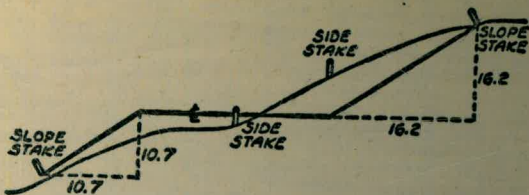


#827



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the center of side stake is located by the double entry method in left column and top row. The number of feet from side stake to slope stake is given in the right column. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not raise the sight instrument needed.

Room 903 Civic Center

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TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Profile (only) South Pl. 188-244+50

alice ✓
1-25

Profile - SUTG. P.L.

King 7-22-52
Williams T.
Jacobs &
McHenry

	+	H-I	-	Elev.
T.B.M.	2.17	1809.53		1807.36

188+00	2.9	1806.5		
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+50	4.6	1804.93		
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188+59.49 P.O.T.	4.86	1804.67		
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188+95	7.4	1802.13		
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189+03	11.6	1797.93		
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T.P.	8.39	1817.55	0.37	1809.16
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189+25	6.7	1810.85		
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+50	5.7	1811.85		
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189+78	5.2	1812.35		
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Nail intro 5' Rt Sta. 188+50

11.6	9.6	2.0	LT 2.0	4.6	Rt.	13.0
+5.0	+1.0	-4.2	+4.6	-2.0	+6.4	
45'	35'	28'	28'	21'	40'	

157 94.1	2.4	22.2	98.9	3.5	9.9	14.9
10.8	-2.5	-5.7	+6.7	+1.4	+5.0	+1.0
40'	18'	16'	10'	8'	28'	42'

23.1	20.6	15.1	98.9	4.1	9.5
+21.0	+18.5	+13.0	3.4	+2.0	+7.4
45'	30'	24'	2'	20'	50'

23.1	20.5	14.9	0.9	97.9	1.9	3.6	9.0
+25.3	+22.5	+17'	+3.0	0.0	+4.0	+5.7	+11.1
45'	35'	25'	35'	3'	6'	24'	51'

20.4	18.9	14.9	3.8	1.3	96.9
+9.5	8.0	4.0	-7.1	-9.6	14.0
42'	28'	14'	27'	40'	50'

22.4	20.5	16.1	4.6	2.1	98.1
+10.0	+8.1	+3.7	-7.8	-10.3	-14.2
40'	28'	14'	22'	40'	47'

Suth. P.L.

1817.55 ✓

+

H1

-

ELEY

189+87 ✓

7.8 ✓

✓1809.75

190+00 ✓

5.4 ✓

✓1812.15

+50 ✓

1.8 ✓

✓1815.75

191+00 ✓

1.2 ✓

✓1816.35

T.P. ✓

5.97 ✓

1822.42 ✓

1.10 ✓

✓1816.45

191+55 ✓

4.6 ✓

✓1817.82

Solid
Rock

191+77 ✓

9.3 ✓

✓1813.12

Drain

192+00 ✓

0.0 ✓

✓1822.42

T.P. ✓

11.57 ✓

1833.99 ✓

0.0 ✓

✓1822.42

1829.09

192+50 ✓

4.9 ✓

✓1829.09

KING
WILLIAMS T
JACOBS T
Mc HORNEY

7-22-52

HOT

2.

(L+)

(R+)

16.8
+3.0
40'
14.9
+5.1
35'
11.3
+1.5
20'

2.8
-7.0
28'
52.7
-10.1
40'
96.7
-13.1
71'

19.3
+7.1
48'
18.2
+6.0
37'
14.5
+2.3
19'

6.8
-5.4
21'
1.7
-10.5
40'
94.2
-18.0
42'

22.8
+7.0
40'
18.8
+3.0
20'
17.6
+1.8
10'

10.4
-5.4
25'
5.4
-10.4
40'

29.1
+12.7
25'
23.2
+6.8
17'
20.1
+3.7
10'

10.4
-6.0
22'
4.2
-12.2
44'

NOV 11 191-191+55-Solid Rock L.H.O.E.

27.7
+9.9
40'
21.5
+3.7
10'

12.7
-5.1
8'
6.4
-9.4
30'
3.8
-19.2
41'

30.8
17.7
45'
25.5
+12.4
30'
20.6
+7.5
18'
16.7
+3.6
10'

6.6
-6.5
16'
4.9
-8.2
32'
1.9
-11.2
45'

35.4
+12.0
42'
26.4
+4.0
10'

15.0
-7.4
33'
11.8
-10.6
30'
5.4
-17.0
41'

+19.0
45'
+10.6
25'
+4.7
10'

8.0
18'
+13.4
31'
-21.9
40'

S44. P2.

KING
WILLIAMS T
JACOBS +
Mc HORNEY

7-22-52

HOT

3

1833.99 ✓

H1

FLEV ✓

T. P. 1.79 ✓ 1835.74 0.04 ✓ 1833.95 ✓

192+82 ✓ 1.3 ✓ 1834.44 ✓

$\frac{+19.1}{45'}$	$\frac{+13.1}{33'}$	$\frac{+4.1}{10'}$	$\frac{-7.1}{16'}$	$\frac{-13.2}{35'}$	$\frac{-20.0}{50'}$
---------------------	---------------------	--------------------	--------------------	---------------------	---------------------

193+05 ✓ 1.4 ✓ 1834.34 ✓

$\frac{+18.0}{45'}$	$\frac{+12.6}{32}$	$\frac{+4.5}{10'}$	$\frac{-5.4}{17'}$	$\frac{-18.6}{47'}$
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 Old 2x2 hnb
 T. B. M. 0.7 ✓ 1835.03 ✓
 193+01-4+15

193+50 ✓ 6.2 ✓ 1829.54 ✓

$\frac{+23.2}{46'}$	$\frac{+18.7}{38}$	$\frac{13.3}{28}$	$\frac{+8.0}{12'}$	$\frac{+5.0}{10'}$	$\frac{-12.1}{27'}$	$\frac{-17.0}{36'}$	$\frac{-22.1}{46}$
---------------------	--------------------	-------------------	--------------------	--------------------	---------------------	---------------------	--------------------

194+00 ✓ 8.9 ✓ 1826.84 ✓

$\frac{+23.8}{49'}$	$\frac{+13.0}{30'}$	$\frac{+7.0}{10'}$	$\frac{-10.0}{21'}$	$\frac{-13.4}{42'}$	$\frac{-14.0}{49'}$
---------------------	---------------------	--------------------	---------------------	---------------------	---------------------

T. P. 1.28 ✓ 1824.16 ✓ 12.86 ✓ 1822.88 ✓

194+21 ✓ 0.0 ✓ 1824.16 ✓

$\frac{+15.1}{50}$	$\frac{+12.0}{35'}$	$\frac{+5.0}{20}$	$\frac{+4.3}{10'}$	$\frac{-5.4}{11}$	$\frac{-10.4}{26}$	$\frac{-16.0}{42}$	$\frac{-20.1}{50'}$
--------------------	---------------------	-------------------	--------------------	-------------------	--------------------	--------------------	---------------------

194+37 ✓ 7.6 ✓ 1816.56 ✓

$\frac{26.4}{45'}$	$\frac{21.0}{37'}$	$\frac{+15.6}{20}$	$\frac{+6.3}{10'}$	$\frac{-5.4}{20'}$	$\frac{-9.9}{39}$	$\frac{-10.9}{45}$
--------------------	--------------------	--------------------	--------------------	--------------------	-------------------	--------------------

194+50 ✓ 3.8 ✓ 1820.36 ✓

$\frac{12.0}{45}$	$\frac{+10.7}{40}$	$\frac{+7.7}{32}$	$\frac{+7.1}{16}$	$\frac{+4.5}{10}$	$\frac{-10.1}{20}$	$\frac{-14.2}{38}$	$\frac{-16.8}{44}$
-------------------	--------------------	-------------------	-------------------	-------------------	--------------------	--------------------	--------------------

Suth. Pl

1824.16 ✓

.H1

FLEX

KING

7-22-52

HOT

WILLIAMS T

JACOBS T

Mc HORNEY

(L+)

(R+)

4

19470.37 ✓
P.O.T

3.4 ✓

✓ 1820.76

$$\begin{array}{r} +9.1 \\ 20' \end{array} \quad \begin{array}{r} +4.1 \\ 32' \end{array} \quad \begin{array}{r} +1.2 \\ 10' \end{array}$$

$$\begin{array}{r} -3.8 \\ 13' \end{array} \quad \begin{array}{r} -13.0 \\ 47' \end{array} \quad \begin{array}{r} -15.8 \\ 49' \end{array}$$

195400 ✓

13.8 ✓

✓ 1810.36

T.P.

9.04

1820.02

13.18

1810.98

195408 ✓

11.9 ✓

✓ 1808.12

$$\begin{array}{r} +16.1 \\ 45' \end{array} \quad \begin{array}{r} +13.0 \\ 36' \end{array} \quad \begin{array}{r} +3.5 \\ 18' \end{array}$$

$$\begin{array}{r} -2.0 \\ 29' \end{array} \quad \begin{array}{r} -5.1 \\ 43' \end{array} \quad \begin{array}{r} -6.1 \\ 50' \end{array}$$

195436 ✓

10.4 ✓

✓ 1809.62 ✓
1809.82
$$\begin{array}{r} +4.1 \\ 50' \end{array} \quad \begin{array}{r} +5.9 \\ 28' \end{array} \quad \begin{array}{r} +0.5 \\ 10' \end{array}$$

$$\begin{array}{r} -2.3 \\ 13' \end{array} \quad \begin{array}{r} -7.9 \\ 30' \end{array} \quad \begin{array}{r} -12.7 \\ 42' \end{array} \quad \begin{array}{r} -1.4 \\ 45' \end{array}$$

195473 ✓

-27.6 ✓

✓ 1792.42

$$\begin{array}{r} +1.0 \\ 46' \end{array} \quad \begin{array}{r} +5.7 \\ 37' \end{array} \quad \begin{array}{r} +6.5 \\ 30' \end{array} \quad \begin{array}{r} +2.7 \\ 18' \end{array} \quad \begin{array}{r} +1.9 \\ 10' \end{array}$$

$$\begin{array}{r} -1.5 \\ 20' \end{array} \quad \begin{array}{r} -6.2 \\ 50' \end{array}$$

196400 ✓

-19.4 ✓

✓ 1800.62

$$\begin{array}{r} +3.0 \\ 45' \end{array} \quad \begin{array}{r} +7.9 \\ 32' \end{array} \quad \begin{array}{r} +0.5 \\ 10' \end{array}$$

$$\begin{array}{r} -6.4 \\ 25' \end{array} \quad \begin{array}{r} -9.0 \\ 35' \end{array} \quad \begin{array}{r} -1.4 \\ 45' \end{array}$$

196465 ✓

1.7 ✓

✓ 1818.32

$$\begin{array}{r} +10.8 \\ 44' \end{array} \quad \begin{array}{r} +5.4 \\ 30' \end{array} \quad \begin{array}{r} +0.5 \\ 10' \end{array}$$

$$\begin{array}{r} -5.0 \\ 23' \end{array} \quad \begin{array}{r} -6.4 \\ 50' \end{array} \quad \begin{array}{r} -8.7 \\ 40' \end{array} \quad \text{P.O.T. OK}$$

T.P.

12.58

1831.34

1.26

1818.76

TURN ON ROCK CHISEL D

197400 ✓

9.2 ✓

✓ 1822.17

$$\begin{array}{r} +12.0 \\ 40' \end{array} \quad \begin{array}{r} +8.7 \\ 30' \end{array} \quad \begin{array}{r} +5.5 \\ 20' \end{array} \quad \begin{array}{r} +2.8 \\ 10' \end{array}$$

$$\begin{array}{r} -3.8 \\ 17' \end{array} \quad \begin{array}{r} -10.5 \\ 26' \end{array} \quad \begin{array}{r} -15.1 \\ 40' \end{array}$$

Suth P2

KING
WILLIAMS T
JACOBS †
Mc HORNEY

7-22-52

HOT

5.

1831.34 ✓

+

HI

-

ELEV.

(LT.)

(RT)

(28)

197+39 ✓

6.8 ✓

✓ 1824.54

$\frac{+9.4}{39}$ $\frac{+4.4}{10}$

$\frac{-2.8}{10}$ $\frac{-10.1}{24}$ $\frac{-14.6}{35}$ $\frac{18.0}{43}$

197+62 ✓

9.7 ✓

✓ 1821.64

$\frac{+15.4}{37}$ $\frac{+10.0}{28}$ $\frac{+4.3}{10}$

$\frac{-6.5}{22}$ $\frac{-8.0}{35}$

198+00 ✓

1.4 ✓

✓ 1829.94

Notes: 196x90 - 197x85
Rectangular
analysis

T.P.

11.38 ✓

1841.29 ✓

1.43 ✓

1829.91 ✓

TURN ON RK BLUE O

198+21 ✓

10.2 ✓

✓ 1831.09

198+50 ✓

-14.3 ✓

✓ 1827.0

198+98 ✓

-18.0 ✓

✓ 1823.3

BOTTOM DRAW

199+20 ✓

5.6 ✓

✓ 1835.69

T.P.

11.29 ✓

1852.38 ✓

0.20 ✓

1841.09 ✓

199+50 ✓

10.4 ✓

✓ 1841.98 ✓

Sht 3+6 Sec I

Syth PL.

KING
WILLIAMS &
JACOBS &
Mc HORNEY

7-22-52

Hot

6.

1852.38 ✓

H1

-

ELEV.

200+00 ✓

2.8 ✓

✓ 1849.58

200+50 ✓

2.4 ✓

✓ 1849.98

201+00 ✓

3.6 ✓

✓ 1848.78

+50 ✓

6.6 ✓

✓ 1845.78

T.P

4.25 ✓

1844.31 ✓

12.32 ✓

1840.06 ✓

ON BOB

201+90 ✓

7.0 ✓

✓ 1837.31

202+23 ✓

31.3 ✓

✓ 1813.01

BOTTOM CREEK

202+58 ✓

5.00 ✓

✓ 1839.31

T.B.M. ✓

3.76 ✓

1840.55 ✓

218 + 67.69 AM.
2x2 HOB. STA A 202+68.57 BK EQUATION

T.P

1.98 ✓

1846.29 ✓

0.00 ✓

1844.31 ✓

Suth P. 2

KING

7-22-52

HOT

7

WILLIAMST

JACOBS +

Mc HORNEY

1846.29

+

HI

-

ELEV.

219+00 ✓

1.4 ✓

✓1844.89

219+42 ✓

6.5 ✓

✓1839.79

~~219+50~~~~9.3~~~~1836.99~~

219+67 ✓

21.4 ✓

✓1824.89

BOTTOM DRAW

219+82 ✓

9.8 ✓

✓1836.49

220+00 ✓

12.1 ✓

✓1834.19

~~220+31.58~~~~1.5~~~~1844.79~~

T.P. ✓

12.42 ✓

1858.53 ✓

0.18 ✓

1846.11 ✓

220+45 ✓

13.8 ✓

✓1844.73

T.P. ✓

12.69 ✓

1870.99 ✓

0.23 ✓

1858.30 ✓

Su H. P. 2.

KING
WILLIAM ST
JACOBS +
McHORNEY

7-22-52

HOT

8.

1870.99 ✓

+ HI - ELEV.

220463 ✓

13.8 ✓

✓ 1857.19

221400 ✓

5.4 ✓

✓ 1865.59

~~221417~~

~~3.5~~

~~1867.49~~

T.P.

✓ 13.23 ✓ 1883.87 ✓ 0.35 ✓ 1870.64

221450 ✓

9.3 ✓

✓ 1874.57

EDGE NAKONEY RD.

222400 ✓

3.9 ✓

✓ 1879.97

EDGE RD.

T.P.

✓ 8.39 ✓ 1892.23 ✓ 0.03 ✓ 1883.84

T.B.M.

6.04 ✓ 1886.19

SPIKE IN GATE POST NAKONEY RANCH

222450 ✓

7.6 ✓

1884.63

223400

4.7

1887.53

Revised
see 768x-19

Suth Pt

KING 7-22-52
WILLIAMST
JACOBS +
MC HORNEY

HOT

9.

1892.23

HI

FLEV

P.O.T.

6.64 1885.59

STA.
2x2 Hub 223+51.95

T.P.

0.94

1880.22

12.95 1879.28

~~223+64~~

223+67

2.6

1877.62

224+00

11.3

1868.92

224+06

15.2

1865.02

BOTTOM RAVINE

224+31

14.9

1865.32

T.P.

0.81

1867.92

13.11 1867.11

224+53

9.2

1858.72

224+88

3.3

1864.62

Revised

713825-19

KING.
WILLIAMS T 7-22-52 HOT
JACOBS +
MC HORNEY

10.

	+	1867.92 HI	-	ELEV.	
T.B.M.			7.27	1860.65	
T.P.	5.16	1863.20	9.88	1858.04	
225+45			10.2	1853.00	
225+59			5.5	1857.70	
T.B.M.	2.35	1863.00	2.55	1860.65	
225+79			5.8	1857.20	
226+00			16.1	1846.90	
T.P.	2.14	1852.97	12.17	1850.83	
226+15			-15.1	1837.87	
226+35			-18.6	1834.37	

STA.
OLD 2x2 HUB 225+25.45 A

OLD 2x2 HUB STA. 225+25.45 A

Revised
7/28/55-19

KING
WILLIAMST 7-23-52 HOT
JACOBS †
Mc HORNEY

11.

	+	1852.97 HI	-	ELEV.	
226+60			5.2	1847.77	✓
226+97			8.4	1844.57	✓
227+09			6.2	1846.77	✓
227+33			16.8	1836.17	✓
227+44			23.4	1829.57	✓
T.P	0.82	1843.97	9.82	1843.15	✓
227+62			9.0	1834.97	✓
228+00			6.1	1837.87	✓
228+35			11.4	1832.57	✓
228+50			15.2	1828.77	✓

BOTTOM DRAW

TOP BANK

Revised
7B 8 25-19

KING
WILLIAMSBIT 7-23-52 HOT
JACOBS †
MC HORNEY

12

	+	1843.97 HI	-	ELEV	
228+64				21.2	1822.77
228+76				13.5	1830.47
229+00				10.1	1833.87
T.P.	0.75	1834.89	9.83	1834.14	
229+32				4.8	1830.09
229+50				4.6	1830.29
229+74				4.1	1830.79
T.B.M.				5.53	1829.36
230+33				8.6	1826.29
230+36				4.7	1830.19

BOTTOM DRAW

Revised
7/28/52

Δ STA 229+96.34

EDGE LARGE ROCK ON ♂

TOP ROCK ON ♂

SuH P2.

KING

WILLIAMS T 7-23-52

HOT

13

JACOBS †

Mc HORNEY

		1834.89 HI	8.9 8.2	ELEV	26.0 1826.69
230 + 50	+				
230 + 40					
231 + 00			13.0		1821.89
T.P.	0.94	1823.75	12.08	1822.81	
231 + 50			8.2		1815.55
232 + 00			11.2		1812.55
232 + 14			12.2		1811.55
T.P.	0.82	1811.41 1811.41	13.16	1810.59	
232 + 40			9.7		1801.71
232 + 50			7.5		1803.91
232 + 78			8.2		1803.21

EDGE ROCK

Revised

FB 8/25/52

ROCK BLUE @ 232 + 19

SOUTH PL.

~~1811~~ 1811 241

+

HI

-

ELEV.

233+00

9.8

1801.61

T.P.

0.44

1799.40

12.45

1798.96

~~233+30~~~~0.3~~~~1799.10~~

233+60

4.3

1795.10

233+87

8.3

1791.10

T.P.

1.07

1787.80

12.67

1786.73

234+71

18.5

1769.30

BOTTOM DRAW

235+00

11.3

1776.50

235+50

4.7

1783.10

236+00

3.5

1784.30

KING
WILLIAMS T
JACOBS +
MC HORNEY

7-23-52

14

HOT

Revised to
233+28
7B 8 1/2 219

SOUTH PL

KING

WILLIAMST

JACOBS +

Mc HORNEY

7-23-52 HOT

15

1787.80 ✓

HI

- ELEV.

236+31 ✓

5.1 ✓

✓1782.70

236+55 ✓

13.1 ✓

✓1774.70

236+89 ✓

3.1 ✓

✓1784.70

~~237+00~~~~2.7~~~~1785.10~~

237+50 ✓

2.67 ✓

✓1785.13 ✓

T.P. ✓

0.81 ✓

✓1785.94 ✓

2.67 ✓

✓1785.13 ✓

237+96 ✓

3.64 ✓

✓1782.30 ✓

1st Hub

238+50 ✓

8.8 ✓

✓1777.14 ✓

238+81 ✓

14.3 ✓

✓1771.64 ✓

T.P. ✓

0.73 ✓

✓1774.10 ✓

12.57 ✓

✓1773.37 ✓

S42P2

1774.10 ✓

#1

ELEV.

KING

WILLIAMST

JACOBS +

7-23-52 HOT

14

MC HORNEY

~~239+00~~~~8.8~~~~1765.30~~

239+31 ✓

18.1 ✓

✓1756.00

T.P.

3.46 ✓

1764.67 ✓

12.89 ✓

1761.21 ✓

239+58 ✓

7.6 ✓

✓1757.07

239+89 ✓

18.1 ✓

✓1746.57

240+02 ✓

27.4 ✓

✓1737.27

BOTTOM CREEK

240+15 ✓

16.8 ✓

✓1747.87

240+60 ✓

5.4 ✓

✓1759.27

240+90 ✓

7.2 ✓

✓1757.47

241+00 ✓

9.8 ✓

✓1754.87

Sydney P.L.

1764.67

+

H1

-

ELEV.

KING
WILLIAMS T
JACOBS T
McHORNEY

7-23-52

HOT

17

241+13 ✓

15.9 ✓

✓1748.77

241+50 ✓

4.5 ✓

✓1760.17

242+00 ✓

3.0 ✓

✓1761.67

242+50 ✓

2.4 ✓

✓1762.27

T.P.

6.96 ✓

1768.99 ✓

2.64 ✓

1762.03 ✓

243+00 ✓

7.5 ✓

✓1761.49

243+50 ✓

5.3 ✓

✓1763.69

244+00 ✓

3.8 ✓

✓1765.19

244+50 ✓

6.7 ✓

✓1762.29

T.B.M

5.30 ✓

1763.69

Back

1763.60

✓ 1764.10 Ahead

OLD 2x2 HUB 22849055

Pass 1-18
CHVD. REC 30-Jan-53

Profile Suth. RL
Sta. 13+50 -

KING
WILLIAMS T
JACOBS +

8-11-52 HOT

18.

Mc HORNEY

$\frac{+200}{40}$	$\frac{+13.0}{29}$	$\frac{+7.6}{21}$	$\frac{0.0}{10}$	$\frac{-0.9}{8'}$	$\frac{+1.7}{12'}$	$\frac{+2.0}{12'}$	$\frac{-10.0}{40'}$
-------------------	--------------------	-------------------	------------------	-------------------	--------------------	--------------------	---------------------

$\frac{+25.0}{33}$	$\frac{+20.0}{27}$	$\frac{+6.1}{12}$	$\frac{-5.4}{7}$	$\frac{-9.1}{13}$	$\frac{-13.0}{35}$
--------------------	--------------------	-------------------	------------------	-------------------	--------------------

$\frac{+27.0}{33}$	$\frac{+20.0}{26}$	$\frac{+13.0}{19}$	$\frac{+7.6}{12}$	$\frac{-17.2}{25}$	$\frac{-22.6}{8}$
--------------------	--------------------	--------------------	-------------------	--------------------	-------------------

$\frac{+22.5}{36}$	$\frac{+15.2}{24}$	$\frac{+13.0}{20}$	$\frac{+7.6}{12}$	$\frac{-5.4}{9}$	$\frac{-16.3}{28}$	$\frac{+21.7}{30}$
--------------------	--------------------	--------------------	-------------------	------------------	--------------------	--------------------

$\frac{+22.1}{42}$	$\frac{+17.2}{31}$	$\frac{+11.8}{20}$	$\frac{-5.5}{12}$	$\frac{-12.0}{24}$	$\frac{-17.4}{32}$	$\frac{-22.8}{40}$
--------------------	--------------------	--------------------	-------------------	--------------------	--------------------	--------------------

+	HI	-	ELEV
TBM 4.94 ✓	1933.26 ✓		1928.32 ✓
13+50 ✓		6.5 ✓	26.8 ✓
14+00 ✓		3.6 ✓	29.7 ✓
14+23 ✓		3.1 ✓	30.2 ✓
14+50 ✓		6.9 ✓	26.4 ✓
15+00 ✓		8.2 ✓	25.1 ✓

T.P. 4.55 ✓ 1936.52 ✓ 1.29 ✓ 1931.97 ✓ on 15+37 hub.

15+50 ✓		4.6 ✓	31.9 ✓
16+00 ✓		5.1 ✓	31.4 ✓ $\frac{+23.0}{40}$
16+50 ✓		6.0 ✓	30.5 ✓

Note Alignment Revision
Sta 13+00 to 15+37.83
FB 825 Pg. 50

gew
11.8

$\frac{+23.2}{46}$	$\frac{+17.2}{34}$	$\frac{+16.8}{24}$	$\frac{+7.6}{13}$	$\frac{0.0}{3}$	$\frac{0.0}{41}$	$\frac{-4.1}{6}$	$\frac{-14.1}{28}$	$\frac{-19.1}{40}$
--------------------	--------------------	--------------------	-------------------	-----------------	------------------	------------------	--------------------	--------------------

$\frac{+18.4}{31}$	$\frac{+13.0}{23}$	$\frac{+7.6}{15}$	$\frac{+0.5}{4}$	$\frac{-6.9}{5}$	$\frac{-5.4}{12}$	$\frac{-14.0}{30}$	$\frac{-21.1}{48}$
--------------------	--------------------	-------------------	------------------	------------------	-------------------	--------------------	--------------------

$\frac{+18.4}{31}$	$\frac{+13.0}{22}$	$\frac{+7.6}{13}$	$\frac{+3.0}{4}$	$\frac{+1.0}{3}$	$\frac{-0.7}{5}$	$\frac{-2.4}{12}$	$\frac{-13.1}{28}$	$\frac{-19.0}{39}$
--------------------	--------------------	-------------------	------------------	------------------	------------------	-------------------	--------------------	--------------------

Profile S₄K₁ P.L.

KINS 8-11-52

19.

1936.52 ✓

17+00 ✓

5.2 ✓

31.3 ✓

$\frac{+18.4}{37}$ $\frac{+13.0}{24}$ $\frac{+7.6}{15}$ $\frac{+4.3}{8}$ $\frac{+0.5}{3}$

$\frac{0.0}{8}$ $\frac{-5.0}{21}$ $\frac{-13.0}{31}$ $\frac{-21.1}{42}$

T.P.

6.85 ✓

1938.82 ✓

4.55 ✓

1931.97 ✓

17+50 ✓

8.3 ✓

30.5 ✓

$\frac{+18.5}{41}$ $\frac{+13.0}{29}$ $\frac{+7.6}{17}$ $\frac{+3.2}{7}$ $\frac{+0.2}{4}$

$\frac{0.0}{3}$ $\frac{-5.4}{11}$ $\frac{-9.2}{28}$ $\frac{-15.9}{26}$ $\frac{-21.9}{33}$

17+98.90 ✓

6.37 ✓

ox hut
32.5 ✓

$\frac{+13.0}{42}$ $\frac{+7.7}{29}$ $\frac{+1.9}{13}$ $\frac{-1.1}{10}$

$\frac{-5.4}{9}$ $\frac{-15.4}{24}$ $\frac{-25.5}{39}$

18+50 ✓

6.5 ✓

32.3 ✓

$\frac{+13.0}{35}$ $\frac{+7.6}{21}$ $\frac{+2.2}{3}$ $\frac{0.0}{1}$

$\frac{-5.0}{7}$ $\frac{-6.8}{21}$ $\frac{-11.8}{29}$ $\frac{-16.7}{37}$

19+00 ✓

8.3 ✓

30.5 ✓

$\frac{+11.2}{27}$ $\frac{+5.6}{24}$ $\frac{+2.8}{7}$ $\frac{+0.5}{5}$

$\frac{-5.4}{13}$ $\frac{-10.9}{26}$ $\frac{-13.6}{33}$

19+50 ✓

9.1 ✓

29.7 ✓

$\frac{+13.0}{36}$ $\frac{+7.1}{17}$ $\frac{+3.3}{18}$ $\frac{+1.2}{6}$

$\frac{-5.4}{11}$ $\frac{-11.0}{23}$ $\frac{-16.0}{28}$

20 ✓

9.0 ✓

29.8 ✓

$\frac{+14.1}{34}$ $\frac{+11.9}{26}$ $\frac{+6.5}{20}$ $\frac{+3.0}{9}$ $\frac{+0.8}{7}$

$\frac{-5.4}{10}$ $\frac{-10.9}{20}$ $\frac{-16.0}{30}$

+50 ✓

8.7 ✓

30.1 ✓

$\frac{+13.0}{30}$ $\frac{+7.6}{20}$ $\frac{+4.5}{12}$ $\frac{+0.9}{6}$

$\frac{-4.4}{7}$ $\frac{-9.4}{17}$ $\frac{-14.4}{27}$ $\frac{-18.4}{36}$

21 ✓

9.2 ✓

29.0 ✓

$\frac{+18.4}{33}$ $\frac{+13.0}{21}$ $\frac{+7.6}{8}$ $\frac{0.0}{4}$

$\frac{-1.4}{15}$ $\frac{-9.0}{25}$ $\frac{-16.1}{30}$

Rock outcroppings

Profile
S. 4th. P. L.

8-11-52
KINS

20.

	1938.82 ✓			LT.	RT.
T.P.	3.43 ✓	1934.22 ✓	8.03 ✓	1930.79 ✓	
21+50 ✓		3.6 ✓		30.6 ✓	
Δ 21+96.00 ✓		3.27 ✓		31.0 ✓	
T.P.	2.73 ✓	1933.20 ✓	3.75 ✓	1930.47 ✓	
22+50 ✓		1.3 ✓		31.9 ✓	
Δ 23+01.64 ✓		3.78 ✓		29.4 ✓	
23+50 ✓		6.7 ✓		26.5 ✓	
23+86 ✓		9.8 ✓		23.4 ✓	
24+00 ✓		12.7 ✓		20.5 ✓	
T.P.	8.45 ✓	29.47 ✓	12.18 ✓	21.02 ✓	
		1928.47 ✓		1920.02 ✓	

				$\frac{+16.0}{33}$	$\frac{+14.9}{28}$	$\frac{+9.5}{15}$	$\frac{+0.9}{6}$	$\frac{-9.9}{18}$	$\frac{-20.0}{35}$
			on hub. 9	$\frac{+11.2}{35}$	$\frac{+6.0}{24}$	$\frac{+2.9}{16}$	$\frac{+2.9}{9}$	$\frac{0.0}{7}$	$\frac{-5.4}{10}$
								$\frac{-14.3}{22}$	$\frac{+23.7}{34}$
				$\frac{+14.0}{38}$	$\frac{+13.0}{28}$	$\frac{+7.6}{15}$	$\frac{0.0}{4}$	$\frac{-4.7}{10}$	$\frac{-11.5}{12}$
				$\frac{+17.0}{36}$	$\frac{+13.0}{31}$	$\frac{+7.3}{20}$	$\frac{+3.9}{7}$	$\frac{0.0}{4}$	$\frac{-0.4}{7}$
								$\frac{-3.4}{16}$	$\frac{-10.2}{21}$
				$\frac{+17.0}{34}$	$\frac{+15.4}{28}$	$\frac{+10.0}{18}$	$\frac{+4.7}{6}$	$\frac{-0.7}{6}$	$\frac{-5.4}{14}$
								$\frac{-11.0}{25}$	$\frac{-16.5}{35}$
				$\frac{+13.9}{40}$	$\frac{+13.0}{30}$	$\frac{+7.6}{20}$	$\frac{+3.5}{10}$	$\frac{+0.8}{8}$	$\frac{-0.2}{2}$
								$\frac{-5.6}{9}$	$\frac{-10.0}{20}$
								$\frac{-17.2}{27}$	
				$\frac{+13.0}{28}$	$\frac{+7.6}{18}$	$\frac{+6.0}{13}$	$\frac{+2.6}{10}$	$\frac{-3.9}{3}$	$\frac{-17.8}{29}$

Profile Suth. P.L.

1929.47 ✓
~~1928.47~~

24+12 ✓	19.9 ✓	✓ 09.6
24+25 ✓	21.5 ✓	✓ 08.0
24+54 ✓	18.5 ✓	✓ 19.0
25+00 ✓	6.9 ✓	✓ 22.6
Δ 25+74.54 ✓	2.24 ✓	✓ 27.2
26+00 ✓	3.5 ✓	✓ 26.0
26+50 ✓	7.2 ✓	✓ 22.3
27+00 ✓	4.6 ✓	✓ 24.9
T.P 9.30 ✓	1933.71 ✓	5.06 ✓ 1924.41 ✓
27+36.15 Δ ✓	7.60 ✓	✓ 26.1

KING - 8-11-52

21.

LT.

RT.

$\frac{+13.0}{28'}$	$\frac{+12.8}{13'}$	$\frac{-6.1}{12'}$	$\frac{-12.1}{29'}$
$\frac{+18.4}{36'}$	$\frac{+13.0}{26'}$	$\frac{+7.6}{16'}$	$\frac{+5.4}{19'}$ $\frac{-9.6}{32'}$
$\frac{+13.0}{30'}$	$\frac{+7.6}{20'}$	$\frac{-4.8}{7'}$	$\frac{-16.5}{33'}$
$\frac{+13.0}{29'}$	$\frac{+7.6}{18'}$	$\frac{+2.8}{5'}$	$\frac{+0.8}{3'}$ $\frac{-0.3}{4'}$ $\frac{-14.1}{30'}$
$\frac{+23.4}{32'}$	$\frac{+18.4}{27'}$	$\frac{+13.0}{17'}$	$\frac{+4.5}{3'}$ $\frac{+0.7}{4'}$ $\frac{+0.5}{9'}$ $\frac{-7.0}{21'}$ $\frac{-13.7}{33'}$
$\frac{+22.6}{35'}$	$\frac{+17.2}{29'}$	$\frac{+11.8}{23'}$	$\frac{+4.2}{3'}$ $\frac{0.0}{10'}$ $\frac{-11.0}{24'}$ $\frac{-17.0}{37'}$
$\frac{20.5}{32'}$	$\frac{+14.0}{23'}$	$\frac{+8.6}{14'}$	$\frac{+1.0}{7'}$ $\frac{0.0}{3'}$ $\frac{-8.4}{11'}$ $\frac{-15.3}{20'}$ $\frac{-21.0}{31'}$
$\frac{+19.4}{33'}$	$\frac{+14.0}{24'}$	$\frac{+8.6}{14'}$	$\frac{+2.6}{3'}$ $\frac{-0.6}{8'}$ $\frac{-5.7}{15'}$ $\frac{-13.7}{26'}$ $\frac{-15.7}{30'}$
$\frac{+14.6}{30'}$	$\frac{+13.6}{27'}$	$\frac{+3.6}{6'}$	$\frac{0.0}{4'}$ $\frac{0.0}{4'}$ $\frac{-15.5}{30'}$

Profile Suth Dam

8-12-52

22

	1933.71 ✓	27.4	LT	RT
27+61 ✓	6.3 ✓	27.4 ✓	$\frac{+12.7}{30'}$ $\frac{+11.8}{27'}$ $\frac{+6.1}{8'}$	$\frac{+2.4}{6'}$ $\frac{-0.3}{13'}$ $\frac{-6.3}{14'}$ $\frac{-10.0}{23'}$ $\frac{-17.0}{30'}$
28+00 ✓	10.8 ✓	22.9 ✓	$\frac{+19.1}{33'}$ $\frac{+13.4}{23'}$ $\frac{+7.7}{13'}$ $\frac{0.0}{3'}$	$\frac{0.0}{4'}$ $\frac{-10.6}{21'}$ $\frac{-14.3}{30'}$
T.P.	0.34 ✓	1921.80 ✓	12.75 ✓	1921.46 ✓
28+46.14 ✓	5.9 ✓	1915.9 ✓	15.9 ✓	
			$\frac{+15.3}{29'}$ $\frac{+9.6}{19'}$ $\frac{+2.3}{3'}$	$\frac{0.0}{5'}$ $\frac{-8.1}{21'}$ $\frac{-12.8}{30'}$
28+54 ✓	8.6 ✓	13.2 ✓		
			$\frac{+10.0}{35'}$ $\frac{+8.7}{30'}$ $\frac{+2.0}{8'}$ $\frac{0.0}{7'}$	$\frac{-10.5}{23'}$ $\frac{-13.2}{30'}$
T.P.	0.73 ✓	1910.49 ✓	12.04 ✓	1909.76 ✓
T.P.	0.28 ✓	1897.73 ✓	13.04 ✓	1897.45 ✓
29+00 ✓	11.6 ✓	86.1 ✓		
			$\frac{+12.3}{40'}$ $\frac{+6.7}{35'}$ $\frac{+3.5}{20'}$ $\frac{+3.4}{13'}$	$\frac{-4.4}{12'}$ $\frac{-11.7}{31'}$
T.P.	0.30 ✓	1884.84 ✓	13.19 ✓	1884.54 ✓
30+00.99 ✓	13.2 ✓	71.6 ✓		
29+50 ✓			$\frac{+10.8}{37'}$ $\frac{+5.6}{21'}$	$\frac{-5.0}{16'}$ $\frac{-9.4}{34'}$
T.P.	0.17 ✓	1872.02 ✓	12.19 ✓	1872.65 ✓

Syth. P. 2.
Profile

KING 8-12-52

23

1872-82 ✓

T.P. 8

0.17

1872-82

1877

1862-11

30+08 ✓

2.8 ✓

70.0 ✓

$\frac{+9.7}{36}$ $\frac{+4.3}{23}$ $\frac{+3.0}{15}$ $\frac{0.0}{10}$ $\frac{-1.5}{4}$

$\frac{-3.4}{19}$ $\frac{-7.7}{38}$ $\frac{-9.7}{45}$ $\frac{-13.7}{49}$

2' out
24' out
2' out
-30+10

30+29

9.4

T.P.

4.48

64.90
1852-96 ✓

12.40 ✓

60.42
1842-48 ✓

30+57 ✓

8.6 ✓

56.3 ✓

$\frac{+13.0}{40}$ $\frac{+8.0}{23}$
+59 E 7' out

$\frac{0.04}{7}$ $\frac{-3.4}{16}$ $\frac{-5.7}{30}$ $\frac{-7.5}{39}$

50' +10
20' out

30+75 ✓

8.9 ✓

56.0 ✓

$\frac{+9.7}{38}$ $\frac{+7.2}{30}$ $\frac{+4.6}{22}$

$\frac{-1.4}{11}$ $\frac{-5.4}{21}$ $\frac{-6.8}{24}$ $\frac{-10.8}{35}$ $\frac{-12.6}{40}$

+80 E 11' out

A 30+86.25 ✓

5.3 ✓

59.6 ✓

$\frac{+10.9}{32}$ $\frac{+7.6}{22}$ $\frac{+4.0}{17}$

$\frac{-0.8}{3}$ $\frac{-3.9}{6}$ $\frac{-5.0}{17}$ $\frac{-7.2}{22}$ $\frac{-10.7}{30}$ $\frac{-13.5}{35}$

31+00
29' out

31+07 ✓

6.8 ✓

58.3 ✓

$\frac{+11.0}{40}$ $\frac{+5.5}{21}$

$\frac{-4.6}{5}$ $\frac{-4.6}{15}$ $\frac{-13.0}{43}$ $\frac{-14.2}{47}$

31+20
16' out

31+20 ✓

11.6 ✓

53.3 ✓

$\frac{+5.9}{38}$ $\frac{+3.0}{21}$

$\frac{-0.9}{5}$ $\frac{-1.3}{11}$ $\frac{-7.3}{36}$ $\frac{-9.3}{46}$

31+40 ✓

14.0 ✓

50.9 ✓

Draw $\frac{+4.0}{40}$

$\frac{-0.3}{9}$ $\frac{-6.5}{21}$ $\frac{-5.5}{27}$ $\frac{-7.6}{44}$

33+65
2' out

Profile S4th.P.L

King 8-12-52 Hot

24

1864.90 ✓
1852.96

LT. ←

RT

32+00 ✓ 3.6 ✓ 61.3 ✓

Rock - $\frac{-20.0}{35}$ $\frac{-11.0}{21}$ $\frac{-1.9}{7}$ $\frac{+12}{5}$ $\frac{+7.6}{12}$ $\frac{+13.0}{22}$ $\frac{+18.4}{32}$

↘ Reversed

T.P. 13.11 ✓ $\frac{74.99}{1863.05}$ ✓ 3.02 ✓ $\frac{61.88}{49.94}$ ✓

32+50 ✓ 5.3 ✓ JW $\frac{57.8}{69.7}$ ✓

Rock $\frac{+14.6}{31}$ $\frac{+9.3}{14}$ $\frac{+1.0}{4}$ $\frac{+0.1}{6}$ $\frac{-7.8}{18}$ $\frac{-15.5}{30}$ $\frac{-19.4}{36}$

☁ +5.5
4' 16' out

T.P. 4.20 ✓ $\frac{77.70}{1865.76}$ ✓ 1.49 ✓ $\frac{73.50}{1861.56}$ ✓

☁ +9.0
3' 18' out

33+00 ✓ 4.4 ✓ 73.3 ✓

$\frac{+17.7}{42}$ $\frac{+12.3}{28}$ $\frac{+8.0}{13}$ $\frac{+2.6}{3}$ $\frac{0.0}{7}$ $\frac{-10.1}{18}$ $\frac{-20.2}{29}$ $\frac{-26.0}{34}$
Rock Rock Rock Rock

33+50 ✓ 9.9 ✓ 67.8 ✓

$\frac{+18.4}{36}$ $\frac{+13.0}{20}$ $\frac{+7.6}{14}$ $\frac{+3.7}{5}$ $\frac{-0.8}{2}$ $\frac{-13.2}{30}$ $\frac{-18.6}{36}$

33+61 ✓ 6.9 ✓ 70.8 ✓

$\frac{+17.4}{36}$ $\frac{+8.6}{18}$ $\frac{-3.6}{5}$ $\frac{-4.3}{11}$ $\frac{-16.4}{30}$ $\frac{-21.7}{35}$

34+00 ✓ 2.6 ✓ 75.1 ✓

$\frac{+18.4}{32}$ $\frac{+13.0}{23}$ $\frac{+7.6}{14}$ $\frac{-5.4}{8}$ $\frac{-9.4}{17}$ $\frac{-11.6}{25}$ $\frac{-18.1}{28}$ $\frac{-21}{32}$

T.P. 12.46 ✓ $\frac{89.21}{1876.27}$ ✓ 1.95 ✓ $\frac{75.75}{1873.81}$ ✓

✓

Suth. P.L.

King

8-13-52

25

H 188.31 ✓
~~187.27~~

34+26 ✓

7.9 ✓ ^(JW) 18.5 ✓ 80.3 ✓

LT
+16.5 +11.1 +1.0
24' 17' 4'
Rock

RT
-4.0 -6.2 -15.6 -16.0
2' 8' 23' 36'
Rock

34+45 ✓

6.2 ✓ 82.0 ✓

+34.0 +19.0
29' 26'
Edge Co. Rd.

-9.0 -14.3 -15.6
20' 23' 29'

T.P.

12.96 ✓ 1901.00 ✓
1889.06 ✓ 0.17 ✓ 88.04 ✓
1876.10 ✓

(JW)

34+98 ✓

2.70 ✓ 1898.3 ✓ Edge Co. Rd.
1886.4 ✓

+5.4 +0.4
28' 20'
Edge Rd.

-5.4 -13.1 -23.4
9' 21' 30'

35+50 ✓

6.8 ✓ 94.2 ✓
82.3 ✓

Note: This is solid

18 Solid
Rock +27.4 +21.8 +12.4 +3.0
25' 15' 10' 7'
Rock

-0.8 -11.3 -13.6
18' 27' 35'

CHECK TO
T.B.M. #3

2.92 ✓ 1898.04 ✓ Edge Rd.
1886.32 ✓ 35700

20 21

CONT'D BK. 828 - Pa 18

1898.04 - 1898.07

{ Checked & Reduced 10/31/52 Jewell
Pa 18-25 ch'kd 1/16/53 vlc

121.6
80.6

1921.77

+ 17

1921.94

- 13.07

1908.87

+ 75

1909.62

- 12.00

1897.62

+ 87

1898.49

- 11.42

1887.07

+ 30

1887.37

- 12.05

1875.32

+ 11

1875.43

- 76

1874.67

+ 12.84

1887.51

- 1.60

1885.91

+ 12.88

1898.79

1200
1100
Profit 23
28
30+00

- 1910.49
- 13.04

1897.45

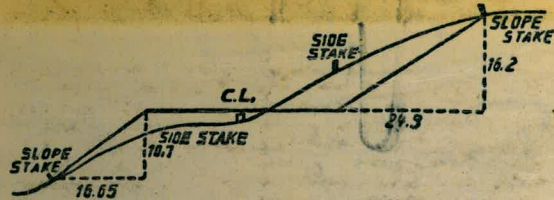
1921.80
- 12.04

1909.76
+ 73

1910.49
- 13.04

1897.45
28

1897.73



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Please Return to
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