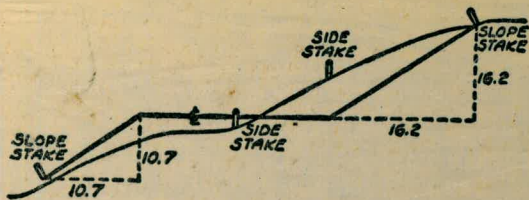


W828

#828



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the side or shoulder stake is located by the double entry method in left column and top row. If ground is not level, estimate the difference in elevation between the side stake and slope stake, lower target by this amount, if cut, or add, if fill. Add this amount to cut or fill distance in table. Set on top of this point, and line of sight should cut target. If it does not, make the same adjustment necessary.

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TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.88	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.877	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

*alice P.*  
 Profile - Sutherland P.L. 189-2V450 1-18  
 " " " 30706-63+75-1920  
 Alignment - Suth. P.L. Sta. 54+50-64+34.51 *alice* 2930  
 New Profile Sta 62+17<sup>20</sup> to 63+80 *alice* 31  
 New Alignment + Profile 32  
 Sutherland R.L. Sta 451+80 - 456+00AH 33  
 Realignment 34  
 451+80 - 456+69<sup>20</sup>  
*alice*

Profile  
Suth. P.L.

TBM	217	1809.53	1807.36
188400		2.9	06.6
450		4.6	04.9
P.O.T. 188458		4.86	X 04.67
188495		7.4	02.1
189402		11.6	MAIN 1197.9 Creek
T.P	8.39	1817.55	1809.16
189425		6.7	10.85
450		5.7	11.85
189478		5.2	12.4

7-23-52  
KING

100°

5' R - 188450 - Nail in tree

+5.0	+1.0	-4.6	-4.6	-2.0		+6.4
43'	35'	28	23	21		40
18.8	-2.5	-5.7	-6.7	+1.4	+5.0	+10.0
40	18	16	10	8	28	42
+21	+18.5	+13.0	-3.4	-3.4	+2.0	+7.4
45	36	24	6	3	26	50

See FB 827 for Pgs 1-4



Suth P.L.

7-23-52

2

1817.53 ✓

189407

7.8

DRAW  
R.L. 098

190400

5.4

12.2

+50

1.8

15.8

191

1.2

16.4

T.P

5.97 ✓

1822.42 ✓

7.10 ✓

1816.45 ✓

191455

4.6

17.8

191477

9.3

R.L. 131  
DRAW

192

0.0

22.4

T.P

11.57 ✓

1833.99 ✓

8.00 ✓

1822.42 ✓

+50

4.7

4.9

29.1



Suth. P. h.

7-23  
KING

3

1833.99 ✓

T.P.

1.79 ✓

1835.77 ✓

0.04 ✓

1833.95 ✓

1924825

1.3

34.6

193405

1.4

34.3

T. P. M.

0.71

1835.03

old svz hub 15 L + 1934 01.07

193450

6.2

29.5

194

8.9

26.8

T.P.

1.28 ✓

1824.16 ✓

128.6 ✓

1822.80 ✓

421

0.09

24.2

437

7.6

164 P+L to 2  
Draw

450

3.8

20.4



Suthi P.L

4

1947037  
P.O.T.

1824.16 ✓

3.4

20.8

195

13.8

10.4

T.P

9.04 ✓

1820.02 ✓

13.18 ✓

1810.98 ✓

+08

11.9

084

+36

10.4

9.8

+73

27.6

1792.42  
R.L to P  
Draw

196

19.4

0.6

+65

1.7

18.3

T.P

12.58 ✓

1831.34 ✓

1.26 ✓

1818.76 ✓

197700

9.2

22.1



Suth. Pl.

King-7-28

5

183134 ✓

197+39

6.8

24.5

+62

9.7

21.6

See BK 826 (Lt.)

(Rt.)

198

1.4

29.9

Color  
Outcroppings $\frac{+19.2}{55'}$  $\frac{+11.5}{27'}$  $\frac{+8.5}{14'}$ From  
B  
E  
A  
H  
+  
1 $\frac{-1.5}{7'}$  $\frac{-6.4}{26'}$  $\frac{-14.2}{32'}$ 

T.P

11.38 ✓

1841.29 ✓

1.43 ✓

182991 ✓

198+21

10.2

31.1

 $\frac{+13.0}{45'}$  $\frac{+10.5}{39'}$  $\frac{+3.0}{10'}$  $\frac{-1.5}{8'}$  $\frac{-6.2}{19'}$  $\frac{-10.4}{32'}$  $\frac{-13.3}{39'}$  $\frac{-16.5}{50'}$ 

+50

14.3

27.0

 $\frac{+19.1}{50'}$  $\frac{+17.1}{43'}$  $\frac{+10.6}{26'}$  $\frac{+3.2}{10'}$  $\frac{-1.7}{10'}$  $\frac{-14.8}{40'}$  $\frac{-17.8}{30'}$ 

+98

18.0

23.3  
Rt. to  
Draw $\frac{+25.6}{50'}$  $\frac{+20.6}{35'}$  $\frac{+13.0}{22'}$  $\frac{+6.1}{10'}$  $\frac{-0.7}{10'}$  $\frac{-3.0}{34'}$  $\frac{-8.1}{38'}$ 

199+20

5.6

35.7

 $\frac{+19.0}{30'}$  $\frac{+0.3}{10'}$  $\frac{-3.0}{11'}$  $\frac{-9.0}{30'}$  $\frac{-12.3}{41'}$  $\frac{-15.0}{50'}$ 

T.P

11.29 ✓

185238 ✓

0.20 ✓

1844.09 ✓

41.1

 $\frac{+18.0}{50'}$  $\frac{+13.0}{36'}$  $\frac{+4.1}{10'}$  $\frac{-5.4}{10'}$  $\frac{-19.3}{50'}$ 

199+50

10.4

42.0



Sutcliffe

King 7-28-52

6

1852.38

(L)

(R)

20440

2.8

49.6

$$\begin{array}{r} +18.0 \\ 48 \end{array} \quad \begin{array}{r} +13.1 \\ 34 \end{array} \quad \begin{array}{r} +5.0 \\ 18 \end{array}$$

$$\begin{array}{r} -5.4 \\ 15 \end{array} \quad \begin{array}{r} -13.3 \\ 35 \end{array} \quad \begin{array}{r} 19.5 \\ 50 \end{array}$$

+50

2.4

50.0

$$\begin{array}{r} +20.6 \\ 50 \end{array} \quad \begin{array}{r} +13.0 \\ 29 \end{array} \quad \begin{array}{r} +4.7 \\ 10 \end{array}$$

$$\begin{array}{r} -5.3 \\ 16 \end{array} \quad \begin{array}{r} -12.9 \\ 35 \end{array} \quad \begin{array}{r} -19.1 \\ 50 \end{array}$$

201

3.6

48.8

$$\begin{array}{r} +18.6 \\ 50 \end{array} \quad \begin{array}{r} +13.0 \\ 39 \end{array} \quad \begin{array}{r} +7.6 \\ 24 \end{array} \quad \begin{array}{r} +3.2 \\ 10 \end{array}$$

$$\begin{array}{r} -5.4 \\ 18 \end{array} \quad \begin{array}{r} -9.1 \\ 25 \end{array} \quad \begin{array}{r} 17.3 \\ 49 \end{array}$$

+50

6.6

45.8

$$\begin{array}{r} +11.8 \\ 50 \end{array} \quad \begin{array}{r} +7.5 \\ 34 \end{array} \quad \begin{array}{r} +2.5 \\ 10 \end{array}$$

$$\begin{array}{r} -5.4 \\ 19 \end{array} \quad \begin{array}{r} -7.4 \\ 26 \end{array} \quad \begin{array}{r} -12.6 \\ 33 \end{array} \quad \begin{array}{r} -19.0 \\ 40 \end{array} \quad \begin{array}{r} -2.1 \\ 49 \end{array}$$

T.P. 4.25 ✓ 1844.31 ✓ 12.32 ✓ 1840.06

201490

7.8

37.3

$$\begin{array}{r} +6.1 \\ 45 \end{array} \quad \begin{array}{r} -0.3 \\ 10 \end{array}$$

$$\begin{array}{r} -1.7 \\ 10 \end{array} \quad \begin{array}{r} -35.8 \\ 50 \end{array}$$

13.0

R.H. to E

Draws

207423

31.3

$$\begin{array}{r} +10.7 \\ 50 \end{array} \quad \begin{array}{r} +9.3 \\ 30 \end{array} \quad \begin{array}{r} +0.7 \\ 10 \end{array}$$

$$\begin{array}{r} -9.9 \\ 26 \end{array} \quad \begin{array}{r} -6.0 \\ 40 \end{array} \quad \begin{array}{r} -1.0 \\ 50 \end{array}$$

202458

5.0

39.3

$$\begin{array}{r} +13.5 \\ 50 \end{array} \quad \begin{array}{r} +7.6 \\ 29 \end{array} \quad \begin{array}{r} +3.1 \\ 10 \end{array}$$

$$\begin{array}{r} -9.6 \\ 50 \end{array}$$

△

T.B.M.

20246857RK

2218467.09

3.76

1844055

2x2 hab.

$$\begin{array}{r} +14.0 \\ 50 \end{array} \quad \begin{array}{r} +7.0 \\ 59 \end{array}$$

$$\begin{array}{r} -10.0 \\ 50 \end{array}$$

T.P. 1.98 ✓ 184629 0.00 ✓ 184431 ✓

Suth. Pt

King 7-28-52

7

1846.29

219 1.4 44.9

+42 6.5 39.8

~~+50 9.3~~

+67 21.4 24.9  
Draw

+82 9.8 36.5

220 12.1 34.2

~~+37 out 7.5~~

T.P. 12.42 1858.53 0.18 1846.11

220+45 13.8 44.7

T.P. 12.69 1870.99 0.23 1858.30

(L)

$\frac{+10.6}{50}$   $\frac{+7.9}{37}$   $\frac{+2.0}{10}$

(R)

$\frac{-2.9}{70}$   $\frac{-9.1}{30}$   $\frac{-14.1}{42}$

$\frac{+15.1}{50}$   $\frac{+7.8}{19}$   $\frac{+5.4}{10}$

$\frac{-23.3}{35}$   $\frac{-15.1}{40}$

Creek

$\frac{+18.1}{50}$   $\frac{+6.9}{25}$   $\frac{+4.0}{10}$

$\frac{-2.4}{70}$   $\frac{+3.0}{27}$   $\frac{+17.0}{40}$   $\frac{+2.2}{54}$

Creek

$\frac{+16.6}{50}$   $\frac{+11.5}{20}$   $\frac{+7.6}{10}$

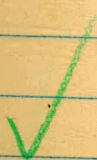
$\frac{-11.0}{13}$   $\frac{-9.7}{23}$   $\frac{0.0}{32}$   $\frac{+8.5}{47}$

$\frac{+21.6}{50}$   $\frac{+16.3}{25}$   $\frac{+5.0}{9}$

$\frac{-4.8}{8}$   $\frac{+7.2}{29}$   $\frac{+2.7}{30}$

$\frac{+20.6}{50}$   $\frac{+12.9}{16}$

$\frac{+6.5}{10}$   $\frac{+17.5}{30}$   $\frac{+19.7}{52}$



Su K. Pl.

King 7-28-52

5

1870.99

220463

13.8

57.2

$\frac{+6.3}{50}$

$\frac{+7.3}{40}$

$\frac{+4.8}{22}$

$\frac{-5.1}{7}$

$\frac{+4.2}{18}$

$\frac{+5.2}{50}$

221

5.4

65.6

$\frac{+7.9}{49}$

$\frac{+6.4}{40}$

$\frac{+3.4}{22}$

$\frac{-4.4}{8}$

$\frac{+3.1}{16}$

$\frac{+2.9}{49}$

So. Edge Rd

221471

3.5

67.5

T.P

13.23

1883.87

0.35

1870.64

221450

9.3

74.6  
Edge Rd  
To Nakone Y  
Ranch  
Edge Rd.  
80.0

$\frac{-3.5}{44}$

$\frac{-0.9}{11}$

$\frac{-0.7}{17}$

$\frac{+1.3}{20}$

$\frac{+2.0}{50}$

Edge Rd

222

3.9

$\frac{+1.7}{30}$

$\frac{+1.6}{42}$

$\frac{0.1}{12}$

$\frac{+0.6}{28}$

$\frac{+1.6}{50}$

T.P

8.39

1892.23

0.05

1883.84

T.P.M

6.04

1886.19

Nail in gate Post

450

7.6

84.6

$\frac{+0.7}{50}$

$\frac{-0.3}{14}$

$\frac{+0.5}{10}$

$\frac{+2.3}{50}$

223

4.7

87.5

$\frac{+0.9}{50}$

$\frac{-1.1}{19}$

$\frac{+1.0}{25}$

$\frac{+2.1}{50}$

Revised  
See FB  
825 p 19

Su Ma Ph.

1892-23

P.O.T.				
223+5195		6.64	1885.59	2x2hls 4T
223+48		7.4	1884.83	Edge Rd 20'
T.P.	0.94	1880.22	1879.28	

223+67		2.6	77.6
--------	--	-----	------

224400		11.3	68.9
--------	--	------	------

224406		15.2	65.0 45° to E Draw
--------	--	------	--------------------------

+31		14.9	65.3
-----	--	------	------

T.P.	0.81	1867.92	1867.11
------	------	---------	---------

+53		9.2	58.7
-----	--	-----	------

+88		3.3	64.6
-----	--	-----	------

King-7-28-52

101°

9

(LT)

(RT)

$\frac{-0.2}{50}$	$\frac{+0.6}{43}$	$\frac{+1.5}{22}$	$\frac{+0.6}{13}$
-------------------	-------------------	-------------------	-------------------

$\frac{+0.5}{12}$	$\frac{-1.3}{28}$	$\frac{+3.1}{20}$	$\frac{+4.0}{40}$
-------------------	-------------------	-------------------	-------------------

Edge Rd.

RED

$\frac{+1.2}{50}$	$\frac{+3.2}{22}$	$\frac{-0.2}{14}$	$\frac{+2.6}{11}$
-------------------	-------------------	-------------------	-------------------

$\frac{-4.6}{4}$	$\frac{+4.0}{17}$	$\frac{+3.0}{18}$	$\frac{+3.1}{37}$	$\frac{+1.6}{47}$
------------------	-------------------	-------------------	-------------------	-------------------

REIN

$\frac{+4.9}{50}$	$\frac{+5.7}{24}$	$\frac{+4.6}{14}$
-------------------	-------------------	-------------------

$\frac{+4.0}{10}$	$\frac{+17.3}{36}$	$\frac{+16.5}{37}$	$\frac{+16.3}{40}$
-------------------	--------------------	--------------------	--------------------

$\frac{+0.1}{50}$	$\frac{-2.9}{35}$	$\frac{+2.5}{28}$	$\frac{-7.7}{10}$
-------------------	-------------------	-------------------	-------------------

$\frac{+4.3}{10}$	$\frac{+13.0}{36}$	$\frac{+16.1}{41}$
-------------------	--------------------	--------------------

$\frac{+6.6}{50}$	$\frac{-1.1}{28}$	$\frac{-6.1}{20}$
-------------------	-------------------	-------------------

$\frac{+5.3}{10}$	$\frac{+13.1}{23}$	$\frac{+20.6}{43}$	$\frac{+22.6}{48}$
-------------------	--------------------	--------------------	--------------------

$\frac{-17.7}{50}$	$\frac{-25.0}{36}$	$\frac{-12.5}{20}$
--------------------	--------------------	--------------------

$\frac{+7.6}{22}$	$\frac{+12.6}{45}$
-------------------	--------------------

+ Above R.F.L.

Suth. P.L.

King - 7-29-52

10

A T.B.M.  
225+25.43

1867.92

7.27

1860.65

old  
2xH.C.T.  $\frac{-37.0}{55}$   $\frac{-37.2}{47}$   $\frac{-25.0}{34}$   $\frac{-12.7}{18}$   $\frac{-5.4}{16}$ 

(L+)

(R+)

 $\frac{+2.7}{17}$   $\frac{+6.0}{34}$   $\frac{+7.7}{48}$ 

T.P.

5.16

1863.70

9.88

1858.04

225+245

10.2

1853.0

 $\frac{-31.5}{59}$   $\frac{-14.8}{47}$  $\frac{-5.4}{12}$  $\frac{+5.3}{10}$   $\frac{+12.1}{40}$   $\frac{+14.0}{51}$ 

+59

5.5

1857.7

 $\frac{-38.5}{48}$  $\frac{-13.0}{19}$   $\frac{-7.7}{140}$  $\frac{+3.4}{10}$   $\frac{+11.2}{39}$   $\frac{+15.2}{58}$ 

T.B.M.

2.35

1863.00

2.55

1860.65

+79

5.8

1857.2

 $\frac{-39.0}{49}$  $\frac{-12.5}{20}$   $\frac{-7.9}{13}$  $\frac{+5.3}{12}$   $\frac{+11.8}{30}$   $\frac{+14.6}{45}$   $\frac{+15.2}{50}$ 

226

16.1

1846.9

T.P.

2.14

1852.97

12.17

1858.83

+15

15.1

1837.87  
~~1837.9~~ $\frac{-16.0}{45}$  $\frac{+27.6}{37}$   $\frac{-27.8}{14}$  $\frac{+7.6}{11}$   $\frac{+20.6}{27}$   $\frac{+23.0}{32}$   $\frac{+24.1}{45}$ 

+35

18.6

1834.37

 $\frac{-17.8}{39}$   $\frac{-25.0}{31}$   $\frac{+25.3}{27}$   $\frac{-19.5}{19}$   $\frac{-13.5}{14}$  $\frac{+8.6}{11}$   $\frac{+14.0}{18}$   $\frac{+21.1}{40}$   $\frac{+24.0}{50}$ 

REMOVED

Suth. P.h.

1852-97

22640

5x2

47.8

+97

8.4

44.6

227409

6.2

46.8

+33

16.8

36.2

+44

23.4

29.6  
Draw

T.P.

0.82

1843.97

9.82

1843.15

227462

0.9

43.2

35.0

228

6.1

37.9

37.9

+35

11.4

32.6

32.6

+50

15.2

28.8

11

(L)

$\frac{-39.8}{42}$   $\frac{-38.8}{35}$   $\frac{-6.6}{6}$

(R)

$\frac{+14.1}{28}$   $\frac{+19.3}{55}$

RED

$\frac{-22.2}{50}$   $\frac{-26.1}{46}$   $\frac{-16.4}{32}$   $\frac{-5.4}{11}$

$\frac{+3.6}{11}$   $\frac{+7.8}{49}$

$\frac{-23.0}{55}$   $\frac{-21.2}{50}$   $\frac{-4.0}{12}$

$\frac{+2.6}{15}$   $\frac{-2.0}{42}$   $\frac{+6.8}{50}$

$\frac{-16.0}{50}$   $\frac{-7.0}{13}$

$\frac{+7.0}{19}$   $\frac{+13.3}{42}$   $\frac{+10.0}{50}$

$\frac{27.3-31.3}{50}$   $\frac{-24.5-13.0}{39}$   $\frac{-7.0}{20}$

$\frac{+4.0}{10}$   $\frac{+7.6}{25}$   $\frac{+13.0}{41}$   $\frac{+15.0}{50}$

$\frac{-27.3}{45}$   $\frac{-5.5}{8}$

$\frac{+4.0}{10}$   $\frac{+9.1}{30}$   $\frac{+14.0}{52}$

$\frac{-3.0}{58}$   $\frac{-21.2}{40}$   $\frac{21.3}{36}$   $\frac{-9.2}{20}$   $\frac{-7.2}{19}$   $\frac{-2.8}{10}$

$\frac{+2.6}{10}$   $\frac{+7.6}{37}$   $\frac{+13.1}{58}$

Suth. P.L.

King 7-29-52 103°

12

L+

(W)

1843.97

228462

21.2

22.8  
Draw $\frac{-16.2}{37}$  $\frac{-5.4}{10}$  $\frac{+1.9}{12}$  $\frac{+10.2}{27}$  $\frac{+21.0}{61}$ 

+76

13.5

30.5

 $\frac{-14.9}{45}$  $\frac{-5.0}{15}$  $\frac{+6.0}{17}$  $\frac{+10.3}{22}$  $\frac{+14.7}{45}$ 

229

10.1

33.9

 $\frac{-19.0}{47}$  $\frac{-9.0}{21}$  $\frac{-4.2}{6}$  $\frac{+5.4}{15}$  $\frac{+7.6}{34}$  $\frac{+13.0}{56}$ 

T.P.

0.75

1834.89

9.83

1834.14

+32

4.8

+50

4.6

30.3

 $\frac{-27-27.7}{50}$   
(creek) $\frac{-63}{27}$  $\frac{-9.2}{17}$  $\frac{-4.2}{8}$  $\frac{+3.1}{10}$  $\frac{+11.1}{50}$ 

+74

4.1

30.8

 $\frac{-28.7}{50}$  $\frac{-1.4}{5}$  $\frac{+4.2}{27}$  $\frac{+9.1}{50}$ 229+9634  
TBM A

5.53

29.4

 $\frac{-28.6}{51}$  $\frac{-4.0}{17}$  $\frac{-2.5}{14}$  $\frac{+2.6}{24}$  $\frac{+8.6}{50}$ 

230+33

8.6

230+36

4.7

DNBack

REVIS E

D

✓

Su M. P. 2

King 7-30-82

13

230<sup>50</sup> + 44

1834.89

8.9  
8.2

26.0

(24)  
-11.1  
50  
-5.3  
25

(R1)  
+2.7  
16  
+5.3  
25  
+12.6  
50

231

13.0

21.9

-10.3  
50  
-7.1  
27

+2.8  
17  
+10.1  
38  
+15.5  
50

T.P. 0.94 1823.75 12.08 1822.81

+50

8.2

15.6

-12.4  
50  
-9.8  
40  
-3.4  
12

+5.4  
10  
+12.7  
34  
+18.1  
47

232

11.2

12.6

-16.1  
50  
-12.6  
40  
-6.9  
28

+3.2  
10  
+7.9  
30  
+13.0  
42  
16  
50

+14

12.2

11.6

-15.6  
45  
-10.2  
38  
-5.2  
19

+2.2  
10  
+5.6  
28  
+9.5  
40  
+12.8  
50

T.P. 0.82 1811.41 13.16 1816.59

+40

9.7

01.7

-12.0  
47  
-9.1  
40  
-7.5  
31  
-6.1  
18

+5.2  
10  
+12.3  
30  
+17.3  
40

+50

7.5

03.9

-18.3  
47  
-15.1  
35  
-12.0  
31  
-6.2  
18

+8.9  
25  
+14.3  
39  
+19.7  
51

+78

8.2

03.2

REVISIT

✓



Sutcliffe

King 7-30-52

14

233

1811.41

9.8

01.6

$$\begin{array}{r} -20.6 \\ \hline 50 \end{array} \quad \begin{array}{r} -16.6 \\ \hline 42 \end{array} \quad \begin{array}{r} -10.3 \\ \hline 29 \end{array} \quad \begin{array}{r} -3.7 \\ \hline 14 \end{array}$$

$$\begin{array}{r} +2.4 \\ \hline 10 \end{array} \quad \begin{array}{r} +5.0 \\ \hline 17 \end{array} \quad \begin{array}{r} +11.9 \\ \hline 35 \end{array} \quad \begin{array}{r} +17.3 \\ \hline 47 \end{array}$$

(L+)

(R+)

T.P.

0.44

1799.40

12.45

1798.96

REVISED TO 233+28 SEE FB  
8'25" p 19

+30

~~0.3~~

+60

4.3

95.1

$$\begin{array}{r} -20.4 \\ \hline 45 \end{array} \quad \begin{array}{r} -14.7 \\ \hline 31 \end{array} \quad \begin{array}{r} -7.9 \\ \hline 16 \end{array}$$

$$\begin{array}{r} +3.7 \\ \hline 10 \end{array} \quad \begin{array}{r} +11.9 \\ \hline 31 \end{array} \quad \begin{array}{r} +17.3 \\ \hline 42 \end{array} \quad \begin{array}{r} +21.0 \\ \hline 49 \end{array}$$

+87

8.3

91.1

$$\begin{array}{r} -21.0 \\ \hline 50 \end{array} \quad \begin{array}{r} -18.0 \\ \hline 43 \end{array} \quad \begin{array}{r} -15.1 \\ \hline 30 \end{array} \quad \begin{array}{r} -7.9 \\ \hline 17 \end{array}$$

$$\begin{array}{r} +4.3 \\ \hline 10 \end{array} \quad \begin{array}{r} +11.6 \\ \hline 27 \end{array} \quad \begin{array}{r} +22.4 \\ \hline 45 \end{array} \quad \begin{array}{r} +27.8 \\ \hline 55 \end{array}$$

T.P.

1.07

1787.80

12.67

1786.73

69.3

234+71

18.5

R+ B+  
DRAW

+

$$\begin{array}{r} -6.6 \\ \hline 38 \end{array} \quad \begin{array}{r} +6.6 \\ \hline 32 \end{array} \quad \begin{array}{r} -7.6 \\ \hline 11 \end{array}$$

$$\begin{array}{r} +9.4 \\ \hline 12 \end{array} \quad \begin{array}{r} +14.8 \\ \hline 23 \end{array} \quad \begin{array}{r} +27.8 \\ \hline 39 \end{array} \quad \begin{array}{r} +33.6 \\ \hline 46 \end{array}$$

235

11.3

76.5

$$\begin{array}{r} -16.3 \\ \hline 50 \end{array} \quad \begin{array}{r} -19.3 \\ \hline 41 \end{array} \quad \begin{array}{r} -17.8 \\ \hline 22 \end{array} \quad \begin{array}{r} -5.6 \\ \hline 11 \end{array}$$

$$\begin{array}{r} +6.3 \\ \hline 10 \end{array} \quad \begin{array}{r} +20.6 \\ \hline 38 \end{array} \quad \begin{array}{r} +26.0 \\ \hline 50 \end{array}$$
38  
39

+50

4.7

83.1

$$\begin{array}{r} -13.0 \\ \hline 47 \end{array} \quad \begin{array}{r} -7.0 \\ \hline 32 \end{array}$$

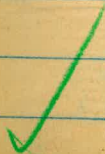
$$\begin{array}{r} +3.0 \\ \hline 10 \end{array} \quad \begin{array}{r} +7.6 \\ \hline 26 \end{array} \quad \begin{array}{r} +13.0 \\ \hline 41 \end{array} \quad \begin{array}{r} +18.1 \\ \hline 52 \end{array}$$

236

3.5

84.3

$$\begin{array}{r} -10.6 \\ \hline 50 \end{array} \quad \begin{array}{r} -7.4 \\ \hline 31 \end{array}$$

$$\begin{array}{r} +3.4 \\ \hline 10 \end{array} \quad \begin{array}{r} +14.4 \\ \hline 50 \end{array}$$


Su M, Pk.

King 7-30-52

54  
18

15

1787.80 ✓

(L)

(R)

236+31

5.1

82.7

 $\frac{-11.8}{50}$  $\frac{-7.2}{27}$  $\frac{+2.6}{10}$  $\frac{+7.3}{37}$  $\frac{+13.0}{48}$ 

+55

13.1

74.7

 $\frac{-6.3}{47}$  $\frac{-3.7}{27}$  $\frac{+3.6}{10}$  $\frac{+9.6}{30}$  $\frac{+16.3}{50}$ 

+89

3.1

84.7

 $\frac{-9.1}{50}$  $\frac{-4.6}{24}$  $\frac{+2.9}{10}$  $\frac{+9.8}{50}$ 

237

2.7

85.1

+50

2.7

85.1

 $\frac{-6.4}{50}$  $\frac{-3.4}{25}$  $\frac{+3.0}{25}$  $\frac{+5.6}{50}$ 

T.P

0.8 ✓

1785.94

2.6 ✓

1785.13

 $\frac{-1.4}{50}$  $\frac{-2.1}{28}$  $\frac{+1.1}{10}$  $\frac{+4.9}{50}$ 

237+96

3.64

1x1 hub  
82.3

238+50

8.8

77.1

 $\frac{-3.0}{50}$  $\frac{-2.1}{27}$  $\frac{+0.4}{10}$  $\frac{+1.5}{26}$  $\frac{+1.9}{50}$ 

+81

14.3

71.6

 $\frac{-1.8}{50}$  $\frac{-3.1}{33}$  $\frac{-1.0}{10}$  $\frac{-3.6}{27}$  $\frac{-3.8}{50}$ 

T.P.

0.73 ✓

1774.10 ✓

12.57

1773.37 ✓



Suth. PL

KING 7-30-52

16

1774.10

(LF)

(RT)

~~239100~~

8.8

65.3

+31

18.2

56.0

 $\frac{-0.8}{35}$  $\frac{-1.2}{28}$  $\frac{+2.1}{12}$  $\frac{+7.0}{40}$ 

T.P.

3.46<sup>v</sup>1764.67<sup>v</sup>12.89<sup>v</sup>1761.21<sup>v</sup>

+58

7.6

57.1

 $\frac{+8.5}{35}$  $\frac{-4.3}{26}$  $\frac{+0.7}{10}$  $\frac{-1.0}{50}$ 

+89

18.1

46.6

 $\frac{+1.5}{40}$  $\frac{+2.2}{21}$  $\frac{-4.0}{27}$  $\frac{-2.5}{35}$ 

240102

27.4

37.3  
Draw $\frac{+7.1}{36}$  $\frac{+7.0}{29}$  $\frac{+4.6}{9}$  $\frac{+2.5}{12}$  $\frac{+4.3}{35}$ 

+15

16.8

47.9

 $\frac{-4.5}{35}$  $\frac{2.4}{24}$  $\frac{-3.0}{9}$  $\frac{+2.5}{15}$  $\frac{+5.0}{35}$ 

+60

5.4

59.3

 $\frac{-9.1}{50}$  $\frac{+2.4}{11}$  $\frac{+7.3}{50}$ 

+90

7.2

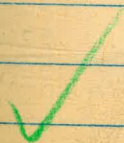
57.5

 $\frac{-10.9}{50}$  $\frac{-1.9}{4}$  $\frac{+3.0}{20}$  $\frac{+6.3}{50}$ 

241100

9.8

54.9



Profile Suthrip L.

King

7-23-52

1000

17

	1764.67		
241+13		159	48.8
+50		4.5	60.2
242		3.0	61.7
+50		2.4	62.3
TIP	6.96	1768.99	2.64
			1762.03

243		7.5	61.5
+50		5.3	63.7
244		3.8	65.2
+50		6.7	62.3

T.B.M.	5.30	1763.69	1763.60
--------	------	---------	---------

(L) (R)

$\frac{-3.2}{45}$	$\frac{-1.5}{31}$	$\frac{+5.0}{17}$	$\frac{+8.6}{50}$
-------------------	-------------------	-------------------	-------------------

$\frac{-3.8}{35}$	$\frac{+2.0}{25}$	$\frac{+2.0}{40}$
-------------------	-------------------	-------------------

$\frac{-4.4}{35}$	$\frac{+6.5}{50}$
-------------------	-------------------

$\frac{-4.7}{40}$	$\frac{-3.4}{28}$	$\frac{+5.0}{40}$
-------------------	-------------------	-------------------

$\frac{-3.4}{35}$	$\frac{+5.9}{40}$
-------------------	-------------------

$\frac{-7.6}{40}$	$\frac{-5.4}{28}$	$\frac{+6.0}{40}$
-------------------	-------------------	-------------------

$\frac{-8.0}{35}$	$\frac{-5.4}{18}$	$\frac{+5.2}{34}$ edge road
-------------------	-------------------	-----------------------------

edge field

$\frac{-3.6}{39}$	$\frac{+3.7}{10}$	$\frac{+5.7}{16}$
-------------------	-------------------	-------------------

BK = 1764.10 Ah.  
 Top of 2x2 hnb - 228 + 98.55 - old Sta

Suth. P. 1.  
Sta 36+06.71-

KING 8-14-52

18

#3  
T.B.M. 0.88 ✓  
98.95 ✓  
1887.21 ✓  
1898.01 ✓  
1886.33 ✓  
T.B.M. 3

RK816

L.T.

R.T.

36+06.71 ✓  
6.0 ✓  
93.0 ✓

$\frac{+25.0}{40'}$   $\frac{+12.0}{19'}$   $\frac{+10.0}{8'}$   $\frac{-1.3}{12'}$   $\frac{-0.8}{22'}$   $\frac{-1.5.0}{38'}$

36+50 ✓  
8.1 ✓  
90.9 ✓

$\frac{+22.0}{39'}$   $\frac{+14.0}{34'}$   $\frac{+13.0}{17'}$   $\frac{-0.8}{3'}$   $\frac{-0.4}{19'}$   $\frac{-9.7}{23'}$   
Rd. Rd.

T.P. 12.12 ✓  
1907.33 ✓  
1895.59 ✓  
3.74 ✓  
95721 ✓  
1889.47 ✓

2 x 2 Hub  
36+86.02 ✓  
1.99 ✓  
05.3 ✓

$\frac{+18.4}{32'}$   $\frac{+13.0}{23'}$   $\frac{+7.6}{14'}$   $\frac{-4.3}{8'}$   $\frac{-18.3}{16'}$   $\frac{-18.0}{36'}$

37+04 ✓  
9.0 ✓  
98.3 ✓

$\frac{+34.0}{48'}$   $\frac{+23.0}{31'}$   $\frac{+13.0}{14'}$   $\frac{+8.2}{6'}$   $\frac{-3.8}{9'}$   $\frac{-11.3}{19'}$   $\frac{-10.5}{40'}$   
Rd. Rd.

+50 ✓  
4.0 ✓  
03.3 ✓

$\frac{+18.6}{41'}$   $\frac{+13.0}{28'}$   $\frac{+7.6}{15'}$   $\frac{+0.5}{8'}$   $\frac{+1.6}{5'}$   $\frac{-5.4}{16'}$   $\frac{-18.4}{38'}$   
Edge Rd.

2 x 2 Hub  
37+86.26 ✓  
3.11 ✓  
04.2 ✓

$\frac{+19.1}{35'}$   $\frac{+13.0}{26'}$   $\frac{+7.6}{18'}$   $\frac{+1.4}{7'}$   $\frac{-5.4}{8'}$   $\frac{-5.4}{11'}$   $\frac{-8.2}{20'}$   $\frac{-15.5}{24'}$

T.P. 6.25 ✓  
1911.35 ✓  
1900.11 ✓  
1.73 ✓  
1905.60 ✓  
1893.86 ✓

38+50 ✓  
5.0 ✓  
06.9 ✓

$\frac{+18.5}{28'}$   $\frac{+13.0}{20'}$   $\frac{+7.6}{12'}$   $\frac{+0.5}{4'}$   $\frac{-0.6}{4'}$   $\frac{-5.4}{10'}$   $\frac{-13.5}{26'}$   $\frac{-18.5}{31'}$

Suth. P.L.

King 8-18-52 100°

19.

	+	18/185 1720.77	-	EL.	EEI
39+00	✓		5.5	✓	06.4

LY.				PX.			
+18.5	+13.0	+7.6	+0.4	-0.9	-5.4	-12.4	-16.5
35	27	18	4	4	10	24	32

+50	✓		4.3	✓	107.6
-----	---	--	-----	---	-------

+23.1	+18.4	+13.0	+7.6	+1.0	0.0	-5.4	-11.8	-18.2
33	27	22	13	3	2	11	21	32

Δ 2x2 HOB.	✓				
39+80.43	✓		1.92	✓	09.9

T.P.	2.67	✓	1913.64	✓	1910.97	✓	1899.23	<del>1898</del>
------	------	---	---------	---	---------	---	---------	-----------------

40+00	✓		2.8	✓	110.8
-------	---	--	-----	---	-------

+24.1	+18.5	+13.0	+7.6	+0.4	-0.5	-5.4	-15.4	-2.6
32	24	19	12	3	5	12	28	38

+50	✓		2.9	✓	110.7
-----	---	--	-----	---	-------

+18.5	+13.0	+5.0			-1.5	-10.8	-20.1
25	17	7			11	21	32

41+00	✓		4.8	✓	08.8
-------	---	--	-----	---	------

+18.2	+13.00	+2.6	+0.4		-0.8	-5.4	-9.4	-13.4
27	20	6	3		5	11	19	27

+50	✓		7.0	✓	06.6
-----	---	--	-----	---	------

+18.0	+13.0	+7.6	+4.0	+0.8	-0.3	-12.8	-25.5
32	23	14	7	4	3	22	41

42+00	✓		8.5	✓	05.1
-------	---	--	-----	---	------

+18.2	+13.6	+7.6	+3.4	+0.4	-1.1	-5.4	-11.6	-17.2
26	18	11	2	1	6	11	23	34

+50	✓		8.8	✓	04.8
-----	---	--	-----	---	------

+18.6	+13.0	+6.3			-1.6	-5.4	-13.8
26	16	4			10	14	28

Suth. Pl.

King - 8-18-52 101

20

3 43+00 ✓  
 + 1913.64 - EL. 7.4 ✓ 06.2 ✓  
~~1901.90~~

LT. RT.  
 Note: Bldr. should be meas. in 1' For Cu. yds etc  
 Huge Bldg 3' 48' 7'  $\frac{+22}{9}$   $\frac{+8.0}{17}$   $\frac{-0.8}{23}$   $\frac{-10.8}{17}$   $\frac{-15.0}{23}$  ✓

T.P. 11.34 ✓ 1913 ✓ 1907.79 ✓  
~~1907.39~~ 5.85 ✓ ~~1896.05~~

Δ 2x2 Hub  
 3 43+10.97 ✓ 12.08 ✓ 07.1 ✓

Same Bldg 3' Lt.  $\frac{+21.0}{9}$   $\frac{-0.4}{8}$   $\frac{-4.3}{9}$   $\frac{-7.4}{19}$   $\frac{-15.5}{23}$   
 Top Rock

43+17.97 ✓ 5.3 ✓ 13.8 ✓

Same Bldg  $\frac{+12.0}{12}$   $\frac{+1.0}{12}$   $\frac{-6.2}{3}$   $\frac{-9.3}{18}$   $\frac{-15.5}{27}$   
 Top Rock

40 T.P. 10.20 ✓ 1928.08 ✓ 1917.88 ✓  
~~1916.34~~ 1.25 ✓ ~~1906.14~~

43+50 ✓ 7.3 ✓ 20.8 ✓

$\frac{+14.9}{32}$   $\frac{+2.3}{17}$   $\frac{+5.6}{16}$   $\frac{-1.3}{6}$   $\frac{5.4}{10}$   $\frac{-10.0}{20}$   $\frac{-10.7}{25}$   $\frac{-14.4}{28}$

41 44+00 ✓ 3.1 ✓ 25.0 ✓

$\frac{+11.2}{29}$   $\frac{+6.4}{19}$   $\frac{-3.7}{5}$   $\frac{-9.6}{24}$   $\frac{-15.5}{40}$

POT 2x2 Hub  
 44+20.42 ✓ 2.7 ✓ 25.4 ✓

40 44+50 ✓ 5.1 ✓ 23.0 ✓

$\frac{+13.0}{39}$   $\frac{+7.4}{20}$   $\frac{-1.7}{8}$   $\frac{-4.1}{16}$   $\frac{-10.5}{30}$

T.P. 1.59 ✓ 1917.42 ✓ 1915.83 ✓  
~~1905.68~~ 12.25 ✓ ~~1904.09~~



Suth. P.h.

King

8-18-52

21

1917.42 ✓  
~~1905.68~~

EL

45+00 ✓

4.3 ✓

1900 ✓13.1

 $\frac{+14.9}{41}$  $\frac{+9.4}{29}$  $\frac{+5.3}{16}$  $\frac{+3.2}{13}$  $\frac{-2.4}{5}$  $\frac{-3.6}{14}$  $\frac{-8.6}{25}$  $\frac{-13.7}{37}$ 

45+05

~~6.6~~

✓10.8

Po. T. 2x2 HOB ✓

45+13.99

7.21 ✓ 1910.21 ✓

45+18 ✓

7.4 ✓

✓10.0

 $\frac{+14.5}{42}$  $\frac{+13.0}{36}$  $\frac{+7.6}{22}$  $\frac{+0.6}{6}$  $\frac{-1.7}{3}$  $\frac{-6.7}{14}$  $\frac{-11.9}{25}$  $\frac{-13.0}{35}$ 

T.P. 1.88 ✓

1906.34 ✓

~~1894.68~~

12.96 ✓

1904.46 ✓

~~1892.78~~45+50 ✓  
40

3.8 ✓

✓102.5

 $\frac{+20.0}{38}$  $\frac{+14.6}{29}$  $\frac{+13.1}{26}$  $\frac{+10.2}{21}$  $\frac{+9.1}{15}$  $\frac{-5.4}{13}$  $\frac{-10.7}{36}$  $\frac{-15.7}{42}$ 

46+00 ✓

4.5 ✓

✓101.8

 $\frac{+16.8}{39}$  $\frac{+14.4}{24}$  $\frac{+5.7}{15}$  $\frac{-5.4}{11}$  $\frac{-8.9}{24}$  $\frac{-12.4}{37}$ 

+50 ✓

6.1 ✓

✓100.2

 $\frac{+18.7}{26}$  $\frac{+13.3}{22}$  $\frac{+7.9}{18}$  $\frac{-5.4}{12}$  $\frac{-11.1}{22}$  $\frac{-16.6}{32}$  $\frac{-20.9}{42}$ 

47+00 ✓

10.7 ✓

✓95.6

 $\frac{+18.5}{34}$  $\frac{+13.0}{24}$  $\frac{+7.6}{14}$  $\frac{-5.4}{10}$  $\frac{-13.7}{27}$  $\frac{-22.0}{44}$ 

T.P. 0.91 ✓

1895.38 ✓

~~1883.62~~

11.89 ✓

1894.43 ✓

~~1882.71~~



Suth. P. Lr

Rings

8-18-52

104°

22

	+	1895.36	-	F <sub>2</sub>	✓	92.9	L.T.		R.T.
47+50 ✓		<del>1843.65</del>		2.7 ✓		✓92.9	$\frac{+18.4}{35}$ $\frac{+13.0}{24}$ $\frac{+7.6}{15}$		$\frac{-5.4}{9}$ $\frac{-12.4}{24}$ $\frac{-17.6}{37}$
48+00 ✓				8.3 ✓		✓87.1	$\frac{+17.7}{37}$ $\frac{+16.1}{33}$ $\frac{+10.7}{21}$ $\frac{+5.8}{10}$		$\frac{-5.4}{11}$ $\frac{-12.4}{25}$ $\frac{-19.6}{40}$
T.P	✓	1885.26	✓	1882.38	✓	1876.24			
	2.88	1873.52	12.98						
48+50 ✓				8.9 ✓		✓76.4	$\frac{+19.9}{40}$ $\frac{+14.6}{31}$ $\frac{+9.3}{22}$ $\frac{+7.2}{19}$		$\frac{-5.4}{13}$ $\frac{-7.4}{27}$ $\frac{-12.2}{31}$ $\frac{-17.3}{44}$
49+00 ✓				4.6 ✓		✓80.7	$\frac{+22.9}{42}$ $\frac{+17.3}{33}$ $\frac{+11.7}{24}$ $\frac{+7.9}{18}$		$\frac{-5.4}{41}$ $\frac{-15.0}{35}$ $\frac{-20.1}{45}$
POT 2x2 HUB									
49+33.98 ✓				5.50 ✓		✓79.8			
49+63 ✓				10.1 ✓		✓75.2	$\frac{+22.0}{41}$ $\frac{+14.3}{31}$ $\frac{+10.9}{21}$		$\frac{-5.4}{10}$ $\frac{10.4}{22}$ $\frac{-14.4}{29}$ $\frac{-18.6}{36}$
T.P	✓	74.42	✓	72.54	✓	72.54	$\frac{18.4}{35}$ $\frac{+13.6}{25}$ $\frac{+7.6}{16}$		$\frac{-5.4}{9}$ $\frac{-11.0}{20}$ $\frac{-18.0}{33}$
49+92 ✓	1.68	4862.68	12.52	1861.00					
				10.2 ✓		✓64.2			
50+00 ✓				12.4 ✓		✓62.0	$\frac{+18.2}{30}$ $\frac{+13.0}{21}$ $\frac{+7.6}{12}$		$\frac{-3.2}{10}$ $\frac{-8.8}{20}$ $\frac{-15.9}{31}$
50+12 ✓				11.0 ✓		✓63.4	$\frac{+15.2}{27}$ $\frac{+7.6}{12}$		$\frac{-5.4}{9}$ $\frac{-15.5}{30}$

Suth. P.L.

King 8-19-52

25

	+	1874.42 <del>1862.68</del>	EL.	LT.	RT.
POT. 2x2 HOB 50+48.33 ✓	✓	12.27 ✓	1862.15 ✓	$\frac{+24.7}{51}$ $\frac{+17.7}{36}$ $\frac{+10.1}{21}$	$\frac{-5.4}{91}$ $\frac{-16.5}{30}$ $\frac{-21.9}{40}$
T.P.	0.57 ✓	1861.75 ✓ <del>1850.81</del> 13.24 ✓	61.18 ✓ <del>1849.44</del>		
T.P.	0.52 ✓	1850.17 ✓ <del>1838.43</del> 12.10 ✓	49.65 ✓ <del>1837.91</del>		
51+00 ✓		2.2 ✓	48.0 ✓	$\frac{+23.7}{39}$ $\frac{+18.5}{31}$ $\frac{+13.9}{23}$ $\frac{+7.6}{15}$	$\frac{-5.4}{11}$ $\frac{-14.3}{35}$ $\frac{-19.8}{44}$
R.H. IN TREE T.P. 51+25 ✓	1.00 ✓	1844.35 ✓ <del>1832.61</del>	1843.35 ✓ <del>1831.61</del>		
+50 ✓		7.5 ✓	36.9 ✓	$\frac{+23.1}{45}$ $\frac{+18.4}{35}$ $\frac{+13.0}{26}$ $\frac{+7.6}{16}$	$\frac{-5.4}{13}$ $\frac{-15.6}{44}$
2x2 HOB POT. 51+62.60 ✓		9.48 ✓	34.9 ✓		
T.P.	1.23 ✓	1833.48 ✓ <del>1822.25</del>	12.10 ✓		
52+00 ✓		2.0 ✓	31.5 ✓	$\frac{+23.3}{46}$ $\frac{+18.5}{35}$ $\frac{+13.0}{26}$ $\frac{+7.6}{16}$	$\frac{-5.4}{12}$ $\frac{-18.8}{44}$
+50 ✓		4.0 ✓	29.5 ✓	$\frac{+18.4}{45}$ $\frac{+13.0}{30}$ $\frac{+7.6}{18}$	$\frac{-5.4}{11}$ $\frac{-19.0}{43}$

Suth. P.L.

King 8-19-52

24

	+	H1	-	EL.
		1893.48		
53+00 ✓			11.0 ✓	✓22.5

	27	Rx.
	$\frac{+18.4}{49}$	$\frac{-5.4}{12}$
	$\frac{+13.0}{33}$	$\frac{-17.0}{40}$
	$\frac{+7.6}{19}$	

T.P.	0.68 ✓	1821.90 ✓	12.26 ✓	1821.22 ✓
------	--------	-----------	---------	-----------

POT 2x2 Hub				
53+44.47 ✓			2.04 ✓	✓19.9

+50 ✓			11.2 ✓	✓10.7
-------	--	--	--------	-------

	$\frac{+13.6}{45}$	$\frac{+5.6}{19}$	$\frac{-5.4}{16}$	$\frac{-15.4}{42}$
--	--------------------	-------------------	-------------------	--------------------

T.P.	0.32 ✓	1809.37 ✓	12.85 ✓	1809.05 ✓
------	--------	-----------	---------	-----------

T.P.	0.50 ✓	1797.36 ✓	12.51 ✓	1796.86 ✓
------	--------	-----------	---------	-----------

53+97 ✓			12.8 ✓	✓184.6
---------	--	--	--------	--------

54+05.73 ✓			20.5 ✓	✓76.9 V.L.C. 6ullay -56.4
------------	--	--	--------	---------------------------------

POT 2x2 Hub				
54+50.73 ✓			0.58 ✓	✓96.8

	$\frac{+2.4}{27}$	$\frac{+2.8}{18}$	$\frac{-2.4}{15}$	$\frac{-6.4}{34}$
--	-------------------	-------------------	-------------------	-------------------

	$\frac{+2.8}{24}$	$\frac{-3.4}{12}$	$\frac{-4.4}{25}$	$\frac{-7.4}{28}$
--	-------------------	-------------------	-------------------	-------------------

	$\frac{+13.0}{45}$	$\frac{+7.6}{27}$	$\frac{-5.4}{22}$	$\frac{-13.0}{47}$
--	--------------------	-------------------	-------------------	--------------------

T.P.	12.28 ✓	1809.64 ✓	0.00 ✓	1797.36 ✓
------	---------	-----------	--------	-----------

54+7.5 ✓			9.0 ✓	✓00.6
----------	--	--	-------	-------

	$\frac{+18.3}{58}$	$\frac{+13.0}{10}$	$\frac{+7.6}{27}$	$\frac{-5.4}{18}$	$\frac{-15.3}{19}$
--	--------------------	--------------------	-------------------	-------------------	--------------------

Suth. P.L.

KING 8-19-52 HOT

25

	+	H/1 1809.64	-	EL	LT	RT
55+00 ✓			6.1 ✓	3.5 ✓	$\frac{+13.0}{43}$ $\frac{+7.6}{24}$	$\frac{-5.4}{17}$ $\frac{-15.3}{47}$
POT 2x2 HUB 55+34.16 ✓			4.35 ✓	5.3 ✓		
R.H. IN OAK 55+30 - ON East side OAK			3.02 ✓	6.6 ✓		
55+50 ✓			5.1 ✓	4.5 ✓	$\frac{+13.0}{43}$ $\frac{+7.6}{24}$	$\frac{-5.4}{15}$ $\frac{-15.9}{46}$
T.P.	4.37 ✓	1801.98 ✓	12.03 ✓	797.61 ✓		
56+00 ✓			1.4 ✓	0.6 ✓	$\frac{+13.0}{42}$ $\frac{+7.6}{22}$	$\frac{-5.4}{14}$ $\frac{-18.3}{49}$
56+50 ✓			10.2 ✓	1791.8 ✓	$\frac{+18.4}{47}$ $\frac{+13.0}{34}$ $\frac{+7.6}{21}$	$\frac{-5.4}{14}$ $\frac{-14.4}{46}$
T.P.	0.77 ✓	1790.07 ✓	12.68 ✓	1789.30 ✓		
57+00 ✓			7.3 ✓	82.8 ✓	$\frac{+15.2}{42}$ $\frac{+7.6}{21}$	$\frac{-5.4}{15}$ $\frac{-10.0}{28}$ $\frac{-15.6}{42}$
T.P.	0.73 ✓	1778.97 ✓	11.83 ✓	782.4 ✓		

Suth. Pt.

King - 8-19-52

26

1778.97 ✓

Lt.

Pt.

57+50 ✓

4.8 ✓

74.2

 $\frac{+18.4}{47}$  $\frac{+13.0}{33}$  $\frac{+7.6}{18}$  $\frac{-5.4}{12}$  $\frac{-16.0}{36}$  $\frac{-21.1}{46}$ 

T.P.

1.04 ✓

1768.83 ✓

11.08 ✓

1767.79 ✓

57+75  
S.P.

Rock

58+00 ✓

6.4 ✓

62.4

 $\frac{+23.8}{49'}$  $\frac{+18.4}{38'}$  $\frac{+13.0}{27'}$  $\frac{+7.6}{16'}$  $\frac{-5.4}{11'}$  $\frac{-17.4}{38'}$  $\frac{-22.3}{51'}$ 

+50 ✓

9.8 ✓

59.0

 $\frac{+18.4}{41'}$  $\frac{+13.0}{27'}$  $\frac{+7.6}{16'}$  $\frac{-5.4}{10'}$  $\frac{-15.1}{35'}$  $\frac{-17.5}{41'}$ 

T.P.

1.04 ✓

1760.62 ✓

9.25 ✓

1759.58

P.O.T.  
58+86.43 ✓

3.99 ✓

04 hub  
56.6

59+00 ✓

5.4 ✓

55.2

 $\frac{+9.8}{57}$  $\frac{+9.8}{31}$  $\frac{+7.6}{23}$  $\frac{-5.4}{12}$  $\frac{-15.0}{36}$ Top bank  
Above Rd

+30 ✓

10.7 ✓

49.9

 $\frac{+7.0}{40}$  $\frac{+2.4}{7}$  $\frac{-5.4}{16}$  $\frac{-13.6}{34}$ 

Top bank

T.P.

1.04 ✓

1748.64 ✓

13.02 ✓

1747.60 ✓

Profile -  
Suth. Pk.

KING 8-20-52

27

1748-64 ✓

LT

RT

59+50 ✓

8.9 ✓

✓ 39.7

$\frac{+2.0}{50}$   $\frac{+2.6}{19}$   
Gulley

$\frac{-8.5}{32}$   $\frac{+4.0}{36}$  - Edge Rd

59+60 ✓

18.9 ✓

✓ 29.7  
Gulley

$\frac{+10.0}{30}$   $\frac{+8.0}{28}$

$\frac{-5.4}{19}$   $\frac{-5.7}{33}$   $\frac{-4.0}{39}$  Edge Road

59+80 ✓

8.2 ✓

✓ 40.4

$\frac{+17.2}{44}$   $\frac{+11.8}{29}$   $\frac{+6.4}{14}$

$\frac{-5.4}{11}$   $\frac{-14.1}{31}$   $\frac{-16.2}{41}$  Edge Rd

60+00 ✓

5.0 ✓

✓ 43.6

$\frac{+15.2}{50}$   $\frac{+13.0}{40}$   $\frac{+7.6}{30}$

$\frac{-5.8}{17}$   $\frac{-12.0}{36}$   $\frac{-19.2}{42}$  Rd

T.P.

16.14 ✓

17.54 ✓

18.4 ✓

4.60 ✓

May. 04 ✓

60+50 ✓

7.2 ✓

✓ 47.0

$\frac{+11.5}{40}$   $\frac{+9.2}{32}$   $\frac{+4.6}{16}$

$\frac{-5.4}{15}$   $\frac{-13.7}{45}$  Top Bank

P.O.T

60+86.79 ✓

7.24 ✓

✓ on high  
46.9

61+10 ✓

10.7 ✓

✓ 43.5

$\frac{+15.3}{44}$   $\frac{+8.8}{23}$

$\frac{-5.4}{15}$   $\frac{-12.8}{35}$   $\frac{-25.8}{38}$  Top Bank Above Rd

61+50 ✓

11.4 ✓

✓ 42.8

$\frac{+8.0}{48}$   $\frac{+4.6}{29}$

$\frac{-4.4}{10}$   $\frac{-11.0}{27}$   $\frac{-24.0}{32}$  Edge Rd

SOUTH Pt.

King 8-70-52

28

Lt.

Rt.

1754.18 ✓

T.P. 0.66 ✓ 1741.54 ✓ 13.30 ✓ 1740.88 ✓

62+00 ✓ 6.5 ✓ 35.0 ✓

+18.4 / 43 +13.0 / 31 +7.6 / 18 -6.9 / 19 -10.4 / 26 -14.6 / 45

\* 62+61 10.7 ✓ 30.8 ✓

+20.7 / 46 +15.3 / 32 +9.9 / 20 -9.3 / 5 -8.3 / 24 -18.3 / 45

T.P. 2.90 ✓ 1733.40 ✓ 11.04 ✓ 1730.50 ✓

62+73 Edge Rd. 11.8 ✓ 21.6

+26.0 / 42 +21.3 / 30 +15.9 / 17 +10.5 / 4 -1.4 / 20 -10.3 / 50

63+00 10.4 ✓ 23.0

+22.2 / 44 +16.8 / 32 +11.4 / 18 0.0 / 10 -0.3 / 13 -2.0 / 15 -7.6 / 38

63+42 ON Culvert 9.0 ✓ 24' (24.4) Culvert

+8.8 / 70 +4.3 / 50 -1.2 / 30 -2.4 / 21 -0.4 / 20 0.0 / 7 -5.1 / 6.6 -14.0 / 47

63+75 8.4 ✓ 25.0

+15.8 / 59 +10.4 / 40 +5.0 / 20 +0.9 / 22 -4.5 / 42

T.P. 3.55 ✓ 1725.16 ✓ 11.79 ✓ 1721.61 ✓

\* New Profile Sta 62+49 to 63+78 12/22/52 see Pg 31 FB 828

T.B.M. 6.36 1718.80 1718.82

T.B.M. #6 on wheel guard - S.W. Cor. Co. Bridge

BK. 816

ch'kd 1/16/53 by Wilbur - 11/3/52

Checked & Reduced

Suth. P.h.  
New Alignment

King - 8-18-52

Hot

29

62+17.90 P.O.T.

60+86.29 P.O.T.

59+60 24" Corr. Pipe 33' R.H. &

58+86.43 P.O.T.

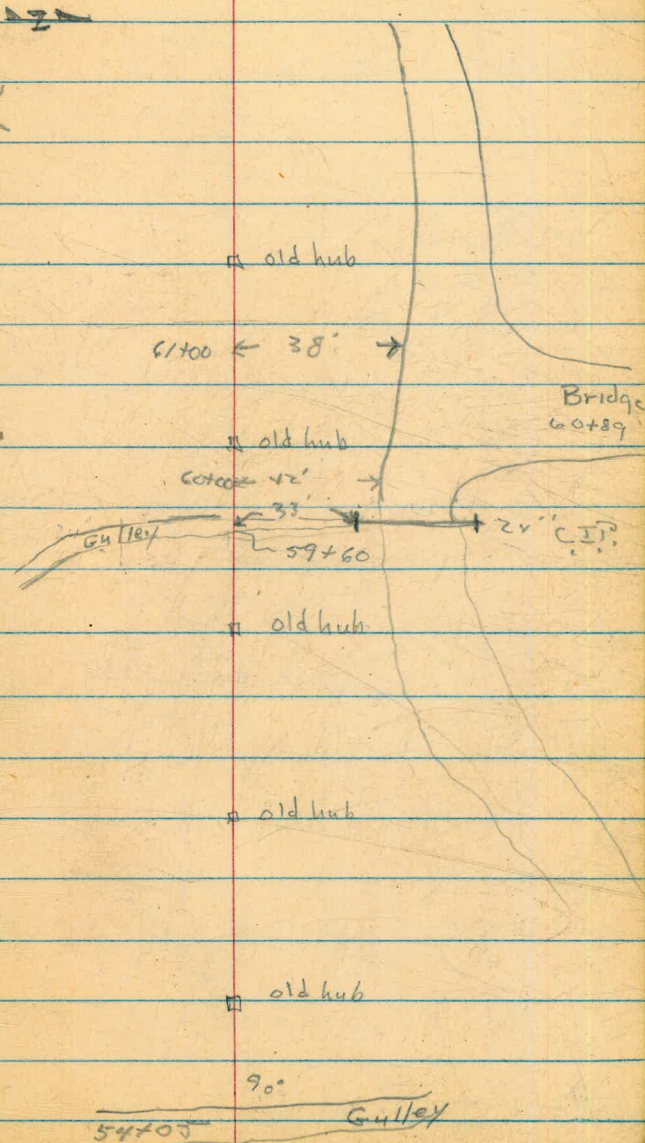
55+34.16 P.O.T.

54+50.73 P.O.T.

(See FB 815) pg. 50 W.H.



No brush - Live Oak Trees  
Good Soil - Uniform Slope





Suth. P.L.  
Alignment

King 8-19-52

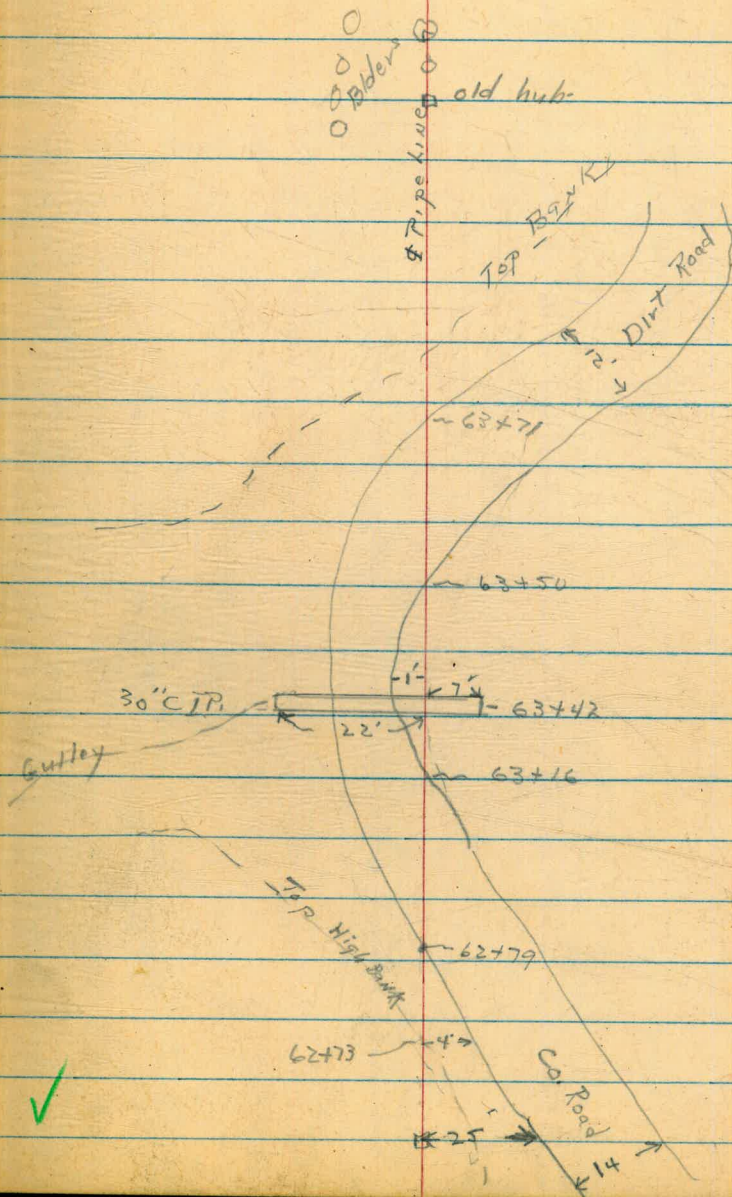
30.

See RK 825 P. 14

64+34.51 P.O.T.

63+42 30" Culvert.

62+17.90 P.O.T.



New Profile Sutherland  
 Pl. 62+17.92 to 63+86  
 (New road, out) See Page 28

	9.05 ✓	1727.87 ✓	1718.82 ✓
62+49 ✓		+3.8 ✓	Top road 24.1 ✓ 31.7 vhc
62+62 ✓		5.9 ✓	Bottom Road Out 22.0 ✓
63+00 ✓		4.4 ✓	23.5 ✓
+50 ✓		3.2 ✓	24.7 ✓
63+78 ✓		3.0 ✓	24.9 ✓
	9.05 ✓	1718.82 ✓	

West  
 market  
 Varen Fakis  
 Kemp

31  
 22 Dec 52

TBM #6 wheel Guard SW Cor. Border

6.6	6.4
80° RT	30 RT
+5.5 Top Bank	6.0
70° LT	5.4
+6.8	4.1
180° LT	10° RT edge road
3.1	5.3
30° LT	18° LT

Bottom of road out on it



Proposed Line Change  
Sta 451+80 to 456+69.09 BK  
= 456+00 AH

= 456+00 AH ? with  
456+69.09 BK  $52^{\circ} 56' 00''$  RT  
?

455+38  $62$   $52^{\circ} 55' 30''$  LT

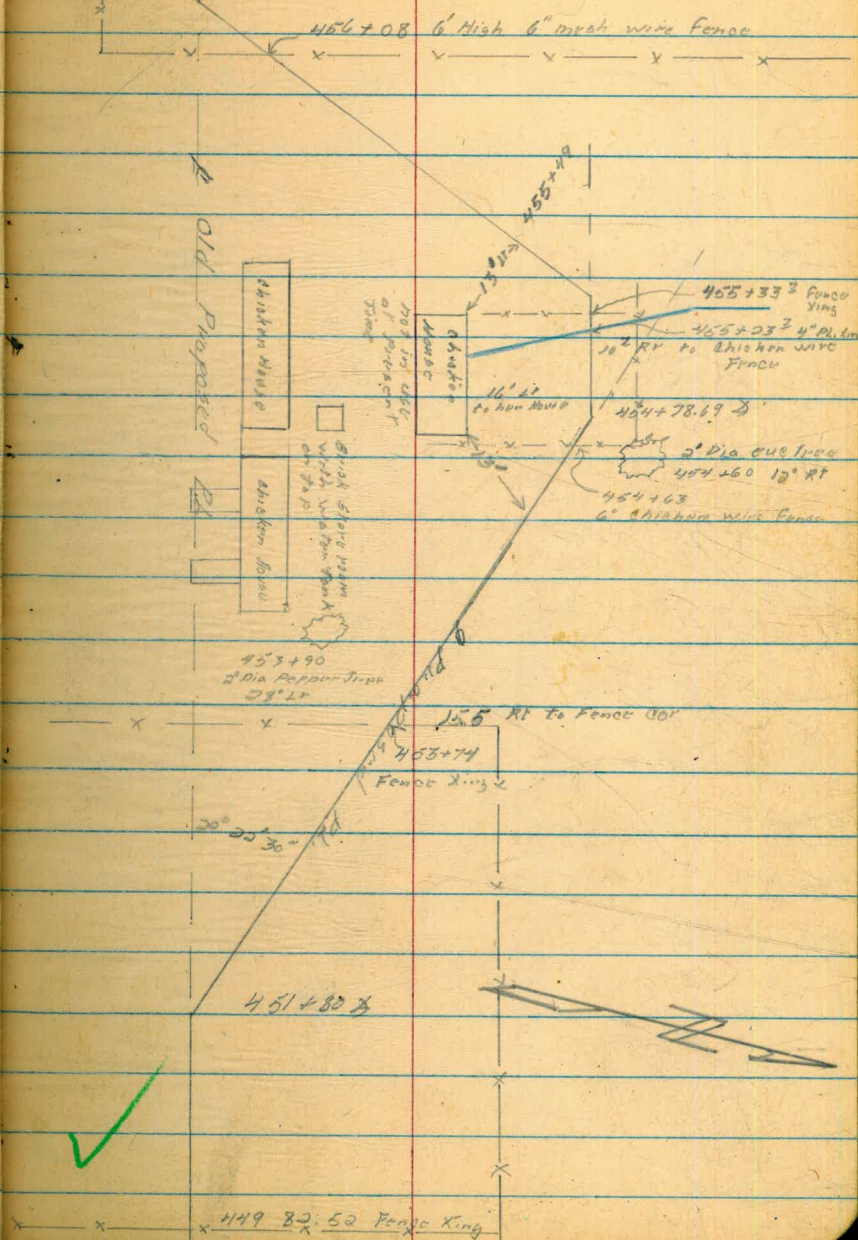
( $20^{\circ} 22' 35''$ )  
454+78.09  $\Delta$   $20^{\circ} 22' 30''$  LT

( $20^{\circ} 22' 30''$ )  
451+80  $\Delta$   $20^{\circ} 22' 30''$  RT

(See Pg 34)

West  
Williams  
Kump  
Vahon Lakes

9 March 53 32  
Warm



Q Profile Proposed P.L.  
 Change 451+80 to 456+69.09 BK  
 456+00 AM

West  
 Williams  
 Kemp  
 Voronfakus

35

9 March 53

Sta	r	H.	-	Elev
	9.37	1430.13		1420.76
	7.26	1426.77	10.62	1419.51
	5.52	1431.95	0.34	1426.43
451+80			9.9	1422.1
452+00			10.2	1421.8
+50			10.3	1421.7
453+00			10.9	1421.1
+50			11.3	1420.7
	9.93	1431.42	10.46	1421.49
454+00			7.8	1423.6
+50			3.9	1427.5
454+79 <sup>ca</sup>	1.61	1430.23	2.80	1428.62
454+78 section				
455+00			2.1	1428.1
455+37 <sup>ca</sup>			3.2	1427.0
455+51			2.9	1427.3
456+00			2.9	1427.3
456+50			8.7	1421.5
456+00 AM			9.5	1420.7
456+69.09 BK			9.5	1420.7
338		1422.65	10.26	1419.27
			18.4	1420.81

BM SW Cor Con Spillway at 10<sup>th</sup> 51

6.0	10.2
<u>20.4</u>	<u>20.8</u>
0.6	5.5
<u>20.4</u>	<u>20.8</u>

Turn on Hub

0.3	2.1
<u>16.2</u>	<u>11.8</u>
1.4	2.3
<u>16.4</u>	<u>11.8</u>

2.0	4.6
<u>13.4</u>	<u>20.8</u>

1.8	3.2	6.6	7.7
<u>20.4</u>	<u>5.8</u>	<u>11.8</u>	<u>20.8</u>

6.2	9.3
<u>20.4</u>	<u>20.8</u>

Checked & Reduced - 3-18-53 - Wilbur  
 = 1420.76 BM

ALIGNMENT CHANGE  
 451+80 TO { 456+69.03 BK  
 { 455+98.58 Ah.

(See Pg 32 for field check)

$$\overline{AB} = \frac{454 + 78.69}{451 + 80.00} = 298.69$$

$$\overline{CB} = 60.00 = \overline{EF}$$

$$\overline{CE} = \overline{BF} = \overline{AB} \sin \alpha = 298.69 \times 0.34816305 = 103.9928$$

$$\overline{CD} = \frac{\overline{CE}}{\sin \beta} = \frac{103.9928}{0.79784705} = 130.3418$$

$$\text{Sta @ D} = \frac{455 + 38.69}{+ 1 \ 30.34} = 456 + 69.03 \text{ BK}$$

$$\overline{AF} = \overline{AB} \cos \alpha = 298.69 \times 0.93743399 = 280.0022$$

$$\overline{DE} = \overline{CD} \cos \beta = 130.3418 \times 0.60285992 = 78.5778$$

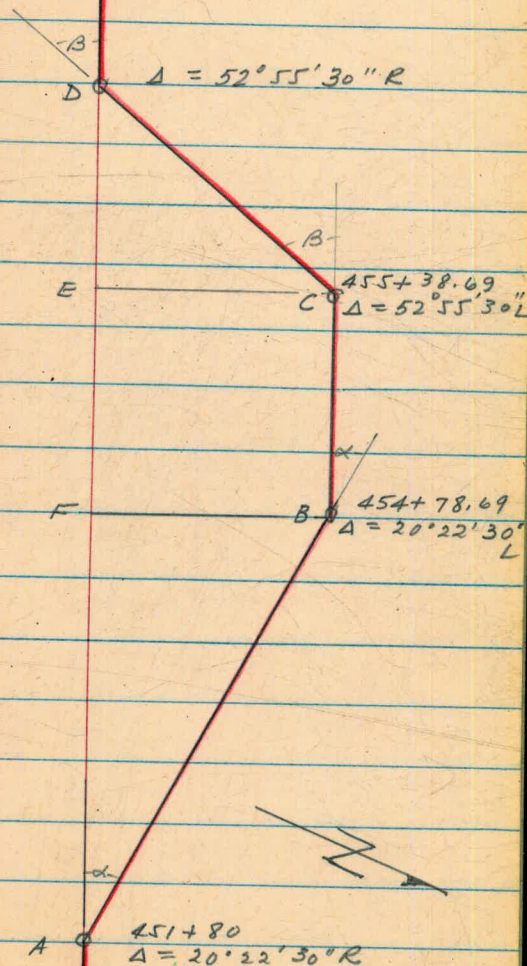
$$\begin{array}{r} \text{Sta @ D} = 451 + 80.00 \\ \quad \quad \quad \sim 80.002 \\ \quad \quad \quad \quad 60.00 \\ \quad \quad \quad \quad 78.578 \\ \hline \end{array}$$

455 + 98.58 Ahead

19 March 53 - Wilbur  
 Supercedes FB 815 Pg 19

34

$$\begin{array}{ll} \sin 20^{\circ}22'30'' = 0.34816305 & \sin 52^{\circ}55'30'' = 0.79784705 \\ \cos \quad \quad \quad = 0.93743399 & \cos \quad \quad \quad = 0.60285992 \end{array}$$





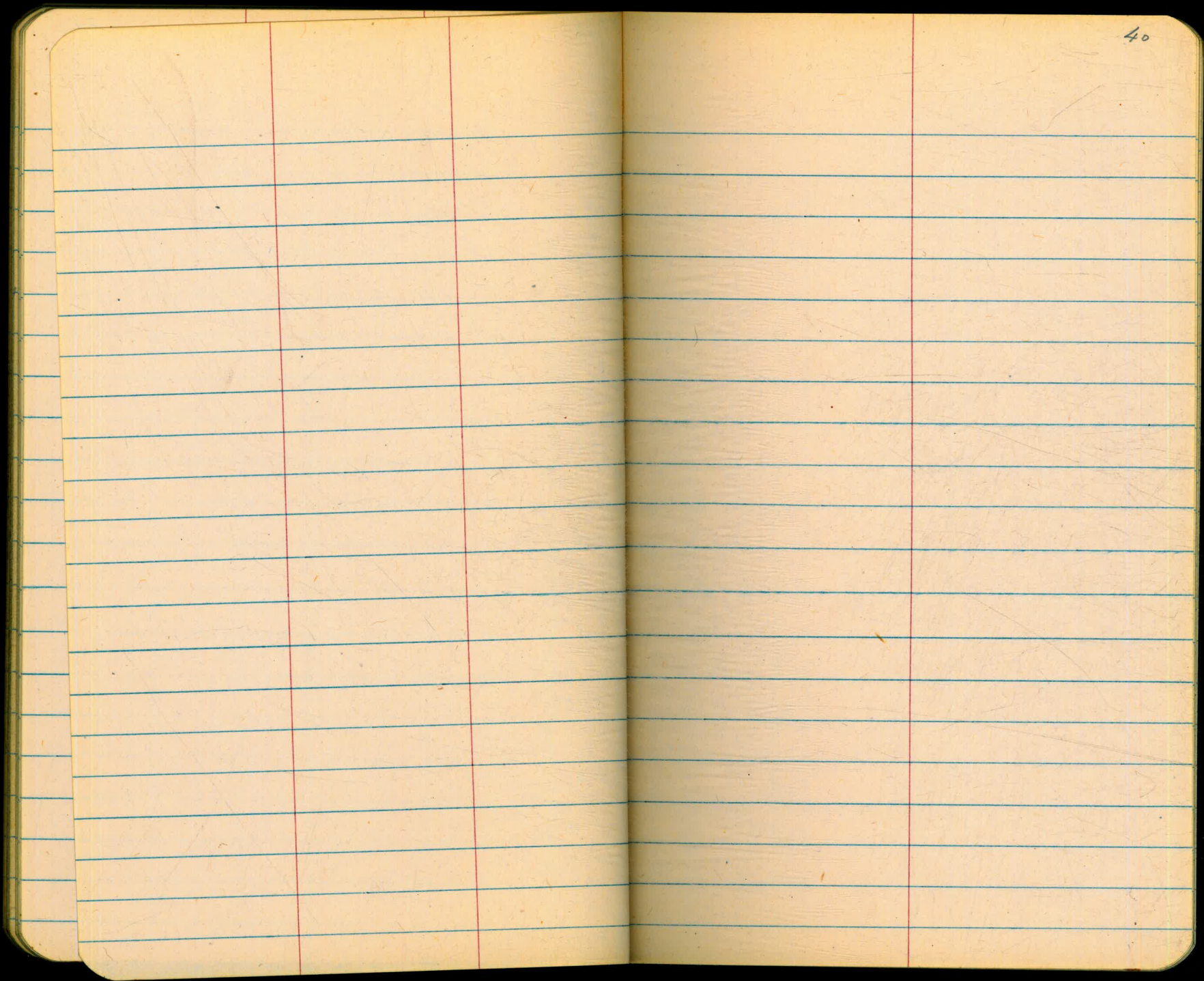


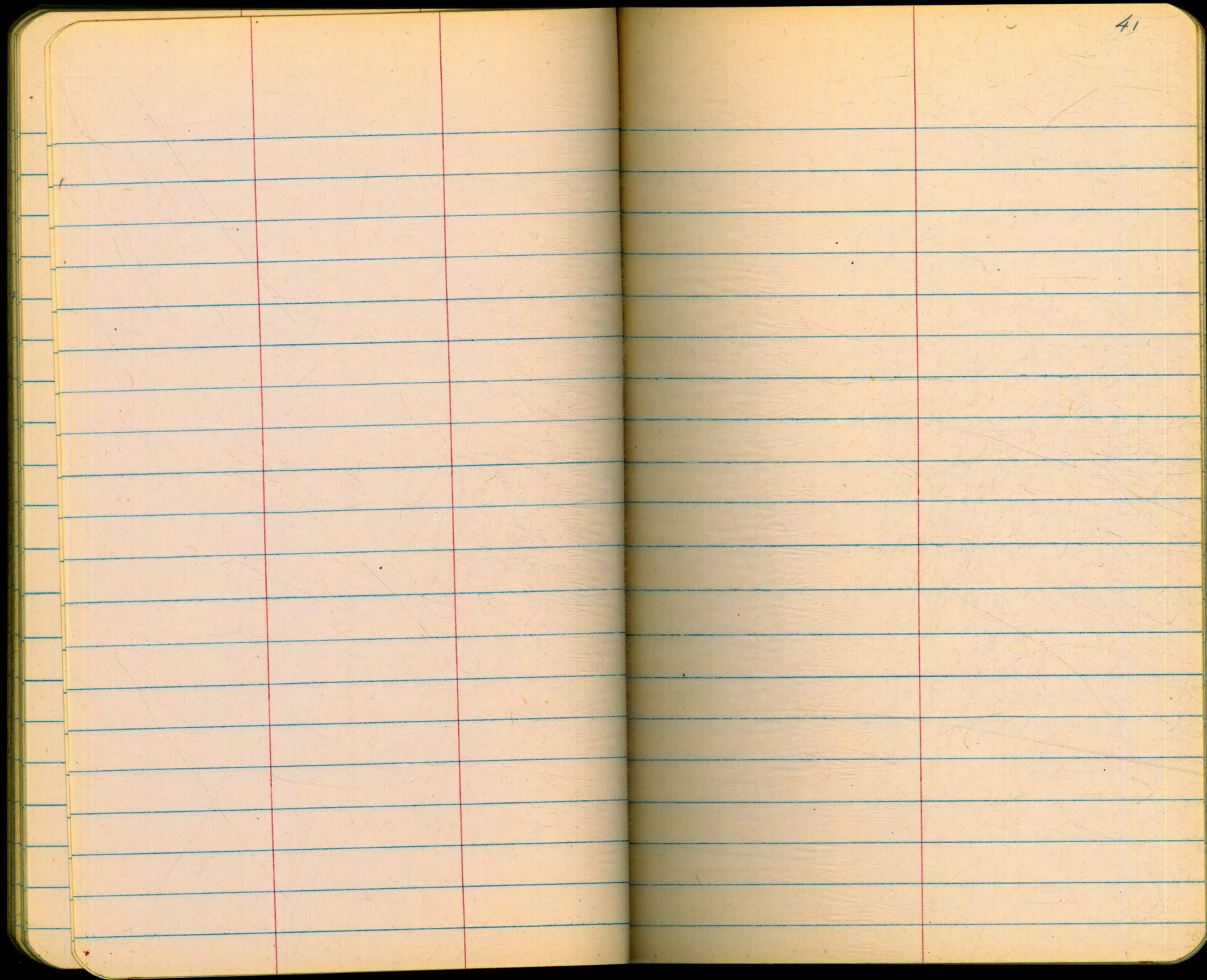








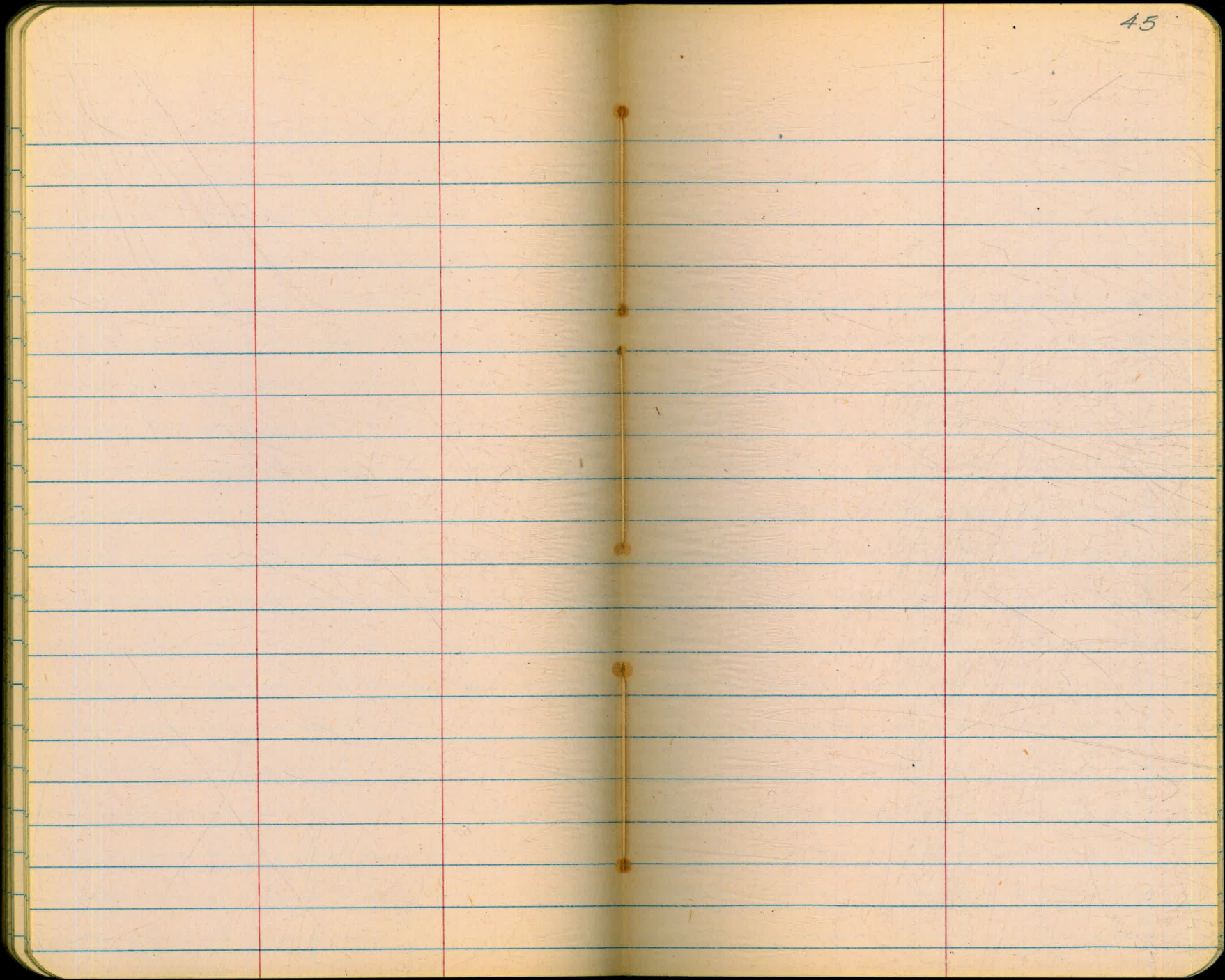






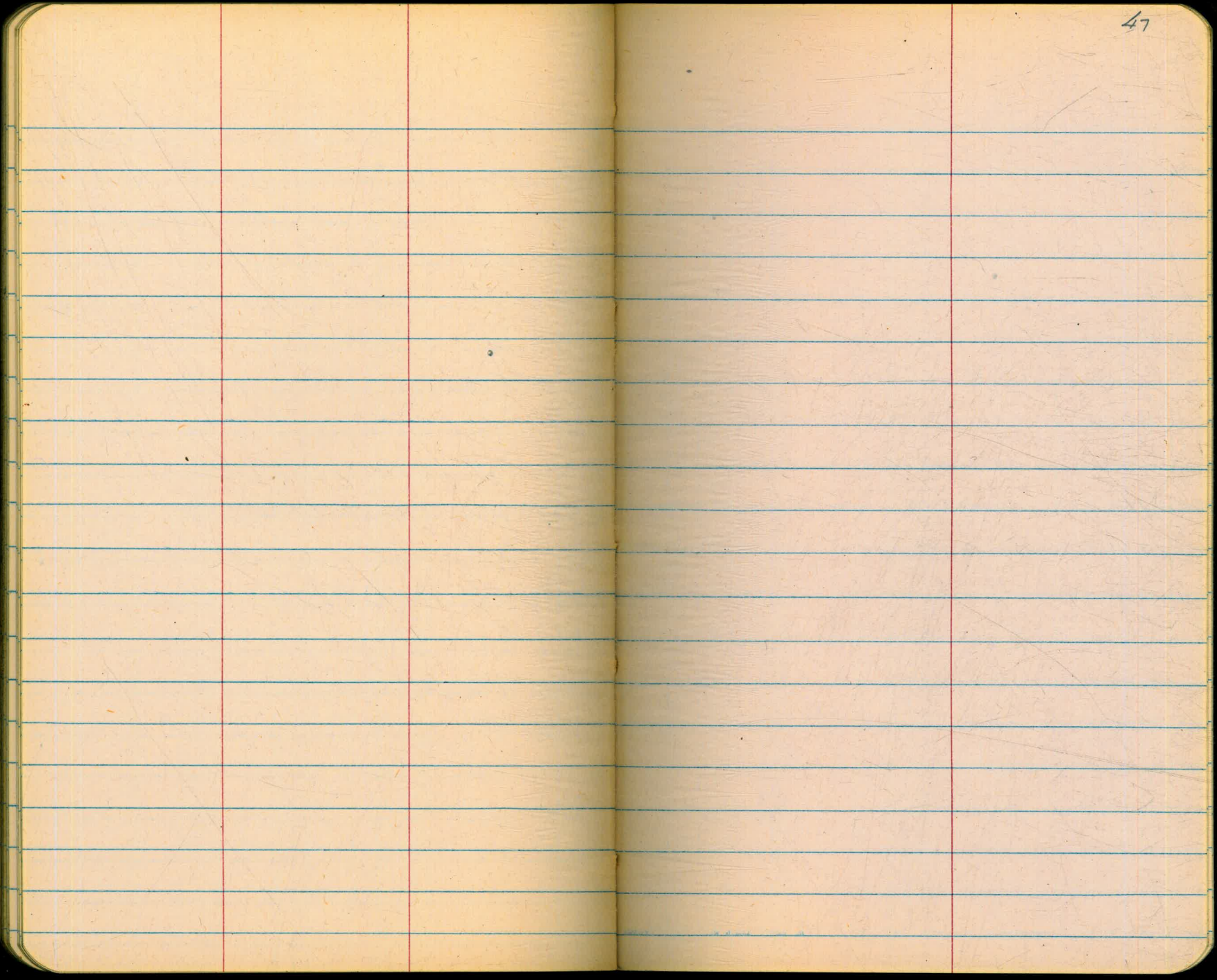


















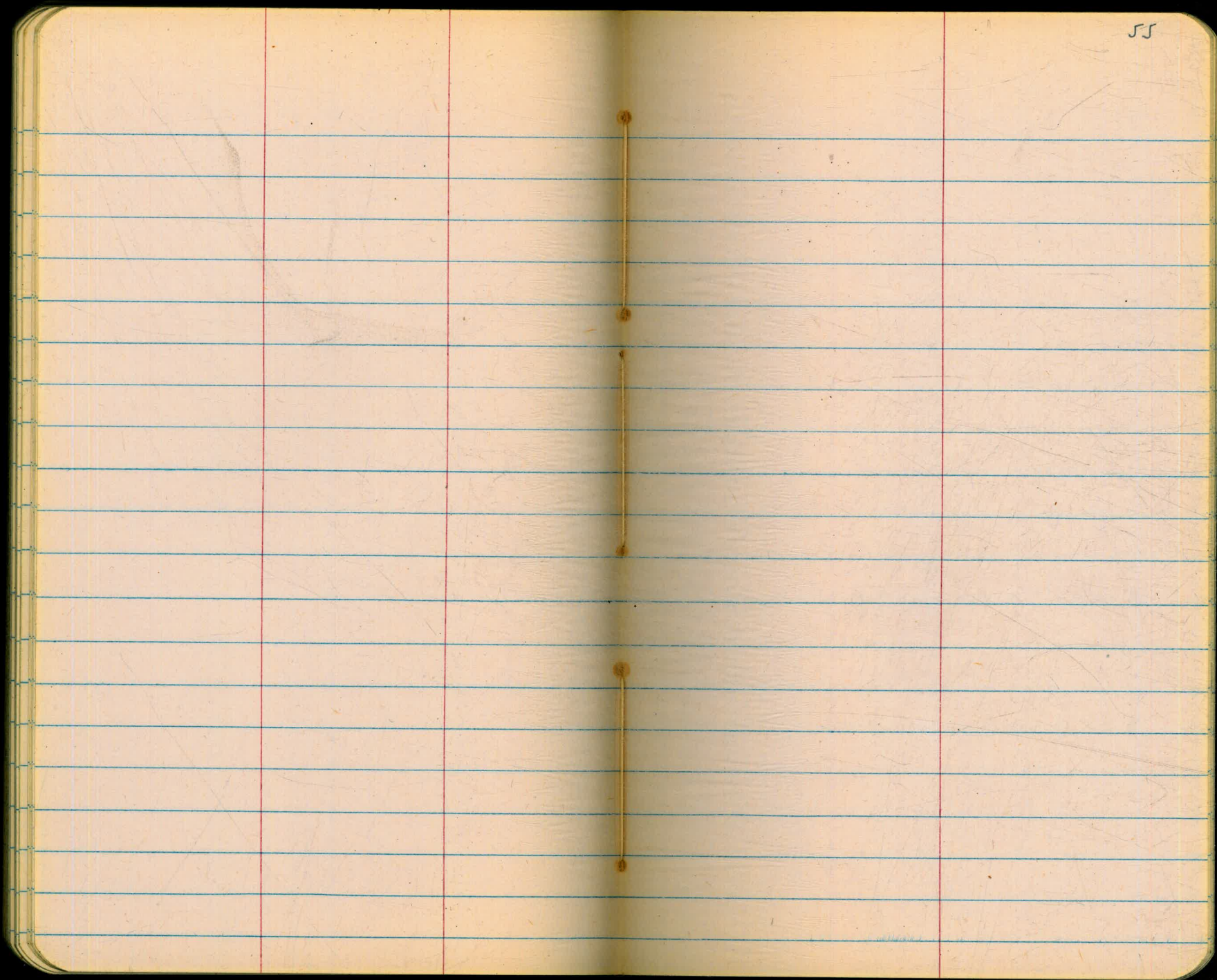




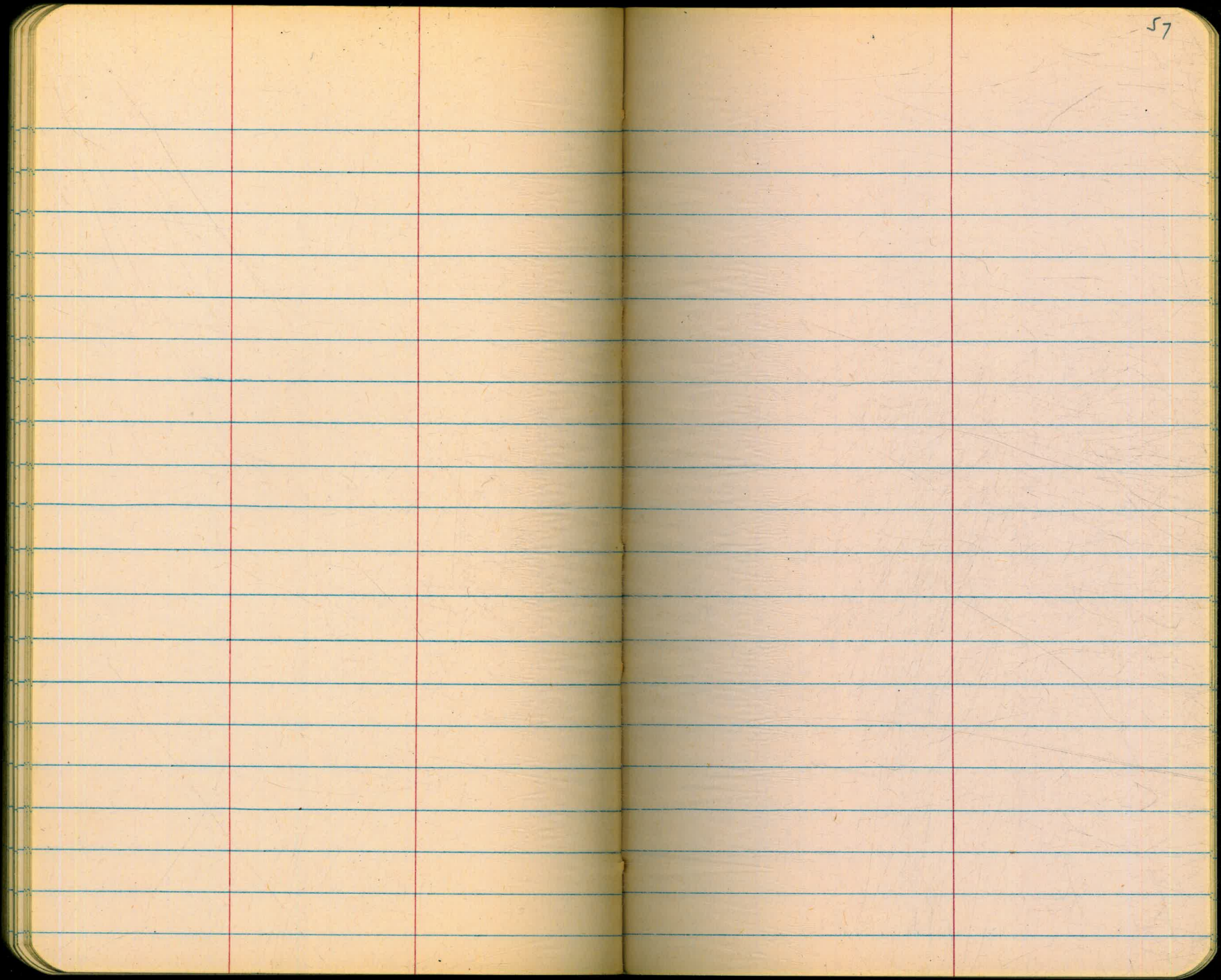
















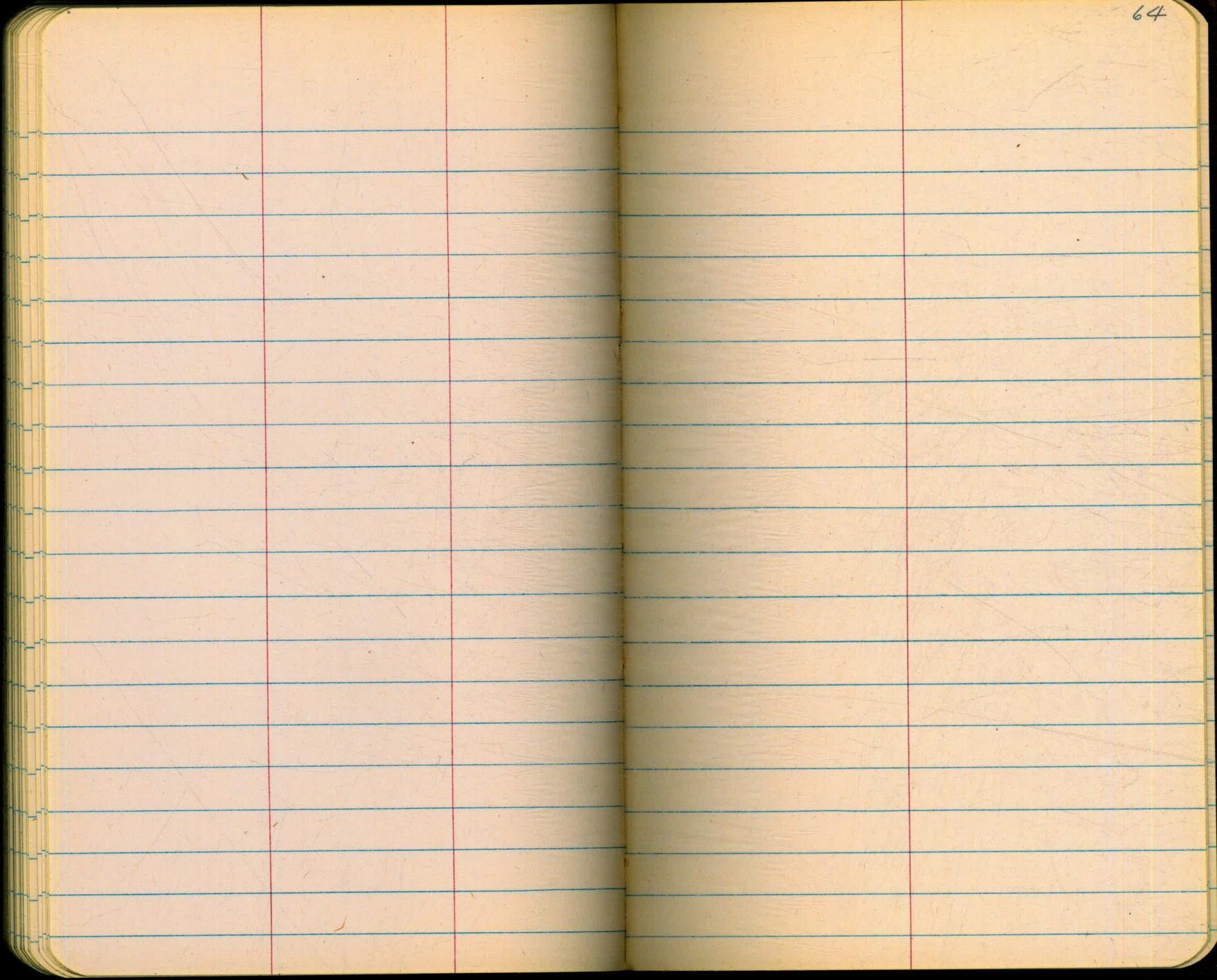


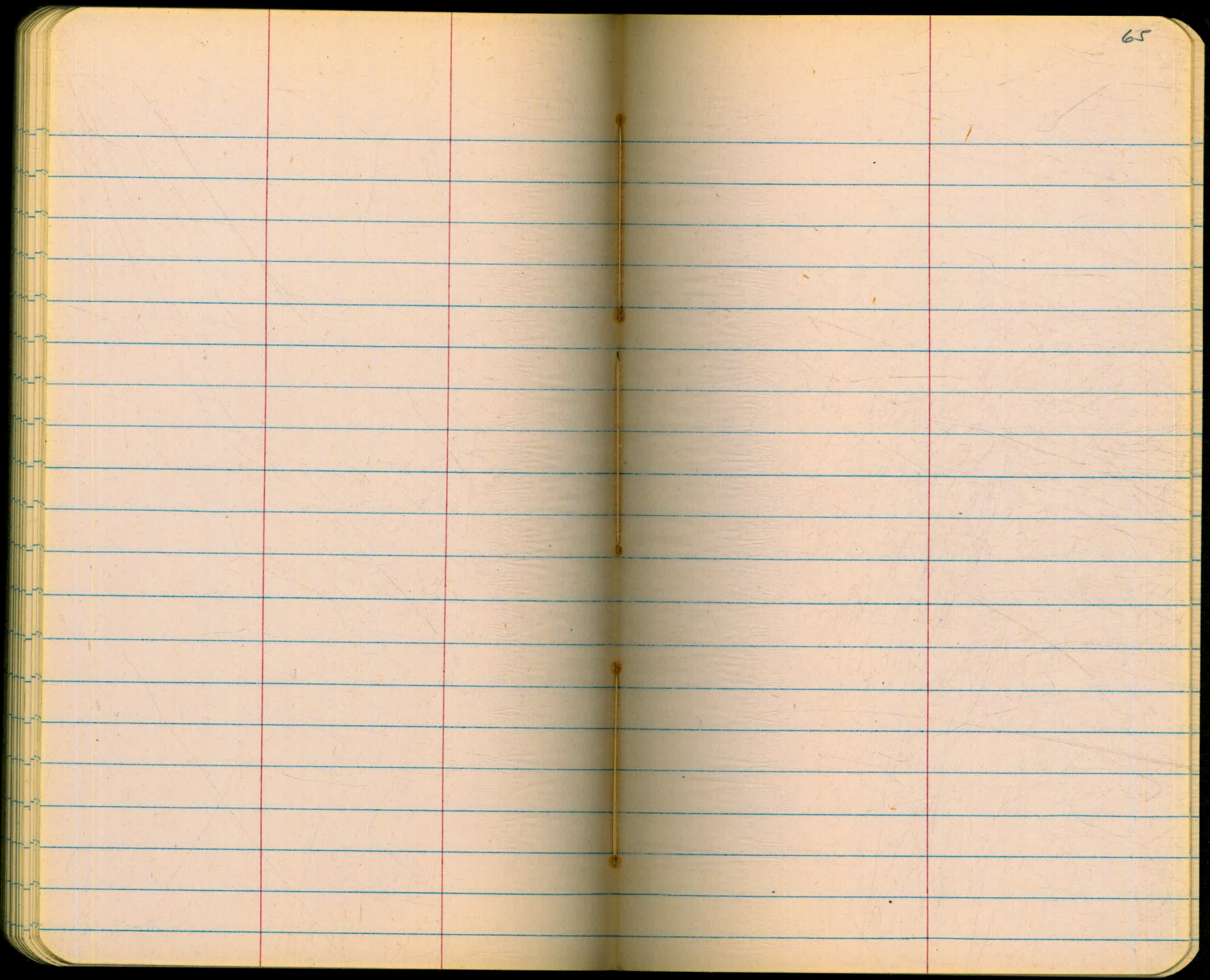






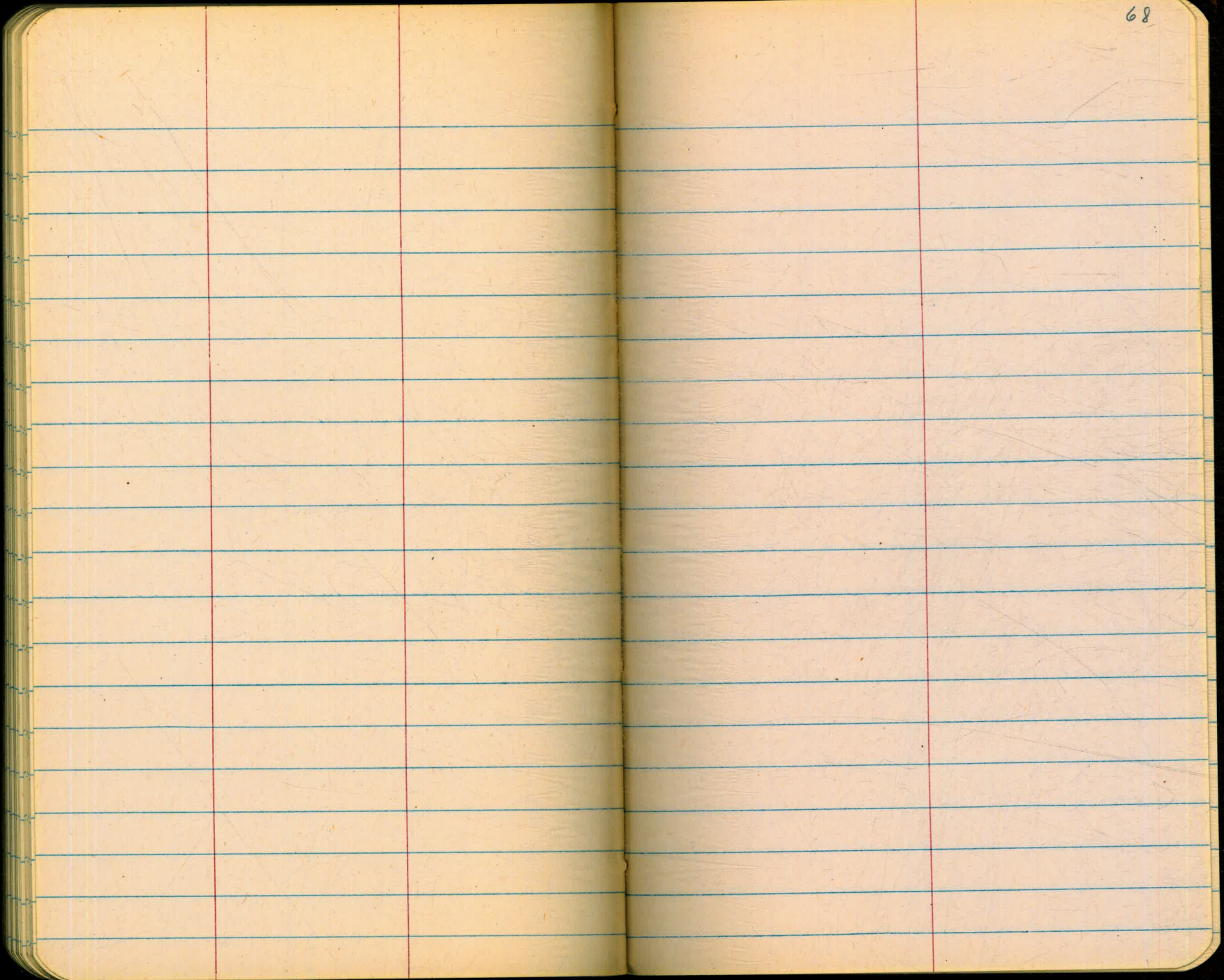
















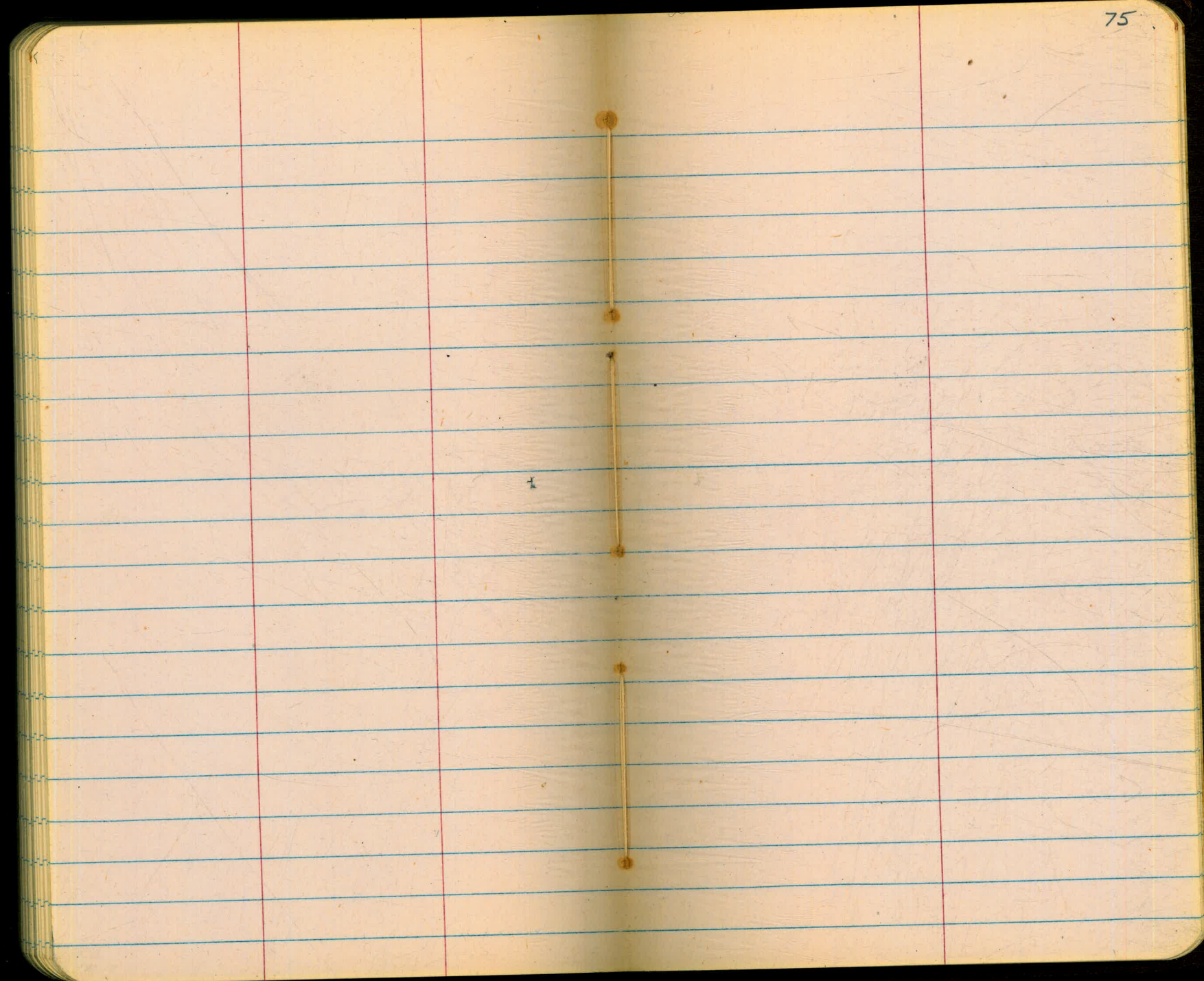


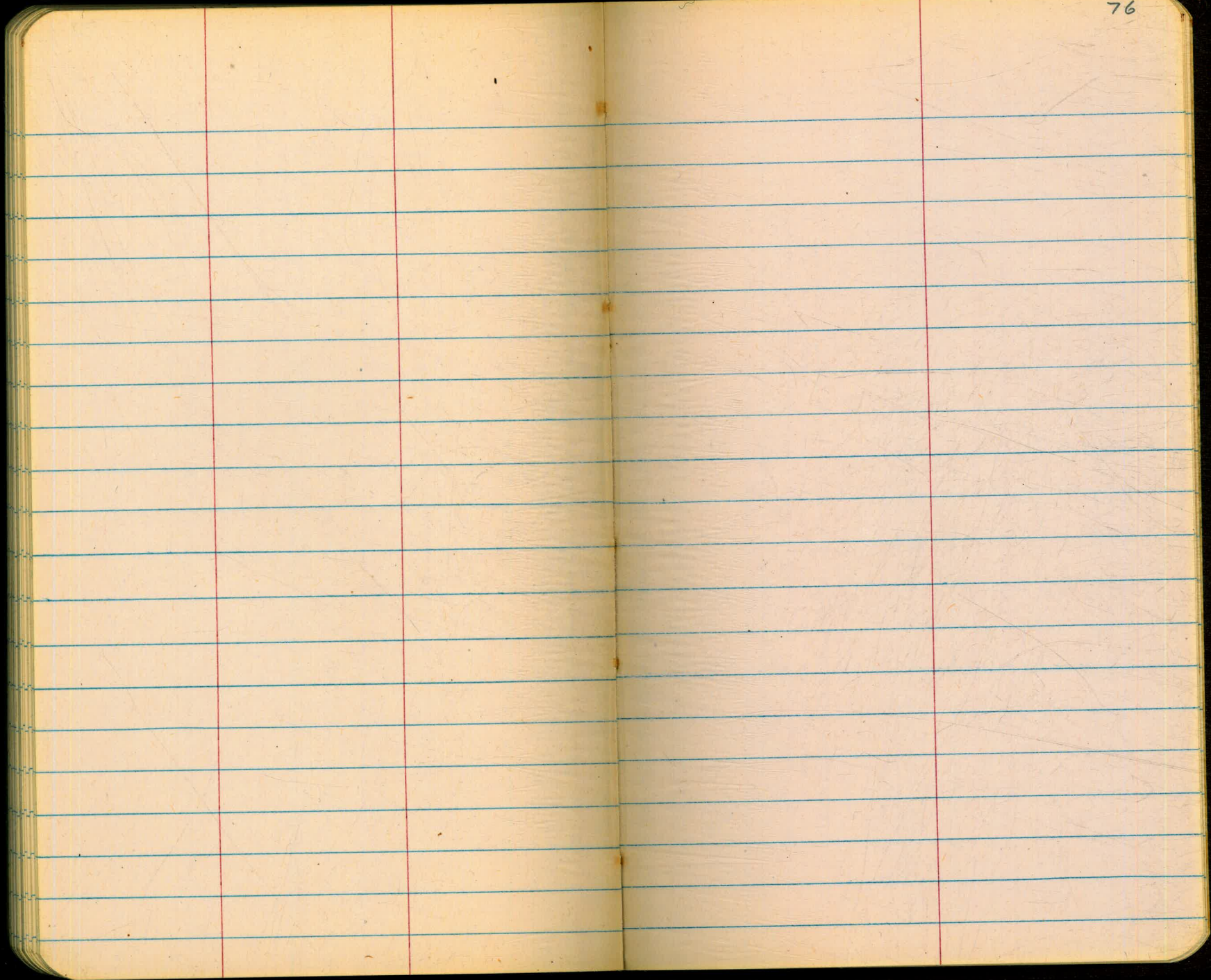






3











#3 - 1898.07

#4 - 1810.78

#5 1767.54

#6 1718.82 - Bridge

#7 1760.67

---

1870

52 56  
52 56  
105 50

62 + 17 90  
31 07

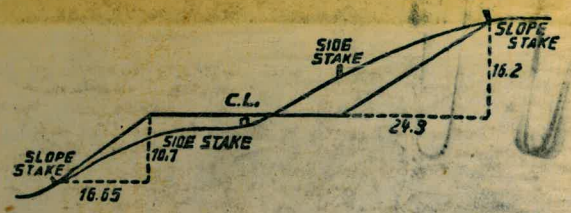
49 00

227 x 6 2

49.3

258 100  
18 15

Please Return to  
City of San Diego Water Dept.  
Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.  
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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