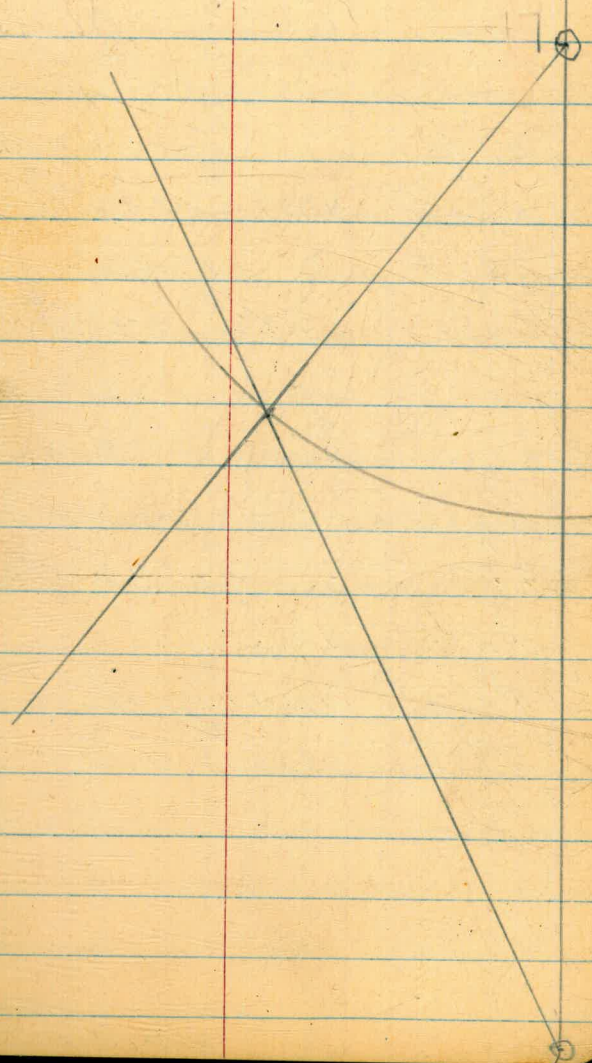
Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

MICROFILMED

JAN 16 1965

All notes to p. 30 have been copied - West 8-11-54
 Bench Levels - Barrett 30-39 a.m.



1168.1		30'	4398.3	1617.1		30'	5484.9	220
1174.8		40'	4612.2	1625.7		40'	5500.9	221
		50'	4626.0	1634.4		50'	5517.0	222
1181.6		78°	4639.8	1643.0		88°	5533.1	223
1188.4	25° C.	10'	4653.6	1651.7	25° C.	10'	5549.2	224
1195.2	T	20'	4667.4	1660.5	T	20'	5565.4	225
1202.0	1.28	30'	4681.3	1669.2	1.53	30'	5581.6	226
1208.9	E	40'	4695.2	1678.1	E	40'	5597.8	228
1215.8	.403	50'	4709.2	1686.9	.558	50'	5614.2	229
1222.7		79°	4723.2	1695.8		89°	5630.5	230
1229.7		10'	4737.2	1704.7		10'	5646.9	231
1236.7		20'	4751.2	1713.7		20'	5663.4	232
1243.7		30'	4765.3	1722.7		30'	5679.9	233
1250.8		40'	4779.4	1731.7		40'	5696.4	234
1257.9	30° C.	50'	4793.6	1740.8	30° C.	50'	5713.0	236
1265.0	T	80°	4807.7	1749.9	T	80°	5729.7	237

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

~ 387.34

Roof Shots

University Hts Tanks

Henry's BM

1	4.115	391.455	387.34			
1 1/2	5.095					
2	5.111	5.115	5.110	5.108	5.110	5.099
2 1/2	5.013	5.040	5.075	5.045	5.051	5.058
3	4.990		5.038	5.041	5.035	5.018
3 1/2	4.932	4.997	4.988	4.985	4.981	4.996
4	4.963	✓	4.955	4.965	✓	✓
4 1/2	4.885	4.919	4.906	4.917	4.913	✓
5				4.885	4.875	✓
5 1/2	4.805	4.855	4.850	4.856	4.847	✓
6	4.822	4.840	4.900	4.843	4.830	✓
6 1/2	4.755	4.800	4.782	4.862	4.792	4.808
7	4.730	4.762	4.754			
7 1/2	4.763	4.754	4.763	4.771	4.771	4.757
8	4.782	4.768	4.770	4.781	4.748	4.758

-4112

Aug 1971

3

D	D-2	E	E-2
5.075	5.088	5.063	5.082
	D-2	E	E-2
5.035	5.038	5.015	5.048
D		E	
5.004	5.008	4.988	5.001
		E	
4.963	✓	4.965	4.961
		E	
✓	4.938	4.944	4.941
4.893	4.895	4.895	4.881
D	D	E	E-2
4.874	✓	4.862	4.850
		E	
4.820	4.855	4.785	4.820
4.801	4.814	4.775	4.800

$\times 66^\circ$
 $\frac{1320}{2}$
 $\frac{1320}{1440}$

61st St
 Q Profile

17 Sept 52 5

	0.43	243.12		242.69
0+00		4.5		
+10		5.88		
+10 ²		6.51	13.0 to Flow Line	
0+30		6.92		
0+45		8.79		
+50		7.4		
+60		8.03		
1+00		12.2		
	0.44	231.54	12.02	231.10
+50		4.3		
2+00		7.3		
+50		9.8		
3+00		12.4		
	2.70	233.70	11.54	230.00 231.00
+30		6.3		
4+00		9.5		
+50		12.6		
	1.57	222.46	12.61	210.09 221.09

SW by Brooklyn Fergus
 North Prop Line Brooklyn
 Top Curb
 Gutter
 Top east edge sewer MH
 Top stem 6" QV
 edge oil

$\frac{10.7}{10.25}$
 $\frac{1.8}{10.25}$
 $\frac{6.5}{10.25}$
 $\frac{9.6}{10.25}$
 $\frac{11.3}{10.25}$

$\frac{8.0}{10}$ $\frac{83}{80}$ $\frac{9.4}{26}$
 $\frac{1.4}{10}$

5+00		222.66	4.6	
+50			6.6	
6+00			8.3	
+50			9.9	
7+00			12.0	
	1.39	212.00	12.05	210.61
+50			3.2	
8+00			4.7	
+50			6.2	
9+00			7.4	
+50			8.6	
+88			11.6	
	1.51	211.20	12.95	209.71
10+00			2.4	
+15			3.9	
+20			6.1	
+25			7.2	
+50			12.0	
9	2.27	200.80	12.69	198.53
11+00			4.8	
+50			5.2	

$\frac{4.1}{10.1}$
 $\frac{5.2}{10.1}$
 $\frac{8.3}{10.1}$

$\frac{10}{10.1}$
 $\frac{10}{10.1}$

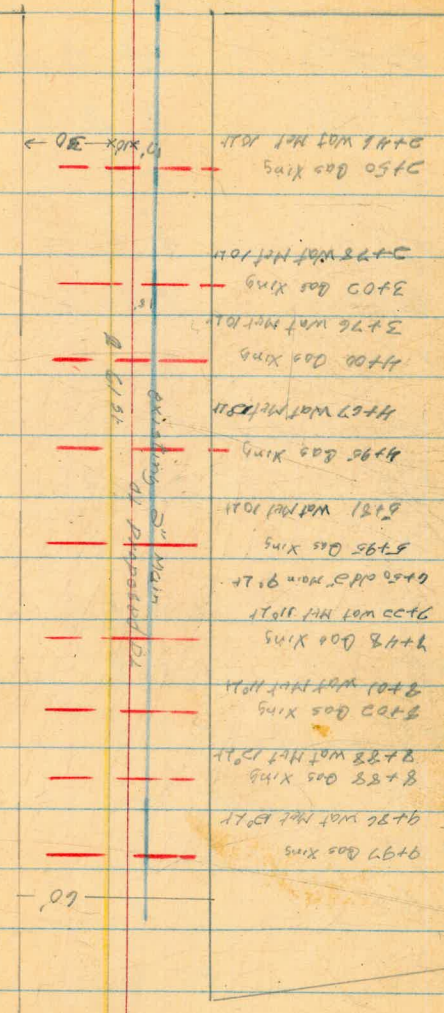
$\frac{2.4}{10.1}$
 $\frac{3}{10.1}$

$\frac{9.2}{15.1}$ $\frac{8.8}{10.1}$ $\frac{8.1}{10.1}$
 $\frac{14.9}{10.1}$ $\frac{11.9}{10.1}$

$\frac{5.1}{10.1}$

11+63	200.80	5.9		
+75		6.8		Creek Bank
+81		10.9		Creek Bott
12+00		10.7		
+82		9.7		
+38		7.02	18.2 To Flow Line	Top east edge Sewer MH
+50		6.1		
13+00		2.6		
+04 ^s		1.96		Top North RR rail.
+09 ^s		1.99		" South " "
8.12	206.67	2.25	198.55	
+19		7.0		
+25		5.1		
+50		5.6		
+55		5.8		
+56		6.9		
+63		6.80		edge oil North line Imperial
+83		6.80		" " South " "
14+00		6.8		
+08		3.4		
14+13 ²⁰		2.7		to South prop line Imperial
		5.15	201.50	Top Sewer MH Fergus + Atkins

D+43 DV 19.11
D+50 Sewer MD 112 RT



D+38 Sewer MD 111 100 RT



D+50 WAT 19.11
D+43 WAT 19.11
D+38 WAT 19.11

North Prop Line Brooklyn

D+40

162nd Imperial to Brooklyn

13

Station

0+50	+0.5	
1+00	+3.0	
0+99	+0.1	9.0 R# IRC Drain
1+50	+1.0	
2+00	+0.6	
2+50	+0.2	
4+00	+0.4	
4+50	+0.3	
5+00	+0.4	
6+00	-0.2	
6+50	-0.3	
7+00	-0.5	
7+50	-0.7	
8+50	+0.5	
9+00	+0.4	
9+50	+0.4	
10+00	+0.8	
11+00	+0.2	
11+50	+0.7	

12+00

+0.7

12+50

+0.2

14

15

Fergus St
Akins + Imperial

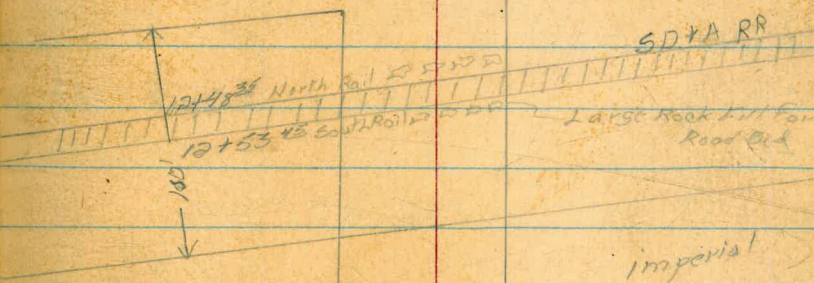
STA.	B.S.	M.I.	F.S.	ELEV.
11+75	5.47	185.75 190.60		179.98 185.13
12+14			11.7	173.75
+33			3.5	181.95
+48			2.69	182.76
+50			3.0	182.45
+53			2.68	182.77
12+70			8.0	177.45
12+91			7.2	178.25
13+00			3.0	182.45
+08			3.79	181.66
+41			3.79	181.66
+50			3.9	181.55
+60			4.1	181.35
12+60	56	South Prop Line	547	185.13 = 185.13 179.98

21218
50.52
146156

12+01
1+61.56
13+62.56

TBM Top Sewer W.H. Akins + Fergus

South side creek
Top Bank
Top North Rail
Top South Rail
Bottom Bank South side
Top Bank
edge oil North side imperial
edge oil South " " South Line Akins



18

Stakes for 12" Main
Orange St
To 57th Place

11.35	396.18		384.83		BM Top curb 11 th St	See FB 787 P. 24
7.96	402.97	1.17	395.01			
0+00		0.0	403.0	389.4	C 13 ⁶	
0+50		5.5	397.5	386.2	C 11 ³	
1+00		12.7	390.3	382.8	C 7 ⁵	391.22
126	391.22	13.01	389.96			638 394.84
+25		5.0	386.2	381.2	C 5 ²	
+50		6.5	384.7	380.4	C 4 ³	
2+00		6.3	384.9	380.5	C 4 ⁴	
+50		6.2	385.0	380.6	C 4 ⁴	
3+00		6.3	384.9	380.7	C 4 ²	
+25		6.1	385.1	380.1	C 5 ⁰	
+50		8.5	382.9	378.0	C 4 ³	
4+75		13.1	378.1	372.0	C 6 ¹	
0.37	379.48	12.11	379.11			
4+00		7.7	371.8	366.0	C 5 ⁸	
+25		12.9	366.6	360.2	C 6 ⁴	
+50	0.70	367.37	12.81	366.67		
+50		5.3	362.1	356.8	C 5 ³	

6 Oct 52

West
Martell
Varonakis

19

4+75	367.37	8.8	358.6	353.2	05 4
5+00		8.3	359.1	353.6	05 5
		6.1	361.3	357.0	04 3
		3.0	364.0	359.5	04 2
12.28	379.02	0.63	366.74		
10.68	388.94	0.76	378.26		
		4.08	384.86	384.83	

64th St Profile
Akins to Imperial

	3.03	219.15		216.12
-0+37			5.3	213.8
-0+45			6.4	212.8
-0+47 ⁹⁸ 2			6.4	212.8
-0+51 ³			5.56	213.6
-0+56 ⁸			5.55	213.6
-0+70			6.2	213.0
-0+80			1.5	217.7
-0+86			1.5	217.9
-0+99 ²³	45.72	224.25	0.60	218.53
			5.2	219.1
			4.4	219.9
			3.78	220.4
			3.2	221.1
			8.14	216.11 = 216.12

BM Top FH Betw Stark + 64 South Carb
Imperial

Top of North Rail

" " South Rail

Bottom of Bank

edge oil by feed store

Gutter South Side

Top Carb

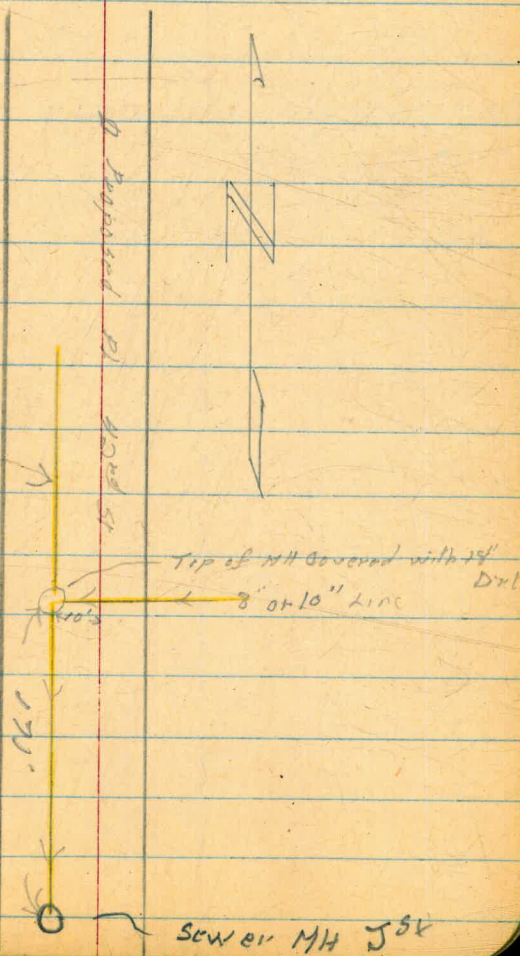
Prop Line on Side walk

+ 4.60

1.64 + 6.8 To Floor Line

West
Martel
Xaroufakis

24 Nov 58

BM Top of Sewer M.H. @ 40th & J StTop South Edge Sewer MH 171'
South of Sewer MH @ J StThis part of line
appears Dead

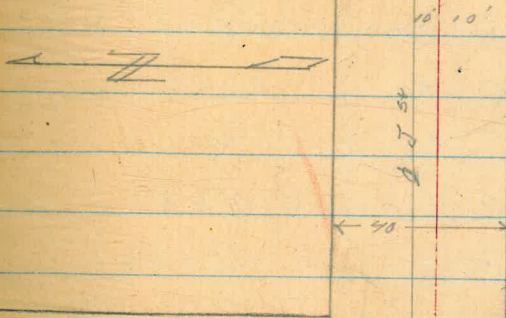
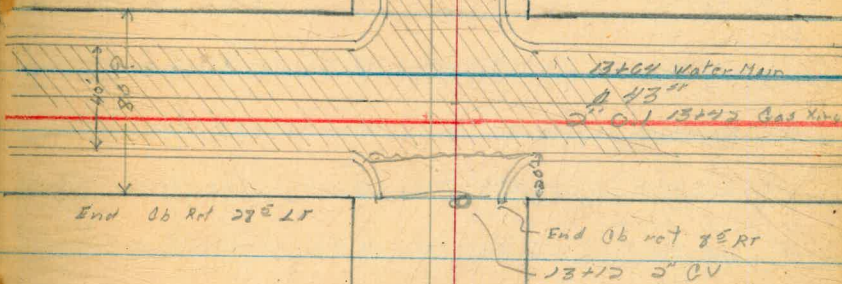
	8.09	136.55	128.46
13+25		4.5	132.0
+33		4.20	132.4
+50		3.92	132.6
+75		4.18	132.4
14+00		3.77	132.8
	8.09	136.55 = 136.55	

West
Marcell
Yarinfakis

24 Nov 50

Br Top east edge
Sewer MH. & J + Dunks

edge oil



D. Demaby St

BENCH BARRETT LEVELS - CHECK TO FAIRCHILD

STA	+	HI	-	EL.
B.M.	0.30	1616.30 ✓		1616.00
T.P.	0.04	1608.00 ✓	8.34	1607.96 ✓
T.P.	5.51	1602.41 ✓	11.10	1596.90 ✓
T.P.	2.72	1597.05 ✓	8.08	1594.33 ✓
T.P.	11.21	1607.71 ✓	0.55	1596.50 ✓
T.P.	11.96	1619.62 ✓	0.05	1607.66 ✓
T.P.	12.45	1631.81 ✓	0.26	1619.36 ✓
T.P.	12.99	1644.75 ✓	0.05	1631.76 ✓
T.P.	12.46	1656.76 ✓	0.45	1644.30 ✓
T.P.	12.51	1669.23 ✓	0.04	1656.72 ✓
T.P.	12.24	1681.17 ✓	0.30	1668.93 ✓
T.P.	12.62	1693.36	0.43	1680.74 ✓
T.P.	12.76	1706.03 ✓	0.09	1693.27 ✓
T.P.	12.82	1718.75 ✓	0.10	1705.93
T.P.	12.62	1731.29 ✓	0.08	1718.67 ✓
T.P.	12.67	1743.52 ✓	0.44	1730.85 ✓
T.P.	13.08	1755.79	0.81	1742.71 ✓
T.P.	12.52	1768.25 ✓	0.06	1755.73 ✓
T.P.	12.37	1780.57	0.05	1768.20 ✓

WILLIAMS X
MIKE KELLHOFER

8/5/54

TOP PIPE #15 SOUTH

R.H. NAIL 8/6/54

BARRETT

STA	+	1790.57 HI	-	EL
T.P.	12.88	1793.28 ✓	0.17	1780.40
T.P.	12.55	1805.38 ✓	0.45	1792.83 ✓
T.P.	12.77	1818.07	0.08	1805.30 ✓
T.P.	12.19	1829.71	0.55	1817.52
T.P.	12.80	1842.36 ✓	0.15	1829.56
T.P.	11.70	1853.20 ✓	0.80	1841.56
T.P.	12.48	1864.92	0.82	1852.44
T.P.	9.23	1869.64	4.51	1860.41
T.P.	11.66	1872.52	8.78	1860.86
T.P.	11.68	1883.75	0.45	1872.07
T.P.	12.24	1895.08 ✓	0.91	1882.84
T.P.	13.02	1906.89	1.21	1893.87
T.P.	12.58	1919.04 ✓	0.43	1906.46
T.P.	12.84	1931.81 ✓	0.07	1918.97 ✓
T.P.	5.17	1930.96 ✓	6.02	1925.79 ✓
T.P.	0.70	1924.82	6.84	1924.12 ✓
T.P.	0.29	1912.32	12.79	1912.03
T.P.	0.28	1900.57	12.03	1900.29
T.P.	0.15	1887.71	13.01	1887.56

MIKE

8/6/54

RK. HOG BACK 1000'± - WEST MIKE

8/9/54

STA	+	HI	-	EL
		1887.71		
T.P.	3.43	1884.96	6.18	1881.53
T.P.	2.65	1885.75	1.86	1883.10
T.P.	9.70	1882.99	12.46	1873.29
T.B.M.			1.38	1881.61 = 1880.79 ←
T.B.M.	1.33	1882.94		1881.61
T.P.	12.56	1895.42	0.08	1882.86
T.P.	11.04	1905.87	0.59	1894.83
T.P.	0.12	1893.69	12.30	1893.57
T.P.	0.29	1881.52	12.46	1881.23
T.P.	0.98	1869.68	12.82	1868.70
T.P.	0.71	1858.90	11.49	1858.19
T.P.	0.24	1846.56	12.58	1846.32
T.P.	0.62	1835.17	12.01	1834.55
T.P.	2.51	1824.82	12.86	1822.31
T.P.	1.08	1813.04	12.86	1811.96
T.P.	1.07	1801.98	12.13	1800.91
T.P.	0.95	1790.14		1789.19
		1800.14	12.79	1799.19
T.P.	0.46	1779.56		1779.10
		1789.56	11.04	1789.10
T.P.	1.17	1768.20		1767.03
		1778.20	12.53	1777.03

8/9/54

← FAIRCHILD # 554



STA	+	HI	-	EL
		1768.20		
		1778.20		
T.P.	4.47	1760.04		1755.57
		1770.04 12.63		1765.57
T.P.	0.52	1748.24		1747.72
		1758.24 12.32		1757.72
T.P.	0.13	1735.83		1735.70
		1745.83 12.54		1745.70
T.P.	0.48	1724.05		1723.57
		1734.05 12.26		1733.57
T.P.	0.78	1711.97		1711.19
		1721.97 12.86		1721.19
T.P.	0.14	1699.29		1699.15
		1709.29 12.82		1709.15
T.P.	0.11	1686.79		1686.68
		1696.79 12.61		1696.68
T.P.	0.32	1675.10		1674.78
		1685.10 12.01		1684.78
T.P.	0.30	1663.33		1663.03
		1673.33 12.07		1673.03
T.P.	0.67	1651.03		1650.36
		1661.03 12.97		1660.36
T.P.	0.65	1639.58		1638.93
		1649.58 12.10		1648.93
T.P.	0.47	1628.25		1627.78
		1638.25 11.80		1637.78
T.P.	1.44	1616.68		1615.24
		1626.68 13.01		1625.24
T.P.	9.35	1618.15		1608.80
		1628.35 7.88		1618.80
T.P.	7.80	1618.47		1610.67
		1628.67 7.48		1620.87
T.P.	4.61	1612.88		1608.27
		1623.08 10.20		1618.47
T.P.	11.48	1613.41		1601.93
		1623.61 10.95		1612.13
T.P.	1.59	1602.50		1600.91
		1612.70 12.50		1611.11
T.P.	8.82	1599.96		1591.14
		1610.16 11.36		1601.34

LARGE ROCK SOUTH JIM. IN DRAW

8/10/54

←

STA.	+	HI	-	FL
		1599.96		
		1610.16		
T.P.	3.15	1599.49	3.62	1596.34
T.P.	4.50	1609.69	8.52	1606.54
T.P.		1595.47		1590.97
T.P.	2.52	1605.67	3.33	1601.17
T.P.		1594.66		1592.14
T.P.	11.29	1604.86	8.21	1602.34
T.P.		1597.74		1586.45
T.P.	8.39	1607.94	5.37	1596.65
T.P.		1600.76		1592.37
T.P.	0.29	1610.96	0.11	1602.57
T.P.		1600.94		1600.65
T.P.	6.12	1611.14	11.39	1610.85
T.P.		1595.67		1589.55
T.P.		1605.87		1599.75
T.P.		1607.40		1595.05
T.P.	12.35	1617.60	0.62	1605.25
T.P.		1617.86		1606.27
T.P.	11.59	1628.06	1.13	1616.47
CHECK				1615.80 =
B.M.			2.06	1626.00 =

MIKE

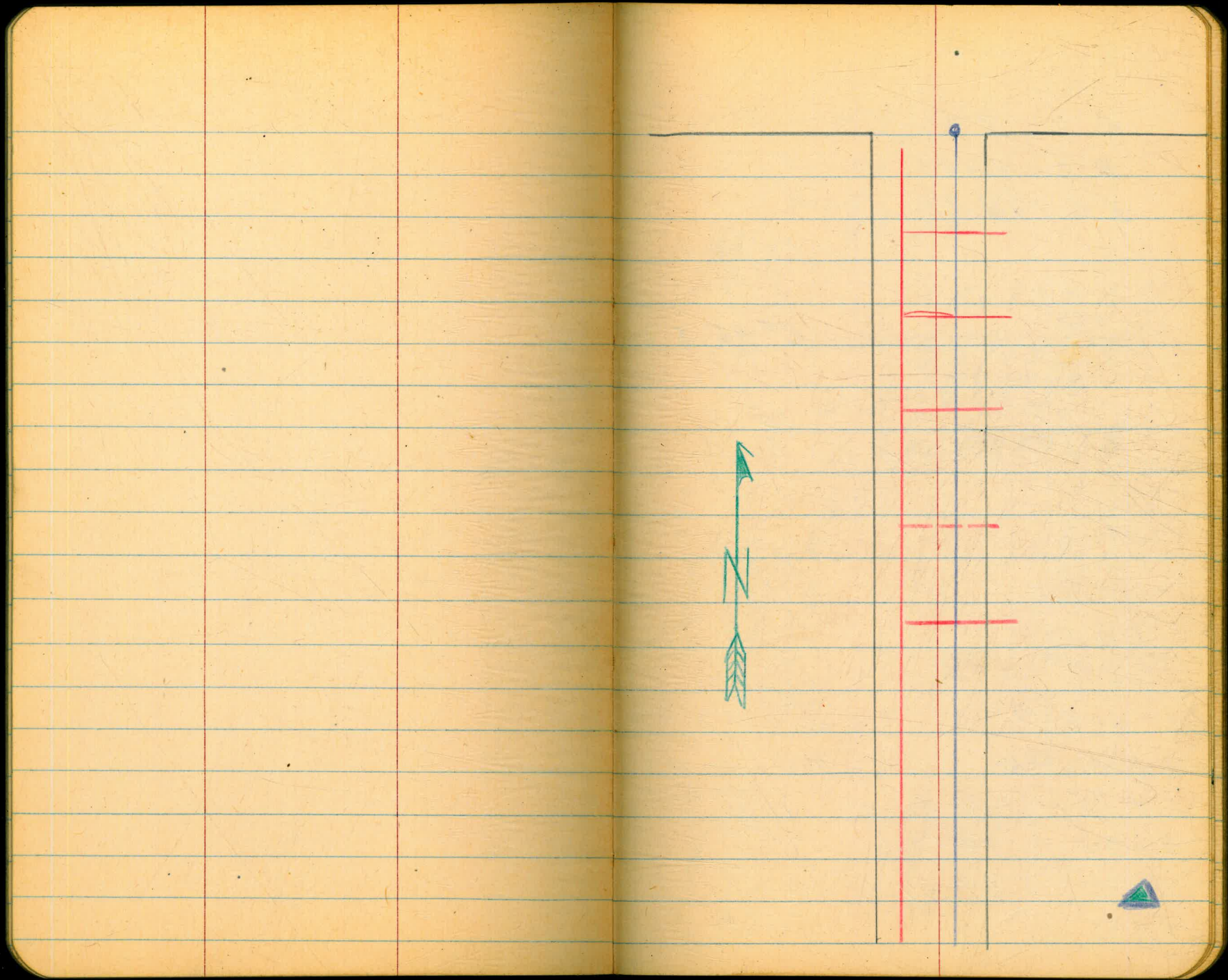
1616.00

1616.00

TOP PIPE # 15 SOUTH

42

43



51st St

$\Delta = 89^\circ 54$
 $R = 124'$
 $L = 194.60$

1385
3

41.65

13'85 1'

9

5°46.3 25

1+83 BC

15 41

3 55.4

2+00

3°55.4

19°36.4

5 46.3

2+25

25°23.7

5 46.3

2+50

31°10.0

5 46.3

2+75

36°56.3

6 46.3

3+00

42°42.6

5 85.4

EC +06.60

44°46.3

50 29

3+50 23 BC

$R = 6129$
67.59

+75

11°32.3

119°22.3

11 41.3

4+00

23°13.0

23°13.6

11 41.3

4+25

34°54.9

34°54.9

5 08.5

4+36 EC

40°03.4

13.85
96
8110
13465
132760

2°027
6)13276
120
2

N 89° 51' E
S 0 03 W
89 54

39
85
124

1.5693419
124

62773676
31396838
15693419

1945983956

1 68
126.60

4405
28

5085

13.85

17

4695

1385

5°46.3
5 46.3
11°32.6
3 55.4
15°27.0

14 183

1541.0115

6.8

60)23546)3°55.4
180

55.4

13.85
68

11880

8310

1+83

1 26.60

3.0960

6 60

45 63

50 23

60)94280)10.54
600

341

Δ 45° 50' RT

$\frac{1}{2} \Delta = 22^\circ 50'$

R = 97.85 T 41.4

L = 78.33

T = 41.4

20+76.80

21+00

+25

+50

+54

22+03

7° 01.2

14 20 0

21 38.8

22° 55.8

CV end of line

Roofing nail

on Tangent of PI

Roofing nail on Tangent line

sta 23+12.93

hoping

hoping

1680
1405

1589
1405
184

7 012

7 188

14 200

7 18.8

21 38.8

1 16

22 55.8

24.94 chord

710.2

7451.20

420

.7853982

0151262

.8005244

20+76

7833

5433

21+50

53 45

22 0 3 45

1 0.9 48

23 12 93

$$\Delta = 70^{\circ} 31' 50'' \quad L = 302.79$$

$$\frac{1}{2} \Delta = 35^{\circ} 15' 55'' \quad L = 203.11$$

$$R = 165 \quad 18 + 70 = 88 \text{ BO}$$

$$19 + 00 \quad 4^{\circ} 42.2 \quad 4 \ 42$$

$$+ 25 \quad 9^{\circ} 02.2 \quad 4 \ 20$$

$$+ 50 \quad 13^{\circ} 22.2 \quad 4 \ 20$$

$$+ 75 \quad 17^{\circ} 42.2 \quad 4 \ 20$$

$$20 + 00 \quad 22^{\circ} 02.2 \quad 4 \ 20$$

$$+ 25 \text{ EC} \quad 26^{\circ} 22.2 \quad 4 \ 20$$

$$+ 50 \quad 30^{\circ} 43 \quad 4 \ 20$$

$$+ 76 \quad 35^{\circ} 16 \quad 4 \ 20$$

$$35 \ 16 \quad 4 \ 20$$

$$30 \ 42$$

$$4 \ 20$$

$$35 \ 02.2$$

$$3 \ 38.6$$

$$38 \ 40.8$$

$$30 \ 43.2$$

$$4 \ 30.6$$

$$35 \ 13.8$$

$$18 \ 72.89$$

$$20 \ 3.11$$

$$20 \ 86.00$$

$$35 \ 15$$

$$2 \ 70 \ 31 \ 50$$

$$10.44 \text{ Per. H. H. } 12 \ 70.66$$

$$6 \ 56.4$$

$$18 \ 72.89 \quad 6 \ 56.25 \quad 3^{\circ} 38.6$$

$$27.11$$

$$60 \ 18.61$$

$$18$$

$$4^{\circ} 20.25 \quad 59 \ 50 \text{ E}$$

$$508.25 \quad 70 \ 31 \ 50$$

$$120$$

$$1.2217305$$

$$.0090175$$

$$.0002424$$

$$1.2309904$$

$$60 \ 82.21 \quad 4^{\circ} 42.2$$

$$24$$

$$242$$

$$142.34$$

$$83.19$$

$$227.73$$

$$18 \ 72.89$$

$$20 \ 3.10$$

$$20 \ 95.99$$

$$70^{\circ} 31' 50'' \quad 38 \ 44 \ 07$$

$$6 \ 56 \ 25 \quad 2 \ 717 \ 28 \ 15$$

$$77 \ 28 \ 15$$

$$260 \ 4^{\circ} 20$$

$$20$$

$$120$$

$$1.3439035$$

$$.4786922$$

$$.0000727$$

$$1.8326684$$

$$70 \ 42.2$$

$$72 \ 82.21$$

$$24$$

$$242$$

$$24$$

110.35
4993082 $\sqrt{58.1000000}$
4993082
8169180
4993082
317609900
14979246
26305540

116.5

Δ 11026
 $\frac{1}{2}$ 55 13
 $R = 477.48 + 92.02$
 68.80

~~12.90
 10 + 75 79 44'
 11 + 00 22 44
 + 25 57 44
 + 50 52 44
 + 54¹² 55 11
 52 44
 22 44
 55 11~~

$T = 58.1$ $L = 107.77$
 $\Delta = 53.04'$
 $\frac{1}{2} \Delta = 26.52$
 $R = 116.36$
 12.90
 10 + 75 3° 10' ✓
 11 + 00 9° 19' ✓
 + 25 15° 28' ✓
 + 50 21 37 ✓ 21 41
 11 + 69.87 26 32 4 06
 12 + 10 45 sta to ⑩ of 50 of
 old Curve

.9250245
 0011636
 .9261881

36
 12.9
 68.81
 1.4388114
 1376
 6281
 6282
 794
 628
 514
 14.8
 20
 1296.02456
 20924
 306

477.48
 477.48
 12.9
 128
 1032
 51.6
 129
 1.43881141
 68.8000000
 57537156
 124754400
 115104912
 96494880

412
 412
 106210
 107.77
 116987
 412
 36
 2472
 1236
 14732
 127
 227.3

$\frac{1}{2} \Delta$ 55 13 60
 Δ 110 26 120
 $L=157.18$ $R=80$
 $10+6210$
 1290

$10+75$	$4^{\circ} 37.4$	437.4
$10+00$	$13^{\circ} 34.9$	857.5
$+25$	$22^{\circ} 32.4$	3349
$+50$	$31^{\circ} 29.9$	857.5
$+75$	$40^{\circ} 27.4$	22334
$12+00$	$49^{\circ} 24.9$	857.5
$+1628$	$55^{\circ} 13$	40274
		857.5
		49249
		550
		55149

68.80 T
 $\frac{1}{2} \Delta$

~~1.9274253
 47.74
 77097012
 134919771
 134919771
 77097012
 92015283822~~

$3^{\circ} 46.8$

221.88
 18
 218
 218
 18

3218
 710
 10518
 710
 19018
 710
 25718
 710
 32218
 710
 39318
 710
 46418
 710
 53518

21.5
 12.9
 19.35
 4.30
 21.5
 27735
 24
 187
 10

170
 12.9
 1548
 344
 170
 591.88
 591.88
 0075631
 1.9274253
 80
 154940840

192.74

1.9274253
 8
 154940840

$10+6210$
 15418
 151628

192.74

1628
 21.5
 8140
 3256
 3256
 $5^{\circ} 50$
 $4^{\circ} 37.4$
 350020
 30
 300

$\Delta 75'41$
 $\frac{1}{2} 37'50.30$
 $\Sigma = 220.44$

$\Delta 128'45'44$
 $\frac{1}{2} \Delta 66'22'52$
 $R = 166.98$

~~$L = 386.68$~~

8 + 50

1° 26'

+ 75

5° 43.5

9 + 00

10° 01.0

+ 25

14° 18.5

+ 50

18° 36.0

+ 75

22° 53.5

10 + 00

27° 11.0

+ 25

31° 28.5

+ 50

35° 46.0

+ 62.10²⁰

37° 50.5

\checkmark POC
POC -

~~11 + 00~~

~~44° 21~~

~~+ 50~~

~~52 36~~

12 + 00

61 31

EC + 28³⁴

66 22' 52

61 31
4 50
44 21

90 00

156 22 52

193.34

2

386.68

10.3

28.34

8.34

10.3

413

28.340

509

289902

824

20

60 / 859 031 1° 20.9

49

60

1259

1° 26

1200

593

1.3089969

0119204

1.3209233

166.98

105473864

8+41.66

105673864

2 20 44

79255398

10+62 10 EC

79255398

13209233

8+41.66

3 86.68

12 28 34 EC

8+41.66

3 75.03

12 16 69

Δ 82° 41' 30" $\angle = 317.66$
 $\frac{1}{2}\Delta$ 41° 20' 45"
 $R = 220.1$

5+50	3° 23'
+75	6° 38'
6+00	9° 53'
+25	13° 08'
+50	16° 23'
+75	19° 38'
7+00	22° 53'
+25	26° 08'
+50	29° 23'
+75	32° 38'
8+00	35° 53'
+25	39° 08'
8+41.66	41° 20' 45"

41° 20' 45"
 90

 1312045

07.8
 16.66

 16'9
 468
 468
 78

 60 7129948)216.6
 12

 99
 60
 394
 360
 344
 50
 41.66

 8'34
 39 08
 2 16.6

 41 24.6

$\Delta = 63\ 27\ 40$
 $\frac{3}{4}\Delta = 31\ 43\ 53$
 $R = 270$
 $L = 272.06$

N 20 32 W
36 55 40
63 27 40

1.0995574

0078540

0002182

1.0076296

270

705396750

20152592

272,059,9920

Δ 128° 45' 44"
 $\frac{1}{2}\Delta = 64$ 22 52
 $R = 166.88$ $L = 375.03$

9+00	0° 22.9
+25	4° 40.4
+50	8° 57.9
+75	13° 15.4
10+00	17° 32.9
+25	21° 50.4
+50	26° 07.9
+75	30° 25.4
11+00	34° 42.9
+25	39° 00.4
+50	43° 17.9
+75	47° 35.4
12+00	51° 52.9
+25	56° 10.4
+50	60 27.9
12+ 72.01	64 23 4

66 47 2

N 14 18 30 W
 N 36 55 46 E
51° 14' 16"

N 89 59 30 W

2,094,395.1	
1,396,263	
0,130,900	
2,133	
<u>5,247,324.7</u>	
166.88	22,01
	<u>10.3</u>
	66.03
	<u>22,010.35.1</u>
	60) 22,67,031
179785976180	
179785976	307
134839482	30
134839482	
<u>22473247</u>	70
	<u>00</u>
	103
<u>375,033,545,936</u>	

720
 50
2201

	22.2
	<u>10.3</u>
	66.6
	22.2
60) 286613415	
348	
<u>348</u>	
	86
	<u>10.3</u>
	266

48 31

$$\Delta = 97^{\circ} 18' 00''$$

$$L = 373.78$$

$$\begin{array}{r}
 130 = 5+24 \\
 373.78 \\
 \hline
 8+97.78 \\
 2.22
 \end{array}$$

		3° 20' 5"
5+50	= 3° 22.8	3° 15'
+75	6° 37.8	<u>435.5</u>
6+00	9° 52.8	315
+25	13° 07.8	<u>950</u>
		315
+50	16° 22.8	<u>13.05</u>
		315
+75	19° 37.8	<u>16.20</u>
7+00	22° 52.8	V.P.O.C.
+25	26° 07.8	
+50	29° 22.8	
+75	33° 37.8	
8+00	35° 52.8	
+25	39° 07.8	
+50	42° 22.8	
+75	45° 47.8	
+97.78	48° 39.1	

$$\begin{array}{r}
 N 7^{\circ} 00' 30'' \text{ W} \\
 N 82^{\circ} 59' 30'' \text{ E} \\
 \hline
 90 00' 00''
 \end{array}$$

$$\begin{array}{r}
 N 82^{\circ} 59' 30'' \text{ E} \\
 N 14^{\circ} 18' 30'' \text{ W} \\
 \hline
 97 08 00'' \\
 68 41 00
 \end{array}$$

$$\begin{array}{r}
 1.6929694 \\
 3141593 \\
 \hline
 2.0071287 \\
 220.10
 \end{array}$$

$$\begin{array}{r}
 200712870 \\
 401425740 \\
 \hline
 40142574 \\
 421.69026870
 \end{array}$$

$$\begin{array}{r}
 1.6929694 \\
 10052360 \\
 \hline
 1.6982054 \\
 220.10
 \end{array}$$

$$\begin{array}{r}
 169820540 \\
 339641080 \\
 \hline
 33964108 \\
 373.775008540
 \end{array}$$

$$\begin{array}{r}
 478 \\
 51.3 \\
 \hline
 391
 \end{array}$$

165°	Dist	261.5	-
	44'	5.6	55.9
	26'	4.9	56.6
	14'	3.9	57.6
180°	14'	2.9	58.6
	33'	3.4	58.1
	47'	3.0	58.5
	60'	2.4	59.1

$$\begin{array}{r} 52 \\ 60 \overline{) 202.8} \\ \underline{180} \\ 22.8 \\ \underline{150} \\ 7.8 \\ \underline{60} \\ 1.8 \end{array}$$

$$\begin{array}{r} .00781 \\ 220.1 \overline{) 17188734} \\ \underline{13407} \\ 37817 \\ \underline{17608} \\ 2013 \end{array}$$

$$\begin{array}{r} .00781 \\ \underline{36} \\ 4686 \\ \underline{1562} \\ 20306 \end{array}$$

$$\begin{array}{r} 3^{\circ} 38.3 \\ 60 \overline{) 20306} \\ \underline{180} \\ 230 \\ \underline{180} \\ 500 \end{array}$$

$$\begin{array}{r} 07.8 \\ \underline{24} \\ 312 \\ \underline{156} \\ 1872 \end{array}$$

$$\begin{array}{r} 22.78 \\ \underline{07.8} \\ 18554 \\ \underline{15946} \\ 2608 \end{array}$$

$$\begin{array}{r} 2028 \overline{) 32} \\ \underline{20} \\ 28 \\ \underline{20} \\ 8 \\ \underline{6} \\ 2 \end{array}$$

$$\begin{array}{r} 3078 \\ \underline{300} \\ 76 \\ \underline{60} \\ 168 \end{array}$$

$$\begin{array}{r} 00781 \\ 2278 \\ \underline{6348} \\ 5467 \\ \underline{1062} \\ 1505 \end{array}$$

$$\begin{array}{r} 60 \overline{) 1779118} \\ \underline{12} \\ 5307 \\ \underline{300} \\ 2307 \end{array}$$

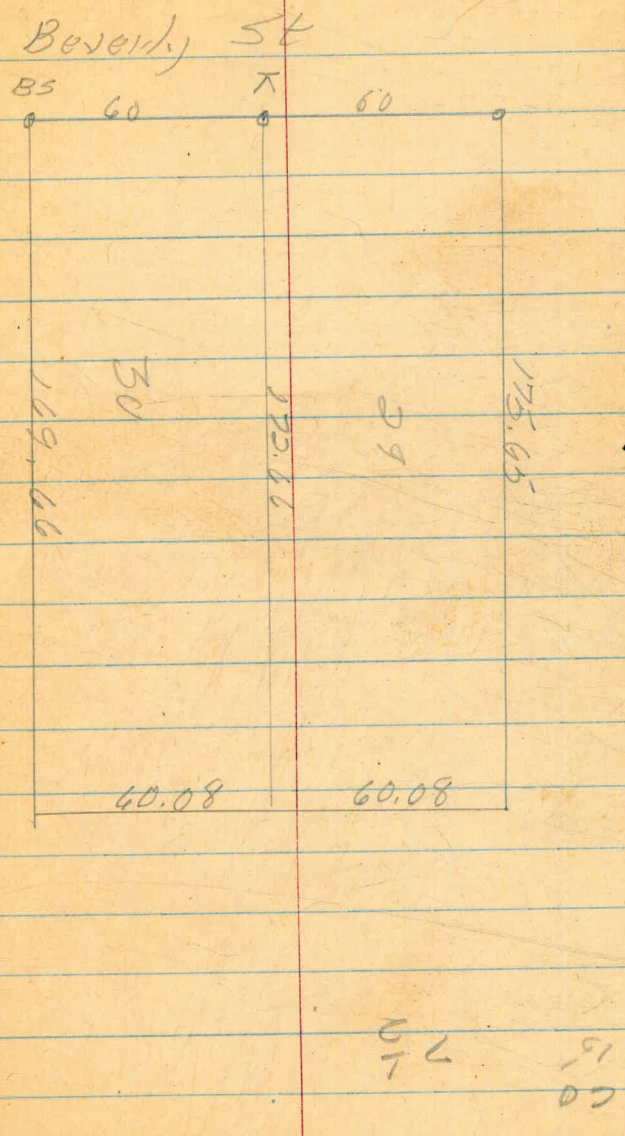
$$\begin{array}{r} .00781 \\ 50 \\ \underline{36} \\ 14130 \\ 60 \overline{) 39050} \\ \underline{36} \\ 305 \\ \underline{300} \\ 500 \end{array}$$

$$\begin{array}{r} 45 \ 35.5 \\ 2^{\circ} \ 51.3 \\ \underline{48 \ 26.8} \end{array}$$

$$\begin{array}{r} 180 \\ \underline{180} \\ 50 \\ 3020.5 \\ 60 \overline{) 203.06} \\ \underline{180} \\ 23 \\ \underline{120} \\ 30 \end{array}$$

Dist	Dist		
25°	16'	5.4	56.1
90°	15'	5.4	56.1
	30'	7.7	53.8
	45'	10.9	50.6
105°	45'	10.9	50.6
	21'	6.6	54.9
	11'	4.8	56.7
120°	14'	5.0	56.5
	30'	7.5	54.0
	41'	9.8	51.7
	55'	12.2	48.3
135°	62'	9.5	52.0
	45'	8.6	52.9
	27'	6.3	55.2
	13'	5.0	56.5
150°	23'	5.5	56.0
	40°	6.9	54.6
	60'	7.9	53.6
165°	60'	5.3	56.2

Del 3	Dist	+	Hi	-
		1.5	261.5	260.
00	20'			3.1 258.4
	30'			3.5 58.0
	50'			3.4 58.1
15°	50'			5.6 55.9
	32'			4.8 56.7
	20'			4.2 57.3
30°	21'			4.7 56.8
	42'			6.2 55.3
	65'			7.8 53.7
45°	60'			9.2 52.3
	40'			7.3 54.2
	20'			4.8 56.7
	0			3.9 57.6
60°	20'			5.4 56.1
	40'			7.9 53.6
	53'			10.2 51.3
75°	50'			11.1 50.4
	30'			7.7 53.8



2+96=3+50 15° 13'

30⁹⁵

1+64² 20° 09' RT

43⁷

19'

64⁷

1+45² 45° RT

0+92⁸ 56° 15' RT

63³

29⁵

92⁸

52⁹

121^{5⁷}

0+63⁵ 40° RT

0+00

0V

Alley Bk 67
North of Landis East of 39

Stk	+	H ₁	-
	4.81	346.00	341.21
	6.93	341.68	334.75
		11.75	+4.10 To Flow
0+00		11.1	330.6
+50		6.3	335.58
1+00		5.2	
+50		4.2	
2+00		3.1	
	7.53	348.46	340.93
2+50		7.7	76
3+00		6.7	341.76
+50		5.6	
4+00		4.9	
+50		3.9	
5+00		3.3	345.16
+50		3.5	
6+00		6.8	
6+23 ²		7.0	
		6.25	.21

TBM Top QV 0+00 See FB 787 Page 77

South Rim Lower MH @ Alley + Landis

North prop line Landis St

348.46

341.21

+5.20

346.41

341.21

3.28

344.93

9.05

335.44

344.49

344.49

3.7

3

0

347.19

344.89

338.60

13.9

341.68

11.75

329.93

344.49

329.93

14.56

8' B.V.

Taft St
Profile

	+	HI	-	
	3.05	125.05		120.00
	7.47	125.00	5.50	117.55
	13.04	138.00	0.04	124.98
	12.13	150.13	0.02	138.00
	3.32	149.95	3.50	146.63
0+00			0.4	
0+17			1.42	
0+17 ²			2.05	
			3.31	+8.50
0+50			3.70	
0+69			3.96	
0+71			4.16	
1+00			3.1	
1+50			4.2	
2+00			6.2	
+50			9.6	
3+00			12.4	
	3.28	140.39	12.84	137.11
+50	"		4.3	
			4.55	+5.0
4+00			4.7	
+50			4.7	
5+00			4.5	

BM N.W. BP Bellview + Midway

South Line Colima Edge side walk

Top Carb

Street

West Rim MH 2 Colima

Edge Pavement

6" GV

$\frac{3.7}{3.0}$

$\frac{2.0}{1.0}$

$\frac{2.8}{1.0}$

$\frac{4.9}{1.0}$

$\frac{8.7}{1.0}$

Turn on Meter Box

West Rim MH 4+00-10²L

5+50	140.39	4.7	
6+00		5.2	
+50		3.0	
6+60		7.4	
6+98		8.38	
7+00		7.8	
		8.5	
+50		8.0	
8+00		6.6	
+50		5.6	
9+00	13.09	4.4	136.11
		4.28	
+50		11.7	
		9.40	
10+00		9.6	
+50		6.9	
11+00		4.7	
+50		3.0	
12+00		1.7	
+50	1.28	0.9	148.98
		0.22	
13+00		0.9	
+30		1.45	
+50		1.20	
+90		2.20	
+80		1.60	
13+99.7		1.75	
		12.73	137.53 = 137.49

2.6
7.0
4.0
10.

Edge Pavement South Prop Line Midway
West Rim MH & Midway

North Prop Line Midway

Edge element
8.1 5.2
3.0 8.0

7.2 4.7
4.0 10

5.5 3.7
4.0 10

4.5 3.4
4.0 6.0

8.4
10

Turn on Rock

West Rim MH

4.5
10

4.5 2.3
7.10

edge Pavement South Prop Forward

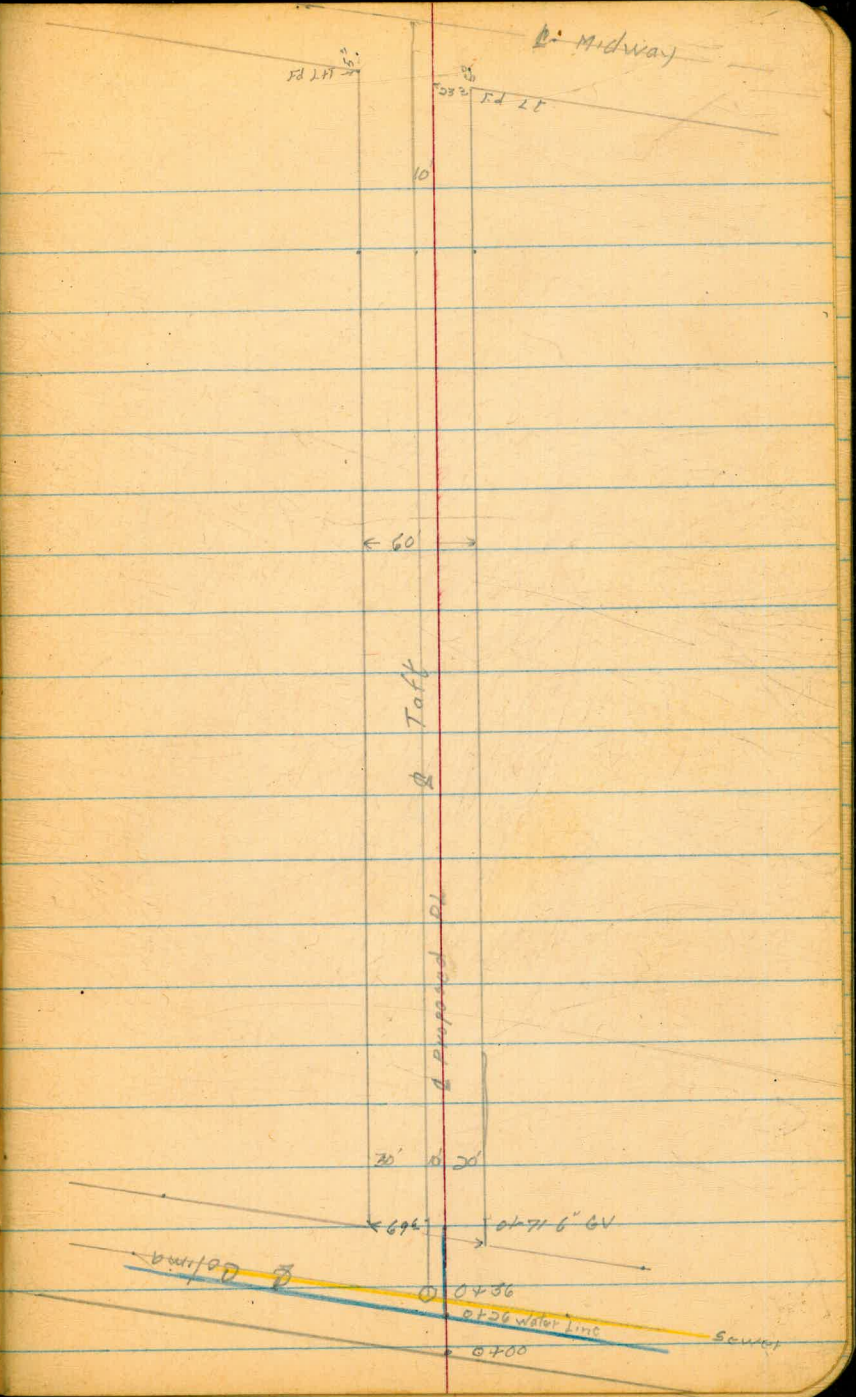
Top curb
North prop line of Forward St on sidewalk

SE Top Hyd Bellview + Forward.

Taft St
Colima to Forward

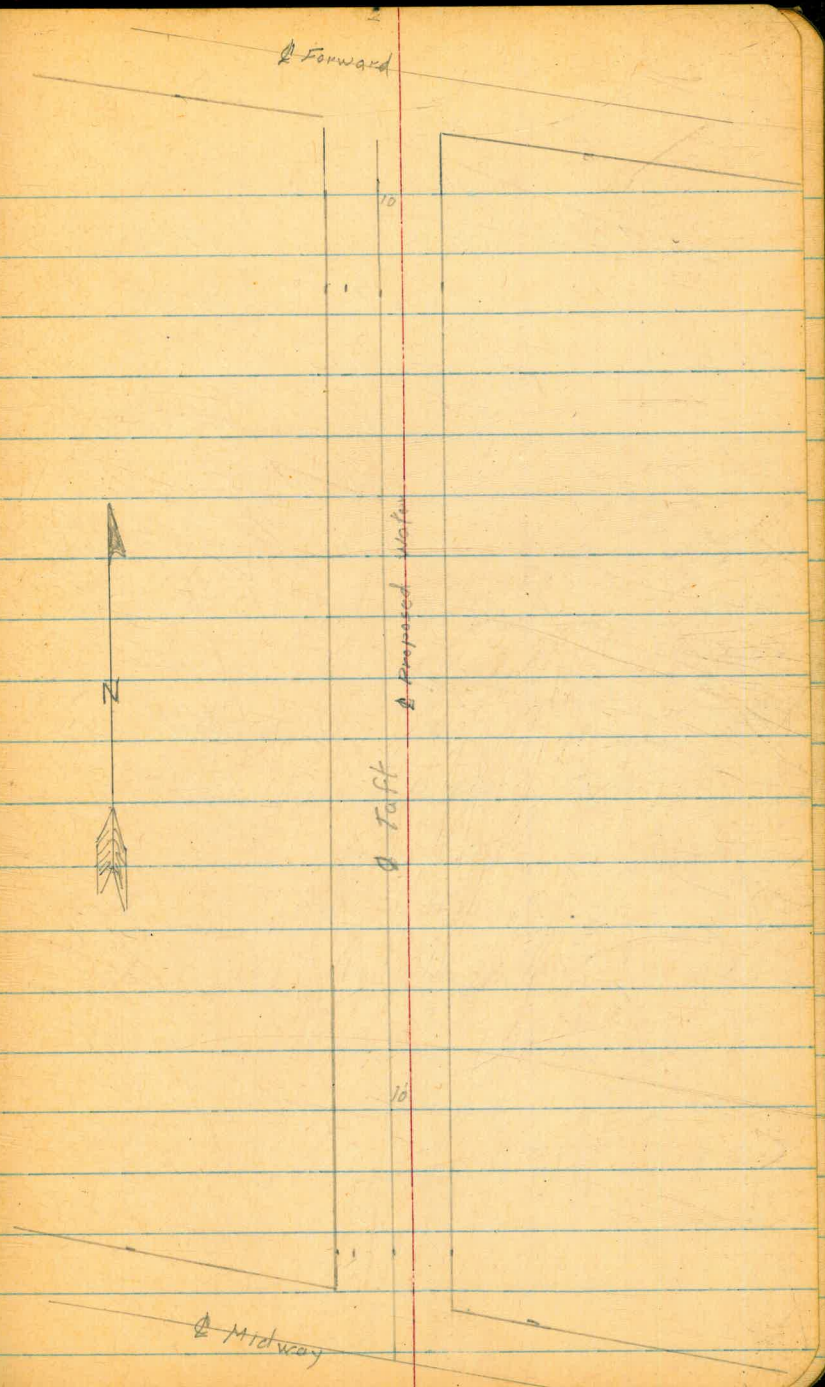
0+00

South prop Line Colima St



13+99²

North Prop Line Forward SE



Profile So Bancroft
Ocean View
to Webster

West
Powell
Kemp

	+	Ht.	-	
	13.04	30.26	0.62	17.22
	13.03	42.67		29.64
0+30			10.7	
0+40			10.36	+7.50 invert
0+70			10.17	
1+00			9.3	
+50			6.0	
2+00			3.0	
+29			0.19	+8.61 invert
	12.83	55.49	0.01	42.66
+50			12.5	
3+00			9.0	
+50			4.1	
			0.44	55.05
	13.04	68.09		
4+00			11.6	
+50			9.1	
5+00			4.9	
			0.12	67.97

Bm Oceanview + 33rd Top Hyd SE Cor

0+30

East Rim MH

edge pavement North prop line

East edge MH 2

Turn on Rock

So Boncroft St

	+	Hi	-	
	10.29	78.26		67.97
5+50			9.5	
6+00			5.0	
+50			2.6	
7+00			3.1	
+50			6.1	
8+00			7.6	
+50			10.8	
	3136	6868		65.32
9+00			4.3	
+50			6.6	
+90			6.81	+610 Flow Line
10+00			7.4	East Rim MH
+50			8.2	
11+00			9.2	
+50			10.1	
			9.20	13 R MH West Rim 3' inside Curb
12+00			9.0	
12+28			8.3	
	12.05	80.64	0.06	68.62
	0.32 ^c	77.09	3.87	76.77
	0.19	65.12	12.16	64.93
	2.39	57.14	10.37	54.75
			8.47	48.67 = 48.61

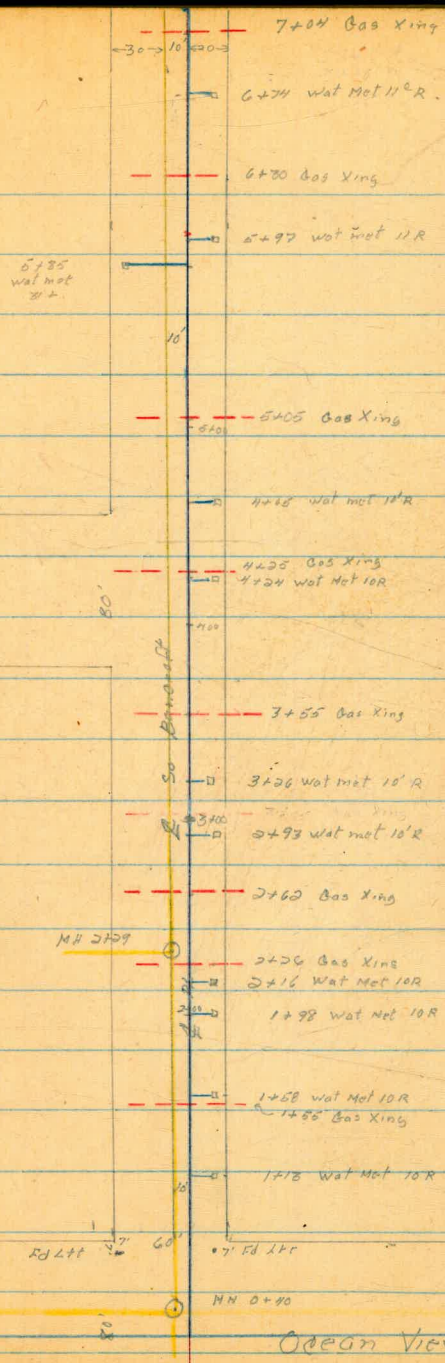
North Prop Webster

NW BP Oceanview + 31.25

D+00

South Prep Line Ocean View

Franklin St



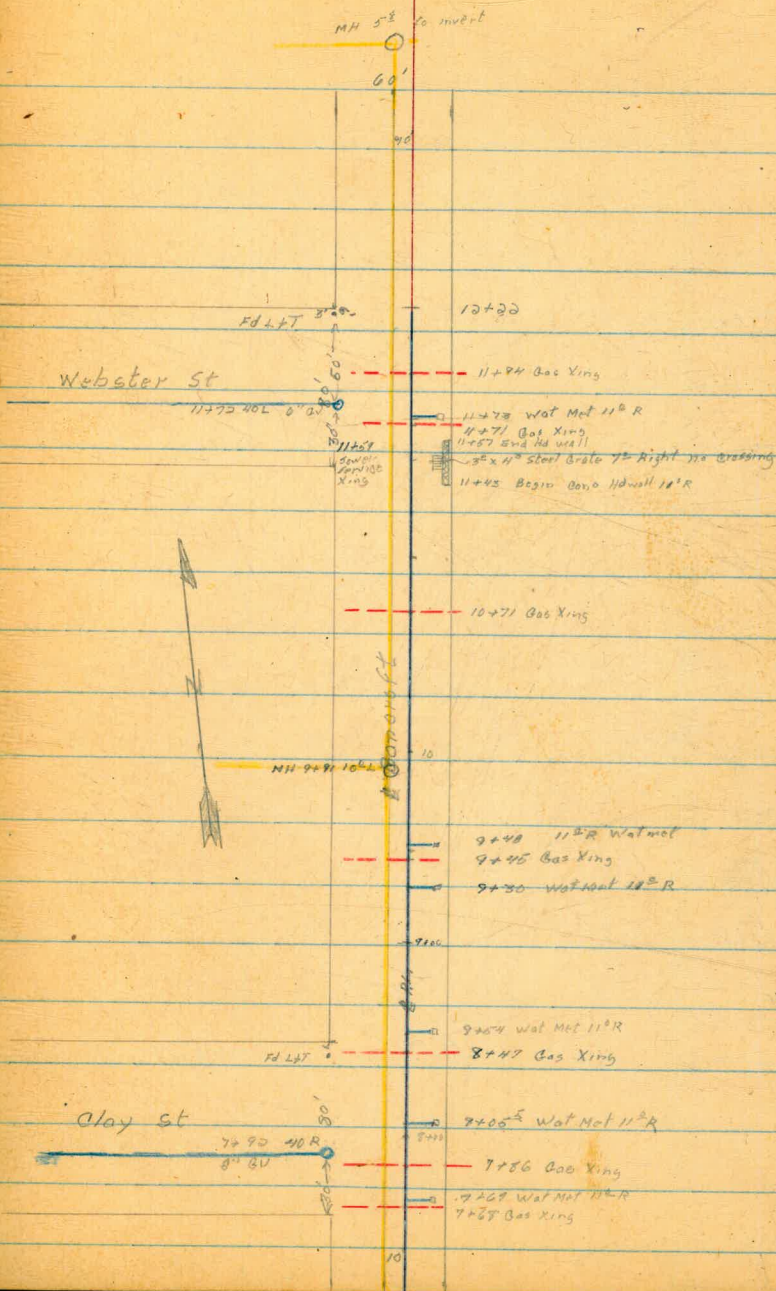
Ocean View

12+22

North Prop line Webster St

North Prop Line Webster St

North Prop Line Webster St



Poppy Place
Q PL Profile

West
Kemp

16 Jan 52

	+	289.58		286.38
	3.20	289.58		286.38
	4.13	282.58	11.13	278.45
0+00			4.8	
0+25			4.89 + 8.51 = 13.40	
0+50			5.7	
1+00			6.0	
+50			5.9	
2+00			5.0	
+30	⁸⁹		4.6	
+67	⁴⁹		4.5	
3+14	¹⁹		3.8	
+40	^{EB} ²²		3.2	
3+50			3.1	
4+00			2.4	
+50			1.3	
	8.55	289.94	1.19	281.39
5+00			0.9	
+35			5.40	MH + 5.10 = 10.50
+50			0.2	
+66			6.12	
			3.53	286.41 = 286.38

BM Top Hyd SE cor Violet + Poplar

West line of manzanita St

South rim MH

5.8
10

6.0 9.2
8 10

5.9 7.6
2 10

9.94
80.58
3.56

Rock by alley

South Rim MH

Top of handle of S Gate valve

- 1.67 288.31 Top FH SE Cor Violet + manzanita

5+62 E

5' BO.
8" ~~AV~~ Max

100.69
16.86
46.89
166.34

9 51

3+410 ^{ED} 79

58° 18' 30"

180.89
36.60

3+414 19

38° 55' 20"

217.49
36.60

2+67 49

19° 26' 10"

54.19
36.60
90.79

2+30 89 BO

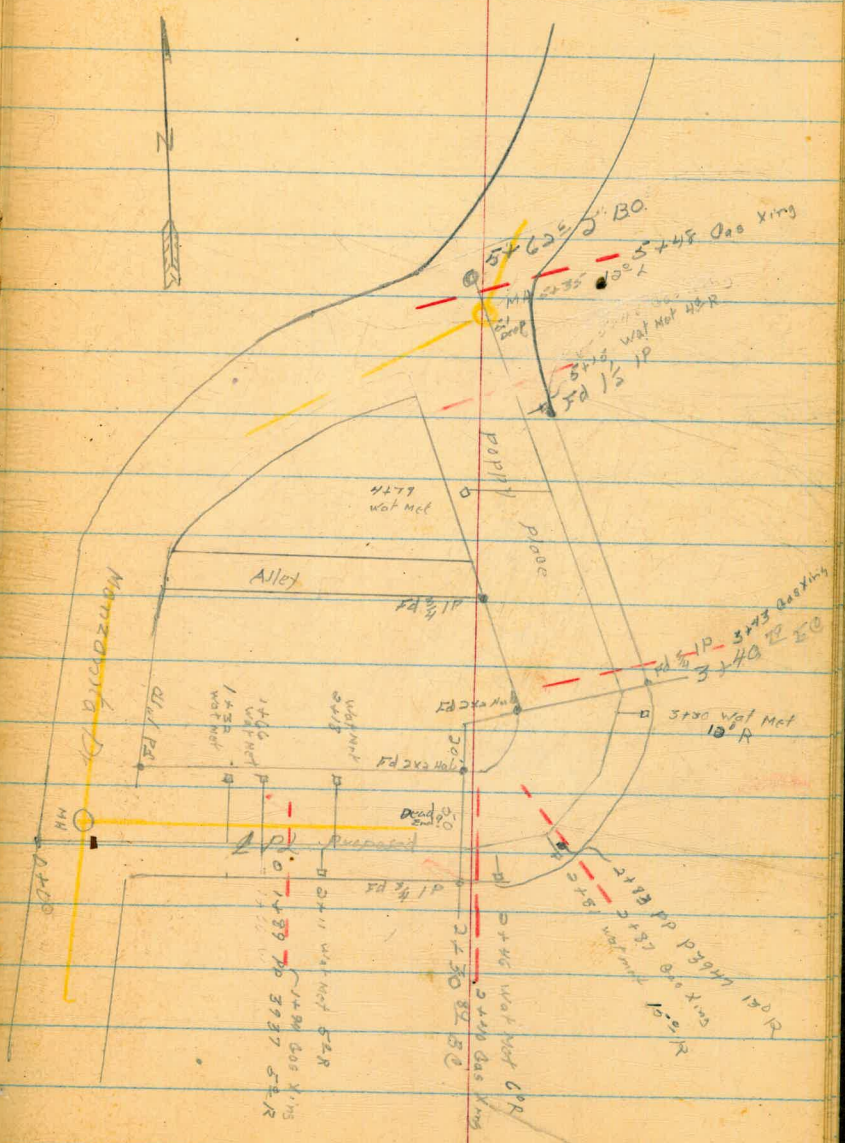
N 43 19 E
5 73 18 E

Δ 2 / 116° 37'

1/2 Δ 58° 18' 30"

R = 55'

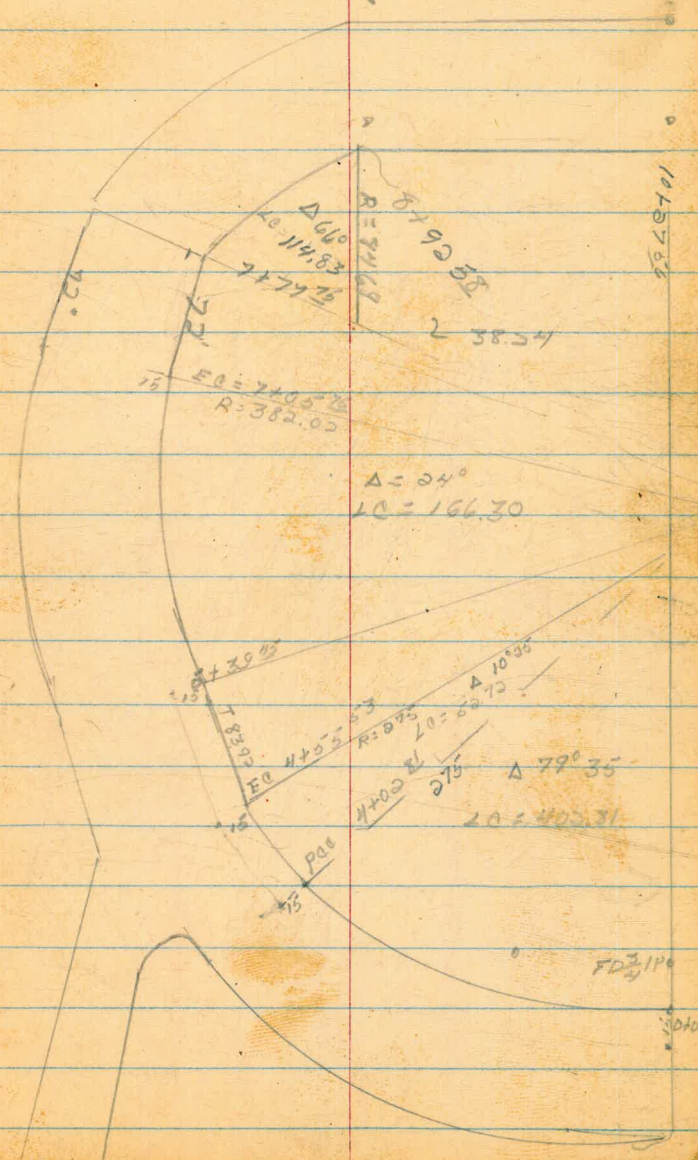
L = 111.94



5+50 45.7'
 +75 2° 34'
 6+00 4° 22.3
 +25 6° 10.6
 +50 7° 58.9
 +75 9° 47.2
 7+00 11 35.5
 7+05 12° 00

777.76
 38.28
816.03
 38.28
854.31
 38.28
892.59
 7.42

38' cord



Madison at 6th
Check Levels

	0.77	333.80		333.03
	1.40	323.00	12.20	321.60
			0.59	321.41
	1.35	313.93	10.42	312.58
0+00			3.4	310.5 307.3
+25			5.2	308.7 306.1
+50			6.4	307.5 304.7
+75			7.8	306.1 303.4
1+00			9.1	304.8 302.3
+25			10.2	303.7 301.0
+50			10.9	303.0 300.3
+75			11.3	302.6 299.5
2+00			11.6	302.3 299.0
+25			11.9	302.0 298.9
+50			11.9	302.0 298.8
			11.6	302.3
	11.37	325.20	0.10	313.83
	8.58	333.76	0.02	325.18
			0.75	333.01 = 333.03

BY 7 CT NW BP MASS + Madison

MW 7.01 NW Hampshire

0 32

0 26

0 28

0 22

0 25

0 22

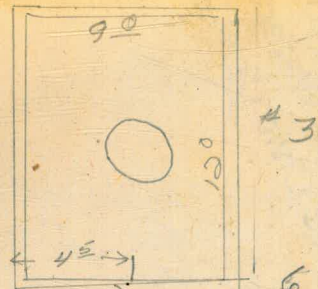
0 22

0 34

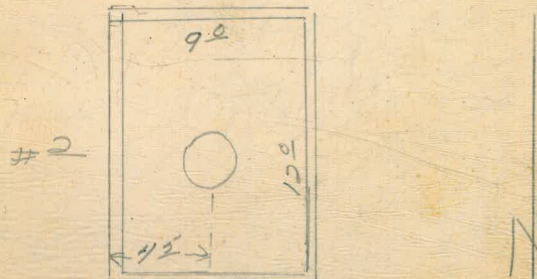
0 32

0 34

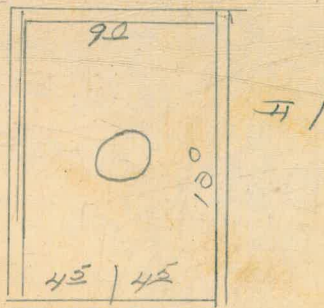
0 32



6 elec cables
 3" to Top cables
 3" to Box Proper



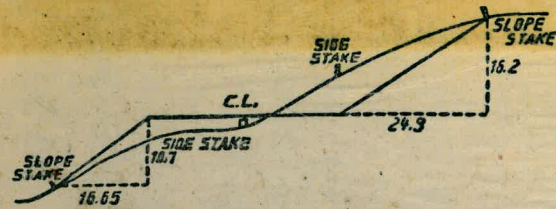
10 1/2" Deep to Botk
 4 1/2" Box



8 1/2" Deep
 2 1/2" to Box proper

Please Return to
 City of San Diego Water Dept
 Room 903 Civic Center

8 + 94 65 06
 50
 9 + 44 65
 13
 117
 \$ 30
 260



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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