

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

MICROFILMED

JAN 10 1960

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.35	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.48
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.096	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

UNIVERSITY HEIGHTS ELEVATED TANK
FOOTING ELEVATIONS

PAGE
✓ alicia
2-19

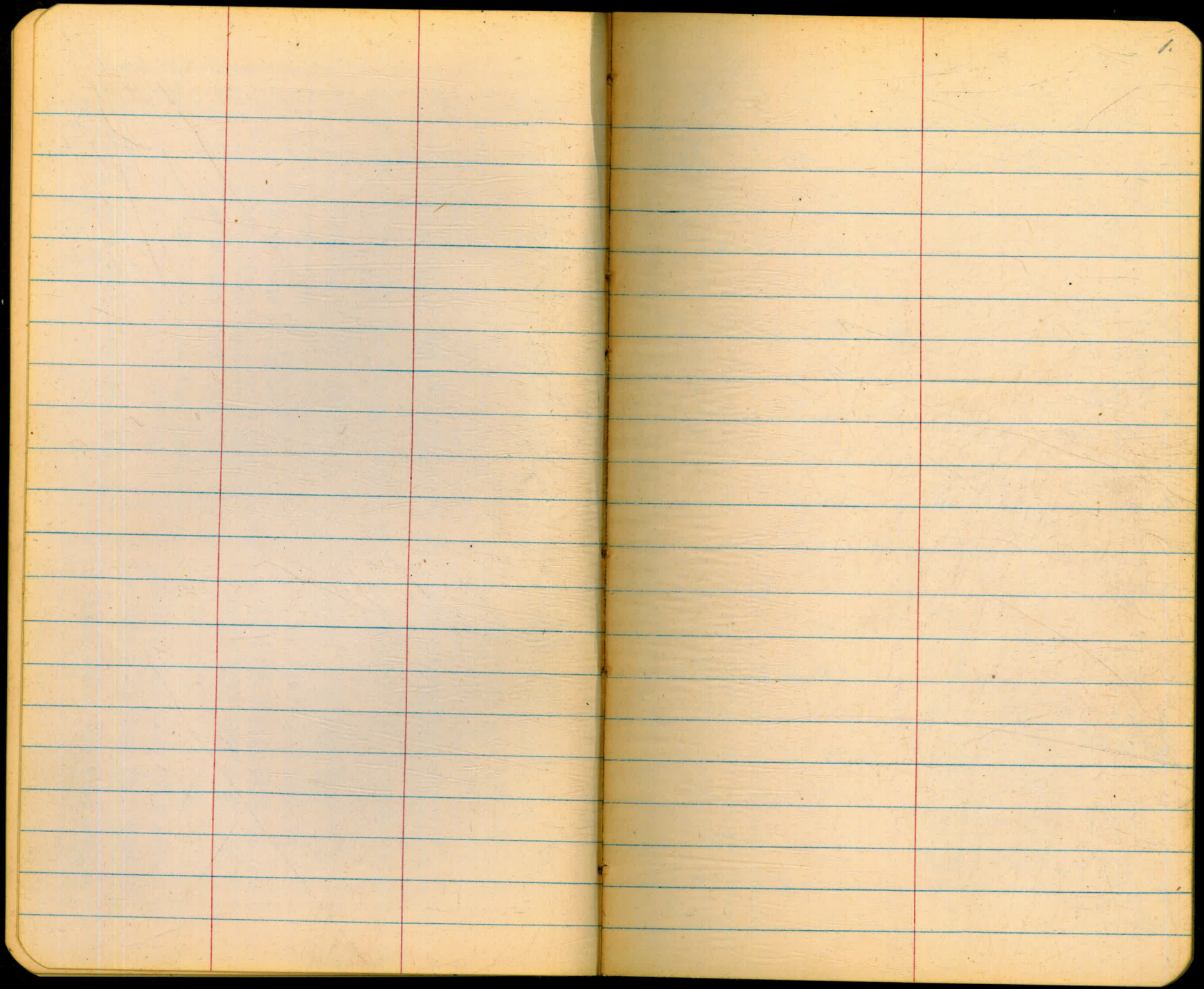
UNIV. HEIGHTS NOR RESERVOIR
ROOF ELEVATIONS

✓ alicia
22-
✓ alicia
32-39

NOR & S. RES. ELEV. WATER SURFACE, BOTTOM & GAUGE
READING 71 ✓
ELEV. of WATER SURFACE, & GAUGE READINGS
NORTH & SOUTH, UNIVERSITY HEIGHTS RESERVOIR 72
✓ alicia
Sketch of Broken PAINT, CURB, & SIDEWALK
OREGON ST. So of El Cajon 73 ✓

Cross-Sections of Existing EXCAV.
VICINITY OF VALVE CHAMBER
OREGON ST. El Cajon 74-75 ✓
alicia

RE-CROSS-SECTION of above item, 76-77 ✓
alicia



#1

UNIVERSITY HEIGHTS ELEVATED WATER TANK

Elevation of Footings of Tank

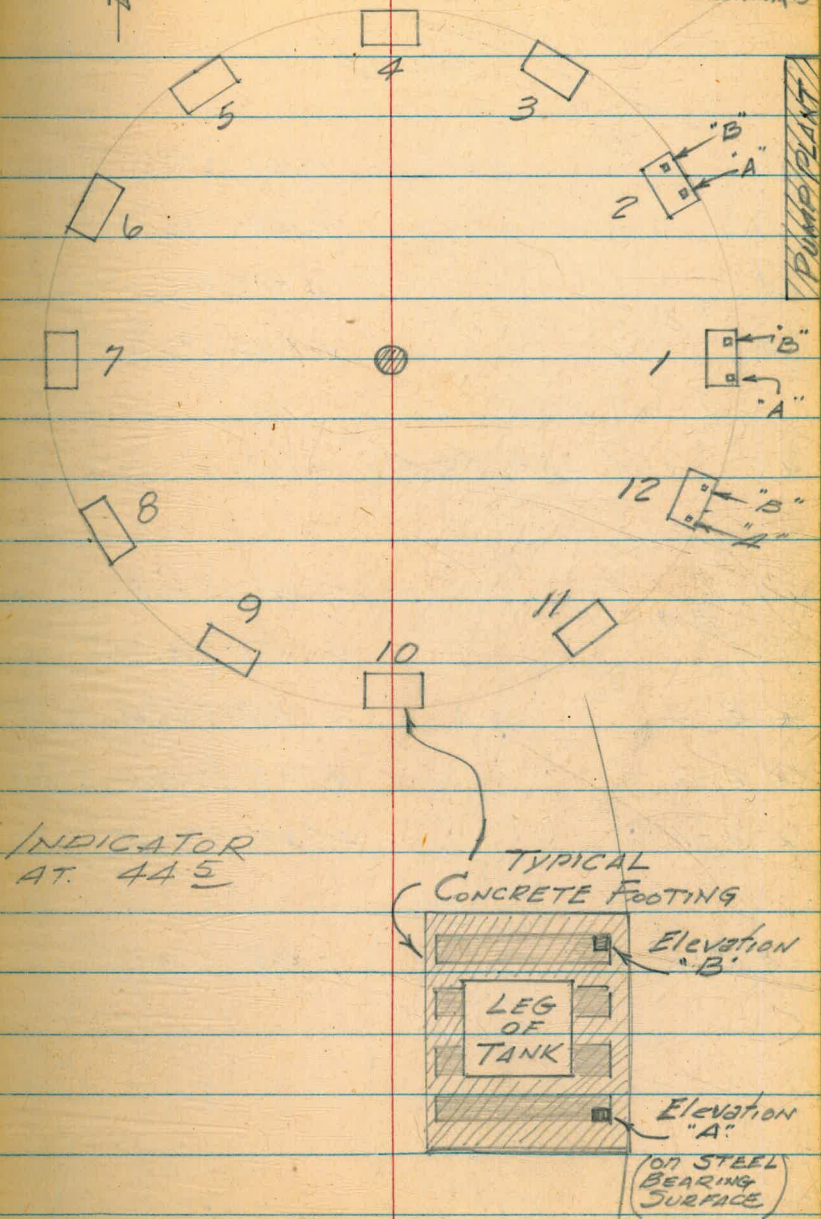
B.M	7.465	380.475	373.01	BP SE. Co. Howard IOWA
A. } #1	✓	4.170	376.305	
B. } #1		4.170	376.305	
A. } #2		4.187	376.288	
B. } #2		4.182	376.293	
A. } #3		4.168	376.307	
B. } #3		4.166	376.309	
A. } #4		4.173	376.302	
B. } #4	✓	4.167	376.308	
A. } #5		4.173	376.302	
B. } #5		4.172	376.303	
A. } #6		4.163	376.312	
B. } #6		4.170	376.305	
A. } #7	✓	4.167	376.308	
B. } #7		4.175	376.300	
A. } #8		4.172	376.303	
B. } #8		4.172	376.303	
A. } #		4.171	376.304	
B. } 10		4.173	376.302	

May 22 1952 2.

2:00 pm BEATTY

POWELL

VARONEAKIS



UNIVERSITY HEIGHTS
TANK
(Cont'd.)

380.475

5/22/52

3

A. } 4.162 376.313 ✓

B. } #11 4.164 376.311 ✓

A. } 4.163 376.312 ✓

B. } #12 4.166 376.309 ✓

H 4.533 380.848 ✓ 4.160 376.315 ✓

A. } 4.547 376.301 ✓

B. } #9 4.547 376.301 ✓

CK B-4 4.542 376.306 = 376.308 ✓

CK A-7 4.542 376.306 = 376.308 ✓

CK A-1 4.546 376.302 = 376.305 ✓

CK. BM. 7.835 373.013 ✓

#2 UNIVERSITY HEIGHTS
ELEVATED WATER TANK
Elevations of Footings of TANK

MAY 26 1952 (4)
1:35 PM
Beatty
KEMP

BM	7.150	380.160 ✓	373.01
#1 { A		3.862	376.298 ✓
{ B		3.863	376.297 ✓
#2 { A		3.880	376.280 ✓
{ B		3.873	376.287 ✓
#3 { A		3.860	376.300 ✓
{ B		3.858	376.302 ✓
#4 { A		3.865	376.295 ✓
{ B		3.858	376.302 ✓
#5 { A		3.865	376.295 ✓
{ B		3.863	376.297 ✓
#6 { A		3.854	376.306 ✓
{ B		3.862	376.298 ✓
#7 { A		3.860	376.300 ✓
{ B		3.866	376.294 ✓
#8 { A		3.864	376.296 ✓
{ B		3.862	376.298 ✓

INDICATOR AT 44.50

UNIVERSITY HEIGHTS
TANK
(Cont'd.)

5-26-52

5

380.160

#10 { A 3.864 376.296 ✓
B 3.863 376.297 ✓

#11 { A 3.853 376.307 ✓
B 3.856 376.304 ✓

#12 { A 3.854 376.306 ✓
B 3.855 376.305 ✓

TP 3.786 380.098 ✓ 3.848 376.312 ✓

#9 { A 3.800 376.298 ✓
B 3.801 376.297 ✓

CK BM 7.091 373.007 ✓

#3 UNIVERSITY HEIGHTS
ELEVATED WATER TANK
Elevation of Footings of Tank

MAY 27 1952
3:30 pm West T
KEMP 9

BM.	7.167	380.177	373.01
1 { A		3.888	376.289 ✓
1 { B		3.888	376.289 ✓
2 { A		3.910	376.267 ✓
2 { B		3.905	376.272 ✓
4 A		3.898	376.279 ✓
5 { A		3.899	376.278 ✓
5 { B		3.895	376.282 ✓
7 B		3.898	376.279 ✓
10 { A		3.890	376.287 ✓
10 { B		3.885	376.292 ✓
11 { A		3.878	376.299 ✓
11 { B		3.882	376.295 ✓
12 { A		3.880	376.297 ✓
12 { B		3.883	376.294 ✓
	4.459	381.264	3372 376.805 ✓
3 { A		4.973	376.291 ✓
3 { B		4.971	376.293 ✓
4 B		4.970	376.294 ✓

indicator at 39.5

(at beginning)

Turn on bolt

381.264

7A 4.969 376.295 ✓

Indicator at 325

8 { A 4.972 376.292 ✓

{ B 4.972 376.292 ✓

9 { A 4.976 376.288 ✓

{ B 4.975 376.289 ✓

P 3.739 380.515 ✓ 4.485 376.779 ✓

C { A 4.225 376.293 ✓

{ B 4.231 376.287 ✓

CK-BM 7.507 373.011 - 373.01 ✓

#4

UNIVERSITY HEIGHTS
ELEVATED TANK

May 28, 1952

(8)

9:30 am.

Elevations of Footings of Tank

BM	7.240	380.250	373.01	INDICATOR at 320
#1 { A		3.958	376.292	
#1 { B		3.961	376.289	
#2 { A		3.980	376.270	
#2 { B		3.972	376.278	
#3 { A				
#3 { B				
#4 { A	✓	3.965	376.285	
#4 { B				
#5 { A		3.963	376.287	
#5 { B		3.960	376.290	
#6 { A		3.950	376.300	
#6 { B		3.958	376.292	
#7 { A				
#7 { B		3.964	376.286	
#8 { A				
#8 { B				
#9 { A		3.962	376.288	
#9 { B		3.961	376.289	

5/28/52

(9)

380.250

#10	{	A	3.961	376.289 ✓
		B	3.963	376.287 ✓
#11	{	A	3.954	376.296 ✓
		B	3.957	376.293 ✓
#12	{	A	3.954	376.296 ✓
		B	3.960	376.290 ✓

H 3.690 380.496 ✓ 3.444 376.806 ✓

#3	{	A	4.204	376.292 ✓
		B	4.202	376.294 ✓
#4	{	A	4.210	376.286 ✓
		B	4.200	376.296 ✓
#7	{	A	4.205	376.291 ✓
		B	4.208	376.288 ✓

D 2.554 378.292 ✓ 4.758 375.738 ✓

CK BM 5.279 373.013 ✓ = 373.010

#5

UNIVERSITY HEIGHTS
ELEVATED TANK
Elevations of Footings of TANK

JUNE 2 1952 (10)

#	BM	7.301	380.311	373.01	INDICATOR AT 320
#10	#1	{	A	4.024	376.287 [✓]
		}	B	4.024	376.287 [✓]
#11	#2	{	A	4.042	376.268 [✓]
		}	B	4.038	376.273 [✓]
#12	#3	{	A		
		}	B		
#11	#4	{	A	4.028	376.283 [✓]
		}	B		
#3	#5	{	A	4.028	376.283 [✓]
		}	B	4.023	376.288 [✓]
#4	#6	{	A	4.020	376.291 [✓]
		}	B	4.023	376.288 [✓]
#7	#7	{	A		
		}	B	4.028	376.283 [✓]
#11	#8	{	A		
CR		}	B		
	#9	{	A	4.026	376.285 [✓]
		}	B	4.026	376.285 [✓]

6/2/52

(11)

380.311

#10	#10	{	A	4.028	376.283	✓
		{	B	4.027	376.284	✓
#11	#11	{	A	4.018	376.293	✓
		{	B	4.021	376.290	✓
#12	#12	{	A	4.021	376.290	✓
		{	B	4.023	376.288	✓

#	#	4.134	380.558	✓	3.887	376.274	✓
					7.027	376.289	←

Not a good turn

#3	#3	{	A	4.270	376.288	✓
		{	B	4.268	376.290	✓
#4	#4	{	A	4.274	376.284	✓
		{	B	4.266	376.292	✓
#7	#7	{	A	4.268	376.290	✓
		{	B	4.275	376.283	✓
#8	#8	{	A	4.271	376.287	✓
		{	B	4.273	376.285	✓

#	#	3633	380.058	4.133	376.275	✓
---	---	------	---------	-------	---------	---

CK BM		7.050	373.008	✓
-------	--	-------	---------	---

373.01 ✓

#6

UNIVERSITY HEIGHTS
ELEVATED TANK

JUNE 5, 1952

(12)

Elevations of Footings.

#	BM	7.170	380.180 ✓	373.01
#1	{	A	3.894	376.286 ✓
		B	3.892	376. ²⁸⁸ 298 ✓
#2	{	A	3.912	376.268 ✓
		B	3.906	376.274 ✓
#3	{	A	3.893	376.287 ✓
		B		
#4	{	A	3.898	376.282 ✓
		B		
#5	{	A		
		B	3.892	376.288 ✓
#6	{	A	3.888	376.292
		B	3.891	376.299
#7	{	A		
		B	3.897	376.283
#9	{	A	3.893	376.287
		B	3.896	376.284

INDICATOR AT 32.50

Bristol Meter at 34.50

6/5/52

(13)

380.180 ✓

#	#10	{ A	3.895	376.285
		{ B	3.896	376.284
#	#11	{ A	3.887	376.293
		{ B	3.889	376.291
#	#12	{ A	3.888	376.292
		{ B	3.888	376.292

4.034 380.459 ✓ 3.755 376.425 ✓

#	#3	{ A	4.171	376.288
		{ B	4.172	376.287
#	#4	{ A	4.175	376.284
		{ B	4.168	376.291
#	#5	{ A	4.174	376.285
		{ B	4.174	376.285
#	#7	{ A	4.169	376.290
		{ B	4.177	376.282
#	#8	{ A	4.173	376.286
		{ B	4.174	376.285

3.840 380.116 ✓ 4.183 376.276 ✓

CK BM.

7.108 373.008 ✓ =

373.01

7

UNIVERSITY HEIGHTS
ELEVATED TANK

Elevations of Footings

BM	7.00	380.011	373.01
#1 { A		3.726	376.285
B		3.724	376.287
#2 { A		3.743	376.268
B		3.738	376.273
#5 { A			
B		3.721	376.290
#6 { A		3.715	376.296
B		3.720	376.291
#7 { A			
B		3.728	376.283
#9 { A		3.727	376.284
B		3.725	376.286
#10 { A		3.727	376.284
B		3.727	376.284
#11 { A		3.718	376.293
B		3.720	376.291
#12 { A		3.720	376.291
B			
II	4.710	380.988	
	4.668	399.746	3.733 376.278

JUNE 10 1952 (14)

9:15 - 9:30 am.

TANK INDICATOR AT 32.50

BRISTOL METER AT 35.0

JUNE 10 1952 (15)

380.988

#12 { A 4.695 376.293 ✓⁰⁰³

{ B 4.697 376.291 ✓⁰⁰³

#3 { A 4.701 376.287 ✓⁰⁰¹

{ B 4.698 376.290 ✓

#4 { A 4.707 376.281 ✓⁰⁰³

{ B 4.700 376.288 ✓⁰⁰⁴

#8 { A 4.704 376.284 ✓⁰⁰³

{ B 4.703 376.285 ✓

P 3.894 380.188 ✓ 4.694 376.294 ✓

OK BM 7.174 373.014 ✓

UNIVERSITY HEIGHTS
ELEVATED TANK

JUNE 12 1952 (16)

9:00 a.m.

8

Elevations of Footings.

BM	7.201	380.211	373.01	
#1	A.	3.928	376.283 ✓	003
	B.	3.927	376.284 ✓	004
#2	A.	3.948	376.263 ✓	005
	B.	3.943	376.268 ✓	006
#4	A			001
	B.	3.928	376.283 ✓	005
#5	A	3.929	376.282 ✓	003
	B	3.929	376.282 ✓	003
#6	A	3.920	376.291 ✓	001
	B	3.927	376.284 ✓	005
#7	A			
	B	3.931	376.280 ✓	003
#9	A	3.931	376.280 ✓	007
	B	3.932	376.279 ✓	005
#10	A	3.932	376.279 ✓	006
	B	3.934	376.277 ✓	001
#11	A	3.923	376.288 ✓	005
	B	3.926	376.285 ✓	006

INDICATOR AT 3750

Bristol Meter AT 350

6/12/52

(17)

380.211

#12	{	A	3.926	376.285	✓	007
		B	3.924	376.287	✓	005

#17	4.713	381.132	3.792	376.419	✓	
-----	-------	---------	-------	---------	---	--

#3	{	A	4.848	376.282	✓	005
		B	4.848	376.284	✓	003

#4	{	A	4.854	376.278	✓	006
		B	4.848	376.284	✓	007

#8	{	A	4.848	376.284	✓	002
		B	4.850	376.282	✓	009

#14	3.650	380.070	4.712	376.420	✓	
-----	-------	---------	-------	---------	---	--

ck BM.			7.057	373.013	✓	
--------	--	--	-------	---------	---	--

#9

UNIVERSITY HEIGHTS
ELEVATED TANK

Elevations of Footings

BM 7.215 380.225 ✓ 373.01

CK TBM 4.320 375.885 ✓ = 375.90

CK TBM 3.486 376.739 ✓ = 376.73

BM. 7.021 380.031 ✓ 373.01

#1 { A 3.737 376.294 ✓

#1 { B 3.737 376.294 ✓

#2 { A 3.757 376.274 ✓

#2 { B 3.749 376.282 ✓

#4 { A
#4 { B 3.742 376.289 ✓

#5 { A 3.738 376.293 ✓

#5 { B 3.739 376.292 ✓

#6 { A 3.730 376.301 ✓

#6 { B 3.738 376.293 ✓

#7 { A

#7 { B 3.739 376.292 ✓

#7 { A 3.738 376.293 ✓

#7 { B 3.738 376.293 ✓

JUNE 16, 1952 18

Beatty
Powell
Fish.

9:00 am

NOTE: - LEVEL PEGGED OUT .002 after Adjust

SET TBM for PUMP HOUSE CONSTRUCTION on Val Box
MISSION VALLEY LINESET TBM on LIGHT STANDARD CURB & EL CAJON & IDAHO
FOR RESERV.
CONSTR. INDICATOR AT = 32.50

BRISTOL METER = 35.0

380.031

#10	{ A	3.739	376.292 ✓
	{ B	3.740	376.291 ✓
#11	{ A	3.729	376.302 ✓
	{ B	3.732	376.299 ✓
#12	{ A	3.730	376.301 ✓
	{ B	3.733	376.298 ✓
IP		5.221 381.104	4.148 375.883 ✓
#3	{ A	4.808	376.296 ✓
	{ B	4.806	376.298 ✓
#4	{ A	4.813	376.291 ✓
	{ B	4.806	376.298 ✓
#7	{ A	4.807	376.297 ✓
	{ B	4.812	376.292 ✓
#8	{ A	4.812	376.292 ✓
	{ B	4.813	376.291 ✓
IP		3.801 380.088 ✓	4.817 376.287 ✓
CK BM.		7.076	373.012 ✓

7/

#

#

#

#

7/

CK

The image shows an open notebook with two facing pages. The pages are cream-colored and feature blue horizontal ruling. Each page is divided into three vertical columns by two red margin lines. The notebook is bound in the center, and the pages are slightly aged. There is no text or other markings on the pages.

UNIVERSITY HEIGHTS
RESERVOIR

Aug. 1, 1952

22.

FINISHED ROOF ELEVATIONS

BM 11.72 384.73 373.01

IP 10.98 391.43 4.28 380.45

2-A 5.08

2-A₂ 5.125

2 1/2-A 5.03

2 1/2-A₂ 5.05

2 1/2-B 5.085

2 1/2-B₂ 5.055

2 1/2-C 5.00

2 1/2-E

3-B 5.045

3-B₂ 5.05

3-C 5.04

3-C₂ 5.02

3-D 5.04

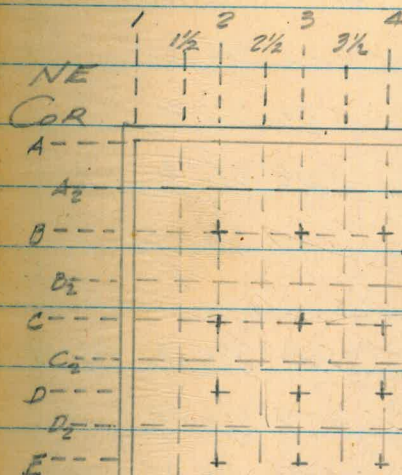
2-C

UNIVERSITY HEIGHTS RES.
FINISHED ROOF ELEV'S

Aug. 1, 1952
West
Kemp

23

BM	11.72	384.73		373.01
\overline{P}	10.98	391.43	4.28	380.45
2-A			5.08	386.35 ^{21/20} 386.27
2-A ₂			5.125	386.315 "
2-C			5.12	386.31. "
2-C ₂			5.12	386.31 "
2-D			5.12	386.31 "
2 1/2-A			5.03	386.40 386.35
2 1/2-A ₂			5.05	386.38 "
2 1/2-B			5.085	386.345 "
2 1/2-B ₂			5.055	386.375 "
2 1/2-C			5.06	386.37 "
2 1/2-C ₂			5.065	386.365 "
2 1/2-D			5.08	386.35 "
2 1/2-D ₂			5.09	386. ³⁴ 36 "
2 1/2-E			5.07	386. ³⁶ 38 "
2 1/2-E ₂			5.08	386.35 "



ELEV'S TAKEN
AS SHOWN IN THIS
TYPICAL SECTIONS
AS PER SHEET #7
RESERVOIR PLANS

NOT ALL SPOTS
TAKEN, DUE TO PILES
OF MATERIAL, FORMS,
REINF. STEEL, ETC. ON
INTERSECTIONS OF COORD'S

ROOF ELEVS
(Cont'd)

391.43

3-B	5.045	386.385	386.340
3-B ₂	5.05	386.38	"
3-C	5.04	386.39	"
3-C ₂	5.03	386.40	"
3-D	5.04	386.39	"
3½-A ₂	5.00	386.43	386.375
3½-B	4.99	386.44	"
3½-B ₂	4.99	386.44	"
3½-C	4.988	386.442	"
3½-C ₂	5.00	386.43	"
3½-D	5.01	386.42	"
3½-D ₂	5.015	386.415	"
4-A	4.976	386.452	386.41
4-A ₂	4.963	386.467	"
4-B	4.97	386.46	"
4-B ₂	4.975	386.455	"
4-D	4.97	386.46	"

ROOF ELEV'S
 (Cont'd)

	391.43	527		391.43			
4 1/2 - A	4.903	386.427	386.445	5 1/2 - A	4.86	386.57	386.515
4 1/2 - A ₂	4.93	386.50	"	5 1/2 - A ₂	4.86	386.57	"
4 1/2 - B	4.92	386.51	"	5 1/2 - B	4.855	386.575	"
4 1/2 - B ₂	4.93	386.50	"	5 1/2 - B ₂	4.86	386.57	"
4 1/2 - C	4.92	386.51	"	5 1/2 - C	4.85	386.58	"
4 1/2 - C ₂	4.94	386.49	"	5 1/2 - C ₂	4.85	386.58	"
4 1/2 - D	4.935	386.495	"				
4 1/2 - D ₂	4.935	386.495	"	6 - A	4.84	386.59	386.55
4 1/2 - E	4.945	386.485	"	6 - A ₂	4.85	386.58	"
4 1/2 - E ₂	4.935	386.495	"	6 - B	4.84	386.59	"
				6 - B ₂	4.85	386.58	"
5 - B	4.886	386.544	386.48	6 - C	4.835	386.595	"
5 - B ₂	4.898	386.532	"	6 - C ₂	4.825	386.605	"
5 - C	4.88	386.55	"	6 1/2 - A	4.77	386.66	386.585
5 - C ₂	4.90	386.53	"	6 1/2 - A ₂	4.80	386.63	"
				6 1/2 - B	4.785	386.645	"
				6 1/2 - B ₂	4.81	386.62	"
				6 1/2 - C	4.79	386.64	"
				6 1/2 - C ₂	4.805	386.625	"
				SET TOM	4.72	387.31	

University Heights Res
Finished Roof Elevations

Aug 18, 52 26
Wash
Powell
Fish

Notes:—

This BM should be 387.310

Beatty 7-4-52

	425 4,115	391.455	Hansen's BM 387.34
1/2 A		5.095	386.36 ³
2 A ₂		5.111	386.34 ¹⁴
2 C		5.115	386.34 ⁰
2 C ₂		5.110	386.34 ¹⁵
2 D		5.108	386.34 ¹⁷
2 D ₂		5.110	386.34 ¹⁵
2 E		5.098	386.35 ⁷
2 1/2 A		5.013	386.44 ¹²
A ₂		5.040	386.41 ⁵
B		5.075	386.38 ⁰
B ₂		5.045	386.41 ⁰
C		5.051	386.40 ⁴
C ₂		5.058	386.39 ⁷
D		5.075	386.38 ⁰
D ₂		5.088	386.36 ⁷
E		5.063	386.39 ²
E ₂		5.082	386.37 ³

425
391.455

3 A	4.990	⁴³⁵ 386.465
B	5.038	³⁸⁷ 386.417
B ₂	5.041	³⁸⁴ 386.414
C	5.035	³⁹⁰ 386.420
C ₂	5.018	⁴⁰⁷ 386.437
D	5.035	³⁹⁰ 6.420
D ₂	5.038	³⁸⁷ 6.417
E	5.015	⁴¹⁰ 6.440
E ₂	5.048	³⁷⁷ 6.407

3 ¹ / ₂ A	4.932	⁴⁹³ 386.523
A ₂	4.997	⁴²⁸ 6.458
B	4.988	⁴³⁷ 6.467
B ₂	4.985	⁴⁴⁰ 6.470
C	4.981	⁴⁴⁴ 6.474
C ₂	4.996	⁴⁵⁹ 6.469 429
D	5.004	⁴²¹ 6.451
D ₂	5.008	⁴¹⁷ 6.447
E	4.988	⁴³⁷ 6.467
E ₂	5.001	⁴²⁴ 6.454

425
391.455

4 A	4.963	386. ⁴⁶² 492
B	4.955	6.500 ⁴⁷⁰
B ₂	4.965	6.490 6.460 ⁴⁶²
D	4.963	6.492 ⁴⁶²
E	4.965	6.490 ⁴⁶⁰
E ₂	4.961	6.494 ⁴⁶⁴

4½ A	4.885	6.570 ⁵⁴⁰
A ₂	4.918	6.537 ⁵⁰⁷
B	4.906	6.549 ⁵¹⁹
B ₂	4.917	6.538 ⁵⁰⁸
C	4.913	6.542 ⁵¹²
D ₂	4.938	6.517 ⁴⁸⁷
E	4.944	6.511 ⁴⁸¹
E ₂	4.941	6.514 ⁴⁸⁴

5 B ₂	4.885	6.570 ⁵⁴⁰
C	4.875	6.580 ⁵⁵⁰
D	4.893	6.562 ⁵³²
D ₂	4.895	6.560 ⁵³⁰

391.455⁹²⁵

5 E 4.895 386.560⁵³⁰

E₂ 4.881 6.574⁵⁴⁴

5¹/₃ A 4.855 6.600⁵⁷⁰

A₂ 4.855 6.600⁵⁷⁰

B 4.850 6.605⁵⁷⁵

B₂ 4.856 6.599⁵⁶⁹

C 4.847 6.608⁵⁷⁸

D 4.874 6.581⁵⁵¹

E 4.862 6.593⁵⁶³

E₂ 4.850 6.605⁵⁷⁵

6 A 4.822 6.633⁶⁰³

A₂ 4.842 ~~6.613~~ 6.583⁶⁰³

B 4.800 6.655⁶²⁵

B₂ 4.843 6.612⁵⁸³

C 4.830 6.625⁵⁹⁵

D 4.820 6.635⁶⁰⁵

D₂ 4.855 6.600⁵⁷⁵

E 4.785 6.670⁶⁴⁰

125
391.455

6 1/2 E ₂	4.820	386.635 ⁶⁰⁵
6 1/2 A	4.755	6.700 ⁶⁷⁰
5 A ₂	4.800	6.655 ⁶²⁵
B	4.782	6.673 ⁶⁴³
B ₂	4.802	6.653 ⁶²³
C	4.792	6.663 ⁶³³
C ₂	4.808	6.647 ⁶¹⁷
D	4.801	6.654 ⁶²⁴
D ₂	4.814	6.644 ⁶¹¹
E	4.775	6.680 ⁶⁵⁰
E ₂	4.800	6.655 ⁶²⁵
7 A	4.730	6.725 ⁶⁹⁵
A ₂	4.762	6.693 ⁶⁶³
B	4.754	6.701 ⁶⁷¹
7 1/2 A	4.763	6.692 ⁶⁶²
A ₂	4.754	6.701 ⁶⁷¹
B	4.763	6.692 ⁶⁶²

Univ Hts Cont

425
391.455

7 1/2 B ₂	4.771	386.684 ⁶⁵⁴
C	4.771	6.684 ⁶⁵⁴
C ₂	4.757	6.698 ⁶⁶⁸
8 A	4.782	6.673 ⁶⁴³
A ₂	4.768	6.687 ⁶⁵⁷
B	4.770	6.685 ⁶⁵⁵
B ₂	4.781	6.679 ⁶⁴⁴
C	4.748	6.707 ⁶⁷⁷
C ₂	4.758	6.697 ⁶⁶⁷

-4.112 387.343³¹³

18 Aug 52

31

corrected BM 9/10/52

BM 387.343³¹³

Jeffers

Notes reduced & checked Jeffers

8/26/52

~~8/27~~

UNIV. HEIGHTS RES.
FINISHED ROOF ELEV'S.

SEPT. 4, 1952

22

TBM	4420	391.730	387.31	391.730		
1-A		5.442	386.288	1/2-A ₂	5.462	386.268
-A ₂		5.482	386.248	-A	5.390	386.340
D		5.504	386.226	2-A	5.378	386.352
B ₂		5.500	386.230	A ₂	5.410	386.320
C		5.468	386.262	B	5.425	386.305
C ₂		5.468	386.262	B ₂	5.410	386.320
D		5.485	386.245	C	5.410	386.320
D ₂		5.488	386.242	C ₂	5.413	386.317
E		5.488	386.242	D	5.410	386.320
E ₂		5.473	386.257	D ₂	5.410	386.320
1/2-E ₂		5.452	386.278	E	5.400	386.330
-E		5.438	386.292	E ₂	5.421	386.309
D ₂		5.440	386.290	2/2-E ₂	5.382	386.348
D		5.410	386.320	E	5.365	386.365
C ₂		5.442	386.288	D ₂	5.387	386.343
C		5.452	386.278	D	5.380	386.35
B ₂		5.452	386.278	C ₂	5.360	386.37
B		5.466	386.264	C	5.355	386.375
				B ₂	5.350	386.38

Notes reduced
9/10/52
849

9-4-52

33

2½-B	391.730	5.380	386.35	3½-B ₂	391.730	5.288	386.442
A ₂		5.345	386.385	B		5.290	386.44
A		5.316	386.414	A ₂		5.300	386.43
3-A		5.285	386.445	A		5.230	386.50
A ₂		5.343	386.386	4-A		5.268	386.462
B		5.336	386.394	A ₂		5.258	386.472
B ₂		5.338	386.392	B		5.260	386.470
C		5.334	386.396	B ₂		5.263	386.467
C ₂		5.320	386.410	C		5.258	386.472
D		5.330	386.400	C ₂		5.273	386.457
D ₂		5.340	386.390	D		5.260	386.470
E		5.320	386.410	D ₂		5.278	386.452
E ₂		5.350	386.380	E		5.253	386.477
3½-E ₂		5.305	386.425	E ₂		5.260	386.470
F		5.288	386.442	4½-E ₂		5.240	386.490
D ₂		5.313	386.417	F		5.245	386.485
D		5.308	386.422	D ₂		5.238	386.492
C ₂		5.298	386.432	D		5.238	386.492
C		5.282	386.448	C ₂		5.236	386.494

9-4-52

24

4 1/2 - C	391.730	5.215	386.515
B ₂		5.220	386.510
B		5.208	386.522
A ₂		5.220	386.510
A		5.188	386.542
5 - A			
A ₂	Mixer Runway		
B			
B ₂		5.190	386.54
C		5.178	386.552
C ₂		5.202	386.528
D		5.194	386.536
D ₂		5.193	386.537
E		5.198	386.532
E ₂		5.182	386.548
5 1/2 - E ₂		5.155	386.575
E		5.163	386.567
D ₂		5.197	386.533
D		5.177	386.553

5 1/2 - C ₂	391.730	5.145	386.585
C		5.148	6.582
B ₂		5.155	6.575
B		5.150	6.580
A ₂		5.160	6.570
A		5.160	6.570
6 - A		5.130	6.60
A ₂		5.147	6.583
B		5.114	6.616
B ₂		5.143	6.587
C		5.132	6.598
C ₂		5.120	6.610
D		5.125	6.605
D ₂		5.155	6.575
E		5.088	6.642
E ₂		5.122	6.608
6 1/2 - E ₂		5.102	6.628
E		5.078	6.652
D ₂		5.118	6.612

9-4-52

35

6½-D	391.730	5.128	386.602	4½-D ₂	391.730	5.062	386.668
C ₂		5.124	6.606	D		5.061	6.669
C		5.096	6.634	C ₂		5.062	6.668
B ₂		5.108	6.622	C		5.078	6.652
B		5.088	6.642	B ₂		5.080	6.65
A ₂		5.104	6.626	B		5.068	6.662
A		5.065	6.665	A ₂		5.060	6.67
7-A		5.035	6.695	A		5.065	6.665
A ₂		5.068	6.662	8-A		5.088	6.642
B		5.060	6.67	A ₂		5.074	6.656
B ₂		5.080	6.65	B		5.074	6.656
C		5.060	6.67	B ₂		5.084	6.646
C ₂		5.075	6.655	C		5.050	6.68
D		5.080	6.65	C ₂		5.061	6.669
D ₂		5.084	6.646	D		5.050	6.68
E		5.062	6.668	D ₂		5.083	6.647
E ₂		5.070	6.66	E		5.055	6.675
7½-E ₂		5.050	6.68	E ₂		5.064	386.666
F		5.058	6.672	8½-E ₂		5.095	6.635

8½-E	391.730	5.065	386.665
D ₂		5.095	6.635
D		5.092	6.638
C ₂		5.084	6.646
C		5.072	6.658
B ₂		5.080	6.65
B		5.085	6.645
A ₂		5.102	6.628
A		5.114	6.616
9-A		5.174	6.556
A ₂		5.142	6.588
B		5.113	6.617
B ₂		5.127	6.603
C		5.128	6.602
C ₂		5.120	6.61
D		5.120	6.61
D ₂		5.128	6.602
E		5.123	6.607
9½ E ₂		5.148	6.582. ✓

9½ E ₂	391.730	5.140	386.570
E		5.131	6.599
D ₂		5.157	6.573
D		5.148	6.582
C ₂		5.160	6.570
C		5.142	6.588
B ₂		5.160	6.57
B		5.142	6.588
A ₂		5.160	6.57
A		5.202	6.528
10-A		5.202	6.528
A ₂		5.205	6.525
B		5.204	6.526
B ₂		5.202	6.528
C		5.185	6.545
C ₂		5.205	6.525
D		5.182	6.548
D ₂		5.201	6.529
E		5.175	6.555
E ₂		5.193	6.537

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$10\frac{1}{2}$ -E ₂	391.730	5.207	386.523
F		5.205	6.525
D ₂		5.228	6.502
D		5.215	6.515
C ₂		5.205	6.525
C		5.221	6.509
B ₂		5.222	6.508
B		5.250	6.48
A ₂		5.220	6.51
A		5.253	6.477
11-A		5.270	6.46
A ₂		5.270	6.46
B		5.272	6.458
B ₂		5.266	6.464
C		5.258	6.472
C ₂		5.275	6.455
D		5.243	6.487
D ₂		5.308	6.422
E		5.260	6.47
E ₂		5.260	6.47

$11\frac{1}{2}$ -E ₂	391.730	5.300	386.430
F		5.308	6.422
D ₂		5.308	6.422
D		5.285	6.445
C ₂		5.302	6.428
C		5.302	6.428
B ₂		5.300	6.43
B		5.280	6.45
A ₂		5.308	6.422
A		5.297	6.433
12-A		5.378	6.382
A ₂		5.372	6.388
B		5.313	6.417
B ₂		5.335	6.395
C		5.322	6.408
C ₂		5.370	6.39
D		5.322	6.408
D ₂		5.335	6.395
E		5.323	6.407
E ₂		5.365	6.365

	391.750	386.355
12 $\frac{1}{2}$ -E ₂	5.375	
E	5.378	6.352
D ₂	5.378	6.352
D	5.372	6.358
C ₂	5.377	6.353
C	5.343	6.387
B ₂	5.365	6.365
B	5.370	6.360
A ₂	5.377	6.353
A	5.340	6.39
13-A	5.436	6.294
A ₂	5.430	6.30
B	5.410	6.32
B ₂	5.418	6.312
C	5.417	6.313
C ₂	5.432	6.298
D	5.420	6.31
D ₂	5.448	6.282
E	5.443	6.287
E ₂	5.430	6.30

	391.730	
13 $\frac{1}{2}$ -E ₂	5.468	386.242
E	5.447	6.283
D ₂	5.465	6.265
D	5.460	6.270
C ₂	5.463	6.267
C	5.440	6.29
B ₂	5.420	6.31
B	5.432	6.298
A ₂	5.441	6.289
A	5.477	6.253
14-A	5.410	6.32
A ₂	5.448	6.282
B	5.440	6.290
B ₂	5.450	6.28
C	5.430	6.30
C ₂	5.480	6.25
D	5.480	6.25
D ₂	5.470	6.26
E	5.450	6.28

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14- E₂

391.730

5.453

386.277

TBM 4.7

4.417

387.313 = 387.31

9-25-52

40

Reedy
Powell
Alexander

TBM	4.26	391.57	387.31		391.57	
1 TBM	4.30	391.57	4.30	387.27	0	5.270 386.300
T 1-F		5.303	386.267	0 ₂	5.290	6.280
F ₂		5.358	6.212	P	5.292	6.278
G		5.342	6.228	1 1/2 F	5.291	6.279
G ₂		5.332	6.238	F ₂	5.292	6.278
H		5.302	6.268	G	5.284	6.286
H ₂		5.322	6.248	G ₂	5.282	6.288
I		5.328	6.242	H	5.290	6.280
I ₂		5.325	6.245	H ₂	5.290	6.280
J		5.294	6.276	I	5.260	6.310
J ₂		5.307	6.263	I ₂	5.310	6.260
K		5.327	6.243	J	5.286	6.284
K ₂		5.294	6.276	J ₂	5.298	6.272
L		5.275	6.295	K	5.230	6.340
L ₂		5.315	6.255	K ₂	5.290	6.280
M		5.270	6.300	L	5.287	6.283
M ₂		5.290	6.280	L ₂	5.298	6.272
N		5.318	6.252	M	5.270	6.300
N ₂		5.283	6.287	M ₂	5.288	6.282

$1\frac{1}{2}$ N	391.57	5.275	386.295	2-1	re-check (5.184)	386.386
N ₂		5.292	6.278	H ₂	5.252	6.318
O		5.281	6.289	H	5.260	6.310
O ₂		5.260	6.310	G ₂	5.242	6.328
P		5.243	6.327	G	Steel in way	
2-P		5.212	6.358	F ₂	5.252	6.318
O ₂		5.262	6.318	F	5.235	6.335
O		5.214	6.356	$2\frac{1}{2}$ P	5.203	6.367
N ₂		5.238	6.332	O ₂	5.206	6.364
N		5.208	6.362	O	5.184	6.386
M ₂		5.241	6.329	N ₂	5.192	6.378
M		5.210	6.360	N	5.182	6.388
L ₂		5.253	6.317	M ₂	5.192	6.378
L		5.223	6.347	M	5.182	6.388
K ₂		5.237	6.333	L ₂	5.215	6.355
K		5.222	6.348	L	5.183	6.387
J ₂		5.242	6.328	K ₂	5.208	6.362
J		5.248	6.322	K	5.160	6.410
$\frac{1}{2}$		5.240	6.330	J ₂	5.208	6.362

2½ J	391.57	5.187	386.383	3-K	5.154	391.57	386.416
I ₂		5.208	6.362	K ₂	5.160		6.410
I	7	5.172	6.398	L	5.160		6.410
H ₂		5.238	6.332	L ₂	5.173		6.397
H		5.210	6.360	M	5.140		6.430
G ₂		5.211	6.359	M ₂	5.150		6.420
G		5.202	6.368	N	5.140		6.430
F ₂		5.215	6.355	N ₂	5.167		6.403
F		5.190	6.380	O	5.162		6.408
3-F		5.173	6.397	O ₂	5.165		6.405
F ₂		5.183	6.387	P	5.150		6.420
G ₂		5.170	6.400	CE TBM		4.30	387.27
G ₂		5.178	6.392	TBM (SET)		4.28	387.29
H		5.184	6.386				
H ₂		5.178	6.392				
I		5.162	6.408				
I ₂		5.168	6.402				
J		5.170	6.400				
J ₂		5.160	6.410				

Notes Revised
1/2

UNIV. HEIGHTS RES.
FINISHED ROOF ELEYS.

WILLIAMS T
JACOBS &

12-2-52

43

CLOUDY

	+	HI	-	EL.
T.B.M.	4.108	391.398		387.29
3 $\frac{1}{2}$ P			4.958	
O ₂			4.969	
O			4.952	
N ₂			4.959	
N.			4.962	
M ₂			4.942	
M.			4.919	
L ₂			4.990	
L.			4.978	
K ₂			4.954	
K.			4.929	
J ₂			4.953	
J			4.968	
I ₂			4.947	
I			4.947	
H ₂			4.975	
H			4.968	
G ₂			4.952	

UNIV. HEIGHTS RES

WILLIAMS T

12 - 2 - 52

44

FINISHED ROOF ELEVS.

JACOBS CLOUDY

	+ HI	- EL.
	391.398	
G		4.960
F ₂		4.974
F		4.983
4 F		4.949
F ₂		4.954
G		4.928
G ₂		4.935
H		4.940
H ₂		4.935
I		4.948
I ₂		4.931
J		4.968
J ₂		4.952
K		4.935
K ₂		4.955
L		4.949
L ₂		4.947
M		4.927
M ₂		4.960

UNIV. HEIGHTS RES.

FINISHED ELEV. ROOF

WILLIAMS T

12-2-52

45

JACOBS

CLOUDY

	HI	EL
	391.378	
N		4.940
N ₂		4.952
O		4.950
O ₂		4.954
P		4.912
4 1/2 P		4.896
O ₂		4.893
O		4.891
N ₂		4.910
N		4.924
M ₂		4.901
M		4.890
L ₂		4.896
L		4.911
K ₂		4.908
K		4.907
J ₂		4.913
J		4.919
I ₂		4.889

UNIV HEIGHTS REG

FINISHED ROOF ELVS.

+ H.I.
391.398

- EL.

I 4,920

H₂ 4,929

H 4,903

G₂ 4,871

G 4,905

F₂ 4,901

F 4,886

CHECK TO B.M.

4,111 387.287

T.B.M. 387.29

T.B.M. 4,521 391.811 387.29

5 F 5,268

F₂ 5,281

G 5,305

G₂ 5,318

H 5,304

H₂ 5,307

I 5,317

I₂ 5,312

J 5,285

5

WILLIAMS T

12-2-52

46

JACOBS CLOUDY

391.811
+ H.I.

- EL.

J₂ 5,307

K 5,298

K₂ 5,301

L 5,305

L₂ 5,286

M 5,275

M₂ 5,311

N 5,273

N₂ 5,280

O 5,214

O₂ 5,276

P 5,220

5¹/₂ P 5,239O₂ 5,239

O 5,230

N₂ 5,267

N 5,263

M₂ 5,266

M 5,269

UNIV. HEIGHTS

FINISHED ROOF

+ #1
391.811

-

RES.

ELEVS.

EL

WILLIAMS T

JACOBS †

391.811
+ #1

FAIR

-

12-3-52

47.

EL

UNIV. HEIGHTS FINISHED ROOF + #1 391.811	RES. ELEVS. EL
L ₂	5,270
L	5,264
K ₂	5,279
K	5,254
J ₂	5,255
J	5,261
I ₂	5,293
I	5,279
H ₂	5,270
H	5,264
G ₂	5,279
G	5,264
F ₂	5,264
F	5,247
6 F	5,217
F ₂	5,220
G	5,202
G ₂	5,206
H	5,210

WILLIAMS T JACOBS † 391.811 + #1	FAIR - EL
H ₂	5,218
J	5,227
I ₂	5,238
J	5,213
J ₂	5,222
K	5,228
K ₂	5,239
L	5,235
L ₂	5,248
M	5,218
M ₂	5,241
N	5,250
N ₂	5,228
O	5,232
O ₂	5,236
P	5,221
6 $\frac{1}{2}$ P	5,190
O ₂	5,192
O	5,197

UNIV FINISHED	HEIGHTS ROOF	RES. ELEV. EL
391.811 + HI		
N ₂		5.195
N		5.199
M ₂		5.160
M		5.175
L ₂		5.185
L		5.183
K ₂		5.197
K.		5.170
J ₂		5.171
J		5.169
J ₂		5.190
J		5.171
H ₂		5.206
H		5.181
G ₂		5.184
G		5.172
F ₂		5.188
F		5.186
CHECK TO B.M.		4.019

WILLIAMS T
JACOBS † FAIR

12-3-53

48.

38.729^{BM}
38.729

12-4-52
 BETTY
 ALEXANDER

49

BM	4.523	391.793	387.27	On \square on Nly curb.	
CK BM		391.833	387.31	On \square on	
7-P			4.503	387.29 = 387.29	
			5.126		
O ₂			5.152	F₂ G	5.128
O			5.128	F F ₂	5.138
N ₂			5.132	7- F	5.140
N			5.116	7 1/2 - F	5.116
M ₂			5.143	F ₂	5.142
M			5.133	G	5.114
L ₂			5.140	G ₂	5.128
L			5.130	H	5.137
K ₂			5.139	H ₂	5.162 (OK) (worse)
K			5.126	I	5.140
J ₂			5.125	I ₂	5.137
J			5.130	J	5.113
I ₂			5.143	J ₂	5.122
H₂ I			5.128	K	5.106 (OK)
H H ₂			5.148	K ₂	5.128
G₂ H			5.142	L	5.143
G G ₂			5.140	L ₂	5.120

391.793

7/2 M.	5.118	J	5.136
7 M ₂	5.122	I ₂	5.146
N	5.140	I	5.142
N ₂	5.141	H ₂	5.128
O	5.130	H.	5.121
O ₂	5.155	G ₂	5.122
7/2 P.	5.128	G	5.105 (OK)
8 P.	5.112	F ₂	5.145 (OK)
O ₂	5.140	F.	5.128
O	5.145	CK BM	4525 387.268 = 387.27
N ₂	5.161		
N	5.125		
M ₂	5.132		
M	5.125		
L ₂	5.132		
L	5.129		
K ₂	5.147		
K	5.123		
J ₂	5.137		

BM	4.370	391 640	387.27
8 1/2 F			5.008
F ₂	ok v		5.028
G	ok v		4.972
G ₂			4.995
H			4.987
H ₂			5.003
I			5.016
I ₂			5.017
J			4.970
J ₂			5.000
K			4.990
K ₂			5.017
L			4.987
L ₂			5.012
M			4.982
M ₂			5.024
N			5.001
N ₂			5.028

8 1/2 O			5.008
O ₂			5.012
8 1/2 P			4.980
9-P	1 out from curb stuck in way		5.069
O ₂			5.063
O			5.033
N ₂			5.067
N			5.062
M ₂			5.063
M			5.040
K ₂			5.058
K ₁			5.042
K ₂			5.063
K			5.050
J ₂			5.051
J			5.048
I ₂			5.057
I			5.061
H ₂			5.058

12-5-52

52

	391.620			391.620	
9-H		5.044		L	5.073
G ₂		5.056		L ₂	5.098
G		5.042		M	5.056
F ₂		5.048		M ₂	5.084
F		5.050		N	5.062
9-E ₂	CHECK PREVIOUS ELEV.	5.066	386.574	386.582 Pg. 36 9/2/52 N ₂	5.070
				O ₂	5.060
9 1/2 F		5.083		O ₂	5.096
F ₂		5.096		9 1/2 - P	5.003
G		5.080		OK BM	4326 - 387.292
G ₂		5.078		BM 4326 391.636	387.290
H		5.078		CORRECTED HI.	
H ₂		5.074		10-P	5.084
I		5.080		O ₂	5.114
I ₂		5.072		O	5.108
J		5.084		N ₂	5.117
J ₂		5.077		N	5.101
K		5.064		M ₂	5.123
K ₂		5.089		M	5.100
				L ₂	5.118

	391.636		10 1/2	391.636	
10-L	5.100		L	5.130	
K ₂	5.103		12	5.160	
K	5.107		J	5.127	
J ₂	5.114		J ₂	5.136	
J	5.118		K	5.127	
12	5.114		K ₂	5.138	
L	5.120		L	5.120	
H ₂	5.128		K ₂	5.122	
H	5.114		M	5.137	
G ₂	5.127		M ₂	5.147	
G	5.111		N	5.128	
F ₂	5.103		N ₂	5.168	OK
10-F	5.110		O	5.149	
10 1/2 F	5.150		O ₂	5.178	
F ₂	5.148		10 1/2 P	5.108	
G	5.153		11-P	5.144	
G ₂	5.162		O ₂	5.208	
H	5.123		O	5.182	
H ₂	5.160		N ₂	5.204	

	391.636		391.636	
H-N	5.192		11/2 F	5.212
M ₂	5.197		F ₂	5.237
M	5.182		G	5.195
L ₂	5.203		G ₂	5.176
L	5.180		H	5.173
K ₂	5.188		H ₂	5.174
K	5.182		I	5.178
J ₂	5.175		I ₂	5.188
J	5.190		J	5.183
J ₂	5.208		J ₂	5.178
I	5.188		K	5.174
H ₂	5.194		K ₂	5.188
H	5.188		L	5.173
G ₂	5.192		L ₂	5.172
G	5.201		M	5.191
F ₂	5.180		M ₂	5.192
F	5.160		N	5.175
11-E ₂	5.170	386.466 = 386.47	11/2 N ₂	5.188
			O	5.164
			O ₂	5.200
			11/2 P	5.187

12-5-52

55

391.636

391.636

12-P

5.220

12 1/2 F₁

5.280

O₂

ok

5.262

F₂

5.303

O

5.233

G

5.266

N₂

5.242

G₂

5.275

N

5.234

H

5.258

M₂

5.263

H₂

5.261

M

5.238

I

5.260

L₂

5.233

I₂

5.267

L

5.223

J

5.250

K₂

5.254

J₂

5.266

K

5.233

K

5.282

J₂

5.248

K₂

5.282

J

5.222

L

5.274

I₂

5.224

L₂

5.260

I

5.230

M

5.281

H₂

5.238

M₂

5.301

H

5.240

N

5.263

G₂

5.248

N₂

5.277

G

5.238

O

5.258

F₂

5.274

O₂

5.285

12-F

5.240

12 1/2 P

5.288

391.636

391.636

13-P.

STEEL IN WAY

13 1/2 F

O ₂	5.341
O.	5.330
N ₂	5.333
N	5.328
M ₂	5.355
M	5.342
L ₂	5.340
L	5.321
J ₂ K ₂	5.332
J. K. K	5.328
K ₂ J ₂	5.335
K J	5.322
I ₂	5.338
I.	5.330
H ₂	5.340
H	5.330
G ₂	5.343
G.	5.335
F ₂	5.336
F	5.326
13.	

F ₂	5.338
G	5.345
G ₂	5.382
H	5.384
H ₂	5.326
I.	5.285
I ₂	5.283
J	5.284
J ₂	5.275
K	5.277
K ₂	5.278
L	5.280
L ₂	5.273
M.	5.299
M ₂	5.297
N	5.306
N ₂	5.282
O.	5.298
O ₂	5.301
O ₂	5.302
13 1/2 P.	5.328

	391.636	
14-B		5.320
O ₂		5.320
O		5.302
N ₂		5.327
N		5.293
M ₂		5.322
M		5.292
L ₂		5.312
L		5.294
K ₂		5.300
K		5.290
J ₂		5.308
J		5.292
I ₂		5.286
I		5.287
H ₂		5.321
H	(6" cur)	5.342
G ₂		5.410
G		5.388
F ₂		5.360
F		5.353
1A		

	391.636	
14 1/2 H		5.306
H ₂		5.284
I		5.250
I ₂		5.256
J		5.260
J ₂		5.278
K		5.267
K ₂		5.263
L		5.262
L ₂		5.262
M		5.252
M ₂		5.297
N		5.260
N ₂		5.287
O		5.262
O ₂		5.286
SET BM	on inside GOR curb SE	4.368 387.268
OK BM		4.367 387.269 = 387.27

391.636
 15-P STEEL IN WAY

O ₂	5.266
O	5.251
N ₂	5.250
N	5.240
M ₂	5.268
M	5.248
L ₂	5.269
L	5.238
K ₂	5.247
K	5.232
J ₂	5.263
J	5.263
I ₂	5.255
I	5.243
H ₂	5.267
H	5.260

391.636
 15 1/2 H

H ₂	5.228
H	5.188
I	5.170
I	5.187
I ₂	5.183
I	5.170
J	5.183
J ₂	5.172
K	5.170
K ₂	5.205
L	5.190
L ₂	5.182
M	5.167
M ₂	5.185
N	5.187
N ₂	5.189
O	5.198
O ₂	5.210

15 1/2 P steel in way

12-5-52

59

	391.636
16-P	STEEL W/FRAM
O ₂	5.163
O	5.162
N ₂	5.167
N	5.172
M ₂	5.170
M ₁	5.163
L ₂	5.175
L	5.132
K ₂	5.158
K	5.160
J ₂	5.162
J	5.144
I ₂	5.171
I	5.172
H ₂	5.175
H	5.212

	391.636
16 1/2 H	5.200
H ₂	5.170
I	5.150
I ₂	5.162
J	5.143
J ₂	5.173
K	5.168
K ₂	5.185
L	5.167
L ₂	5.173
M	5.167
M ₂	5.175
N	5.143
N ₂	5.155
O	5.162
O ₂	5.173
16 1/2 P	5.168

12-5-52

60

391.636

17-P	5.182
O ₂	5.196
O.	5.182
N ₂	5.188
N.	5.184
M ₂	5.192
M.	5.182
L ₂	5.193
L	5.202
K ₂	5.201
K.	5.192
J ₂	5.192
J.	5.180
I ₂	5.186
I.	5.170
H ₂	5.193
H	5.188

391.636

17 1/2 H.	5.226
H ₂	5.207
I	5.163
I ₂	5.194
J	5.212
J ₂	5.220
K	5.215
K ₂	5.207
L	5.218
L ₂	5.232
M	5.218
M ₂	5.226
N	5.202
N ₂	5.206
O	5.198
O ₂	5.212
P.	5.186

	391.636
18-P.	5.253
O ₂	5.252
O	5.243
N ₂	5.237
N	5.243
M ₂	5.258
M	5.242
L ₂	5.258
L	5.250
K ₂	5.247
K	5.234
J ₂	5.230
J	5.248
I ₂	5.228
I	5.218
H ₂	5.231
H.	5.258

	391.636
18 1/2 H.	5.250
H ₂	5.263
I.	5.263
I ₂	5.280
J	5.281
J ₂	5.282
K	5.285
K ₂	5.297
L	5.292
L ₂	5.303
M	5.290
M ₂	5.302
N	5.272
N ₂	5.265
O	5.260
O ₂	5.290
P	5.322

19-p	5.337
O ₂	5.335
O	5.325
N ₂	5.323
N	5.322
M ₂	5.338
M	5.322
L ₂	5.350
L	5.340
K ₂	5.343
K	5.358
J ₂	5.360
J	5.323
I ₂	5.330
I	5.318
H ₂	5.326
H	5.299

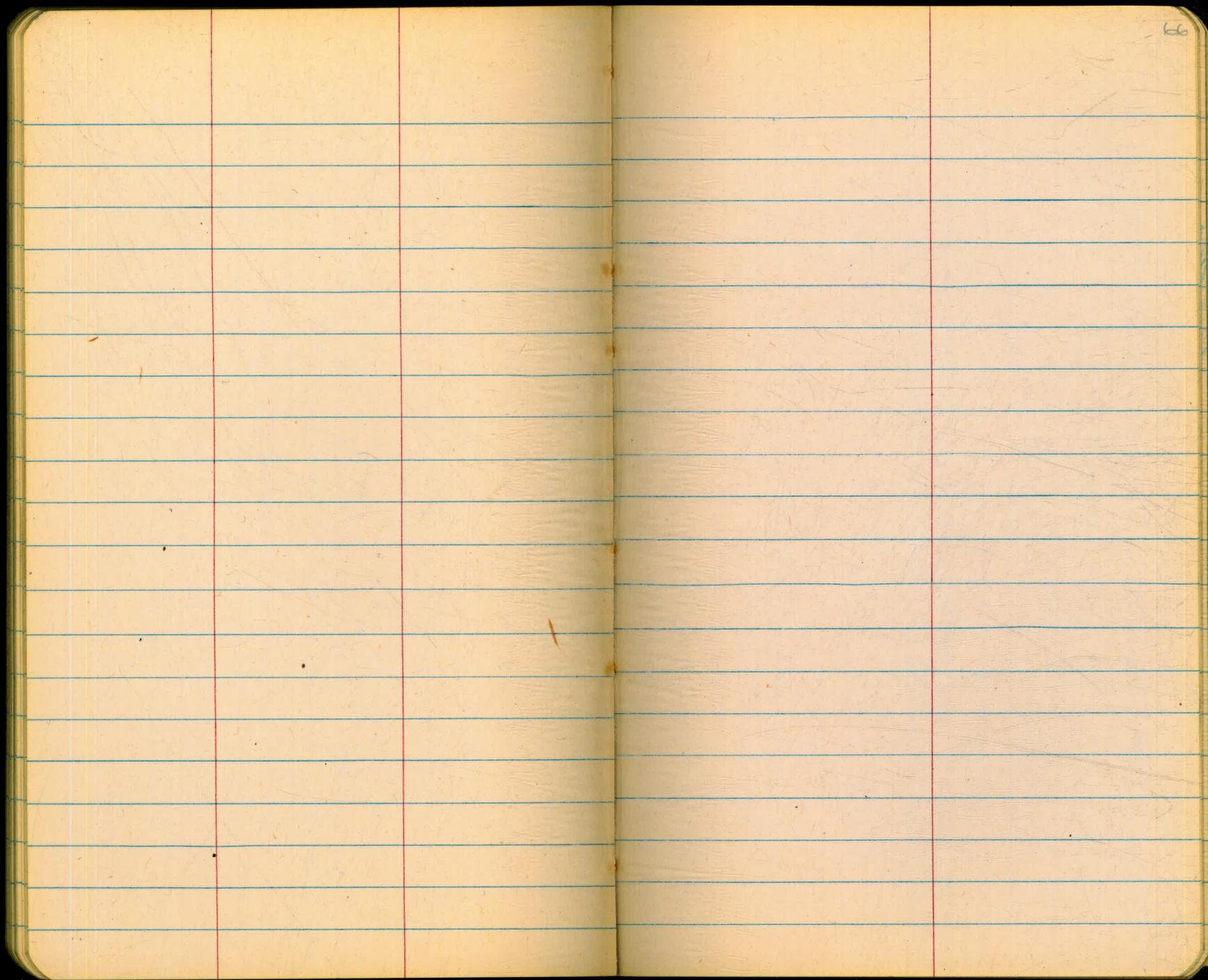
19 1/2 H	5.335
H ₂	5.342
I	5.340
I ₂	5.362
J	5.380
J ₂	5.382
K	5.388
K ₂	5.378
L	5.380
L ₂	5.382
M	5.392
M ₂	NOT IN YET

12-5-52.

63

391.636

20 M	5.418		
L ₂	5.406		
L	5.395		
K ₂	5.410		
K	5.412		
J ₂	5.432		
J	5.410		
I ₂	5.402		
I	5.398		
H ₂	5.410		
H	5.425		
CK BM	4.368	387.268 =	387.268 on inside Cor
CK BM	4.369	387.267 =	387.267 on Nor curb



66

7
7
5
5

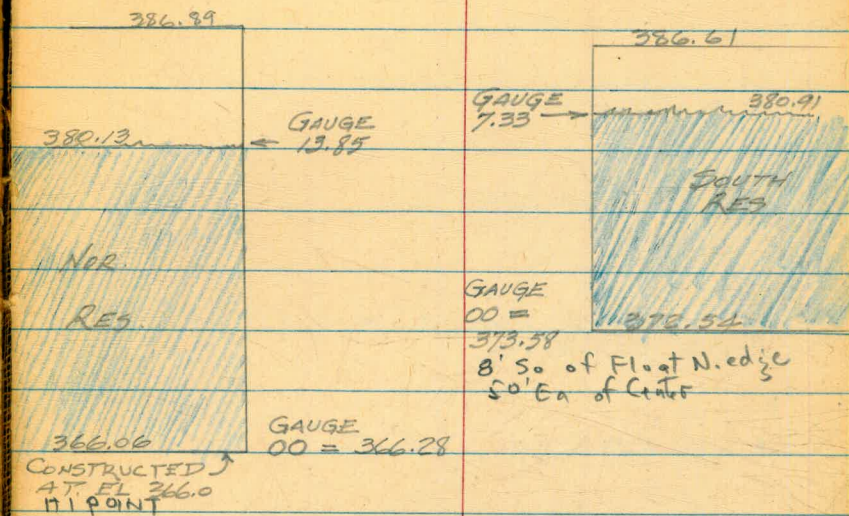
Nor. & So. UNIV. HEIGHTS. RES.
 ELEVATIONS { WATER SURFACE
 BOTTOM OF RESERVOIRS
 GAUGE READINGS.

BM.	4.10	391.368	387.268
NORTH RES.	Top of Hatch	4.48	386.89
		- 6.76	
	WATER SURFACE	11.24	380.13
		- 12.07	
	BOTTOM RES	25.31	366.06
	GAUGE READS		<u>13.85</u>
SOUTH RES.	Top of Roof	4.76	386.61
		- 5.70	
	WATER SURFACE	10.46	380.91
		- 8.37	
	BOTTOM RES.	18.83	372.54
	FLOAT GAUGE READS	7'4" = 7.33	1.17 Eqnt.
	BRISTOL GAUGE IN PUMP HOUSE	<u>8.5</u>	

JAN. 28 1954 3:30 p.m.

Beatty
Shroy
Martell
Alexander

71



$$\text{EQUATION } \begin{cases} 0.0 \text{ GAUGE So. RES} = 373.58 \text{ EL} \\ 0.0 \text{ GAUGE Nor. RES} = 366.28 \text{ EL} \\ \hline 9.30 \end{cases}$$

$$0.0 \text{ FLOAT GAUGE So. RES} = 7.30 \text{ Nor. RES.}$$

$$0.0 \text{ BRISTOL GAUGE So. RES.} = 6.13 \text{ Nor. RES.}$$

JUNE 11, 1953
Beatty
Martell
Alexander

ELEVATIONS OF WATER SURFACE
&
RESPECTIVE GAUGE READINGS
AT NORTH & SOUTH UNIV HEIGHTS RES

TBM 4.10 391.37 387.268

on curb Interior Cor
Roof of Nor. Res.

Elev. of WATER SURFACE 11.33 380.04
NORTH RESERVOIR

GAUGE READING 14.55

ELEV. OF WATER SURFACE 9.68 381.69
SOUTH RESERVOIR

GAUGE READING 8-13/4"

Elevated Tank
GAUGE READING 42.9

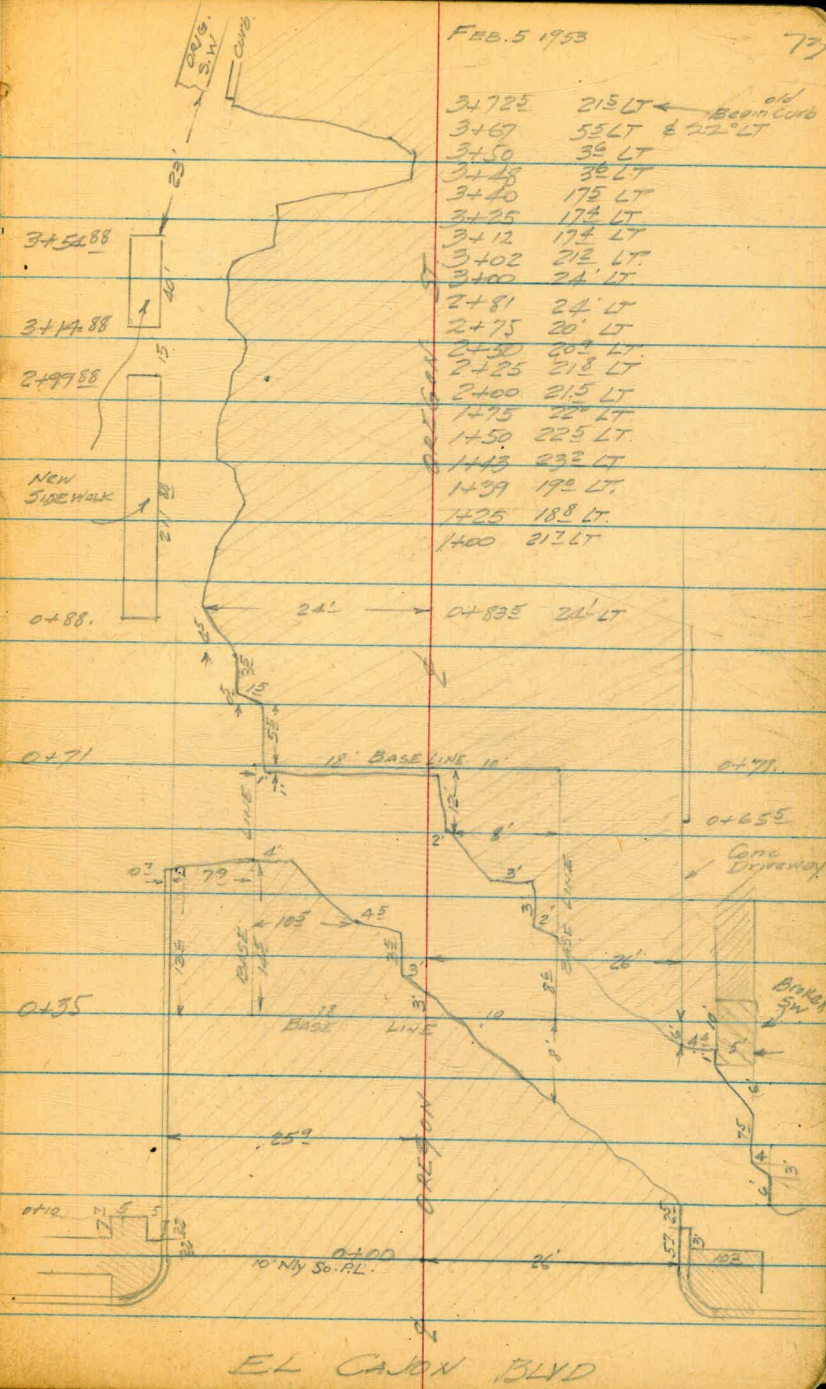
OK BM 4.10 387.27

THESE READINGS TAKEN at 1:00 pm
June 11, 1953

SKETCH OF
BROKEN PAVT, CURB &
SIDEWALK
OREGON ST - So. of EL CASON

FEB. 5 1953

77



Cross-Sections
Contd

2/6/53

75.

0+67.5

379.76

371.1 371.6 369.7 363.2 360.8 360.9
87 82 101 15.6 19.0 18.9
41 30 24.5 23.1 18. 2

375.0
4.27
2

0+70.

371.4 372.1
74 77
41 34

371.2 364.3 361.8 363.8 362.9 368.9 368.5 375.1
16 13.5 14.0 16.0 16.3 10.9 11.3 4.0
30 26 21 24. 13 7 4 2

375.1
4.08
1

0+71.

372.4 373.0 371.4 365.5 363.7 364.7 366.7 374.7
74 68 82 14.3 16.1 12.1 12.1 5.03
41 37 32. 28. 23 22 17E 17

0+76.

375.0 374.2 371.8 367.8 366.2 372.7 374.7
48 56 80 13.0 13.6 7.1 5.07
41 37E 35 31. 25. 22. 17.
20
24

0+82.

375.6 375.2 372.4 370.4 370.4 374.4
42 46 74 9.4 9.4 5.06
41. 35E 33 29 26 21. *

0+88^e Begin Sidewlk

0.0 Excav

375.5 374.9 372.86 374.4
43 48.5 49.0 5.32
41 30. 31 25E

299.88 End Sidewlk
15' No Sidewlk
40' New Side wlk
23' E Side wlk

E Oregon St

RE-CROSS-SECTION OF
EXISTING EXCAVATION, VICINITY
OF VALVE CHAMBER
OREGON ST S of EL CANYON

MAR. 12 1953

26

BM 0.24 376.32 376.08

0+50

378.2
378.3
371.0
375.0
375.9
370.1
370.2
374.6
374.7
374.9
375.2
1.0
1.3
5.6
6.1
1.7
1.6
1.22
15.8
Edge
AC

0+53

367.2
366.0
366.0
365.3
369.6
374.2
374.6
374.9
375.2
91 12.9 12.5 11.0 6.7 2.1 1.7 1.22 1.3
40 36 36 29.5 22.2 20 16 15.8
Edge
AC

0+57.50 Edge Conc & AC

367.0
364.7
365.4
368.8
373.8
374.5
374.9
375.2
9.3 11.6 10.9 7.5 2.5 1.8 1.22 1.15
40 36 29 22 20.5 15.8 15.8
Edge
AC

0+59.5

371.2
364.7
365.5
368.7
371.5
372.3
374.7
375.1
373.6
374.1
375.1
9.1 11.6 10.8 7.6 4.8 4.0 1.58 1.27 2.7 2.2 1.24
40 36 29.5 22.5 20. 15.5 13.6 4.8 4.8
2.5 Edge Broken Conc
TOP
CHAMB.

0+60

(duplicate above)

375.1
1.25
2.8 " "

0+62

367.6
367.5
370.5
370.6
369.4
369.1
370.2
370.5
374.8
375.0
372.5
372.8
375.0
8.7 8.8
40 37 30 26 25 22 19.6 15.5 15.5 4.8 4.8
TOP
CHAMB.

375.0
1.25
3.0 " "

0+66 Sa Edge Val. Chamb

369.7
370.3
371.3
370.0
368.3
367.8
368.3
371.2
372.7
375.1
6.6 6.0 5.8 6.3 8.0 8.5 8.0 5.1 3.6 1.27
40 34 29 25.5 24 12. 8. 4.8
2.4 " "

0+67.5

370.4
371.5
370.6
368.2
368.2
368.7
374.4
375.1
5.9 4.8 5.7 8.1 8.1 7.6 1.3 1.27
41. 31 28 26. 11.5 7
2

0+70

371.7
372.1
371.1
368.5
368.6
370.7
375.2
4.6 4.2 5.2 7.8 7.7 5.6 1.15
41. 30 30 29 7 3

3/12/53

77

0+71

376.32

372.0	372.3	371.1	368.5	369.3	371.3	375.2
4.3	4.0	5.2	7.8	7.0	5.0	1.5
41	34	30	29	9	5	4

0+76

374.8	374.5	373.5	369.2	369.2	374.0	371.2	371.7	374.8	375.1
1.5	1.4	2.8	7.1	7.1	2.3	5.1	4.6	1.54	1.20
41	39	36	32	30	20	18	112	112	4

0+82

375.5	375.4	370.0	374.7	372.9	373.7	375.1	375.1
2.8	0.9	5.3	1.6	2.7	2.6	1.25	1.25
41	38	30	204	185	13	11.0	4

0+88

374.87	374.4	373.6	375.0	375.1
1.55	1.9	2.7	1.20	1.25
31	23	19	10	4

Edge
Sidewalk

OK BM

024 = 376.08

12-30-52

BM	4.11	380.19	376.08
		SW 5.08	375.11
		Curb 5.24	374.95
		SW 6.28	373.91
		Curb 6.32	373.87
			1' High
0+00		✓ 4.08	376.11 375.11
+25		✓ 4.16	376.03 375.06
+50		✓ 4.24	375.95 374.95
+75		✓ 4.32	375.87 374.96
1+00		✓ 4.39	375.80 374.91
	1+21	4.45 375.74 374.74	374.90
+25		✓ 4.47	375.72 374.72
+50		✓ 4.55	375.64 374.81
+75		✓ 4.63	375.56 374.81
2+00		✓ 4.71	375.48 374.76
+25		✓ 4.79	375.40 374.74
+50		✓ 4.87	375.32 374.66
+75	+67	4.92 375.27 374.27	374.61
3+00		✓ 4.95	375.24 374.56
+25		✓ 5.01	375.18 374.51
+43		✓ 5.09	375.10 374.46
		5.15	375.04 374.46

3+84.3

3+43.3

376.08
3.21
379.29

9.29
375.97
3.32
3.37
3.42
3.46
3.52
3.57
3.63
3.68
3.73
3.78
3.83

1.5

1.1

3.8

7.7

5.16
7

375.11
373.91
3843 } 1.2.000
11.529
4.710
28.43
8670

.00312
25
1560
624
107800

.00312
18
2496
312
05616

.00312
20
106200

.0312
15
1560
312
0.0680

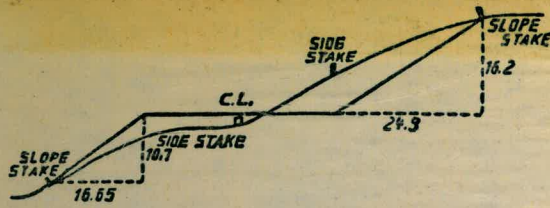
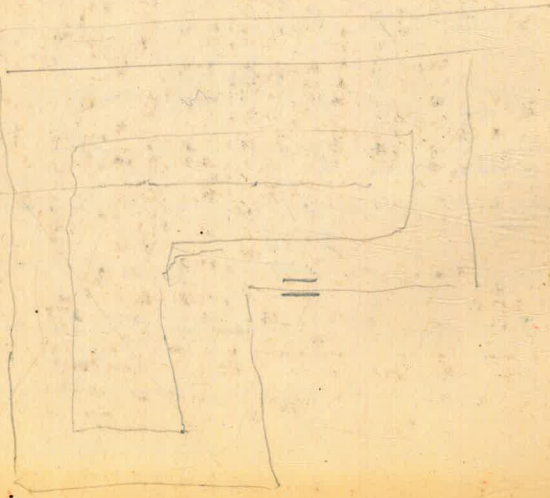
375.11
374.46
343 } .650(19
343
3070
3087

.0019
25
25
38
0425
1025

716
 - 811 Bond

255
 3.46
 6.01

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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