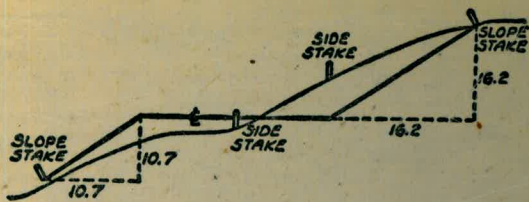


818

Top F.H. 269.02
Brooklyn
Stork

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

JAN 16 1965

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.11	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.12	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.35	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

alice
 F ST 30TH TO 28TH & Profile proposed water 3-4
 Pacific Beach DR. " " " " 5-6
alice
 SHAMROCK, & Profile proposed water ✓ 7-8
 " & of proposed water ✓ 9.
 SYCAMORE, & " " " " " " " " 10-12
 " & Profile " " " " " " " " ✓ 13-15
 SYCAMORE & of proposed water, Snowdrop Hollywood Park -
 " " Profile " " " " " " " " ✓ 17
 Tuberose St. Profile Poplar to Tuberose Lane *alice*
 Pepper Dr. Violet to Tuberose St. Profile 20 ✓
 MALLARD ST - Springfield to Alameda - Proposed WATER 21-22
 " " " " " " " " " " ✓ 23-26
 Alley Block # 9 - Proposed Water & Profile ✓ 27-28
 " " " " " " " " " " Proposed Water ✓
 Alley Block # 16 - & Profile ✓ 29-31
 " " " " " " " " " " Proposed Water ✓
 Alley Block # 16 - & Profile ✓ 32-34
 " " " " " " " " " " Proposed Water ✓
 Alley Block # 3 - & Profile ✓ 35-37
alice
 Alameda Mallard to Mulberry 38-40
alice
 SHAMROCK ST, JUNIPER to SYCAMORE, STS & Grds 6" WATER 41-43 ✓
 SYCAMORE, TULIP TO VIOLET, STS & Grds 6" WATER 44-46 ✓
 " " VIOLET, TO TUBEROSE " " " " " " " " ✓ 47 ✓
 TUBEROSE, Poplar to Tuberose Place " " " " " " " " ✓ 48-50
 PEPPER DR. VIOLET TO TUBEROSE " " " " " " " " ✓ 51-52
 Alley Bix 55, Near Wightman, E of 38TH " " " " " " " " ✓ 53-55
alice

INDEX (cont'd)

SUMAC DR, JUNIPER TO LAUREL, STR'S & GRDS for 8" WATER ✓ 55-57

SYCAMORE DR, SNOWDROP to HOLLYWOOD PARK " " " 6" " ✓ 58-59

64TH ST, AKIN TO BROOKLYN " " " " " " ✓ 60-61

POPPY PLACE, MANZANITA TO MANZANITA, " " " " " " ✓ 62-63

SUMAC DR & LAUREL ST. " " " 8" " ✓ 64-65

LAUREL ST. FAIRMOUNT TO SUMAC " " " 6" " ✓ 66

SUMAC & LAUREL, " " " " " " " " ✓ 67-68

STORK ST, AKIN TO BROOKLYN " " " 6" " " " ✓ 69-71

NARANJA ST. EUCLID TO 54TH ST " " " 6" " " " ✓ 72-74

62ND ST, AKIN TO BROOKLYN " " " 6" " " " ✓ 75-77
alice

ALLEY BUX 3 ^{MYRTLE TO THORN} BETWEEN BOUNDARY & NINE " " " " " " " " ✓ 78
alice

"F" ST
30TH To 28TH
& PROFILE
PROPOSED 6" WATER MAIN

Mar. 31 1952

BEATTY
PEWELL
BERGER

21

BM	0.94	158.74		157.80 = 157.35
P	0.16	145.72	13.18	145.56
13+10			10.83	+133.4 134.9
13+00			10.70	+133.6 135.0
			13.35	-130.9 132.4
12+93			10.55	+133.7 135.2
12+83			10.3	+133.96 135.4
12+50			7.2	+137.1 138.5
12+00			1.0	+143.3 144.7
P rock	11.62	157.22	0.12	145.60
11+50			5.95	+149.81 151.3
P	13.32	170.50	0.04	157.18
11+00			13.3	+155.7 157.2
10+50			7.6	+161.4 162.9
10+00			3.4	+165.6 167.1
9+50			1.8	+167.2 168.7
9+25			2.1	+166.9 168.4
9+00			3.1	+165.9 167.4
8+75			4.8	+164.2 165.7

BP SE Cor. 28TH & F
City Engr. calls this (Plug in Man?)

on AC \ of 28TH ±

Top of stem of W.V. 12 @ 134.00

Begin of A.C.

E. Curb line 28TH

11+41 }
11+21 } Approx. Alley
(unimproved)

10+77 38' RT WAT. MET

10+73 16' LT. WAT. MET

10+53 Gas Jer King

10+50 2" Wat. 45 LT

10+39 { 16' LT WAT. MET
38' RT "

16' LT 9+963 End of Curb

36' RT 9+85 " " "

9+74 38' RT. WAT. MET

"F" St.
(Cont'd.)
Profile

170.50

8+50 7.0 162.0 163.5

8+00 12.1 156.9 158.9

P 0.23 158.00 12.73 157.77

7+50 5.0 151.5 153.0

7+00 8.6 147.9 149.4

6+50 11.5 145.0 146.5

P 3.15 148.44 12.71 145.29

6+00 4.7 142.2 143.7

14° LT 25.50

35° RT 24.35

5+50 5.8 141.1 142.6

5+00 4.9 142.0 143.5

4+50 2.7 144.3 145.7

P 12.35 160.77 0.00 148.42

4+00 11.7 147.8 149.1

3+50 7.7 151.6 153.1

3+00 3.3 156.0 157.5

P 11.08 171.78 0.07 160.70

2+50 10.2 159.9 161.8

3/31/52

2.

9+27 38' RT WAT. MET.

9+21 18' LT " "

9+15 GAS SER Xing.

36' RT 8+71 Begin of Curb

8+23 GAS SER Xing.

36' RT 8+23 End curb

8+10 18' LT WAT. MET.

16' LT 8+09 Begin curb

7+96 36' RT WAT. MET.

36' RT 7+72 Begin curb

7+64 GAS SER Xing.

7+23 17' LT WAT. MET.

5+615 } 140° LT

35° RT

12" Drain Intet's into
30" RCP. Cross
Drain

4+10 36' RT End curb

3+82 38' RT WAT. MET.

3+82 16' LT End curb.

3+69 GAS SER Xing.

3+53 18' LT WAT. MET.

3+33 18' LT WAT. MET.

3+32 GAS SER Xing.

3+11 38' RT WAT. MET.

3+00 GAS SER Xing.

2+83 38' RT WAT. MET.

2+74 18' LT WAT. MET.

2+48 38' RT WAT. MET.

2+40 18' LT WAT. MET.

"F" St.
(CONT'D)
± PROFILE

3/31/52

3.

2+00	171.78	7.0	163.3 164.8
1+50		5.4	164.9 166.4
1+00		4.6	165.7 167.2
0+60		4.35	165.97 167.43
IP	13.25	184.32	0.71 171.07
IP	6.61	^{188.74} 190.20	0.73 183.59
CK BM		2.57	187.63

on Conc Pavt.

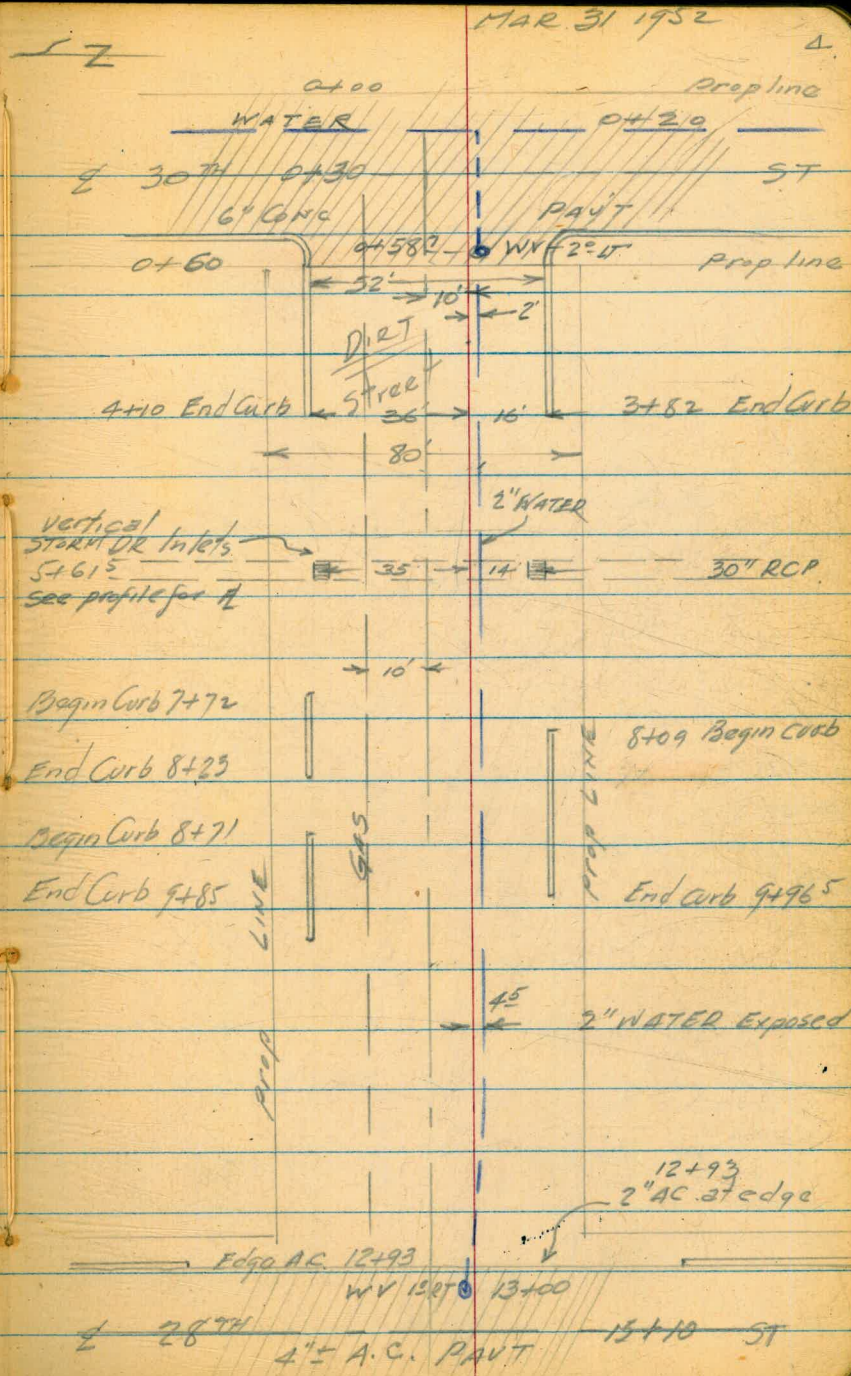
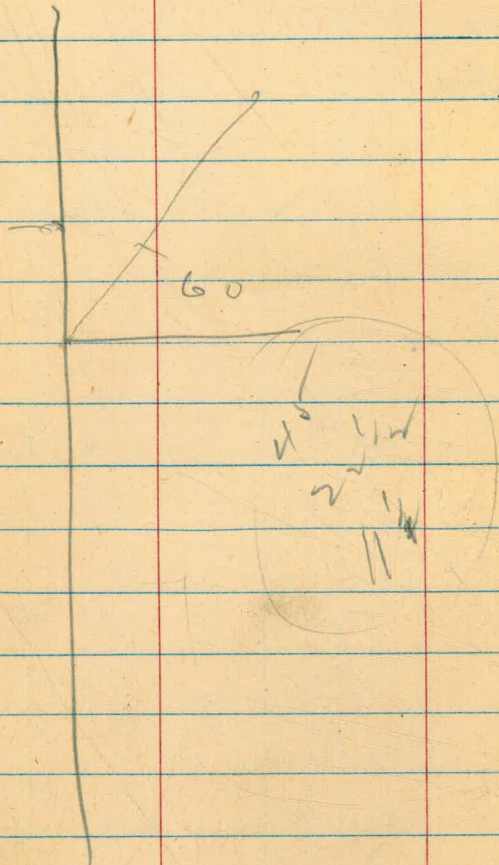
0+58.2 2' LT W.V.

182.13

OR NW Cor 30th & E

N.W. cor 30th & E 187.63

F. ST.
 30TH ST. TO 28TH ST
 & PROPOSED 6" WATER



PACIFIC BEACH DRIVE
 Morrell to Lamont
 & Proposed Proposed Water

10' 50' E ST.

& MORRELL

1+56 WAT MET 26 RT

2+41 WAT MET 26 RT

3+27 WAT MET 26 RT

3+98 WAT MET 26 RT

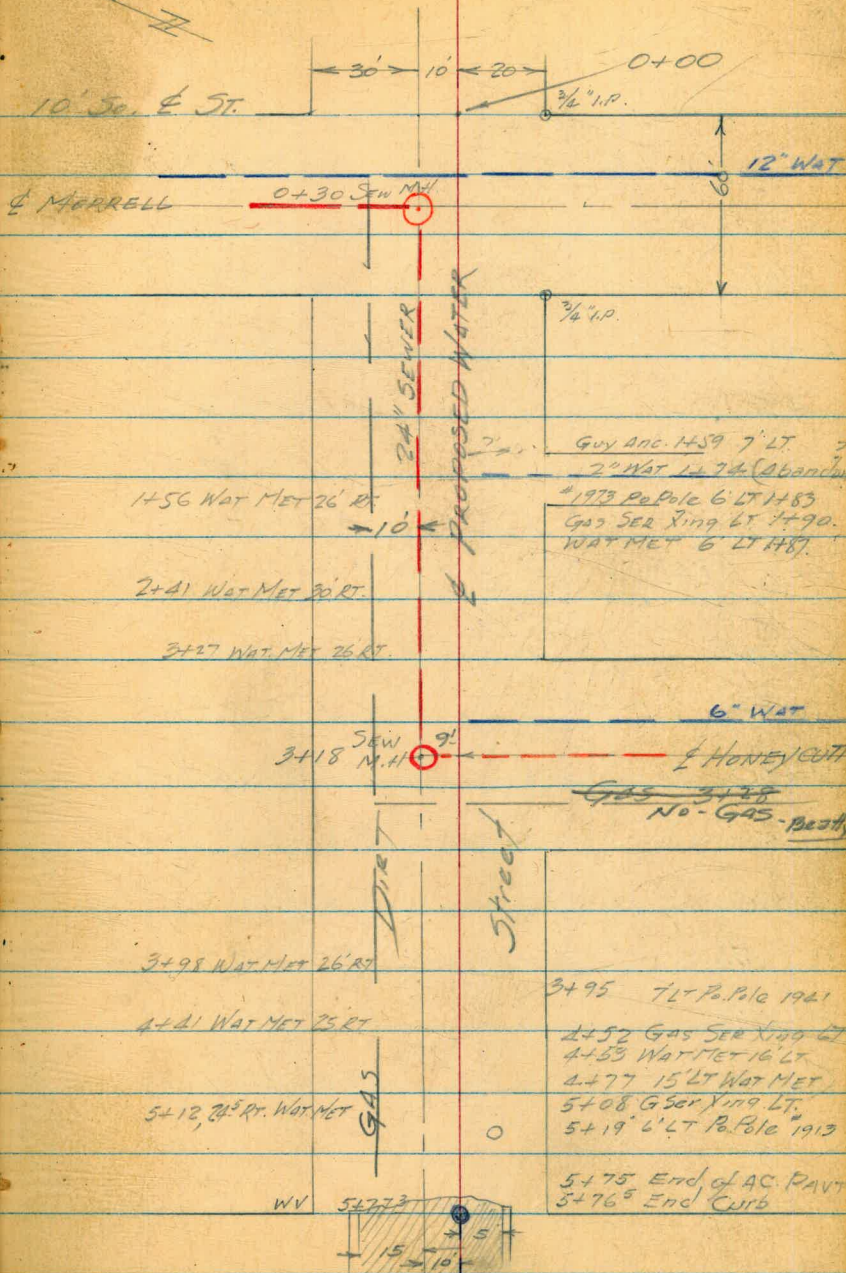
4+41 WAT MET 26 RT

5+12 24" RT. WAT MET

WV 5+77.3

May 12, 1952

5



PACIFIC BEACH DRIVE

May 12, 1952

6

	+B.S	H.I.	-F.S	Elev.
BM	1.81	37.09		35.28
5+77.3			3.0	34.1
+50			3.8	33.3
5+00			4.4	32.7
+50			4.4	32.7
4+00			4.2	32.9
+50			4.6	32.5
	24.5	M.H	Rim 4.71	
	3+18		100. 23.51	
3+00			5.1	32.0
+50			6.1	31.0
2+00			7.1	30.0
+50			8.8	28.3
1+00			11.0	26.1
0+50			12.4	24.7
0+20			14.2	22.9
0+00			15.0	22.1

7' offset LET NE COR.

Pipe Line Survey
 (10) L Shamrock

JUNE 6, 1952
 West
 Camp
 Wilson

7.

	+	HI	-	
	0.45	286.83		286.38
	1.16	278.12	9.87	276.96
	3.00	269.68	11.44	266.68 - 15.0
5+72 ¹²			2.8	266.88
+50			2.9	266.78
+00			3.5	266.27
4+50			4.2	265.57
+00			5.0	267.4 264.7
3+50			6.0	266.4 263.7
+00			6.9	265.6 262.8
2+50			8.7	263.7 260.98
+00			9.8	262.6 259.9
1+50 ²³			10.3	262.1 ³⁰ 259.4 ³⁰
+00			10.9	261.5 258.8
0+80 ²			11.6	260.8 ³⁰ 258.1 ³⁰
+50			13.0	259.4 256.7
+00			15.4	257.0 254.3
	5.72	272.37	3.03	266.65
			10.35	262.02 Nail in RP on
	11.40	281.99	1.78	270.59

DP on Fire Hyd NE Cor Violet + Poplar

Turn on MH Cover E edge X of Shamrock + Sycamore
 257.68 sewer invert Sycamore

Sycamore

SHAMROCK ST.

Profile Proposed Water
From JUNIPER - SYCAMORE

6-6-52

8

11.23	281.99	1.80	280.19
6.62	286.81	0.48	286.33 = 286.38

SHAMROCK ST.
 & PROPOSED WATER
 FROM JUNIPER TO SYCAMORE

5+72.15 End proposed water
 on SHAMROCK

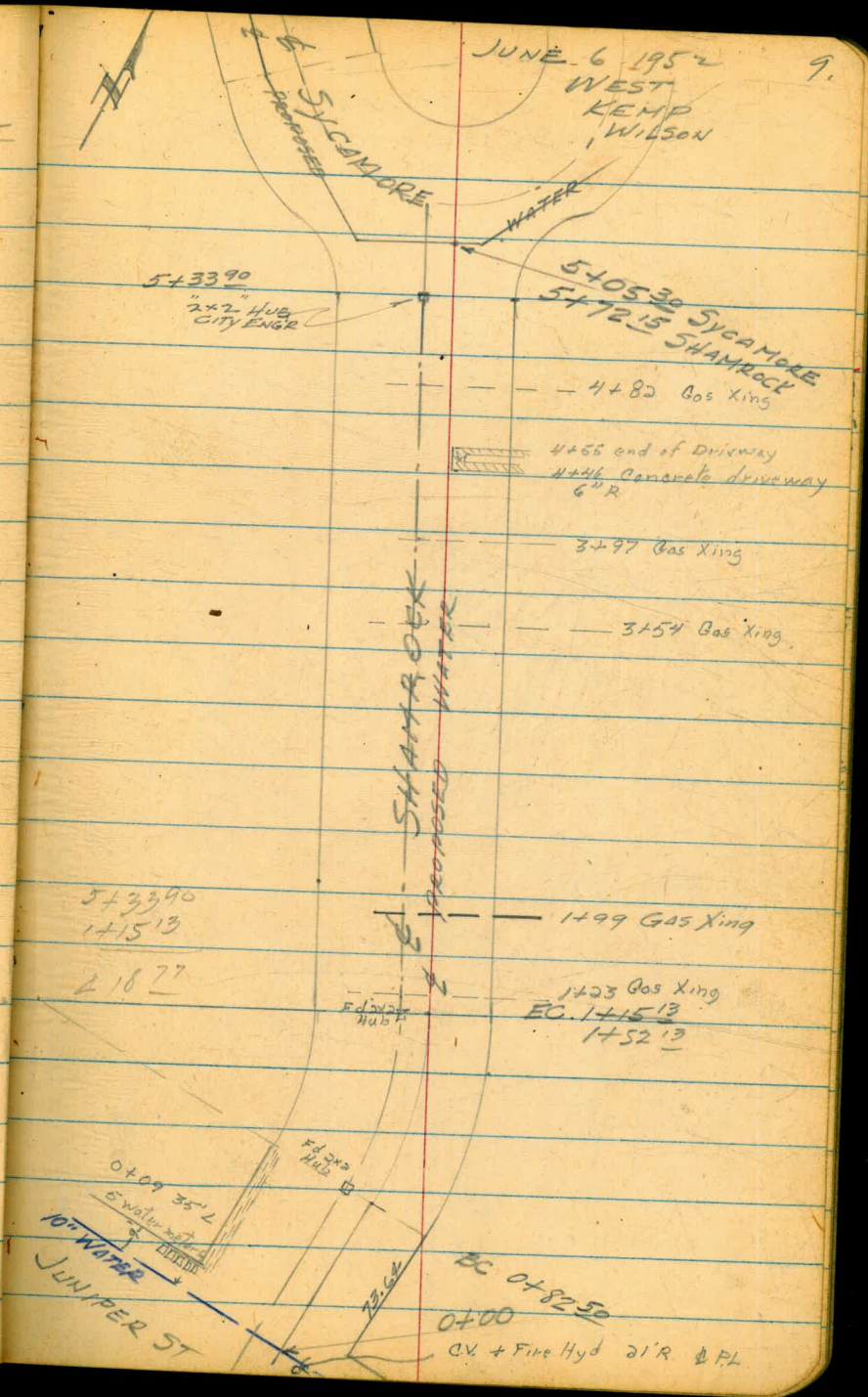
1452.13
 1115.13 EC

$\Delta = 29^{\circ}33' 47''$
 $R = 135.00$
 $L = 69.63$

0+82.50 BC

0+00

82.50
 69.63
 12.87
 13



5+33.90
 1+15.13

2+16.77

Edwards
 Hub

1+23 Gas Xing
 EC. 1+15.13
 1+52.13

BC 0+82.50
 0+00

C.V. + Fire Hyd 21" R & FL

SYCAMORE ST
FROM TULIP - VIOLET TUBEROSE
& PROPOSED WATER

JUNE 4, 1952 10.
BEATTY
POWELL
VARON FARU

2+95.46 EC

10'
South-
eastly
of
Street.

$\Delta 47^{\circ}37'25''$ RT
R = 175.00
L = 145.46

144.68?

Proposed
Water.

1+50 B.C.

0+76 X.P.T. $68^{\circ}13'$ LT

0+71.8 AT & of Existing TEE

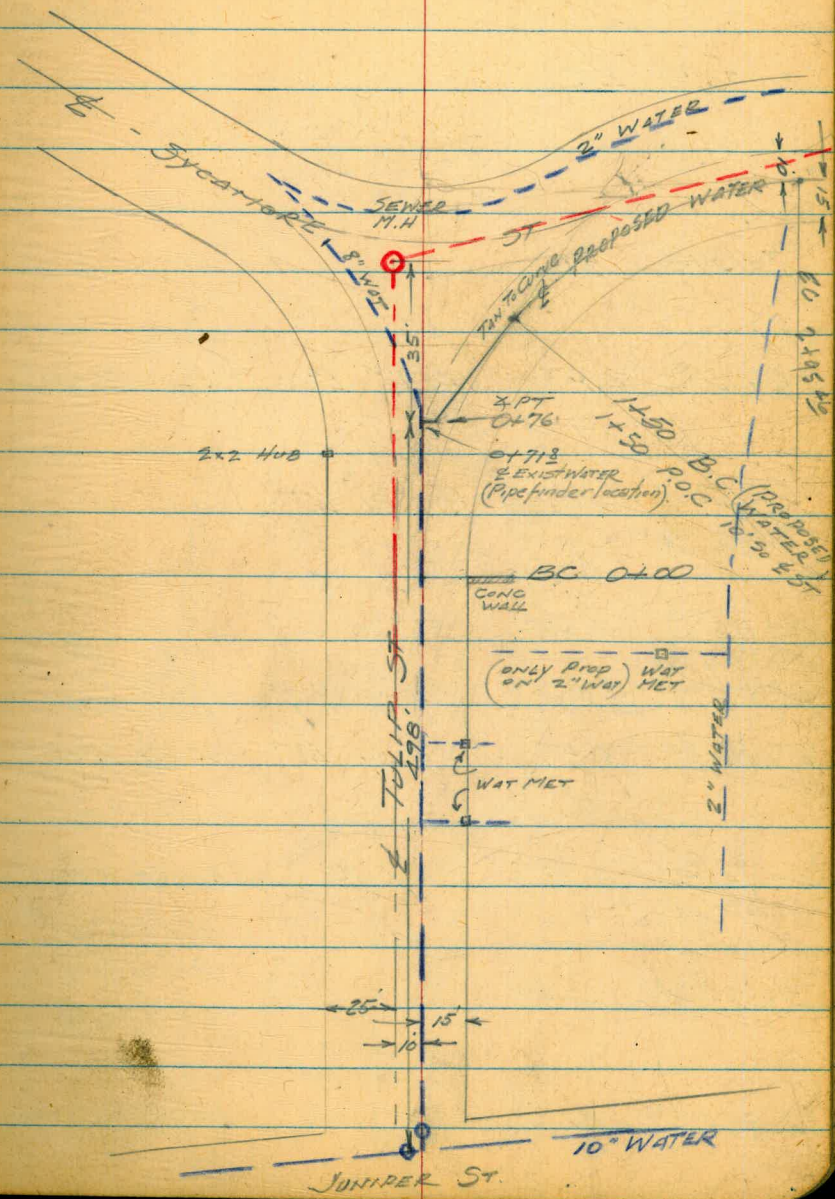
2+95.46 EC

$\Delta = 96^{\circ}44'$ RT
R = 175.00
L = 295.46

274.33?

10'
South
eastly
of the
St.

0+00 B.C.



SYCAMORE ST
TULIP to VIOLET TUBEROSE
& PROPOSED WATER

JUNE 6 1952 11.

8+73²⁸ E.C.

$$\Delta = 51^{\circ}10' RT$$

$$R = 149.83$$

$$L = 133.78$$

7+39⁵⁰ BC

6+11⁸⁰ X PT 14°17' LT (E.C. of STREET)

5+50 X PT (37°31' LT)

5+00 X PT 42°30' LT

4+96⁵⁴ X PT (57°30' LT)

4+54⁶⁸

E.C.

4+06⁵⁴ X PT (22°30' LT)

3+74⁸² X PT (12°01' RT)

3+34⁹⁴ X PT (29°51' RT)

2+95⁴⁶ E.C. (11°15' RT)

USE 15' H

USE 85' H

$$\Delta = 32^{\circ}15'$$

$$R = 85.0'$$

$$L = 47.97'$$

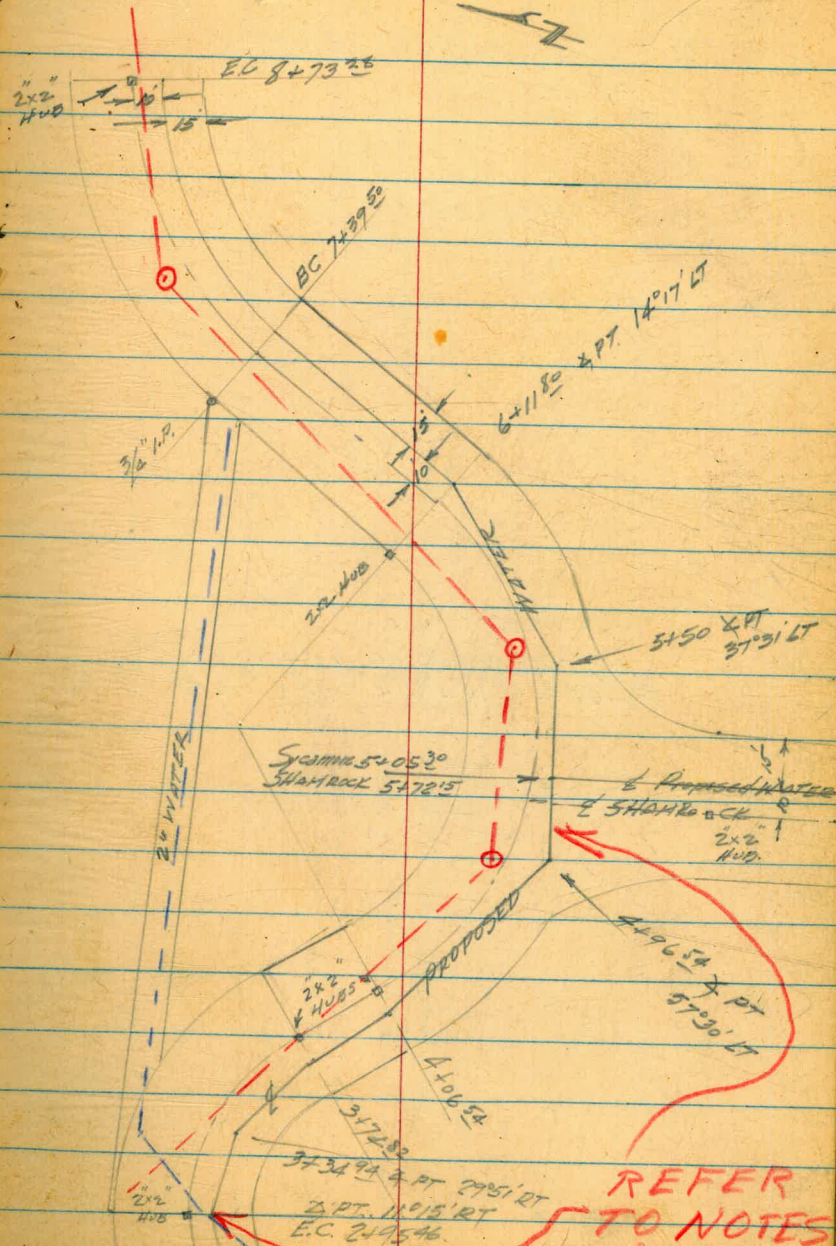
USE 85' H

$$\Delta = 53^{\circ}04'$$

$$R = 85.10'$$

$$L = 79.36'$$

(P.R.C. OF STREET)



REFER TO NOTES
D. Wilson

SYCAMORE ST
 TULIP TO VIOLET TUBEROSE
 & PROPOSED WATER

Intersection
 of proposed water with
 Existing water on Violet.

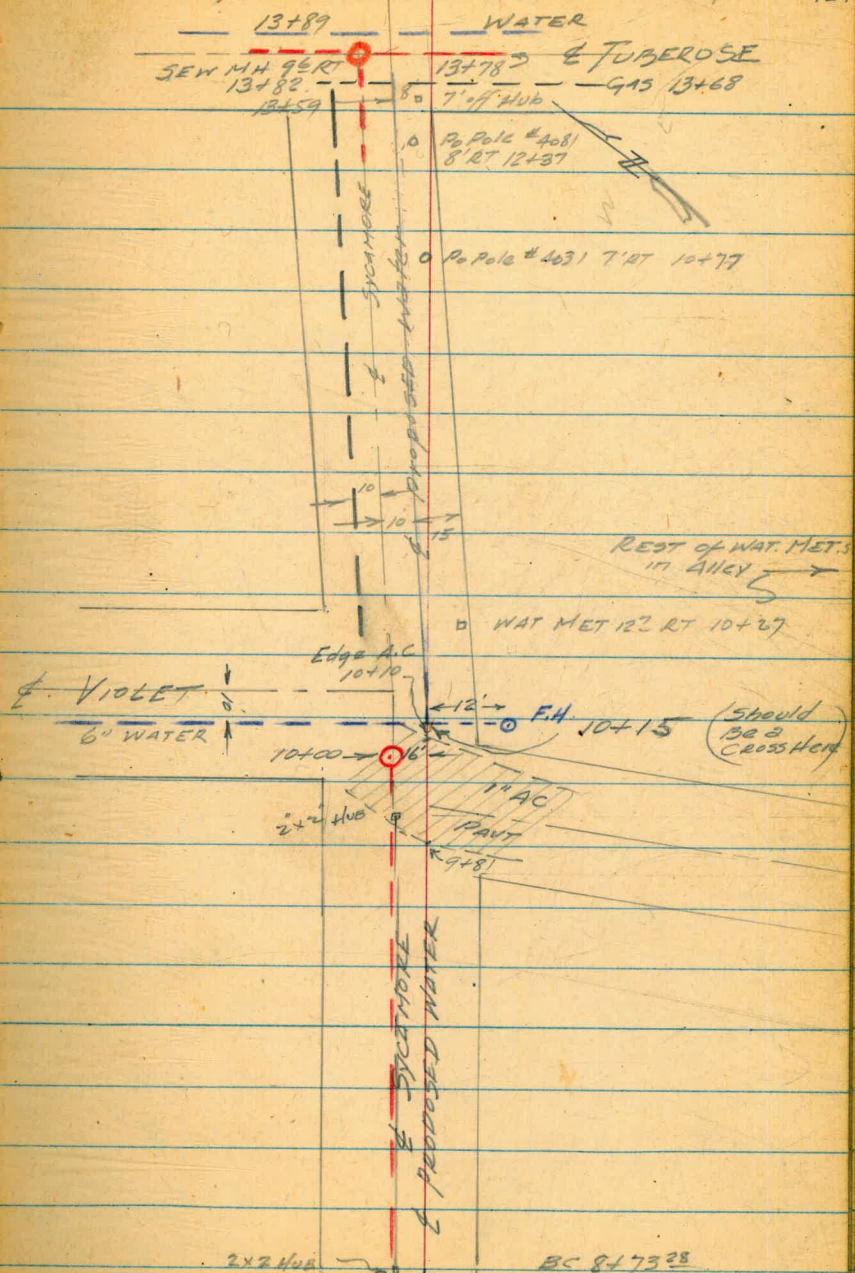
$10+10^{85}$ & PT $11^{\circ}43'LT$

8+73²⁸ EC.

E Prop line 14+04⁶

JUNE 6, 1952

12.



2x2 HUB

BC 8+73²⁸

SYCAMORE ST
TULIP to VIOLET TUBEROSE
& PROFILE PROPOSED WATER

JUNE 9 1952
BEATTY
Powell
Veronfus

BM 2.83 264.90 262.07

0+71⁸ (Existing Tee.) 2.7 262.2 ✓

0+76 3.2 261.7 ✓

1+00 5.3 259.6 ✓

+25 6.0 258.9 ✓

+50 7.4 257.5 ✓

+55 6.7 258.2 ✓

+67 6.6 258.3 ✓

+70 9.4 255.5 ✓

1+76 7.6 257.3 ✓

Rim 2.13 262.8
100.16.13 248.8

2+00 5.0 259.9 ✓

+50 3.5 261.4 ✓

+77 2.4 262.5 ✓

2+95⁴⁶ EC. 3.0 261.9 ✓

3+00 3.1 261.8 ✓

+3494 & PT. 3.0 261.9 ✓

+50 2.8 262.1 ✓

+74⁸² & PT 2.2 262.9 ✓

Nail in Pole 35' LT 1420

261.4 261.8 261.9
LEFT 3.5 3.1 3.0
Edge Road 10 7

1+16 36' LT WAT MET
30' LT 2" WAT

5.1 4.7 9.8
30' LT 1445 WAT MET Edge Road 7 10

24' LT 2+13 WAT MET

SEW. MH' 35' LT 0492

5.1 4.4 5.3
Edge Road 3 10

4.3 4.4 10
Edge Road 2

25' LT 2+90 WAT MET

3.6 7.1 10
Edge Road

3.2 2.3 3.0
4 6
Edge Road

2.7 1.7 2.2
3 10

1.7 2.4
7 10

Sycamore St
(Cont'd)
E Profile Proposed Water

6-9-52

14.

	264.90		
4+06 ⁵⁴ X PT	1.1	263.8	✓
9.07	273.85	0.12	264.78
4+50	8.2	265.7	✓
4+96 ⁵⁴ X PT	7.1	266.8	✓
	Rim 7.12	266.7	
	In. 22.12	251.7	
5+05 ³⁰ Sycamore	6.9	267.0	✓
5+72 ¹⁵ Shamrock	6.9	267.0	✓
5+50	Rim 6.56	267.3	267.29
	In.		
6+11 ⁸⁰ X PT	6.6	267.3	✓
+50	5.3	268.6	✓
7+00	3.7	270.2	✓
+39 ⁵⁰ B.C	2.1	271.8	✓
+10	2.2	271.7	
+41	3.0	270.9	
+50	3.0	270.9	
8+00	2.0	271.9	
+50	0.7	273.8	

LEFT 1.0 0.2
Edge Road 4

1.7 Right
8.3 8.0 8.0
Edge Road 2 3 10

SEW. M.H. 210 LT 4+96⁵⁴ RT GO TO FWD TAN

SEW. M.H. 120 LT 5+69

5+68 6' RT FENCE COR

5 RT 6+26
5 RT 6+58
Yard with new LAWN

4.2 3.4
Edge Road 5 4

2.2 2.0
Edge Road 2 3

4.7 2.7
8' RT 7+38
GUY POLE

7+87 29' LT.
WATER MET

3.2 2.6 3.5
Edge Road 5 4 10

SEW. M.H. 8+17 19' LT

2.2 1.8 2.5
Edge Road 4 3 10

1.3 0.9 0.9 5.0
Edge Road 5 4 2 10

Sycamore St.
(Cont'd)
E. PROFILE Proposed Water

		273.85		
8+73 ²⁸ EG.			3.5	270.4 ✓
TP	7.13	280.21	0.77	273.08
9+00			11.3	268.9 ✓
+10			11.0	269.2 ✓
+17			8.1	272.1 ✓
+50			6.1	274.1 ✓
+89 ²⁵			4.1	276.1
10+00			3.9	276.3
+15			3.7	276.5
SET TBM			1.66	278.55
		Rim Inv.	32.2	276.99
TBM	8.19	286.74	1.66	278.55
CK BM			0.35	286.39 = 286.38

6-9-52

15.

Edge Road 6 ^{1.3} 0.5 c 7.1

Edge Road 9 ^{2.5} 7.0 c 15.3

9+81 Edge 1" AC.

10+10 = Edge 1" AC

Top F.H. 12⁵⁰ RT 10+15 (SE Cor Sycamore Violet)

Jew M.H. 16⁰⁰ LT 10+00

Stub Tele pole 6 RT 10+16

F.H SE Cor Poplar & Violet

SYCAMORE ST
& Profile Cont'd

JUNE 23rd 1952 16

TBM	6.78	285.33	278.55
10+10'5	X PT		9.3 276.0
+50			8.2 277.1 ✓
11+00			7.0 278.3 ✓
+50			6.1 279.2 ✓
12+00			5.2 280.1 ✓
+50			4.9 280.4 ✓
13+00			4.7 280.6
+50			5.1 280.2
+88			6.5 278.8
+90			6.4 278.9
13+92			7.1 278.2
14+04.6			8.5 276.8
	Rim 5.52		279.81
	INV 17.32		
CK TBM	6.78		278.55

Top F.H. SE Cor Violet Sycamore

Guy Anc 6' RT 10+26

Wat Met 123 RT 10+27

GAS SER Xing 10+76
*72071 P. TEL P.M. 7' RT 10+77

GAS SER Xing 11+15

GAS SER Xing 11+55

GAS SER Xing 11+94

GAS SER Xing 12+35

*4081 P. TEL P.M. 8' RT 12+37

E Prop line Tubercose
6" SEW Xing 13+78
SEW MH 13+82 9' RT

Sycamore
 Snowdrop to Hollywood Park
 Profile

	+	H _i	-	
	0.95	288.84		287.89
0+00			8.8	280.0 ✓
+50			9.0	279.8 ✓
1+00			9.7	279.1 ✓
+50			10.7	278.1 ✓
2+00			10.1	278.7 ✓
+50			8.5	280.3 ✓
3+00			6.9	281.9 ✓
+50			6.1	282.7 ✓
4+00			5.7	283.1
+38 ⁹³			6.8	282.0
			0.95	287.89 = 287.89

West
 Kemp
 Wilson

June 9 52 18

*BM Fire Hyd SE Cor Popular + Hollywood
 0+00 at North Prop line of Snowdrop

Wilson

Tuberose St.
Poplar to Tuberose Lane
& Profile

July 10, 1952

19.

TBM	+	M.H.	-	M.H. RIM Sycamore and Violet
	9.56	284.95		276.99
0+00			4.7	279.8 ✓
0+50			6.8	277.8 ✓
1+00			7.5	277.1 ✓
1+50			8.4	276.2 ✓
2+00			10.8	273.8 ✓
-0+50			4.5	280.1 ✓
-1+00			3.7	280.9 ✓
-1+50			2.8	281.8 ✓
-2+00			2.3	282.3 ✓
-2+50			2.3	282.3 ✓
-3+00			2.5	282.1 ✓
TP-3+50	4.25	287.24	1.56	282.99 ✓
-4+00			3.5	283.7 ✓
-4+50			2.6	284.6 ✓
-5+00			1.2	286.0 ✓
-5+50			1.0	286.2 ✓
-6+00			0.5	286.7 ✓
-6+50			0.6	286.6 ✓

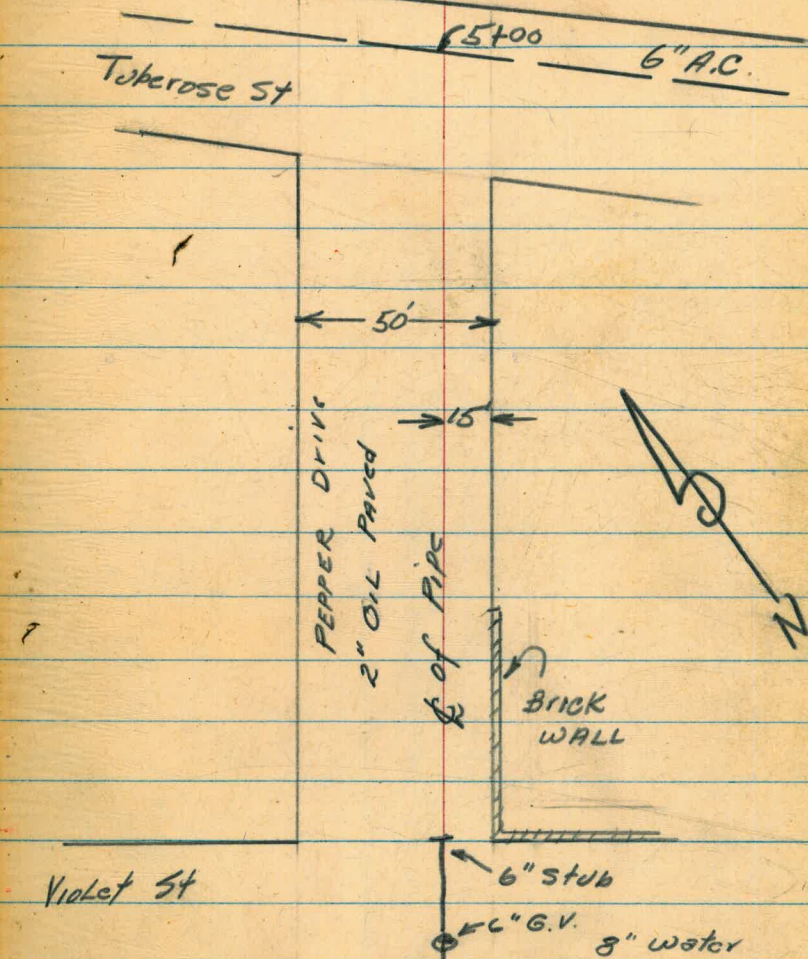
Note: This Rough Profile
was made by D. Wilson 6th
Floor so as to be included in
this particular group. The
center line of Profile is
Approx. only. Needs complete
survey. D. Wilson

Pepper Drive
 Profile Proposed 6" A.C.
 Violet to Tuberosa

T.B.M.	8.48	H.I. = 285.45	276.99
0+00		4.9	280.5
0+50		4.0	281.4
1+00		3.4	282.1
1+50		2.6	282.9
2+00		1.5	284.0
2+50		0.7	284.8
3+00		0.2	285.3
3+50		0.2	285.3
4+00		1.6	283.9
4+50		2.8	282.7
5+00		2.6	282.9

July 10, 1952 Bob Ebeling 20.

S.M.H. ON Violet & Sycamore



0+00 = W.P.L. of Violet,
 ⚠ Set over 6" G.V. @ Violet & Pepper 0+18

MALLARD ST
 SPRINGFIELD TO ALCEDO
 & PROPOSED WATER

SEPT. 14 1952 21

BEATTY
 POWELL
 ALEXANDER
 843807

MULBERRY
 (No Road)

NOT
 IMP.

UNIMPROVED
 ROAD.

0+00 to 17+83

7+20 W.M. 14' LT.

2" WATER

5+14 W.M. 17' LT.

PROPOSED WATER
 CITY OF SAN DIEGO
 COUNTY OF SAN DIEGO

SPRINGFIELD
 6" WATER

2x2 Hub

Off Edge

END 6" C.I. WAT 0+95?

0+9055

0+50 12' LT 9.5 W.M.

FH GV. 22' LT 0+26
 FH 26' LT 0+20

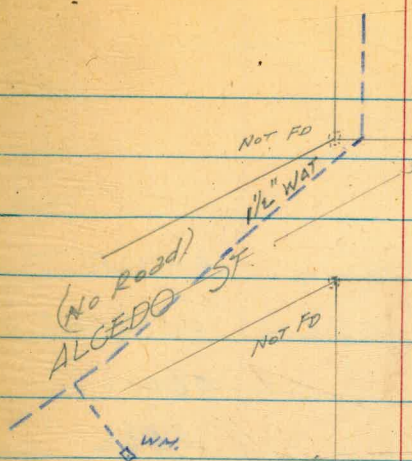
0+24 6" WYE 10' LT.
 0+00

2x2 Hub
 City Square

MALLARD ST
(Cont'd)

9-15-52

27



18+53

17+73.07

END 2" WAT. 12+26

WM 12+24 10' LT

W.M. 11+42 9' LT

CITY OF SAN DIEGO
COUNTY OF SAN DIEGO

F₂ 2+2
100
10' HOR

8+38.07

MALLARD ST
 SPRINGFIELD TO ALCEDO

SEPT. 15 1952

23

465.17

BM	1.86	465.72		463.86
TOM	1.17	463.58	3.31	462.41
0+00			3.4	460.1
+50			3.9	459.6
1+00			5.3	458.2
+50			5.5	458.0
2+00			5.2	458.3
+50			3.7	459.8
3+00			3.3	460.2
+50			8.4	455.1
IP	0.06	450.36	13.28	450.30
4+00			0.1	450.2
+50			3.4	446.9
5+00			6.9	443.4
+50			9.8	440.5
6+00			10.8	439.5
+50			10.3	440.0

Corc. Man NE Cor 69th & MALLARD

Top F.H. NE Cor Springfield & MALLARD

MALLARD ST
(Cont'd)

9/15/52

24

450.36

7+00 9.0 44 1.3

+50 6.4 44 3.9

8+00 5.1 44 5.2

+50 3.6 44 6.7

9+00 1.1 44 9.2

10+00 10.92 460.89 0.41 449.95

+50 8.5 45 2.3

10+00 3.5 45 7.3

11+00 2.32 463.18 0.03 460.86

+50 1.5 46 1.6

11+00 4.3 45 8.8

+50 10.6 45 2.5

12+00 0.35 450.19² 13.34 449.84

+50 2.2 44 8.0

+50 7.5 44 2.7

13+00 0.19 437.21 13.17 437.02

+50 0.6 43 6.6

+50 7.1 43 0.1

12+00 12.3 424.9

13+00 0.50 424.40 13.31 423.90

7.1 7.1 6.0 6.0
1 2 8

13.0 13.0 12.1 12.3 13.2
5 3 3 * 8

MALLARD ST
Cont'd

9/15/52

25

	424.40		3.1	421.3
14+50			6.7	417.7
15+00			9.0	415.4
+50			11.0	413.4
16+00				
H.P.	0.00	411.20	13.20	411.20
+50			20	409.2
17+00			7.1	404.1
H.P.	6.76	404.75	13.21	397.99
+50			7.5	397.2
+73.07			11.4	393.83
18+53			25.0	379.7
SET TOM	13.30	415.14	2.91	401.84
H.P.	12.98	428.00	0.12	415.02
H.P.	12.80	440.71	0.09	427.91
H.P.	12.75	453.24	0.22	440.49
H.P.	11.11	464.14	0.21	453.03
CK TOM			1.07	462.47 = 462.41

4.1 2.8 3.1
Edge Road 5 4
7.0 7.0 6.7 6.5
10 2 5

1.1 1.5 (E - Edge Road)

2.1 5.6 6.0
2 3 8

Edge
20

MALLARD

20' LT. To Inters'n Fly Line of Alcedo

20' LT. To " Fly Line " " " "

NAIL IN P. & TEL POLE # 271166 18' LT. 17+62

Top F.H. MALLARD & Springfield

MALLARD ST
(Cont'd)

9-22-52

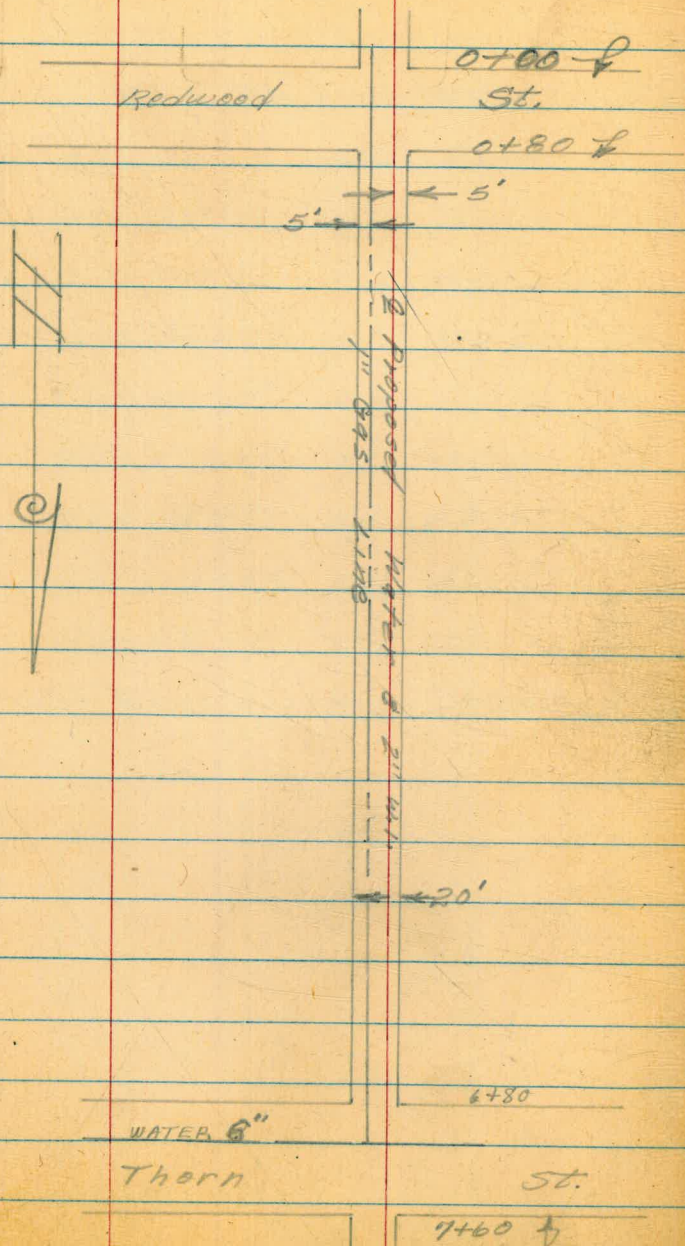
26

	+	-	Elev	
PM	9.60	354.37	344.77	CITY DOWNTOWN Top E. Radio Dr & ATTIX Dr
TP	12.76	366.79	0.34	354.03
	11.04	377.73	0.10	366.69
	13.16	389.11	1.78	375.95
	12.03	401.06	0.08	389.03
	12.23	413.09	0.20	400.86
	13.33	425.47	0.95	412.14
	12.84	438.12	0.19	425.28
	12.91	450.53	0.50	437.62
	12.86	462.42	0.97	449.56
TBM			0.01	462.41
				Top E. SE Cor Springfield & Mallard

Preliminary Alley Bk. # 9
 & Profile N. of Redwood, E. of Chamorro

Wilson
 Williams
 Jacobs
 Kemp

Oct. 21, 1952 27.



RIGHT

LEFT

S/L Redwood	0+00
N/L Redwood	0+80
	1+30 BUSH 3'
	1+51 P.P. 12'
	2+03 WAT.
	2+04 GAS
	2+05 WAT.
	2+38 WAT.
	2+47 WAT.
	2+57 P.P. 9'
	WAT. 2+86
	GAS 2+87
	2+90 WAT.
	3+00 GAS
	3+37 WAT.
	3+38 GAS
	4+09 P.P. 9'
	WAT. 4+10
	GAS 4+14
	4+19 WAT.
	4+29 GAS
	GAS 4+40
	WAT. 4+76
	GAS 4+85
	WAT. 5+02
	5+06 WAT.
	5+31 P.P. 9'
	WAT. 5+75
	GAS 6+62
S/L Thorn	6+80
	6+93 P.P. 14'
N/L Thorn	7+60

L Profile Alley Blk. #49

Wilson
Williams K
Jacobs 1st
Kemp 2nd

Oct. 22, 1952
28.

STA.	+	HI	-	Elev.
BM	2.28	335.24		332.96
7+60			5.0	330.2
7+00			5.8	329.4
6+80			5.1	330.1
6+50			5.3	329.9
6+00			5.8	329.4
5+50			6.6	328.6
5+00			7.3	327.9
4+50			8.1	327.1
4+00			9.3	325.9
3+50			9.8	325.4
3+00			11.3	323.9 323.9
2+50			12.3	322.9
TP	2.09	325.98	11.35	323.89
2+00			4.6	321.4
1+50			5.7	320.3
1+00			7.0	319.0
0+80			7.6	318.4
0+50			8.1	317.0
0+50			8.9	314.3
TP	9.81	335.09	11.6	323.28
TP			0.70	332.91
TP			2.12	332.91

N.W. B.P. Thorn & Chamoux

N. Prop. Line Thorn

S. Prop. Line

S. Prop. Line Thorn

Turn of Prop. Pipe (iron stake)

N. Prop. Line Redwood

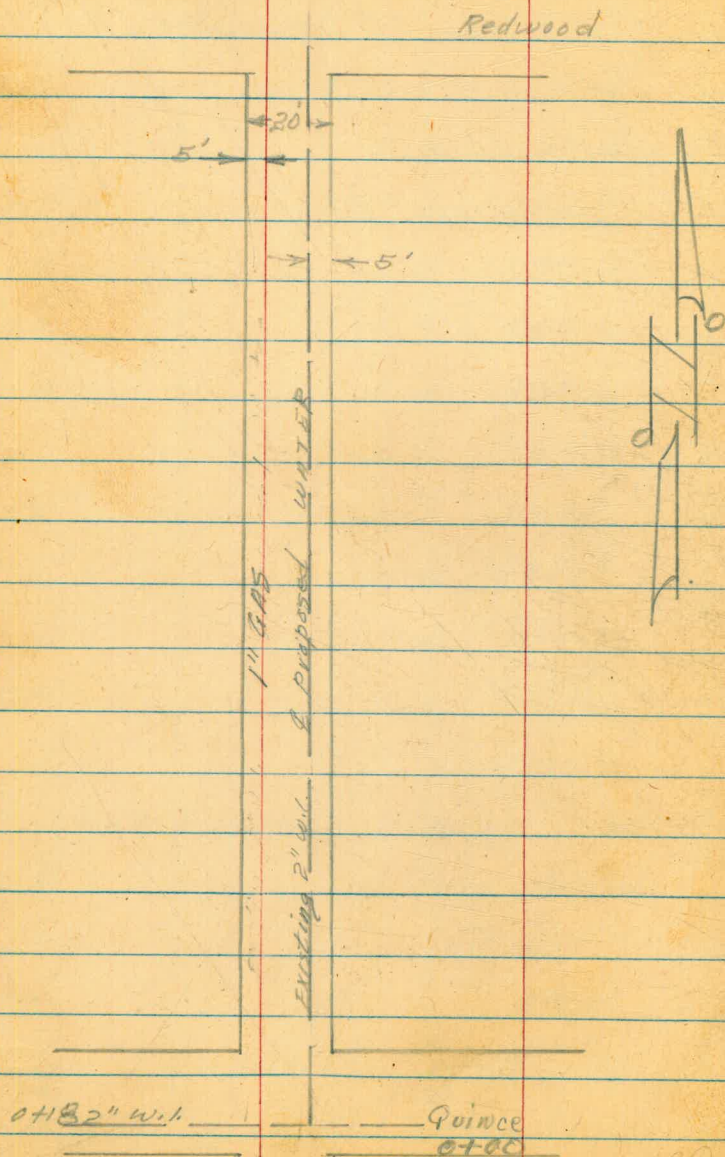
S. Prop. Line Redwood

CK. BM +.01 OK

E Proposed Water
 Alley Bk. #16
 N. of Quince E. of Chamouns

Wilson
 Williams
 Jacobs
 Kemp

Oct. 22, 1932 29.



WATER

LEFT

RIGHT

NORTH 6+04 PROP. LINE
 13' P.P. 5+40
 5+27 WAT. MET.
 SOUTH 5+24 PROP. LINE
 GAS 5+02
 GAS 5+00
 WAT. MET. 4+98
 4+07 GAS
 13' P.P. 3+99
 3+86 WAT. MET.
 3+60 GAS
 WAT. MET. 3+51 WAT. MET.
 4' 24" DIA. TREE 3+35
 3' 8" DIA. " 3+28
 2' 24" DIA. " 3+23
 6' 20" DIA. " 3+13
 6' 12" DIA. TREE 3+06
 3+03 GAS
 5' 14" DIA. TREE 3+02
 5' 9" DIA. TREE 2+99
 9' 9" DIA. TREE 2+95
 8' 15" DIA. TREE 2+91
 15' P.P. 2+80
 7' 8" DIA. TREE 2+72
 2+69 WAT.
 6' 12" DIA. TREE 2+68
 2+64 GAS
 13' P.P. 1+23
 WAT. MET. 0+81
 0+80 N. Prop. Line Quince
 0+18 2" W.I.
 0+16 P.P. 4'
 0+00 S. Prop. Line Quince

Alley Block # 16

Wilson
Williams
Jacobs
Kemp

Oct. 23, 1952 30.

	+	+	-	Elev
BM	1.60	325.49		323.89
TP	1.41	316.01	10.89	314.60
5+24			1.8	314.2
5+00			2.3	313.7
4+50			3.8	312.2
4+00			6.4	309.6
3+50			10.2	305.8
TP	1.72	306.58	11.15	304.86
3+00			7.00	299.6
2+50			5.4	301.2
2+00			11.1	295.5
TP	1.79	295.45	12.92	293.66
1+65			2.7	292.8
1+50			3.0	292.5
1+27			10.4	285.1
1+20			9.2	286.3
1+00			16.3	279.2
TP	1.49	284.37	12.57	282.88
0+85			10.8	273.6

Prop. (iron stake) E. side Alley # 9

Rock

S/L Redwood

LT.	2.8	7.3		
	10'	4'		RT.
	3.2	7.6		
LT.	10'	4'		RT.
	2.9	12.0		
	10'	5'		
	1.1	5.4		
LT.	10'	10'		RT.
	6.6	3.0	3.0	6.2
LT.	10'	4'	2'	7'
			10'	6.8
				RT.
	13.1	6.1		
LT.	10'	10'		RT.
	18.5	11.4		
LT.	10'	10'		RT.
	3.0	9.2		
LT.	10'	10'		RT.

Q Proposed Water
Alley Bk. # 6
N. of Quince E. of 44th

Wilson
Williams
Jacobs
Kemp

Oct. 24, 1952 32

Redwood

Q
WATER
LINE

LEFT

RIGHT

NORTH 6+07 PROP. REDWOOD

11' P.P. 57 57 2 DEAD MEN 8'

SOUTH 54 47 PROP. REDWOOD

WAT. MET. 54 37

WAT. MET. 44 97

12' P.P. 44 80

GAS 44 61

WAT. MET. 44 58

WAT. MET. 44 22

12' P.P. 44 15

GAS 34 35

WAT. MET. 34 25

10' P.P. 24 74

WAT. MET. 24 58

GAS 24 53

WAT. MET. 14 77 WAT. MET.

14 69 GAS

12' P.P. 14 26

14 12 GAS

FENCE 0+86 BARRICADE

NORTH 0+40 PROP. QUINCE

12' P.P. 0+12

SOUTH 0+00 PROP. QUINCE

Quince

Profit
Alley Block - 6.

Wilson
Williams
Jacobs
Kemp

Oct. 24, 1952 33.

BM	.97	323.56		322.59	N.W. B.P. Thorn & Highland		
TP	.88	311.52	12.92	310.64			
			4.82	306.70	Est. B.M. Top of Hydrant SE Thorn & 44 th		
TP	4.22	309.56	6.18	305.34			
TP	6.10	308.22	7.44	302.12			
			5.08	303.14	Est. B.M. L.T. N.W. Redland & 44 th		
TP	.84	296.63	12.43	295.79			
TP	.49	284.88	12.24	284.39			
H00			3.1	281.7			
0+50			14.5	270.4	LT.	16.6	
						10'	
0+40			18.0	266.9		262.7	16.5
						10'	4'
TP	.58	272.77	12.69	272.19			RT.
0+35			11.7	261.1			
0+30			15.0	257.8			
0+10			15.0	257.8	LT.	17.6	13.9
						10'	5'
0+00			21.0	251.8	LT.	23.5	19.0
						10'	5'
TP	12.95	281.23	4.49	268.28			
TP	12.37	293.33	.27	280.96			
H51			6.0	287.3			

Q Profile Alley Blk. #6

Wilson
Williams
Jacobs
Kemp

34.

293.33

2+00			2.8	290.5				
2+50			4.2	289.1				
3+00			3.0	288.3	LT.	2.3 10'	5.9 5'	RT.
TP	10.56	299.35	4.54	288.79		7.3 10'	10.5 5'	RT.
3+50			9.2	290.2	LT.			
3+63			5.9	293.5				
3+88			5.2	294.2				
4+00			7.6	291.8	LT.	5.6 10'	9.6 10'	RT.
4+50			6.6	292.8	LT.	4.2 10'	8.7 10'	RT.
5+00			6.3	293.1	LT.	2.9 10'	8.3 10'	RT.
5+47 ⁹³			6.5	292.9	5/2 Redwood LT.	8.9 10'	4.5 10'	RT.
6+07 ⁹³			8.8	290.6	N/2 Redwood LT.	10.8 10'	6.6 10'	RT.
TP	11.17	308.96	1.56	297.79				
			5.83	303.13	CK Est. B.M. Redland & 44 th			(-.01)
TP	6.99	310.66	5.29	303.67				
TP	11.29	315.40	6.55	304.11				
TP	9.25	324.05	.60	314.80				
			1.50	322.55	CK B.M. NW Thorn & Highland			-.04 OK

Proposed Water
 Alley Bk # 3
 N. of Redwood E. Highland

Wilson
 Williams
 Jacobs
 Kemp

Oct. 24, 1952 35.

THORN

LEFT

RIGHT

← 20' →
 → ← 5' →
 ← 5' →

6+07
 BRICK
 DRIVE
 WAY
 5+84

1" GAS
 2" W.I. & PROPOSED WATER



REDWOOD

14' NORTH 7+40 PROP. THORN
 P.P. 6+72
 SOUTH 6+60 PROP. THORN
 6+59 P.P. 4'
 6+25 GAS & WAT. MET.
 6+17 GAS
 6+07 END BRICK 8'
 5+95 WAT. MET.
 5+84 GAS BEGINNING BRICKS
 13' P.P. 5+60
 GAS 5+48
 WAT. MET. 5+45
 5+33 WAT. MET.
 5+10 P.P. 4'
 5+06 GAS
 4+88 ANCHOR-DM. 4'
 13' ANCHOR - D.M. 4+58
 13' P.P. 4+36
 3+97 CEMENT 4'
 3+91 SLAB
 3+84 GAS
 3+67 WAT. MET.
 15' P.P. 3+10
 WAT. MET. 2+44
 GAS 2+39
 1+92 WAT. MET.
 1+90 GAS
 12' P.P. 1+85
 GAS 1+48
 WAT. MET. 1+37
 NORTH 0+60 PROP. REDWOOD
 0+55 JUNK PILE
 15' P.P. 0+17
 SOUTH 0+00 PROP. REDWOOD

Profile
 Alloy B/4 # 3

Wilson
 Williams
 Jacobs
 Kemp

36

Sta	+ HI	-	Elev.
BM	7.82	330.41	322.59
7+40		5.2	325.2
7+00		6.0	324.4
6+60	SAME STA.	6.3	324.1
6"GV		7.6	322.8
6+50		5.0	325.4
6+00		5.4	325.0
5+50		7.0	323.4
5+00		8.5	321.9
4+50		10.2	320.2
4+00		11.9	318.5
TP	1.75	319.53	12.63 317.78
3+50		2.8	316.7
3+00		4.7	314.7
2+50		6.6	312.9
2+00		8.9	310.6
1+50		11.5	308.0
TP	.58	307.15	12.96 306.57
1+37		4.2	307.4

N.W. B.P. Thorn & Highland Sts.

N/L Thorn

Top of stem of G.V.

LT.

+2.8
7

RT.

Q Profile Alley Blk. #3

Wilson
Williams
Jacobs
Kemp

Oct. 24, 1952-32

307.15

1400			5.6	301.6
TP	102	295.99	12.18	294.97
0+50			3.1	292.9
0+25			7.7	288.3
0+00			17.1	278.9
TP	12.54	307.39	1.14	294.85
TP	12.16	318.70	.85	306.54
TP	12.55	330.29	.96	317.74
CK BM			7.71	322.58 =

5.6 6.9 7.3
0 4' 5' 10' RT.

9.5
0 10' RT.

13.0
0 10' RT.

-01 OK N.W. B.P. Thorn & Highland

Profile Alameda
Mallard to Mulberry
Transit Line on N.E. Prop. Line Alameda

West
Williams
Marshall
Varenforkis

38
8 Dec 53

	0.50	402.34		401.84
0+00		15.7		386.6
+30		9.5		392.8
+33		5.5		396.8
+40 ⁰²		3.7		398.6
+50		1.1		401.2
	8.87	410.31	0.90	401.44
1+00		1.1		409.2
	11.34	420.20	1.45	408.86
+10		9.0		411.2
+50		7.0		413.2
2+00		3.8		416.4
+50		4.2		416.0
3+00		6.2		414.0
+50		9.6		410.6
	2.09	412.69	9.60	410.60
4+00		6.0		406.7
+50		10.8		401.9
	1.71	401.33	13.07	399.62

TBM Spike in Pole	See page 25
of Mallard St	City County
Bottom Roadcut	10' East <u>WATER</u> <u>Prop. Line</u>
Top of Road Cut	396.7 390.9
South Prop. Line Mallard	5.6 <u>20' RT</u> 11.4 <u>60' RT</u> SW Prop. Line
	406.6 403.4
	3.7 <u>20' RT</u> 6.9 <u>60' RT</u>
1+00	411.6 408.5
	8.6 <u>20' RT</u> 11.7 <u>60' RT</u>
1+50	5.6 411.6 10.4 408.8
2+00	5.9 414.3 10.4 409.8
2+30	7.8 412.4 11.8 408.4
3+00	11.2 409.0 14.6 405.6
3+50	7.5 405.2 12.0 400.7
4+00	10.9 401.8 19.1 393.6
4+50	

E/W
Prop. Line

10' East
WATER

W/L
PROP.
LINE

5+00	401.33	8.1	393.2
3.15	391.73	12.25	388.58
+50		6.2	385.5
6+00		11.6	380.1
2.46	381.21	12.98	378.75
+50		4.8	376.4
+89 ²⁸		9.8	372.4
+99 ²⁸		10.2	371.0
+12.02	390.44	2.79	378.42
12.15	401.98	0.61	389.83
13.06	414.94	0.10	401.88
12.77	427.21	0.50	414.44
12.90	439.41	0.70	426.51
12.04	451.36	0.09	439.32
6.68	450.98	7.06	444.30
12.58	463.13	0.43	450.55
5.16	467.59	0.70	462.48
		3.71	463.88 =

463.86 Line Men NE Cor 69th & Mallard

391.2	
10.1	15.6 385.7
5+00	20.21 60' RT
8.3	383.4
5+50	20.21 60' RT
12.3	379.4
6+00	60' RT
13.1	378.6
6+00	20.21 60' RT
16.3	375.4
	60' RT
375.1	371.0
6+50	6.1
	20' RT
	10.2
	60' RT

1 Mulberry

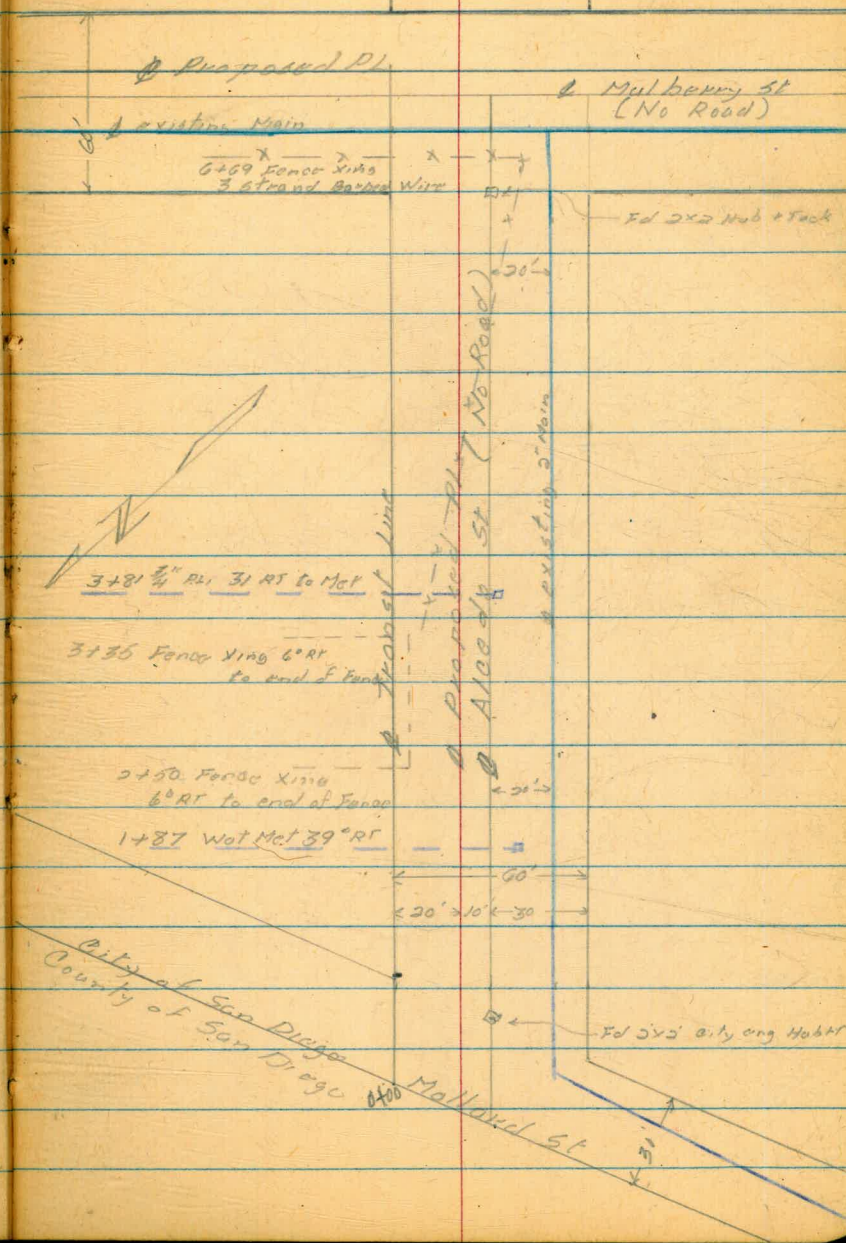
10' East of Mulberry & Proposed Pd.

6+99²²

Proposed Pl. Mulberry

6+89²²

Mulberry St



0+00

Mallard St City County Line

SHAMROCK ST.
 JUNIPER TO SYCAMORE
 (A) STKS & GRDS. FOR 6" WATER

APRIL 2 1953

41

BRATTY
 MARTELL
 ALEXANDER

TBM	122	267.90	266.68	Ret Sew M.H. (pg 7)
0+00 = 6" 10" C/I		Top Pipe 18.85	249.05	
0+05		13.3	254.6	GRADE Bottom Pipe 248.3 C62
0+09 B.C.		13.1	254.8	248.5 C63
+34		11.7	256.2	249.8 C64
+59	D=300' LT R=260'	10.7	257.2	251.1 C64
+84	E L=126' L=132'	9.9	258.0	252.4 C5E
1+09		9.7	258.2	253.6 C49
1+34		9.2	258.7	254.8 C39
1+43 ⁰⁴ E.C.				
1+50		9.0	258.9	255.8 C3L
2+00		8.1	259.8	256.5 C33
+50		6.7	261.2	259.1 C41
3+00		5.6	262.3	257.8 C43
+50		4.7	263.2	258.6 C48
4+00		3.8	264.1	259.1 C50
+50		3.0	264.9	259.7 C52
5+00		1.7	266.2	260.4 C52
① +50	4.77	271.90	0.77 267.13	261.0 C61

12.55
 5.3
 17.85

SHAMROCK ST
(Cont'd.)

4/2/53

42

271.90

5+793 GN. ENDWORK 5.7 266.2 261.4 C48
 5+843 = Y = (4+7346)
 CK TBM (Sycamore) 5.22 266.68 = 266.68 rim of Mt

WATER METERS) 4/3/53

TBM 2.45 269.13 266.68 BK of MET STD'd 25' DT & LT & ST
 (D) 5.82 265.48 9.47 259.66

1+430⁰⁴ EC. & of ST.

rad 105 = 5' off PL

1+085 W (2314 Shamrock) 7.3 258.2 257.6 C04

0+465 W (2310 ") 9.2 256.3 255.8 C05

1+20 E (2315 ") 5.3 260.2 257.9 C03

1+47 E (2322? No Number) 5.6 259.9 258.6 C13

1+78 W (2320 ") 6.2 259.3 259.5 F02

1+78 E (2333 ") 5.7 259.8 259.5 C17

2+12 W (2324 ") 5.2 260.3 260.2 C02

2+47 W (2332 ") 4.0 261.5 260.9 C06

2+92 E (2351 ") 2.2 263.3 261.8 C15

2+98 W (2342 ") 3.2 262.3 261.9 C04

3+34 E (2357 ") 1.6 263.9 262.3 C16

3+52 W (2348 ") 2.2 263.3 262.7 C06

(D) 6.10 270.28 130 264.18
 3+76 E (2403 ") 5.6 264.7 264.2 C15

3+78 W (2404 ") 6.7 264.1 263.2 C02

SHAMROCK ST.
(Cont'd.)

4/3/53

43

270.28

3+96 W (2410 Shamrock) 5.8 264.5 263.5 C10

4+06 E (2409 ") 4.7 265.6 263.7 C19

4+54 E (2415 ") 4.0 266.3 264.4 C19

4+68 W (2416 Shamrock) 4.5 265.8 264.6 C13

4+84 W (2424 ") 4.3 266.0 265.0 C10

5+47 W (2428 ") 3.1 267.2 265.6 C16

OK TBM 3.59 266.69 - 266.68

April 12, 1953

BEATTY
MARTELL
ALEXANDER

44

SYCAMORE JT
TULIP TO VIOLET
⑥⑩ STKS & GRDS FOR 6" WATER

BM1	3.69	265.76	262.07			
Nail in pole. Nly Inter's'n Tulip & Sycamore (pg. 13)						
0+69 ²	= Existing TEE 93° Nly of BG					
0+74 ²	= Begin Work					
	⑩	3.4	262.4	258.0	C44	
1+00		4.5	261.3	256.0	C52	
1+05	FH TEE		4.7	261.1	255.8	C53
1+50	B.C.		6.0	259.8	252.6	C52
1+75		6.2	259.6	252.7	C59	
	⑩	5.8	260.0		C49	
2+00	⑥	6.0	259.8	255.1	C47	
2+25		5.5	260.3	256.5	C38	
2+50		4.9	260.9	259.8	C31	
2+75		4.6	261.2	258.2	C32	
2+95 ⁴⁶	FC		4.3	261.5	258.5	C32
3+15 ⁵⁰	3 PT (22 1/2° RT)		3.7	262.1	258.8	C33
3+55 ⁵⁶	3 PT (22 1/2° RT)		3.4	262.4	259.4	C32
3+74 ⁵²		2.8	263.0	259.8	C32	
4+00		1.9	263.9	260.2	C37	
4+06 ⁵⁴	3 PT (22° 01' LT)		1.6	264.2	260.3	C39
4+50	6.36	271.92	0.20	265.56	261.0	C46
4+73 ⁴⁶	= Y (= 5+84 ³⁶ Shamrock)					
4+89 ⁸⁰	BK 3 PT (48° 21' LT)		5.1	266.9	261.7	C52
4+94 ³⁰	AH					
CK TBM		5.22	266.70	= 266.68		

SYCAMORE
Cont'd

4-16-53

46

276.95

9+50		2.9	274.1	2690	C51
9+64	End Work	2.2	276.8	2709	C37
10	5.54	2.24	274.73		
OK TBM		1.76	278.51 = 278.55		

Top FH, SE Cor Violet & Sycamore pg 15-16

WATER METERS & F.H.

TBM	6.47	268.54		262.07	Nail in Pole	
49' E Wly of PRC No. PL	3.9	264.6		262.5	C21	0+90 Nly
24' E W of PRC " "	5.4	263.1		262.1	C10	1+07 F.H.
2' Ely of PRC " "	6.5	262.0		262.0	C09	1+23 Nly
80' F of " " "	4.9	263.6		262.3	C13	1+54 Nly
88' E " " " "	4.5	264.0		262.4	C16	2+15 Nly
164' Ely of PRC " "	4.5	264.0		262.1	C19	2+20 Nly
41' Wly of PRC F.H.	12.2	256.3		261.2	F4 ⁹ TO FLANGE	2+88 Nly
12' Wly of EC NELY PL	3.9	264.6		263.7	C09	1+07 Sly
10	6.38	273.72	1.20	267.34		3+62 Ely
38' Sly of EC F.H.	6.53	266.8		267.0	F0 ² TO FLANGE C33	5+81 F.H. -
57' S. of EC	6.2	267.5		266.7	C08	5+65 Ely
46' Nly of EC	5.3	268.4		268.6	F0 ²	6+56 Ely
65' Nly of EC	5.7	268.5		268.9	F0 ⁴	6+90 Ely
77						

Sycamore St.
Cont'd

April 20, 1953

47.

BEATTY
MARTELL
ALEXANDER

TBM	6:16	284.71	278.55			
10+50	=	10' in Work (Ely P.L. VIOLET Nly SIDE Sycamore)	7.6 277.1	272.7	C44	
11+00			6.6 288.1	273.5	C46	
+50			5.5 279.2	274.2	C50	
12+00			4.9 279.8	275.0	C48	
+50			4.3 280.4	275.8	C46	
13+00			4.1 280.6	276.5	C41	
+25			4.3 280.4	276.9	C35	
+50			4.7 280.0	276.2	C38	
+81.70						
+82.2	=	5' from & water on Tuberosa	5.7 279.0	275.2	C38	
		WATER MET.				
0+00 - Prop line		Nly Sycamore				
10+60 Sly		(Ely Violet)	7.5 277.2	276.6	C06	4173 Sycamore
10+88.5 Sly			6.9 277.8	277.0	C08	4175 "
11+03 Nly			5.8 278.9	277.6	C13	4164 "
11+33 Sly			6.1 288.6	277.7	C09	4177 "
11+70.4 Sly			4.8 279.9	278.3	C16	4181 "
12+00 Nly			4.2 280.5	278.8	C17	4160 "
12+11 Sly			4.8 279.9	278.9	C10	4183 "
12+23 Nly			3.4 281.4	279.6	C18	4170 "
12+69 Nly			3.0 281.7	280.4	C13	4172 "
13+57 Nly			3.2 281.5	281.6	FOL	4190 "
					CK BYT	616 278.55

April 22 1953
BEATTY

49

TUBEROSE JT.

POPLAR TO TUBEROSE PL
④ STKS & GRDS. FOR 6" WATER.

BM							
71D	6.65	293.03		286.38		Top FH Violet & Poplar	Elev
	2.82	289.21	6.64	286.39			E PIPE
0+00 = at GL							283.0
0+05 90° BEND			3.0	286.2	282.9	C33	2.2
0+24 90° BEND			2.7	286.5	282.7	C38	2.7
0+50			2.7	286.5	282.5	C40	2.7
1+00			2.8	286.4	281.9	C45	2.8
1+50			3.2	286.0	281.4	C46	3.2
1+59.21 BC	$\Delta = 38.51$	(72.87 52.21)	3.1	286.1	281.3	C48	3.1
	$R = 192.35$						E
1+75	$L = 91.03$		3.2	286.0	281.2	C48	3.2
2+00			3.7	285.5	280.9	C46	4.8° 20'
2+25			4.1	285.1	280.6	C45	4.7
2+50.31 PRC.			5.0	284.2	280.4	C38	5.219 25' 30"
3+00			6.4	282.8	279.8	C30	C 00° 00' 00" 3.495
3+40 6" TEE			7.2	282.0	279.4	C26	6.5 2° 53' 12"
3+50			7.5	281.7	279.3	C24	6.8
4+00			6.9	282.3	278.8	C35	C 5° 28'
4+20.79 EC			6.7	282.5	278.5	C40	7.0 8° 43'
4+50			6.7	282.5	278.0	C45	7.0 9° 57'
5+00			7.1	282.1	277.2	C49	7.0
5+50			8.1	281.1	276.5	C46	7.3
71D	4.57	285.64	8.14	281.07			8.3

TUBEROSE ST.
(Cont'd.)

285.64

6+00		5.3	2803	275.7
6+50		7.0	278.6	274.9
6+72 (5) FH		8.31	277.33	278.4
6+75 ³ Cross		7.4	278.2	272.6
7+00		7.8	277.8	274.2
7+50		8.6	277.0	273.4
8+00		9.4	276.2	272.6
8+40	End Work	10.5	275.1	271.5 272.8
8+80	End Work	12.5	273.1	270.4 271.4
CK BM.		7.12	278.52	=278.55

C46 54
 C37 65
 FIL C25
 C36 69
 C36 76
 C36 84
 C36 91
 C36 104
 C27 123

Top FH VIOLET & Syasmore (pg. 16)

TUBEROSE ST.
(Cont'd)
WATER METERS

4/24/53

50

	4/ 289.21					
1+37 Fly	2.8	286.4	285.6	C08		2627 Tuberosa
1+71 Fly	2.9	286.3	285.4	C02		2621 "
2+12 Fly	3.2	286.0	285.1	C09		2615 "
2+55 Fly	5.0	284.2	284.6	F04		2609 "
3+94.5 Fly	8.8	280.4	283.6	F27		2559 "
4+05 Fly	6.4	282.8	282.5	C03		2551 "
4+90.5 Fly	6.6	282.6	281.7	C09		2549
5+35.5 Fly	} 7.75	281.46	280.9			2545
5+34.5 Fly			280.9	C06		2543
	4/ 285.64					
5+64 Fly	4.7	280.9	280.4	C05		No Number new house
6+12 Fly	5.0	280.6	279.6	C10		" " " "
6+45 Fly	8.0	277.6	279.0	F14		2529 Tuberosa
6+86 Fly	8.2	277.4	278.3	F09		2525 "
7+38 Fly	8.9	276.7	277.5	F08		2523 "
8+08 Fly	9.8	275.8	276.3	F05		2513 "
8+78 Swly	10.6	275.0	275.5	F05		2527 "
8+92 Swly	12.25	273.4	275.5	F21		2525 "

APRIL 30 1959

51

BETTY
MARTEL
ALEXANDER

PEPPER DRIVE

VIOLET TO TUBEROSE

④ GRADES & STKS FOR 6" WATER

TBM	7.51	286.06	278.55 286.38		Top FH VIOLET & Sycamore pg. 15-16 Top FH VIOLET & Poplar St pg. 7
0+55	FH TEE		5.0 281.1	277.5	c35
	⑤ FH		4.74 281.72	280.4	c38 to E11
1+00			4.56 281.5	278.2	c33
1+50			3.76 282.3	279.0	c33
2+00			2.96 283.1	279.8	c33
2+50			1.94 284.1	280.6	c35
3+00	6.72	291.63	1.15 284.91		c36
3+50			6.6 285.0	281.4	c36
4+00			5.3 286.3	280.9	c54
4+50			5.4 286.7	280.4	c58
5+00			7.6 282.0	279.9	c41
5+00 = End Work			8.9 282.7	279.4 273.0	c33 (see TEE 3+00 pg. 48 TUBEROSE)
5+02 1/2 = 22 1/2° Bend					280.1 Top TEE
5+05 1/2 TEE					11.5 279.4
			9.70	281.93	

PEPPER DRIVE

(Cont'd)

(2) STKS & GRDS FOR WAT. METS.

5-1-53

52

286.06

1+44 Sly	3.35	282.70	281.9	C08		
1+64 Nly	2.47	283.6	282.8	C08		
1+75 Sly	3.10	283.0	282.5	C05	4167	Pepper Dr
2+31 Sly	1.73	284.33	283.5	C08	4173	" "
2+53 Nly	10.6	285.0	284.5	C05	4176	" "
2+78 Sly	6.35	285.28	284.3	C12	4177	" "
3+01 Sly	5.9	285.7	284.7	C10	4181	" "
3+38 Sly	5.2	286.4	286.5	C19	4185	" "
3+60 Nly	4.8	286.8	286.3	C05	4186	" "
3+87 Nly	4.94	286.7	286.1	C06	4190	" "
3+90 Sly	5.3	286.3	285.5	C08	4191	" "
4+32 Nly	5.9	285.7	285.2	C05	4192	" "
4+62 Nly	6.71	284.92	284.4	C05	4198	" "

291.63

ALLEY BLK 55
 NOR of WIGHTMAN, EAST OF 38TH
 (5) STKS & GRDS for 6" WATER.

May 5, 1953

53

BM							GRADE FOR SAND BACK-FILL 0.6 Below EST. GRD		
	4.45	351.75	347.30		NW. CO. 39TH & UNIV.				
6+75	END WORK = 5 from GV	Exist. 4.2	347.6	342.2	C54	345.6	0.56	✓	
6+50		3.96	347.79	342.1	C57	346.2	0.00	✓	
6+00		4.80	347.0	341.9	C51	345.8	0.36	✓	
5+75		5.0	346.8	341.8	C50	345.3	0.86		
5+50		5.8	346.0	341.3	C47	344.8	1.36	✓	
5+00		6.75	345.0	340.2	C52	343.8	2.36	✓	
4+50		7.6	344.2	339.0	C52	342.8	3.36	✓	
4+00		9.65	342.1	337.9	C42	341.1	5.06	✓	
3+87		10.03	341.7	337.6	C41	340.5	5.66	✓	
TP	1.38	342.27	10.86	340.89					
3+37		2.7	339.6	334.6	C50	337.4	8.76	✓	346.16
3+00		6.96	335.3	331.0	C43	334.1	0.44	✓	334.50
2+50		11.15	331.1	326.0	C51	329.7	4.84	✓	
TP	2.10	331.26	13.11	329.16					
2+12		4.75	326.5	322.2	C43	326.4	8.12	✓	
1+87		5.9	325.4	320.4	C50	324.4	11.14	✓	
1+62		6.4	324.9	320.0	C49	323.5	11.04	✓	
1+37		6.86	324.4	320.4	C40	323.8	10.74	✓	
1+12		6.1	325.2	322.0	C32	325.6	8.94	✓	
0+80 = Nly Prop. line WIGHTMAN		1.8	329.5	325.0	C45	328.6	3.94	✓	
CK PD & Nail 0+80		2.07	329.19	329.19	pp. 75 F.B. 787				
						329.19 TP			
						324.35			
						324.30			
						11.82			
						324.30			
						324.30			
						324.30			

ALLEY BLK 55

5-13-53

52

(CONTD)

WAT. METS.

(Geos. Profile SHT. 617-A)

4) 6+50	3.25	351.04	347.79		
6+97 W 6+80		4.0	347.0	346.6	CO4
4+96 W 6+79		"	"	346.6	
4+95 W 6+78		"	"	346.6	
6+32 W.		3.2	347.8	347.5	CO3
5+84 E 5+86		4.2	346.8	346.8	CO0
5+82 E		4.1	346.9	346.7	CO2
5+81 W		4.3	346.7	346.6	CO1
5+67 W		4.6	346.4	346.4	CO2
5+54 E None Existing				346.1	
5+16 W None Existing				345.3	
5+09 W 5+10		5.8	345.2	345.1	CO1
5+09 E 5+10		6.0	345.0	345.1	FO1
4+50 W 4+55		7.2	343.8	344.0	FO2
4+49 E 4+52		6.9	344.1	343.9	CO2
3+99 W 3+99		8.8	342.2	342.1	CO1
3+60 W None Existing				340.7	
3+58 E 3+57		10.1	340.9	340.3	CO6
3+51 W		10.6	340.4	339.8	CO6
3+16 W 3+19		12.7	338.3	336.7	CO6
11) 3+16 E ✓	1.38	339.74	12.68	338.36	
			2.6	337.1	CO6
2+81 W 2+82		5.2	334.5	333.7	CO8
2+47 E 2+48		9.2	330.5	330.4	CO1
2+45 W		7.7	332.0	330.5	CO5

ALLEY BLK 55

(CONT'D)

WAT. METS.

339.74

2+15 E 2+16 13.1 326.6 327.5 FO⁹

2+05 W 2+06 13.2 326.5 327.0 FO⁵

TP 5.32 333.02 12.04 327.70

1+74 E 1+76 8.1 326.9 325.0 FO¹

1+23 E 1+24 } 8.3 326.7 325.7 } F1⁰

1+22 E 1+23 } 325.8 }

1+14 E 1+125 7.6 325.4 326.5 F1¹

CK TP 3.85 329.17 = 329.19

~~26 MET.~~

5/13/53

55

SUMAC DRIVE
 JUNIPER TO LAUREL
 (4) STRS & GRDS FOR 6" WATER

5/5/53
 BEATTY
 MARTELL
 ALEXANDER

56

TBM								
0-01	GV							
0+04	Begin Work	1.4	258.3	251.2	C71	Top G.V. Stem (FB 817 pg 49) El. 253.76 Bot. 10" C.I. Cross	VOID	4 pipe 55 E & ST
0+50		4.5	255.2	250.0	C52			4 pipe 70 E & ST
1+00		4.84	254.9	248.8	C61			4 pipe 10 E & ST
1+50		6.2	253.5	247.7	C58			
1+88		6.84	252.9	246.8	C61			
2+02.55	BC	6.94	252.8	246.8	C62			4 pipe 10' E & ST
2+50		7.04	252.7	246.8	C59	256.40 TD 7.51 263.91		
2+75		6.5	253.2	246.8	C64	11.40 252.51 Top 8" C.I. 251.8 Bot 8" C.I.	Relocated F.H.	261.40 @ 5+50 5.52
2+89.78	EC	5.6	254.1	247.2	C69	9.25 254.66 Top 10" Cross 253.76 Bot 10" Cross	266.92 H. 9.93 257.00 @ F.H. 259.2 Grd. F 23 to Flange C 25 to E.H.	
3+00		5.2	254.5	247.5	C70			
3+50	10.02	263.67	6.09	253.65				
4+00		5.6	258.1	250.3	C78			
4+50		4.67	259.0	251.7	C73			
5+00		3.0	260.3	253.1	C72	15.1	266.3	C70 To Flange
5+25	F.H. TEE	2.5	261.2	253.8	C74	Grd 259.3		C 12 E to EUL
5+50		2.3	261.2	254.5	C69			
5+53	F.H. TEE							
6+00		1.17	262.5	255.9	C66			
6+12		1.1	262.6	256.2	C64			
6+20	1/2" & Nail	5.32	267.97	1.02	262.65			
6+20 1/2"		5.2	262.8	256.3	C65			

SUMAC, DR
(Cont'd.)

5/6/53

57

		267.97			
6+20 ^{2d}	(22 1/2° Bend) Δ 25° 24' RT		256.3		
6+50	2.9	265.1	256.6	C85	
6+67 ¹⁷ 6+73 ²⁹	(22 1/2° Bend) Δ 26° 06' RT	4.7	263.3	256.8	C65
7+00	4.65	263.3	257.1	C62	
7+50	5.7	262.3	257.6	C47	
7+88	8" GN	7.2	260.8	257.5	C33
7+93	= 8" x 6" TEE		257.4 256.9		
CK (6)	6+58 ⁴⁵	7.16	260.81		

79
45
24
260.8
2.4
257.4

Bottom 6" Saw lat. 7+69
757.4
pipe laid below this

NOTE

8" x 8" TEE { STA. 6+63⁴⁵ M. DESTO
STA. 7+93⁰⁰ SUMAC.
EQUIV. { 8+13³⁹ BR. SUMAC
7+92⁵⁰ AN. 45° Bend

WATER METERS

5+81 E.	+44	6+00	266.9	260.0	C69
4+28 E.	+33	4+50	262.3	256.0	C63
3+98 W.	-23	4+00	255.8	253.8	C22
4+06 E.	+36	4+00	261.7	255.0	C62
3+61 E.	+41	3+50	260.1	253.8	C63
3+04 E.	+34	3+00	257.9	252.3	C56
2+55 E.	+23	2+50	255.0	250.5	C45
1+88 W.	-24	1+88	250.5	250.3	C02

61
581
00

2421

?

2402

2355

2347

2339

2333

2318

16 64
25 84
108

SYCAMORE DRIVE
 SNOW DROP TO HOLLYWOOD PARK
 (4) STKS. & GRDS for 6" WATER

May 6, 1953

58

BM	0.87	288.76	287.89		Top FH Poplar & Hollyweed
0+63 = G.V.	} BEGIN WORK 23' E SE Cor. Sycamore & Snowdrop				
0+68 =		8.4	280.4	275.2	C52
1+00		8.7	280.1	275.0	C51
1+60		10.27	^{278.45} 278.5	274.7	C38
2+00		10.77	278.0	274.4	C36
2+50		10.4	278.4	275.3	C31
3+00		7.36	281.4	276.3	C51
3+50		5.8	283.0	277.3	C57
4+00		5.7	283.1	276.6	C65
4+50		5.8	283.0	276.0	C70
4+85 F.H. TEE		7.6	281.2	276.6	C46
5+00 END WORK		7.84	280.9	275.4	C55
TD		8.47	280.29		

284.0
8.8
C

Curb 9rd

279.5

(5) 279.71

C03 Flange
C32 Bolt.

Sycamore Drive
Cont'd

May 11, 1953

59.

WATER METERS

P	6.17	284.66		278.49		
0+78 ⁵ Nly			2.5	282.2	279.4	C28 4202 Sycamore
1+09 Sly			4.8	279.9	279.2	C07 4205 "
1+23 ⁵ Sly			6.0	278.7	279.6	F09 4209 "
1+96 Nly			4.0	280.7	280.7	C02 4212 "
2+28 Nly			5.0	279.7	280.9	F12 No Address
2+34 Sly			6.4	278.3	280.5	F22 4217 "
2+68 Nly			4.4	280.3	281.3	F10 4218 "
2+93 Sly			4.0	280.7	281.1	F04 4227 "
D	7.18	289.92	2.92	281.74		
3+47 Nly		288.92	5.7	284.2 283.2	282.0	E12 4226 "
3+92 Nly			5.3	284.4 283.6	281.9	C17 4230 "
H 4+79 Nly			4.5	285.4 284.4	280.3	C41 4238 "
5+00 Nly			5.3	284.6 283.6	279.7	E3? 4244 "
(5) FH			9.15	280.77 279.77		
CK (2) 4+50			6.0	283.9 282.9	283.0	
CK (2) 4+00			5.9	284.0 283.0	283.1	
			10.41	278.51 279.51		

64TH ST.
AKINS TO BROOKLYN
(5) STKS. & GRDS. for 6" water

May 11 1953

BRYAN
MARTIN
ALEXANDER
VARDY PAVES

60

BM							
BM	1.21	213.89		212.68		Top F.H. 63 rd & Imperial	
CK BM	2.32	211.35	6.86	207.03	203.71	Mon 64 TH & AKINS.	
0+30 ³⁶		Begin work	(w 6.2	205.2)	200.8	C44	
			(E 6.2	205.2)		C43	
0+55		STR'D 5+164	(w 6.65	204.7)	201.0	C37	
		F.H. TEE	(E 6.2	205.0)	201.4	C40	
0+75		AKIN ST. FB 86 ²	(w 6.15	205.2)		C38	{ & pipe offset 05
0+90		199 6	w 5.65	205.7	202.7	C39	" " " 20
1+00			5.4	206.0	202.9	C21	" " " 40
		(Elev. Top Sill	6.85	202.5)	204.5		" " " 60
1+05	22 1/2°	BEND	5.2	206.2	204.2	C17	" " " 60
		(Elev. Top Sill	6.85	204.5)	204.5		" " " 60
1+51	22 1/2°	BEND	4.9	206.5	204.2	C20	" " " 20
1+65			5.25	206.1	203.2	C29	" " " 00
1+80			6.05	205.3	201.0	C43	
2+12			6.85	204.5	199.2	C53	
2+50			6.35	205.0	199.7	C53	
3+00			3.95	207.4	202.5	C49	
3+50	13.29	224.24	0.36	210.95	208.8	C43	
4+00			1.4	222.8	217.3	C55	
4+50	13.01	237.12	0.11	224.13	225.8	C62	
4+80			1.04	236.1	231.0	C51	
5+12	10.69	247.78	0.05	237.09	234.5	C50	
5+50			6.3	241.5	234.8	C67	
5+86		F.H. TEE	5.25	242.5	235.1	C74	{ El. 242.13 GRD 239.4 C42 to Flange
6+00			5.07	242.7	235.3	C74	{ 365 C82 to Ell.
6+50			5.3	242.5	235.7	C68	

5/12/53

61

64TH ST.
(CONT'D)

247.78

7+00		6.00	241.8	236.2	C56	
7+25		7.07	240.7	235.5	C52	
7+50	0.26	235.7d	12.33	235.48	232.6	C29
7+88		11.45	224.3	222.0	C23	
8+12		10.06	225.68	222.0	C37	
8+62		2.73	233.0	228.6	C42	
8+70	End Work	0.9	234.8	230.2	C46	
SETTDM		3.35	232.39		Top 18" RCP.	

WATER METERS

GRADE From 3568-Profile.

1+90 Ely	Ni	211.35	7.85	203.5	206.0	F25	521	64 TH
2+04 Ely	"		7.7	203.7	205.6	F19	525	"
2+37 Wly	"		6.5	204.9	205.3	F04	526	"
3+32 Ely			1.8	209.6	210.6	F10	607-609	"
3+63 Wly	Ni	224.24	9.00	215.2	214.8	C06	622	"
4+27 Wly	Ni	237.14	9.0	228.1	227.4	C07	664	"
4+82 Wly	"		1.64	235.5	235.4	C01	642	"
5+06 Ely	Ni	247.78	8.10	239.7	237.5	C12	641	"
5+22 Wly	"	"	8.7	239.1	238.6	C05	650	"
5+62 Ely	"	"	4.76	243.0	239.3	C37	651	"
6+08 Ely	"	"	4.4	243.0	239.6	C38	705	"
6+94 Ely	"	"	5.6	242.2	240.0	C22	727	"
7+29 Ely	"	"	5.6	242.2	240.0	C22		

C42 - MET. DN & Property - Vacant

PODDY PLACE
 MANZANITA DR. TO MANZANITA DR.
 (A) STR. S & GRDS FOR 6" WATER

May 12, 1953
 BEATTY
 MARTELL
 ALEXANDER
 VANDERFAKES

62

TBM						
	0.79	281.74		280.95		Top FH MANZANITA & VIOLET (FB 817-53)
TP	7.72	285.41	12.04	277.69		Rim of Sew M.H. 0425
0+34.5	6" TEE BEGIN WORK		8.6	276.8	271.2	C56
0+50			8.4	277.0	271.4	C56
0+55	F.H. TEE		8.3	277.1	271.5	C56 (5)
1+00			9.4	276.0	271.9	C41
1+50			9.0	276.4	272.4	C40
2+00			8.1	277.3	273.0	C43
2+30.89	2 PT. (11/4")		7.7	277.7	273.3	C44
2+60	2 PT. (47'00)		7.8	277.6	273.6	C40
3+00			6.6	278.8	274.1	C47
3+13.80	2 PT. (47'09)		6.6	278.8	274.3	C45
3+43.0	2 PT. (11/4")		6.0	279.4	274.6	C48
3+75			5.8	279.6	275.0	C46
4+00			5.4	280.0	275.9	C45
4+50			4.3	281.1	277.7	C34 & pipe 10' sly & st.
5+00			2.2	283.2	279.5	C37 -0.8 282.4 C29 & pipe 7' sly & st.
5+27	End Work				280.6	
5+50			6.5	282.9	281.3	C36 -1.3 283.6 C30 & pipe 5.3 sly & st.
5+32	Existing G.V.					
TP	7.62	291.66	1.37	284.04		
			3.35	288.31		Top FH Violet & MANZANITA
			5.23	286.43 = 286.38		" " " & Poplar

132/4.70
 506
 7.40
 7.3
 37
 -36
 284.9
 3.6
 281.3
 280.6

5/13/53

67.

POPPY PLACE
(Cont'd)
WATER METERS

B.M.	6.75	284.44	277.69	Run Sew Mt-H	
1+32 Ely.	5.3	279.1	276.6	C25	4010 Poppy
1+66 Ely.	4.6	279.8	276.8	C30	4020 "
2+17 Ely.	4.2	280.2	277.1	C31	4028 "
2+11 Wly.	7.9	276.5	276.7	F02	4025 "
2+52 Wly.	7.3	277.1	277.3	F02	4029 "
2+86 Sly.	6.7	277.7	277.8	F01	4033 "
3+33 Sly.	5.4	279.0	278.7	C03	4045 "
4+82 Nly.	1.4	283.0	282.7	C03	4050 "
5+17 Sly.	0.9	283.5	284.3	F08	4063 "
0+55 (5) F4	11.2	273.2	275.1	F19 to HANGE	C20 F16
ck @ 4+50	3.40	281.04	= 281.1		

62

78

4

May 20 1953

64

SUMAC DRIVE & LAUREL ST.
 JUNIPER TO LAUREL
 Cont'd from p. 57

TBM.	0.53	268.93.	268.40	NAIL IN Pole SUMAC & Laurel FB. 817 pg 51	(see pg 57 for Equation)
8+1322 BK 9+925 AN (45° Bend)			257.1		
7+95	7.8	261.1	257.1	040	
8+25	8.6	260.3	256.5	038	
8+75	8.0	260.9	257.2	037	
9+25	6.1	262.8	259.3	035	
9+5905 BC	4.3	264.6	260.7	039	
9+7365 8x6 TEE = (2497.25 Laurel)	3.3	265.6	261.3	042	
9+75	3.2	265.7	261.4	042	
10+00	2.2	266.7	261.9	048	
10+25	1.2	267.7	262.4	053	
10+50	Ⓐ 0.5 Ⓑ 0.1	268.4 268.8	262.9	055 057	
10+75	6.98	275.76	0.15 268.78 4.9 270.9	074	
10+810 P.R.C	4.7	271.1	269.7	074	
11+00	5.0	270.8	264.1	067	
11+28 FH TEE	4.5	271.3	264.7	066	276.95 6.65
⑤ FH	3.45	272.3	266.5	038 076 E EII	272.3
11+310 FC			264.8		
11+50	4.0	271.8	265.8	066	
12+00	3.6	272.2	266.2	062	

JUMAC DRIVE & LAUREL ST.
(Cont'd.)

5/21/53

65.

	+85.4	275.76	- F.S	Elev.		
12+15 ¹⁸	BC		4.1	271.7	266.6	C51
12+50			2.2	273.6	267.3	C63
13+00			1.0	274.8	268.3	C65
P	11.69	285.68	1.77	273.99		
13+50			11.2	274.5	269.4	C51
13+81 ⁹³	EC		11.0	274.7	270.1	C46
14+00			10.8	274.9	270.5	C44
14+25			10.1	275.6	271.0	C46
14+54 ⁸³	POT. (EC of Road)		9.5	276.2	271.6	C46
14+84 ³⁶	X PT 22 1/2° Bend		9.0	276.7	272.2	C45
15+13 ⁹⁰	X PT 22 1/2° Bend		6.9	278.8	272.9	C60
15+44 ⁵⁰	X PT 22 1/2° Bend		4.8	280.9	273.4	C75
15+74 ⁰²	POT (EC of Road)					
15+81 ⁵²	- E Alley S. Rim M.H.	3.6	282.1	274.2		C79
		3.37	282.31			
16+00		3.0	282.7	274.4		C83
16+50		3.2	282.5	274.9		C76
17+00		5.3	280.4	275.4		C50
17+56	= End Work = 5' from 8" MAIN	6.1	279.6	276.0		C96
17+61	= TEE					
P	0.06	279.33	6.41	279.27		
P	5.83	272.19	12.97	266.36		

15+20 to 15+30 SEWER Confliction
see pg 68 for elev. Top. Sewer

LAUREL ST.
FAIRMOUNT TO SUMAC.
② STKS & Grds for 6" Water

272.19

0+00 = 8x6 Cross			260.5		
0+05 = Peg in Work	8.7	263.5	261.5	C30	
0+50 = (w/ly Prop line Fairmt)	8.5	263.7	260.7	C30	
0+55 F.H TEE	8.4	263.8	260.8	C30	
③ FH	4.1	268.1	264.5		C36 TO FLANGE C73 TO POTH. E11. 4/10
1+00	8.0	264.2	261.1	C31	
1+50	7.4	264.8	261.2	C36	
2+00	7.1	265.1	261.3	C38	
2+50	7.1	265.1	261.3	C38	
3+00 P.R.C	6.6	265.6	261.3	C43	
3+50	6.2	265.8	261.3	C45	
3+92.25 = 5' from 8x6 TEE	6.8	265.4	261.3	C41	
3+97.25 = 8x6 TEE (9+73.65 SUMAC)			261.3 262.2	(See pg 64.)	
CKTBM	3.78	268.41 = 268.40		NAIL IN POLE	

SUMAC & LAUREL
Cont'd
WATER METS

5/29/53

67

70M	221	270.61	268.20				
7+20 = BC							
7+32 Nly	(14' Fly of BC)	8.5	262.1	261.3	C08	2448	SUMAC
7+44 Sly	(24' Fly of BC)	6.6	264.0	262.0	C20	2433	"
7+70 Nly	(50' Fly of BC)	9.0	261.6	261.7	F01	2452	"
8+30 Wly	(129' Sly of BC)	8.9	261.7	262.4	F07	2460	"
8+45 Fly	(114' Sly of BC)	10.2	260.4	262.1	F27	2459 & 2461	
8+67 Wly	(92' Sly of BC)	8.8	261.8	262.2	F14	2464	SUMAC
9+12 E	(47' Sly of BC)	8.9	261.7	264.5	F28	2469	SUMAC
9+26 W	(33' Sly BC)	7.8	262.8	264.4	F16	2468	SUMAC
(9+59 ²⁵ BC E&W)							
(10+81 ⁰ EC E&W)							
						268.4	
						1.3	
						267.1	
10+53 Wly	(28' Sly PRC)	3.9	266.7	266.8	F01	2504	" or LAUREL
10+00 ⁶⁵ Ely	(6' Wly Sly line Lot 11)		267.1	266.2	C09	2302	LAUREL
10+81 Ely	(999 PRC)	+08	271.40	267.6	C38	2503	LAUREL
11+03 ^E Wly	(22 ^E Nly PRC)	3.7	266.9	267.9	F10	2508	"
11+11 Ely	10.55	278.95	2.21	268.20	C42	2511	"
11+59 Fly		6.6	272.4	268.2	C33	2517	"
11+87 ^E Ely		6.45	272.5	269.2	C79	2525	"
12+41 Fly		6.25	272.7	270.8	C35	2535	"
12+68 Fly		4.65	274.3	271.4	C32	2539	"
13+09 Fly		3.25	275.7	272.2	C35	2521	"
13+72 Ely		4.0	275.0	273.4	C16	12555	
(13+81 ⁷⁵ EC)	9.67	284.51	4.11	274.82			

LAUREL ST.
(Cont'd)

WAT MET. 5

284.51

14+15 Fly	7.10	277.0	274.5	C22	2569 Laurel
14+54.83 (oc. Road)					
14+61 Sely	6.9	277.6	275.4	C22	2573 "
15+13 Nly	7.0	277.5	276.3	C18	2562 "
15+24 Nly	5.3	279.2	276.5	C27	2574 "
15+50 Nly	2.7	281.8	276.9	C49	2588 "
(6) 15+00.50	3.67	280.84	= 280.9		
Laurel St. N ₁ 270.61					
2+45 Nly	5.8	260.8	265.6	F08	4320 "
2+66 Sly	4.1	266.5	265.5	C10	4321 "

Top Existing 8" SEWER

	284.50			Top 8" C.1	
15+44.50 Top 8" SEW	11.40	273.1	274.8		
15+20 " " "	11.00	273.1	274.7	(15+32)	
15+04 end 8" C.1 as laid	12.1	272.4	274.0		
			273.6		

6/1/53

68.

STORK ST.
IMPERIAL TO BROOKLYN
⑤ STRS & GRDS. for 6" WATER

May 22, 1953
BEATTY
WARTELL
ALEXANDER

69

BM.		0.32	213.00		212.68		Top F.H. 3E Cor 63rd & Imperial (Fig 824 pg 13)
0+26	Beginning Work	3.7	209.3	205.5	C38		
0+40		3.65	209.35	201.3	C805		209.0 8.7
0+50		4.0	209.0	201.8	C72		200.3 205.5 201.52 (.2146 21.606
0+75		3.9	209.1	203.0	C61 ✓		20 20 200 100
0+90	encased	4.8	208.2	202.7	✓C55 } C58	} 16" steel.	2.7
1+30		6.6	206.4	201.9	C45 } C48		10.8% 32.7
1+40		7.3	205.7	201.7	C40		209.1 3.8
1+75		9.2	203.8	198.5	C53		205.3 Top 36" 2.6
1+97	6" Cross	11.3	201.7	196.4	C53		201.7 1.5
2+00		11.6	201.4	196.4	C50		
2+22	1/6	12.2	200.8				
2+19	FH TEE	201.64	12.52	200.48	196.6	C39-C42	GRD 201.4 EL 201.3
2+50		1.3	200.3	196.8	C35		
3+00		3.8	197.8	192.0	C38		
3+50		4.1	197.5	191.2	C63		
3+87		5.4	196.2	191.2	C50		
4+25		0.6	201.0	195.2	C58		
4+50		1.2	200.4	196.2	C42		57 49
4+00	9.01	210.54	0.11	201.53			.8
5+00		8.2	202.3	198.2	C41		

3/22/53

70.

STORK ST.
(Cont'd.)

		210.54							
5+50			6.3	204.2	200.2		C40		
6+00			2.9	207.6	203.9		C37		
6+13 F.H. TEE	12.96	222.67	0.83	209.71	204.9		C42		
6+25			11.8	210.9	205.8		C51		
6+50			8.9	213.8	209.7		C41		
7+00	12.73	235.03	0.37	222.30	217.4		C29	OK	
7+50			4.3	230.7	223.2		C55	C75	
8+00	13.03	247.60	0.87	234.56	229.0		C37	C77	
8+50	3.03		5.6	242.0	232.3		C41	C77	
9+00	9.45	256.89	0.16	247.44	239.6		C52	C78	
9+50			4.6	252.3	244.9		C53	C74	
10+00	12.88	269.49	0.28	256.61	250.2		C50	C69	
10+50			9.2	260.3	255.5		C41	C48	
11+00	(END WORK)		5.1	264.4	260.8		C36	OK	
11+30					264.0				
CK BM			0.47	269.02	269.02				

5/25/53
RENTY

Grade Change
due to incorrect
est grade.

Top F.H. SE Cor Brooklyn & Stork

5/25/53

71

STARK ST
(Contd.)② STKS. & GRD for
WAT. METS

	No	Existing MET				
2+58 E	No	Existing MET	200.3	201.0	F01	
3+80 W	No	Existing MET	193.2	201.0	F78	
4+62 E	+0.3	4+50	200.7	202.7	F70	
4+61 W	0.0	4+50	200.4	202.6	F22	604 STOK
5+31 E	-0.5	5+50	203.7	206.2	F25	619 "
5+57 W	+0.1	5+50	204.3	208.0	F32	608 "
5+88 E	-0.6	6+00	207.0	210.5	F35	627 "
6+92 E	-0.1	7+00	222.2	221.4	C08	657 "
8+11 E	+2.2	8+00	238.9	233.7	C32	(?) 645 "
8+67 W	-2.4	9+00	245.0	240.1	C51	No Number
8+86 E	-1.2	9+00	246.2	242.1	C41	709 "
9+70 E	-1.7	10+00	254.9	250.7	C42	731 "
9+88 W	-0.3	10+00	256.3	252.6	C32	732 "
11+06 E	+1.5	11+00	265.9	266.0	F01	709 "

May 27 1953

72

BRATTY,
MARTEL,
ALEXANDER.

NARANJA ST.

EUCLID To 54TH ST.
⑤ STKS & GRDS FOR 6" WATER

BM.							
	7.60	112.05		104.45		BP. on Bridge EUCLID S of MARKET	
0+40	8" x 6" TEE		4.65	107.4	103.2	Grade Bottom Pipe	C42
0+45	Begin Work		5.0	107.1	103.1		C40
0+85	F.H. TEE		5.5	106.6	102.8	GRD 107.6	C38
	⑤ F.H.		5.2	106.9	107.6	106.9	C4 L Bot Ell.
1+00			5.4	106.7	102.6	Flange FO 2	107.6 106.7 FO 9 To #
+50			4.4	107.7	104.0		C37
2+00			1.5	110.6	106.4		C42
①D	10.15	121.82	0.36	111.69			
+50			9.6	112.2	107.8		C44
3+00			8.1	113.7	109.2		C45
+50			6.9	114.9	110.6		C43
4+00			5.6	116.2	112.0		C42
+50			4.0	117.8	114.5		C33
①D	12.01	133.11	0.71	121.10	117.0		C41
+50			7.7	125.4	119.5		C59
6+00			5.8	127.3	122.0		C53
+50			5.0	128.1	123.6		C45
+90	F.H. TEE		4.65	128.45	124.0	GRD 129.65	C45
	⑤ F.H.	(24.5 from #5)	3.26	129.65	128.2	128.2	C145 Flange 5.65 To Ell.
7+00			4.5	128.6	124.1		C45
+50			2.1	129.0	124.6		C44

128.1
0.5
128.6 C04

5/27/53

73.

NARANJA ST.
Cont'd.

	133.11					
8+00		3.5	129.6	125.1	C45	
+50		2.7	130.4	125.6	C48	
9+00		1.7	131.4	126.2	C52	
P +50	7.74	140.53	0.37	132.79	126.7	C61
10+00		6.85	133.7	127.2	C65	
+50		5.8	134.7	127.7	C70	
11+00		5.0	135.5	128.2	C73	
+50		4.9	135.6	128.7	C69	
12+00		5.7	134.8	129.2	C56	
+50		6.5	134.0	129.7	C43	
13+00		6.7	133.8	130.2	C36	
+50		5.7	134.8	130.7	C45	
+60	6" TEE	5.3	135.2	130.8	C44	
13+88	FH TEE	4.1	136.4	131.1	C53	
	(5) FH	3.2	137.3	135.0		
14+00		3.2	137.3	131.2	C61	
P +50	4.25	142.34	2.44	138.09	131.7	C74
			3.2	139.1		
15+00		1.75	140.6	132.2	C84	
+50		1.8	140.5	131.8	C87	
+75		2.0	140.3	131.6	C87	

GRD 137.3
135.0
C 2.3 RANGE C63 Bottom Ell.

5/27/53

74

NARANJA ST.
(Cont'd.)

	142.34				
16+15	5.65	136.7	130.5	C62	
16+55	8.55	133.8	129.4	C44	
End Work	8.91	133.42 = 133.45			edge part (Fig. 811 129 45)
	9.27	133.07			S. rim of M.H.

WATER METERS

						Naranja
2+56 So.	+0.7	2+50	112.9	111.8	C12	
6+68 So.	+0.1	6+90	128.6	127.9	C07	5193 "
7+19 Nor	0.0	7+50	129.0	127.9	C11	5252 "
9+25 Nor	+0.1	9+00	131.5	129.9	C16	5260 "
10+67 Nor	+0.3	10+50	135.0	131.4	C36	5256 "
13+01 So	+0.2	13+00	134.0	134.7	F07	
13+97 So	0.0	14+00	137.3	135.0	C23	5305 "
14+63 So	+1.1	14+50	140.2	135.7	C45	5315 "
15+05 Nor	0.0	15+00	140.6	135.8	C48	5324 "
15+46 So	+0.9	15+50	141.4	135.8	C56	5325 "
15+92 Nor	-0.4	15+75	139.9	135.6	C43	5320 "

62ND ST.

AKINS To BROOKLN

③ STKS. & GRDS FOR 6" WATER

BM _{TD}	1.30	213.98	13.22	212.68	
BM	0.23	200.99		200.76	
TD	7.84	195.67	13.16	187.83	GENE
2+00	6 TEE	Begin Work	8.2	187.5	184.0
+29					
+24	F.H. TEE		8.35	187.32	183.4
	⑤ F.H.		8.3	187.37	191.3
+50			8.1	187.6	184.2
+75			7.35	188.3	185.9
3+00			6.4	189.3	185.0
				187.8	187.8
				185.8	185.8
+125	1 1/2 Bend	not necessary	4.8	190.9	188.4
				186.37	186.5
				188.30	
+58.5	1 1/2 Bend	Top Basin 7.30	4.9	190.8	188.4
		Top Basin 7.37			188.5
+75			6.3	189.4	187.8
4+00			6.6	189.1	186.3
				186.1	186.0
+25			6.9	188.8	185.6
+50			6.4	189.3	185.2
5+00			4.6	191.1	187.1
TD	12.71	207.88	0.50	195.17	191.3
+50			11.3	196.6	195.5
6+00			5.98	201.9	199.8
+50			2.08	205.8	204.0
TD	19.24	221.12	0.00	207.88	207.1
7+00			11.4	209.7	212.65
40			8.1	213.0	208.2
+37	F.H. TEE		8.02	213.1	
	⑤ F.H.		7.2	213.9	
+50					

May 27, 1953

BEATTY,
MARTEL,
ALEXANDER.

75

Top F.H. 63rd & Imperial SE Cor
Harkins pole NW Cor 62nd & Imperial

C35		& pipe 10' Ely & St.
C39	F.H. 21.5 from & St.	
C39	F39 Flange C40 to E11.	& pipe 10' Ely & St.
C34		" " 25' " " "
C30		" " 10' " " "
C15		
C25		& pipe 11.5 Ely & St.
C24		& pipe 11.5 Ely & St.
C16		" " 9.8 " " "
C30		" " 7.5 " " "
C32		& pipe 5' Ely & St.
C41		& pipe 5' Ely & St.
C40		
C53		
C64		
C60		
C57		
C59	C40 to E11 (elev. 208.5)	
C03 Flange	C6 to E11	
C57		

207.55 Top Top
207.65 Top 18" RCP
Side Dr
208.30 Top Bell
4" SEW

REVISED TO GET
OVER TOP OF 18" RCP
DRAIN & 4" SEW. LOT.
10' LT. & of pipe

62nd St.
(Cont'd.)

5/28/59

76

		221.12					
8+00			3.02	218.1	212.5	C56	
9)	13.33	234.22	0.23	220.89			
+50			11.8	222.4	216.8	C56	
9+00			7.0	227.2	221.0	C62	
+50			3.0	231.2	223.6	C76	
10+00			0.9	233.3	225.5	C78	254.94 11.11 243.83 = 242.66
+50			0.6	233.6	228.8	C48	
11)	13.11	247.21	0.12	234.10			
11+00			12.1	235.1	231.4	C37	
+50			9.0	238.2	234.0	C42	6 pipe 5' Ely E. St.
+75			7.2	240.0	235.8	C42	6 pipe 6' Ely E. St.
12+00			5.4	241.8	237.5	C43	" " 78 Ely E. St.
+25			3.9	243.3	239.2	C41	" " 92 " " "
+34 29' FH TEE			3.7	243.5	239.5	C40.5	" " 98 " " "
+34' End Work			3.5	243.7	239.8	C39	" " 102 Ely E. St.
12+47 39' Prop Line					240.8	C42	6 pipe 102 Ely E. St.
CL BM.	End 6" C.I. Exist.	205	245.16	BP. 62nd Brook	240.1		
CL BM.	9.78 254.94	12.13	242.81	= 242.69 (Brook & Fergus)	40' St. 22' RT & LT.		
WATER METERS							
2462 E	1+335	16	195.67	8.05	187.6	190.5	F32 } BK. Met. 505 62nd
3+09 W	1+035	16	195.67	7.5	188.4	190.1	F17 } BK. Met. 522 "
3+79 E	1+17	(No Existing Met)		7.0	188.7	190.4	F17 } BK. Met. 537 "
4+54 E	2+46	16	195.67	6.0	189.7	191.0	F13 } BK. Met. 545 "
5+35 E	3+275	16	195.67	1.1	194.6	195.6	F10 } BK. Met. 604 "
5+67 W	3+59	16	202.88	8.5	199.4	198.2	C12 } BK. Met. 605 "
5+90 E	3+82	"	"	7.06	200.4 200.8	200.3 200.0	C25 ✓ C01 } BK. Met. 612 "
6+09 W	3+96	"	"	6.0	203.9	201.6 201.9	C20 ✓ } BK. Met. 612 "

62nd St.
(Cont'd.)

5/28/59

77

6+19 E 4+11	Ni 207.88	4.7	203.2	202.7 202.4	C08 C05 ✓	611	62nd
6+59 E 4+48	"	0.98	206.9	205.9	C10	619	"
6+75 W 4+68	Ni 226.12	11.2	209.9	202.4 207.0	C08 C25 ✓	622, 626	"
7+31 F 5+22	"	8.9	212.2	212.0 211.6	C08 C02 ✓	625	"
7+82 W 5+74 ✓	"	3.2	217.9	216.0	C19	656	"
7+89 E 5+81	"	4.4	216.7	216.5	C03	635	"
8+09 E 6+42	"	2.6	218.5	218.2	C03	645	"
9+14 E 7+06	Ni 230.22	6.2	228.0	226.1	C19	657	"
9+35 W 7+27	"	4.1	230.1	227.5 227.5	C28 C25 ✓		
10+05 E 7+97	"	0.4	233.8	231.2 230.9	C28 C29 ✓	707	"
10+47 E 8+19	"	0.0	233.8 234.2	233.5 233.2	C03 C12 ✓ C06	717	"
10+95 W 8+81	Ni 247.21	13.1	234.1	236.3	F22	726	"
11+19 E 9+11	(No Existing Met)	10.9	236.5 236.3	237.5	F12 F10		

ALLEY BLOCK 3.

MYRTLE To THORN

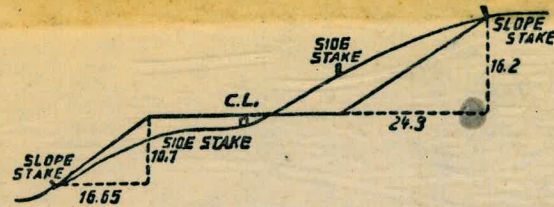
Between BOUNDARY & NILE
 (2) STKS & GRADES FOR WAT. METS

OCT. 19, 1953
 BEATTY
 MARTELL

78.

BM.	6.45	310.14		303.69		BP. NE. COR. THORN & NILE
5+61 E			5.67	304.5	302.1	C24
5+39 E			5.04	305.1	304.2	C09
4+92 E			3.3	306.8	306.6	F03
4+83 E			2.9	307.2	306.8	C04
4+48 E			2.32	307.8	307.6	C02
H Rock.	7.53	317.19	0.48	309.66		
3+74 E			7.19	310.0	309.3	C07
3+63 W			7.16	310.0	309.5	C05
3+35 E			6.32	310.8	310.2	C06
2+86 W			5.64	311.55	311.3	C03
2+61 E			4.5	312.7	311.9	C08
2+37 W			4.4	312.8	312.5	C03
2+37 E			4.5	312.7	312.4	C03
1+83 E			3.5	313.7	313.6	C01
T1	6.67	320.56	3.30	313.89		
1+10 E			5.73	314.83	314.3	C05
1+06 E			5.30	315.3	315.2	C01
0+95 W			5.33	315.23	315.3	F01
0+88 E			4.6	315.6	315.5	C01
0+75 W			4.77	315.8	315.8	C00
0+52 E			4.43	316.1	316.0	C01
T1	0.10	315.11	5.55	315.01		
CK BM.			11.40	303.71	= 303.69	

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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