

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level, estimate the difference in elevation between the side stake and slope stake, slope being by the amount of cut or fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

City of San Diego Water Dept.
Room 903 Civic Center

832 Return to
City of San Diego Water Dept.
Room 903 Civic Center



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JAN 10 1965

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE															
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°		
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46		
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68		
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90		
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14		
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39		
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66		
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94		
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21		
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48		
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77		
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07		
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39		
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72		
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09		
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46		
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89		
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32		
95°	.39	.79	1.19	1.55	1.92	2.30	2.68	3.06	3.44	3.84	4.24	4.64	5.05	5.46		
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34		
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60		
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22		

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE															
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°		
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020		
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051		
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083		
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135		
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188		
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264		
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341		
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445		
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550		
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700		
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851		
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01		
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17		
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.887	.977	1.07	1.18	1.29		
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62		
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91		
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20		
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58		
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96		
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96		
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32		

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Sept. 18, 1952

DEATY
POWELL
ALEXANDER

1.

ERIE ST.

INGULF TO MILTON

⑥ STKS & GRADES SET FOR 6" WATER

STATION	+B.S.	H.I.	-F.S.	ELEV.	GRADE Bot. Pipe	
TBM.	5.89	71.24		65.35		50 x 60 Rim Sewer M.H. 10' W of L.S. FB 817 pg 34
0+60			4.9	66.3	60.5	c58
+80		Noe Prop line Ingulf.	5.3	65.9	60.5	c54
+90	F.H. TEE		5.2	66.0	60.6	c54
	⑤ F.H.		3.85	67.39	64.5	c29 c64
1+50			4.4	66.8	60.9	c59
2+00			4.6	66.6	61.2	c54
+50			3.0	68.2	61.4	c68
3+00			2.8	68.4	61.7	c67
+50			3.8	67.4	61.9	c55
3+90			4.5	66.7	62.1	c46
4+00			2.8	66.4	62.0	c44
+30			4.2	67.0	61.7	c53
+70		4 JELLETE	4.0	67.2	61.3	c59
5+20	F.H. TEE		4.3	66.9	60.8	c61
⑤	133	69.42	3.13	68.11 (687)	62.9	c33 c62
+50			2.9	66.5	60.0	c65
6+00			4.4	65.0	58.8	c62
+50			6.1	63.3	57.7	c56
7+00			7.3	62.1	56.7	c54
+50			8.5	60.9	55.6	c53
8+00			9.5	59.9	54.6	c53

ERIE ST
(Cont'd.)

9-18-52

2

69.44

8+60		11.3	58.1	53.4	C47	
9+00		11.6	57.8	52.8	C50	
+10 (E KANE ST)		11.5	57.9	52.6	C53	
P +60	3.54	60.33	12.65	56.79	51.9	C49
+70 F.H. TEE		3.6	56.7	51.7	C50	
(5) F.H.		1.74	58.59	55.8		C 28 C 63
10+00		3.9	56.4	51.2	C52	x on cone
+50		4.0	56.3	50.4	C59	
11+00		4.4	55.9	49.5	C64	
+50		5.0	55.3	48.6	C67	
12+00		5.4	54.9	47.8	C71	
+50		5.8	54.5	46.9	C76	
13+10		7.3	53.0	45.9	C71	
+50		8.4	51.9	45.4	C65	
+90		9.5	50.8	44.9	C59	
14+00 F.H. TEE		9.8	50.5	44.7	C58	
(5) F.H.		7.03	53.30	48.8		C 43 C 80
+50		11.3	49.0	43.7	C53	
P 15+00	1.41	48.47	13.27	47.06	42.7	C44
+50		3.4	45.1	41.7	C34	
16+00		4.5	44.0	40.7	C33	

ERIE ST.
(Cont'd.)

9-18-52

3.

48.47

16+50

4.8 43.7 39.7 C42

17+00

5.3 43.2 38.7 C45

+10

5.6 42.9 37.9 C50

+85

+90

END
WALK

5.5 43.0 37.8 C52

6.40 42.07 = 42.07

BR. SW COR MILTON & ERIE

VAN NUYS ST.
 (2) STKS & GDS FOR WAT. MET. S
 LA JOLLA MESA DRIVE, Easterly

SEPT 26 1952
 BETTY
 POWELL
 ALEXANDER

PK MET. BOX = 245 ft. 4 ST.
 5.27 123.49
 1.43 128.96 12.96 127.53
 0.26 140.29 12.60 140.23

3/4" IP Prop Cor SE Cor
 ARCHER & LA MESA DR

0+00 = E Prop line La Jolla Mesa Dr.

0+41 So **NOTE** 9.53 143.3 142.2 C1'

10+85 So **LEVEL NOTES** 7.7 145.1 144.1 C10

**RUN UP
 THE PAGE**

1+35 Nor 4.13 148.7 146.2 C12

1+52 So 6.7 146.1 146.1 C02

1+79 Nor 3.99 148.9 147.0 C19

2+25 Nor 6.23 128.6 147.3 C13

2+49 So 6.7 126.1 147.1 F10

2+71 Nor 2.9 147.9 147.8 C01

3+20 Nor 4.2 148.6 148.5 C01

3+23 So 5.8 147.0 148.2 F08

IP 4.57 152.83 13.32 148.26

3+74 So 13.2 148.2 149.5 F11

3+77 Nor 11.0 150.6 150.0 C06

4+28 Nor 8.3 153.3 152.1 C11

4+35 So 10.3 151.3 151.8 F02

4+67 Nor 6.6 155.0 153.8 C12

4+70 So 7.9 153.7 153.3 C04

5+05 Nor 2.3 157.3 155.3 C20

5+43 So 5.0 156.6 156.4 C02

161.58

VAN NUYS ST. (WAT. MET)
(Cont'd)

9/26/52
10/2/52

5.

5+82 So.		3.5	158.1	158.0	C01
6+21 Nor.		+1.2	162.8	160.2	C26
6+38 So.		1.2	160.1	160.4	C00
	0.10	161.58	13.29	161.48	
6+82 Nor.		9.7	165.1	162.6	C25
6+88 So.		12.6	162.2	162.2	C00
7+30 So.		11.8	163.0	163.1	F01
+41 Nor.		7.7	167.1	163.8	C33
8+10 So		10.87	163.9	163.8	C02
8+66 So.		10.15	164.6	164.4	C02
9+26 So		10.6	164.2	164.8	F04
9+64 Nor		8.6	166.2	165.9	F03
9+89 So		9.7	165.1	165.8	F02
10+15 So		9.17	165.6	166.4	F08
10+68 So.		7.1	167.7	167.7	F00

P	5.42	169.61	164.19	C285
8+17 ⁰² Nor	w 2.47		167.15	1642
3-METS	E 2.51		167.10	
	5.79		163.8	C28

TBM		6.20	168.57	
P	6.93	174.77	0.02	167.84
BM	13.36	167.86		154.50

SW Cor
7' Conc Mon VAN NUYS E C299

7' Conc Mon NW Cor Square of Cor

NOTE
LEVEL NOTES
Go
UP THE PAGE

Van Nuys St. (WAT MET.)
(Cont'd.)

9-29-52

6.

TBM	13.33	136.82		123.49			
TP	13.32	149.86	0.30	136.52			3/4" I.P. Prop Cor SE Cor La Jolla Mesa Dr & ARCHER
TP	13.31	163.05	0.12	149.74			
TP	4:27	167.11	0.21	162.84			
SET TBM			4.01	163.12			7' Conc Mer SW Cor Cass & ARCHER
CK TBM			12.56	154.55 = 154.50			7' " " NW Cor " & Agate

TBM	3.33	143.56		140.23			
0+00 - W. PL. La Jolla Mesa Dr							
0+27 So			4.2	139.4	139.7	FO3	143.6
0+33 Nor			2.9	140.7	140.3	CO4	143.3
0+76 So			5.9	137.7	138.1	FO4	
1+08 Nor			5.2	138.4	137.2	C12	
1+26 So			8.4	135.2	136.1	FO2	
1+49 Nor			7.5	136.1	135.7	CO4	
1+69 So			10.3	133.3	132.5	F12	
1+92 Nor			9.3	134.3	134.0	CO3	143.56
2+22 So			12.15	131.4	132.4	F12	9.05
2+40 Nor			9.9	133.7	132.1	C12	134.51
2+86 So			13.6	130.0	129.9	CO1	135.0-
2+91 Nor			11.3	132.3	130.3	C2e	
3+02 So	3.87	132.16	13.27	130.29	129.4	C25	
3+58 Nor			4.1	130.1	127.6	C25	
3+92 Nor			6.0	128.2	126.2	C20	
4+39 Nor			7.7	126.5	124.6	C12	
4+69 So			10.7	124.0	123.6	CO4	

TP 12.56 143.28 1.44 132.72

CK TBM 3.05 140.23

P.M. 4.79 122.23 139.56 Conc Mer.

α TP 4.10 140.23 = 140.23

Ⓟ FH 5.46 138.87 139.40 FO⁵³

DENVER ST.
 In Gulf to MILTON
 ⑥ STKS & GRDS for 6" WATER

SEPT 29 1952

7.

BEATTY
 POWELL
 ALEXANDER

BM	0.02	65.37		65.35			
77	1.82	54.99	12.20	53.17			
17+65	END WORK		1.1	53.9	49.0		C49
17+60	= So Prof line In Gulf.						
17+37	FH TEF		1.4	53.6	48.8		C48
	⑤ "		0.32	54.67	51.85		C 28 963
17+00			2.0	53.0	48.0		C50
17+50			2.9	52.1	46.9		C52
16+00			4.3	50.7	45.8		C49
16+50			5.1	49.9	44.7		C52
15+00			6.9	48.1	43.6		C45
14+50			8.6	46.4	42.5		C39
14+00					41.4		
13+90			9.1	45.9	41.2		C47
13+50	E JELLETS	9.4	45.6	40.75			C49
13+10		8.3	46.7	40.3			C64
13+00	FH TEF	7.8	47.2	40.1			C71
	⑤ FH	5.90	49.09	44.41			C47 C82
+50	2.57	51.66	3.4	48.2	39.7		C85
12+00			3.7	48.0	39.3		C87
+50			4.7	47.0	38.9		C91
11+00			5.1	46.6	38.5		C81

Sx on M.H In Gulf & ERIE
 CONC. MON In Gulf & DENVER

DENVER
(CONT'D)

9-30-52

8.

21.66

10+50		5.3	46.4	38.1	c83	✓
10+00		7.1	44.6	37.7	c69	✓
9+75		7.8	43.9	37.5	c64	✓
9+50		8.7	43.0	37.1	c64	c59
9+10	E KANE					
9+00		10.5	41.2	36.4	c48	
8+50	0.09 F.H. TEE	40.53	11.22	40.44	35.4	c50
	⑤ FH		+0.7	41.23	39.5	c12 52
8+00		1.3	39.2	34.3	c42	
+50		1.8	38.7	33.1	c56	
7+00		3.0	37.5	32.0	c55	
+50		4.9	35.6	30.8	c48	
6+00		5.2	35.3	29.7	c56	
+50		5.7	34.8	28.5	c63	
5+00		7.0	33.5	27.4	c61	
4+50		8.0	32.5	27.0	c55	
4+20	F.H. TEE		8.6	31.9	26.7	c52
	⑤ FH		7.6	32.9	31.0	c12 c52
4+00			8.5	32.0	26.8	c52
+50			8.7	31.8	27.0	c48
3+00			8.5	32.0	27.2	c48
+50			7.7	32.8	27.4	c54
⑪	5.51	38.44	7.60	32.93		

DENVER ST
(CONTD)

9-30-50

9.

38.44

12+00		5.5	32.9	27.6	C53 ✓	
10 +50		4.5	33.9	27.8	C61 ✓	
9 1+00		4.4	34.0	28.0	C60 ✓	
9 +90	FH TEE	4.4	34.0	28.0	C60 ✓	
9	(5) FH	3.82	34.60	32.45		C2L C56
9 +80		4.3	34.1	28.1	C60 ✓	
8 0+35	BEGIN WORK	4.7	33.7	28.4	C53 ✓	
8 11 P	7.71	45.74	0.41	38.03		
CKBM		3.65	42.09	= 42.03		BD SW COR ERIE & MILTON

ERIE ST.

(2) STKS # GRDS for WAT. MET.

Pk. Met. 24E 47 & RT E ST

TBM	7.31	72.66	65.35			
0+00 = Nor. RL	In Gulf.					
0+83 E		5.7	67.0	64.5	C25	
1+16 W		8.5	64.2	63.4	C06	
1+55.5 E		4.3	68.4	64.9	C35	
1+70 W		8.8	63.8	64.0	F02	
2+05 W		8.7	67.0	64.2	F02	
2+06 E		4.0	68.7	65.2	C35	
2+50 W		8.4	64.3	64.5	F02	
2+55 E		3.9	68.8	65.2	C34	
2+89 W		7.5	65.2	64.7	C05	
3+62 E		5.1	67.6	66.1	C15	
3+67 W		7.66	65.0	65.1	F01	
4+11 W		8.2	64.5	65.0	F02	
4+12 E	3.44	70.98	5.12	67.54	66.4	C13
5+33 E		2.9	68.1	64.6	C35	
6+26 E		5.5	65.5	62.5	C30	
6+75 E		6.6	62.2	61.4	C30	
7+69 E		9.6	61.4	59.5	C19	
7+89 E		10.0	61.0	58.0		

10/2/52

10.

85
40.5

ERIE ST

WAT MET

(Cont'd)

70.98

10/2/52

11.

8+54 E		10.6	60.4	57.6	C28		
CK gmk 8+60 (6)	3.00	61.09	12.89	58.09 = 58.10			
9+85 E		3.1	58.0	55.6 56.6	C14 C24		
10+43 E		3.25	57.8	✓ 54.6	C32 ✓		
11+00 E		3.4	57.7	52.7	C40		
11+21 E		3.2	57.9	53.3	C46		
11+80 E		4.36	56.7	52.3	C14		
12+27 E		4.8	56.3	51.5	C28 ✓	61.07 6.55	
12+76 E		5.4	55.7	50.7	C50 ✓	57.54	
13+98 E		8.8	52.3	48.8	C35 ✓		
14+02 W	1.54	50.53	10.9	50.2	48.4	C18 ✓	
14+51 E			12.10	48.99	47.8	C22 ✓	
15+05 W			0.5	50.5	47.8	C22 ✓	
15+25 W			3.3	47.2	46.4	C08 ✓	
15+70 E			4.6	45.9	45.5	C04 ✓	BM 65.4
15+71 W			6.5	42.0	45.0	F10 ✓	6.0 45
(CK gmk 15+50)			5.48	45.05 = 45.1			+15 W = 66.9 C24 64.3
							E = +19 67.3 C28 64.5

LINCOLN AVE
BOUNDARY TO 32ND

OCT. 2 1952

12

BEATTY
POWELL
ALEXANDER

④ STKS & GRDS FOR 8" WATER
KI

BM.	5.93	339.79	333.36	BP NW Cor UNIV & BOUNDARY
P	9.22	347.76	0.75 338.54	
0+16.			63 341.5 337.8	C32
+30			5.7 342.1 336.8	C33
+48	8" TEE		5.4 342.4 337.7	C47
+87			5.0 342.8 339.2	C36
1+00			4.9 342.9 339.3	C36
+50			4.8 343.0 339.5	C35
2+00			4.6 343.2 339.7	C35
+50			4.5 343.3 339.9	C34
3+00			4.2 343.6 340.1	C35
+50			4.1 343.7 340.3	C34
3+80			4.0 343.8 340.4	C34
3+87			3.9 343.9 340.5	C34
3+98	FH TEE		3.8 344.0 340.5	C35
4+25			3.5 344.3 340.5	C38
		6" AC. CONN.		
0+00 = 0+48	AT TEE			
0+04			5.4 342.4 337.7	C47
0+49			5.7 342.1 337.7	C44
CBM			4.66 343.10 =	BP SW COR LINCOLN

MORENA BRIDGE
WATER LINE

⑥ STKS & GROSS Set for 16" WATER

10/3/52

13

Partly
Pavement
Alexander

BM	4.10	24.17	20.07		BP SW End of Old Morana Bridge (on sidewalk)
14+76 ⁶⁸	Top 24" RCP	9.72 - 11.32 21.06	12.45 03.11	12.83	on end of NE Wingwall - Nor. Abut. of over pass ($\Delta = 85^{\circ}14'$ LT - location by P. Fender)
14+66 ²	⑩ E	12.75	11.4	01.2	C10 ² = 10' Nly of existing 24" RCP pipe.
14+54 ²	⑩ SE	12.57	11.6	01.2	C10 ⁴ = 2' PT $\Delta = 34^{\circ}58'$ RT. (45° Bend)
14+54 ²	⑩ NE	12.59	11.6	01.2	
④	8.52	32.39	0.30	23.87	
14+14	E of Pipe at side	4.7	27.7	19.5	(C8 ²)
14+03	⑥ SW	4.77	27.6	24.5	C3 ¹ } - 2' PT $41^{\circ}28'$ LT (45° Bend)
14+03	⑥ W	4.78	27.6	24.5	C3 ¹ }
14+03	⑩ E	5.51	26.9	24.5	C7 ⁴
13+50	⑥ W	4.54	27.9	25.3	C2 ⁶
13+30	⑥ W	4.86	27.5	25.3	C2 ² = A PT $4^{\circ}38'$ LT
13+23.5	Protein 2' Hole in Sout	7.19	25.20	-25.5	
13+23.5	⑥ W	4.80	27.6	25.5	C2 ¹ } Face of S. Abut. of Bridge
④	3.88	30.86	5.41	26.98	
CK BM		8.43	22.43		BP on Wingwall NE Cor of bridge

NOTE: - This station should be
13+24.57
24.9650
MEAS 10. - 28.07
13+24.57

0.45508 prof.

MORENA BRIDGE
WATER LINE

10-6-52

12

⑥ STKS & GRDS SET FOR 16" WATER

BM	0.41	22.84	22.43			
2+965		0.5	22.3	19.2	BP NE Cor BRIDGE on Wingwall	1.87 Top 2' plane
2+83 EC		0.2	22.4	18.8	C30 FACE of Nor Abut	3.87 = 18.97
2+45		2.14	20.7	16.2	C36 ✓	19.2
2+1319 AC		3.2	19.4	15.0	C42	} Δ = 8°00' LT R = 500. T = 35.00 L = 69.81
2+00		3.9	18.9	15.0	C40	
+50		5.1	17.7	13.4	C39	
1+392 EC		5.2	17.4	13.1	C43	
1+00		6.6	16.2	11.8	C44	} Δ = 8°55' 50" R = 882 L = 13720
0+50		7.7	15.1	09.6	C55 ✓	
0+20		8.5	14.3	08.3	C60	
0+02	Begin WORK	8.9	13.9	08.3	C56 ✓	
CK P		6.94	15.90 = 15.85		Nail on Grd. Rail	
CK P		8.91	13.93 = 13.97		Run of Chamber - 14026	

BM	12.46	32.53	28.07			
13+295		4.06	28.47 = 28.44		Rdwy Deck of Bridge at curbline, Sely Cor/Bridge	
13+235		3.23	29.30		Top Cone Walk of Bridge	
13+275		5.78	26.75		Top 16" C.I.	Rdy Elev. 28.55
13+387		5.75	26.78	26.0	Top 16" C.I. Hi PT.	29.58
13+841		6.20	26.33	10 Top CHAM	Top 16" C.I. (at well)	
12+02		6.91	25.62		Top 16" C.I. (at well) beginning of 45° Bend down	

29.38
26.73
2.6

27° = 2.33

ORANGE AVE
 SPARTON DR TO 58TH PLACE
 (4) STKS & GRD for 12" WATER

10/6/52

15.

WEST
 MARTELL
 VARONFAKIS

B.M.	11.35	396.18		384.83		on curb (see F.B. 787 pp 24)
P	7.96	402.97	+1.7	395.01		
0+00			0.0	403.0	389.4	C136
+50			5.5	397.5	386.2	C113
1+00			12.7	390.3	382.8	C75
P	1.26	391.22	13.01	389.96		
+25			5.0	386.2	381.2	C50
1+28	12.16	TEE				
+50			6.5	384.7	380.4	C43
2+00			6.3	384.9	380.5	C44
+50			6.2	385.0	380.6	C44
3+00			6.3	384.9	380.7	C42
+25			6.1	385.1	380.1	C50
+50			8.3	382.9	378.0	C49
+75			13.1	378.1	372.0	C62
P	0.37	379.48	12.11	379.11		
4+00			7.7	371.8	366.0	C58
+25			12.9	366.6	360.2	C64
P	0.70	367.37	12.81	366.67		
+50			5.3	362.1	356.8	C53

ORANGE AVE
(Cont'd.)

10-6-52

16.

4+75	367.37	8.8	358.6	353.2	C54
5+00		83	359.1	353.6	C55
5+083		6.1	361.3	357.0	C43
5+183		3.2	364.2	359.3	C49
TP	12.28	379.02	0.63	366.74	
TP	10.68	388.94	0.76	378.26	
OK TP		4.08	384.86	= 384.83	

WREN ST.
 KLAUBER ST.
 SCIMITAR TO BROADWAY
 (A) STK'S & GRDS FOR 12" WATER

BM	1316	325.53		312.37			
15+78	END WORK		11.95	313.6	309.8	C38	
15+229	X PT	37°50' LT	⑤ 11.75	313.8	310.0	C38	
			11.70	313.8		C38	
15+00			10.85	314.7	310.6	C41	
14+75			9.9	315.6	311.4	C42	
14+50			8.1	317.4	313.2	C42	
14+00	X PT	TELL	4.9	321.2	316.7	C45	
13+50			10.90	335.81	320.2	C47	
			0.62	321.91	320.2	C47	
13+00			7.1	328.7	323.7	C50	
12+50			3.5	332.3	327.2	C51	
12+27.00	TEE		4.9	333.9	329.8	C41	
12+00			1.77	335.78	334.01		
12+00			1.7	332.1	329.8	C43	
11+50			0.65	323.98	319.4	C39	
11+25			5.9	318.1	314.2	C39	✓
11+00			0.62	315.09	309.6	C51	✓
10+75			3.76	311.33	304.9	C64	✓
10+50			8.8	306.3	300.3	300.7	C55
10+25			12.5	302.6	298.3	298.8	C38
10+00	B.O.		12.6	302.5	298.0	298.4	C41
9+75			9.8	305.3	299.2		C61
9+50			11.82	322.21	305.0		C54
9+00			4.70	310.39	305.0		

SEE ALIGNMENT
 REVISED
 Page 23

WREN. ST.

(Cont'd)

10-7-52

18.

		322.21					
9+00	13.07	325.23	0.05	322.16	316.8	C54	
8+75			6.6	328.6	322.5	C61	
8+50	12.05	346.31	0.97	334.26	327.1	C72	
8+00			2.4	343.9	336.2	C72	
7+62	11.79	358.10	0.00	346.31		C61	
			8.8	349.3	343.2	C61	
7+37			9.01	349.09	348.95	C55	1st P Prop Cor.
			6.3	351.8	346.3	C55	
7+00			4.0	354.1	348.4	C57	
6+50			1.3	356.8	349.7	C71	
6+00			0.9	357.2	351.0	C62	
5+50			1.9	356.2	351.5	C47	
5+28 ³³			3.4	354.7	351.7	C39	
5+27 ⁹⁸							
5+00	12.66	368.80	1.96	356.14	352.0	C41	
4+54 ⁰²			9.4	359.4	355.3	C41	
4+00			4.5	364.3	360.0	C43	
3+00	13.21	381.52	0.49	366.31			
+50			12.0	369.5	364.4	C51	
3+00			7.9	373.6	368.8	C48	
+50			3.5	378.0	374.0	C42	
2+00	12.84	393.43	0.93	380.59			

WREN ST.
(Cont'd.)

10-7-52

19.

4	2+00		393.43	8.6	384.8	379.3	C55
8	+50			4.05	389.4	384.5	C49
8	1+28 ³³ PK						
8	1+29 ¹⁹ AK	PRC		2.4	391.0	386.9	C12
4		13.08	405.88	0.63	392.80		
8	1+00			11.4	396.5	390.8	C37
7	0+71.6			6.5	399.4	395.2	C42
7	0+50	13.29	415.80	3.37	402.51	398.5	C22
7	0+13			5.7	410.1	406.2	C39
7	0+05	(0+11.4 Begin C1 - Corner Block)		3.8	412.0	409.0 410.6	C30
6	PD	756	417.15	6.21	409.59		= 1" WP prop Cor SE Cor Scimitar & Wren
6	CK TBM			0.43	416.72 = 416.69		Top F.H. S.E. Cor Scimitar & Wren

WAT. METS

5	5+48 (10'S)	② W	354.3	357.3	F30	354.7	369.5 19
5	5+30 (10'S)	② E ② W	359.3 353.3	357.9	F36	376.0	367.6
4	3+31 (16 ^S W / E St)	② S ② N	367.6 368.7	372.6	F50 F41	19	
4	2+21 (16 ^S E / E St)	② S ② N	384.1 384.4	385.0	F09 F06	376.1	384.8

ARCHER ST.
LA JOLLA MESA DRIVE, WESTERLY
(2) STKS & GRDS FOR WAT MET.

Oct. 9, 1952

BEATTY
POWELL
ALEXANDER

20

BM.	205 123	125.33 124.53	123.28	Top Conc. Mon SE Cor	La Jolla Mesa Dr & Archer
0+00 - W. Propline La Jolla Mesa Dr.					
0+23 Nor			0.03 125.3	123.9	C14
0+40 So			2.1 123.2	123.0	C02
0+79 Nor			0.4 124.9	122.7	C26
0+79 So			3.0 122.3	121.8	C05
1+21 So			4.2 121.1	120.6	C05
1+22 Nor			2.2 123.1	121.0	C21
1+69 Nor			4.1 121.2	119.7	C15 v
1+98 So			7.1 118.2	118.3	F02
2+17 Nor			5.7 119.6	118.2	C14
2+53 So			9.3 116.0	116.7	F02
2+88 Nor			7.4 117.9	116.2	C17
3+15 So			10.0 115.3	114.8	C05
3+31 Nor			8.4 116.9	114.9	C20
3+69 So			11.1 114.2	113.3	C09
3+80 Nor			9.9 115.4	113.4	C20
4+25 So			13.1 112.2	111.7	C03
4+30 Nor			11.6 113.7	112.0	C17
BM	5.09	128.37	123.28		
(3) F.H			5.25 123.12	123.08	C004

ARCHER. JT.

LA JOLLA MESA DR. EASTERLY

(2) STRS & GRDS FOR WAT. METS

10-9-52
10-10-52

21.

B.M.	13.21	136.69	123.28	Conc Mon SE Cor La Jolla Mesa Dr. & ARCHER
0400 - E. Propline La Jolla Mesa Dr.				
0446 So.		12.1	124.6	125.4 F08
0458 Nor.		9.4	127.3	126.3 C12
0480 So.		10.8	125.9	126.5 F06
1406 Nor.		7.3	129.4	127.8 C16
1457 Nor.		5.8	130.9	129.4 C15
2402 Nor.		4.7	132.0	130.7 C13
2468 Nor.		2.3	134.2	132.8 C16
3400 ^{So.} Nor.		3.8	132.9	133.3 132.8 F04
3447 Nor.		0.3	136.4	135.3 C11
3447 So.		2.3	134.4	134.8 F04
TP 3467 Nor.	13.11	149.22	0.58	136.11 12.3 136.9 136.0 C09
4479 So.		10.0	139.2	138.9 C03
5447 So.		8.0	141.2	141.1 C01
5471 Nor.		6.4	142.8	142.3 C05
6407 Nor.		5.4	143.8	143.5 C03
6413 So.		6.2	143.0	143.2 F02
6466 So.		4.3	144.9	144.9 C02
7402 Nor.		2.2	147.0	146.5 C05

ARCHER ST.
(Cont'd)

		149.22				
7+50 Nor			+0.1	149.3	148.0	c13
7+62 So	13.31	162.09	0.44	148.78	148.0	c08
8+29 Nor			12.4	149.7	150.6	FO9
9+00 So			8.5	153.6	153.0	c05
9+48 Nor			6.2	155.9	156.0	FO1
9+54 So			6.7	155.2	155.6	FO2
9+95 So			4.5	157.6	157.6	c02
10+18 Nor			0.9	161.2	160.7	c05
TD	6.03	167.24	0.88	161.21		
OK B.M			4.05	163.19 = 163.12		

Cont. Mon Archer & Cass

TP	5.42	169.61		164.19		
8+17 ⁰⁷ Nor	3-METS		W 2.47	167.15	} 164.3	c285 c280
			E 2.51	167.10		

5.79

1000
1000.5
1000.5
1000.0
1000.5
1000.5

7+50
3+62
c13
0⁹⁷

1.9
1.93
147
3+99
7+27 = 147.3
146.8
c05
So
11.26
c067

WREN ST. PIPELINE
 REVISED ALIGNMENT &
 (5) STKS & GRADES FOR 12" WOT

OCT. 14, 1952

23

BETTY
 POWELL
 ALEXANDER

BM.	13.27	325.64	312.37			
15+16 ³	EXISTING 12x8 Grass					
15+11 ³	END WORK		11.9	313.7	3098	C39
15+00			11.6	314.0	3099	C42
14+75			10.7	314.9	3100	C49 ✓
14+55	x PT 39°05'17"		10.2	315.2	310.7	C47
14+50			10.3	315.3	310.9	C44
14+00			6.9	318.7	314.5	C42
+50			3.1	322.5	318.1	C42 ✓
7	9.81	335.45	0.0	325.64		
13+00			9.2	326.3	322.0	C43
+50			5.45	330.0	325.9	C41
12+00			1.6	333.9	329.8	C41
11+99 ³	12" TEE				329.8	
10+94 ³	12" GV.					
CK 12+50			3.15	332.3	= 332.3	

Rev. GRD DITCH Excav.

310.2

310.2

314.2

310.9

310.9

314.6

318.1

14+75³ } GAS. MH. 25 V 25 18 LT & PIPE

12+77⁸ }

DENVER ST
 (2) STKS # GRDS SET FOR
 WATER METS

10-12-52

21

TP	3.39	56.56	53.17			
17+40 = So Propline In Gulf						
17+14 E		2.10	54.5	518	C27	
16+54 E.		3.3	53.3	510	C23	
16+26 W.		6.26	50.3	497	C06	
16+00 E.		4.66	51.9	498	C21	
15+52 E		5.76	50.8	486	C22	
15+52 W.		8.74	47.8	479	F01	
15+06 E		7.15	49.4	475	C19	
14+54 E		8.75	47.81	463	C16	
14+07 E	5.83	53.49	8.90	47.66	456	C21
11+89 W		7.7	45.8	430	C28	
11+31 W		9.0	44.5	425	C22	
11+18 E.		5.5	48.0	429	C51	
11+18 W	0.61	40.87	13.23	40.26		
7+80 W		4.0	36.9	375	F06	
7+17 W		4.17	36.7	36.1	C06	
7+00 W		4.77	36.6	35.7	C09	
6+41 W		6.1	34.8	34.5	C03	
5+88 W		7.07	33.8	33.2	C06	
5+44 W		7.44	33.4	32.2	C12	

↓ ord 11/10/52 = 2"

DENVER ST

WAT. METS

Cont'd.

40.87

4+05 E		8.2	32.7	31.1	C16	
4+01 W		9.9	31.0	30.7	C03	
3+78 E	4.12	36.97	8.02	32.85	31.2	C13
3+68 W		6.1	30.9	30.8	C01	
3+17 E		4.2	32.8	31.5	C13	
2+93 W		5.8	31.2	31.1	C01	
2+54 E		3.7	33.3	31.8	C15	
2+45 W		5.77	31.7	31.3	C04	
2+27 E		3.2	33.8	31.7	C19	
2+08 W		5.3	31.7	31.5	C02	
1+56 W		4.8	32.2	31.7	C05	
0+94 E		2.57	32.4	32.45	C20	
OK 1500 ©		2.9	32.07 =	31.0		

10-12-52

25.

CHICAGO ST
MILTON TO INGOLF
⑥ STKS & GRDS - 6" WATER

OCT. 14, 1952

26

TBM	0.91	52.08		53.17			
	1.04	43.84	11.28	42.80			
17+65	END WORK		1.04	42.80	30.0	C128	171.40
17+30	FH TEE		2.1	41.7	29.8	C119	15+96 1.44
	⑤ FH.		1.10	42.74	32.10	C862 C1214 1/2 ELL	
17+00			3.0	40.8	29.6	C112	✓
16+75			4.15	39.7	29.5	C102	✓
+50			5.5	38.3	29.0	C98	✓
16+00			8.3	35.5	28.1	C74	✓
+50			11.2	32.6	27.2	C54	✓
15+00			12.1	31.7	26.3	C54	✓
+50			12.86	30.91	25.4	C56	✓
④	3.13	32.11					22 5 17
14+00			2.0	30.1	24.5	C56	✓
13+90			2.1	30.0	24.4	C56	✓
+50	E Jellote		5.3	28.8	23.9	C49	
13+10			4.6	29.5	23.2	C61	*
13+00	FH TEE		4.5	29.6	23.3	C63	✓
	⑤ FH.		3.9	30.2	26.8	C34 C69	
12+50			4.2	29.9	27.5	C74	
12+00			6.1	28.0	21.7	C63	
11+50			6.8	27.3	20.9	C64	
11+00			8.3	25.8	20.1	C57	✓

Cont'd on pg. 29

ARCHER ST.

CASS TO DAWES & TO ELY TERMINUS
 (2) STRS & GRDS FOR WATER METS

Oct. 27, 1952

27

BEATTY
 POWELL
 ALEXANDER

TBM	1046	173.58	163.12	Gene. Man. S.W. Co. Archer & Cass
0+00 = Ely Prop line Cass				
0+39 So.	2.1	166.5	166.9	C02
0+77 Nor.	4.06	169.5	167.8	C17
0+88 So.	5.7	167.9	167.5	C04
1+17 Nor.	3.6	170.0	168.4	C16
1+31 So.	5.07	168.5	168.1	C04
1+74 Nor.	3.9	169.7	168.7	C10
2+03 So.	6.1	167.5	168.0	F05
2+09 Nor.	4.0	169.6	168.5	C11
2+65 So.	6.1	167.5	167.8	F02
2+81 Nor.	3.5	170.1	168.0	C21
3+33 So.	6.3	167.3	167.2	F01
3+91 So.	5.7	167.9	166.9	C10
4+29 So.	6.0	167.6	166.3	C13
4+72 Nor.	3.8	169.8	165.7	C41
4+75 So.	7.6	167.0	165.1	C21
5+05 Nor. (= 744 on So.)	5.1	168.5	164.7	C38
TD 11.75 178.00	7.33	166.25		
0+00 = Ely Prop line Dawes				
0+23 Nor.	10.3	167.7	165.2	C25

ARCHER ST.

(Contd.)

10-27-52 572.0
10-29-52 920.0

28.

178.00

0432 So		13.6	164.4	164.6	F02
0470 Nor		9.3	168.7	167.3	C14
0497 So		11.6	166.4	167.6	F12
1411 So		11.2	166.8	168.7	F19
1436 Nor		7.0	171.0	170.3	C07
1472 So		8.5	169.5	171.2	F17
2402 So		6.3	171.7	172.5	F08
2475 Nor		4.7	179.7	176.3	C34
TP	4.13	172.12	899	170.01	
CR TBM		10.01	164.13	=163.12	

Chicago St.
Cont'd from pg 26.

10-12-52

29

32.11

10+50		10.3	23.8	19.3	C45 ✓
10+00		11.4	22.7	18.5	C43 ✓
9+60		11.8	22.3	17.9	C44 ✓
9+10	8 KANE	12.1	22.0	17.4	C45 ✓
8+60		12.2	21.9	16.9	C50
8+50	FH Tee	12.43	21.68	16.9	C48
	⑤ FH	10.62	23.5	20.9	C25 C61
P	3.15 2483	17.43	21.68		
7+8+00		3.4	21.4	16.6	C48
7+50		3.3	21.5	16.3	C52
7+00		3.9	20.9	15.9	C50
6+50		4.4	20.4	15.5	C49
6+00		4.9	19.9	15.1	C48
5+50		4.6	20.2	14.7	C55
5+10		4.6	20.2	14.4	C58
4+70		4.5	20.3	14.4	C59
4+30		4.3	20.5	14.4	C61
4+20	FH Tee	4.2	20.6	14.5	C61
	⑤ FH	2.75	22.08	118.5	C36 C71

Chicago St
Cont'd

10-12-52

20

24.83

4+00			4.0	20.8	114.6	C62
3+50			4.2	20.6	114.9	C57
3+00			3.9	20.9	115.3	C56
2+50			4.1	20.7	115.6	C51
2+00			3.8	21.0	116.0	C50
P 1+50	7.18	28.79	3.22	21.61	116.3	C53
1+00			7.2	21.6	116.7	C49
0+90 F.H. Tee			7.0	21.8	116.9	C49
⑤ F.H.			5.93	22.86	120.4	C25 C60
0+80 Nor prep line Mutan			6.9	21.9	116.9	C50
+35 Begins Work			6.4	22.4	117.2	C52
P 8.33	37.10	0.02	28.77			
4 P			2.92	34.18	= 34.10	0+80 Denver
P 3.81	34.79		30.98			
12+85 W			6.7	28.1	26.6	C15
12+48 E			4.6	30.2	26.6	C30
12+38 W			6.6	28.2	25.8	C24
⑤ F.H. Tee			4.58	30.21	= 30.21	
P 1.56	44.70		42.74			
15+96 W			7.6	36.7	31.7	C50
17+12 E			2.9	41.4	34.3	C81
CK ⑥ 16+00			8.78	35.52	= 35.5	

AGATE JT

Cont'd

WAT. METS

137.50

2+74 Nor			12.3	125.2	124.5	CO ¹	
3+17 So			11.8	125.7	125.6	CO ¹	
3+33 Nor			9.8	127.7	126.7	C10	
3+96 Nor			7.6	129.9	128.9	C10	✓
4+21 Nor			7.3	130.2	129.7	CO ⁵	
4+87 Nor			5.4	132.1	132.0	CO ¹	
5+12 Nor			9.7	127.8	132.8	F50	
5+68 Nor			10.1	127.6	134.7	F73	} wow!
6+26 Nor			8.3	129.2	136.5	F73	
6+82 Nor			2.0	135.5	138.4	F29	✓
7+00 So			1.4	136.1	138.5	F24	✓ ✓
7+04 So			1.1	136.4	138.6	F22	
7+47 Nor	13.36	150.86	0.00	137.50		F14	
7+93 Nor			11.7	139.2	140.6	F14	
8+18 Nor			9.0	141.9	142.0	FO ¹	
8+18 Nor			8.0	142.9	142.9	CO ⁰	
8+71 So			6.3	144.6	144.1	CO ⁵	
8+75 Nor			5.6	145.3	144.8	CO ⁵	
9+53 Nor			2.6	145.3	147.4	CO ⁹	
9+56 So			3.1	147.8	146.9	CO ⁹	

AGATE ST
Cont'd

Wor. METS

150.86

10+33 So 0.9 150.0 149.5 C05

10+25 Nor 10.1 151.0 149.7 C13

P 6.83 156.75 0.92 149.92

OK BM 6.96 161.46 2.34 154.21 = 154.50

C+00 = Ely Pl. Cass.

0+74 Nor 4.55 156.9 155.0 C19

1+20 So 6.4 155.1 155.0 C04

1+21 Nor 2.74 156.7 155.5 C12

1+60 Nor 5.14 156.3 155.7 C06

1+87 So 6.5 155.0 155.2 F02

2+00 Nor 5.00 156.5 155.7 C08

2+06 So 6.6 154.9 155.2 F03

2+48 Nor 4.77 156.7 155.5 C08

2+75 So 6.9 154.6 154.9 F02

3+07 Nor 5.8 155.7 155.1 C06

P 3+55 Nor 3.93 158.26 7.13 154.33

3+59 So 2.60 155.70 154.4 C03

4+16 Nor 4.35 158.9 154.0 F01

4+56 So 3.94 154.3 153.3 C12

4+97 Nor 5.7 152.6 151.9 C07

P 4+97 Nor 5.85 152.4 151.3 C11

P 4.82 160.49 2.59 155.67

OK BM 5.98 154.51 = 154.50

BM 6.30 169.42 163.12 Conc Mon Archer & Cass

FH Cass Archer Flange 5.59 169.89 163.80 C02

BM 5.90 174.47 168.57 Conc Mon Cass & Van Noy

FH Cass - Van Noy's FLANGE 3.82 170.65 171.40 F05

TBM 6.17 139.33 133.16

Flange 6.83 132.50 135.2 F22

326 136.05

Conc Mon Agate & Cass

153.91 153.38 C053

0374
Flange
153.72
7.72

11-19-52
Same Party

CHICAGO ST

② GRDS & STKS FOR WAT. METS.

BK MET 24E RT #17 4 ST

B.M	3.52	25.13	21.61	② 1450	1930
0493 E			2.5 22.6	208	C18
1401 W			4.5 21.0	203	C07
1467 E			2.7 22.4	20.4	C20
1470 W			4.8 20.3	198	C05
1494 E			3.1 22.0	20.2	C18
1497 W			5.0 20.1	197	C04
2+46 W			5.3 19.8	193	C05
2+56 E			3.7 21.4	198	C16
2+96 E			2.8 21.3	194	C19
3+09 W			5.5 19.6	189	C07
3+38 E			2.1 21.0	192	C18
3+44 W			5.6 19.5	186	C09
4+08 W			5.5 19.6	18.2	C14
4+05 E			3.8 21.3	18.7	C26
5+33 E			3.8 21.3	18.6	C27
5+51 W			6.5 18.6	18.3	C03
5+73 W			6.2 18.9	18.4	C05
5+85 E			4.15 21.0	18.9	C2L

Nov 5 1952
B. BEATTY
D. WELLS
ALEXANDER

34

CHICAGO ST.

11-5-52

35

	25.13					
6+35 E.		4.4	20.7	19.3	C14	
6+46 W.		5.7	19.4	19.0	C04	
6+75 W.		5.4	19.7	19.7	C05	
6+83 E.		3.9	21.2	19.7	C15	
7+32 E.		3.2	21.9	20.0	C19	
7+47 W.		4.2	20.9	19.7	C12	
P 7+85 E.	701	29.52	2.62	22.51	20.3	C22
7+87 W.		8.6	20.9	20.0	C09	
8+32 W.		8.10	21.4	20.4	C10	
9+80 E.		5.7	23.8	22.3	C15	
10+27 E.		5.5	24.0	23.0	C10	
10+50 W.		6.1	23.4	22.8	C06	
10+75 W.		5.2	24.3	23.3	C10	
11+00 E.		3.5	26.0	24.2	C18	
11+35 E.		1.8	27.7	24.7	C30	
11+77 E.		0.4	29.1	25.3	C38	
11+83 W.		2.8	26.7	25.0	C12	
P	430	33.12	0.70	28.82		
		2.11	31.01	= 30.98		

9+67 W ? use C05 AR.

④ 14+50 pg. 26

ALLEY Block 51
 UNIVERSITY, 51y 110'
 BETWEEN 41ST & MARLBOROUGH

Nov. 24, 1952

DEATY
 POWELL
 ALEXANDER

30

(A) STKS & GRDS FOR 6" MAIN

W.O. #

BM	408	357.95	353.87			
0+00 = N.Y. P.L. UNIV.						
0+80	G.V.	5.05	352.90	349.6	C33	
+88	F.H. TEE	5.03	352.9	349.4	C35	110 12.40
1+00		5.07	352.88	349.1	C38	200
+45						.176
+50-		5.68	352.27	348.1	C42	264
						1100
+90		6.12	351.83	347.2	C46	.880
						110
						88
1+45 W		5.03	352.92	352.3	C06	
7+54 W.		5.75	352.20	352.1	C01	
1+67 E.		5.80	352.15	351.6	C06	
CK BM	408	353.87				

FRESNO ST.
RILEY ST. TO YUMA ST.
⑥ STKS & GRDS FOR 6" WATER

DEC. 1 1952

37

B.M.	13.19	100.81		87.62	
④	7.12	107.49	0.44	100.37	

Top PL pipe No. Cor { RILEY
EUREKA } FA BK 819 pg. 11

0+00 = Nly Prop line Riley

0+35	Begin Work		0.4	107.1	102.6	C45
------	------------	--	-----	-------	-------	-----

+50			3.2	104.1	100.1	C40
-----	--	--	-----	-------	-------	-----

1+00			10.5	97.0	91.7	C50
------	--	--	------	------	------	-----

④	0.00	92.28	13.21	92.28		
---	------	-------	-------	-------	--	--

+50			6.0	88.3	83.3	C50
-----	--	--	-----	------	------	-----

④	0.13	80.99	13.22	80.86		
---	------	-------	-------	-------	--	--

2+00			1.1	79.9	74.9	C50
------	--	--	-----	------	------	-----

+50			9.9	71.1	66.2	C46
-----	--	--	-----	------	------	-----

④	0.49	68.50	12.98	68.01		
---	------	-------	-------	-------	--	--

3+00			3.8	64.7	58.0	C67
------	--	--	-----	------	------	-----

+35			6.8	61.7	52.0	C97
-----	--	--	-----	------	------	-----

④	1.22	56.52	13.20	55.30		
---	------	-------	-------	-------	--	--

+65			3.5	53.0	48.9	C41
-----	--	--	-----	------	------	-----

3+75 (E GAINES)

+90			3.7	52.8	48.9	C32
-----	--	--	-----	------	------	-----

4+10	F.H. TEE		1.0	55.5	48.8	C67
------	----------	--	-----	------	------	-----

CK ④			2.47	53.05 =		
------	--	--	------	---------	--	--

+50			1.0	52.5	47.2	C53
-----	--	--	-----	------	------	-----

5+00			7.4	49.1	45.1	C40
------	--	--	-----	------	------	-----

+50			9.8	26.7	23.0	C37
-----	--	--	-----	------	------	-----

6+00			11.5	45.0	41.0	C40
------	--	--	------	------	------	-----

+25			12.4	42.1	40.0	C41
-----	--	--	------	------	------	-----

④	0.37	43.62	13.27	43.25		
---	------	-------	-------	-------	--	--

+50			0.7	42.9	35.0	C79
-----	--	--	-----	------	------	-----

GRADE CHANGE
TO 11 FEET
8" x 6" CROSS

⑤ F.H. 56.0
52.5 C35 C90

1041 1041 1041
820 1100 2050

FRESNO ST.

Cont'd

12-1-52

38

43.62

6+95 9.6 24.0 26.0 c8°

7+25 15.6 28.0 25.0 c3°

9) 13.27 56.52 0.37 43.25

CK P 3.47 53.05 =

← NAIL GAINES & FRESNO BK

WATER METS

BK MAT Box 25' from E ST

6+21 Wly -1.5 4+20 43.5 43.2 C03

5+70 Wly -1.6 5+50 45.1 45.3 F02

5+28 Wly +0.5 5+55 47.2 47.1 C01

4+77 Wly -2.0 4+50 50.5 49.7 C13

4+18 Ely 55.5 52.2 C33

4+07 Ely +2.8 4+10 56.3 52.7 C36

11.6

4

2+19 Ely } 7-WAT METS -1.7 78.2 76.5 C12

2+08 Ely } -0.3 2+00 79.6 78.5 C11

2+15 Wly -3.4 2+00 76.5 76.8 F03

1+08 Ely -0.8 (400) 96.2 96.0 C02

6.7

2.9

3.4

DEC. 1. 1952

39

BRIGHTON AVE
ABBOTT TO SPRAY

(4) STRS & GRDS FOR 6" A.C. WATER

B.M.	3.77	13.92	10.15	NW 1/4	ABBOTT & BRIGHTON	
0+00	EH. PL. ABBOTT					
0+21	Begin Work					
0+24	6" G.V.	3.85	10.07	06.6	C35	
4	0+58	4.20	09.72	06.1	C36	
CK	1+00	4.85	09.07	05.5	C36	
6	+50	5.55	08.27	04.8	C36	
5	2+00	6.26	07.66	04.1	C36	
5						
4	+50	6.95	07.0	03.5	C35	
4						
4	3+00	7.7	06.2	02.8	C34	
	+50	8.5	05.4	02.1	C33	
2						
2	4+00	9.22	04.7	01.5	C32	
	+07	EH. TEE	9.3	04.6	01.4	C32
	+50		9.9	04.0	00.8	C32
1	5+00		9.0	04.9	00.1	C48
	+53	END WORK	11.43	03.5	00.8	C42
CK	BM	3.77	10.15			

DEC. 9 1952

20.

LILLIAN ST

VIOLA TO GERTRUDE

④ STKS & GROS for 6" WATER

BM	11.85	72.23		60.38		on Conc Map SE COR Lillian & Gertrude
11D	12.98	72.19		59.21		on Sew M.H. BK 781 pg. 62
5+15	Begin Work					
5+10			12.12	60.05	55.6	044 ✓
5+00 = Jolly Pl Gertrude			11.1	61.1	56.5	046 ✓
+50			6.1	66.1	60.9	052 ✓
4+00			2.0	70.2	65.3	049 ✓
11D	12.83	82.32	0.68	71.51		
+50			10.1	72.2	69.8	044 ✓ ✓
3+00			6.15	78.19	73.5	047 ✓ ✓
+62			3.2	81.1	76.2	049 ✓
+50			2.5	81.8	76.2	056 ✓
2+00			2.9	81.4	76.3	051 ✓
+63			4.8	79.5	76.4	031 ✓
+50			5.5	78.8	75.6	032 ✓
1+00			9.1	75.2	72.4	030 ✓
+75			10.5	73.8	70.8	030 ✓
+30			10.3	74.0	70.8	032 ✓
CR 11D			9.38	74.96	74.91	SEW M.H. 0471 BK 781 pg. 62

Lillian St

WAT. METS

12-12-52

41

2+17 SWly

81.5

80.7

C08

2+25 NEly

84.4

81.7

C32

✓

3+38 SWly

75.8

72.8

C10

3+97 NEly

73.2

69.9

C33

✓

4+29 SWly

68.8

66.4

C24

4+52 NEly

66.8

64.9

C19

✓

HUXLEY AVE

WATER STUBS ACROSS STREET
AT CHICAGO, DENVER, FRANKFORT
ALSO GALVESTON & CLAIRMONT

12-9-52

42.

Beatty
Powell
Alexander
Kemp

BM	5.45	47.21	41.81			23.81	Nail in Root
0+00	FACE CURB SOUTH	4.7	42.6	43.4	38.9	curb Bottom	c37
0+35	& HUXLEY	4.00	43.3	38.9	c24		
0+70	FACE CURB NORTH	3.85	43.4	43.4	38.9	c15	10' Eastly Chicago
		9.80				(2) c25	4+00'
IP	13.24	59.94	0.56	46.70			
	13.23	72.53	0.64	59.30			
0+00	= 55' 50" & Huxley	10.25	62.3	59.8	55.3	c70	
+20	= 35' " " "	11.3	61.2	60.6	56.1	c51	
+55	& Huxley	10.73	61.8	60.7	56.2	c56	10' Easterly Denver
+90	35' Nor & Huxley	11.4	61.1	60.8	56.3	c48	
1+10	55' " " "	3.2	69.3	61.6	57.1	c122	
IP		0.43	72.10				
IP							
IP	10.50	119.53		109.03			
0+00	= Face Curb So	(2) 5.0	114.5	115.1		c39	
		& 5.85	113.68	110.6			
0+35.5	& Huxley	(2) 6.8	112.7	108.75		c39	10' Easterly & Frankfort
		7.70	111.83				
0+70	= Face Curb Nor	(2) 7.7	111.8	106.9		c29	
		8.15	111.38				
			(Top of curb)				

CLAIREMONT DRIVE

④ STKS & GRDS. for 8" WATER
Galveston & Clairemont Ct.
& GESNER

12-10-52

43

BM	0.19	176.67		176.48
D	1.23	164.99	12.91	163.76
0+00	PLUG		70.7	154.3 149.8
+50			9.8	155.2
1+00			8.3	156.7
+25	PT (50°23'26" RT)		7.3	157.7 153.2
1+25		(165.89 NEW H.)	9.1	156.8 153.2
1+55	PLUG		4.7	160.3
1+80			6.4	159.5 155.7
11	11.93	176.88	0.05	164.95
CK. BM		0.20		176.28

NAIL IN POLE @ Clairemont, E of GALVESTON

	176.29 BM
	174.21
	172.69
	171.16 D
C45	148.6
	133
	165.89 W
	165.88
C45	150.9
	11.38
	177.26
	0.80
C45	150.2
	178.46

10' EASTERLY GALVESTON

THIS IS OUT NOW & IS ALL
10' ELY E GALVESTON
10' SOUTHERLY CLAIREMONT
DRIVE

BM	2.51	202.8		200.30
0+00	AT TEE		7.10	195.7 191.2
0+60			9.50	193.3 188.8
CK. BM		2.51		200.30
BM	9.85	186.33		176.48
1+20			6.8	181.5
0+70			2.6	183.7
+45	12x6 TEE		2.0	184.3 180.6
0+00			+0.3	186.6 182.1
0+00 = (0+45 12")				
0+05			2.0	184.3 180.6
0+35			3.4	182.9 179.4

BR NELY Clairemont Ct.
Clairemont Dr

C45

C45

45 So E Clairemont
DRIVE
W. of Intersection of
Clairemont Ct.

NAIL IN POLE Clairemont, E of Clairemont

C36

C37

C37

C45

12" WAT 10' SWLY E GESNER

C37

C35

6" WAT STUB OFF 12" WAT.

MISSOURI ST
LAMONT TO JEWELL
② STRS & GRDS FOR
WATER METERS

Dec 11, 1952

44

BEATTY
POWELL
ALEXANDER
KEMP

BM	0.80	124.21	9.8	123.41
①	0.26	131.44	13.03	131.18
②	6.19	124.64	12.99	118.45
CKIP			8.23	116.21

7 LET LAM & LAMONT

LET SE Cor LAMONT & MISSOURI

0+00 = W. PL LAMONT

1+30 So			5.8	118.8	118.4	C04	118.8
1+13 Nor			3.7	120.9	119.6	C13	120.0
1+52 So			5.4	119.2	118.6	C06	119.1
1+80 So			5.3	119.3	118.8	C05	119.3
1+84 Nor			3.3	121.3	119.8	C15	120.3
2+41 Nor			3.0	121.6	119.8	C18	120.3
2+51 So			5.2	119.4	118.7	C07	119.2
3+18 So			5.4	119.2	118.4	C08	118.9
3+24 Nor			3.8	120.8	119.2	C12	119.8
3+54 So			6.0	118.6	118.0	C06	118.5
3+74 So 2 METS			6.0	118.6	117.7	C09	118.2
3+85 So			6.2	118.4	117.5	C09	118.0
3+88 Nor			4.2	120.4	118.4	C20	118.9
4+17 So			6.8	117.8	117.0	C08	117.5
4+45 Nor			5.8	118.8	117.3	C15	117.7
4+73 So			8.5	116.1	115.5	C06	115.9

CHECKED PROFILE
FROM GRAVE 1593
5/11/50
BEATTY

Missouri ST

Wat. MET. 5

Cont'd

12-11-52

45

4+95 Nor	12.64	6.9	117.7	115.9	C18	116.3
5+015 So		9.4	115.2	114.6	C06	115.1
5+29 So		9.9	114.7	113.8	C09	112.3
5+99 Nor 010	114.63	10.31	112.33	112.7	C16	113.2
6+26 So		2.1	112.3	110.6	C17	111.2
6+76 Nor		2.8	111.6	110.1	C15	110.6
6+86 So		4.2	110.2	108.7	C15	109.2
7+12 Nor		4.5	109.9	108.0	C19	109.4 ?
7+50 So	2-METS	6.5	107.9	106.8	C1	107.0
7+75 Nor		7.4	107.0	107.1	F01	107.3
8+05 So		8.6	105.8	105.3	C05	105.5
8+24 Nor		9.4	116.0	105.9	C01	105.9
8+58 So		9.5	104.9	104.4	C05	104.3
8+82 Nor		8.9	105.5	104.8	C07	104.8
9+01 Nor		8.8	105.6	104.6	C10	104.6
9+05 Nor So		10.5	103.9	103.5 104.5	C04	103.5
9+55 So		11.1	103.3	102.8	C05	102.8
9+78 Nor		10.0	104.4	103.5	C1	103.6
10+05 So		11.6	102.8	102.2	C06	102.2

MISSOURI ST.

Cont'd

12-12-52

46

114.63

10+26 Nor

10.9

103.5

102.9

006

102.8

10+39 So.

12.2

102.2

101.7

005

101.6

④ 12.30

116.24

10.49

103.91

Top FH. JEWELL & Missouri

OK DM

2.69

113.55

= 113.28

pp. NE Cor Chalcedony & Jewell

①

0.00

103.94

103.94

113.28

Nor
NE Cor Diamond & Jewell

9.4

94.5

94.0

005

E
NE Cor

" " "

9.7

94.2

93.9

003

NOR
NW Cor

" " "

10.2

93.5

93.0

005

55TH ST.MONTEZUMA - Northw. City
⑥ STKS. & GRDS. FOR 8" CI. WATER

DEC. 15, 1952

BRATTY
POWELL

47.

BM.	3.84	454.78	450.94		2" LP 10' N of Montezuma, d. 55 TH (CITY ENGR. FB. # 2189) Pg. 10.	
0+00	Nly Prop Line Montezuma					
0+55		3.2	451.6	447.1	C45	
1+00	Nly Prop Line Montezuma					
		3.0	451.8	447.1	C47	
+50		2.2	452.6	447.8	C48	
2+00		1.8	453.0	448.6	C44	
+50		1.5	453.3	449.3	C42	
3+00		2.6	457.3	447.9	C44	
+50		3.7	451.1	446.6	C45	
4+00		5.2	449.6	445.3	C43	
+26	8" 6" TEE					
		6.07	448.7	444.6	C45	
+50		6.8	448.0	443.9	C41	
5+00		8.17	446.6	442.6	C42	
+50		9.45	445.3	441.2	C41	
6+00		11.07	443.7	439.9	C38	
+50	2.45	444.62	12.61	442.17	438.5	C32
7+00				437.2		
+02	8" 6" TEE					
		3.9	440.7	437.1	C36	
+50		4.9	439.7	435.7	C37 C42	
				436.0		

0+29 C42 { End of
6" WAT at
Existing 6" 6"
29° RT
4+26

0+29? C42 { End of
6" WAT
at Existing
6" G.V.
29° RT
STA 7+02

55TH ST.

(Cont'd.)

12-15-52

48.

444.62

+70

8x6" FH TEE

5.1

439.5

435.0

~~435.9~~

C

C45

12-16-52
GRADE CHANGE 7+00 - 9+21⁷⁵ due to
conflicting. # of 18" RCP Cross Drain = 436.20
at 7+67E

8+00

5.1

439.5

435.0

~~435.7~~

C98

C45

+50

5.3

439.3

435.0

~~435.4~~

C99

C43

9+00

5.5

439.1

435.0

~~435.1~~

C40

C41

+21³⁵

5.5

439.1

435.0

~~435.0~~

C41

C41

ck TP

4.53

chis d. on NE curb RET 55TH & Hardy

TP

13.17

456.91

0.89

443.74

ck BM.

5.95

450.96 = 450.96

PACIFIC BEACH DRIVE
 MORRELL TO LAMONT
 (A) STKS & GRDS FOR 6" WATER

Dec. 16, 1952
 Best
 Powell
 Alexander

29

BM	1.06	36.34	35.07 (on SW.?) 35.28	NE 7' CT	LAMONT Pac Beach Dr
8+000 = Fly Prop line, Morrell					
0+25 Begin Work		17.2	23.1	19.3	C38
0+75		11.2	25.1	20.8	C37
1+00		10.1	26.2	21.9	C43
+50		7.9	28.4	22.1	C43
2+00		6.3	30.0	26.3	C37
+50		5.4	30.9	27.4	C35
3+00		4.5	31.8	27.9	C39
+95 6" TEE		4.4	31.9	28.0	C39
+50		4.15	32.2	28.3	C39
4+00		3.6	32.7	28.8	C39
+50		3.7	32.6	29.5	C33
5+00		3.7	32.6	29.8	C38 C30
+25		3.5	32.8	30.0	C38 C30
+75		2.5	33.8	32.8	C30
6+05 End Work		2.35	34.0	30.9	C32
CK BM	1.06	35.28			

GRADE

NOTE
 NAT Ground at
 E of PIPE 15
 the same as (A)

PAC. BEACH DRIVE
CONT'D
WATER MET. 3
36-34

1+42 So	8.1	28.2	27.5	007
1+56 Nor	7.8	28.5	27.8	007
1+88 So	6.4	29.9	29.2	007
2+21 Nor	4.7	31.6	30.3	013
2+44 Nor	4.4	31.9	30.8	012
3+28 Nor	2.9	33.2	32.3	012
4+00 Nor	2.1	34.2	33.1	012
4+25 Nor	2.2	34.1	33.6	005
4+54 So	3.5	32.8	32.9	F0L
4+79 So	4.0	32.3	32.2	F09
5+15 Nor	2.1	34.2	32.4	F02

12-17-52

50

PK of MET ²²⁵
~~RT & LT & ST~~

5.85

4.9

1.5

GALVESTON ST

HARTFORD ST

AT MILTON ST

⑤ STRS & GRDS for 6" WATER

Dec. 18, 1952

51

BM	12.80	54.83		42.03			BR SW Cor Fore & Milton
IP	13.14	67.86	0.11	54.72			
IP	13.25	81.07	0.04	67.82			
0+00	⑤	2 Wat on Milton	4.41	76.7	75.0 70.5	C62	} GALVESTON ST. (Nly)
0+50	⑤	Nly Prop line Milton	5.30	75.8	70.5	C43	
IP	13.35	94.39	0.03 -1.39	81.04			
IP	13.13	107.12	0.20	93.99			
IP	13.16	120.06	0.22	106.90			
IP	13.10	133.01	0.15	119.91			
0+865		Nly Prop Milton	7.4	125.6	124.2 119.7	C59	} HARTFORD ST. (Nly)
0+365		2 WAT on Milton	7.4	125.9	125.0 120.5	C54	
CK BM	10.19	127.78	5.42	127.59	127.56		
0+365		2 WAT on MILTON	4.0	133.8	133.0 128.5	C53	} HARTFORD ST. (Sly)
0+00		EC CURB RET So	0.8	137.0	132.5 128.0	C90	
CK BM			10.19	127.59 = 127.56			NAIL IN Pole SW Cor Hartford & Milton

MILTON JH
WATER METERS STAKED

1-20-53

52

BM 10.13 52.16 42.03 80 SW Cor Erie & Milton

56' W. of W Prop. line ERIE
Nor. side Milton 13.06 39.10 38.9 0.02

236' E. of E Prop. line ERIE
Nor. side of Milton 1.58 50.6 50.8 E02

P 8.65 60.08 0.73 51.43

30' E. of E Prop. Line Frankfurt
Nor. side Milton 4.90 55.18 54.0 C08

P 13.33 73.19 0.22 59.86

P 8.41 80.92 0.68 72.51

4.16

12' E. of E Prop. line Galveston
Nor. side Milton 2.16 78.76 78.9 E01

P 2.23 82.74 0.41 80.51

CR BM #3 0.26 82.48 = 82.46

BM 4.40 131.96 127.56

PL. BC. of W. of W Prop. line Hartford
So. side Milton 6.20 125.8 125.2 C06

2' East of BC W of W P.L. Hartford
So. side Milton 5.65 126.31 125.3 C12

BM 4.00 131.56 127.56

10' E. of Ely Prop. line Hartford
Nor. side of Milton (175 from
Nor. prop. line) 1.75 129.80 128.4 C14

WAT MET at 52' E. of Ely prop. line
of Milton

& Milton @ post = 11.12

+ 4.6

15.72

Curb Grid 13.4

C2.3

(1-29-30)

OAKCREST DRIVE
UNIVERSITY TO POLK
⑥ SIKS & GRDS. SET FOR 6" WAT.

DEC. 17, 1952
23,

53

BM	0.70	330.85		330.15			
71)	8.26	325.83	13.28	317.57			
0+63 AT GV		Top Post	14.9	310.9	307.0		
0+69			9.6	316.2	307.4		
1+00 B.C.			7.1	318.7	311.2		
1+22			4.65	321.2	313.5		
1+27 F.H. TEE			4.15	321.7	312.0		
1+50	13.25	338.91	0.17	325.66	312.0		
			14.0	324.9	317.9		
1+65.48 B.C. PRC			10.7	328.2	317.7		
					319.8		
1+75			8.1	330.8	318.6		
					320.8		
2+00			5.7	333.2	321.1		
					323.0		
+25			4.4	334.5	325.4		
+33 F.H. TEE				335.0	323.5		
+50			2.6	336.3	324.3		
					325.5		
					327.0		
+75			1.5	337.4	328.4		
RP	11.87	350.67	0.11	338.80	331.1		
3+00			11.4	339.3	330.8		
					333.0		
+20.9 F.C.			10.6	340.1	332.1		
					334.6		
+50			9.85	340.8	333.9		
					336.0		
4+00			8.7	342.0	337.0		
					337.6		
+50			7.7	343.0	338.0		
					338.5		
5+00			6.9	343.8	339.0		
					339.2		
+50			6.4	344.3	340.0		

SW BR 50TH & UNIV

DITCH
NAT GROUND

NOTE:
GRADE REVISION
0+63 & 5+50
DUE TO ERROR
IN ESTAB. GRID
AS SHOWN ON
PLANS.

NOTE: -
F.H. Reloc
eted due
to proposed
re-alignment
of UNIVERSITY
of 70'
105' W. of
approx STA
1+63 & ELEV
of 328.0

Remaining
& Ditch
Same as Orig Prelim. Survey

⑤ F.H. 304.4
331.9 curb
225 To Flange 70
To Station
E.L.

OAKCREST DR

(Cont'd)

12-23-52

54

350.67

6+00		5.95	344.7	340.4	CA3	
+50		5.6	345.1	340.8	CA3	
7+00		5.4	345.3	341.2	CA4	
+50		4.9	345.8	341.6	CA2	
+61	6" G.V.	4.8	345.9	341.7	CA2	
+66	F.H.	4.8	345.9	341.8	CA1	
					③ 346.3 CO2 345.5 CA3	
8+00		4.5	346.2	342.0	CA2	
+10	6" TEE	4.3	346.4	342.1	CA3	
+50		3.7	347.0	342.4	CA6	
9+00		3.25	347.4	342.8	CA6	
+50		2.9	347.8	343.2	CA6	
10+00		2.7	348.0	343.6	CA4	
10+16 ⁷²	B.C.	2.55	348.1	343.7	CA4	
+25		2.55	348.1	343.8	CA3	
④ +50	3.56	351.76	2.47	348.2	344.0	CA2
+75	$\Delta = 75^{\circ} 40' L$ $R = 237.7$ $L = 104.78$	3.3	348.5	343.9	CA6	
11+00		3.2	348.6	343.8	CA8	
11+21 ⁵⁰	FC E x RT	④	3.2	348.6	343.7	CA9
	27° 55' LT	⑤	3.6	348.2		CA5
+50		3.5	348.3	343.6	CA7	

NOTE: -

F.H. Relocated, as plan
Sta. 13 approx correct as
to prop. line, but centers
two adjoining drive ways.

OAKCREST DRIVE
(Cont'd.)

12-23-52

55

	351.76				
12+00		3.2	348.6	343.4	C52
12+49.2 = EN Prop line WINONA ST. +50		5.4	346.4	343.1	C33 ✓
12+60 End of Work		5.9	345.9	343.0	C29
IP 0.73	339.19	13.30	338.46		
IP 6.80	337.04	8.95	330.24		
CK BM		6.89	330.15 = 330.15		

WATER METERS

2+58 Fly	-0.8	336.6	332.2	C24
2+61 Wly	+06	338.0	332.3	C57
3+15 Fly	+01	340.2	338.5	C12
3+14 Wly	+03	340.4	338.1	C23
3+41 Fly	.00	340.8	340.0	C08
4+04 Fly	+09	342.9	341.5	C14
4+04 Wly	+09	342.9	341.7	C12
4+30 Fly	+06	343.4	342.0	C14
4+84 Wly	+05	344.3	343.4	C09
5+00 Fly	+05	344.3	343.9	C12
5+37 Fly	-01 +5-	344.2	343.7	C05

BRK of MET = 2.05 RT. & LT
± ST

OAK CREST DR
(CONT'D.)

12-29-52

56

5+80 Fly	+02	344.9	344.0	C09
6+37 Fly	+08	345.5	344.4	C12
6+92 Fly	+04	345.7	345.0	C07
7+61 Fly	+06	346.4	345.4	C10
8+12 Fly	+03	346.7	345.8	C09
8+36 Fly	-01	346.9	346.0	C09
8+81 Fly	00	347.4	346.4	C10
8+87 Wly	00	347.4	347.0	C04
9+57 Fly	+03	348.1	346.8	C13
9+39 W	+03	348.3	347.3	C10
9+92 Wly	+02	348.2	347.8	C04
10+04 Fly	+03	348.3	347.3	C10
10+18 Fly			347.5	
10+26 Fly	-02	347.9	347.6	C03
10+83 Fly	00	348.5	347.8	C07
11+79 Fly	+02	348.8	347.3	C15
12+63 Fly	-01	348.5	346.9	C17

17° S. E. ST

CAPE MAY AVE
 ABBOTT - WLY Δ 50'
 (4) 5TK & GRDS FOR 6" WATER

DEC 24 1952

57

BM	4.79	13.68	8.89		
0+00	Ely PL Abbott St				
0+60	Existing GV	5.4	08.3	2.80	c35
1+00		6.0	07.7	4.40	c33
+50		6.35	07.3	04.0	c33
2+00		6.75	06.9	03.5	c34
+50		7.2	06.5	03.0	c35
3+00		7.8	05.9	02.5	c34
+50		8.3	05.4	02.0	c34
4+00		8.5	05.2	01.5	c37
+50	2" 9.0	11.7	02.0	01.0	c10
CK BM	4.79	08.89			

BP NW Cor ABBOT & CAPE MAY

NOTE:

LOCATION OF MAIN
 REVISED FROM PLAN
 LOCATION OF 10' NLY & ST
 TO 10' SLY & ST

Holyoke St.
(Cont'd)

12-26-52

59

7+50		5.20	C10		
8+00		5.20	C10		
+22	F.H. TEE	5.20	C10		
	⑤ F.H.	4.50	C01	C 36	
+36	6" TEE	5.15	C40		
	END WORK				
		4.38			
				24+00 SICK CO ⁹¹	Frontier BLVD
				-0+01	5.00
0-04	2" WAT	5.4	C40	+40	4.75
0+60		4.75	C38	+925	44
0+825		44	C38		

CYPRESS AVE
 ALBERT ST. - W/ly
 ④ STRS. & GRDS. for 4" WATER

DEC. 26, 1952

BETTY
 WILLIAMS
 KEMP
 ALEXANDER

W/O # 24325
 FILE # 5780-W

BM	3.79	284.10		280.31		BP NE Cor Cypress & Albert
0+00	= Ely Pl Albert					
0+20	Existing Tee?	4.2	279.9	273.5		C64 ?
0+24	4" GV. Basin Noor	4.35	279.7	273.0		C63
0+52		5.4	278.7	272.0		C62
HP	3.39	274.45	13.04	271.06		
0+65		2.45	272.00	265.4		C66
				262.4		C65 Excessive Cut
HP	1.04	262.99	12.50	261.95		
0+89		4.7	258.3	251.0		C63
1+00		10.15	252.8	248.7		C61
HP	1.17	251.76	12.40	250.59		
+50		7.35	244.4	238.0		C60
	1.50	240.87	12.39	239.37		
+88		5.4	235.5	230.0		C55
2+00		7.2	233.7	230.0		C37
2+45	B.O. End Work	7.7	233.7	230.0		C32
HP	12.46	252.94	0.39	240.48		
HP	12.81	265.47	0.28	252.66		
HP	12.37	277.15	0.69	264.78		
HP	12.61	289.28	0.48	276.67		
HP	2.42	288.62	3.08	286.20		
ck BM.			8.31	280.31 = 280.31		

MOORE ST.
AMPUDIA TO CONDE
⑥ STKS & GRDS. SET FOR 6" WATER.

DEC. 30 1952
BRITTY
WILLIAMS
KEND
ALEXANDER

61

BM.	1.49	32.92	31.45				
			3.88	29.06	-29.07 RT	Top FH SE Co Ampudia Place	FB 810 pg 42
			4.87	28.07	-28.06 L	Top curb } FB 1580-64 (Sally PL Smoodie)	Top curb }
0+00	= Ely PL Ampudia						
0+16	EXIST 6" CI. WAT.						
0+20	Begin Work		4.26	28.7	23.9	048	7
0+25	6" SEW INV.		± 8.60	24.3	23.8		
0+50			4.1	28.8	-24.0	050	
1+00			4.8	28.1	23.7	044	
+50			4.85	28.1	23.4	047	
2+00			5.05	27.9	23.1	048	
+50			5.2	27.7	22.8	049	
3+00			5.25	27.7	22.5	052	
+50	Ely prop line Arista		5.0	27.9	22.3	050	6" Cross added As per instructions from Huntington
+65	6" Cross			26.9	22.0	049	
4+00	Wly prop line Arista		5.65	27.3	21.4	059	
+50			8.05	24.9	18.7	062	
④ 5+00	0.83	21.06	12.71	20.23	13.9	063	
+50			4.55	16.5	09.1	074	
④ 6+00	0.97	10.06	11.97	09.09	04.3	048	
6+25			4.6	05.5	+01.8	037	
6+75			6.8	03.3	-01.0	043	
6+90	FH. TEE		7.05	03.0	-01.2	042	(FH = 165 N & ST) ② 03.0 02.6 GRD 004 042
7+15	End Work		7.35	02.7	-01.6	043	
OK ④ 7+00			6.73	03.33	= 03.31		Nail in Po Pole E Moore Nwly PL Conde FB 810 pg 43

MOORE ST
Cont'd

JAN 6 1952

62

0400	Ely prop line Ampudis.				
1+03	Sully		28.1	27.6	C05
1+18	NEly ? (No MET STR'd)				
1+60	SWly		28.2	27.1	C12
1+72	NEly	00	28.1	27.5	C06
2+26	NEly	+0.2	27.9	27.2	C07
2+38	SWly	+0.4	28.1	26.6	C15
2+74	SWly	+0.1	27.8	26.4	C14
3+37	SWly	+0.5	28.4	26.1	C23
3+97	NEly (No MET STR'd) put in later				
4+05	NEly	+0.2	27.1	25.3	C18
4+41	SWly ✓	-0.3	24.6	23.0	C16
4+43	SWly Missed this - the first time				
4+71	NEly	-0.0	22.9	21.2	C17
5+27	NEly	+2.4	18.9	16.1	C28
5+30	SWly	+0.6	16.9	15.0	C19
5+63	SWly	5.50 -2.5	14.0	11.7	C33
5+68	NEly	-0.9	15.6	12.2	C34
5+94	SWly	+0.7	09.8	08.8	C10
6+12	NEly	+1.0	07.5	07.4	C01
6+22	SWly	+1.5 +0.7	06.2	05.7	C05

JEFFERSON
(Cont'd.)

12-31-52

64

29.83

5+50 47 25.1 21.3 038

6+00 40 25.8 21.9 039

+50 39.5 25.9 21.9 040

+80 40.5 25.8 21.9 039

7+15 AT GV. 45.5 25.9 21.6 037

7+25 G JEWEL ^{7/2} 11.3 18.5
pipe

7+50 47 25.1 21.0 041

11 0.11 16.84 13.10 16.73

CK 11 13.52 03.32 = 03.31 NAIL IN POLE MOORE & CANDE

JEFFERSON ST
Cont'd
WATER METERS

2-6-52

65

0+00 = Ely prop line Arista

0+66 Sly -2.8 19.2 19.3

2+10 Sly -2.2 08.2 08.7

4+20 Sly +1.3 21.0 20.9 COL 7 other

4+48 Nly (curb in)

4+87 Nly (curb in)

5+18 Nly (curb in)

5+20 Sly 24.2 20.6 FO²

5+78 Nly (curb in)

6+01 Sly (curb in)

6+62 Sly (curb in)

TALBOT ST.

BANGOR TO AKRON

④ STKS & GRDS FOR 6" & 8" WATER

DEC. 31 1952

Beatty
Williams
Kemp
Alexander

66

P	12.62	158.27		145.65	
P	11.05	164.78	4.54	153.73	
	1 1/4 BEND TO RT.				
0+00	3rd WLY SEC COR BANGOR TALBOT, & MARTINEZ		0.25	164.5	155.5
+05	E.H. TREE		0.75	164.0	155.1
+22	1 1/4 BEND TO RT.		2.6	162.2	153.6
+50			5.7	159.1	149.0
1+00			10.95	153.8	145.7
H	2.45	152.35	12.88	151.90	
+80			5.3	149.1	142.2
2+00			9.6	144.8	139.0
P	0.81	146.46	8.69	145.66 = 145.65	
+50			6.0	140.5	135.9
+80	8x6 TREE		8.45	138.0	134.0
3+00	Fly prop line BANGOR ST		9.9	136.6	132.7
P	0.47	132.15	12.78	133.68	
+50			0.85	133.2	129.6
4+00			4.20	130.0	126.4
+50			7.35	126.8	123.3
5+00			10.05	122.1	120.1
P	0.24	121.49	12.90	121.25	
+50					

1 1/2" ID 954 of Bangor & TALBOT FB 810 pg 52-55

(Top
Existing 8" CI. 1592)NOTE: - E. of PIPE {0+22 to
3+05
started at 21± Nor
of Sly prop line of TALBOT
which makes it 5'50± ST.Elev. d of pipe Ground line
is 50'± as @ Elev.

11.70 = NWly cor

TALBOT ST
(Cont'd.)

1-2-53

67

121.29

5+50		0.2	121.3	117.0	C43	
6+00		3.2	118.3	113.8	C45	
+50		6.0	115.5	110.7	C48	
7+00		9.0	112.5	107.5	C50	
① +50	4.21	113.44	12.26	109.23	104.4	C48
8+00		7.15	106.29	101.2	C51	
+05	6" CROSS	8.0	105.4	101.1	C43	
+25		7.35	106.09	100.8	C53	
+40	END WORK	7.2	106.2	100.8	C54	
① 8+69	12"-14" Spruce Tree on E of pipe	(See below)	8.50	104.9d = 105.02	SW GR SW 70' + Fly 8+40	
8+75	End of Work End of Existing 6" WAT from Nor	6.3	107.1	103.8 103.2	Top 6" C.I. Exist WATER Bottom 6" C.I. " "	

④ W 8+05 FH ② E		109.3 108.7	104.8	C45 } To Flange C39 } " " " "	C80 } To Bottom of EUL. C75 } " " " "	STAKED 8' 50. E of PIPE
② W. 0+22 FH ② E		163.7 162.5	159.8	C39 } 27 } " " " "	C97 } C85 } " " " "	STAKED 125' E 25' South & ST.

Talbot St

Cont'd.

WAT. METS.

1-14-53

68

PK of MET Strid at 68' Nly of Talbot

8+12 = Ely propline Akron

7+29 Nly.

6+78 Nly.

5+95 Nly.

5+57 Nly.

5+19 Nly.

4+14 Nly.

0+03 Nly

163.4

161.4

c20

(3428 Talbot)

0+55 Nly ?

160.2

154.5

c59

vacant lot no met front or back

1+74 Nly = wly propline
2-METS
Bangor (Nly)

149.1

146.0

c31

1010 Bangor

1+75 Nly

148.1

146.0

c21

1018 Bangor

2+58 Nly

c0°

3374 Talbot

3+28 Nly

c0°

3370 Talbot

3+90 Nly

c0°

3368 Talbot

4+15 Nly

c0°

3366 Talbot

3+00 Sly

143.8

137.0

c68

3365 Talbot

BANGOR ST.
 HARBOR VIEW DR. TO TALBOT ST
 (4) JK'S & GRDS FOR 8" WATER

Jan. 8, 1953

69

Boyd
 Williams
 Kerin
 Alexander

BM	0.17	257.58		257.41		Top FH. 55'ly Cor Harbor View Dr & Bangor St
0+00 =	A. Point 5' Nor of NW Corner Harbor View Dr. Edge Conc. Pavt.			249.2		
0+04.9			5.4	252.2	248.8	C34
0+50			9.8	247.8	244.4	C34
IP	0.53	244.95	13.16	244.42		
1+00			0.85	244.10	244.6	C45
+50			3.6	241.2	242.8	C66
IP	1.00	239.20	12.75	232.20	228.0	
2+00			2.7	230.5	230.0	C25
IP	0.83	221.40	12.63	220.57		
2+25			7.4	214.0	210.5 216.0	C35
IP	0.30	208.80	12.90	208.50		165 132
2+50			12.0	196.8	193.5 196.0	C32
IP	0.96	196.61	13.15	195.65		
IP	5.39	188.21	13.29	183.32	176.9	176.9
2+75			6.9	181.8		C49
IP	0.86	176.65	12.92	175.79		
IP	0.52	164.26	12.91	163.74		
IP	5.21	157.12	12.35	151.91	153.1 166.7	C30
3+00			1.0	156.1		
3+30			5.9	151.2	147.0	C42
3+50			6.4	150.7	147.0	C37
CK BM	0.82	146.50	11.44	145.68	145.65	
3+75			8.4	138.1	131.0	C41
3+81.40 8" TEE			9.2	137.3	133.6	C32
CK BM	0.82	145.68				

BANGOR ST.

Cont'd

WAT. MET.

70

0400 - Nor. prop line Harbor View

0465 Wly 224 206.5 246.6 F01

0483 Fly 208 244.9 244.7 C02

WARNER ST.

JAN. 14, 1953

71.

CRATTY
WILLIAMS
KEMP
ALEXANDER

SILVERGATE TO CATALINA

(A) STRKS & GRDS. FOR 6" WATER

BM.				FB 89	
	3.19	296.79	293.60	199.20	BR on curb 85' 30" prop. line of Dudley; on Silvergate
0+00 = Fly prop. line Silvergate					
0+20	BR on Walk	7.1	289.7	286.6	C31
	Existing 6" TEE				
+25	6" G.V.	6.8	290.0	286.7	C32
+62		4.5	292.3	287.2	C51
1+00		2.3	294.5	289.5	C52
(D)	12.99	309.39	0.39	296.40	
+50		12.0	297.4	292.5	C49
2+00		9.2	300.2	295.5	C47
+50		6.2	303.2	298.5	C47
3+00		3.7	305.7	301.5	C42
+37		1.7	307.7	303.8	C39
(D)	2.74	312.09	0.04	309.35	
+87		2.2	309.9	305.7	C42
4+12		1.6	310.5	306.6	C39
+50		0.9	311.2	306.6	C46
+75		0.6	311.5	306.6	C49
5+00		0.9	311.2	306.3	C49
+37		1.7	310.4	305.8	C46
+50		2.1	310.0	305.0	C50
6+00		4.4	307.7	302.0	C52

WARNER ST.
Cont'd

1-14-52

72.

	312.09					
6+50		7.8	304.3	298.9	C54	
7+00		11.4	300.7	295.9	C48	
7+10	0.81	12.88	299.21			
+50		2.6	297.4	292.8	C46	
8+00		6.0	294.0	289.8	C42	
+50		9.3	290.7	286.7	C40	
9+00		12.3	287.7	283.7	C40	
+16		13.3	286.7	282.7	C40	
+10	F.H. TER.	13.0	287.0	283.1	C38	(S) 287.9
						286.7
						C12 To change C52 Post.
+25		13.4	286.6	282.2	C44	16
9+26	= Prop line Catalina					061
9+50	= End work	13.3	286.7	282.6	C41	16
9+58	=					26
9+66	= E CATALINA BLVD					774
ck'd		13.20	286.82 = 286.83			
						F.B. 819 pg 20 real E pipe & E CATALINA

WARNER ST.
(Cont'd)
WAT. METS

1-21-53

73

2+09 Nor	+1.2	301.0	300.5	C09
2+12 So.	+1.0	301.2	300.7	C05
2+71 So	-1.4	304.3	304.1	C02
3+68 So	-0.8	309.1	309.2	F02
4+05 Nor	-0.5	310.0	309.7	C03
5+00 Nor	+0.2	311.4	309.8	C16
5+57 So	+0.1	310.1	308.6	C15
5+58 So	+0.1	310.1	308.5	C15
5+84 So	-1.0	309.0	307.6	C14
6+10 Nor	-3.1	306.9	305.1	C18
6+30 So	+2.1	306.4	304.4	C20
6+91.5 So	+1.7	302.4	300.5	C12
7+21 Nor	+2.5	299.9	298.1	C18
7+48 So	+1.3	298.7	296.7	C20
8+04 So	+0.8	294.8	293.1	C17
8+33 Nor.	+1.5	292.7	290.7	C20

PACIFIC BEACH DRIVE
 HAINES TO RIVIERA
 ⊕ STKS & GRDS FOR 8°C.I. WATER

JAN. 19, 1957

74

BEATY
 WILLIAMS
 HAINES
 ALBANY

N.O. #23455

BM

58.11 (41 from fulcrum, 1949)

0+00 = 15 E of East GK

WEST
 0+65 = Prop. Line HAINES

0+51 = BEGIN WORK
 Edge AC PAVT. 9.35 48.8 45.0 C38

1+00 12.85 45.3 40.4 C49

4) 0.35 25.63 12.83 45.28

+50 5.8 39.8 35.7 C41

2+00 11.15 34.5 31.0 C35

11) 0.31 32.77 11.17 34.46

+38 3.6 31.2 27.3 C39 ✓

2+60 END WORK
 Begin CONC PAVT. 4.8 30.0 26.8 C32

P 9.39 31.60 12.56 22.21

OK BM 10.42 21.18 = 21.17 NW 1/4 Gresham & Pac. Riv. Dr.

PACIFIC BEACH DRIVE
 PROMONTORY TO INGRAHAM
 (4) STRS. & GRDS. FOR 8" C.I. WATER

BM	11.98	58.11		46.13	
BM			9.82	48.29	= 48.02
0+00	= W prop line Promontory St				(No 5300)
+75	= P prop line "		11.5	46.6	44.0
1+80			12.0	46.1	39.1
+50			12.6	45.5	36.8
+75			12.7	45.2	36.9
2+00			12.7	45.2	38.0
+50			12.7	45.2	40.2
3+00			12.3	45.8	42.4
+50			12.3	45.8	42.4

(HI carried to preceding page)

WATER METS

BM	4.35	26.13			
2+95 = Wly PL	50 28	INGRAHAM			
2+94 Nor	07 14 PL	3.9	46.6	46.5	C01
2+63 Nor	20 ⁰⁰ 50/PL	4.3	46.2	44.9	C13
2+225 Nor	20 ⁰⁰ 50/PL	4.6	45.9	43.7	C22
1+860 Nor	20 ⁰⁰ 50/PL	4.35	46.1	43.2	C29
1+570 Nor	20 ⁰⁰ 50/PL	4.4	46.1	43.2	C29
1+170 Nor	20 ⁰⁰ 50/PL	4.05	46.4	44.0	C29
0+75 = Ely PL	Promontory				
		4.42	46.06		

Jan. 19, 1953
 Same Party

75

W.O. # 23455

L & T. of Ingraham on 2 prop. line
 Top F.H. SE Cor Ingraham & Pac. Bch. Dr.

C25

C70

C87

C86

C74

C52

C34

C34

C01

C13

C22

C29

C29

C29

0+75
 2
 2
 2+95
 1.785
 1+175

33
 39
 375
 285
 80
 1795

Alley Cont'd

1-22-53

77

									Elev. Top 4" C.I. (Easting)
		177.94							
5+75 Nec			2.3	175.6	174.6	C10	✓		
HP	12.50	190.27	0.23	177.71				-2.5	173.1 CC. 06 High
6+47 So.			4.2	186.1	184.7	C14	✓		
HP	12.40	202.57	0.16	190.11				-2.7	183.4
6+83 Nec			11.5	191.0	198.5	C05	✓	-2.7	188.3
7+08 Swly.			8.3	194.2	194.0	C02	✓		
7+25 NEly			4.5	198.0	196.3	C17	✓		
HP	11.65	214.02	0.14	202.37				-4.0	194.0
7+90 NEly			12.0	204.0	203.7	C03	✓		
								-3.8	200.2
8+74 NEly			4.3	209.7	210.3	F06	✓		
HP			0.41	213.61	213.64			-3.9	215.8

E of Alley at End of AC point
w/ prep line Novars.

MOANA & LA PALOMA
WAT MET. 5

B.M.

① MARKED on Curb - No Grade NECESSARY

②

0+07.2 0+22.5 S

0+20

0+50 2+36 E

1+00

1+57.4 3+50 E

1+71.5 4+06 E

1+85

2+00 4+65 E

2.50

③ 5+31 E

3+00

+50 5+39 E

4+00

+50 5+97 E

5+00

④ 7+10 E

+50

+85 7+85 E

6+00

+50

+85

7+00

+50

+80

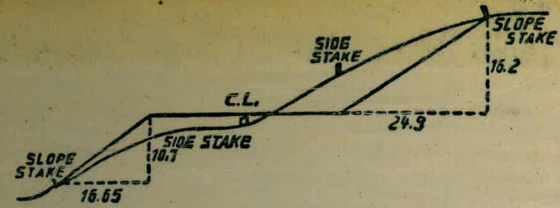
8+00

+15

CR BM

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

B.M.
 40
 40
 0+0
 0+20
 0+40
 1+0
 1+50
 1+70
 1+85
 2+00
 +50
 3+00
 +50
 4+00
 +50
 5+00
 48
 6+00
 +50
 48
 7+00
 +50
 +80
 8+00
 +15
 08 11



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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