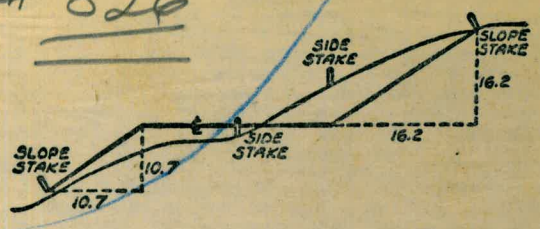


826



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. *If it does not make the slight adjustment necessary.

MICROFILMED
JAN 16 1965

Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.41	1.51
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	1.92	2.30	2.68	3.06	3.44	3.82	4.22	4.62	5.03	5.43
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.054	.060	.065
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.887	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

GRAND AVE. INGRAM TO CASS.

TOP EXISTING P.I. 68 Alice
~~SEE Page 80 for Continuation of Index~~

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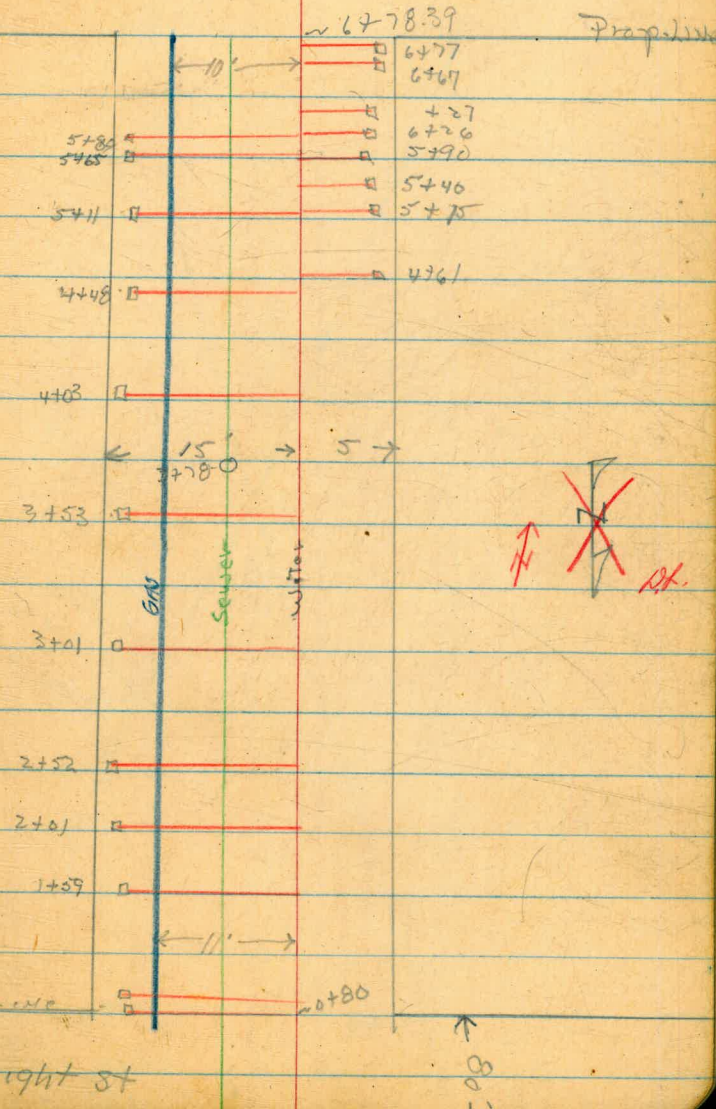
Plan & Profile
 Alley # 18
 No. of Dwight
 East " N. 1es

King 7-15-52

Dwight's Vite
 N.E.R.P.

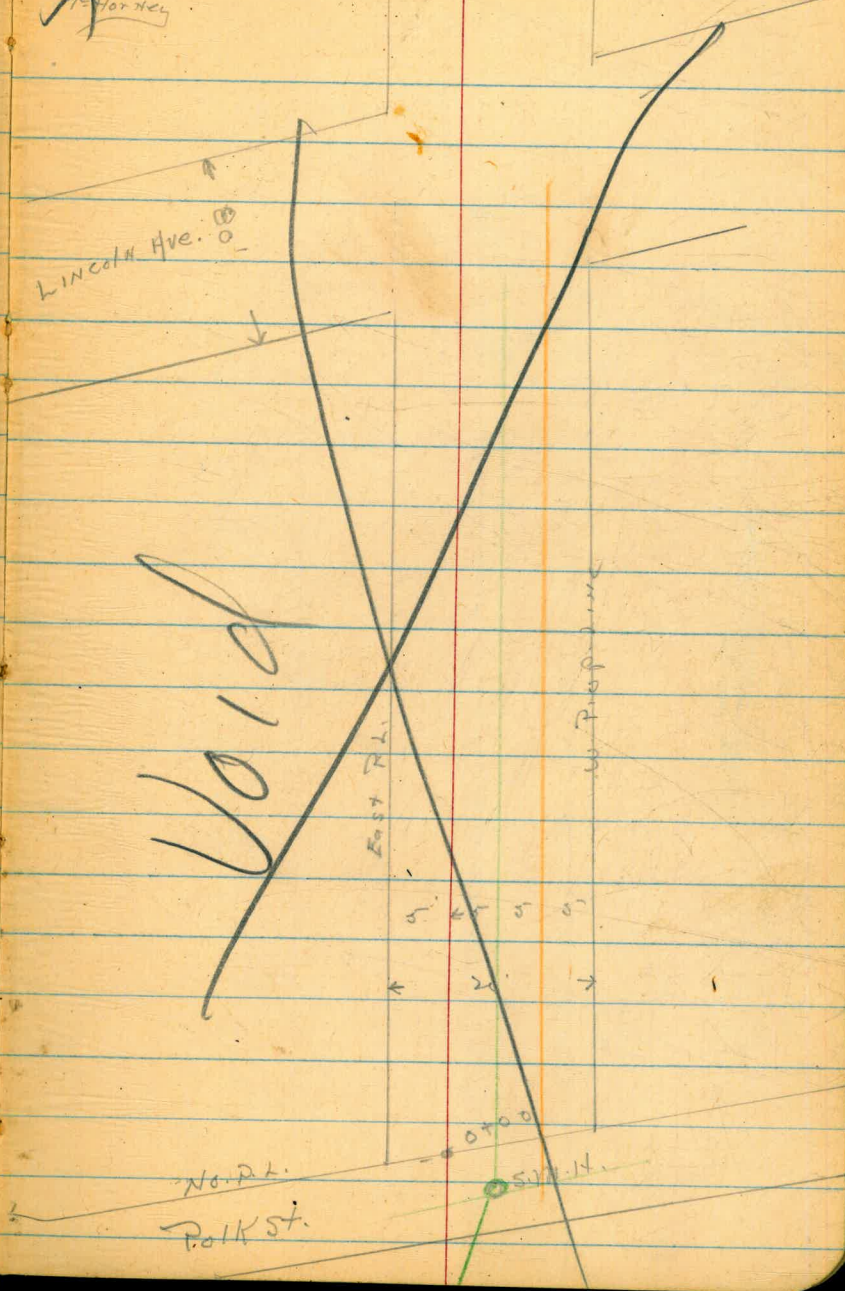
B.M.	4.17	321.82		317.15
0+00			5.6	316.2 ✓
+50			5.4	316.4 ✓
1+00			4.9	316.9 ✓
+50			6.9	314.9 ✓
2+00			8.1	313.7 ✓
+50			8.9	312.9 ✓
3+00			10.6	311.2 ✓
T.P.	8.15	319.65	10.32	311.50
+50			8.8	310.9 ✓
TOP 5" DIA 3+78			8.5	311.2 ✓
4+00			7.9	311.8 ✓
+50			7.8	311.9 ✓
5+00			6.8	312.9 ✓
+50			5.8	313.0 ✓
6+00			4.8	314.0 ✓
+50			3.7	316.0
6+85.39			2.9	316.8
T.P.	10.12	321.74	8.03	311.22
B.M.			4.61	317.13
				317.15

LANDS



~~Hiley # 201
Elev of Boundary
No. of ...~~

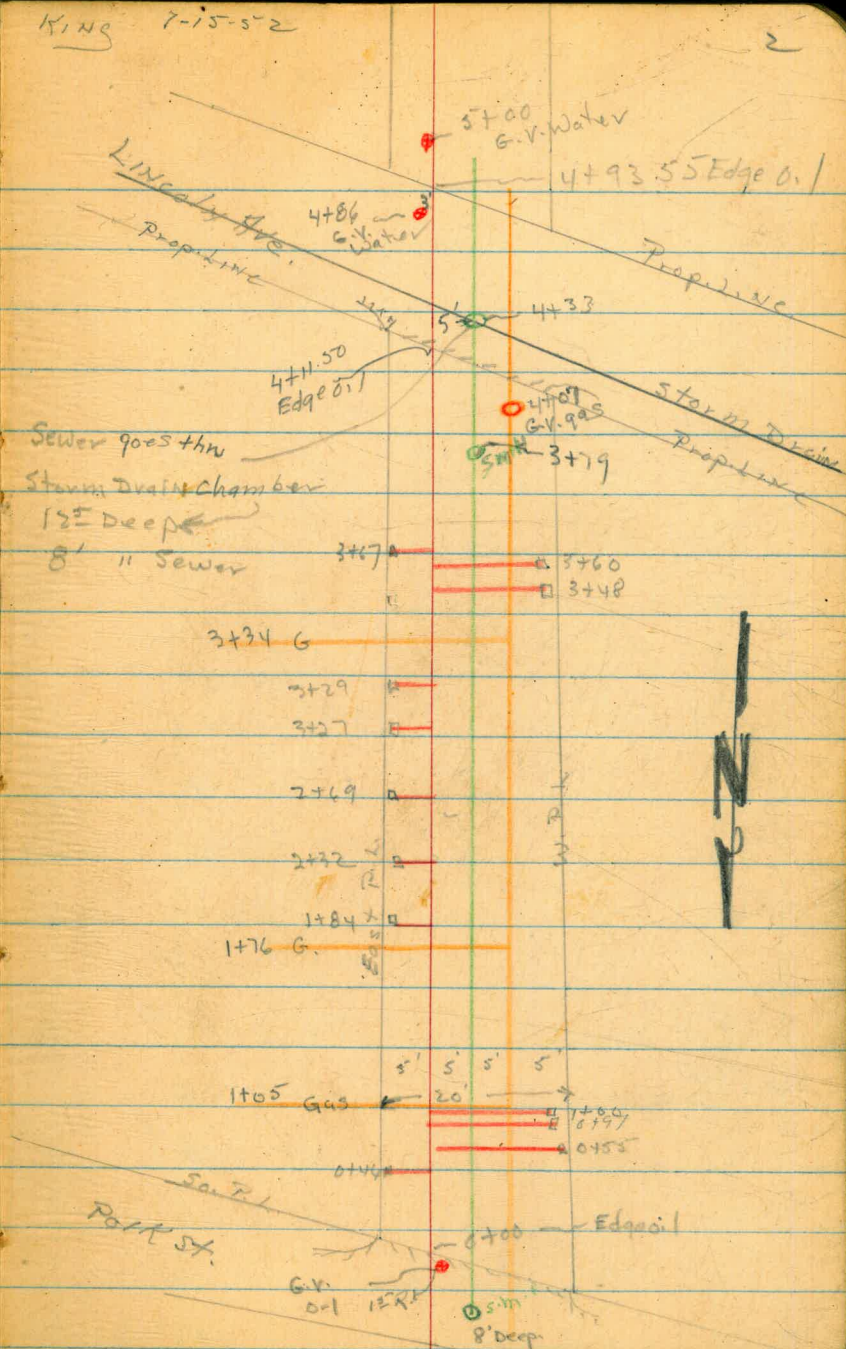
King
Williams
James
Motel
Hornley
7-15-52



Plan & Profile
Alley - 201
North of Lincoln
East of Boundary

KING 7-15-52

2



Profile Alley 201
 East of Boundary
 North of Lincoln

King 7-10-52

3

B.M.	8.21	325.36		37.15	B.P. N.E. Mile 4 Dwight
T.P.	2.15	324.54	2.97	322.39	
T.P.	5.68	320.41	9.81	314.73	
T.P.	8.80	327.75	1.44	316.95	
T.P.	12.73	339.30	1.18	326.57	
T.P.	5.92	342.51	2.71	336.59	
4+93.55					
4+50					
4+36 ^{top} M.H.			5.92	336.6	✓
4+38			18.4	324.1	✓
4+36			13.9	328.6	✓
4+12			5.6	336.9	✓
4+00			5.6	336.9	✓
3+76 ^{Sewer} M.H.			5.2	337.3	✓
3+76 ^{Fr} Sewer			10.2	332.3	✓
3+50			4.7	337.8	✓
3+00			2.5	340.0	✓
T.P.	10.35	352.72	0.14	342.37	
2+50			10.3	342.4	✓

Bottom Storm Drain

Sewer Pipe in M.H.

352.72

2+00			8.5	344.2	✓
1+50			6.7	346.0	✓
1+00			5.4	347.3	✓
0+50			3.5	349.2	✓
0+00			4.4	348.3	✓
S.M.H.			4.7	348.0	
Sewer F.h.			12.7	340.0	
T.P.	0.09	342.46	10.35	342.37	
TP	1.02	335.07	8.41	334.05	
TP	2.68	327.58	10.11	324.90	
T.P.	1.65	322.02	7.21	320.57	
TP	8.67	320.55	9.94	312.08	
TP	8.64	327.29	2.10	318.65	
TP	3.64	324.99	5.94	326.35	
CK. B.M.			7.84	317.15	

Edge 0.1

Q #11ey + Poik sl.

921.17

6+80		-7.7	313.5	
6+92		-4.4	316.8	
7+00		-0.6	320.6	SPOIL DIRT
7+05		-1.7	319.5	AVERAGE LEVEL
7+18 ²		-3.1	318.1	NIGHTMAN
7+22		-1.6	319.6	STEEP SLOPE DOWN HILL
7+38		-2.1	319.1	"
7+56		-8.7	312.5	"
T.P. +1.63	309.92	-12.88	308.29	ROCK
7+76		-8.5	301.4	
7+87		11.6	298.3	TOE OF FILL DIRT
8+00		11.7	298.2	
T.P. +4.57	302.71	-16.78	298.14	ROCK
8+30		-4.9	297.8	
8+35 - 90° VERT. BEND IN 2" PIPE		-5.20	297.5	TOP OF HILL
8+35		-7.8	294.9	GROUND
8+44 ENTER WASH		-9.1	294.6	TOP OF DRAIN
8+47 - 5" L.I.		-11.12	291.6	TOP OF 12" SEWER
8+51		-13.0	289.7	CREEK BED

302.71

8+89		-12.3	290.4	BOTTOM OF GREEN BANK
8+82		-5.4	297.3	TOP OF BANK
9+00		-2.6	300.1	
9+20	S. Rim M.H. 12" SEWER, 7.7 LG	-9.52	293.19	FLOW LINE
		-0.60	302.11	TOP M.H.
T.P.	+12.26 314.87	-0.60	302.11	SOUTH FACE RIM M.H.
9+20	-2	-13.1	301.3	GROUND
9+50		-9.4	305.0	
"	4' RT.	-7.5	306.9	
9+75		-5.0	309.4	
"	4' RT.	-2.4	312.0	
10+00		-1.9	312.5	
"	4' RT.	-1.8	313.6	
"	5' LG.	-2.7	311.7	
T.P.	+12.60 326.39	-0.58	313.79	ROCK
10+50		-11.0	315.4	
10+94	7.5' LG. SEWER M.H.	-16.9	302.5	FLOW LINE
		-9.12	317.3	SEWER RIM SEWER LATERAL FROM EAST.
10+94	TOP 4" PIPE	-12.1	314.3	
11+00		-8.1	318.3	
11+50		-5.9	320.5	

326.39

11+79	3.1 FT. ON EDGE CONC. SLAB	-3.2	323.2	
11+88.5	3.1 FT. ON EDGE CONC. SLAB	-2.9	323.5	
12+00	6" CONC. 2" ASPHALT TOP	-2.3	324.1	
12+39	EDGE PVT.	0.2	326.2	
	TOP 6" GATE VALVE S. SIDE UNIV. AVE.	-0.82	325.6	ON STRE
12+46.15	- 7' OFFSET LINE	0.0	326.4	
12+58.5	GUTTER ON UNIV. AVE.	0.15	326.2	
T.P.	+2.90	328.75	0.54	325.95 ON PVT. D.A. SIDE
CHECK B.M.		-6.58	322.17	UNIV. SIDE

Mulberry St
 2 Profile
 Paradise to Mallard

	12.76	446.93		434.17
	12.13	458.49	0.57	446.36
	6.25	463.69	1.05	457.44
0+00			3.7	460.00
+50			5.0	458.7
1+00			6.1	457.6
+10			6.5	457.2
+37			10.2	453.5
	1.50	452.94	12.55	431.44
+50			3.4	449.5
2+00			10.4	442.54
	2.24	442.56	12.62	440.32
+50			7.0	435.66
	1.13	430.66	13.03	429.53
3+00			3.3	427.4
	0.62	419.46	11.82	418.84
+50			2.7	416.8
+75			8.7	410.8
	0.57	407.63	12.40	407.06
4+00			3.3	404.3
+25			9.8	397.8
	1.19	396.38	12.44	395.19
+50			6.0	390.4
+75	1.00	384.92	12.46	383.92
5+00			6.8	378.1
+50			14.9	370.0
6+00			9.6	375.3
+50			3.6	381.32

West
 Martell
 Varontakis

3 Oct 50

11

BM Top FH SE. Cor Springfield + Paradise

South Prop Line Paradise

		384.92	-	21.0
	11.98	394.76	0.14	382.78
7+00			5.4	389.4
+50	10.92	404.94	0.74	394.00
			7.4	397.5
8+00			4.6	400.3
+50			3.1	401.8
9+00			3.7	401.2
+50			6.4	398.5
10+00			13.1	391.8
	0.25	392.77	12.42	392.52
+50			13.2	379.6
	0.47	380.73	12.41	380.36
11+00			8.3	372.4
+50			11.4	369.3
12+00			10.3	364.4
+50			13.0	367.7
13+00			8.3	372.4
+50			2.2	378.5
	13.01	392.19	1.55	379.18
14+00			8.2	384.0
+50			2.8	389.4
	12.05	403.94	0.30	391.89

creek Bolt

7.2	3.8
<u>10.2</u>	<u>10.2</u>
3.1	0.0
<u>10.2</u>	<u>10.2</u>
9.7	6.9
<u>10.2</u>	<u>10.2</u>
5.9	2.5
<u>10.2</u>	<u>10.2</u>
7.7	6.5
<u>10.2</u>	<u>10.2</u>
10.3	10.7
<u>10</u>	<u>10.2</u>
14.6	11.9
<u>10.2</u>	<u>10.2</u>
9.3	6.8
<u>10.2</u>	<u>10.2</u>
11.2	15.2
<u>10.2</u>	<u>10.2</u>
7.3	11.2
<u>10.2</u>	<u>10.2</u>
1.7	3.2
<u>10.2</u>	<u>10.2</u>
7.7	9.5
<u>10.2</u>	<u>10.2</u>
1.4	3.8
<u>10.2</u>	<u>10.2</u>

15+00	403.94	8.0	395.9	87 10RT	6.3 70R
+50		0.5	403.4	+1.0 10L	1.9 20R
	12.74	416.39	0.39	403.65	
16+00		5.9	410.51	3.7 10RT	7.3 10°RT
	13.02	429.06	0.35	416.04	
+50		12.2	416.9	11.7 10R	14.9 10RT
17+00	13.61	441.37	3.5 0.70	425.6 428.36	3.0 70 5.4 70
+50		13.3	428.07	12.1 10L	15.1 10R
18+00		8.2	433.2	6.7 70	9.6 10R
+50		3.1	438.27	2.2 10L	4.3 10R
	8.47	449.45	0.39	440.98	
19+00		7.1	442.4		
+50		5.8	443.7		
20+00		5.3	444.2		
+50		5.7	443.8		
20+68 ³		4.8	444.165		
		4.59	444.86 = 445.2		

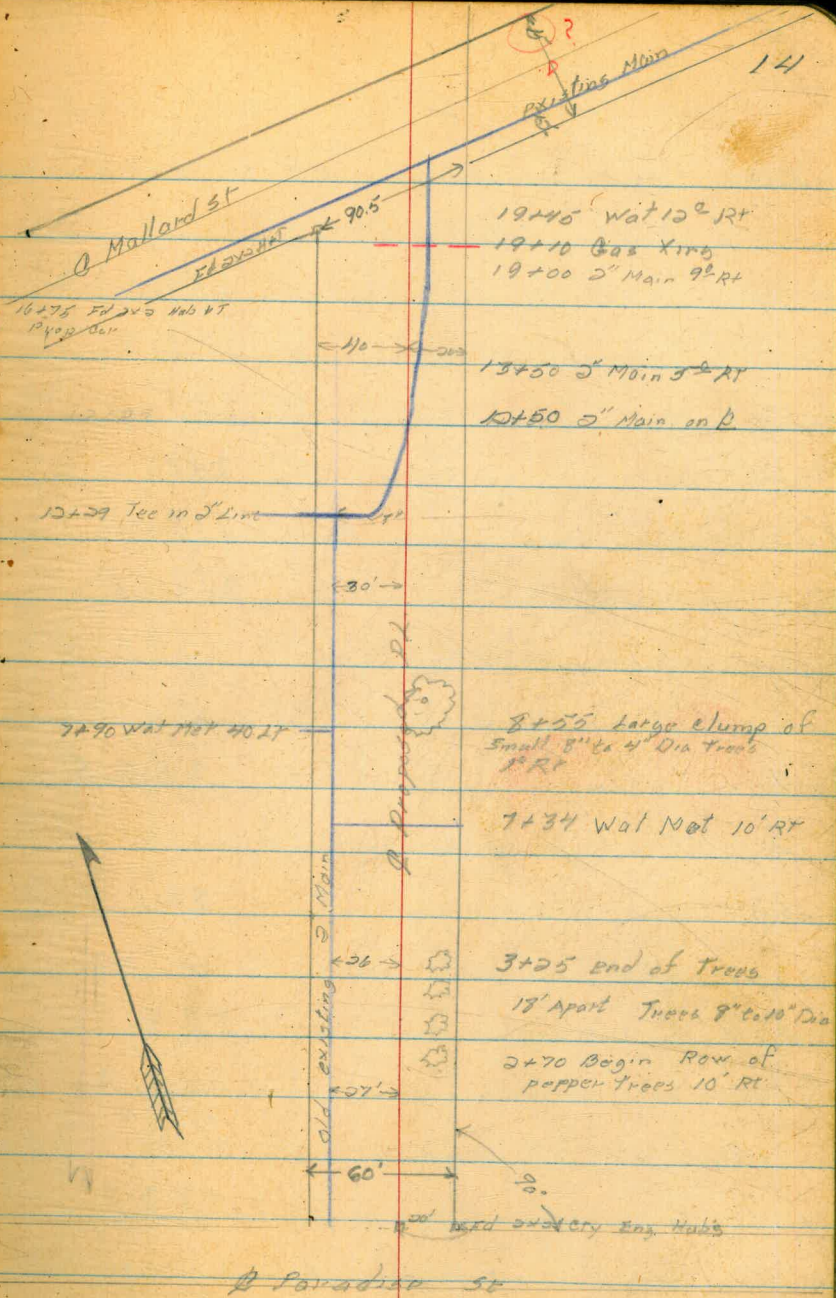
20+68 ³/₄

North Line Mallard St

20+44.7 = 7+60 on mallard

0+00

South prop line Paradise



Paradise St

Cypress Ave

240' West of the east line
of Albert St

Sta	B.S.	I.I.	F.S.	60' ST. ELE
	4.96	285.27		280.31
0+00			5.06	280.2
0+07			9.5	275.7
0+32			11.85	273.4
0+41 ²			6.56	278.7
0+41 ⁵			5.87	279.4
0+50			6.5	278.7
	1.14	274.24	12.17	273.10
	0.05	261.46	12.83	261.41
1+00			8.9	252.5
	1.36	250.36	12.46	249.00
+50			7.9	242.4
	4.66	242.93	12.09	238.27
+87			7.8	235.1
2+00			9.2	233.7
				234.4
+08			8.54	+7.5 to Powder
+40			9.6	233.3
	13.09	284.40	1.62	291.31
	12.69	265.69	1.40	253.00
	12.30	277.51	0.48	265.21
	9.10	285.18	1.43	276.08
			4.85	280.35 = 280.31

8 Oct 52

15
Clear + Warm

West
Marlett
Varenfakis

NE BP Cypress + Albert

East Prop Line Albert 10' North Curb Line

- Flow Line 19" Storm Drain 14° LT

- Flow " " " " 11° RT

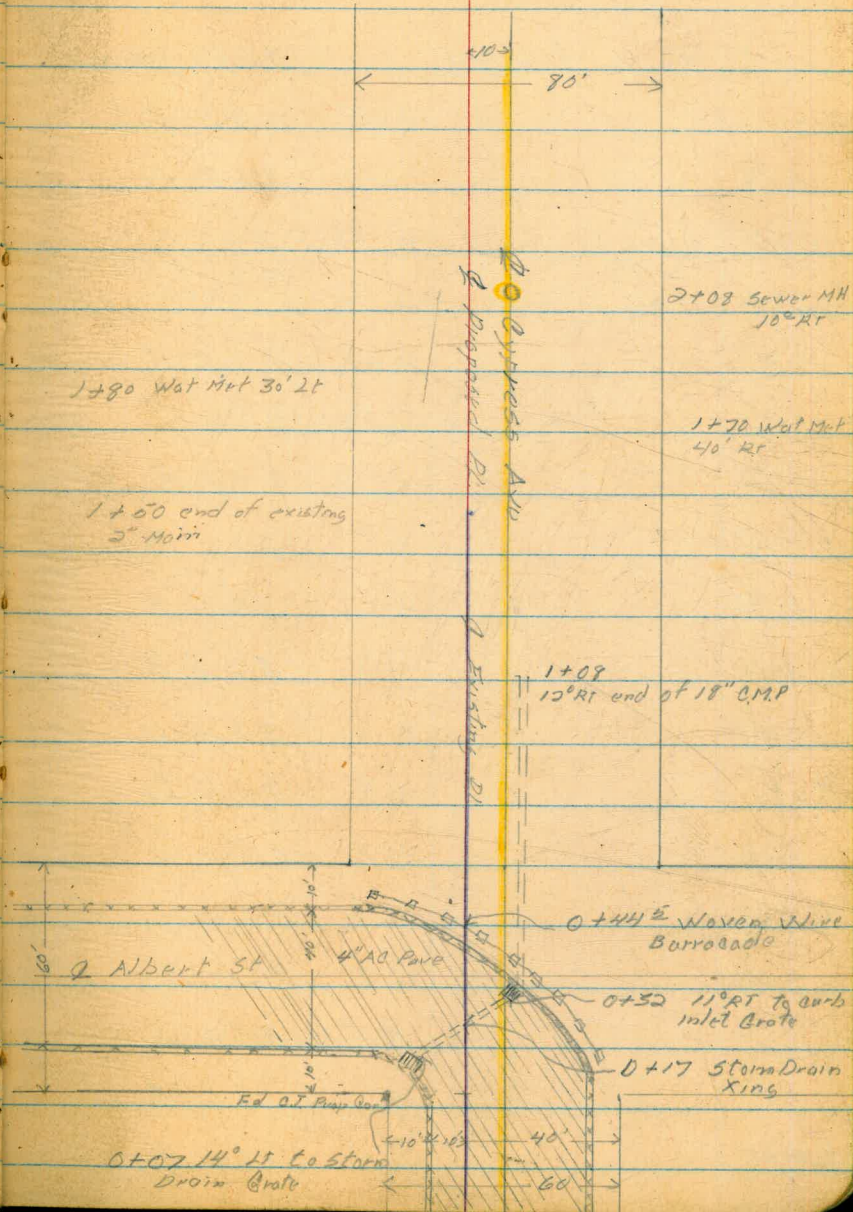
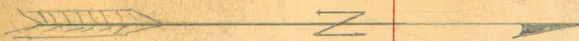
Center Line

Top curb

Top of steep 30° Bank

Bottom of Slope

Top south edge sewer MH 10° RT



0+00 East Prop Line Albert St

Profile Proposed
 Alley 24 N of Orange
 E of 42nd

West
 Martell
 Yaron Fakis

17
 5 Jan 53

Station	Offset	Elevation	Notes
	4.11	368.56	BM S.W. BP 42 nd El Cajon
0+00	6.35	364.45	On sidewalk South side Orange St
+14	6.44	362.2	Top sb
+14 ²	6.91	362.1	Gutter
+40	5.86	361.7	Top east edge sewer MH & Orange
+50	5.82	362.8	328 26
+67	6.50	362.7	Gutter line
+80	6.31	362.1	edge oil
1+00	5.7	362.3	
+50	5.7	362.9	
+50	5.1	363.5	
2+00	5.3	363.3	
+50	4.2	364.4	
3+00	4.8	363.8	
+50	5.1	363.5	
4+00	4.6	364.0	
+50	4.4	364.2	
5+00	4.4	364.2	
+50	4.1	364.5	
6+00	3.3	365.3	

368.56

6+50	3.5	365.1
+67 ²¹	4.98	363.6
7+07 ²¹	5.3	363.3
7+07 ²¹	7.5	361.1
	4.85	363.7 + 7.9 to Flowline
	4.12	364.44

= 364.45

edge oil

B.V. on gutter line

Top stem B.V.

Top east edge Sewer MH & alley
20' east of North prop line El Cajon

Alley 24 N of Orange E of 42nd

Q PL is 3²⁵ east of Q of Alley

6+87²⁰

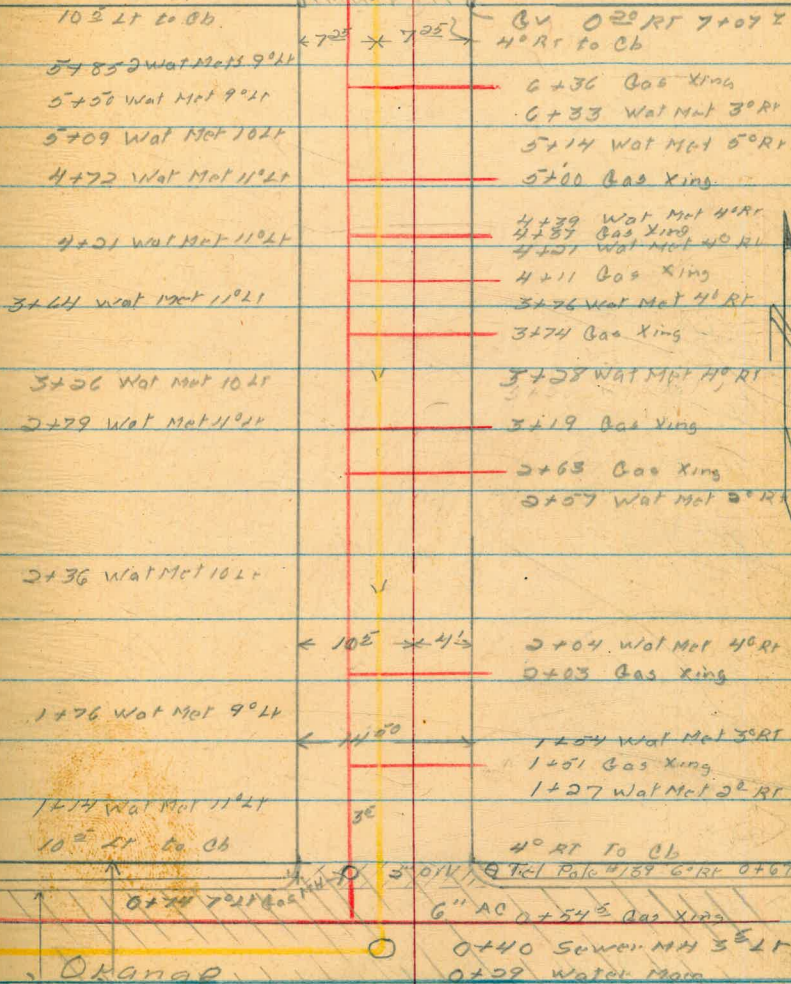
South Prop Line El Cajon

El Cajon Ave

6"-3" CONC. PAVT.

Sewer MH

19



0+00

South Prop Line Orange St

Dream St @ Pl. Profile
 Churchward St NE To Sub Line

West
 Martell
 Varon Fakis

6 Jan 53 20

	9.09	194.21		185.12	BM BP SE Ob Churchward + Imperial
	13.09	205.61	1.69	192.52	
	11.83	216.94	0.50	205.11	
	11.37	227.28	1.03	215.91	
	11.87	236.60	2.55	224.73	
0+00			11.8	224.8	South Prop Line Churchward St
+15 ²⁰			11.85	224.8	Top Ob
+15 ³			12.45	224.2	Butter Line
0+45			12.01	4.78 To Flow	Top east edge Sewer MH 10 ² LT
+50			11.83	224.8	" " " "
+70 ²			11.85	+6.6 To Flow	Top east edge Sewer MH 10 ² LT
+85 ²			11.29		Top Ob
1+00			10.5	226.1	
+50			9.2	227.4	
2+00			7.3	229.3	
+50			5.0	231.6	
3+00			1.6	235.0	
	9.21	245.53	0.28	230.32	
3+50			7.2	237.3	
+71			6.68	+6.90 To Flow	Sewer NH 10 ² LT

245.53

3+96 5.3 240.2

3+96 1.40 241.95 4.98 240.55

1.81 230.95 12.81 229.14

6.35 224.60

Top of 10th RT TBM

= 224.40

3+96 end of 6" AC Water Main

3+79 Wat Net 26 ft

3+71 Sewer MH 10' RT

3+58 end of 2" Main 10' LT

main
2+50 2" 16' LT

1+00 20' LT to 2" Main

0+70 Sewer MH 10' RT
A/100

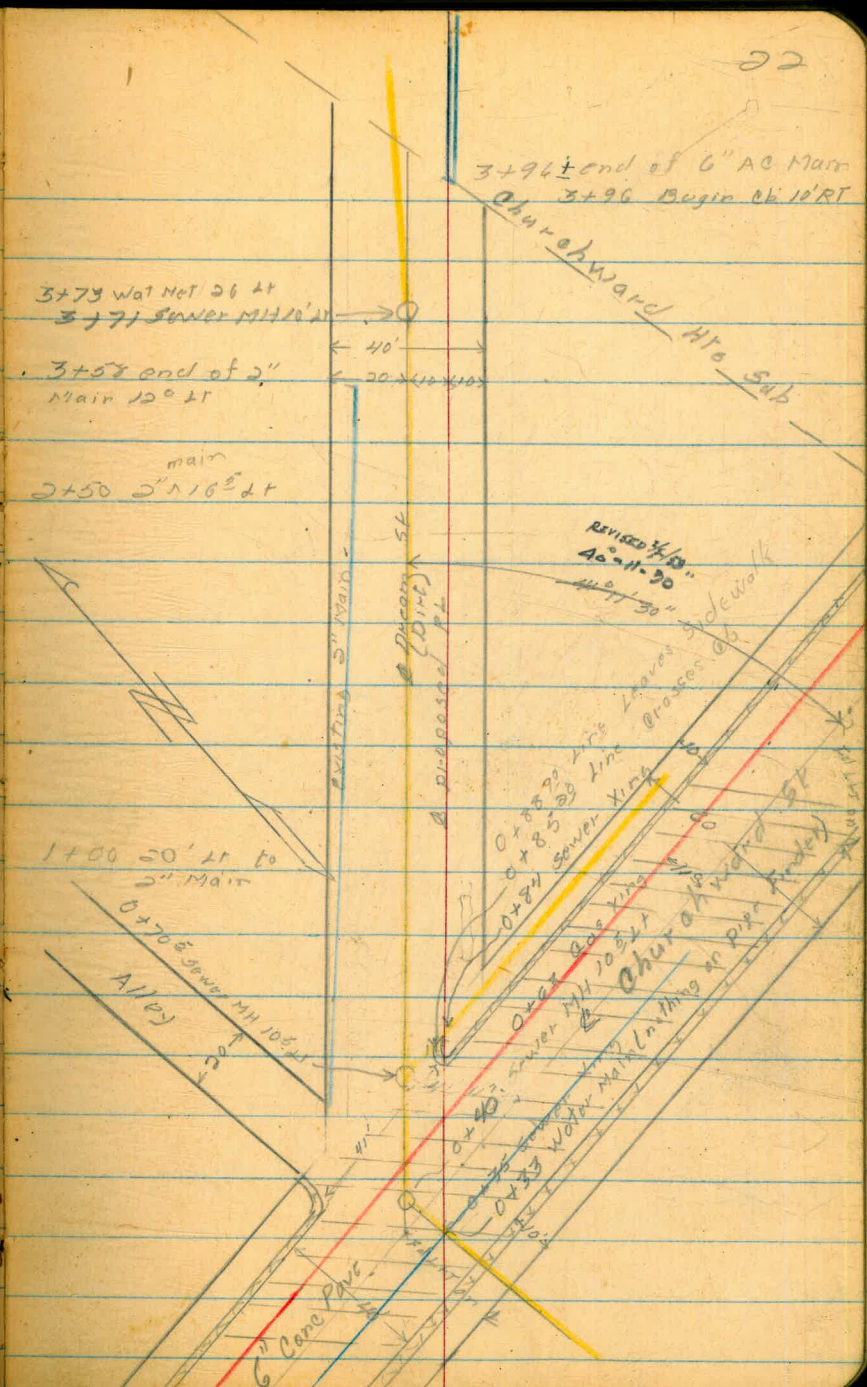
0+00

South Prop Line Cur ahead

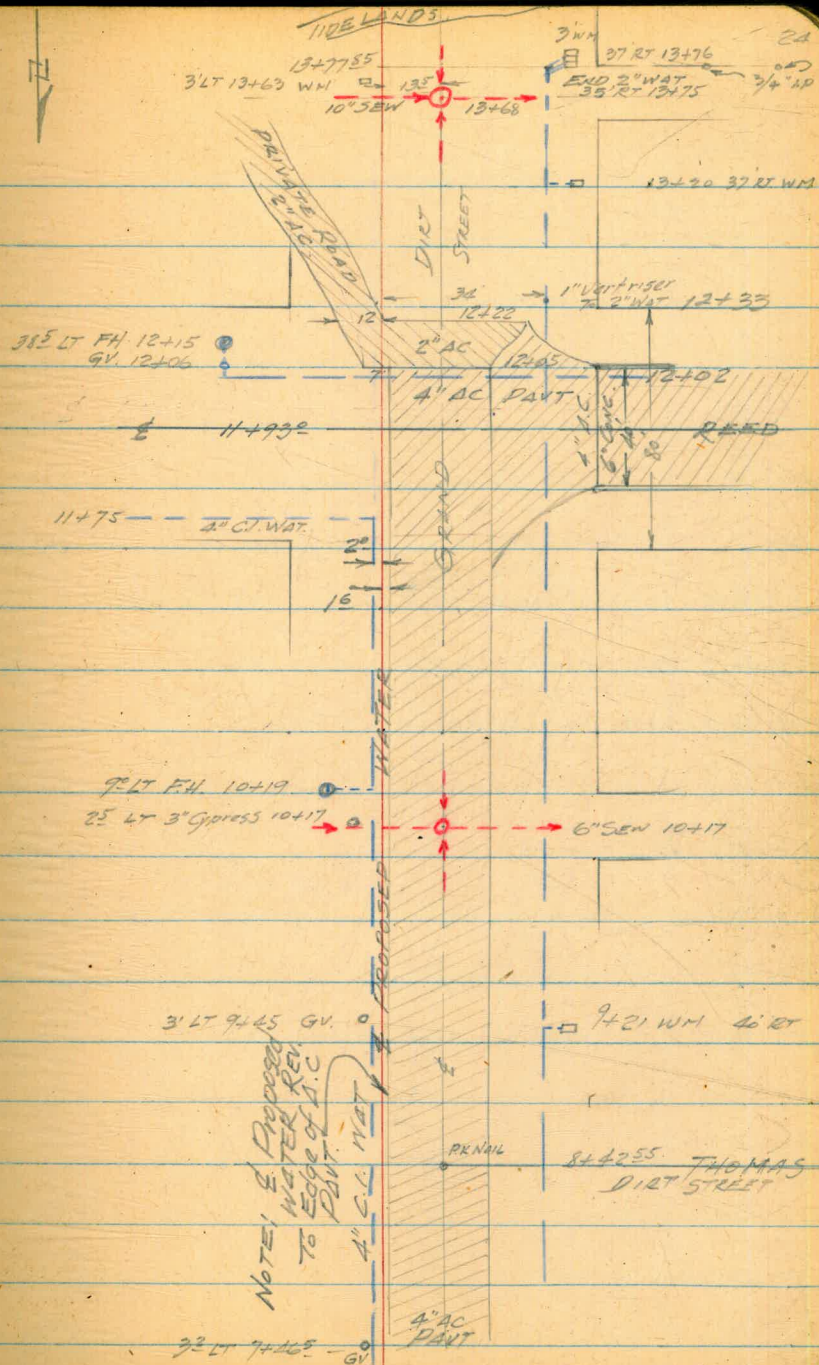
22

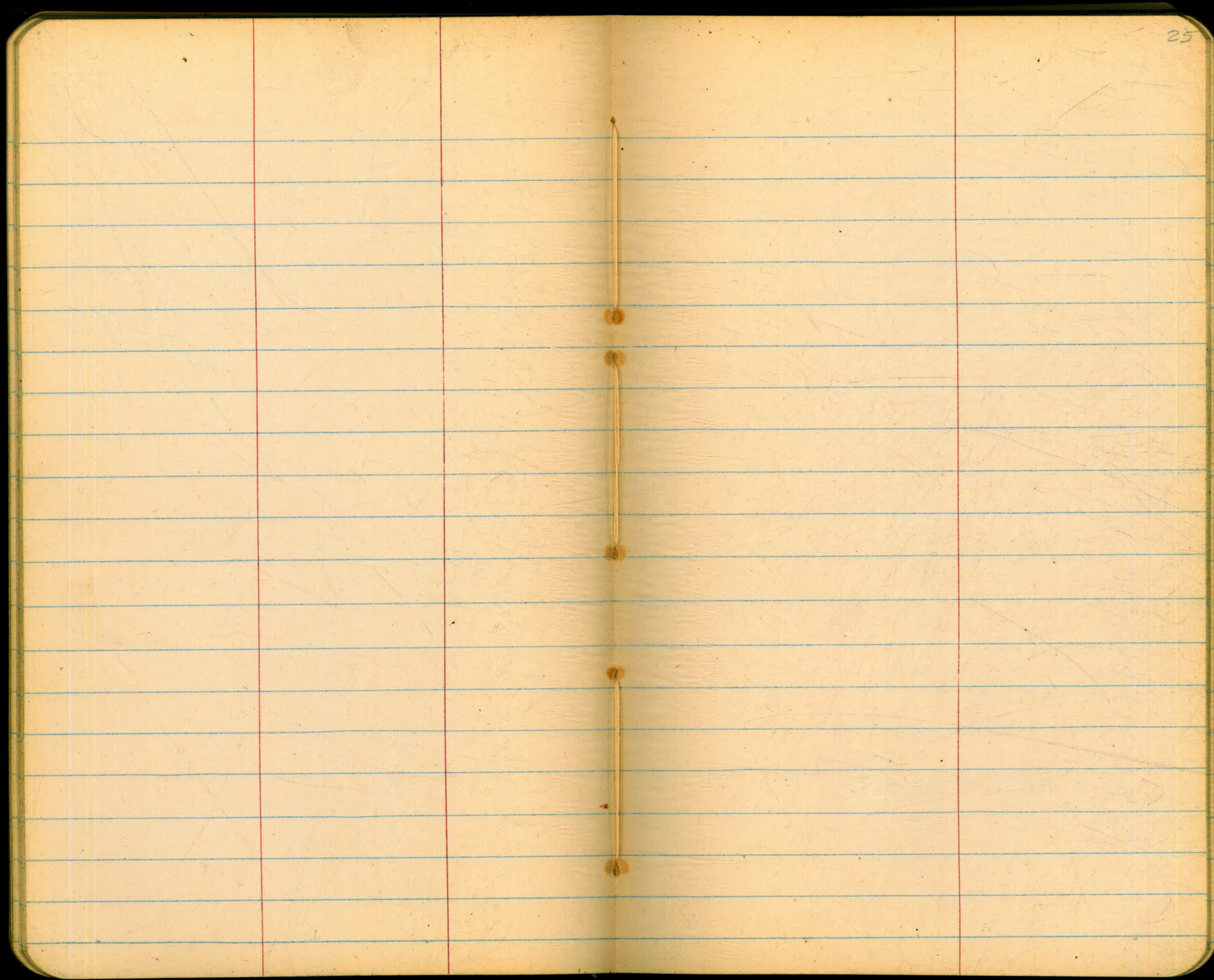
3+96± end of 6" AC Main
3+96 Begin CB 10' RT

Churchward Hts Sub



13+7785 = Sly Prop line of Alley





OLNEY ST.
BALBOA TO OLIVER
♀ PROFILE
PROPOSED WATER

BM	1.47	38.39	36.92
HP	5.59	42.63	1.35 37.04
SET TBM	2.17	41.82	2.98 39.65
0+00		TOP 4" C.I. 175 LT	6.00
			2.5
+50			3.6
1+00			4.4
+50			4.7
2+00			5.4
+10			5.85
+12			5.90
+14.5			5.95
+41			6.32
+50			6.2
3+00			7.2
+01			7.50
+29.5	SEW M.H.	Run 7.45 In 14.85	24.37 26.97
+32			8.05
+50			8.2
4+00			10.1

Mar. 26 1953

26.

B.P. NW Cor Gannet & Pandleton.

NOTE:
♀ Proposed
Water Revised
To Edge of A.C
PAVT.

Ely RIM TELE M.H. 100' RT 0+07

2.60 Header Board Edge
1.7 4" A.C. PAVT.

3.50

1.7

4.05

2.0

4.92

1.7

5.65

1.7

Begin 2' AC Walk (2" THICK)

End 2' AC Walk

Begin 4" AC Driveway

End " "

6.05

1.7

7.40

1.0

Begin 4" AC Driveway

End " "

Begin 25' AC Walk 2" THICK

End 25' AC "

SEW M.H. 135 3+23 6' 7"

8.68

1.7

10.25

1.7

OLNEY ST
(Cont'd.)

3/25/53

27.

	41.82				
4+50		12.47		Begin 4" A.C. Pavt Grand Ave	
HD	0.28	29.50	12.60	29.22	
4+90		1.48		End 4" A.C. Pavt	
5+00		1.5			1.7 Header End Edge 4" A.C.
	SEW M.H.	Rim 10.9	28.41	33' RT 5+02	1.6
+50		INV 13.10			2.52
		2.4			1.6
6+00		3.7			2.85
+07		4.23		Begin 2" A.C. Walk	1.6
+115		4.35		End A.C. Walk	
+33		5.05		Begin 4" A.C. Driveway	
+50		5.3		End " "	
	SEW M.H. 6"	Rim 6.22			5.15
		INV 12.60		133' RT 6+67	1.5
7+00		6.7			6.52
7+01		6.72		Begin 4" A.C. Driveway	1.2
7+24		7.15		End " "	
+50		7.45			7.55
8+00		8.9			1.4
+50		9.7			8.80
9+00		10.8			1.4
+50		12.1			10.0
					1.5
					11.02
					1.6
					12.20
					1.5

OLNEY ST.
(Cont'd.)

3/26/53

28

9+57.5 29.50 12.50

+62 12.65

+83.5 13.10

10+00 2.45 18.83 13.12 16.38

10+00 2.2

SEW M.H. Rim 3.19
11.00

+50 3.25

+51.5 3.18

+73 3.48

+77.5 3.45

11+00 3.9

+50 4.2

+72.40 4.80

12+00 5.30

+22 5.95

+40 in drain ditch 6.4

+41 7.7

+50 8.0

13+00 9.5

Begin 2" AC Walk

End Walk Begin A.C. Driveway

End 4" AC Driveway

13.5 RT 10+17.5

Begin 4" A.C. Driveway

End 4" A.C. "
Begin 2" A.C. Walk

End " " "

4"
Begin A.C. REED ST

End AC PAVT

2.25
1.5

3.05
1.2

3.65
1.5

4.31
1.5

OLNEY ST.
(Cont'd)

3/26/53

29.

18.83

13+50

SEW MH

Rim 12.43
Inv. 20.33 06.40
11.4 -01.50

+77.85

135 RT. 13+68

P

4.19 09.64 13.35 05.45

14+00

4.7

+17

6.3

+27

10.8

+50

11.1

15+00

11.4

SET TBM

11.37 18.95 20.6 07.58

Nail in pole # 4224 40 RT 13+80

SET TBM

3.20 15.75

End curb NW Cor REED & Olney

P

10.74 29.08 0.61 18.34

P

12.08 40.81 0.35 28.73

P

4.66 40.81 4.66 36.15

CR BM

3.85 36.96 = 36.92

4.81
41.64
12.40
29.41

40.81
41.64
6.54
29.20
36.37

SIXS Fair Water Main + Meters
 Alley BIK 201
 East of Boundary
 North of Lincoln

WEST
 WILLIAMS
 VARONFAKIS

8/31/53

30.

	309	351.11	348.02
0+48		1.4	349.7 348.0
40+50		1.4	349.7 344.2
1+0+57		2.5	348.6 347.9
0+77		2.5	348.6 347.8
0+90		3.7	347.4 347.4
1+00		2.9	348.2 343.7
1+1+03		4.0	347.1 347.2
5+1+26		3.5	347.6 346.6
5+50		4.2	346.9 342.1
4+81		6.5	347.0 344.8
4+88 ?		6.1	345.0 344.6
4+2+00		6.3	344.8 340.6
CR 1+34		7.7	343.4 342.6
2+50		8.2	342.9 338.5
+72		9.0	342.1 340.8
3+00		10.7	340.4 336.4
+30		12.0	339.1 338.5
+50		12.8	338.3 334.2
+50		13.1	338.0 338.0

TBM Top Sewer MH Polk

C 1 ³	Wet Met L
C 5 ⁵	
C 0 ⁷	Wet Met RT
C 0 ⁸	W Met LT
C 0 ⁰	W Met RT
C 4 ⁵	
7 0 ¹	WM RT
C 1 ⁰	WM LT
C 4 ⁸	
7 0 ²	WM RT
C 0 ²	WM LT
C 4 ²	
C 0 ⁸	WM LT
C 1 ³	WM LT
C 4 ⁰	
C 0 ⁶	WM LT
C 4 ¹	
C 0 ⁰	WM RT

ALLEY Block 201
CONT.

3+61	351.11	13.4	337.7	337.8
+69		13.5	337.6	337.6
+73		13.8	337.3	337.6
H+00		14.0	337.1	333.4

30 348.1

WEST
WILLIAMS
VARONFAKIS

31

70 ¹	WM RI
C0 ⁰	WM LP
70 ³	DWM LP
C3 ⁷	

Stks For G" AB Main
and Motors
Alley Bk 18, 188, 193
North of Dwight E of Nile

92-53

32

Went
Williams
Varonakis

	4.95	322.00		317.15		130 NE Cor Dwight & Nile
0+30			5.2	316.8	312.2	C4 $\frac{6}{}$
+50			6.6	315.4	312.4	C3 $\frac{0}{}$
+70			5.6	316.4	312.6	C3 $\frac{8}{}$ FH Top
+70			4.3	317.7	317.4	C0 $\frac{3}{}$ (5) Fil
+80			4.7	317.3	317.0	C0 $\frac{3}{}$ 2 WM W
1+00			5.1	316.9	312.8	C4 $\frac{1}{}$
+30			3.6	318.4	312.0	C6 $\frac{4}{}$
+50			7.5	314.5	311.4	C3 $\frac{1}{}$
+59			5.9	316.1	316.0	C0 $\frac{1}{}$ WM W
2+00			5.6	316.4	315.1	C1 $\frac{3}{}$ WM W
2+00			8.8	313.2	310.2	C3 $\frac{0}{}$
Turn +50	5.74	319.15	9.59	313.41		
+50			6.7	312.5	309.4	C3 $\frac{1}{}$
+52			4.7	314.5	313.5	C1 $\frac{0}{}$ WM W
3+00			8.4	310.8	307.7	C3 $\frac{1}{}$
3+00			6.1	313.1	311.9	C1 $\frac{1}{}$ WM W
+50			8.3	310.9	307.3	C3 $\frac{6}{}$
+52			6.7	312.5	311.3	C1 $\frac{2}{}$ WM W

	319.15					
4+00		7.6	311.6	307.5	C4 $\frac{1}{1}$	
+04		6.5	310.7	311.7	C1 $\frac{0}{1}$	W M W
+50		7.6	311.6	308.3	C3 $\frac{3}{1}$	
+48		5.6	313.6	312.5	C1 $\frac{1}{1}$	W M W
+61		7.3	311.9	312.4	F0 $\frac{5}{1}$	W M E
5+00		6.7	312.5	309.0	C3 $\frac{5}{1}$	
+11		4.8	314.4	313.5	C0 $\frac{9}{1}$	W M W
+15		6.1	313.1	313.2	F0 $\frac{1}{1}$	W M E
+40		5.7	313.5	313.5	C0 $\frac{0}{1}$	W M E
5+50		5.2	314.0	309.7	C4 $\frac{3}{1}$	
+65		4.0	315.2	314.4	C0 $\frac{8}{1}$	W M W
+80		3.8	315.4	314.6	C0 $\frac{8}{1}$	W M W
+90		4.4	314.8	314.5	C0 $\frac{3}{1}$	W M E
6+00		4.5	314.7	310.4	C4 $\frac{3}{1}$	
+27		3.7	315.5	315.0	C0 $\frac{5}{1}$	D W M E
+50		3.2	316.0	311.1	C4 $\frac{9}{1}$	
+78 ¹		2.8	316.4	311.5	C4 $\frac{9}{1}$	End of Work
+78 ²		2.6	316.6	316.3	C0 $\frac{3}{1}$	W M W
8.06	324.23	2.78	316.17			Two in Fall ab valley + sandus

304.23

6+90	8.5	315.7			(3) @ FH
7+60	6.9	317.3	312.8	C4 $\frac{5}{3}$	Begin work
760	7.4	316.8	316.5	C0 $\frac{3}{1}$	WMW
+60	6.8	317.4	316.3	C1 $\frac{1}{3}$	WM E
798	5.1	319.1	317.8	C1 $\frac{3}{1}$	DWM W
8+00	6.1	318.1	314.0	C4 $\frac{1}{1}$	
808	5.8	318.4	317.7	C0 $\frac{1}{8}$	WM E
+25	5.4	318.8	318.0	C0 $\frac{7}{9}$	WM W
+35	5.4	318.8	318.1	C0 $\frac{7}{9}$	WM W
+50	6.1	318.1	314.2	C3 $\frac{0}{2}$	
+70	6.3	317.9	317.9	C0 $\frac{2}{4}$	WM E
+72	4.8	319.4	318.2	C1 $\frac{7}{9}$	WM W
9+00	6.3	317.9	314.5	C3 $\frac{1}{9}$	
+11	5.2	319.0	318.3	C0 $\frac{4}{4}$	WM W
+40	4.9	319.3	318.4	C0 $\frac{0}{2}$	WM W
+50	6.2	318.0	314.6	C3 $\frac{0}{2}$	
+78	5.9	318.3	318.3	C0 $\frac{2}{2}$	W E
+93	5.5	318.7	318.5	C0 $\frac{2}{2}$	W W
10+00	6.2	318.0	314.8	C3 $\frac{2}{2}$	

324.23

10+36		5.4	318.8	318.6	C0 $\frac{2}{2}$	WNW
+50		6.4	317.8	314.6	C3 $\frac{2}{2}$	
+79		6.5	317.7	317.7	C0 $\frac{0}{0}$	WNW
+96		5.9	318.3	317.6	C0 $\frac{1}{1}$	W W
11+00		6.6	317.6	313.6	C4 $\frac{0}{0}$	
+12		6.1	318.1	317.0	C1 $\frac{1}{1}$	WNW
+50		8.3	315.9	311.0	C4 $\frac{9}{9}$	
+55		7.2	317.0	315.8	C1 $\frac{2}{2}$	WNW
+75		11.0	313.2	307.6	C5 $\frac{6}{6}$	
+80		8.12	316.11			East 1 st sewer MH
3.27	318.15	9.37	314.86			
7.06	322.11	3.08	315.05			
		4.94	317.17		- 317.15	BD NE Cor Nite + Dright

Alley Bk 18, 188, 193 Cont

West
Williams
Varonakis

9-4-53

36

	4.15	300.26		316.11	
11750			5.3	315.0	311.0
+75			11.5	308.8	306.0
12+12			12.4	307.9	314.0
	1.55	309.59	12.22	308.04	
12+00			5.9	303.7	299.5
+25	4.84	301.55	12.88	296.71	293.3
+50			10.7	290.9	287.0
+65			12.3	289.3	285.4
+75			13.1	288.5	283.6
13+00			12.6	289.0	284.4
+25			8.0	293.6	290.0
	11.42	312.27	0.70	300.85	
+50			9.6	302.7	300.0
+75	6.15	317.38	1.04	311.23	308.6
14+00			1.8	315.6	310.7
+25			5.4	312.0	307.5
+33			1.0	316.4	309.9
	1.23	306.06	12.55	304.93	
+50			4.0	302.1	300.5

	Top east rim	several MH
C 40	$\frac{5.0}{102}$	
C 27	$\frac{11.2}{102}$	
F 6		WM W
C 42	$\frac{5.3}{102}$	
C 34	$\frac{12.6}{92}$	
C 37	$\frac{9.9}{70}$	
C 58	$\frac{13.0}{102}$	
C 41	$\frac{11.9}{72}$	
C 36	$\frac{6.1}{102}$	
C 27	$\frac{9.6}{102}$	
C 26	$\frac{1.0}{102}$	
C 47	$\frac{1.1}{102}$	
C 45	$\frac{5.4}{92}$	
C 65		WM W
C 16	$\frac{3.2}{92}$	

306.06

+75		8.5	297.6	294.0	C 3 6	$\frac{8.2}{104}$	
15+00		8.4	297.2	291.7	C 5 5	$\frac{9.0}{91}$	
+18		4.9	301.2	301.3	F 0 1		WM W
+29		13.3	292.9	288.4	C 4 4	$\frac{13.5}{91}$	Basin Cape engagement
+54		12.8	293.3	288.4	C 4 2	$\frac{12.8}{91}$	und
+91		5.3	300.8	296.1	C 4 2		
16+06		3.9	302.2	303.2	F 1 0		WM E
15+95		5.2	300.9	302.5	F 1 6		WM W
16+25		0.0	306.1	300.6	C 5 5		
	12.74	318.76	0.04	306.02			
16+50		7.8	311.0	304.0	C 7 0		
+50		7.0	311.8	308.0	C 3 3		WM E
+75		5.3	313.5	306.6	C 6 2		
+80		6.1	312.7	310.8	C 1 2		WM W
17+00		3.8	315.0	308.6	C 6 4		
+18		2.3	316.5	313.4	C 3 1		WM E
+46		1.2	317.6	315.5	C 2 1		WM E
+50		0.9	317.9	311.6	C 6 5		

		318.76				
	11.78	329.23	1.31	317.40		
17+96			9.7	319.5	317.8	C 12 WME
18+00			9.3	319.9	314.5	C 54
+15			9.5	319.7	318.5	C 12 WMW
+46			7.5	321.7	320.8	C 03 WME
+50			7.4	321.8	317.5	C 43
+70			5.5	323.7	322.8	C 02 WMW
+75			5.3	323.9	319.0	C 42
19+00			3.5	325.7	320.8	C 49
219			2.9	326.3	326.7	C 06 WMW
T.P.	4.36	330.53	3.06	326.17		
T.P.	7.35	337.77	0.11	330.42		
CHECK To B.M.			4.30	333.47 = 333.40		UNIV. + BOUNDARY N.W.B.P.

34th St Alley S of Adams
to Mountain View Dr \

West
Varonakis

39

	6.42	394.74		388.32		BM	BP	NW	Cor Felton + Adams
0-10			5.4	389.3	386.0	C 43			
0+00			5.4	389.3	385.0	C 43			
+50			5.3	389.4	385.0	C 44			
+75			5.3	389.4	385.0	C 43			
1+00			5.3	389.4	384.5	C 43			
+50			4.9	389.8	383.5	C 63			
+50			4.8	389.9	383.4	C 63			
+75			4.8	389.9	383.0	C 62			
2+00			5.3	389.4	383.0	C 63			
+50			5.0	389.7	384.2	C 55			
3+00			4.8	389.9	385.4	C 42			
+50			4.8	389.9	385.0	C 43			
4+00			4.8	389.9	385.7	C 43			
+50			4.9	389.8	385.7	C 42			
5+00	5.43	395.41	4.76	389.98	385.9	C 42			
+50			5.4	390.0	386.0	C 42			
+66			5.4	390.0	386.0	C 42			FH Tee
+78			5.4	390.0	386.0	C 42			6" QV
+83			5.5	389.9	386.0	C 32			10" x 6" Cross
6+00			5.2	390.0	386.0	C 43			

6+50		395.41	5.3	390.13861	0.42
7+00			5.2	390.23862	0.42
8+50			5.1	390.33863	0.42
9+00			5.1	390.33864	0.39
10+50			5.1	390.33865	0.38
11+00			5.0	390.43865	0.39
12+50			4.6	390.83866	0.42
13+00			4.3	391.13867	0.44
14+50			4.3	391.13868	0.43
15+00			4.3	391.13869	0.42
16+50			4.3	391.13870	0.41
17+00			4.1	391.33871	0.42
18+50			4.1	391.33872	0.41
19+00			3.8	391.63873	0.43
20+50			3.8	391.63874	0.42
21+00	6.56	398.22	3.75	391.663875	0.42
22+50			6.5	391.7387	0.41
23+50			6.3	391.93877	0.42
24+50			6.3	391.93878	0.41

398.22

15170			6.3	391.9	3887	040	6" QV
+75			6.2	392.0	3879	041	6" x 6" Cross
+80			6.2	392.0	3879	041	6" QV
16100			5.9	392.3	3880	042	
+50			5.7	392.5	3880	042	
17110			5.8	392.4	3881	042	
+50			5.5	392.7	3882	042	
18100			5.4	392.8	3883	042	
+50			5.2	393.0	3885	042	
19100			5.2	393.0	3887	043	
+50			5.0	393.2	3889	043	
20100	6.02	399.31	4.93	393.2	3889	042	
+50			6.0	393.3	3893	040	
21100			5.8	393.5	3891	041	
+50			5.9	393.4	3896	038	
22100			5.6	393.7	3891	040	
+32			5.6	393.7	3894	039	6" QV
+37			5.5	393.8	3898	040	6" x 4" Cross
+50			5.3	394.0	3899	041	

399.31

23+00		5.2	394.1	390.0	041
1.50		5.0	394.3	390.2	041
24+00		4.8	394.5	390.3	042
1.50		4.7	394.6	390.5	041
25+00		4.6	394.7	390.6	041
1.50		4.5	394.8	390.7	041
26+00		4.4	394.9	390.9	040
1.50		4.3	395.0	391.1	039
27+00		4.1	395.2	391.2	040
1.50		4.1	395.2	391.3	039
95		4.2	395.1	391.4	039

3.16 396.67 5.80 393.51

4.39 395.30 5.76 390.91

6.92 388.38 = 388.32

390.47
 3.00
 393.53
 3.31
 388.22

388.66
 + 3.06
 391.72
 3.31
 386.41

Qst AC Main C"
30th to 30nd

West
Varanfakie 9-16-53
Kemp

43

	1138	156.33		144.95		USGS Plug NE Cor 30 th + Market
	3.13	158.18	1.28	155.05		
0+00			0.9	157.3	153.5	C 3 ⁹ Beginning of work
1+00			6.4	151.8	148.1	C 3 ²
+50	0.51	146.04	12.65	145.53	141.6	C 3 ⁹
2+00			4.0	142.0	138.6	C 3 ⁴
+50			5.3	140.7	137.8	C 2 ⁹
3+00			5.7	140.3	137.0	C 3 ⁵
+50			6.4	139.6	136.2	C 3 ²
4+00			7.3	138.7	135.3	C 3 ⁴
+50			8.1	137.9	134.5	C 3 ⁴
5+00			9.0	137.0	133.6	C 3 ⁴
	160	138.94	8.70	137.34		
+25			1.8	137.1	133.2	C 3 ²
+50			2.2	136.7	132.9	C 3 ³
6+00			2.8	136.1	132.4	C 3 ²
+50			2.5	136.4	131.8	C 4 ⁶
7+00			3.1	135.8	131.3	C 4 ⁵
+25			4.2	134.7	130.4	C 4 ³
+30			4.8	134.6	130.3	C 4 ³
+50			4.5	134.5	130.2	C 4 ³

FIN Feb

138.94

8+00

5.1 133.8 129.1

0.42

+50

9.1 129.8 126.2

0.32

0.58 126.05 12.94 125.47

9+00

4.8 121.3 117.7

0.36

0.55 114.43 12.17 113.88

+50

1.5 112.9 109.3

0.42

10+00

10.0 104.4 101.3

0.31

0.05 101.49 12.99 101.44

+25

0.7 100.8 97.2

0.31

+50

2.9 98.6 95.3

0.33

11+00

6.3 95.2 91.8

0.34

+50

9.8 91.7 88.3

0.34

0.40 89.49 12.40 89.09

12+00

1.3 88.2 84.6

0.36

+50

4.9 84.6 81.1

0.35

13+00

8.3 81.2 72.6

0.36

+10

9.0 80.5 76.0

0.45

7.77 81.72

= 81.52

Toy. FH SE Cor. 32nd St

81.71

Stks for 8" AC Main + Meters
 Vancouver St. Kalmia to Juniper-

West
 Varonakis
 Kemp 9-17-53

45

	2.15	269.50	267.35			
0+19		4.2	265.3	265.8	FO 5	WM E
+32		4.7	264.8	261.2	C3 6	
+50		4.6	264.9	261.3	C3 6	
+75		6.0	263.5	265.5	F2 0	WM W
+83		2.3	267.2	265.5	C1 7	WM E
1+00		3.7	265.8	261.3	C4 5	
+25		3.3	266.2	261.4	C4 8	
+27		3.1	266.4	265.2	C1 2	WM E
+50		4.1	265.4	261.2	C4 2	
+55		4.5	265.0	266.1	FO 1	WM E
2+00		4.9	264.6	260.9	C3 7	
+02		6.5	263.0	264.9	F1 9	WM E
B C +11		5.1	264.4	260.8	C3 6	
+31		6.0	263.5	264.6	F1 1	WM E
+48		4.0	265.5	264.5	C1 0	WM W
+50		4.8	264.7	260.5	C4 2	
+85		5.3	264.2	264.4	FO 2	WM E
DL 3+01		4.0	265.5	260.2	C5 3	

	269.50					
3+25		3.8	265.7	260.0	C 5	2
+34		4.2	265.3	263.9	C 1	4
	0.81	267.27	3.04	266.46		
3+50		1.2	266.1	263.8	C 2	3
+75		1.0	266.3	259.7	C 6	6
4+25		0.8	266.5	259.3	C 7	2
1+72 ⁶⁴		1.7	265.6	259.0	C 6	6
4+90		3.7	263.6	252.8	C 0	8
5+00		2.8	264.5	258.8	C 5	2
+141		2.7	264.6	263.0	C 1	6
+50		4.2	263.1	258.5	C 4	6
+67		4.0	263.3	262.5	C 0	8
+77		4.7	262.6	262.0	C 0	6
6+00		5.1	262.2	258.0	C 4	2
+08		4.9	262.4	262.2	C 0	2
4+15		4.4	262.9	261.7	C 1	3
+50		5.5	261.8	257.6	C 4	2
+53		3.6	263.7	261.4	C 2	3
7+00		5.5	261.8	256.4	C 5	4
+05		5.5	261.8	256.3	C 5	5

FH. Tee

267.27

7+05

6.1

261.2

261.0

C 0 3

(67) FN

7+30

5.7

261.6

255.7

C 5 9

4.64

262.63

=

262.59

Top of edge Sewer Mill 7+21 10' RL

Birch St Regel to 36th
 Stk. for 6" AO Main + meters

West
 Varon Fakris
 Kemp 9-18-53

48

	4.05	11.50	7.45			1/2" Spike in PP	SE	Over Buta + Bunt
	11.39	22.82	007	11.43				
0+60			5.8	17.0	13.5	C3 ⁵		
1+00			7.7	15.1	12.3	C2 ⁸		
+43			8.1	14.7	15.8	F1 ¹		5 Wat Md
+50			8.1	14.7	11.3	C3 ⁴		
+89			9.1	13.7	14.3	F0 ⁶		WM 5
2+00			9.3	13.5	10.0	C3 ⁵		
+21			9.9	12.9	13.5	F0 ⁶		WM 5
+50			10.0	12.8	13.0	F0 ²		WM 5
2+50			10.0	12.8	9.3	C3 ⁵		
+73			7.5	15.3	13.0	C2 ³		WM N
3+00			11.1	11.7	8.6	C3 ¹		
+50			10.3	12.5	10.0	C2 ⁵		
+60			10.5	12.3	13.8	F1 ⁵		WM 5
+52			7.7	15.1	14.1	C1 ⁰		WM N
+91			5.0	17.8	15.3	C2 ⁵		WM N
4+00			6.7	16.1	11.6	C4 ⁵		
+05			6.6	16.5	15.4	C0 ⁸		WM 5

2282

4+30		4.1	18.7	10.0	C 2 ⁷	WMS
+50		3.4	19.4	13.0	C 6 ⁴	
5+00		2.8	20.0	12.2	C 7 ²	
+26		3.5	19.3	15.5	C 3 ⁸	WMS
+50		4.0	18.8	11.0	C 7 ⁸	
6+00		2.5	15.3	8.9	C 6 ⁴	
	0.55	13.37	10.00	12.82		
+50		1.0	12.4	6.7	C 5 ⁷	
+55		1.4	12.0	6.5	C 5 ⁵ FH Tee	
+55	(5) FH	1.7	11.7	8.7	C 3 ⁰	
7+00		3.0	10.4	4.7	C 5 ⁷	
+20		1.9	11.5	8.0	C 3 ⁵	WMS
+50		5.1	8.3	0.8	C 7 ⁵	
+82		5.0	8.4	-2.0	C 10 ⁴	
8+00		5.0	8.4	-2.0	C 10 ⁴	
+50		6.3	7.1	-2.0	C 9 ¹	
+92		7.1	6.3	-2.0	C 8 ³	
7+00		7.4	6.0	-1.8	C 7 ⁸	
+50		11.5	1.9	-0.8	C 2 ³	

13.37

10+00

8.5

4.9 0.2

C 4 ²

+50

7.8

5.6 0.5

C 5 ¹

11+00

9.5

3.9 0.9

C 3 ⁰

+50

7.8

5.6 1.3

C 4 ³

+85

7.9

5.5 1.6

C 3 ⁹

6.37

10.86

8.78

4.49

3.44

7.42 =

7.45

5.31

5.55

5 P.M. Survey 11/18 10+24

Stks for 6" Main + Motors
Montclair-St Kalmia 550' South

West
Voronfakis
Kemp

9-21-53

51

	2.51	272.01	269.50		BM RD NE cor Kalmia + Montclair	
0+60			5.0	267.0	263.4	C 3 6
+91			2.8	269.2	266.2	C 3 0
1+00			5.0	267.0	262.8	C 4 2
+25			6.2	265.8	260.8	C 5 0
+50			8.2	263.8	260.1	C 3 2
2+00			8.3	263.7	258.6	C 5 4
+00			6.5	265.5	262.5	C 3 0
+50			9.1	262.8	256.6	C 6 3
+54			8.4	263.6	260.7	C 5 2
+87			12.9	259.1	259.9	C 0 2
3+00			11.2	260.8	254.4	C 6 4
+25			12.2	259.8	253.4	C 6 4
+34			12.3	259.7	257.8	C 7 2
+50			13.2	258.8	251.4	C 7 4
	0.63	259.76	12.88	259.13		
+76			2.7	257.1	253.6	C 3 5
4+00			3.1	256.7	247.8	C 8 2
+50			7.3	252.5	242.6	C 9 2
	0.43	247.33	12.86	246.90		

WM E

WM E

WM E

WM W

WM E

WM W

247.33

5+00

2.3 245.0 237.4

C 7 6

+50

11.3 236.0 232.2

C 3 8
C 2 3

+65

14.6 232.7 230.5

FH Tee (C)

moved FH

+65

17.9 229.4 234.3

F 4 9

(5) FH Tee to Avoid

+75

16.7 230.6 228.4

C 2 2

End of work

Fill

12.64 259.34 0.63 246.70

12.03 271.14 0.23 259.11

1.66 269.48 = 269.58

5.70 241.70 236.00

5+25

1.5 240.2 234.8

5 4 FH Tee

5+25

4.4 237.3 239.0

F 1 7

(5) 2 FH

Stks for 6" AC Main + Meters
 Alley BIK #4 E of Chamounc
 N of Orange

West
 Yaronfakis
 Kemp

9-23-53

53

	3.66	356.22		352.56		BM BP NW	Cor 45 th + Orange
0+85	6.40	360.58	2.04	354.18	349.0	C5 ²	Turn on Binney
1+00			5.2	354.8	349.4	C5 ⁴	
+26			5.4	355.2	354.5	C0 ²	WM E
+27			5.4	355.2	354.7	C0 ⁵	WM W
+50			5.2	355.4	350.9	C4 ⁵	
+66			4.8	355.8	355.2	C0 ⁶	WM W
+66			4.9	355.7	355.0	C0 ⁷	WM E
2+00			4.9	355.7	351.0	C4 ⁷	
+19			5.1	355.5	355.3	C0 ²	WM W
+50			4.9	355.7	351.1	C4 ⁶	
+57			4.8	355.8	355.3	C0 ⁵	WM E
+71			4.7	355.9	355.4	C0 ⁵	WM W
3+00			4.9	355.7	351.2	C4 ⁵	
+02			4.8	355.8	355.5	C0 ³	WM W
+50			4.85	355.73	351.4	C4 ³	
+60			4.8	355.8	355.6	C0 ²	WM W
4+00			4.7	355.9	351.5	C4 ⁴	
+05			4.6	356.0	355.8	C0 ²	WM W

		360.58					
4+50	5.38	361.40	4.56	356.02	351.6	C4 ⁴	Turn on Bigger
+54			5.1	356.3	355.8	C0 ⁵	W M W
+82			5.2	356.2	355.9	C0 ³	W M W
5+00			4.9	356.5	351.7	C4 ³	
+32			4.9	356.5	355.1	C0 ⁴	W M W
+32			5.2	356.2	355.9	C0 ³	W M W
+50			4.9	356.5	351.9	C4 ⁶	
+75			5.1	356.3	352.0	C4 ³	
+98			5.0	356.4	356.2	C0 ²	W M W
6+00			4.8	356.6	352.0	C4 ⁶	
+50			4.9	356.5	351.9	C4 ⁶	
+66			5.2	356.2	355.7	C0 ⁵	W M W
+66			4.8	356.6	355.8	C0 ³	W M W
7+00			5.1	356.3	351.8	C4 ⁵	
+08			5.1	356.3	355.8	C0 ⁵	W M W
+50			5.3	356.1	351.7	C4 ⁴	
8+00			5.2	356.2	351.7	C4 ⁵	
+25			5.3	356.1	351.7	C4 ⁴	
+50			6.0	355.4	351.3	C4 ¹	
+75			7.4	354.0	351.0	C3 ⁰	

361.40	357.62
- 5.51	+ 0.34
355.89	356.96
+ 1.35	- 4.40
357.24	352.56 = 352.56
357.63	
357.62	

Alley BIK 62
 Betw Felton & 34th
 From Madison to Alley So of Adams

West
 Williams
 Varonfakis
 Kemp

9-30-53

55

Madison See FB 852-P 23

Nail & proposed PL 7° So of Nly prop line

	765	394.81	387.16			
0+60			6.9	387.9	383.6	C4 $\frac{3}{1}$ Begin work
1+00			4.1	390.7	384.6	C6 $\frac{1}{1}$
+06			4.9	389.9	388.2	C1 $\frac{7}{1}$ W M E
+50			5.4	389.4	385.0	C4 $\frac{4}{1}$
+87			5.4	389.4	388.6	C0 $\frac{8}{1}$ W M W
2+00			5.2	389.6	385.1	C4 $\frac{5}{1}$
+46			4.9	389.9	388.8	C1 $\frac{1}{1}$ W M W
+50			5.1	389.7	385.3	C4 $\frac{4}{1}$
3+00			4.8	390.0	385.4	C4 $\frac{6}{1}$
+07			4.5	390.3	388.9	C1 $\frac{4}{1}$ W M E
+35			4.9	389.9	389.0	C0 $\frac{9}{1}$ W M W
+50			4.7	390.1	385.5	C4 $\frac{6}{1}$
+85			4.4	390.4	389.3	C1 $\frac{1}{1}$ W M W
+89			4.8	390.0	389.3	C0 $\frac{7}{1}$ W M E
4+00			4.9	389.9	385.7	C4 $\frac{2}{1}$
+25			4.3	390.5	389.4	C1 $\frac{1}{1}$ W M W
+34			4.8	390.0	389.5	C0 $\frac{5}{1}$ W M E
+50			4.5	390.3	385.9	C4 $\frac{4}{1}$

394.81

4+98	4.2	390.6	389.6	C1	$\frac{0}{0}$	W M W
+98	4.5	390.3	389.7	C0	$\frac{6}{6}$	W M E
5+00	4.6	390.2	386.0	C4	$\frac{2}{2}$	
+47	4.2	390.6	389.7	C0	$\frac{9}{9}$	W M W
+30	3.9	390.9	389.9	C0	$\frac{3}{3}$	W M E
+50	4.3	390.5	386.2	C3	$\frac{3}{3}$	W M E
+83	4.1	390.7	390.0	C0	$\frac{7}{7}$	W M E
+88	4.1	390.7	389.8	C0	$\frac{9}{9}$	W M W
6+00	4.1	390.7	386.3	C4	$\frac{4}{4}$	
+46	3.9	390.9	390.1	C0	$\frac{8}{8}$	W M E
+48	4.2	390.6	390.0	C0	$\frac{6}{6}$	W M W
+50	3.9	390.9	386.5	C4	$\frac{4}{4}$	
+75	4.2	390.6	386.6	C4	$\frac{0}{0}$	
7+00	3.7	391.1	386.4	C4	$\frac{7}{7}$	
+10	4.0	390.8	386.2	C4	$\frac{6}{6}$	End of Work
	4.39	390.42				

390.39

W edge Gen MH 7+18 49

Poinsettia Dr
Elliott to Alcott
Proposed PL

B.M.	5.70	151.83		146.13
0+00			1.7	150.1
0+15			2.2	149.6
0+50			5.3	146.5
1+00			6.0	145.8
B.C.			8.8	143.0
1+08.73			11.1	143.7
1+50			12.5	139.3
2+00			12.8	139.0
E.C. & B.C.			11.6	140.2
2+53.42			9.8	142.0
4+00			8.1	143.7
4+50			7.1	144.7
5+00			6.5	145.3
5+50			5.70	146.13 = 146.13
Sx. To			7.0	145.5
B.M.	6.34	152.97		
6+00			6.9	145.6
6+50			6.5	146.0
E.C. & B.C.			6.5	146.0
6+25 = B.C.			6.5	146.0
7+00				

West
Williams
Varonfska
Kamp

10-7-53

07

Quits + Poinsettia
End of Top of ab 3-E return
E/L of Elliott

Poinsettia Dr.
Elliott to Alcott
Proposed P.L.

152.47

Shorey
Martell
Alexander

10/8/53⁰⁰ 71

Cont'd

38

7+50	6.3	146.2
8+00	6.2	146.3
8+50	5.9	146.6
9+00	5.4	147.1
9+50	4.8	147.7
10+00	3.5	148.97 = 149.0
10+50	2.4	150.1
11+00	1.3	151.2
11+18 ⁵⁹ = F.C.	0.90	151.6
11+38 ⁵⁹	0.70	151.8
11+70 ⁵⁹	1.07	151.4
Ch. B.M	1.76	150.71 = 150.71

Turned 27°45' to Gate Valve on Alcott St.

Edge Pav't on Alcott St.

Top of Gate Valve Cover

Nail in P.P. @ 10+13 10' Lt.

Poinsettia Dr.
Elliott to Alcott St
Proposed P.L.

Detail on Poinsettia Dr.

0+15 W.M. 1' Rt.
0+27 Gas Main Xing 13' Lt to Gas Valve
0+48 Water Main Xing
0+68 Possible Elec. Conduit for St. Lights
0+80 Intersection Proposed P.L. & Gasline
0+52 4" Water Gate Valve 18' Rt.
1+00 Gasline 3' Rt.
1+03 Water Xing
1+50 Gasline 2' Rt. & W.L. 15' Rt.
2+00 Gasline 2' Rt.
2+13 W.M. 24' Rt. & W.L. 15' Rt.
2+50 Gasline 2' Rt.
2+66 18" Storm Drain 5' Lt. & 23' Rt.
3+00 Gasline 2' Rt. & W.L. 15' Rt.
3+33 W.M. 26' Rt.
3+53⁴² PRC Gasline 3' Rt. & W.L. 15' Rt.
4+00 Gasline 5' Rt. & W.L. 15' Rt.
4+33 W.M. 20' Lt.
4+40 W.M. 21' Lt.
4+50 W.L. 15' Rt. & Gasline 12' Rt.

Shorey
Martell
Alexander

10/8/53

59

7+86 P.L. Xing
+5+00 W.L. 15' Rt. & Gasline 15' Rt.
5+28 12" Storm Drain Xing 56' Lt. & 110' Rt.
Elev. 199.51 139.06
5+46 12" " " " Elev. 192.06
2' Lt.
5+75 W.M. 24' Rt.
7+59 W.M. 5' Lt.
7+65 W.M. 5' Lt.
8+00 W.L. 15' Rt. & Gasline 15' Rt.
8+47 Gas Xing
8+76 W.M. 6' Lt.
9+77 W.M. 6' Lt.
10+08 Gas Xing
10+60 W.M. 26' Rt.
11+36 Telephone Conduit Xing
11+75 2 Gate Valves on Water main 4' Lt & 4' Rt.

Pomsettia St

N-16-53

West
Williams
Varonfakis
Kemp

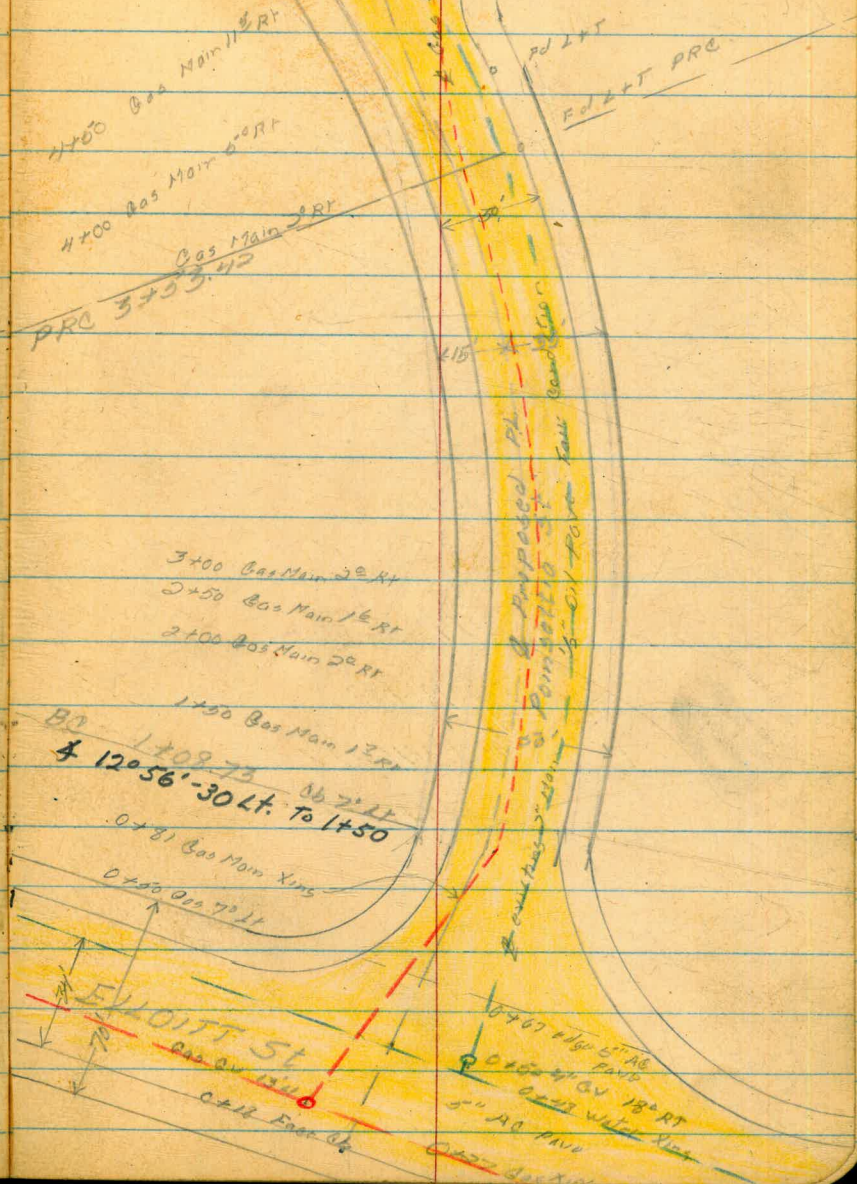
Curtis Co
Curtis St
(Dist in this portion)

3+53.42 PRC + 50
 Δ 11' 06"
 1/2 Δ 5° 33' 00"
 R = 1263.05
 L = 244.69
 1.360891' Dist per ft

BC 1+08.73

0+50

North Prop Line Elliff St



11+18.32

EO

$$\Delta = 11^{\circ}09'30''$$

$$\frac{1}{2}\Delta = 5^{\circ}34'45''$$

$$R = 2174'$$

$$L = 423.39'$$

6+95

EO + POC

$$\Delta = 14^{\circ}36'$$

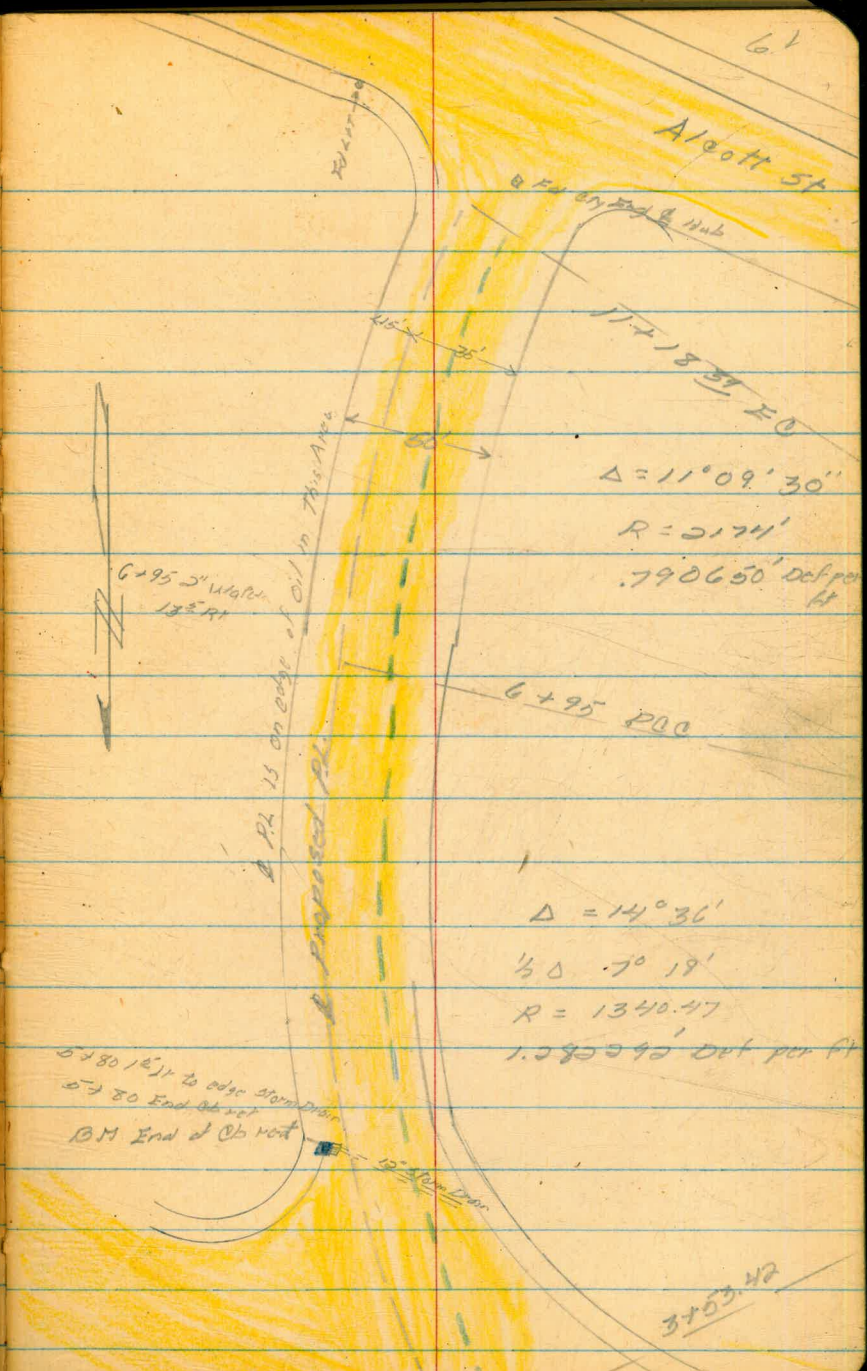
$$\frac{1}{2}\Delta = 7^{\circ}18'$$

$$R = 1340.47$$

$$L = 341.58'$$

3+53.42

EO + POC



61

Alcott St

11+18.32 EO

$$\Delta = 11^{\circ}09'30''$$

$$R = 2174'$$

$$.790650' \text{ offset}$$

6+95 POC

$$\Delta = 14^{\circ}36'$$

$$\frac{1}{2}\Delta = 7^{\circ}18'$$

$$R = 1340.47$$

$$1.285990' \text{ offset}$$

3+53.42

5x80 1/2" to edge of road
5x80 End of set
BM End of Ob vert

6+95 5" Water 18" R1
A Pt. is on edge of Oil in This Area
Proposed Pt.

Alley BIKS 110-123-138
 E of 39th
 Myrtle to Quince St

West
 Williams
 Kemp

12/24/53 65

	5.81	308.78	302.97		BM BP NW Cor	40 th + Redwood
	11.94	313.44	7.28	301.50		
	7.11	320.01	0.54	312.90		
0+85		6.2	313.8	308.8	C5	$\frac{0}{0}$ Begin Work
1+00		6.3	313.7	308.7	C5	$\frac{0}{6}$
1+21		7.2	312.8	312.2	C0	WMW
1+50		7.6	312.4	307.2	C5	$\frac{2}{2}$
	0.45	311.78	8.68	311.33		
1+95		0.3	311.5	310.4	C1	$\frac{1}{1}$ WME
2+00		0.6	311.2	306.0	C5	$\frac{2}{8}$
2+06		1.0	310.8	310.0	C0	WMW
2+18		1.1	310.7	309.7	C1	$\frac{0}{1}$ WME
2+50		1.9	309.9	304.7	C5	$\frac{2}{5}$
2+67		3.4	308.4	307.9	C0	$\frac{5}{8}$ WMW
3+00		3.9	307.9	303.1	C4	$\frac{1}{8}$
3+04		3.8	308.0	306.9	C1	$\frac{1}{1}$ WME
3+41		4.8	307.0	305.8	C1	$\frac{2}{2}$ WME
3+50		5.2	306.6	301.4	C5	$\frac{2}{8}$
3+32		5.2	306.6	305.8	C0	$\frac{8}{8}$ WMW

ALLEYS 110 123 138
CONT.

311.78

3+73 5.6 306.2 304.7

C1 $\frac{5}{3}$

WM E

4+00 6.7 305.1 299.8

C5 $\frac{6}{6}$

WM W

+02 7.7 304.1 303.5

C0 $\frac{2}{2}$

WM E

+07 7.1 304.7 303.5

C1 $\frac{0}{0}$

+50 8.6 303.2 298.2

C5 $\frac{2}{2}$

+63 8.9 302.9 301.7

C1 $\frac{6}{6}$

WM E

5+00 10.6 301.2 296.6

C4 $\frac{4}{4}$

WM W

+15 11.6 300.2 299.8

C0 $\frac{8}{8}$

+50 12.1 299.7 294.9

C4 $\frac{8}{8}$

+72 12.7 299.1 298.3

C0 $\frac{8}{8}$

WM E

0.20 299.17 12.81 298.97

6+00 2.5 296.7 290.6

C6 $\frac{1}{8}$

+10 4.0 295.2 298.0

F2 $\frac{2}{2}$

WM E

+25 7.6 291.6 286.4

C5 $\frac{6}{6}$

+36 9.8 289.4 283.8

C5 $\frac{3}{3}$

20° Bend

+62 10.1 289.1 283.8

C5 $\frac{6}{6}$

20° Bend

+75 3.2 296.0 289.4

C6 $\frac{6}{6}$

+78 3.0 296.2 300.8

F4 $\frac{6}{6}$

WM E

11.89 310.22 0.84 298.33

WEST
WILLIAMS
KEMP

12/24/53

63

ALLEYS

110 123 138

CONT.

310.22

7+00		11.2	299.0	295.4
+50		10.0	300.2	296.4
+90		7.5	302.7	301.7
+92		6.7	303.5	301.8
8+00		7.1	303.1	298.2
+50		6.0	304.2	299.8
+57		6.0	304.2	303.4
+86		5.4	304.8	304.2
9+00		4.9	305.3	300.4
+37		3.7	306.5	305.0
+50		3.5	306.7	301.0
10+00		4.3	305.9	301.6
+10		4.3	305.9	305.2
+50		5.0	305.2	301.1
+90		5.3	304.9	304.6
11+00		5.5	304.7	300.6
	1.20	306.03	5.39	304.83
+50		1.6	304.4	300.1
+52		1.5	304.5	304.0

WEST
WILLIAMS
KEMP

12/24/53

64

11¹/₄ BEND

C3 ⁶/₈
 C3 ⁰/₉
 C1 ⁷/₉
 C1 ⁷/₉
 C4 ⁴/₈
 C4 ⁸/₉
 C0 ⁶/₉
 C0 ⁹/₅
 C4 ⁷/₃
 C0 ⁷/₁
 C4 ¹/₃
 C0 ³/₁
 C4 ¹/₃
 C4 ³/₅
 C0 ⁵/₅

WME

W.M.W.

W.M.W.

WME

WME

WME

2 W.M.W.

WME

ALLEYS

110 123

138

WEST
WILLIAMS
KEMP

65

CONT.

12/24/53

306.03

11+60		16	304.4	304.0	C0	$\frac{4}{5}$?	WMW
12+00		18	304.2	299.7	C4	$\frac{5}{8}$		
+39		21	305.9	303.1	C0	$\frac{8}{5}$		WME
+50		23	303.7	299.2	C4	$\frac{5}{4}$		
+95		29	303.1	298.7	C4	$\frac{4}{5}$		Water meter on even sto
13+00		3.0	303.0	302.5	C0	$\frac{5}{1}$		WM E
+50		4.1	301.9	297.8	C4	$\frac{8}{5}$	297.1	C4
14+00		5.7	300.3	296.8	C3	$\frac{5}{1}$		
+35		5.0	301.0	296.3	C4	$\frac{7}{5}$		Fit Tee
+35		4.9	301.1	301.0	F0	$\frac{5}{5}$		⊙ ⊙ FIT
+39			301.5				?	WM E
15+35		4.3	301.7	300.2	C0	$\frac{5}{1}$		WMW
+40		5.8	300.2	300.1	C0	$\frac{5}{5}$		WMW
+50		6.5	299.5	296.0	C3	$\frac{5}{5}$	294.0	C5 $\frac{5}{5}$
16+00		6.5	299.5	296.0	C3	$\frac{5}{5}$	294.0	C5 $\frac{5}{1}$
+50		6.9	299.1	295.6	C3	$\frac{5}{5}$	294.0	C5
	1.93	301.50	6.44	299.59				
17+00		2.5	299.0	295.0	C4	$\frac{0}{8}$	294.0	C5
+50		2.7	298.8	294.6	C4	$\frac{2}{8}$	294.0	C4

ALLEYS

110

123

138

CONT.

301.52

18+00

3.3

298.2 293.9

C4 $\frac{3}{0}$

294.0

C4 $\frac{2}{0}$

+50

4.7

396.8 292.8

C4 $\frac{0}{2}$

19+00

5.6

395.9 291.7

C4 $\frac{2}{1}$

+50

6.8

294.7 290.6

C4 $\frac{1}{5}$

20+00

7.5

294.0 289.5

C4 $\frac{5}{0}$

+50

9.1

292.4 288.4

C4 $\frac{0}{4}$

+85

9.5

292.0 287.6

C4 $\frac{4}{4}$

2" @ V

+90

9.6

291.9 287.5

C4 $\frac{4}{8}$

6" CROSS

21+00

10.4

291.1 287.3

C3 $\frac{8}{5}$

+15

11.0

290.5 287.0

C3 $\frac{5}{2}$

FH T&D

+15

10.8

290.7 290.5

C0 $\frac{2}{1}$

② Q FH

+25

11.2

290.3 290.2

C0 $\frac{1}{F}$

RM F

6.11

305.90

1.78

299.79

2.89

303.01 = 302.97

4.05

307.02

302.97

11/13/54

BM BP NW1 Cor. 40th & Redwood

13+75

6.5

300.5 296.3

C4 $\frac{2}{5}$

14+05

6.2

300.8 295.3

C5 $\frac{5}{7}$

+35

6.1

300.9 294.2

C6 $\frac{7}{4}$

+50

7.6

299.4 294.0

C5 $\frac{4}{4}$ WEST
WILLIAMS
KEMP

66

12/24/53

ALLEYS

110 123

128

CONT.

307.02

15.00

2.6 299.4 294.0

15.0

2.6 299.4 294.0

4.05 302.97

WEST

WILLIAMS

VARONFAKIS

KEMP

1/13/54

67

C 5 ⁴

C 5 ⁴

Grand Ave Ingraham
to Cass
Top of existing PL

4.73	59.17	54.44		
287.5	East	401	55.16	
3+14 ⁹²	west	13.11	46.06	
0.37	46.74	12.80	46.37	
7+66 ⁸⁰		8.02	38.72	
9+91 ³⁰		11.44	35.38	
1.34	36.81	11.27	35.47	
13+69 ⁵⁰		6.49	30.32	
16+11 ⁴⁰		9.67	27.14	
17+78 ³⁰	582	30.55	12.08	24.73
20+25 ²⁵		8.50	22.05	
10.11	39.82	0.89	29.71	
7.58	46.83	0.57	39.25	
		3.36	43.47 = 43.47	

West
Williams
Vorontakis
Kemp

1-21-54

68

NW (S) plug Grand + Hayes

0+00 west prop line baints

Mon NE Cor. Grand + Gresham

POINSETTIA DR.
 ELLIOTT TO ALCOTT
 ③ STKS & GRDS FOR 8" A.C. WATER

FEB. 10, 1934

DEATTY
 SHREY
 MARTELL
 ALEXANDER

69

BM	4.23	150.36	146.13	
0+48		0.6	149.8	145.0 C48 ±
0+53		0.8	149.6	144.7 C49
0+55	Begin Work	0.8	149.6	144.6 C50
1+00		3.9	146.5	142.1 C44
1+08 ⁷³	B.C.	4.7	145.7	141.6 C41
1+50		7.6	142.8	139.1 C37
2+00		9.9	140.5	136.55 C40
2+50		11.2	139.2	134.0 C52
3+00		11.4	139.0	134.0 C50
3+50		10.2	140.2	136.1 C41
3+53 ⁴²	P.R.C.	10.1	140.3	136.2 C41
4+00		8.6	141.8	138.2 C36
4+50		7.1	143.3	140.0 C33
5+00	8'x6" Cross	6.1	144.3	140.0 C43
5+50		5.4	145.0	140.0 C50
6+00		5.1	145.3	141.5 C38
6+50	7.00	4.94	145.42	141.8 C36
6+95	P.R.C.	6.7	145.7	142.1 C36

POINSETTIA DR
(CONT. D)

2/10/54

70.

152.42

7+00	6.7	145.7	142.1	C36
7+50	6.4	146.0	142.4	C36
8+00	6.2	146.2	142.7	C35
8+50	5.9	146.5	143.0	C35
9+00	5.5	146.9	143.2	C37
9+50	4.7	147.7	144.2	C35
10+00	3.7	148.7	145.1	C36
RP nail in pole	1.72	150.68 =	150.71	
10+50		149.8	146.3	C35
11+00		150.9	147.5	C34
11+ ³⁵ 28 END WORK		151.4	148.0	C34±
11+47±? EXISTING 6" A.C.				
WATER METS.				

2+12 Wly
3+35 Wly
4+33 Ely 2' met
5+18 Wly
5+26 Wly

behind
existing
cut

152.42

7+54 Ely	4.9	147.5	147.3	C02
7+65 Ely	4.9	147.5	147.4	C01
8+97 Ely	4.5	147.9	148.1	F03
9+77 Ely	2.9	149.5	149.7	F02
10+60 Wly	1.4	151.0	150.6	C04
CK BM	6.29	146.13		

2435 Poinsettia

2425 "

STERLING COURT
 ALTADENA TO LEMONA
 ⑤ STKS & GRDS FOR 6" A.C. WATER

FEB. 15 1954

71.

BARTY
 SUREY
 MARTELL
 ALEXANDER

BM.	11.11	319.67	308.56	3/4" I.P. SE COR 51ST & Sterling Ct.
CK H			8.63 311.04 = 311.05 = 311.03	(pg 12 C. Engr. FG 2230) CITY ENGR. DISK & 51ST 26' N & 5' West of Sterling
0+47			3.6 316.1	C49
0+55	Begin Work		3.6 316.1	C47
0+50			3.6 316.1	C47
1+00			2.8 316.9	C50
1+50			2.6 317.1	C45
2+00			3.2 316.5	C45
2+50			5.5 314.2	C43
3+00			7.3 312.4	C47
3+25			8.7 311.0	C44
3+50			9.1 310.6	C56
3+70	6" TEE		10.6 309.1	C49
3+95	F.H. TEE		12.2 307.5	C42
3+90	⑤ F.H.		11.3 308.4	C12 C51
4+25	2.26 309.56		12.37 307.30	C35
			3.8 305.8	
4+50			4.9 304.7	C32
5+00			6.9 302.7	C27
5+50			6.1 303.5	C45
5+72	2" B.O. End Work		6.1 303.5	C49
CK BM			1.00 308.56 = 308.56	

303.7

2.7

303.5

0.1

303.6

0.0

2/15/54

72.

51ST ST.STERLING COURT TO SO. TERMINUS
(5) STKS & GRDS FOR 6" AC. WATER

BM		320.83	308.56	3/4" IR Jc. Cor. 51 ST & Sterling Ct.	
0+35	6" TEE		11.3 309.5	304.2	C53
0+40			11.2 309.6	304.7	C49
0+50			10.5 310.3	303.7	C46
1+00			5.5 315.3	310.9	C44
1+10	905	327.88	2.00 318.83		
1+50			6.3 321.5	316.0	C45
2+00			3.0 324.9	318.6	C63
2+50			4.3 323.6	317.6	C60
3+00			8.7 319.2	314.8	C44
3+10	2.01	318.57	11.32 316.56		
3+50			4.3 314.3	310.0	C43
4+00			11.3 307.3	302.6	C47
4+10 ⁴⁰	2" B.O. End work		14.2 304.4	301.2 300.2	C33
IP pin			11.62 306.95		

2/15/54

STERLING COURT

51ST ST

② STKS & GRDS for WAT. METS.

STERLING COURT

BM	7.06	318.10	311.04	
1+04 S			1.4 316.7	315.8 C09
1+62 N			0.3 317.8	316.8 C10
1+91 S			1.1 317.0	315.8 C12
2+29 N			3.3 314.8	314.7 C01
3+10 N			6.0 312.1	311.3 C08
4+38 N	0.45	311.49	4.3 307.2	305.9 C13
4+60 S			7.7 303.8	304.8 F10
5+72 Ely			4.7 306.8	302.5 C43
5+72 Ely			6.3 305.2	303.0 C22
CK BM			2.94 308.55 = 308.56	

OK of MET STK. D. @ 25 RT & LT & ST.

? Altadena
 5116 Sterling Ct.
 5119 " "
 5128 " "
 5138 " "
 New House Number "
 5151 " "
 17' Nly of Sly Line Sterling Ct. 3659 Lemonia
 18' Sly of Sly Line Sterling Ct. 3647 "

51ST ST

IP p10	12.76	319.71	306.95	(109.72)
3+24 E			4.5 315.2	316.2 F10
IP (310)	8.08	327.28	0.51 319.20	
3+02 W			6.8 320.5	318.3 C22
2+37 W			2.3 325.0	322.6 C24
2+26 E			5.2 322.1	322.4 F03
1+78 E			5.0 322.3	322.2 C01
1+26 W			6.8 320.5	318.3 C22
IP	3.45	318.10	12.63 314.65	
0+72 W			3.9 314.2	311.9 C23
CK BM			7.06 311.04 = 311.04	

3611 51ST ST
 3616 " "
 3628 " "
 3627 " "
 3635 " "
 3644 " "
 3652 " "

MASON ST.
 CONGRESS - JEFFERSON
 ② STRS & GRDS FOR WAT. METS.
 (10996-L)

FEB. 23, 1954

Beatty
 Shroyer
 Marfell
 Alexander

74

BM	6.92	25.42	18.50	BP W. Cor Congress & Mason		
0+00 - SWly Prop line CONGRESS				C13	3930 Mason	
1+14 NWly		5.0	20.4	19.1	C13	3928 "
1+41 "		4.9	20.5	19.3	C12	3929 "
1+47 SEly		4.3	21.1	19.8	C13	3904 "
1+71 NWly		4.7	20.7	19.4	C13	3914 "
2+19 "		4.4	21.0	19.7	C13	?
2+92 SEly		4.3	21.1	20.5	C06	

FEB. 23 1954

75

"K" ST
 FRANCIS TO 35TH
 ④ STR. S & GRDS FOR 6" A.C.

Beatty
 Sherry
 Martell
 Alexander

BM. 3.16 88.08 84.92
 TP 12.28 95.95 4.41 83.67

B.P. SW. COR.
 PARDEE & L

TP 2.24 97.85 0.34 95.61
 ID 8.32 93.07 13.10 84.75

on @ LT. W. side

35TH ST.

9+00 AT 6" TEE 11.9 81.2 77.4

C38

81.1

12.0

2

9+25 11.1 82.0 78.0

C40

82.3

10.8

2

9+50 5.3 87.8 79.4

C84

85.2

7.9

2

10+00 6.5 86.6 82.0

C16

86.7

6.2

2

10+50 9.9 83.2 82.0

C12

85.1

8.0

2

11+00 2.4 90.7 84.4

C63

91.0

2.1

2

ID 9.56 98.51 4.12 88.95

C67

93.8

2.7

2

11+25 4.6 93.9 87.2

C54

96.1

2.4

2

11+50 2.6 95.9 90.5

C41

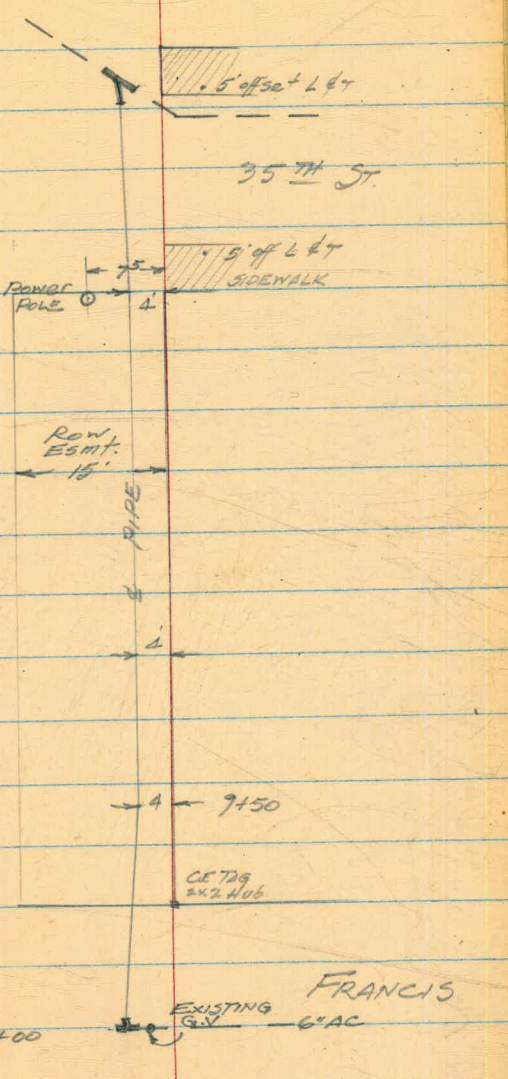
96.5

2.0

2

11+80¹⁵ AT End of WYE 2.4 96.1 92.0

CK TP 2.90 95.61



EXISTING G.V.

FRANCIS 6" A.C.

9+00

FEB. 24, 1954

DEATY
SHOEN
MARTELL
ALEXANDER

76

ARBOR DRIVE
INGALLS TO 11315
②. GRDS & STRS FOR 6" A.C.
6245-W

BM	1.13	274.16	273.03		SW. CP. ARBOR DRIVE & JACKSON
0+05	6" GV	12.3	261.9	258.9	C30
0+00	AT FH TEE	12.6	261.6	258.5 259.0	C31
0+13	45° BEND	12.1	262.1	256.8 255.4	C53
0+25		13.2	261.0	254.8	C62
0+32.15	DK. 45° BEND	12.9	261.3	255.3 254.8	C65
0+39.33	AH.			254.8 255.2	C70
0+50		12.4	261.8		
1+00		7.5	266.7	262.2	C45
1+50		5.8	268.4	264.4	C40
2+00		3.5	270.7	266.6	C41
2+50		1.8	272.4	269.0	C34
2+88.5	6" CROSS	1.3	272.9	270.0 269.0	C29
3+00		1.7	272.5	269.6 269.0	C29
3+50		3.6	270.6	266.8	C38
4+00		5.9	268.3	264.6	C37
4+35	End Work	7.1	267.1	263.4	C37
CK. BM.	1.13	273.03			

0+13 258.6
15.6 Both End Existing 6"

0+13 259.1
15.1 Top 18" CMP.

0+27 256.6
17.6 Top 12" CMP

0+27 257.2
17.0 Top 6" Conc Sewer

1/2" A.C. on
6" Conc PAVT } 2+54.8
2+88.5 16' RT. 6" } Top 270.53
C.I. } 266.3
3+05

OLIPHANT ST
90' SELY of Evergreen ST
To EXISTING TEE on Evergreen
(4) STK.S & GRDS for 6" WATER

3/1/53
BRATTY
SHOVEL
MARTELL
ALEXANDER

PLAN 6174-W

BM	10.03	50.70		40.67	
0+00			Top of Edd of Curb		
0+05			11.3	39.4	35.3 35.0
0+25			4.4	46.3	38.0 36.8
IP	13.18	63.82	0.00	50.66	41.0
0+50			9.7	54.1	39.1
0+75			1.7	62.1	43.0 41.4
IP	12.92	76.51	0.25	63.59	
IP	13.34	85.03	4.82	71.69	65.4
1+20			8.7	76.3	75.5
			Bottom Exist 6" TEE		
			9.5	75.5	
IP	10.70	95.67	0.06	84.97	

L & T SELY Cor NEWELL & EVERGREEN

10.9
3.5
14.4
28.3

C41
C95 C93
C150 C131
C207 C191
C63
C08

3/1/54

POE ST.
 100' Sely of Evergreen ST
 To Existing TEE on EVERGREEN
 (4) GRDS & STRS for 6" WATER
 95.67

	Top Bell 6" TEE	5.5	90.2		
		6.3	89.4		
1+29	AT END Existing 6" TEE on Evergreen	2.6	93.1	89.4	C37
1+00		10.1	85.7	81.8	C39
IP	0.85	83.18	13.34	82.33	
0+75		7.8	75.4	71.2	C42
IP	0.46	70.29	13.35	69.83	
0+50		5.3	65.0	60.6	C44
IP	0.46	57.59	13.16	57.13	
0+25		2.8	54.8	50.0	C48
IP	0.22	44.57	13.24	44.35	
0+00	End Exist 6" newly installed	0.2	44.4	34.4 43.4	C112
IP	0.03	31.67	12.93	31.64	
IP	0.61	19.04	13.24	18.43	
IP	5.36	11.95	12.35	06.69	
CK BM		5.83	06.12 = 06.03		

2 ft 7' SW POE & R-SECRAS

INDEX

6137-W ^{90'} ~~8~~
 PONDSETTA DR, Elliot to Alcott, - 8" A.C. WATER 69-70 ✓
 6138-W ~~8~~
 STERLING COURT, ALTADENA to LEMONA - 6" AC WAT 71. ✓
 51ST ST Sterling Ct to Sly Terminus - 6" AC WAT 72 ✓
 Sterling Ct & 51ST, Wat Meters 73. ✓
 5464-W
 Mason St, Congress to Jefferson - Wat Meters 74 ✓
 "K" St, Francis to 35TH St - 6" A.C. Water 75 ✓
 ARBOR Drive, Ingalls to Ibis - 6" A.C. Water 76 ✓
 6174-W
 Elephant St 90' SEly to Evergreen - 6" Wat. 77 ✓
 POE ST 100' SEly to Evergreen - 6" Wat. 78 ✓
 alive

48	81
2.0	20
2.8	61
	118
	17.9

6.9
2.0
4.9
11.8
16.7

11.8
2.8
14.6

271.1
12.3
258.8

80. 5226
 9.85
 9.056

9.40
 5.51
 3.91

9.27
 5.50
 3.77

7.025
 3.200
 3.825

9.21
 5.50
 3.71

6.95
 3.12
 3.83

61
 POISS East West
 7.025 13.20

5157
 Starck
 Mason
 "K" ST
 ARBO
 Olph
 ROE

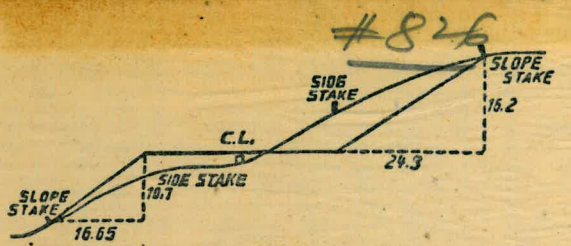
105.33
 20.75
 146.25
 8.90
 139.85
 2.80
 140.15
 12.09
 128.06
 58
 128.64
 3.17
 125.47

Birch
 Top Sewer Mt
 10+74 5.91

45
 3.2
 1.3

128.64
 12.05
 116.09 60
 50 1.9
 116.59 4.1
 12.80
 103.79
 1.45
 105.24
 3.80
 102.44

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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