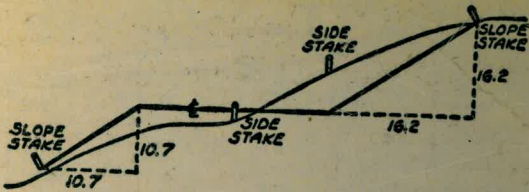


W 858



Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distances of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the out or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.08	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.777	.877	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.98
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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INDEX  
(Cont'd.)

alice

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CLOVE ST  
MACAULAY to OLIPHANT  
⑥ STKS & GRDS FOR 6" WATER

JAN 27, 1953

BEATTY  
WILLIAMS

1.

BM	8.77	123.26		112.49	
0+00				113.1 Top	
				112.5 Root	
+10 F.H. TEE		6.5	116.8	112.4	
				113.4	
+50		7.55	115.7	112.0	
1+00		8.96	114.3	110.1	
+50		10.5	112.8	108.3	
2+00		11.66	111.6	106.4	
+25 6" TEE					
+50	0.31	110.22	13.35	109.91	104.6
3+00		3.32	106.9	100.6	
+25		6.02	104.2	98.6	
+50		7.93	102.3	95.9	
				95.4	
4+00	2.50	100.56	12.16	98.06	90.6
				89.0	
+50		7.6	98.0	82.2	
				82.7	
+65 F.H. TEE		9.3	91.3	82.5	
				82.8	
+75 END WORK		10.68	89.88	81.2	
				79.2	
P	12.01	102.67	9.90	90.66	
P	12.34	114.40	0.61	102.06	
P	7.20	121.55	0.05	114.35	
CK BM		7.03	112.52	112.49	

NAH IN POLE (F.D. 822 pt. 6)

Top Existing 6" CI

C44  
C34

⑤ F.H. 116.4 C0-C40

C37

C42

C45

C52

C53

C63

C56

C69 C64

C91 C75

C103 C88

C105 C88

C104 C87

C104 C87

C104 C87

C104 C87

C104 C87

C104 C87

NOTE:-

GRADE REVISED  
0+10 TO FIT EXISTING  
6" C.I. MAIN

GRADE REVISED  
3+25 TO 2+75  
To put main 3"  
below Est. Grade  
25 per profile 1682

91.1 - Curb Gas  
85.2 - C59 - C94

3/4" ID Sully Cor Oliphant & Clove



CLOVE ST.

WAT. METS

1-28-53

2.

BEATTY  
WILLIAMS  
ALEXANDER

0+33 NWly	205 from E st	+1.7	117.4	116.2	c12
1+00 NWly		+0.7	115.0	114.0	c12
1+02 SELV		-0.2	114.1	113.3	c08
1+30 NWly		-0.1	114.2	113.0	c12
1+625 SELV		..	112.8	111.3	c15
1+77 NWly		+0.6	113.4	111.4	c20
2+01		-0.1	111.5	110.0	c15
2+02	SELV 2+025 & 4 MET STRIP BK TO P.L. @ 30' from E ST				
2+03					
2+04		-0.4	111.2	109.9	c12
2+65		-0.7	109.2	107.5	c17
2+66	SELV				
2+67					
2+68		-1.4	108.5	107.3	c12
2+57 NWly		-0.6	109.3	108.7	c06
3+48 NWly		-0.1	102.2	101.3	c09
4+18 SELV		-0.7	97.4	91.4	c60
4+27 NWly		-1.4	96.7	91.0	c57



CLOVE ST.

WAT. MET.

1-28-53

3

2476 } +11 91.0 85.6 C54

2477 } NWly 30' from st

2478 } -02 89.7 85.6 C41

3455 } -05 101.8 100.4 C14

3456 } NWly 20' from st

3457 } NWly 20' from st

3458 } -07 101.6 99.9 C17



31<sup>ST</sup> ST.

CEDAR TO ELM

⑤ STKS &amp; GRADES FOR 6" WATER

Jan. 30, 1933

BEATTY  
WILLIAMS  
KEMP  
ALEXANDER

B.M.	0.53	226.00		225.47			
HP	1.32	214.38	12.92	213.06			
0+00 = Sly Prop. line Cedar.							
0+80	Begin Work		1.32	213.06	209.8		
					204.4		
1+00			2.75	211.63	207.8		
					205.3		
+50			8.55	205.83	202.0		
HP	0.88	202.23	13.03	201.35	203.0		
2+00			1.3	200.9	197.7		
+50			6.4	195.8	192.4		
+75			8.85	193.4	189.7		
3+00							
3+25			12.6	189.2	185.2		
HP	11.18	200.09	13.32	188.91			
3+75	B.O.		12.55	187.54	184.0		
4+25			11.45	188.6	185.0		
4+75			6.5	192.6	189.0		
5+00			4.4	195.7	191.7		
HP	12.88	212.67	6.30	199.79			
+50			11.1	201.6	197.1		
6+00			5.75	206.9	202.6		
HP	12.85	224.87	0.65	212.02			
+50			12.65	212.2	208.0		
7+00			7.3	217.6	213.5		
+50			2.0	222.9	218.9		

B.P. SW COR. GROVE & CEDAR  
NAT. Ground  
Elev  
& Pipe

C32 +0.1 213.2

C38 00 211.6

C32 +0.7 206.5

C32 +0.5 201.4

C34 +0.3 196.1

C32 +0.3 192.7

C42 +0.2 189.8

C35 -0.3 187.2

C35 00 188.6

C46 -0.2 193.3

C40 +0.1 195.8

C45 -0.3 201.3

C43 -0.5 206.4

C42 -0.6 211.8

C41 -0.4 217.2

C42 -0.5 222.4

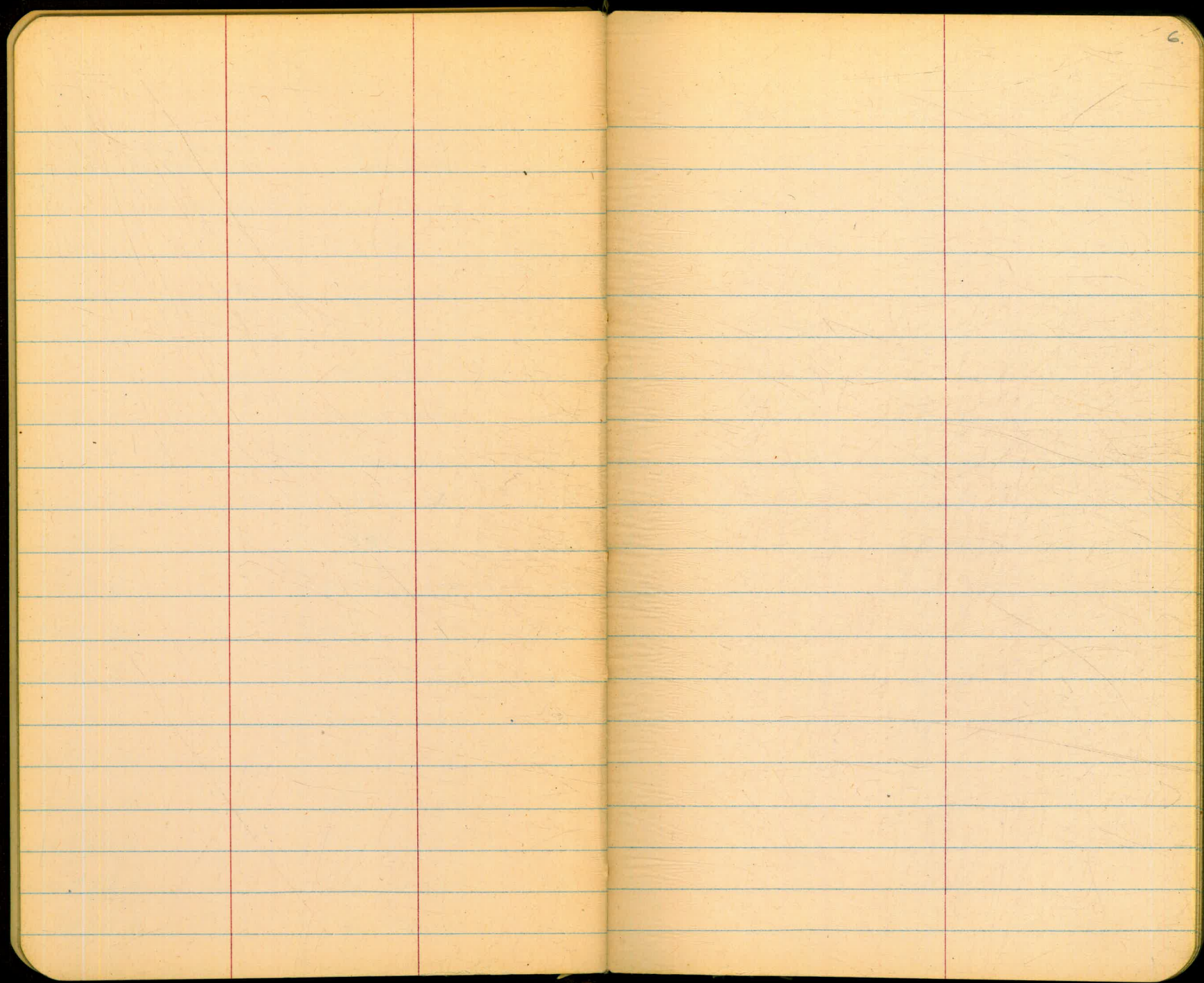
E of 6" WATER AS STRK

E of 21<sup>ST</sup> ST.5' offset marked  
on curb 3.75'  
7+6125'  
90'  
75'15'  
3" Conc. Gutter.  
0" Conc. Curb.EXISTING &  
AS PER  
1099-L











BALTIC ST.

ATLAS ST. Wly for 138'

(5) STKS. & GRDS FOR 16" C.I. WATER

TBM.	3.68	385.98	382.30
31+01.05 = End of Existing 16" C.I.	9.88	376.10	376.10
30+98.02	End work	4.91	381.07
			375.6
+50		4.34	381.64
			378.0
30+00		4.21	381.76
			377.2
29+60	16"x8" TEE	3.66	382.32
			377.8
	8" T	7.36	378.6
			- .8
			377.8 OK

Feb. 2 1953

7

W.O. # 25025 W-5748

1 1/4" I.P. 40' LT. 30+98.02 See E.P. 74-7 pg 24.

C50

C36

C45

C45



FEB. 2, 1953

8.

DREAM ST.

CHURCHWARD, NELY 358'

④ STKS &amp; GRDS for 6" WATER.

12.77	237.52		224.75		Top of curb 0+15.20 - see PK 826 pg 20.
0+83		12.2	225.3	221.8	c35 moved 7' 1/2 LT to fit GV
1+00		11.4	226.1	222.1	c40 moved 6' 1/2 LT
+50		9.6	227.9	223.6	c43
2+00		8.0	229.5	226.0	c35 on. LINE
+50		5.6	231.9	228.2	c37
+75		4.2	233.3	229.3	c40
3+00		2.2	235.3	230.8	c45
3.35	240.63	0.24	237.28		
+50		2.25	238.4	234.0	c44
3+58	End of Work	2.0	238.6	234.5	c46
ck TBM.			240.60 = 240.55		Top curb 3+96+



39<sup>TH</sup> ST  
 HILLTOP TO FEDERAL  
 (A) & (C) STKS. & GRDS FOR 16' C.I.

FEB. 4, 1953

BETTY  
 WILLIAMS  
 WIFE  
 Alexander

9

REVISED 045<sup>th</sup> 3481<sup>st</sup>  
 SEE SKETCH PAGE 11

BM	5.52	172.05	166.53
0+05 (A) Begin Work	4.9	167.2	159.0
0+20	4.95	167.1	159.0
0+40	4.95	167.1	158.9
0+75	5.15	166.9	158.7
1+00	5.25	166.8	158.1
1+50	4.6	167.5	157.6
2+00	4.75	167.3	157.0
2+25	5.45	166.6	156.7
2+68 (A) } 4 PT.	6.5	165.6	154.7
2+68 (C) }	6.45	165.6	154.7
3+00	8.6	163.5	153.2
TP	0.27	159.00	13.32 158.73
3+50	1.6	157.4	150.8
3+81 <sup>st</sup> 4 PT & B	5.9	153.1	148.4
4+00	7.2	151.8	147.0
+25	9.1	149.9	145.1
+50	10.1	148.9	143.2
+75	11.5	147.5	140.6

BR Sta. Cor. 39 <sup>TH</sup> & Hilltop	BM 572	172.27	166.53
C8 <sup>2</sup> 0+05	2.91	167.4	159.0 C84
C8 <sup>1</sup> 0+20	4.66	167.3	159.0 C83
C8 <sup>2</sup> 0+40 Near Prop line	5.2	167.1	158.9 C82
C8 <sup>2</sup> 0+75	5.3	167.0	158.7 C83
C8 <sup>2</sup> 1+00	5.2	167.1	158.1 C90
C99 1+50	4.65	167.6	157.6 C100
C103 2+00	4.75	167.5	157.0 C105
C99 2+25	5.55	166.7	156.7 C100
C109 2+67	7.19	165.1	154.6 C105
C109 3+00	9.67	162.6	153.0 C96
C103 3+30 <sup>62</sup> } BC.	12.63	159.6	151.5 C81
3+35 <sup>0</sup> }			
C6 <sup>0</sup> TP 0.27	162.67	9.09	163.18
C47 3+50	6.7	157.0	150.8 C63
C48 3+75	9.88	153.8	148.9 C49
C48 3+81 <sup>st</sup> POC.	10.53	153.1	148.4 C47
C57 OK TP	4.94	158.73	=158.73
C69			



39TH ST  
(Cont'd)

2/4/53

10

	159.00				
5+00		12.5	146.5	1379	C86
①	0.15	125.96	1319	145.81	
+25		1.4	144.6	1353	C93
+50		3.35	142.6	1326	C100
+75		5.35	140.6	1300	C106
6+00		8.0	138.0	1275	C105
6+25.82	E.C.	11.75	134.2	1248	C94
①	0.21	133.06	13.11	132.85	
6+50		2.75	130.3	1221	C82
7+00		9.65	123.4	116.8	C66
CK, TBM		6.53	126.53		NAIL IN POLE 35' LT 7+25+
①	0.08	120.00	13.14	119.92	
7+50		2.85	117.15	111.5	C57
7+68.81	BC	4.45	115.55	109.6	C60
+75		4.85	115.15	109.0	C62
8+00		7.35	112.65	106.0	C63
+25		9.6	110.4	103.9	C65
+50		12.3	107.7	101.4	C63
①	0.63	108.33	12.30	107.70	



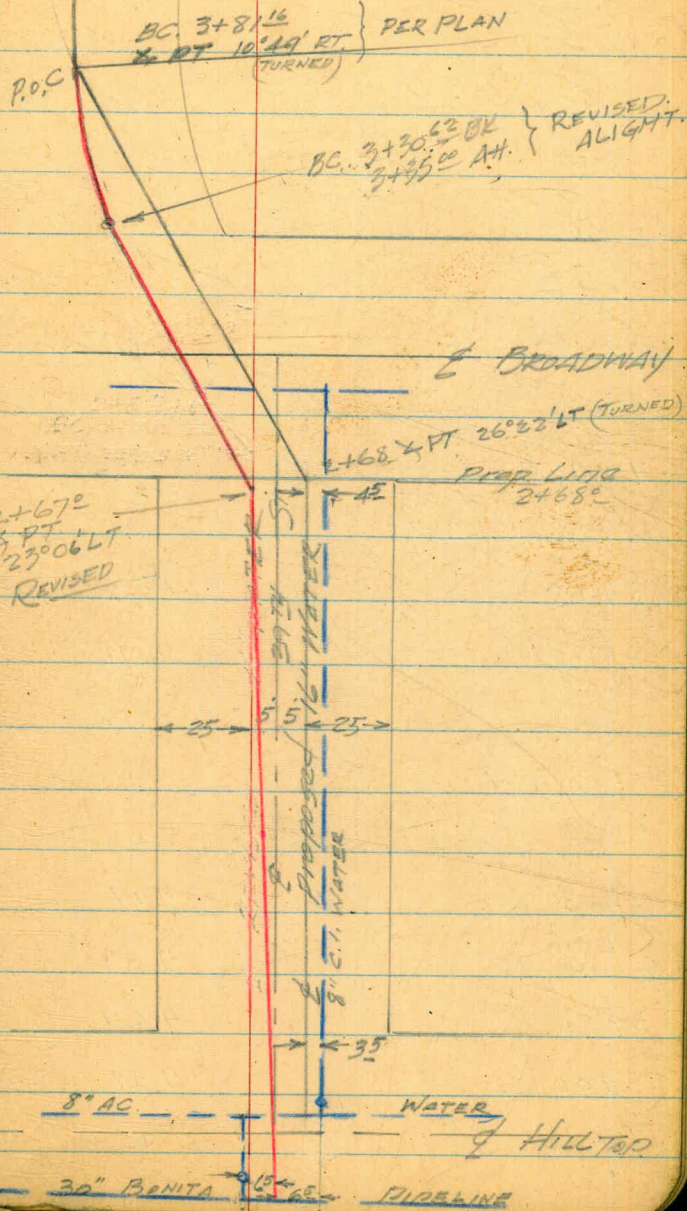
39th St  
(Cont'd)

108.33

8+66.43 EC		2.15	106.2	99.7	C65
9+00		4.7	103.6	96.3	C72
+50		8.65	99.7	91.2	C85
10+00		13.35	95.0	86.1	C89
IP	0.51	95.87	12.97	95.36	
+50		6.05	89.8	81.0	C88
11+00 (2 RT 1 1/2° RT.)		11.25	84.6	76.0	C84
IP +50	5.62	89.56	11.93	83.94	C95
IP	2.50	82.20	9.86	79.70	
11+76.89 (2 RT 1 1/2° RT.)		4.25	78.0	74.3	C37
OK BM		7.07	75.13 = 75.35		

2/4/53

11.





MORENA BLVD  
 Profile & X-Sections over  
 16" C.I. to be Salvaged  
 PIPE FINDER LOCATION

Bottom of Pipe  
 Below offset  
 & to offset  
 offset 67

LT.

RT.

DM	4.43	24.50	20.07								
11407 End 16" C.I. Pipe.						6.55	6.55	5.25	5.19	5.2	5.2
11400 = End EXCAV. AT. Abut.				-5.1	⊙	5.	3.0'	1.5'	0.5'	2.	5.2
+75				-5.1	⊙	6.1	6.06	5.3		5.3	5.2
+50				-5.1	⊙	5	4.0'	3.0'		2.	5.2
10400				-4.5	⊙		5.79	6.13		6.18	5
4							4.0'	3.0'		5	⊙
9+70				-4.5	⊙		7.6	7.6		7.5	17.0
9+50				-5.1	⊙		5			5	15.6
4							8.7	8.7		8.9	⊙
9+50				-5.4	⊙		9.1	9.1		9.0	15.5
4							13.9			5	13.7
9+50				-6.1	⊙	⊙	10.7	10.7		10.8	5
T.P.	3.59	17.18	10.91				5.				13.29
8+88				-6.0	⊙	⊙	13.22			3.74	3.87
8+50				-5.6	⊙	⊙	3.96			3.0'	3.0'
8+00				-5.3	⊙	⊙	3.0'			1.0'	3.0'
7+50				-5.0	⊙	⊙	4.85			4.39	4.44
7+00				-4.8	⊙	⊙	3.0'			1.5'	3.0'
6+50				-5.3	⊙	⊙	5.20			4.78	4.75
6+00				-5.0	⊙	⊙	3.0'			1.0'	3.0'
5+50				-5.0	⊙	⊙	5.3			4.9	4.9
5+00				-4.8	⊙	⊙	3.0'			0.5'	3.0'
4+50				-4.7	⊙	⊙	5.13			4.72	4.64
				-4.7	⊙	⊙	3.0'			1.0'	3.0'
				-5.0	⊙	⊙	4.92			4.52	4.51
				-5.0	⊙	⊙	3.0'			1.0'	3.0'
				-5.5	⊙	⊙	4.82			4.45	4.58
				-5.5	⊙	⊙	3.0'			1.0'	3.0'
				-6.4	⊙	⊙	4.65			4.25	4.26
				-6.4	⊙	⊙	3.0'			1.0'	3.0'
				-6.4	⊙	⊙	4.52			4.25	4.18
				-6.4	⊙	⊙	3.0'			1.0'	3.0'
				-6.4	⊙	⊙	4.36			3.86	4.04
				-6.4	⊙	⊙	3.0'			1.0'	3.0'

offset 67



MORENA BLVD  
Cont'd.

2/4/53

13

	17.18		
T.P.	5.88	18.78	4.28 12.90
4+00			5.70 13.08
3+50			5.41 13.37
3+00			5.11 13.67
2+50			4.83 13.95
2+00			4.62 14.16
1+50			4.63 14.15
1+00			4.19 14.59
0+64	Begin pipe removal		4.57 14.26
	Begin EXCAV.		
T.P.	7.39	25.23	0.90 17.80
CK BM.			2.74 22.29 22.35

LT

RT

	13.1		13.41	4.8
-65 (45) (5)	5.71	5.31	5.37	1.5
	3.0'	1.0'	3.0'	
-63 (4) (5)	5.44	5.03	5.02	13.76
	3.0'	1.0'	3.0'	
-62 (4) (5)	5.05	5.17		
	3.0'	3.0'		14.12
-58 (42) (5)	4.91	4.50	4.66	
	3.0'	1.0'	3.0'	
-56 (42) (5)	4.90	4.48		
	3.0'	3.0'		
-57 (45) (5)	4.81	4.4		
	3.0'	3.0'		
-57 (54) (5)	4.69	3.91	4.53	14.25
	3.0'	3.0'		
-58 (7) (5)	4.67	4.29	4.49	
	3.0'	3.0'		

OP NE Wing Wall  
New Morans  
Bridge



FEB. 9 1953

12

Quincy St  
ROSECRANZ TO EVERGREEN  
⑥ STKS & GRDS FOR 6" WAT.

BM	4.68	11.46		06.78			7 offset disk Olyphant & Rosecranz, FB 822, pp. 3-4
P	12.57	18.06	5.97	05.29			
0+26	Begin Work		10.4	07.7	038		C37
0+50			10.0	08.1	041		C40
1+00			6.4	11.7	078		C39
+50			2.55	15.5	11.5		C40
P	13.00	30.76	0.30	17.76			
2+00			11.5	19.3	15.2		C41
+50			8.1	22.7	18.9		C38
+69					20.3		
+94	FN TRF		6.8	24.0	22.2		C37
3+00			4.8	26.0	22.6		C32
+50			1.0	29.8	24.9		C39
P	13.24	43.86	0.14	30.62			
+75			12.0	31.9	26.0		C59 ✓
4+00			9.9	34.0	28.9		C52
+50			6.15	37.7	32.7		C30
5+00			1.0	42.9	39.3		C36
P	13.31	57.08	0.09	43.77			
+50			6.0	51.1	47.0		C41
P	13.17	69.99	0.26	56.82			
6+00			10.45	59.5	54.6		C47
27							
6+30	END WORK		+0.6	70.6	64.0		C66
			+1.6	71.6			Edge Case Drive



Quimby St.  
Cont'd

2/13/59

15

WAT. MET 2 staked

3+58	1976 Locust +35	33.3		cgl	
3+59 NELY	1976 Locust +38	33.6	30.2	c	
				34	
3+94 SWly	1924 Locust -0.9	33.1	32.0	c/l	
4+375 SWly	3111 Quimby -1.0	36.7	37.0	F03	
4+99 SWly	3119 Quimby -0.3	42.6	42.7	F2-	
5+345 SWly	3229 " +5.4	48.3	49.8	F12	
5+80 SWly	3135 " +5.7	56.8	57.5	F07	
6+28 SWly	3145 Quimby -0.5	70.1	66.5	c36	
4+075 NELY	1954 Locust +5.2	39.2	32.0	c52	
4+78 NELY	3116 Quimby +5.0	42.7	42.4	c03	

195 NELY

E  
|  
ST.

195 SWly



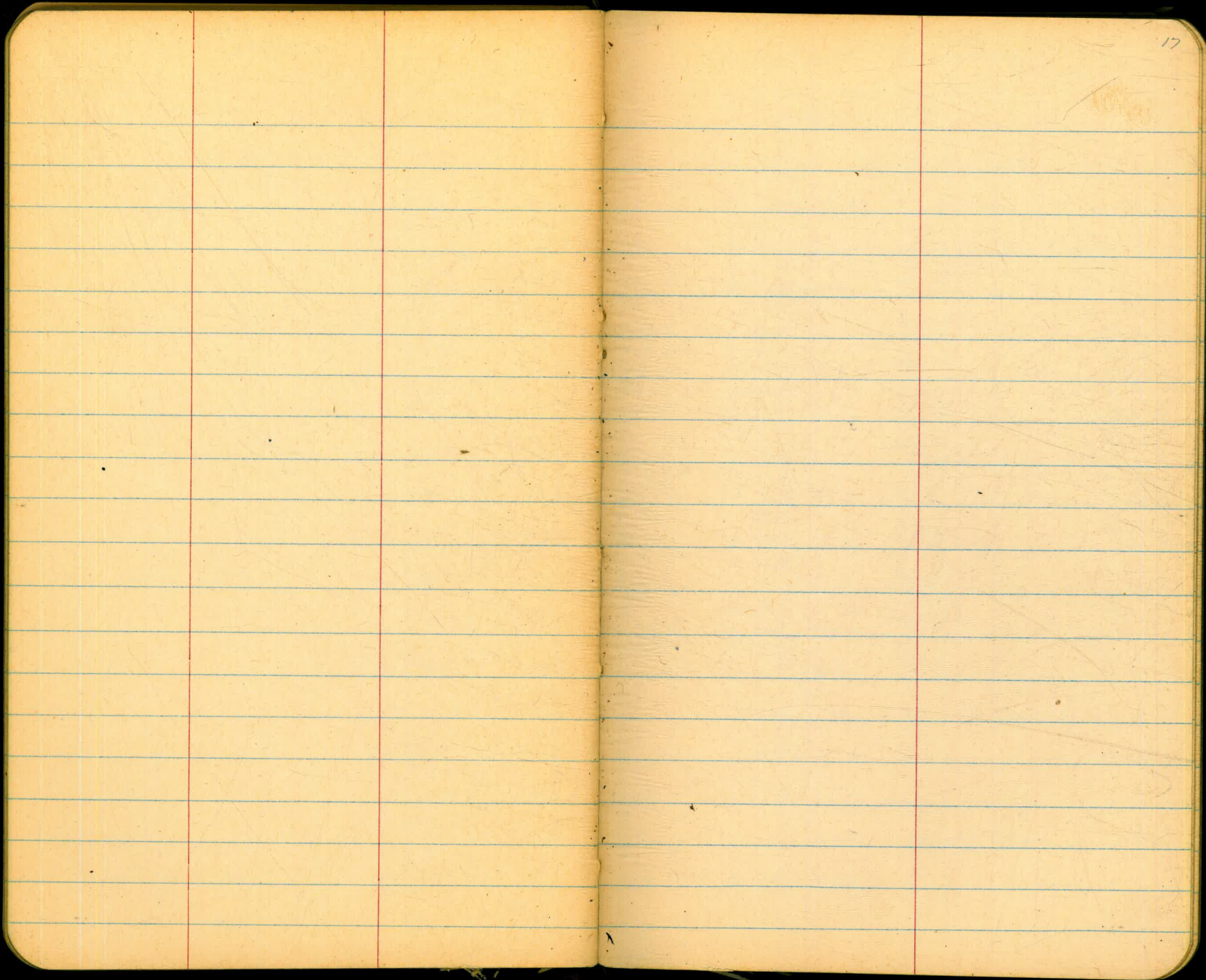
WINONA ST  
UNIVERSITY to POLK  
⑥ STKS. & GRDS FOR 6" WATER

FEB. 9 1953 16

BM				Grade		
	5.25	335.00	330.15			
0+80	Begin Work.	5.9	329.5	325.4	C45	
1+00		5.7	329.7	325.9	C38	
1+20		5.2	330.2	326.4	C38	
1+60		4.75	330.65	327.3	C34	
2+00		3.9	331.5	327.9	C30	
2+50		2.9	332.5	328.7	C38	
3+00		2.0	333.4	329.4	C40	
3+20	12.96	346.77	1.59	333.81	329.7	C41
3+60		12.15	332.6	331.0	C36	
4+00		11.2	335.6	332.3	C33	
4+40		9.9	336.9	333.5	C34	
4+70		9.0	337.8	334.5 332.8	C30 C33	
5+00		7.9	338.9	335.6 336.1	C28 C33 v	
5+50		5.95	340.8	337.3 335.3	C25 C35 v	
5+60		5.6	341.2	337.6 338.8	C24 C36 v	
6+00		4.3	342.5	339.0 337.8	C27 C35 v	
6+50		2.4	342.4	340.7 341.0	C34 C37 v	
6+78	F4 TEE	1.65	345.1	341.5 341.0	C35 C36 v	
6+85	End Work	0.6	346.2	341.9	C43 v	
		0.35	346.22	= 346.2		

7' off Tag Sely Cor Winona & Polk







OREGON ST. PIPELINE  
 (10) STKS & GRADES SET FOR 48"  
 RCP WATER

TBM	1.38	376.49	375.11	
SET TBM		2.38	374.11	
SET TBM	5.22	375.09	6.62	369.87
10+77 <sup>00</sup>	& VALVE	9.25	365.84	360.0
10+50		8.9	366.2	360.05
+25			366.50	360.09
10+00		8.2	366.9	360.13
+75			367.25	360.77
9+50		7.55	367.54	360.22
+25			367.95	360.27
9+00		6.95	368.14	360.31
+75			368.45	360.35
8+50		6.35	368.74	360.39
+25			369.00	360.43
8+00		5.75	369.34	360.48
+75			369.70	360.52
7+50		5.15	369.94	360.56
+25			370.30	360.60
7+00		4.45	370.64	360.65
+75			371.00	360.69
6+50		3.8	371.3	360.74
TD	7.42	378.74	3.77	371.37
OK TBM		3.64	375.10	= 375.11
OK TBM		4.64	374.10	= 374.11
TD	5.26	380.01	3.99	374.75 (2+50)
OK		3.94	376.07	= 376.08

FEB. 10, 1952

18

BETTY  
 KEMP  
 ALEXANDER

Cor. Retaining wall. See EB 794 pp. 76

7 LET. SWly cor Howard & OREGON

Cor. Retaining wall NEly Cor. PAIK & OREGON

6584 (6 PIPE = 10' Ely  
 E of Oregon.)

662	366.15
664 ✓	366.15
668	366.92
671 ✓	367.27
673	367.62
673 ✓	368.09
678	368.09
682 ✓	368.59
684	369.24
686 ✓	369.24
689	369.87
692 ✓	369.87
694	370.54
697 ✓	370.54
700	371.12
703 ✓	371.12
706	371.12

ed E Lamp Post Base  
 El Cajon & Oregon



OREGON ST. PIPELINE  
Cont'd

2/18/53  
Same Party

17

TBM					PIPE	
4.25	379.36		375.11			
6+50 <sup>(10)</sup> CXP		8.05	371.31 = 371.3 360.74		C106	371.10 5.26
6+25		7.74	371.62	360.78	C1085	
6+00		7.41	371.95	360.82	C111	371.85 7.51
5+75		7.12	372.24	360.87	C114	
5+50		6.91	372.45	360.91	C1155	372.21 7.15
5+25		6.50	372.86	360.95	C119	
5+00		6.20	373.16	360.99	C123	373.00 6.36
4+96 <sup>23</sup> EC		6.15	373.21	361.0	C122	
4+75		5.96	373.40	361.04	C124	373.09 5.27
4+50	$\Delta = 3^{\circ}58' RT$ $R = 1043$ $L = 72.20$	5.60	373.76	361.08	C127	373.56 5.86
4+297 <sup>23</sup> PRC		5.46	373.90	361.12	C128	
4+100	$\Delta = 3^{\circ}58' LT$ $R = 1043$ $L = 72.20$	5.28	374.08	361.17	C129	373.90 5.14
3+75		5.07	374.29	361.21	C131	
3+51.83 BC		4.97	374.39	361.25	C135 C132	374.21 5.16 = 165 = 15' Ely & Oregon
3+25		4.92	374.44	361.29	C135 C132	
3+00		4.85	374.51	361.29	C132	374.40 5.26
2+75		4.76	374.60	361.29	C133	
2+50		4.77	374.59	361.29	C133 ✓	374.48 4.88



OREGON ST PIPELINE  
(Cont'd.)

2/18/53

20

	379.36					
2+25	4.65	374.71	361.29	C134		
2+00	4.62	374.74	361.29	<del>C134</del> C135	374.62 ✓ 4.74	
1+75	4.54	374.82	361.29	C135		
1+50	4.52	374.84	361.29	<del>C135</del> C136	374.70 ✓ 4.66	
CK TBM.	3.29	376.07	= 376.08			

SET GRADE (17) ELY. 3/2/50

B.M.	3.17	379.25	376.08	
0+88.12	Regr'd Spec	11.00	368.25	361.29 C70
1+00.87	End "	8.17	371.08	361.29 C98
+50		2.43	372.8	361.29 C135
2+00		4.51	374.74	361.29 C135
+50		4.65	374.6	361.29 C133
3+00		4.78	374.47	361.29 C132
		4.38	374.87	= 374.87

1 1/2' s. of edge of box

372.90  
4.35

(7) = 10' easterly & st.

374.80  
4.45

(7) = 16' easterly & st.

(10) 1+50  
above



OREGON ST. P.L

Contd

GRADES SET for Sidewalk  
& Curb replacement

3/5/51

21

TBM	1.50	376.61	375.11	369.18	375.45	369.87
CK TBM			6.73	369.88 = 369.87	9.2	369.87
0+00			9.72	366.89	366.89	365.98
+50			9.19	367.42	366.50	366.58
1+00			8.66	367.95	367.07	367.28
+50			8.12	368.49	367.65	367.98
2+00			7.59	369.02	368.22	368.50
+50			7.05	369.56	368.79	369.06
3+00			6.52	370.09	369.37	369.75
+50			5.99	370.65	369.93	370.26
4+00			5.46	371.21	370.51	371.06
+50			4.93	371.76	371.09	371.72
5+00			4.39	372.32	371.65	372.32
+16 <sup>35</sup> = 100' 50" P.C. CURB RET				372.90	372.98	
+50			3.86	372.88	372.23	372.97
6+00			3.32	373.44	372.81	373.53
+22 <sup>05</sup> (Top existing S.W. @ wall)			3.10	373.68	373.05	373.73
CK BM	1.50	375.11				374.12 = 374.11

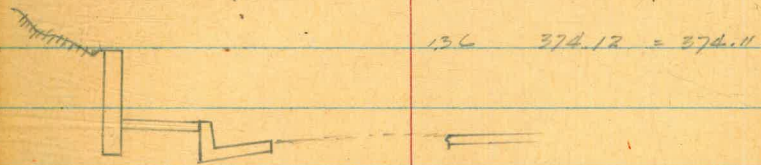
0.1066%

Formed  
to here  
7/10/51

0.1115%

Revised  
see pg 51

PT of Retaining Wall





44<sup>TH</sup> ST.  
 HILLTOP TO "A" ST  
 (4) STKS & GROSS FOR 6" WATER

FEB. 11, 1953  
 BETTY  
 WILLIAMS  
 KEMP  
 ALEXANDER

22

BM	9.44	179.66	170.22				
0+30 = 1/2 Hilltop			Top 6" TEE 165.6	Bot 165.0		NAIL IN Pole SW Cor Hilltop & 44 <sup>TH</sup>	
0+40 Begin Work			8.6	171.1	167.1	C40	
0+70 F.H. TEE			7.05	172.6	166.2	C64	
					167.2	C54	# Grd. 174.5
							# Grd. 171.7 C28 C82 (24' from & ST)
1+00			6.65	173.0	167.4	C56	
+50			7.4	172.3	167.8	C45	
2+00			7.65	172.0	168.2	C38	
+50			7.2	172.5	168.6	C39	
3+00			6.5	173.2	169.0	C42	
+50			5.6	174.1	169.4	C47	
4+00			5.2	174.5	169.8	C47	
+50			4.3	175.4	171.3	C41	
5+00			2.8	176.9	172.8	C41	
+25			1.5	178.2	173.5	C47	
+50	8.90	187.99	0.57	179.09	174.7	C44	
6+00			7.0	181.0	177.1	C39	
+50			4.4	182.6	179.4	C42	
79					180.6		
6+85 6" TEE			2.2	185.8	180.8	C52	
7+00			1.8	186.2	181.4	C28	
22							
7+30 F.H. TEE			0.03	187.96	182.3	C52	# Grd 188.9
(4)	11.38	199.11	0.26	187.73			# Grd 186.5
							C24 C64

60 240 30  
 120



44<sup>TH</sup> ST  
(Cont'd)

2/11/53

23

199.11

7+50		10.0	189.1	183.5	C56
8+00		8.45	190.7	185.5	C52
+50		7.0	192.1	186.9	C52
9+00		5.4	193.7	188.3	C54
+25		4.9	194.2	189.0	C52
+50		4.4	194.7	189.0	C57
10+00		4.4	194.7	189.0	C57
+50		5.4	193.7	187.4	C63
11+00		6.9	192.2	185.8	C64
+50		9.6	189.5	182.6	C69
HP	1.25	187.48	1308	186.03	
12+00		2.4	185.1	179.4	C52
+50		4.2	183.3	176.2	C71
13+00		7.2	180.3	173.1	C72
13+55	END WORK	13.7	173.8	169.7	C41
CK T.D.M.		7.91	179.57	= 179.60	NOTE IN GUY PILE 6' BT 13+56 BK 817 pg. 57



44<sup>TH</sup> ST.

(Cont'd)

WAT. MET.S.

24

1+48 Ely	1+50	+19	174.2	171.7	C25	No Existing METER HERE!
1+92 Wly	2+00	-0.1	171.9	171.8	C01	924 44 <sup>TH</sup>
2+69 Ely	2+50	+0.8	173.3	172.7	C06	935 44 <sup>TH</sup>
2+85 Wly	3+00	-0.4	172.8	172.4	C04	936 44 <sup>TH</sup>
3+04 Wly	3+00	+0.1	173.3	172.6	C07	938 44 <sup>TH</sup>
3+54 Wly	3+50	-0.2	173.9	172.9	C19	948 44 <sup>TH</sup>
3+54 Ely		+0.4	174.5	173.2	C13	943-945-947 44 <sup>TH</sup>
3+90 Ely	4+00	+0.2	174.7	173.2	C12	No Existing MET. HERE!
4+16 Wly	4+00	+0.4	174.9	173.7	C12	1016 44 <sup>TH</sup>
4+38 Ely	4+50		175.7	174.2	C13	No Address - Vacant
5+65 Wly	Should move 5+63 63	+1.1 5+50	180.2	178.8	C14	1028 44 <sup>TH</sup>
6+02 Ely	6+00	+0.2	181.2	181.8	F06	1037 44 <sup>TH</sup>
6+48 Wly	6+50	+0.5	184.1	183.7	C04	? Nursery (1051 43 <sup>rd</sup> )
6+96 Ely	6+99	+1.0	186.8	185.6	C12	1057 44 <sup>TH</sup>
7+15 Wly	7+22	-1.4	186.6	185.6	C10	? address
7+72 Wly	8+00	-1.1	189.6	188.2	C14	1104 44 <sup>TH</sup>
7+81 Ely	8+00	0.0	190.7	189.0	C12	1101-1111 44 <sup>TH</sup>
8+18 Wly	8+00	0.0	190.7	190.0	C07	1122-1124 44 <sup>TH</sup>
8+70 Ely	8+50	+0.7	192.8	191.3	C15	No Existing MET. HERE!
9+30 Wly	9+25	-1.6	192.6	192.1	C05	1136 44 <sup>TH</sup>
9+65 Ely	9+50	+1.0	195.7	193.3	C24	1137 44 <sup>TH</sup>
10+18 Ely	10+50	+2.4	196.1	192.8	C33	1201 44 <sup>TH</sup>
11+09 <sup>5</sup> Ely	11+00	+1.2	193.2	189.7	C37	1215 44 <sup>TH</sup>
11+09 <sup>5</sup> Wly	11+00	-2.3	189.9	189.2	C07	? Broken MET. Box, No SER. or MET
11+77 Wly	11+50	-4.9	182.6	185.2	F06	1230 44 <sup>TH</sup>

STAKED  
PER  
PLAN  
Per Bell  
via Bots



CARLTON ST  
SCOTT to SHAFER  
⑥ STKS & GRDS

2/13/53

25

BM	136	15.89	14.53			SW curb Rosecrans & Carlton
0+10			10.65	05.24	01.6	c36
+50			11.35	04.54	01.0	c35
P 1+00	485	08.63	12.11	08.78	00.3	c35
1+45			5.6	03.0	-00.4	c34
2+00			6.4	02.2	-01.3	c35
+50			7.2	01.4	-02.1	c35
3+00			7.6	01.0	-02.8	c38 curb actually 01.5 Est Gen 01.0
+50			7.4	01.2	-02.8	c10
+70	End Work		7.3	01.3	-02.8	c41
P	6.08	12.11	2.60	06.03		
OK BM			20' Sta. 4.08	08.03		
			15' Sta. 1.66	07.25	= 07.59	NE Cement Sta Byron & Scott
3+70	FH TEE		01.0		01.0	c00 # c15
3+71	WAT MET		01.0			c00
3+73	WAT MET		01.0			c00
CHIS H	NWly Cor of Conc					
	5136 in					
	front of					
	Pump Sta		7.68	00.95		



FEB. 16, 1953

26

BATTY  
KEND  
ALEXANDER

## PEPPER DRIVE

VIOLET TO TULIP; TULIP ST.

PEPPER DR TO SYCAMORE

④ STRS &amp; GRDS. FOR 8" WATER

BM	0.11	286.49	286.38		Top F.H. Violet & Poplar
0+00	(2 TEE) (1.15 1/2 RT) OF TANGENT	11.7	274.8	275.0	Bot pipe
0+05		6.5	280.0	274.8	C52
0+38	F.H. TEE	78	278.7	273.9	C48
HP	X PT 105 1/2 RT - EC Prop Line				278.8 GRD 278.0
0+57.45	0.59 NLY Side St	7.92	278.57	273.3	C53
1+00	279.16	2.0	277.2	272.0	C52
1+50		3.2	276.0	270.5	C55
2+00		4.6	274.6	269.0	C44
2+38		5.8	273.4	267.9	C52
2+42.2	X PT 22' 30" RT	6.0	273.2	267.8	C54 ✓
2+50		6.1	273.1	267.6	C55 ✓
3+00		8.0	271.2	266.4	C48 ✓
3+32.72	X PT -(E.C. & ST)	8.9	270.3	266.0	C43 ✓
3+50		9.4	269.8	265.2	C45
4+00		10.0	269.2	264.0	C52
HP					
4+12	1.65	10.21	268.95	263.8	C52
4+50		2.4	268.2	263.0	C52
5+00		3.5	267.1	262.0	C51
+50		4.7	265.9	261.0	C49
6+00		5.4	265.2	260.0	C52
+265 +25	F.H. TEE on Prop. Line.	5.4	265.2	259.4	C58
					W. 262.8 GRD 262.0
					E 264.4
					C18 C53
					C12 C49

6.0 S

6.5 W

5.4



PEPPER DRIVE  
(Cont'd.)

2/17/53

27

	270.60				
6+50		5.6	265.0	258.9	C61
6+63 <sup>70</sup>	X PT. 6°05' RT.				
7+00		5.0	265.6	257.8	C70
7+50		6.3	264.3	256.8	C75
8+00		9.6	261.0	255.8	C52
+04 <sup>70</sup> +08 <sup>70</sup> +12 <sup>70</sup>	X PT. (87°51' LT.)	9.7	260.9	255.6	C53
8+25		10.0	260.6	255.4	C52
8+70		10.2	260.4	255.4	C50
9+10 <sup>70</sup>	X PT. (65°00' LT.)	10.3	260.3	255.4	C19
9+25		10.1	260.5	255.4	C51
9+50		9.2	261.4	256.4	C50
10+00		7.1	263.5	258.0	C55
10+50		6.6	264.0	259.5 258.4	C56 C45
10+63 <sup>60</sup>	End Existing 8" CI (X PT. 19°10' RT.)	7.0	263.6	259.8 258.6	C38
10+63 <sup>40</sup>		10.75	259.85		Bot. Exist 8" CI
P.	4.85	268.49	7.06	263.64	
			6.37	262.12 = 262.07	NAIL IN POLE

663.70  
1.41  
800.70

8+08<sup>70</sup>  
6+25<sup>70</sup>  
183<sup>70</sup>



Pepper Drive  
Cont'd  
WATER METERS

2/8/53

28

1+56 <sup>5</sup> Sly.	2+31 +2.6	276.0	272.7	C2 <sup>3</sup>	4127	Pepper	143'
13' <sup>wly</sup> from BC. Sly.	2+31 +1.2	274.8	272.8	C2 <sup>0</sup>	4141	Pepper	194'
21 <sup>5</sup> <sup>Ely</sup> from PRC. Sly.	3+32 -0.5	269.8	270.6	F0 <sup>8</sup>	4133	"	280'
3' <sup>Ely</sup> from PRC. Nly.	2+32 +1.0	271.9	269.5	C1 <sup>8</sup> ✓	4127	"	298'
3' <sup>wly</sup> from PRC Sly.	2+32 -0.6 -0.1	269.7 270.2	269.8	F0 <sup>1</sup> ✓	4132	"	325'
35' <sup>wly</sup> PRC Nly	3+32 -1.1 4+12 -0.3	269.2 268.7	268.8	C0 <sup>4</sup>	4130	"	336'
66' <sup>wly</sup> PRC Nly.	4+12 -0.2	268.8	268.0	C0 <sup>2</sup>	4124	"	367'
98' <sup>wly</sup> PRC Sly	4+12 0.0	269.0	267.9	C1 <sup>1</sup> ✓	4121	"	399'
133' <sup>wly</sup> PRC Nly.	4+12 -0.7	268.3	266.8	C1 <sup>5</sup> ✓	4120	"	434'
149 <sup>5</sup> <sup>wly</sup> PRC Nly.	5+50 +1.9	267.8	266.9	C1 <sup>5</sup> ✓	4116	"	450'
205 <sup>5</sup> <sup>wly</sup> PRC Nly.	5+50 +0.2	266.1	265.2	C0 <sup>9</sup> ✓	4110	"	507'
285 <sup>5</sup> <sup>wly</sup> PRC Nly.	6+26 <sup>5</sup> 0.0	265.2	263.6	C1 <sup>6</sup> ✓	4102	"	587'







50<sup>TH</sup> ST.  
UNIVERSITY To WIGHTMAN  
⑥ STKS & GRADES FOR 8" WATER

FEB. 18, 1953  
BEATTY  
KEMP  
ALEXANDER

20.

BM.	0.88	331.03		330.15	Grade Bot. Pipe	BR SWly. Cor. 50 <sup>TH</sup> ST & UNIVERSITY	
0+05	Begin Work		1.8	329.2	325.8	C34	✓
+50			2.4	328.6	324.3 324.8	C38 C42	✓
+75			2.7	328.3	323.5 322.3	C40 C48	✓
1+00			3.5	327.5	322.0 322.8	C47 C55	✓
+50			6.5	324.5	318.8 319.7	C48 C57	
2+00			9.5	321.5	315.6 316.6	C49 C59	
IP	2+038 P.L. EN						
+50	0.22	318.52	12.73	318.30	312.5 313.5	C48 C58	
3+00			3.7	314.8	309.4 309.2 310.4	C44 C56 C54	✓
+25			6.0	312.5	307.0 308.9	C36 C55	✓
IP +50			9.2	309.3	306.7	3050 C26 C43	
4+00	0.54	305.91	13.17	305.37	302.2	300.7 C23 C37	
+50			1.5	304.4	296.1 297.2 299.2	C36 C54 C65	
5+00			4.2	301.7	291.4 293.7	C80 C103	
+50			(Replaced) 8.8	297.1	285.8	C92 C87 C113	
			8.2	297.7	288.4		
6+00	2.93	295.64	13.20	292.71	280.4 283.0	C97 C123	
+50			9.5	286.1	277.0 279.8	C63 C91	
6+65	END WORK		10.7	284.9	276.0 279.3	C55 C89 C88	
SET IP on 2 <sup>ND</sup> P.			4.75	290.89			
IP	12.59	308.23	0.00	295.64			
IP	13.43	321.57	0.09	308.14			
IP	11.62	333.13	0.06	321.51			
OK BM			2.95	330.18 = 330.18			

GRD LINE  
328.1  
2.4  
327.3  
2.7  
324.2  
2.8  
320.5  
10.5

NOTE:  
GRADE REVISED  
TO HAVE SURRENDER  
COVER  
STA 2150 - 2100  
GRADE REVISED  
DUE TO REVISIONS  
OF EST. GRD OF  
PLANS.

286.1  
1.3  
284.8  
276.0  
8.8

Replaced



50TH ST  
(Cont'd)  
WATER METERS.

2/24/58

31

0+77 = EC Prop E SIDE

0+02 W	0+05		329.4		4985 UNIV.	
0+26 W	+1.0	330.2	329.1	C1 <sup>1</sup>	3890 50 <sup>TH</sup>	
0+69 W	+0.2	329.4	327.6	C1 <sup>8</sup>	3886(?) 50 <sup>TH</sup>	
1+33 W	1+50	+2.2	326.7	324.6	C2 <sup>1</sup>	3872 50 <sup>TH</sup>
1+68 E	1+50	-0.2	324.3	321.9	C2 <sup>4</sup>	3865 50 <sup>TH</sup>
1+84 W	1+50	-0.9	323.6	321.3	C2 <sup>3</sup>	3868 50 <sup>TH</sup>
2+20 E	2+00	-0.9	320.6	318.7	C1 <sup>9</sup>	3859 50 <sup>TH</sup>
2+26 W	2+00	-1.5	320.0	318.6	C1 <sup>4</sup>	3860 50 <sup>TH</sup>
2+55 E	2+50	+0.3	318.6	316.4	C2 <sup>2</sup>	3853 50 <sup>TH</sup>
2+62 W	2+50	-1.8	316.5	316.2	C0 <sup>3</sup>	3854 50 <sup>TH</sup>
3+97 E	3+00	+0.3	304.7	306.9	F2 <sup>2</sup>	3839 50 <sup>TH</sup>
4+24 W	4+00	+2.8	307.2	305.3	C1 <sup>9</sup>	3834 50 <sup>TH</sup>
4+95 W	5+00	+3.6	305.3	296.8	C8 <sup>5</sup>	3822 50 <sup>TH</sup>
5+35 E	5+50	+1.9	299.0	291.0	C8 <sup>0</sup>	3811 50 <sup>TH</sup>
5+56 W	5+50	+3.8	300.9	289.2	C11 <sup>2</sup>	3810 50 <sup>TH</sup>
5+67 E	6+00	+3.9	296.6	287.6	C9 <sup>0</sup>	3805 50 <sup>TH</sup>

BR. MET. 20' FROM E ST.



FEB. 26 1953

32

BETTY  
MARTEL  
ALEXANDER

COMMERCIAL ST.  
30<sup>TH</sup> To 31<sup>ST</sup>  
② STKS & GRDS FOR WAT. METS.

(9523-L W.O. = 462.11)

BM 2.40 77.37 74.97 BR. NW COR 30<sup>TH</sup> & IMPERIAL0+00 = Ely Prop line 30<sup>TH</sup> ST.(BK of MET on So Prop line  
" " " 135 from Nor Prop line)

0+42 S. 4.1 73.3 721 C12

1+15 N. 4.8 72.6 724 C02

1+77.5 N. 4.8 72.6 724 C00

2+27 S. 2.1 73.3 727 C06

2+28 N. 4.6 72.8 728 C00

2+75 N. 4.0 73.4 729 C05

3+23 N. 3.8 73.6 730 C06

3+29 N. 4.07 73.3 731 C02

3+67 N. 3.8 73.6 732 C04

4+10 S. 6.20 79.27 4.30 73.07 734 C03

4+28 S. 5.57 73.7 734 C03

4+28 S. 5.5 73.8 735 C03

4+43 N. 5.3 74.0 735 C05

5+01 S. 5.15 74.12 737 C04

4.30 77.33 6.24 73.03

0+30 N. 5.0 72.3 721 C02

0+86 } Staffs 4.8 72.5 723 C02

0+80 N. 79.27

5+05 N. 5.5 73.8 736 C02

5+13 (removed out of driveway)

CK. BM 2.40 74.93 = 74.97



ALLEY 157  
 CASS TO BAYARD  
 BETWEEN DIAMOND & EMERALD  
 (2) JTL'S & GRDS FOR WAT. METS

FEB. 26 1953

33.

BM. 4.02 34.94 30.92 S.W. CP. Diamond & Mission

4 8.63 42.54 1.03 33.91

0+00 = Wly Prop line Cass

0+02 S. 2.0 40.5 40.3 C02

0+24 N. 1.8 40.7 40.2 C05

0+51 N. 2.0 40.5 39.9 C06

1+01 S. 3.2 39.3 38.8 C05

1+03 N. 3.2 39.3 39.0 C03

1+28 N. 3.2 39.3 38.7 C06

1+52 S. 4.0 38.5 38.2 C03

1+55 N. 3.6 38.9 38.4 C05

2+00 S. 4.7 37.8 37.5 C03

2+24 N. 4.3 38.2 37.7 C05

2+71 S. 5.6 36.9 36.8 C01

2+80 N. 5.2 37.3 37.2 C01

2+86 S. 6.0 36.5 36.7 F02

3+15 N. 5.3 37.2 36.7 C05

3+25 S. 6.05 36.5 36.3 C02

3+76 N. 6.05 36.5 36.1 C04

3+95 S. 6.85 35.7 35.5 C03

4+27 S. 7.1 35.4 35.1 C03

4+32 N. 6.8 35.7 35.5 C02

4+56 S. 7.7 34.8 35.0 F02

4+79 N. 7.1 35.4 34.8 C06

5+00 N. 8.3 34.2 33.4 C08



2/26/53

34

## ALLEY BLK 156

MISSION TO BAYARD  
Between Diamond & Emerald.  
② STKS. & GRDS FOR WAT. METS.

42.5A

0+00 = Wly Prop. Line Bayard

0+20 N		8.55	34.0	33.9	CO <sup>1</sup>
0+48 S.		8.75	33.8	33.6	CO <sup>2</sup>
11)	0.72	34.63	8.63	33.91	
0+73 N.		0.95	33.7	33.7	CO <sup>0</sup>
0+76 S		1.1	33.5	33.3	CO <sup>2</sup>
0+80 N		1.1	33.5	33.6	FO <sup>1</sup>
1+04 S		1.1	33.5	33.0	CO <sup>5</sup>
1+37 N.		1.0	33.6	33.0	CO <sup>6</sup>
1+62 N		0.9	33.7	32.6	CI <sup>1</sup>
1+74 S.		2.4	32.2	32.2	CO <sup>0</sup>
1+85 N.		1.5	33.1	32.4	CO <sup>7</sup>
2+12 N.		2.5	32.1	31.9	CO <sup>2</sup>
2+26 S.		3.0	31.6	31.6	CO <sup>0</sup>
2+70 N		3.2	31.4	31.4	CO <sup>0</sup>
2+98 S.		3.6	31.0	30.8	CO <sup>2</sup>
3+09 S.		3.8	30.8	30.7	CO <sup>1</sup>
3+47 N.		3.8	30.8	30.5	CO <sup>3</sup>
3+69 N.		4.3	30.3	30.3	CO <sup>0</sup>
3+95 S		4.8	29.8	29.7	CO <sup>1</sup>
4+02 N		4.3	30.3	29.9	CO <sup>4</sup>
4+50 S		5.4	29.2	29.1	CO <sup>1</sup>
4+53 S.		5.1	29.5	29.0	CO <sup>5</sup>
ck BM		3.70	30.93	30.93	



ISLAND ST  
30<sup>TH</sup> TO 32<sup>ND</sup> ST.

⑥ STKS & GRDS for 6" WATER

Mar. 2, 1953

35.

RAIN  
2:20 pm

Beath  
Martell  
Alexander

BM 2.41 116.31 113.90 SW Cor. 30<sup>TH</sup> & Island

0+00

0+75<sup>2</sup> (Gv. in Conc. Pav't.)

0+85 Begn Work

80

2.55 113.7 109.7

115.0 C42

(Edge Conc. pav't. 0+80)

1+05

TP 1+30 0.30 103.33

7.5 108.8

105.0

C38

1+30

13.28 103.03

101.1

C36

1+65

6.6 112.7

97.6

C18

2+05

7.8 95.5

93.7

C18

2+50

9.7 93.6

90.2

C33

3+00

TP 0.86 90.83

11.5 91.8

86.6

C52

3+30

13.36 89.97

84.4

C55

3+55

2.0 88.8

83.7

C41

4+05

3.6 87.2

83.7

C35

4+50

4.5 86.3

82.9

C34

5+00

5.6 85.2

82.0

C32

+50

6.5 84.3

81.1

C32

6+00

7.3 83.5

80.2

C33

+50

8.1 82.7

79.3

C34

7+00

9.0 81.8

78.4

C34

+50

9.8 81.0

77.6

C34



15LAND ST.  
30<sup>th</sup> to 32<sup>nd</sup>  
(Cont'd.)

3/3/53

36

	90.83					
8+00		10.7	80.1	76.8	C33	
+55		11.3	79.5	75.8	C37	Tic SHEETS SHW
P +74	6.62	85.88				
+65	End work	11.57	79.26	75.8	C35	Aver & dist 30 <sup>th</sup> to 31 <sup>st</sup> 7' offset line 808.57
+35						14.
9+55	Begin work	6.7	79.2	75.8	C34	Prop line to pt. = 794.57
+50		6.5	79.4	75.9	C35	30 <sup>th</sup> 80
10+00		6.2	79.7	76.1	C36	Aver & dist 31 <sup>st</sup> to 30 <sup>th</sup> 7' offset line 614.55
+50		6.0	79.9	76.3	C36	14.00
						PL to PL 600.55
11+00		5.9	80.0	76.5	C35	31 <sup>st</sup> 60.
+50		5.6	80.3	76.7	C36	660.55
12+00		5.5	80.4	76.9	C35	874.57
+50		5.2	80.7	77.2	C35	1535.12
13+00		5.0	80.9	77.4	C35	
+50		4.8	81.1	77.6	C35	
14+00		4.6	81.3	77.8	C35	
+50		4.5	81.4	78.0	C34	
15+00		4.2	81.7	78.2	C35	
+30						
15+25	End work	3.7	82.2	78.4	C38	
P	5.24	87.22	3.90	81.98	83.18	OP Cor. Mon NE Cor inside PL 32 <sup>nd</sup> & Island
CR BM						OP SW Cor 32 <sup>nd</sup> & Market
	4.23	86.29	5.83	81.39 =	81.21	
			5.16	82.06		
			7.05	79.24		



Island St.  
Cont'd.  
WAT. MET. S

11631

1+10 N	3.45	112.8	112.0	CO <sup>8</sup>	505	3074
1+63 N	8.90	107.4	107.7	FO <sup>3</sup>	3006	Island
1+92 N	11.50	104.8	104.7	CO <sup>1</sup>	3014	Island
3+33 S	<u>90.57</u> 1.4	89.5	89.5	CO <sup>2</sup>	3037	Island
4+31 S	2.3	86.6	86.5	CO <sup>1</sup>	3041	Island
4+78 N	4.2	86.7	86.6	CO <sup>1</sup>	3026	Island
5+21 S	5.6	85.3	85.1	CO <sup>2</sup>	3049	Island
5+47 N	5.1	85.8	85.5	CO <sup>3</sup>	3050	Island

PK of MET 285 RT #LT & ST.

PK MET 445 LT

old curb 52'

12E RT of @ offset line



TULIP ST.  
 SYCAMORE TO JUNIPER  
 (2) STKS & GRDS. FOR WAT. METS

MAR. 3 1953  
 BEATTY  
 MARTELL  
 ALEXANDER

TBM.	3.10	265.17	262.07	NAIL IN P. Pole	See pg.	25' RT & LT & ST (2K of MET on Prop. line)
0+00 = BC W. SIDE		(Nor Cor Lot 27 BLK 29)				
0-03 W		1.6	263.6	261.7	C19	2416 TULIP
0+43 W.		2.27	262.9	260.7	C22	2410 TULIP
0+74 E.		4.87	260.3	259.5	C08	2409 TULIP
1+14 E		5.8	259.4	258.7	C07	2357 TULIP
1+20 W		3.67	261.5	259.1	C24	2414 TULIP
1+40 W.		5.7	260.0	258.7	C13	2344 TULIP
1+87 W.		6.17	259.0	257.7	C13	2404 TULIP
1+55 E		6.57	258.6	257.9	C07	2351 TULIP
2+00 E		8.5	256.7	256.9	F02	2345 TULIP
2+02 W		6.5	258.7	257.4	C13	2332 TULIP
2+89 E		10.5	254.7	255.1	F04	2325 "
2+96 W		9.37	255.8	255.4	C04	2318 "
3+42 E		11.0	254.2	253.9	C03	2319 "
3+84 E		10.87	254.3	253.2	C1	No Number
3+80 W.		11.07	254.1	253.7	C04	2308 TULIP
4+50 E		11.7	253.5	251.6	C19	2309 "
CK TBM.		3.10	262.07 = 262.07			



3/4/33

39

SAN BERNARDO TERR.  
 (2) STK'S & GRADES FOR  
 WATER METS

BM 183 185.23 183.40

NW CP. San Jacinto & San Bernardo

0+00 = EC NE Cor San Bernardo  
 San Jacinto

0+09 N		2.5	182.7	182.1	C06	526	San Jacinto
0+66 N		4.1	181.1	181.1	C08	5324	San Bernardo
1+26 S		5.3	179.9	179.7	C02	5305	"
1+16 N		5.2	180.00	180.1	F01	5312	"
1+78 N		5.6	179.6	179.0	C06	5306	"
2+38 N		6.1	179.1	178.1	C10	5292	"
2+98 N		7.3	177.9	177.1	C08	5286	"

11 0.17 173.61 11.79 173.44

0+00 = NEly Cor Lot 4  
 Blk 20..

0+45 S		1.2	172.4	172.7	F03	5265	"
0+63 S		2.1	171.5	172.3	F08	5259	"
1+65 S		9.8	163.8	165.5	F12	5251	"
1+92 S	?	12.7	160.9	162.1	F12	5243	"

11 0.20 162.01 12.00 161.61

Nail in Pole

11 8.15 158.77 11.39 150.62



## LA PAZ ST

② STR. 5 & GROSS FOR  
WATER METS.

CR 13M 2.94 183.35 = 183.60

4.10 186.29 0.14 182.19

0+00 - EC NEly Cr La Paz & San Bernardo

0+79<sup>3</sup> Ely (45 from PL) 8.6 173.7 173.2

11.16 182.33 0.26 171.17

2+21 Nly 5.5 165.9 165.8

2+59<sup>2</sup> S 7.7 163.7 164.0

2+80 Nly 9.4 162.0 162.7

3+19<sup>0</sup> S 10.3 161.1 161.1

3+50<sup>5</sup> N 12.2 159.2 159.7

3+78<sup>5</sup> S 12.0 159.2 158.0

3+97 B.C. " 12.6 158.8 # 157.9

4+08 S.F.H. (4.8K) 13.05 171.43 0.39 158.38

4+16 N. 19 2.3 156.5 157.3

4+36 S. 39 2.3 156.5 157.0

4+74 N. 77 3.8 155.0 155.1

4+93 S. 96 3.9 154.9 154.8

5+37 N. 140 5.6 153.2 152.9

5+49 S. 152 6.1 152.7 153.0

6+07 N. 210 8.5 150.3 150.3

6+17 S. 220 (moved 4 eastly) 7.5 151.3 150.5

6+37 N. 240 (from Orig. loc.) 8.8 150.0 149.6

6+53 S. 256 9.6 149.2 149.3

158.77

3/9/53

do.

Note: Level Note go up the page

BP. NW Cor San Bernardo  
San Jacinto

CO5 5293 LA PAZ

CO1 5274 " "

FO3 5263 " "

FO2 5266 " "

CO0 5255 " "

FO5 5260 " "

C14 5249 " "

CO9 C42

FO8 5252 " "

FO5 5241 " "

FO1 5246 " "

CO1 5233 " "

CO3 5238 " "

FO3 5225 " "

CO0 5232 " "

CO8 5217 " "

CO4 5226 " "

FO1 5209 " "



So. BANCROFT  
 OCEAN VIEW TO WEBSTER  
 (4) STK.S & GRDS FOR 8" WATER

MAR 5 1953  
 BETTY  
 MARTELL

41

BM.	12.02	48.25			36.23	
0+00	(at Gr. Edge (conc part))	15.5	32.8	29.4		C34
+50		12.5	35.8	32.4		C34
1+00		9.5	38.8	35.3		C35
+50		6.2	42.1	38.3		C38
2+00		2.95	45.3	41.2		C41
(11)	13.31	61.24	0.12	48.13		
+50			11.9	49.5	45.8	C37
3+00			6.4	56.0	51.0	C50
+50			2.9	58.5	54.5	C40
+75			1.6	59.8	56.3	C35
(11)	13.40	74.70	0.14	61.30		
4+00			13.0	61.7	57.8	C39
+50			2.9	66.8	63.5	C33
5+00			2.7	72.0	69.0	
(11)	1.94	76.19	0.25	74.25	69.3	C27 C30
+50			0.8	75.4	72.3	C31
6+00			0.2	76.0	72.8	C32
+50			2.4	73.8	70.2	C36
7+00			5.3	70.9	67.6	C33
<sup>10</sup> +15	8" TEE		5.8	70.4	67.1	C33
+50			2.7	68.5	65.0	C35



So. BANCROFT ST.  
(Cont'd.)

3/5/53

42

	76.19					
8+00		10.4	65.8	62.5	C33	
+25		11.8	64.4	61.2	C32	
P +50	2.19	65.80	12.58	63.61	60.6	C30 ?
9+00		3.7	62.1	59.4	C22	C32
+50		4.6	61.2	58.1	C31	
10+00		5.7	60.1	56.9	C32	
+50		6.6	59.2	55.6	C36	
10+87		6.7	59.1	55.6	C35	} IDENTICAL
10+91 = 90° LT. 8" TEE				55.6	C35	
10+95						
11+26 = 5' Ely from GV.		5.7	60.1	57.4	C37	
P	10.41	76.19	0.02	65.78		
P	0.08	63.85	12.42	63.77		
P	0.18	50.99	13.04	50.81		
P	0.05	42.05	8.99	42.00		
CK BM		5.77	76.28	= 36.23		



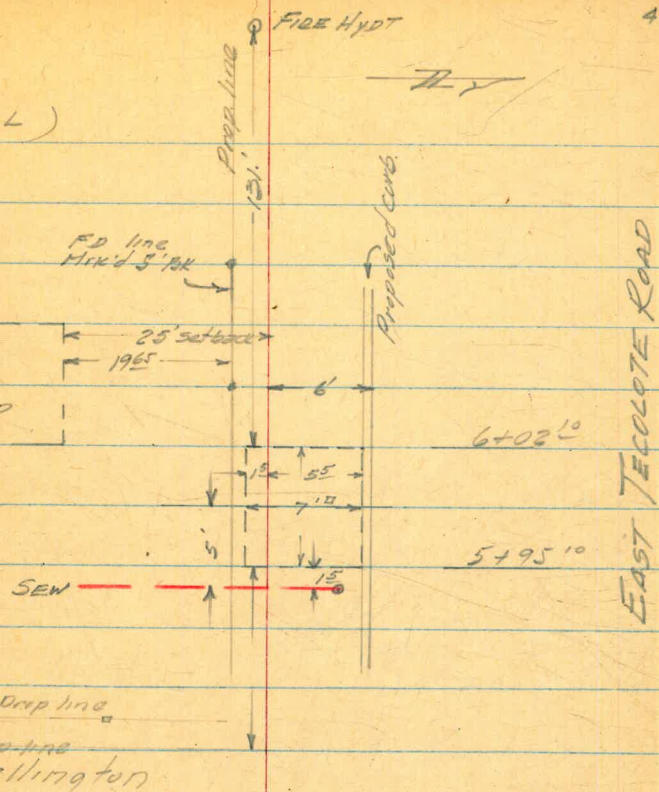
METER VAULTS AT LINDA VISTA SCHOOL

U.O. 29004

VAULT #1

(9174-L)

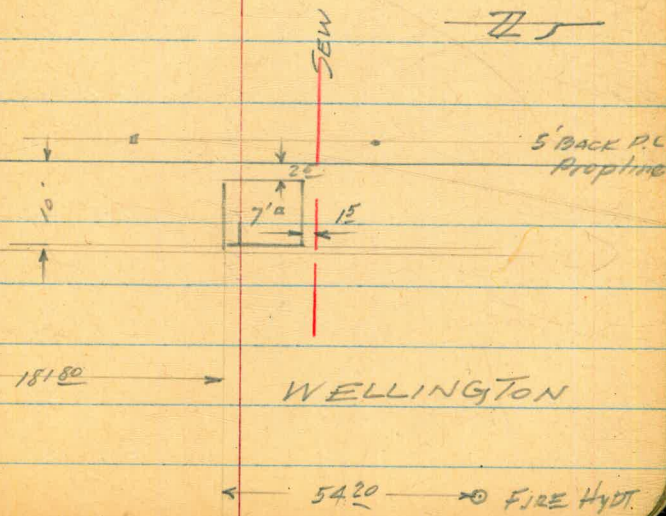
BM	5.80	366.28	360.48	NAIL IN Pole
③ NE COR. = 275° Wly	3.63	362.65	362.3	C035
③ NW COR. = 282° Wly	3.40	362.88	362.4	C048
Wly Prop Line Wellington.				
③ SW COR	3.34	362.92	362.4	C054
③ SE COR.	3.40	362.88	362.3	C058
(6+10)	3.43	362.85	C05	✓



(U.O. 29005)

VAULT #2

BM	0.82	361.32	360.48	
NE	9.75	351.57	352.4	F083
SE	9.80	351.52	352.3	F078
SW	9.91	351.41	352.3	F089
NW	10.38	350.94	352.4	F146
(8+50)	10.0	351.32	F10	✓





Mar. 9, 1933

44

"F" ST.  
30<sup>TH</sup> to 28<sup>TH</sup>  
© STR. & GRDS FOR 6" WATER

B.M.	0.85	188.48		187.63				
B.M.	0.28	175.39	13.37	175.11				
B.M.	2.33	169.25	8.95	166.44	166.92			
		168.77						
0+60	Begin work			167.1	163.7			
	Wly Prop. Line 30 <sup>TH</sup> St		1.7	167.6	164.2	C3A	Existing G.V.	2° LT. of line
1+00			2.0	166.5	163.2	C3B		
				167.3	163.7			
1+50			2.7	166.1	162.5	C3C		
				166.6	163.0			
2+00			4.4	164.4	160.7	C3D		
				162.9	161.2			
2+25			5.8	163.0	159.9	C3E		
				162.5	160.4			
2+50			7.6	161.2	157.8	C3F		
				161.7	158.3			
3+00			11.8	157.5	153.5	C3G		
				157.5	154.0			
3+50	0.06	155.63	13.20	156.05	155.57	C3H		
		156.11						
4+00			3.1	153.0	149.7	C3I		
				152.5	149.2			
4+50			7.1	148.5	144.9	C3J		
				148.0	145.4			
5+00			10.1	145.5	140.5	C3K		
				146.0	141.0			
5+50			12.3	143.3	137.5	C3L		
				143.8	138.0			
6+00			13.4	142.2	137.5	C3M		
				142.7	138.0			
6+30			12.1	143.5	139.5	C3N		
				144.0	140.0			
6+55	F.H. TEE		10.5	145.1	141.7	C3O		
				145.6	142.2			
6+60			9.0	146.6	143.5	C3P		
				147.1	144.0			
6+90			8.7	146.9	143.9	C3Q		
				147.4	144.4			
7+20			6.9	148.7	145.4	C3R		
				149.2	145.9			
			5.2	150.4	146.9	C3S		
				150.9	147.4			

B.P. NW Cor 30<sup>TH</sup> & E

CITY ENR. CK 1652-40  
(CK 818 E ST.)

247 W. Curb SE Cor 30<sup>TH</sup> & E

167.5

NOTE:-

GROUND LINE & PIPE  
IS SHOWN AS ©  
EXCEPT AS SHOWN.

148.18  
+45.66 El. (S) Gnd 147.6 C05 C45  
7.45



"F" ST.  
(Cont'd.)

3/9/53

45

		<del>156.11</del> 155.63		152.8 <del>152.3</del>	149.3 149.8			
7+50			2.8			C35		
①	13.35	<del>169.31</del> 168.83	0.15	<del>155.96</del> 155.46				
8+00			10.6	158.7 158.2	154.6 154.1			C41
8+50			5.4	<del>163.4</del> 163.9	160.6 160.1			C33
9+00			1.5	167.3 167.8	164.5 164.0			C33
9+50			0.1	168.7 169.2	165.0 165.5			C32
10+00			1.9	160.9 167.4	163.9 164.5			C30
10+50			5.8	163.0 163.5	160.0 160.6			C30
①		156.73		156.63	153.6			C30
①	0.10	<del>157.91</del>	12.20	<del>157.11</del>	<del>164.4</del>			C30
11+50			5.7	151.0 151.5	147.2 147.7			C38
①		145.10		144.25	141.3			C30
①	0.85	<del>145.58</del>	12.48	<del>144.73</del>	<del>142.1</del>			C30
12+50			6.5	138.6 139.1	135.0 135.9			C36
							138.2 6.9	
12+80			9.8	135.3 135.8	132.0 132.2			C33
12+95				131.9	131.5			C34
①			10.2	<del>135.4</del>	<del>132.0</del>			C34
								Existing GV on RT. of line
①	13.37	148.46 148.94	10.01	135.57	135.09			Top. G.V. cover
①	12.31	160.55 161.03	0.22	148.24 148.72				
CK BM			2.72	157.83 158.31	= 157.80			130 SE 28 <sup>th</sup> E (BK 818)



F. ST.  
Cont'd  
WAT METS STD

3/9/53

46

7+23 S	156.11 Hi. 155.6	4.95	150.6	150.4	CO <sub>2</sub>	2887 F
10+40 S	Hi. 169.31 168.83	3.80	165.0	165.1	FO <sub>2</sub>	2843 F
10+40 N	Hi 169.31	2.90	165.9	165.6	CO <sub>2</sub>	2836 F
10+76 N	Hi 169.31	6.60	162.2	161.9	CO <sub>2</sub>	2826 F
10+73 S	169.31	7.30	161.5	161.8	FO <sub>2</sub>	2825 F



ALLEY BIK H #1  
 From ORANGE To EL CAJON  
 Between 33<sup>rd</sup> & FELTON

Mar 10, 1952

27

BM	7.85	374.51	366.66	BP NW Cor 33 <sup>rd</sup> & ORANGE	(Looks as if this has been done before.)
0+00	= Nly Propline ORANGE				
0+35 W	3.9	370.6	370.1	C05	
0+37 E	3.3	371.2	370.2	C10	
0+74 W	2.6	371.9	371.0	C09	
1+28 W	1.6	372.9	372.3	C06	
1+31 E	1.4	373.1	372.3	C08	
1+48 W	1.5	373.0	372.5	C05	
1+72 W	1.4	373.1	372.7	C04	
1+72 E	5.27	378.76	1.02 373.49	C09	
2+21 E	5.1	373.7	372.8	C09	
2+42 W	4.5	374.3	372.9	C14	
2+42 W	5.3	373.5	372.9	C08	
2+83 E	4.2	374.6	373.0	C16	
3+00 W	5.2	373.6	373.1	C05	
3+06 E	4.4	374.4	373.1	C13	
3+43 E	4.8	374.0	373.2	C08	
3+45 W	4.5	374.3	373.2	C12 = 3+01 W	
3+81 E	4.6	374.2	373.4	C08	
3+98 W	4.6	374.2	373.4	C08	
4+02 W	4.6	374.2	373.4	C08	
ck 9	2.29	374.47 = 374.45		Nail in pole.	
4+20 E	4.7	374.1	373.5	C06	
4+35 W	4.9	373.9	373.5	C04	
4+76 W	4.7	374.1	373.6	C05	
4+93 E	4.2	374.6	373.8	C08	
5+37 W	4.5	374.3	374.1	C02	
5+54 E	3.8	375.0	374.3	C07	



GRAND AVE  
BOND ST. Wly. to PRIVATE ST  
STKS & GRDS For 8" C.I. WATER

Mar. 13, 1953  
BEATTY  
MARTELL  
ALEXANDER

48

TBM	434	09.47 <del>09.27</del>	05.13 <del>04.93</del>	Nail in Pa. Pole #2461
			Pipe Elev	
0+00		5.05	04.42 <del>04.22</del>	-0.25 C45 C47
0+37.5	} 8" TIE	4.67	04.8 <del>04.6</del>	-0.50 C51 C53
0+37.5		4.47	05.0 <del>04.8</del>	-0.50 C535 C54 C55 C55
0+75	Wly Prop line Bond St.	4.31	05.2 <del>05.0</del>	-0.50 C56 C58 C52
0+75	Wly Prop line Bond St.	4.77	04.7 <del>04.5</del>	-0.50 C58 C55 C52
1+00		4.87	04.60 <del>04.40</del>	-0.50 C55 C57 C51
1+50		5.0	04.5 <del>04.3</del>	-0.50 C57 C59 C50
2+00		5.0	04.5 <del>04.3</del>	-0.50 C62 C62 C50
2+50		4.8	04.7 <del>04.5</del>	-0.50 C65 C67 C52
3+00		4.87	04.6 <del>04.4</del>	-0.50 C67 C69 C51
3+50		4.9	04.6 <del>04.4</del>	-0.50 C70 C72 C51
4+00		5.77	03.7 <del>03.5</del>	-0.50 C64 C66 C42
4+50		6.07	03.4 <del>03.2</del>	-0.50 C64 C66 C39
5+00		6.87	02.6 <del>02.4</del>	-0.50 C59 C61 C31
5+50		5.57	03.9 <del>03.7</del>	-0.50 C75 C77 C44
6+00		6.20	08.81 <del>08.61</del>	-0.50 C65 C67 C31
6+17.5	6.20	6.86	02.91 <del>02.71</del>	-0.50 C65 C67 C31
6+47.5		13.11	-0.3 <del>-0.5</del>	-6.00 C65 C57 C53 C17

NOTE: - Elev marked on pole in error as subsequent check shows see pg 50

NOTE: - 0437.5 to 0437.7  
GRD Revised per Huntington  
3/16/53



3/13/53

49

GRAND AVE  
Cont'd.

		08.61 08.81							
7+6750			10.3	-01.5 -01.7	-6.00 -02.55	<del>c785</del>	<del>c79</del>	<del>c81</del>	<del>c45</del>
8+00			5.1	+03.7 +03.5	-1.10 -03.25	<del>c675</del>	<del>c68</del>	<del>c72</del>	<del>c48</del>
8+375			2.7	+06.1 +05.9	+03.95	<del>c205</del>	<del>c21</del>	<del>c22</del>	
+50			2.3	06.5 06.3	03.90	<del>c24</del>	<del>c25</del>		
9+00			2.3	06.5 06.3	03.70	<del>c27</del>	<del>c28</del>		
+50			2.6	06.2 06.0	03.50	<del>c25</del>	<del>c27</del>		
10+00	F.H. TEE		2.3	06.5 06.3	03.30	<del>c30</del>	<del>c32</del>		
+50			2.9	05.9 05.7	03.10	<del>c26</del>	<del>c28</del>		
11+00			2.7	06.1 05.9	02.9	<del>c32</del>	<del>c32</del>		
+50		09.41 09.21	3.40	06.01 05.81	02.7	<del>c31</del>	<del>c33</del>		
12+00			3.0	06.4 06.2	02.5	<del>c37</del>	<del>c39</del>		
+295	TEE		3.0	06.4 06.2	02.4	<del>c38</del>	<del>c40</del>		
+50			3.2	06.2 06.0	02.3	<del>c37</del>	<del>c39</del>		
13+00			3.2	06.2 06.0	02.1	<del>c38</del>	<del>c41</del>		
+50			3.2	06.2 06.0	01.9	<del>c41</del>	<del>c43</del>		
14+00			3.2	06.2 06.0	01.7	<del>c43</del>	<del>c45</del>		
+50			3.0	06.4 06.2	01.5	<del>c47</del>	<del>c49</del>		
+645	F.H. TEE		3.2	06.2 06.0	01.4	<del>c46</del>	<del>c48</del>		

GAD 02.00  
 El. 06.65 F035 c32  
 2.16  
 E 165 from (3) pipe  
 = 265 from South prop. line Grand

E F.H. 165 from (3) pipe  
 = 265 from S. prop. line



GRAND AVE  
(CONT'D.)

2/16/53

50

14+90 15+00		<del>89.21</del> 09.41	3.7	05.7 <del>05.9</del>	01.4	cut C43
15+39.5	3" B.O.		5.5	03.9 <del>03.7</del>	01.30	cut C26
IP 2" i.p.	7.95	11.38 <del>4.18</del>	5.98	03.43 <del>03.23</del>		
IP	11.45	20.63 <del>20.43</del>	2.20	09.18 <del>08.98</del>		
IP	11.91	32.15 <del>31.95</del>	0.39	20.24 <del>20.04</del>		
IP	8.65	40.31 <del>40.11</del>	0.29	31.66 <del>31.46</del>		
CK BM.			3.20	36.91 <del>36.71</del>	= 36.92	
BM	0.03	36.95		36.92		
IP	0.26	24.70	12.51	24.44		
IP	0.48	13.85	11.33	13.37		
IP	5.56	11.63	7.78	06.07		
CK IP 2" i.p.			8.17	09.46	= 03.23	-0.23 diff
			6.50	05.13	= 02.93	0.20 diff

20.04  
08.98  
11.06

-11.52  
+ .49  
11.03

IP. N.W. Cor. Garnet & Pendleton St.  
0.71 diff



OREGON ST DL  
 REVISED GRADE, BACK of SIDEWALK

2/28/53

51

TBM	2.78	377.89	375.11	
6+16 <sup>35</sup> AT BC Curb Ret.	4.21	372.68	372.68	Curb
6+00	4.32	372.57		
5+50	4.67	372.22		
5+16 <sup>35</sup>	4.91	372.98	372.90	Curb
5+00	5.14	372.75		
4+50	5.84	372.05		
4+00	6.54	371.35		
3+50	7.24	370.65		
CK BM	2.78	375.11		

.007 per ft

AS per 4880-B  
 Received 3/25/53

.012 per ft



OREGON ST. PL  
 CURB RETURNS STKD & GRADED  
 OREGON & HOWARD

2/25/53

52

AS PER 4882-B

TBM	7.57	382.68	375.11		
BC	}	9.28	373.40	373.60	F020
SE Cor.		6.86	375.82	373.70	C212
EC		4.06	378.62	373.80	C482
FC	}	7.70	374.98	374.10	C088
NE Cor		8.38	374.30	374.05	C025
B.C.	}	8.41	374.27	374.05	C022
Cor sidewalk		outside 8.29	374.39		
		mark 8.25	374.43		
CK TBM		7.57			
Top 4" Conc. pipe		8.43	374.25		

TBM	4.51	379.62	375.11		
		5.04	374.58	370.82	C376
				374.40	
				3.58	
				370.82	FIX FLOOR AV CHAMBER



OREGON ST. PIPE LINE  
 So. of OLD UNIV. HEIGHTS RES.  
 (IN ATHLETIC FIELD)  
 STKS & GRDS for 30" & 24" C.I. WATER

3-19-53

53

BEATTY  
 MARTELL  
 ALEXANDER

TBM 6.09 375.96  
 CK 7.91 372.24 11.63 369.87  
 364.33 = 364.33

Cor Ret. Wall S.W. Cor Univ Heights Res  
 2<sup>nd</sup> Top SW Cor Oregon & Folk (1953 FB. 794)

				GRADE		CR. GRD & PIPE	
0+00	E. End	36" TEE	5.20	367.04	360.00	C704	(10' offset So. 367.0 5.2
"	"	"	4.94	367.30	"	C730	(6" Nor
0+02 <sup>42</sup>			5.20	367.04	360.25	C68	(10' offset So. 367.1 5.1
"	"		4.87	367.37	"	C71	(7" Nor
0+00			4.77	367.47	360.95	C65	(10" So. 367.5 4.7
"	"		4.37	367.87	"	C69	(15" Nor
0+80			4.48	367.76	361.71 367.95	C605↑ C58↓	(10" S 367.9 4.3
"	"		3.90	368.34	"	C67↑ C64↓	(24" Nor
1+20			3.96	368.28	362.72	C555	(10" S 368.2 4.0
"	"		3.50	368.74	"	C60	(33" Nor
1+38 <sup>33</sup>	W Edge	36" RCP	3.70	368.54	363.05	C55	(10" S 368.6 3.6
"	"	"	3.29	368.95	"	C59	(37" Nor

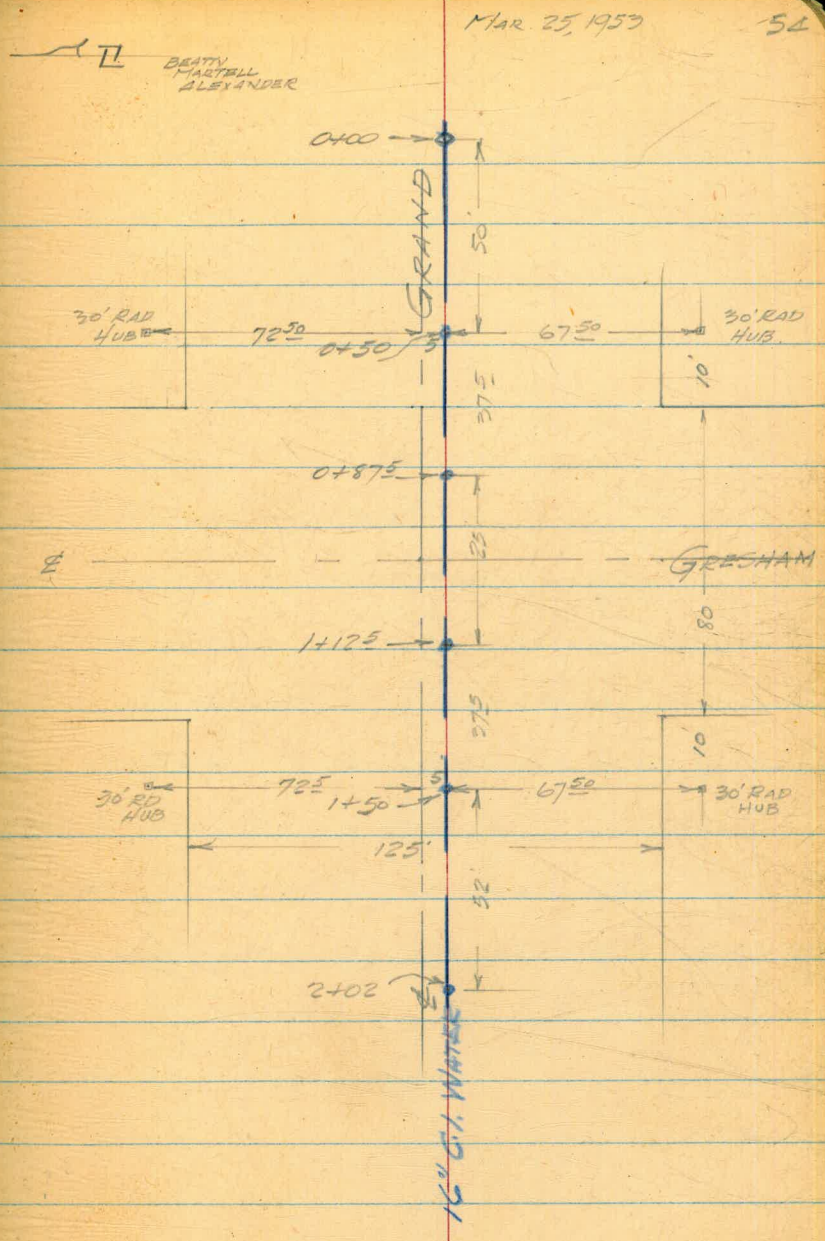
TBM	3.81	373.68	2.37	369.87	9.20	362.18	E PIPE
NE Cor (5)			4.86	368.82	361.50	C732	
SE Cor (5)			5.12	368.56	361.40	C716	
SW Cor (5)			5.25	368.43	361.45	C700	
NW Cor (5)			4.94	368.74	361.50	C725	
			5.15	368.53	368.54		

3/25/53 Valve Chamber Stud.



PROFILE  
TOP 16" C.I. WATER  
GRAND AVE  
AT GRESHAM

IP	5.22	47.90	42.68
		4.23	43.67
0+00	Top 16" C.I.	3.90	44.00
	Ground line	2.50	45.40
0+50	Top 16" C.I.	4.78	43.12
	FIN PAVT GRD		44.00
	Ground line	3.73	44.17
0+87.5	Top 16" C.I.	5.50	42.40
	FIN PAVT GRD		42.95
	GRD line	4.63	43.27
1+125	Top 16" C.I.	5.70	42.20
	FIN PAVT GRD		42.56
	GRD line	5.10	42.80
1+50	Top 16" C.I.	6.18	41.72
	FIN PAVT GRD		42.33
	GRD line	5.00	42.90
2+02	Top 16" C.I.	7.26	40.64
	GRD line	5.65	42.25
CK BM		2.26	45.56
		64	45.50



See 9331-L  
(For FIN GRD OF PAVT)



OREGON ST PIPELINE  
GRADES SET  
FOR Edge of  
PAV'T Replacement  
(05) of 195 ELY & ST

April 13 1953 55

B.M.	450	379.61	375.11
		6.60	373.01
		6.02	373.57
B.C. Howard St	5.48	374.13	
	4.93	374.68	
	4.91	374.70	
	5.04	374.57	
	5.07	374.54	
	5.26	374.35	
	5.12	374.49	
	5.11	374.50	
	5.40	374.17	

GRADES  
RAKED  
IN

T.B.M.	353	378.64	4.50	375.11
0-35	35' Sly. B.C.	NE Cor Howard	5.25	373.39 = 373.40
		SW 11.2 RT	4.26	372.38
		PAV. 12.6 LT	4.34	372.30
0+00	B.C.	Header	4.71	372.93 = 372.96
		SW 11.6 RT	4.20	372.44
		PAV. 12.6 LT	4.33	372.31
0+50		Header	4.61	372.63
		SW 11.5 RT	4.07	372.57
1+00		PAV. 12.2 LT	4.11	372.53
		Header	4.53	372.11
1+50		SW 11.4 RT	3.97	372.67
		Con. Pav. 12.5 LT	4.04	372.60
		Header	4.42	372.22
2+00		SW RT	3.97	372.67
		11' LT	4.32	372.32
		Header	4.35	372.39
2+50		SW 11.5 RT	3.78	372.86
		11.0 LT	3.78	372.88
		Header	4.25	372.39

pt of Gutter 6' Nly of EC SE COR  
" " " 23' Sly of Nly prop line  
E ST Gutter Eurb W. SIDE ST.  
374.61 373.85 372.35 373.41

375.15 374.41 372.91 ✓  
Top Conc Pav

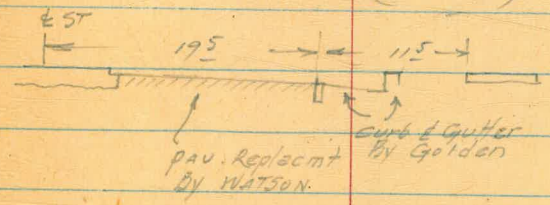
on R.H. NAIL  
on P.C.  
on Conc

E Side Fin. AV. Chamber

W side Fin. AV. Chamber

Give top for pav't app. Chamber

CHECK on Header for Conc PAV'T  
(4-16-53) Replacmt.



2+91.50	on Header	3.97	372.67
	PAV. 21.2	3.71	372.93
	3.95 LT	3.91	372.73
2+75.3	Sly Edge VAL. CHAMBER	Header	4.13
			372.51 = 372.51



THOMAS, JT  
 KENDALL To JEWELL  
 (2) STKS. & GROS. FOR WATER METS

April 13, 1953  
 BEATTY  
 MARTELL  
 ALEXANDER

56

BM						
	10.44	62.28	51.84			
0+42 So.		6.20	55.9	55.5	C04	
0+47 Nor.		5.14	57.14	55.6	C15	
0+78 Nor.		6.02	56.3	55.9	C04	
1+06 Nor.		3.98	58.3	56.2	C21	
1+11 So.		4.78	57.50	56.2	C13	
1+36 Nor.		4.28	58.0	56.3	C17	
2+08 So.		4.08	58.2	56.6	C16	
2+30 Nor.		4.35	57.9	56.2	C17	
2+49 So.		3.98	58.3	56.5	C18	
2+79 Nor.		5.28	57.0	55.7	C13	
3+03 So.		3.78	58.5	56.1	C24	
3+28 Nor.		5.4	56.9	55.0	C19	
3+38 So.		4.2	58.1	55.7	C24	
4+03 So.		6.7	55.6	53.3	C23	
4+26 Nor.		11.7	50.6	51.2	F06	
4+28 So.		8.22	54.1	52.2	C19	
4+70 So.		11.2	51.1	50.3	C08	
4+86 Nor.		14.45	47.8	48.6	F08	
	3.68	59.11	6.85	55.43		
			5.98	53.13		

(W.O. 46211) (9779-6)

NW 1/4 Grand & Jewell

(BK of MET - 225 from & ST  
 175 " Prop line)

12.68  
 77  
 10 45

55.43 TD  
 5.80  
 61.23 LL  
 9.38  
 51.85 = 51.84 OK

- 7' off the Kendall & Thomas



TUSTIN ST.

② STKS &amp; GRDS FOR WAT. MET.

April 20, 1953

57

Beatty,  
MARTIN  
ALEXANDER

(9137-6)

BK. of MET. 25' from E ST

NAIL IN POLE NWLY. Cor. MACAULEY &amp; TUSTIN

BM	2.16	150.85		128.69					
0+00-									
0+45 NWly			1.70	149.15	148.1	C11			1812 TUSTIN
1+13 "			8.0	142.85	142.3	C06			1820 "
1+30 Sely			11.05	139.8	138.9	C09			1821 "
① 1+70 Sely	0.98	139.26	12.37	138.48			(1+40 = 137.26)	C10	1825 "
1+71 NWly			3.6	135.9	134.2	C12			1830 "
2+32 Sely			12.2	127.3	125.7	C16			1833 "
① 2+52 Sely	1.22	128.45	12.23	127.23				C15	1839 "
2+52 Sely			3.70	124.75	122.9				
2+83 Sely			2.78	120.7	119.3	C14			1845 "
① 3+22 Sely	0.92	116.24	13.13	115.32					
3+22 Sely			0.9	115.3	114.3	C12			1851 "
3+67 Sely			6.4	109.8	108.7	C11			1857 "
4+10 Sely			10.84	105.4	105.0	C04			1863 "
4+36 NWly			11.06	105.2	104.3	C09			
4+44 Sely			13.34	102.9	103.0	F01			1869 "
			13.73	102.51	= 102.07				
									NAIL IN Pole SE Cor. OLIPTAOT & TUSTIN



## NEWTON AVE

331' Wly of 43rd to 7' Wly of 43rd

④ STKS &amp; GRDS. for 6" WATER

BM	0.14	70.83	70.69		
BM	5.19	70.77	65.58		
IP	2.91	60.98	12.70	58.07	
0+00	= 331' Wly W.P.L. 43rd		2.9	58.1	55.0
+27	F.H. TEE		3.6	57.4	53.7
+50			4.7	56.3	52.6
1+00			7.3	52.7	50.2
IP	1.35	49.26	12.87	48.11	
+50			1.2	48.3	44.0
2+00			7.3	42.2	38.4
IP	1.25	37.68	13.04	36.42	32.8
3+00			6.0	31.7	27.2
+50			9.9	27.8	24.0
3+82			12.3	25.4	22.8
IP	11.97	49.40	0.25	37.43	
IP	11.68	60.79	0.29	49.11	
IP	8.81	68.26	1.34	59.45	
CK BM:			2.67	65.59	= 65.58

Top F.H. SECR 43rd &amp; Newton

BR Nely Cor 43rd & Newton 55.53 top 6" c1  
5.45

c31

c37

c37

c35

c43

c38

c36

c25

c38

c26

59.25 SW. 57.83  
1.73 3.15

c120 to Flange  
c290 to Ell



NEWTON AVE  
(Cont'd)

WATER METERS

70.77

4/21/53

59

0-66 Nly (= 265' W. W. P. L. 43 <sup>rd</sup> )	11.1	59.7	58.7	019	4216 Newton
-1404 Nly (= 227' " " " )	10.7	60.1	59.2	009	4224 Newton
-1461 Nly (= 170' " " " )	10.0	60.8	60.2	006	4230 Newton
-2476 Nly (= <sup>470.77</sup> 55' " " " )	7.10	63.7	63.3	004	
0-200 Nly (= 331' W. W. P. L. 45 <sup>th</sup> )	11.90	58.8	58.4	008	4208 "
0-450 Nly = 381' " " "	3.15	57.83	57.3	005	4194 "
1-400 Nly = 431' " " "	6.0	55.0	55.4	FO4	4186 "
1-449 Nly = 480' " " "	9.8	51.2	51.4	FO2	4179 "
1-477 Nly = <sup>49.26</sup> 508' " " "	2.2	47.3	48.3	F10	4172 "
2-429 Nly = 560' " " "	9.9	39.6	40.1	FO5	4166
2-450 Nly = 581' " " "	12.4	37.1	37.0	CO1	4160 "



SAPPHIRE ST  
MISSION BLVD TO BAYARD ST.  
© STKS & GRDS for Existing Wat. MET.S

DEC. 8, 1953

Beatty  
J. J. Martell  
Alexander

60.

	+ B.S.	H.	- F.S.	Elev	Curb Grade		Street 225 RT &
BM	12.62	111.16		98.54		NW BP Mission & Sapphire	
0+365 Nly.			9.3	101.9	99.4	C25	5153 Mission Blvd
0+96 Sly.			9.7	101.5	100.9	C06	815 Sapphire St.
1+16 Nly.			7.4	103.8	102.3	C15	816 " "
1+36 Sly.			9.1	102.1	102.1	C09	821 " "
1+54 Nly.			6.2	104.8	103.2	C16	824 " "
2+01 Nly.			5.9	105.3	103.8	C15	830 " "
2+18 Sly.			7.5	103.6	103.2	C04	831 " "
2+67 Sly.			7.1	104.1	103.7	C04	839 " "
2+67 Nly.			5.1	106.7	104.4	C17	838 " "
2+97 Nly.			5.1	106.1	104.7	C14	844 " "
3+18 Sly.			6.9	104.2	104.2	C09	845 " "
3+61.5 Nly.			4.4	106.8	105.6	C08	862 " "
3+64 Sly.			6.4	104.8	104.9	F01	855 " "
4+07.5 Nly.			4.1	107.1	106.4	C07	867 " "
4+05 Sly.			5.9	105.2	105.7	F05	863 " "
4+54 Nly.			2.7	108.5	107.3	C13	880 " "
4+93.5 Nly.			1.3	109.9	108.1	C18	884, 886, " "
5+08 Sly.			2.7	108.5	107.8	C07	901 " "



SAPPHIRE ST.  
(Contd.)

12/8/53

61

111.16

5+38 Sly		1.7	109.3	108.5	C08	905. Sapphire St.
4P	816	118.47	0.85	110.31		
5+44 Nly		6.2	112.3	109.4	C29	904. " "
5+72.5 Nly		5.5	113.0	110.3	C27	910 " "
6+30 Sly		6.1	112.4	116.8	C06	5126-5138 Bayard
6+43.5 Nly		4.5	114.0	113.0	C10	5150 Sapphire
6+44.5 Nly		4.5	114.0	113.1	C09	5160-5163 1/2 Bayard
	N. side end Curb	4.85	113.62			
4P	4.09	110.05	12.91	105.56		
CK BM		11.50	98.55			



SHAFTER STREET  
SCOTT TO CARLTON  
④ JTK'S #GRDS FOR 6" AC. WATER  
(10934-L)

DEC. 9 1953

BEATTY  
SHOEBY  
MART

62

BM 0.81 07.14 06.33

7' OT. Wly cor. Scott & Carlton

0+00 = Ely prop line Carlton

0+50 = 6" G.V. Begin Work 6.1 01.0 -02.2 C42

1+00 5.9 01.2 -02.1 C43

① 5.60 06.81 5.93 01.21 -03.0 C45

1+50 5.3 01.5 -03.0 C45

2+00 5.2 01.6 -02.9 C45

2+50 5.6 01.2 -02.7 C39

3+00 5.5 01.3 -02.6 C39

3+10 = 6" G.V. END WORK 5.6 01.2 -02.5 C37

Sew M.H. 5.57 01.24

② 4.19 07.29 3.71 03.10

Top FH Cor Carlton & Shafter

CK B.M. 0.96 06.33



DEC. 10, 1953

BEATTY  
SHOREY  
MARTELL  
ALEXANDER

63

CALLE AQUADULCE  
ROANOKE TO CUMBERLAND  
③ STRS & GRDS FOR 6" WATER.

T.B.M.	13.35	305.47	292.12			3/4" IR. 15' RT @ +50 (EB. 787 pg. 38.)	
0+00 =	Sly line of Roanoke						
0+25 =	Nly line of Roanoke	15.2	290.3	2890	C73	15.2	
	Begin Work						
0+50	F.H. TEE	13.2	292.1	2851	C70	13.5	
	③ F.H.	13.2	292.3	2892	C31 C72		
0+75		10.8	294.7	2873	C74	10.9	
1+00		8.8	296.7	2895	C72	8.9	
1+25		6.7	298.8	2916	C73	6.7	
1+50		4.5	301.0	2937	C73	4.7	
1+75		2.5	303.0	2959	C71	2.6	
① D							
2+00	11.1 ( $\frac{1}{2}$ pipe moved 0 <sup>3</sup> LT)	316.26	0.32	305.15	2981	C71	0.5
2+25	( $\frac{1}{2}$ pipe moved 0 <sup>75</sup> LT)	8.2	305.1	3002	C72	8.2	
2+50	( $\frac{1}{2}$ pipe moved 1 <sup>5</sup> LT)	6.6	309.7	3024	C73	6.6	
						2+50 E 6.6	
						Top Sew 6.55	
						Rim 309.71 - 8.75 = 300.96	
2+75	( $\frac{1}{2}$ pipe moved 0 <sup>75</sup> LT)	4.4	311.9	3045	C74	5.1	
3+00	( $\frac{1}{2}$ pipe moved 0 <sup>3</sup> LT)	2.8	313.5	3066	C69	3.0	
3+25		1.5	312.8	3075	C73	1.8	
3+50		0.7	315.6	3085	C72	1.0	
3+52 <sup>33</sup>	B.C. 7.92	323.57	0.6	315.65	3086	C71	0.9
3+75			7.2	316.4	3094	C70	7.6
4+00			7.0	316.6	3097	C69	7.4



CALLE AQUADULCE  
(CONT'D.)

12/10/53

69

323.57

4+50		6.5	317.1	310.2	C63	✓		69
4+90	F.H. TEE	6.1	317.5	310.6	C69			66
	⑤ F.H.	5.0	318.6	312.6	C70	C80		
5+00		5.5	318.1	310.7	C72			65
5+45	74 B.C.	5.9	317.7	311.2	C65	✓		67
5+50		5.8	317.8	311.3	C65	✓		68
							5+56	Sew M.H. 315.69 - 12.2 303.3 Top Inv. Rim - 7.28
6+00		6.3	317.3	311.8	C55			71
6+50		5.6	318.0	312.3	C57	✓		66
7+00		4.0	319.6	312.8	C68	✓		52
7+50		3.5	320.1	313.2	C69	✓		46
8+00		3.1	320.5	313.3	C72	✓		41
8+25		3.9	319.7	313.4	C63	✓		39
		6.5	317.1	317.5	F02			
④ 8+75	119	4.52	319.05	311.7	C74	✓		42
9+25		3.3	316.9	310.0	C69	✓		33
9+70	45 F.C. F.H. TEE	7.1	313.1	306.7	C64	✓		71
	⑤	5.8	314.4	311.8	C26	C77		
10+05	6" TEE	9.8	310.4	304.2	C62	✓		78
	0.15	307.41	12.98	307.26				
10+50		0.9	306.5	300.9	C56	✓		89
11+00		5.1	302.3	297.3	C50	✓		56

W.M. 8+28 Wly 2.400 Aqua dulce



CALLE AQUADULCE  
(CONT'D)

12/10/53

65

307.41

11+50			10.0	297.4	293.7	C37	10.2
4)	1.79	296.28	12.92	294.09			
12+00			2.5	293.8	290.9	C38	2.5
12+50			4.1	292.2	287.0	C52	4.2
+75			5.8	290.5	286.0	C35	
13+00 <sup>76</sup>	END WORK		6.7	289.6	286.0	C36	4.7

13+05<sup>76</sup> Existing 8" C.I.

4) 2.25 285.79 12.74 283.54

4) BM 7.67 278.12 = 278.15 this is Cumberland & Calle Serena

CK BP 7.69 278.10



CATOCTIN DRIVE  
 MONTEZUMA NLY  
 ② STKS & GRDS for Existing  
 WATER METERS

12/10/53

66

BM.	10.78	438.73	447.95		SWBP. Catoctin & Montezuma	
0+00 =	E of Sarabac					
0+22 Wly		2.7	454.0	453.8	C02	5092. Catoctin
0+36 E	FH. 21 <sup>60</sup> LT	3.7	455.0	453.8	" 12 to flange	
0+67 Ely		4.4	454.3	452.2	C01	5089.
2+02 Wly		5.1	453.6	451.0	F04	5080.
2+56 Ely		4.6	454.1	452.5	C06	5035.
3+13 Ely		5.3	453.4	452.5	C09	5015
3+98 Wly		7.0	451.7	450.9	C08	5020
5+10 Wly		7.3	451.4	448.7	C27	5010
CK BM.		10.78	447.95			



62nd ST  
 BROOKLYN TO AKIN  
 REV. WAT. MET. & F.H.  
 (See pg 77 FB 815 for Orig.)

BM	0.52	245.59		245.07	
BE 10+20 CITY			1.5	244.1	603 = 243.8
F.H. 10+22 City, = 12+29			1.4	244.2	244.1
WM. 9+11 City, = 11+19 E			8.5	237.1	237.9
WM. 8+87 City, = 10+95 W			10.3	235.3	236.4
WM. 8+40 City, = 10+47 E			10.4	235.2	233.6
WM. 7+97 City, = 10+05 E			11.6	234.0	231.1
TP	0.30	233.59	12.30	233.29	
WM. 7+27 City, = 9+35 W			3.8	229.8	227.1
WM. 7+06 City, = 9+14 E			5.4	228.2	225.8
TP	0.44	221.56	12.47	221.12	
WM. 6+02 City, 8+09 E			3.1	218.5	218.5
WM. 5+81 City, 7+89 E			5.2	216.4	216.8
WM. 5+74 City, = 7+82 W.			3.4	218.2	216.4
F.H. 5+32 City, = 7+40			8.8	212.8	212.8
WM. 5+22 City, 7+31 E			9.6	212.0	212.1
WM. 4+68 City, = 6+75 W			11.6	210.0	207.8
TP	0.89	209.27	12.98	209.58	= 206.0
WM. 4+48 City, = 6+59 E			2.6	206.9	206.1
WM. 4+11 City, 6+19 E			6.2	203.3	203.0
WM. 3+96 City, 6+04 W			5.4	204.1	201.6
WM. 3+82 City, = 5+90 E			8.6	200.9	200.5

12/16/59

67.

SWBP 62nd & Brooklyn

Mets stud 275 RT & LT & ST  
 originally " 22E " " " "  
 FH " 26E " " " "  
 originally " 21E " " " "

CO1

FO8 ✓

F1 ✓

C16 ✓

C29 ✓

C27 ✓

C24 ✓

CO0 ✓

FO4 ✓

C18 ✓

CO0 ✓

FO1 ✓

C22 ✓

+ + 50 E C26 OK

CO8 ✓

CO3 ✓

C25 ✓

CO4 ✓



62 NO ST  
(Cont'd.)

209.47

WM 3+59 City = 5167 W

9.6

199.9

198.7

C12 ✓

D 0.11 196.72

12.86

196.61

WM 3+275 City = 5135 E

2.2

194.5

195.8

F13 ✓

WM 2+46 City = 4154 E

7.3

189.2

191.1

F13 ✓

WM 1+71 City = 3+79 E

7.4

189.3

190.3

F12 ✓

WM 1+02 City = 3+09 W

9.2

187.5

190.1

F26 ✓

WM 0+53 City = 2+62 E

9.1

187.6

190.9

F33 ✓

EH 0+21 City = 2+285 E

9.1

187.6

191.32

F32 ✓

OK TBM

2.21

194.51 = 194.55

Nail in pole

12/15/53

68



WEAVER ST  
60th TO BURIAN  
⑤ STKS & GRDS for 6" A.C. WATER  
(GROUP 10)

Mar. 1, 1954  
HEATH  
SIMPSON  
MARSHALL  
ALEXANDER

69

TBM.							
	0.78	352.82		352.04		2'x2' 20' RT	6+87.24 BURIAN ST.
TD	1.91	341.79	12.94	339.88			
TD	1.73	330.35	13.17	328.62			
TD	0.02	317.13	13.24	317.11	290.2		290.8
6+87	1.29	306.13	12.21	304.70	294.0	<del>068</del> C75	9.6
0+83	⑤ F.H.	BEGIN WORK	8.5	297.9	292.7	001 C37	
1+00			12.5	293.9	293.8	<del>068</del> C70	294.9
			8.6	297.8	291.3		9.5
					290.8		
1+25			8.4	298.0	292.0	062	290.6
							9.8
1+50			8.9	297.5	292.8	038 C47	296.2
					292.7		10.2
2+00			6.1	300.3	295.6	<del>027</del> C47	299.5
					292.6		6.2
TD					300.0	<del>034</del> C47	303.9
2+50	12.83	317.55	1.71	302.72	301.3		2.5
3+00			9.2	308.4	302.0	<del>034</del> C44	10.2
					305.0		
3+50			5.2	312.4	307.0	<del>044</del> C54	6.2
					308.0		
4+00			3.2	314.4	310.0	<del>044</del> C44	4.2
					311.0		
4+50			1.5	316.0	312.0	<del>028</del> C40	2.2
					313.2		
TD	10.44	327.87	0.18	317.43	314.0	<del>029</del> C43	10.6
5+00			9.6	318.3	315.4		
5+50			8.1	319.8	315.5	<del>037</del> C43	9.2
					316.1		
6+00			6.8	321.1	316.8	C43	7.7
6+50			6.2	321.7	316.8	<del>042</del> C49	7.2
					317.4		
6+90	GV.		6.1	321.8	316.9	<del>039</del> C49	7.1
					317.9		
6+95.10 (PC)	F.H. TEE		6.1	321.8	316.9	<del>039</del> C49	7.2
	⑤ F.H.		9.5	318.4	317.4	F38 C15	7.0
					322.3		
7+00			6.1	321.8	317.0	<del>038</del> C48	7.1
					318.0		
TD	4.20	331.99	0.08	327.79			



WEAVER ST.  
(CONT'D)

3/2/54

70

331.99

7+25			9.9	322.1	<del>318.0</del> 318.8	C53 C41	10.5
7+50			8.4	323.6	<del>319.0</del> 319.6	C40 C40	9.4
7+75			6.3	325.7	<del>320.1</del> 320.4	C53 C50	7.3
8+00			5.0	327.0	321.1	C52 C59	6.0
8+25			3.7	328.3	321.9	C64	4.7
8+50			2.3	329.7	322.7	C70	3.7
8+75			1.2	330.8	323.4	C74	2.0
8+89.42 (EC)	10.71	342.20	0.50	331.49	323.9	C76	1.4
9+00			10.2	332.0	324.2	C78	11.4
9+50			8.0	334.2	325.8	C80	9.3
10+00			6.0	336.2	327.4	C88	7.2
10+50			5.1	337.1	329.0	C81	6.3
10+76.02	* PT	3'43'15" RT	4.7	337.5	329.9	C76	5.8
10+96.56	* PT	" " "	4.6	337.6	330.6	C70	5.5
11+17.00	* PT	28'34" LT	3.4	338.8	331.3	C75	3.9
11+62	GV.	1310	2.33	339.87	332.9	C70	3.0
OK TBM.			0.96	352.01	= 352.04		



## WEAVER ST

(Cont'd.)

## WATER METERS

	306.43					
1+88 S	306.43	9.3	297.1	300.7	F36	1211 WEAVER
4+82 N	327.87	6.5	321.4	319.0	C24	? "
5+90 S	"	9.6	318.3	321.0	F27	1271 "
6+66 N	"	0.9	327.0	322.1	C49	? Weaver
6+66 S		9.2	318.7	321.6	F29	? Radio Dr.
6+90 S		8.8	319.1	322.0	F29	1273 Weaver

3/2/54

76



BURIAN ST  
 RADIO RD TO WEAVER  
 (5) STR. S & GRP. S for 8" WATER  
 (GROUP 10)

3/3/54

72

BM	12.72	292.14		279.42				
0+17	8" G.V.	Begin work	11.9	280.2	274.5	C57		2 PT 32+57 <sup>65</sup> Radio Road
0+22			11.9	280.2	274.5	C57		
0+50			11.0	281.1	<del>274.6</del> 275.3	C58		
1+00			4.8	287.3	279.0	C82		
TP								
1+50	12.23	304.27	0.10	282.04	283.5	C85		
1+63 <sup>96</sup>	BC		12.1	292.9	284.7	C82		10.7 WAT. MET
1+75			11.5	293.5	285.8	C77		
2+00			9.7	295.3	288.0	C73		
2+25			7.9	297.1	290.6	C65		
2+50			6.0	299.0	293.2	C58		
2+75			3.9	301.1	295.8	C53		
3+00			1.8	303.2	298.4	C48		
TP								
3+16 <sup>10</sup>	13.32	317.77	0.52	304.45	300.0	C45	3+10	317.77
								WAT. MET. EAST 207.9 GRD C 10.7 303.3 97
3+50			10.6	307.2	303.5	C37		
4+00			5.8	312.0	308.5	C35		
4+50			0.4	317.4	313.6	C38		
5+00	TP 13.22	330.87	0.10	317.67	320.5	C32		
5+46 <sup>10</sup>	B.C. 12.72	343.59	6.5	321.4	326.9	C46		
			0.02	330.87				
			12.1	331.5				
5+50	F.H. TEE		11.4	332.2	327.4	C48		
(5) F.H.			7.0	336.6	331.7	C49 C92		



BURIAN ST  
(Cont'd.)

3/3/54

73

343.57

5+75

73

336.3

~~330.5~~  
331.9

C58

6+00 8x6" WYE

38

339.8

~~333.5~~  
336.4

C62

6+05 8" G.V.

3.4

340.2

333.7

C65

CK 7D

3.71

339.86 = 339.87

11+62 (5) G.V. pg. 70



MAR. 16 1954

BEATTY  
SUDREY  
MARTELL  
ALEXANDER.

74.

PIDGEEON ST.  
JAMACHA To FOSTER  
⑤ STKS & GROS FOR 6" A.C. WATER  
(GROUP. II)

TBM.	13.26	273.15	259.89	E. Edge Jew. M.H. Ridgeon & Jamacha. FB. 852, 79, 44		
0+40	6" G.V. CITY	12.6	260.6	256.6	C40	
0+45	Begin Work	11.3	261.9	257.0	C49	
0+50	Nly Prop line Jamacha.	10.5	262.7	257.5	C52	
1+00		6.5	266.7	260.5	C62 ✓	
1+50		3.0	270.2	264.4	C58	
1+00	12.61	285.71	0.05	273.10	269.2	
2+00			11.4	274.3	269.9	C51
2+50			6.1	279.6	275.0 275.4	C46
3+00			0.0	285.7	281.0	C47
3+00	9.50	295.16	0.05	285.66		
3+25			6.2	289.0	283.8	C52
3+50			2.2	293.0	286.2	C68
3+75			1.3	293.9	287.7	C62
4+00			1.0	294.2	288.5	C57
4+25			2.1	293.1	288.0	C51
4+50			3.7	291.5	286.7	C48
4+75			6.0	289.2	284.9	C43
5+00			6.6	288.6	284.0	C46
5+04			6.9	288.3	284.0	C43
5+24			6.8	288.4	284.0	C44
5+50			4.7	290.5	284.7	C58.

5+00 7/10



3/16/54

75

RIDGEON ST.  
(Cont.d.)

295.16

5+75		1.9	293.3	2859	C74	37
④ 6+25	11.49	306.30	0.35	294.81	2897	C51
6+50		8.1	298.2	2917	C69	54
7+00		4.2	302.1	2945	C75	48
7+50		1.5	304.8	2967	C81	31
8+00		0.8	305.5	2974	C81	23
8+50		0.8	305.5	2971	C84	20
9+00		1.9	304.4	2949	C95	47
9+50		6.5	299.8	2919	C79	69
10+00		7.8	298.5	2878	C107	97
10+50	6" F.H. TEE END WORK	10.5	295.8	2826	C122	121
⑤ F.H.		7.0	299.3	2880	C113.953	✓

④ 4.09 298.54 11.85 294.45

④ 6.45 292.09 - 292.06 Rem of M.H. RIDGEON & FOSTER E.B. 852 pg. 46

## WATER METERS

1+77 W	N 273.15	27	270.5	270.0	C05	570 Ridgeon
2+28 W	N 285.7	10.1	275.6	276.0	F04	578 "
2+92 E	"	0.9	284.8	284.7	C01	635 "
2+92 W	"	3.1	282.6	283.7	F11	608 "



PIDGEON ST  
(Cont'd)

3+43 E	295.16	2.7	292.5	289.6	C29 ✓	611 Pidgeon
3+52 E	"	2.1	293.1	290.5	C26	611 " REAR
4+89 E	"	4.4	290.8	288.8	C22	635 "
5+87 E	"	1.3	293.9	290.7	C32 ✓	705 "
6+55 E	N: 306.3	6.8	299.5	296.2	C33 ✓	719 "
6+91 W	"	8.3	298.0	298.0	C00 ✓	720 "
7+38 W	"	7.0	299.3	299.9	F06	730 "
7+57 E	"	0.2	306.1	301.0	C5L	725 "
7+73 W	"	6.4	299.9	300.9	F10	736 "
8+06 W	"	5.4	300.9	301.0	F0L	742 "
8+39 E	"	+1.5	307.8	301.3	C6E ✓	745 "
8+75 W	"	7.3	299.0	299.9	F09 ✓	754 "
9+00 W	"	10.7	295.6	298.7	F3L	764 "
9+81 W	"	12.8	293.5	292.9	C0E	776 "
9+83 E	"	4.8	301.5	293.3	C8E ✓	767 "
10+30 E	"	6.7	299.6	289.5	C10L ✓	775 "
		11.5				



3/16/54

77.

FLICKER ST.  
LISBON 400' Nly  
⑤ GRADES & STAKES  
FOR 6" A.C. WATER

BM. 253.15  
TP. 7.66 283.22 275.56

FB 862 pg 20.  
2" pipe Bridge 69th & Imperial EB. 852 pg 41  
E. Edge SEW MH. FLICKER & LISBON.

0+20	6" G.V. (CITY)	7.1			
0+25	Begin Work	6.9	276.3	271.4	C59
0+50	= Nly Prop Line LISBON	5.6	277.6	271.9	C57
1+00		4.6	278.6	273.1	C55
1+50		3.4	279.8	273.4	C64
2+00		3.8	279.4	273.1	C63
2+50		5.0	278.2	272.1	C61
3+00		6.3	276.9	271.1	C58
3+25		7.4	275.8	270.4	C54
3+50		8.0	275.2	269.6	C56
3+75		8.5	274.7	267.9	C68
4+00	2" B.O. END WORK	8.4	274.8	265.0	C98
TP	0.27	270.35	13.14	270.08	
OK BM	2.56	257.55	13.76	256.99	
			6.20	253.15 = 253.15	

## WATER METER

1+18 E	283.22	3.4	279.8	276.9	C29
1+80.5 E		1.7	281.5	277.2	C43
1+98 W		7.6	275.6	276.8	C12
2+24 E		1.6	281.6	276.7	C49
2+35 W		7.4	275.8	276.0	C03
2+69 E		3.6	279.6	275.8	C38
3+62 E		5.1	278.1	272.7	C54
4+00 E		5.9	276.3	269.3	C70

711 Flicker  
719 Flicker  
6925 Imperial  
727 Flicker  
6959 Imperial  
735 Flicker  
755 Flicker  
6975 Imperial



LOGAN & CO. TH  
F.H. LOCATED  
3ELY COR

GM.	1.58	84.63	83.05
H	0.11	71.63	13.11 71.52
P	6.40	71.49	6.54 65.09
		3.85	67.62 = 67.60
		3.64	67.85 = 67.80
		2.0	69.49 67.93
		1.5	70.0 64.4

Mar 29 1954  
Beatty  
Sydney  
Marfell  
Alexander

78.

3W BP 39TH & National

ck exist curb SW ret Prop. line

ck " " " " E.C

C156 (5) F.H. C51 To ELL

C56 (4) F.H. TEE



AM.

4

4

28

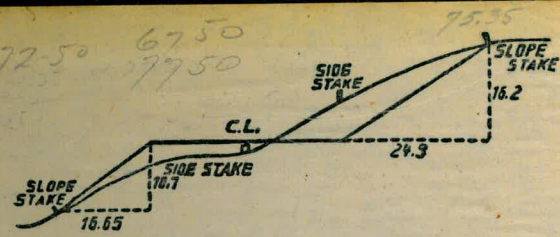
2. 10/10 2  
2

31<sup>st</sup> Cedar

7  
17



Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**

SLOPE 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

*Handwritten notes:*  
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