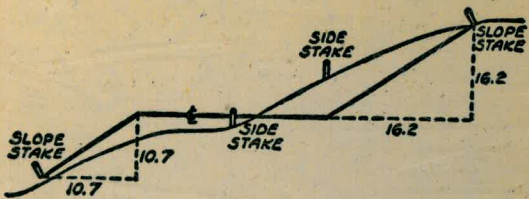


W

868

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

179 60
 106 59
 73° 01'



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

San Clemente - Tennyson, Voltaire	1-5 ✓
Soto - Green to Castellar	6-8 ✓
Plum - Macaulay to Newell	9-11 ✓
Newell - Plum to Clove	12-14 ✓
Russell - Willow to Evergreen	15-20 ✓
Electric Ave, Colma St. Sly sec	alice ✓ 21-23 ✓
Fern Glen, Monte Vista to Vista Del Mar	alice ✓ 24-26 ✓
Walnut St. Jackdaw to Ibis	27-31 ✓
(Preliminary) Seventh Ave Cedar to Date	32-34 ✓
" Richmond St, Myrtle to Cypress	alice ✓ 35-40 ✓
Franklin Ave, Evans to 28th	alice ✓ 41-45 ✓
Muirland 12" Feeder Line - La J. Shores Dr. to Beccano Dr.	46-49 ✓
" " " " " 5th & Grand, 12" MAIN	alice ✓ 50-58 ✓ alice ✓

INDEX

Wert
Kemp
Holahan

5-27-54

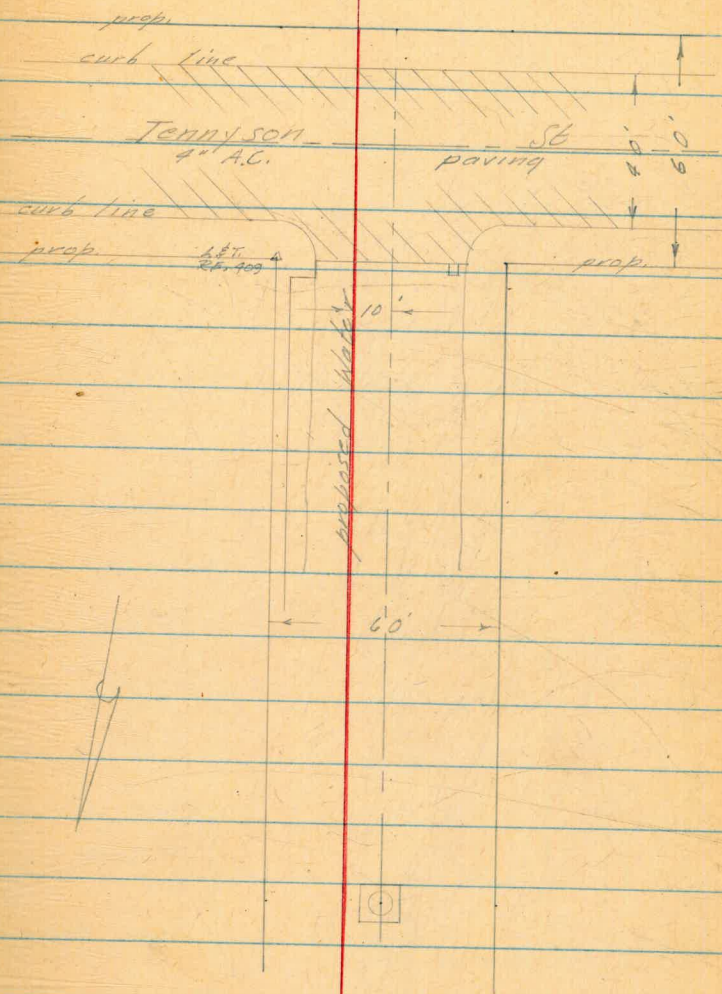
Profile & Proposed Water

San Clemente St., Tennyson

to
Voltaire

- 0+00 So. line Tennyson.
- +07 F.H. 15' R.L.
- +10 So. curb line
- +50 No. curb line
- +60 Edge 4" A.C. paving
- +62 12" service box (not opened)
assumed to be gas

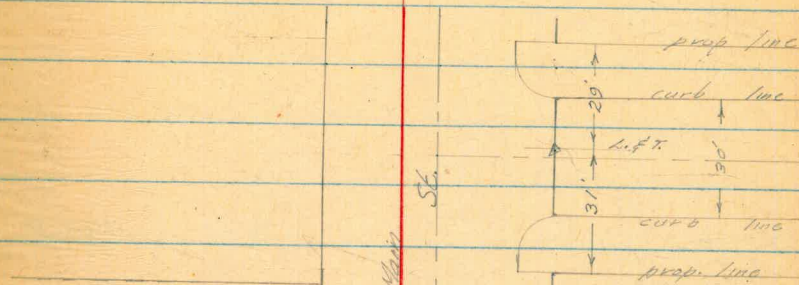
4+14 Gas & Elec. M.H. 10'x10' Box
no visible services



Profile San Clemente Cont.

3+59

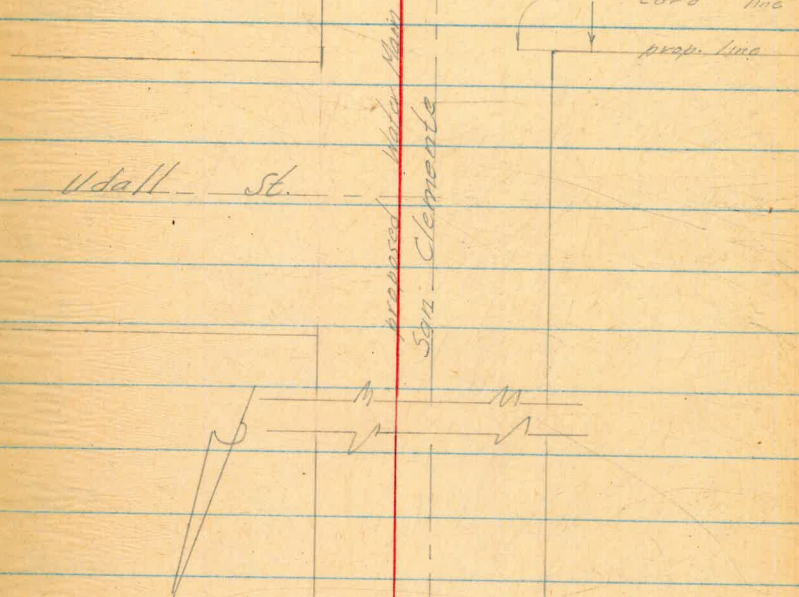
E Udall St.



4+35

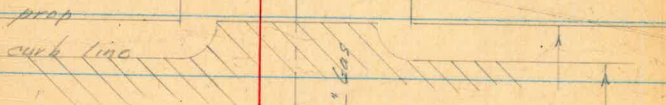
E Udall St.

Udall St.



6+71

So. prop. Voltaire

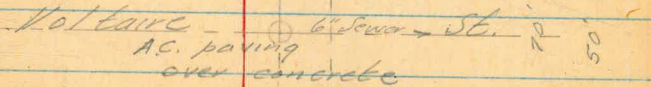


+81

So. curb line

7+06

E Voltaire & Sewer M.H. 10' 6"



+27

4-way 2", Gas M.H. 15' 11"

+31

curb line



+41

prop. line



Profile of San Clemente

Cont.

126.64
1.66
128.30
5
125.4

126.64

W. line, S. 5' line 150 Tennyson

2.46 129.10

0+00 2.3 126.8

San prop. Tennyson

+10 3.0 126.1

San curb line

+50 3.5 125.6

No. " "

+60 3.7 125.4

Non prop. line Tennyson, edge pavement

1+00 6.7 122.4

+50 10.2 118.9

T.P. 12.08 117.02

0.58 117.60

2+00 3.2 114.4

+50 7.4 110.2

3+00 11.2 106.4

T.P. 13.21 104.39

2.33 106.72

3+50

28.4
5.4
8

5.4
3

4.2
0

3.2
5

103.5

25

Profile of San Clemente

Cont.

	106.72	
4+00		
T.P.	11.97	95.25
	9.36	99.61
4+07		
		95.4
4+14	9.24	
+16		
+50	9.0	90.6
T.P.	12.31	87.30
	0.74	88.04
5+00	7.4	80.6
+50	7.9	80.1
6+00	10.9	77.1
T.P.	13.15	74.89
	1.51	76.44

	16					
	$\frac{10.0}{2}$	$\frac{10.1}{4}$	$\frac{7.4}{3}$	$\frac{7.6}{8}$	$\frac{7.9}{3}$	98.8
	$\frac{3.7}{9}$	$\frac{3.7}{4}$	$\frac{1.1}{3}$	$\frac{1.1}{8}$	$\frac{1.9}{5}$	97.7
						94.6
	$\frac{5.1}{5}$	$\frac{4.5}{8}$		$\frac{5.0}{5}$		

Gas & Elec. M.H.

88.0
 2.4
 85.6

Profile of San Clemente Cont.

76.44

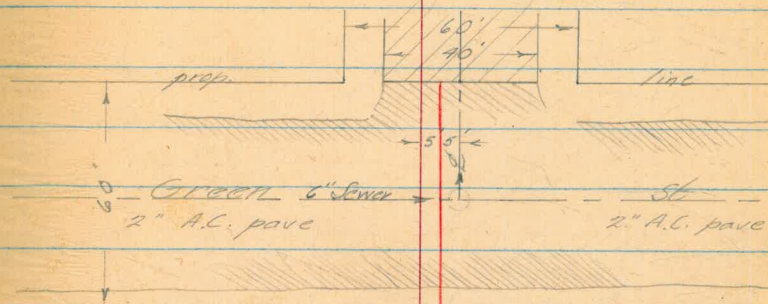
6+50	3.9	72.5	
+71	5.0	71.4	So. prop. & edge 9" A.C. paving
+81	5.5	70.9	So. curb line Voltaire
7+06	4.9	71.5	& Voltaire
7+06	5.05	71.4	Sewer M.H. 12.0 to fl.
+27	5.42	71.0	Gas M.H. 2.3 to pipes (4-way, 2")
+31	5.5	70.9	No. curb line Voltaire
+41	5.6	70.8	No. prop. line Voltaire
	3.06	73.38	Top F.H. El. 73.62

Circuit closed to original B.M. 001
closure

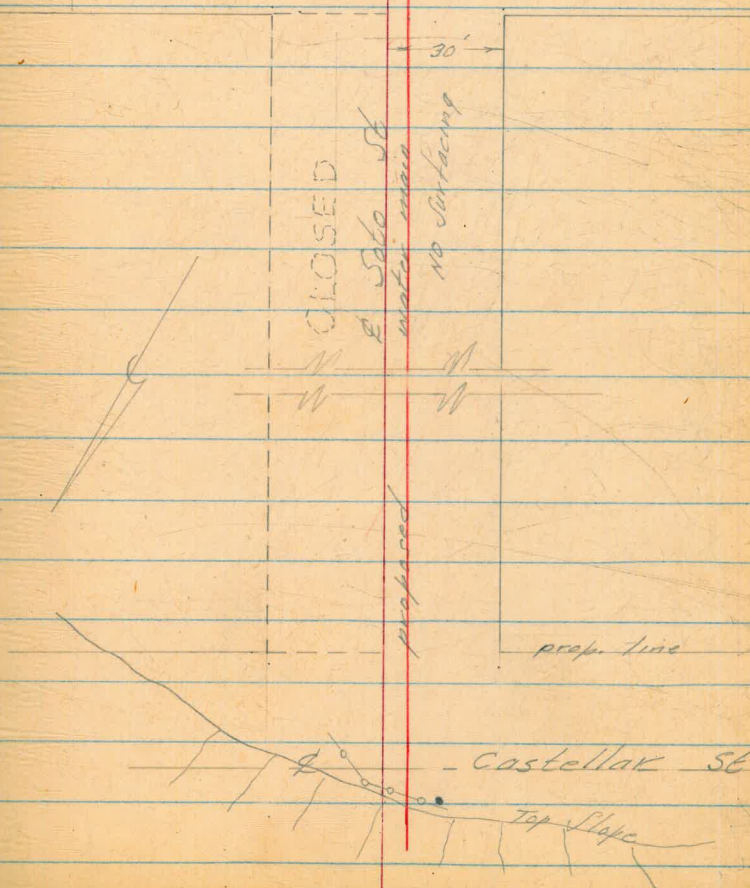
Went
Camp
Holahan 5-28-53 6

Profile of Proposed Water on
Soto St., Green to Castellar

0+00 So. prop. line of Green St.
+30 E. Green St. & Sewer M.H.
+56 Edge of 2" A.C. paving.



6+60 So. prop. Castellar
+91 Wooden barricade
7+00 Top of Slope
+10 Random point on slope



Profile Solo St. Green

to Castillar St

33.68

S.W. B.P. Etiwanda & Castillar St.

8.17 41.85

T.P. 3.49 38.36

6.14 44.50

T.P. 0.25 44.25

12.68 56.93

T.P. 0.40 56.53

3.35 59.88

0+00 1.2

To prop Green St.

+30 0.9

& Green St.

+30 1.18

Sewer MH rim 5' to 6.5 to flow line

+50 1.7

+56 2.2

Edge 2" H.C. paving

1+00 5.4

+50 8.0

2+00 10.7

T.P. 12.67 47.21

029 47.50

Profile of Soto St. Cant.

	47.50		
2+50		1.0	
3+00		3.7	
+50		6.1	
4+00		8.1	
+50		10.0	
5+00		11.5	
T.P.		11.53	35.97
	0.54	36.51	
5+50		2.0	
6+00		3.5	
+50		4.9	
+60		4.9	
+91		4.5	
7+00		4.8	
+10		9.4	
T.P.		6.03	30.48
	5.67	36.15	
		2.47	33.67

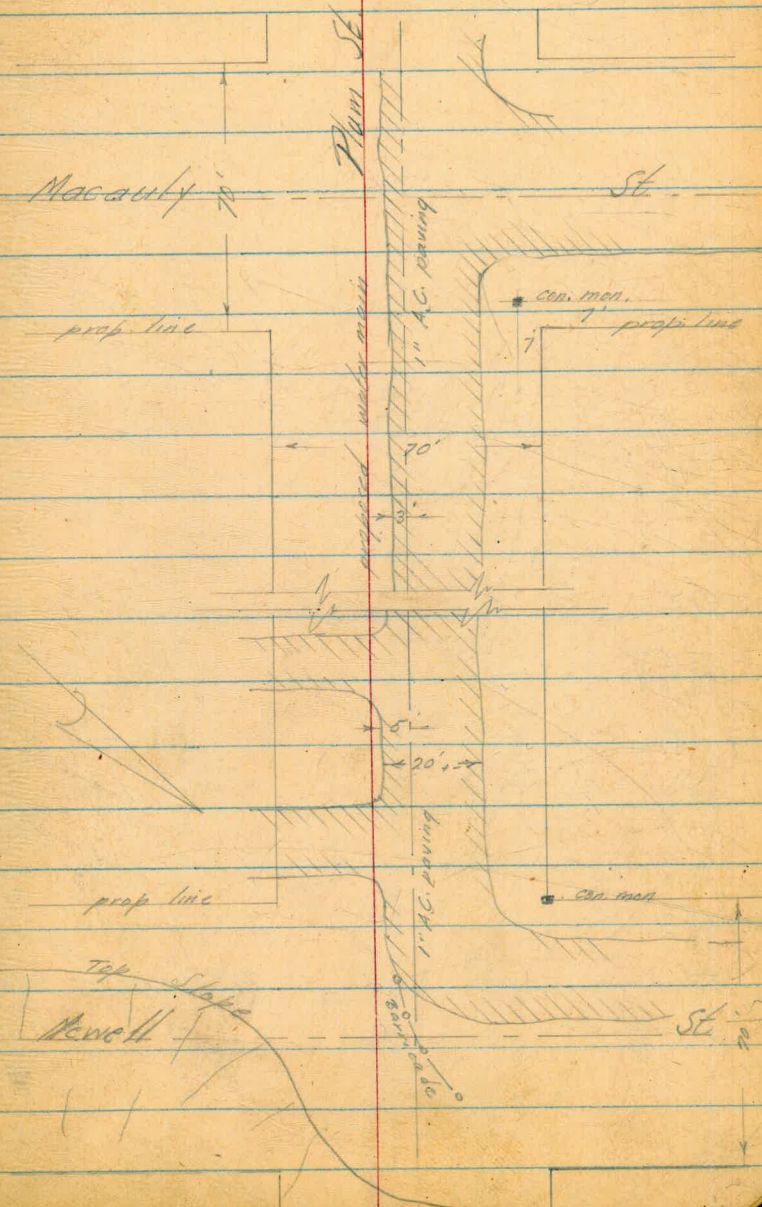
So. prop. Castillar

BP. S.W. Ebiwanda & Castillar = 37.68

Next
Kemp
Holahan 6-1-54

Profile & Proposed Water on
Plum St., Macaully to Newell

0+00	So. prop. line Macaully St.
+70	No. " " "
1+96	Edge 1" A.C. drive
2+13	Edge " " "
2+97	Edge 1" A.C. drive
+64	" " " "
2+70	So. prop. line Newell



Profile of Plum St. Cont.

			93.25
	11.59	109.84	
T.P.		0.53	109.31
	10.76	115.07	
T.P.		12.86	102.21
	0.63	102.84	
T.P.		12.14	90.70
	10.37	101.07	
0+00		8.0	93.07
+50		2.9	98.17
1+00		2.3	98.77
+50		7.1	93.97
+96		12.3	88.77
2+00		12.7	88.37
+13		13.1	87.97
T.P.		11.23	89.84
	4.99	79.83	

S.W. F.H. Oliphant & Clove

S.W. Con Man Plum & Newell

So. prop line Macaully St.

So. edge 1" A.C. drive way

No. edge 1" A.C. drive

Profile of Plum St. Cont.

	94.03		
2+97		8.3	86.53
+50		8.5	86.33
+64		9.0	85.83
X 3+00		11.9	82.93
+25		15.8	79.03
+40		18.8	76.03
T.P.		0.13	94.70

12.56 107.26

T.P.		0.12	107.14
------	--	------	--------

7.86 115.00

T.P.		6.82	108.18
------	--	------	--------

2.90 111.08

T.P.		8.91	102.17
------	--	------	--------

1.15 103.32

10.08 93.24

See edge 1" A.C. driveway

No. " " " "

See TBM. NE. 2x2" Hub & track
Newell & Clove

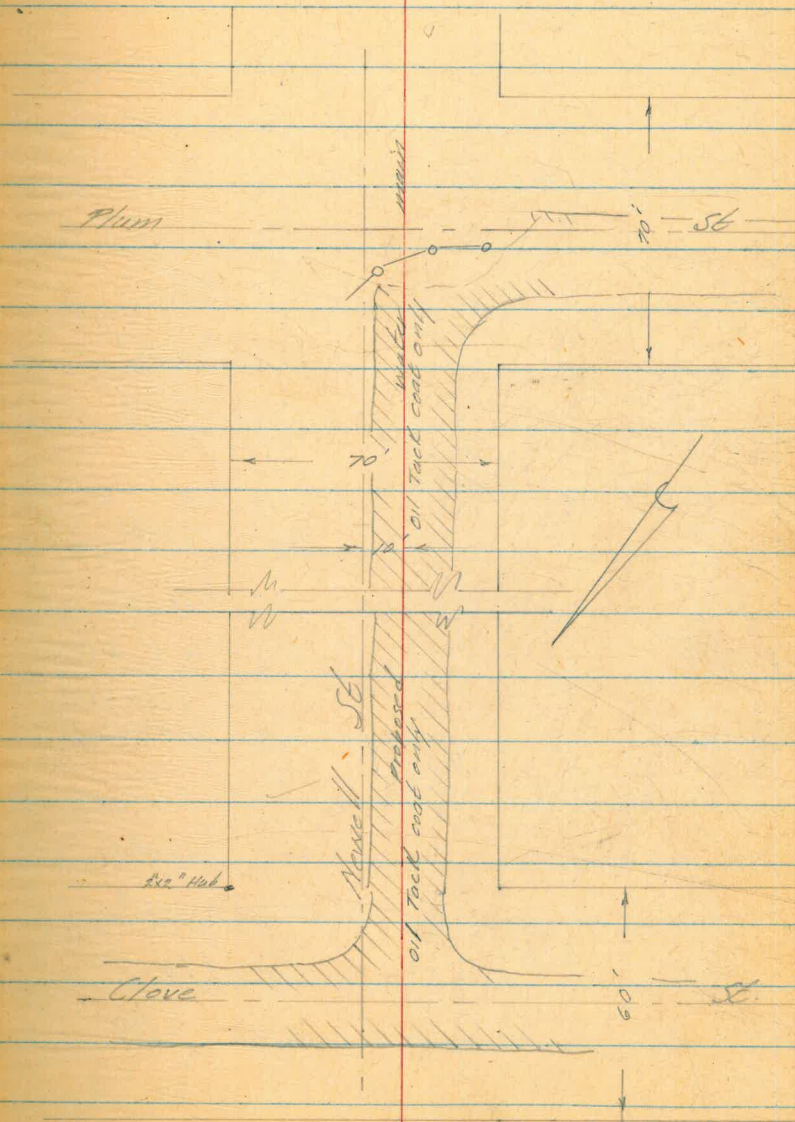
SW. T.H. Oilyant & Clove 93.25

Wert
Kemp
Holahan 6-2-54 12

Profile of Proposed Water on
Newell St., Plum to Clove

0+00 E. prop. line of Plum
+35 E Plum
+45 Wooden barricade
+70 W. prop. line of Plum

3+48.40 E/L of Clove
+78.40 E of Clove
+93 W. gutter of Clove
4+08.40 W/L of Clove



Profile of Newell Cont.

			90.70
	3.47	94.17	
0+00		16.7	77.47
+50		5.7	88.47
1+00		2.5	91.67
T.P.		0.29	93.88
	12.43	106.60	
		106.51	
1+50		3.2	97.40
2+00		5.0	101.60
+50		0.2	106.40
			106.41
T.P.		0.19	106.12
	9.48	115.89	
		115.60	
3+00		6.2	109.61
+50		4.7	111.19
+78.40		5.3	110.59
+93.		5.5	110.39
4+00		4.0	111.89

S.W. corner Plum & Newell

E. prop of Plum St.

E. Corner Clave St.

W. gutter of Clave

Profile of Newell Cont.

115.89
~~115.60~~

408.40

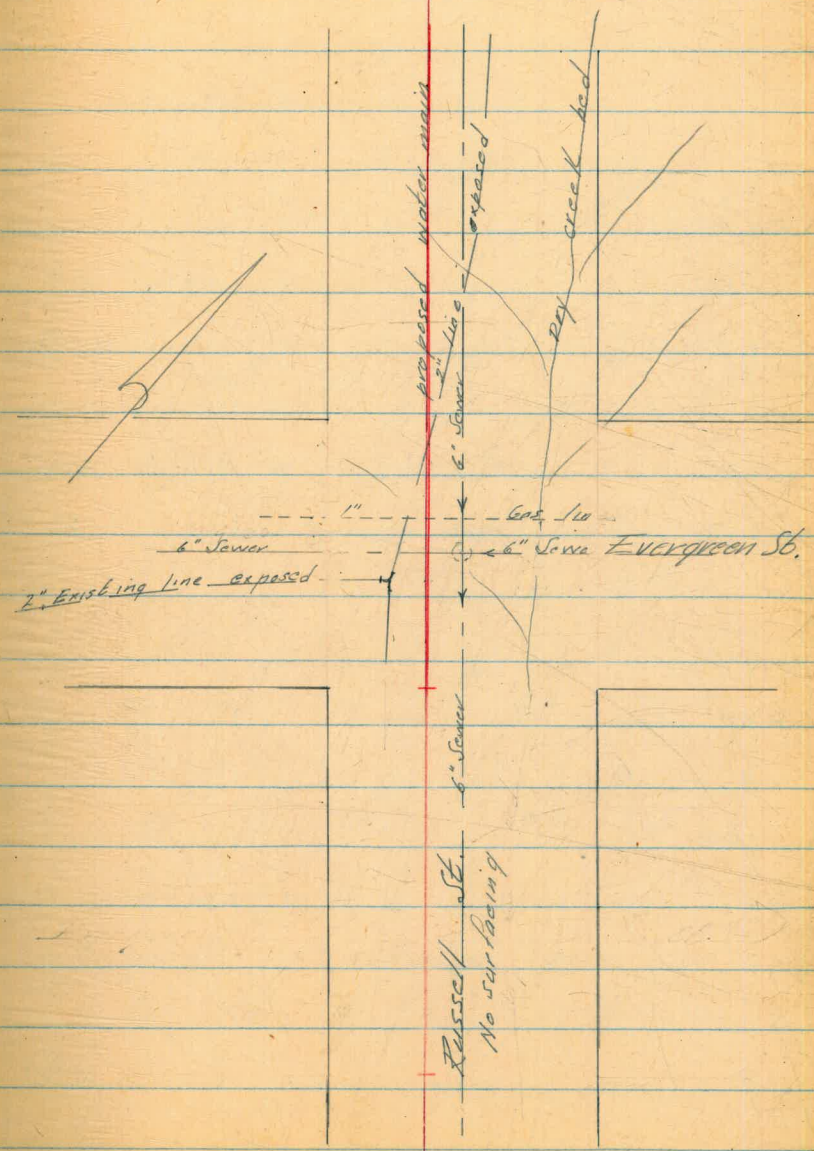
4.2 111.69
7.41 108.48
~~108.19~~

W. prop line Clove St

2' x 2" Hub NE. cor Clove & Newell

Profile of Russell St. Cont.

- 3+70 W/L Evergreen
- 3+75 Crossing of 2" existing & proposed lines
- 3+95 1" gas exposed, cut 1.0 over line
- 4+05 Sewer M.H.
- 4+12 2" Tee in existing line
- 4+40 E/L Evergreen



Profile of Russell Cont

	152.55		
+20	8.2	144.4	
+20	6.4	146.2	
+25	8.6	144.0	
T.P.	12.64	139.91	
	1.08	140.99	
2+50			
+75	10.9	130.1	
T.P.	10.36	130.63	
	0.95	131.58	
3+00			
T.P.	11.99	119.59	
	2.46	122.05	
3+50			
+75	10.1	112.0	
T.P.	13.12	108.93	
	0.38	109.31	
4+00			

22. 26.

Ground line at rock wall
Top rock wall

	135.4	139.7	136.0	130.3	126.3
+5.6	19	1.6	5.0	10.7	14.7
		70	0	70	20
	126.3	130.6	123.9	119.8	117.0
+5.3	1.0	7.7	11.8	14.6	
	70	0	70	20	
	117.2	121.7	116.7	111.4	110.4
+4.9	0.4	5.4	10.7	11.7	18.7
	70	0	70	75	20
	104.2	109.1	104.1	98.8	92.8
+5.1	0.2	5.2	10.5	16.5	
	70	0	70	20	

Profile of Russell Cont

26

26.

	109.31		
4+05		12.3	97.0
T.P.		12.85	96.46
	0.89	97.35	
4+40			
T.P.		11.74	85.61
	0.12	85.73	
T.P.		12.36	73.37
	0.57	73.94	
		12.85	60.99
	0.07	61.06	
		12.91	48.15
	0.75	48.90	
		13.07	35.83
	0.36	36.19	
		13.07	23.17
	0.91	23.58	
		10.96	12.62
	0.81	13.43	

Sewer M.H. 15' - to flow line

$\frac{+1.6}{20}$ 95.8 $\frac{2.8}{70}$ 94.6 $\frac{3.5}{70}$ 93.9 $\frac{9.5}{70}$ 87.9 $\frac{14.1}{76}$ 83.3
 creek
 bottom

Profile of Russell Cont

13.43

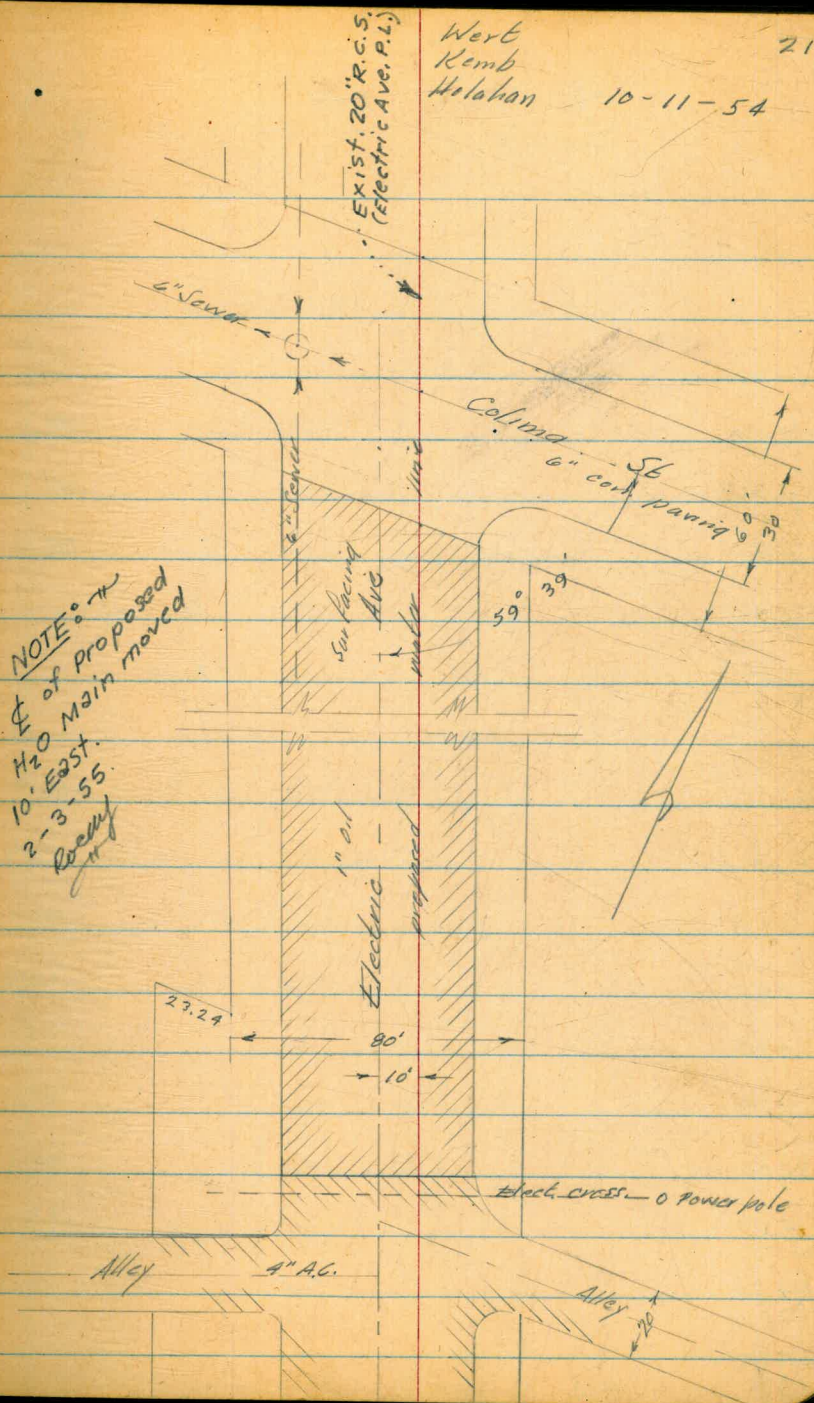
7.88 5.55

S.W. B.P. Rosecrans & Russell 5.54

Profile & proposed water on
Electric Ave, Colima Sully 500'

0+00	N/H of Colima St.
0+18.5	No. curb line
0+34	to Colima & Sewer Cross.
0+52.5	So. curb line
0+69.5	So. edge con. paving
5+03.4	End oil Surfacing, begin A.C. (4")
+09	Elect
+10.5	No. edge alley
+34	So " "

NOTE: The
E of proposed
H₂O Main moved
10' East.
2-3-55
Roemly



ELECTRIC AVE.
Colima St. to S'ly 500'

			77.98	SE. CP. La Jolla Blvd. & Colima St	
	7.41	85.39			
0+00			1.3	84.1	NH of Colima
+18.5			1.4	84.0	No curb line Colima
+34			1.5	83.9	& Colima & Sewer crossing
+34			1.96		Sewer M.H. 30' Rt
T.P.			1.76	83.63	
	5.03	88.66			
0+52.5			4.8	83.9	So. curb line Colima
+69.5			4.8	83.9	So. edge con. pavement
1+00			5.0	83.7	
+50			4.8	83.9	
2+00			4.6	84.1	
+50			4.4	84.3	
3+00			4.1	84.6	
+50			3.6	85.1	
4+00			3.3	85.4	

88.66

4+50	3.8	84.9	
5+00	5.0	83.7	
+03.4	5.0	83.7	begin 4" A.C. paving
+09	5.1	83.6	Elect. crossing
+10.5	5.1	83.6	No. curb of Alley
+34	5.3	83.4	So " " "
T.P.	10.15	78.51	

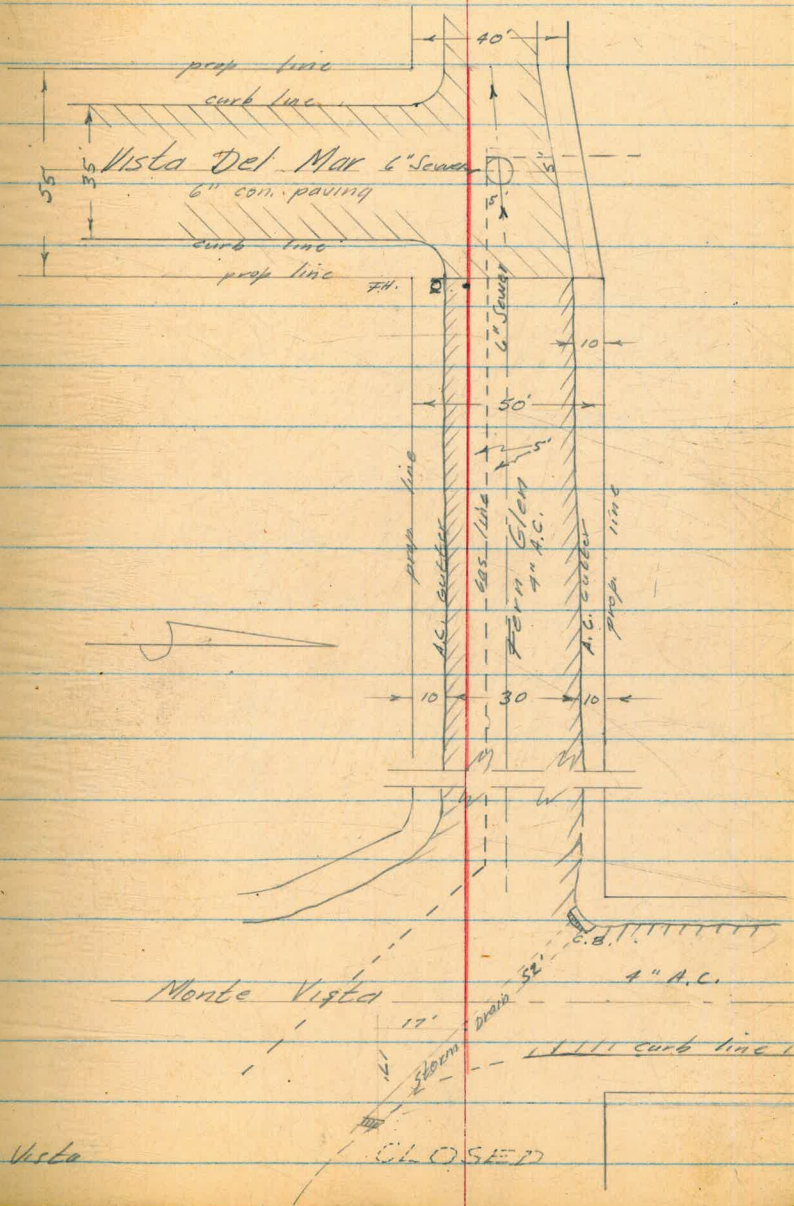
3.16 81.67

3.69 77.98 = 77.98

10-13-54

Profile & Proposed Water on
Fern Glen, Monte Vista to
Vista Del Mar

0+00	W/L of Vista Del Mar
+10	W curb " " "
+27.5	E Sewer & " " "
+45	E curb " " "
+55	E/H " " "
+56	F.H. & G.H.



5+03	Angle point in gas
5+07	Gas crossing
5+40	Sewer Crossing
5+50	Storm Drain Crossing
5+56	Curb line produce, E, Monte Vista

Profile Fern Glen Cont

			59.52	S.W. B.P. Monte Vista & Belvedere
	2.49	62.01		
T.P.			11.87	50.14
	1.96	51.60		
T.P.			10.51	41.09
	8.34	49.43		
0+00			12.5	36.93
				W/H Vista Del Mar
+27.5			11.4	38.03
				E Vista Del Mar & Sewer crossing
+27.5			11.38	38.05
				Sewer M.H. 10' 16" 4.5 to flow
0+50			10.9	38.53
+55			10.8	38.63
				E/H. of Vista Del Mar, edge of con. pave.
1+00			8.5	40.93
1+50			6.2	43.23
2+00			4.2	45.23
2+50			2.5	46.93
T.P.			2.05	47.38
	5.25	52.63		
3+00			4.5	48.13

Produced by J. Gray
 6-16-55

52.63

3+50 4.7 47.93

4+00 5.7 46.93

4+50 6.2 46.43

5+00 6.2 46.43

5+03 6.0 46.63

Angle point in Gas line 5' lb.

5+07 6.0 46.63

Gas crossing

5+90 4.9 47.73

& Monte Vista & Sewer crossing

5+50 4.6 48.03

5+56 4.5 48.13

E curb line produced on Monte Vista

T.P. 4.17 48.46

12.95 60.91

1.37 59.54

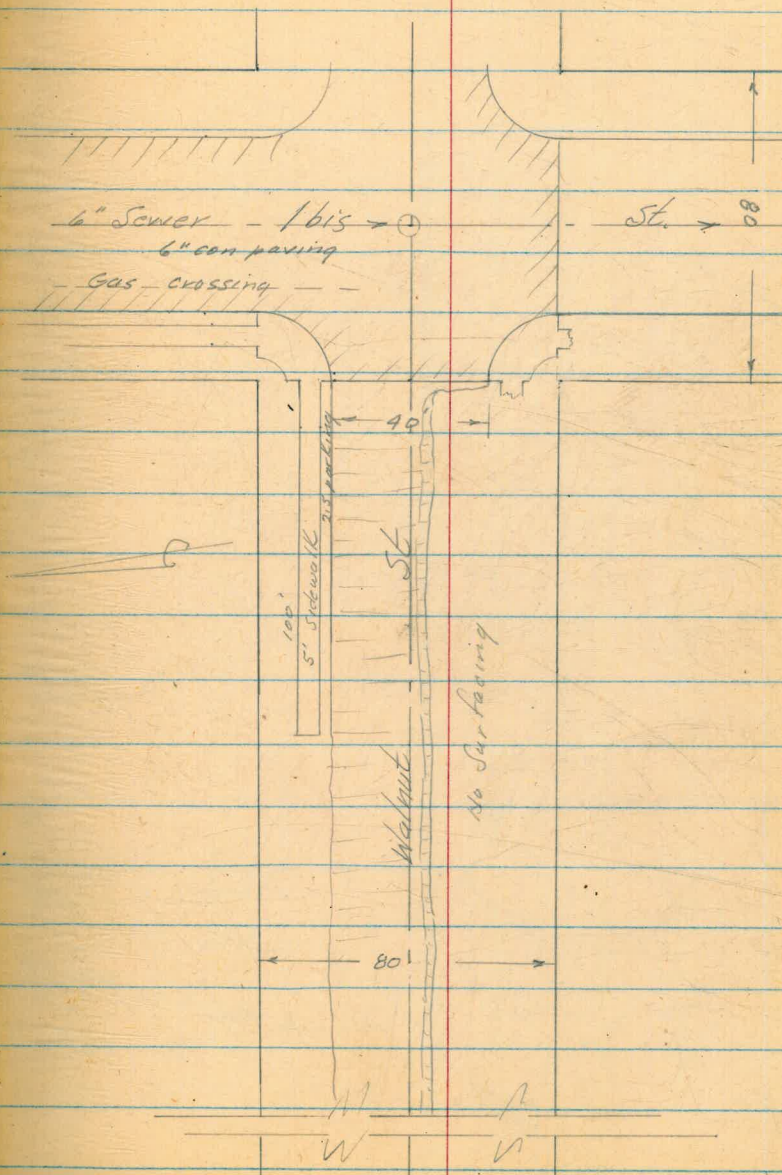
Wert
Kemp
Holahan

27

10-21-54

Profile & Proposed Water Line
Walnut St. 1bis to Jackdaw

0+00	E/H of 1bis
+14	E curb
+40	4 1bis & Sewer crossing
+54	Gas crossing
+80	W/H of 1bis



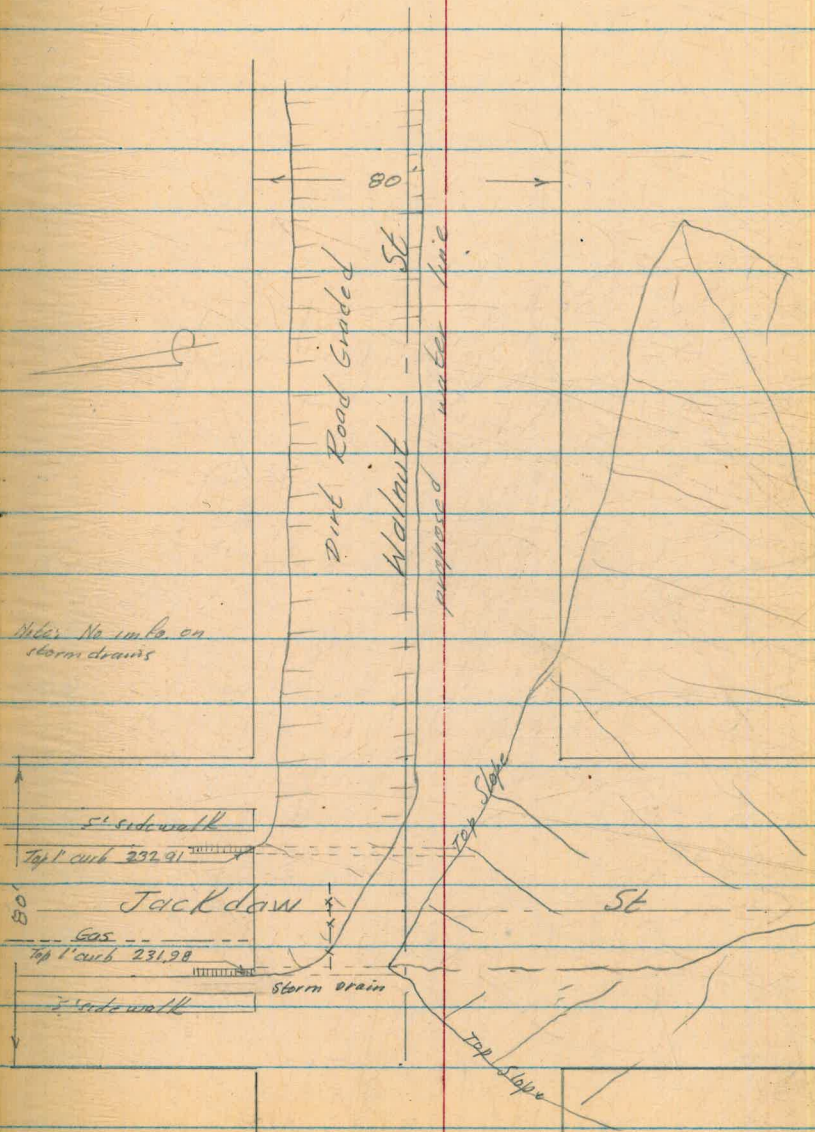
1+80 End 5' sidewalk

2+80

W/1 of Jackdaw

3+60

W/1 of Jackdaw



Profile Walnut Cont

			247.48	
4.43	251.91			
		6.58	245.73	
4.55	249.88			
		5.76	249.12	
5.10	249.22			
		3.91	245.81	
3.79	249.60			
0+00		6.2	243.4	
+14		6.0	243.6	
+40		5.8	243.8	
+40		5.69	243.91	
+50		5.8	243.8	
+54		5.7	243.9	
+60		5.7	243.9	
+80		5.6	244.0	
+83		4.4	245.2	

Brookes

NW BP. Brooks & Jackson

E/L of this St.

E curb line this St.

E this & Sewer crossing

Sewer MH. 10 ft

Eas crossing

W curb line this

W/L of this & edge of 6" concrete

	249.60								
0+83		4.4	245.2			$\frac{5.4}{10}$	$\frac{4.4}{8}$	$\frac{4.6}{10}$	
1+00		4.0	245.6			$\frac{5.3}{10}$	$\frac{5.2}{7}$	$\frac{9.0}{5}$	$\frac{9.0}{8}$
1+50		5.8	243.8			$\frac{6.3}{10}$	$\frac{6.7}{7}$	$\frac{5.6}{7}$	$\frac{5.8}{8}$
2+00		9.9	239.7			$\frac{10.2}{15}$	$\frac{10.6}{10}$	$\frac{9.6}{6}$	$\frac{9.9}{8}$
T.P.		12.86	236.74						
	1.77		238.51						
3+50		4.0	234.5			$\frac{3.0}{10}$	$\frac{4.0}{8}$	$\frac{5.2}{10}$	
4+84		6.2	232.3			$\frac{5.4}{10}$	$\frac{6.2}{8}$	$\frac{9.6}{6}$	$\frac{9.1}{10}$
3+00		10.2	228.3			$\frac{6.1}{10}$	$\frac{10.2}{8}$	$\frac{14.5}{10}$	
3+10		12.2	226.3			$\frac{6.7}{50}$	$\frac{6.3}{30}$	$\frac{5.2}{25}$	$\frac{7.3}{17}$
4+36		23.6	214.9			$\frac{7.8}{10}$	$\frac{9.9}{6}$	$\frac{12.2}{4}$	$\frac{18.2}{10}$
						$\frac{16.6}{10}$	$\frac{23.6}{8}$	$\frac{29.5}{10}$	

edge con.
281.8

232.3

233.3

231.2

230.7

228.6

226.3

238.51

3160

23.0

215.5

RE

16.

17.0

23.0

26.0

70070

T.P.

2.84

235.67

Sol TOM. N.E. #4. Jackdaw & Walnut

12.40 248.07

0.48

247.59

5.67 253.26

5.79

247.97

= 247.48 NW BR Brooks & Jackdaw

10-29-54

Profile & Proposed Water Main 7th Ave Cedar St to Date St

2+90

End 4.0 parking

1+80

Start 4.0 parking

0+60

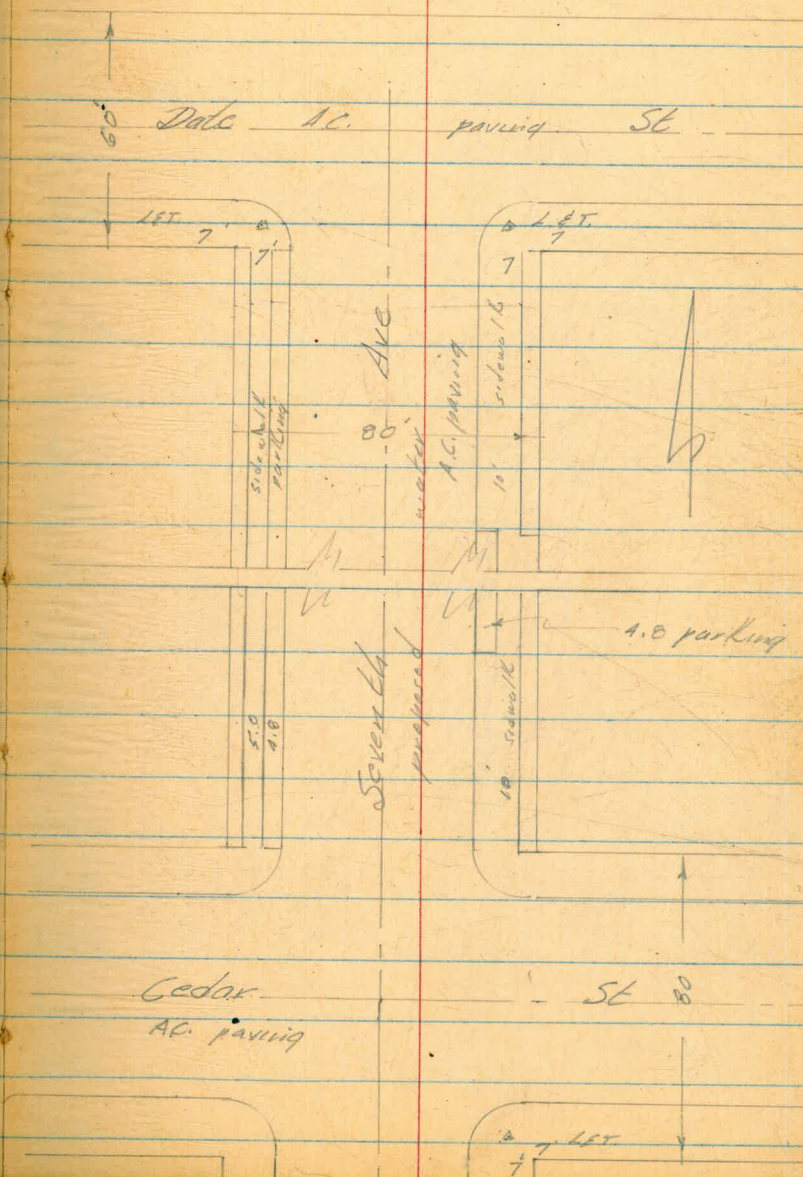
No curb

1+4

No curb

0+00

So. of Cedar



Seventh Ave Cont.

161.88

SE 89. Seventh & Cedar

3.06 164.94

0+00	4.1	160.8
+14	4.1	160.8
+50	4.5	160.4
+66	4.7	160.2
+80	5.0	159.9
1+00	5.1	159.8
+50	5.7	159.2
2+00	6.3	158.6
T.P.	6.42	158.52

3.76 162.28

2+50	4.3	158.0
3+00	5.4	156.9
+94	6.5	155.8
4+00	6.5	155.8
+46	7.0	155.3
+40	6.6	155.7

S/H at Cedar

So curb line

No curb line Cedar

GV. on line & 1/2 of Cedar

So curb line Dale St

No curb line Dale St.

Top curb.

162.28

T.P.

4.68 157.60

7.33 164.93

3.05 161.88

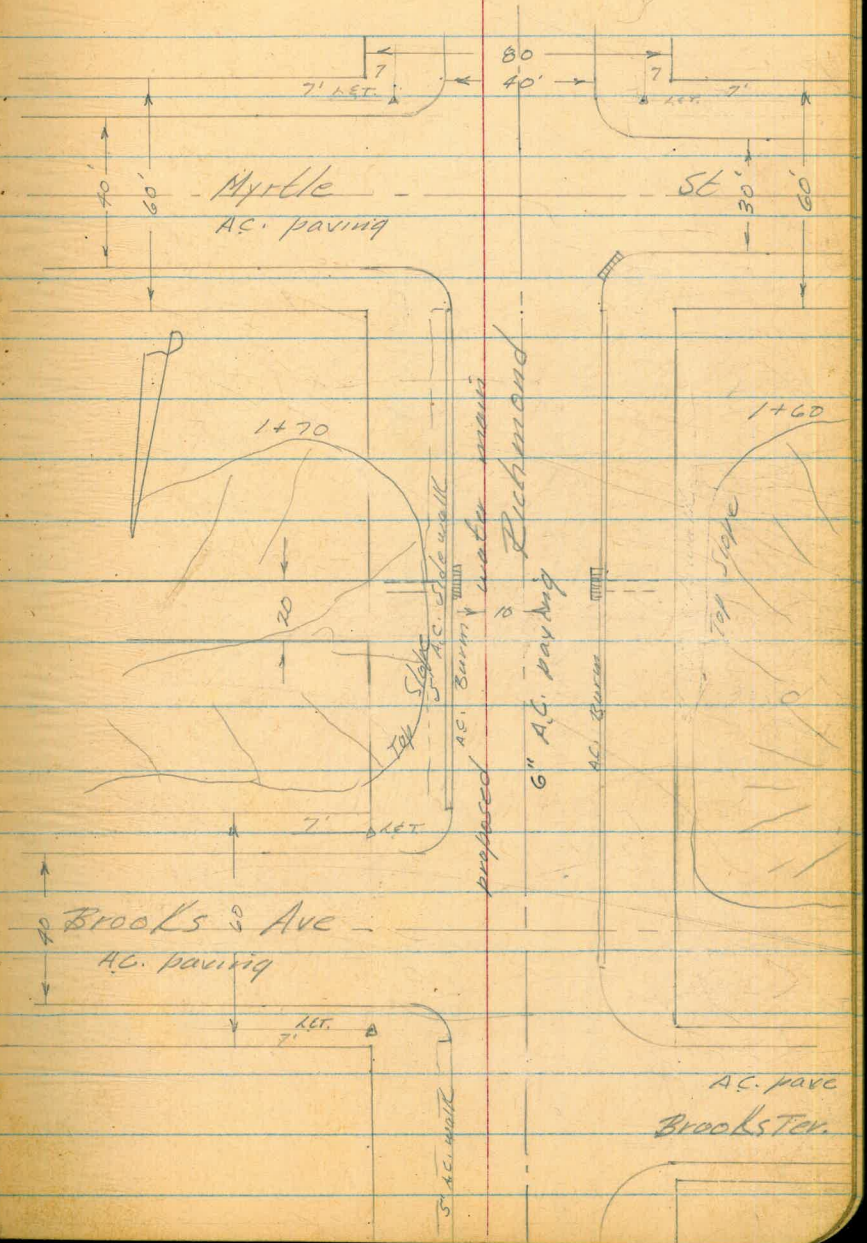
SEPP Seventh & Cedar

Wert
Kemp
Holahan

11-1-54 35

Profile & Proposed Water Main
Richmond St. Myrtle to Cypress

- 0+00 S/L of Myrtle St
- 1+10
- 2+10 S/L of Alley
- 2+30 N/L of Alley
- 2+40 3'x6' Storm Drain (no crossings)
- 3+00 S/L of Brooks
- 4+40 N/L of Brooks
- 4+40 So. curb line of Brooks Terrace
- 4+43 & water G.V. opposite Sewer M.H. Brooks Terr.
- 4+55 & Sewer M.H. Brooks Terrace
- 4+70 No curb line Brooks Terrace



Richmond St. Cont.

5+90

S/L Alley

6+10

N/L Alley

7+50

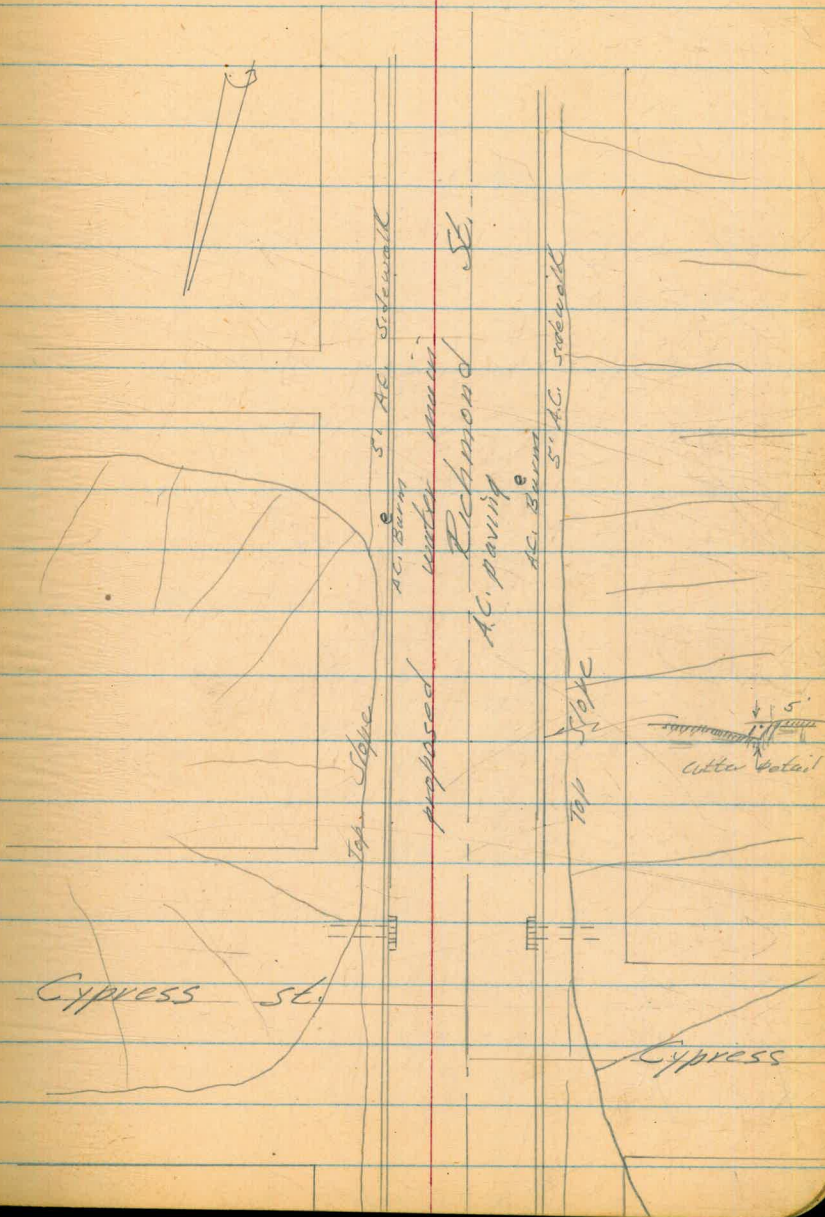
S/L of Cypress

7+70

Storm Drains (3'x6' no crossing)

8+30

N/L of Cypress



Profile of Richmond Cont

280.04

134 281.38

0+00	2.1
+10	2.3
+50	3.2
1+00	4.4
+50	6.5
2+00	9.0
+25	9.58
+50	10.8
3+00	9.5
+50	6.6
+90	4.5
4+00	4.0
+30	3.3
+50	3.0
5+00	4.3

S/H of Myrtle

So. curb line

No. curb line

Sewer M.H. 10' 11"

So curb line Brooks Ave

No " " " "

Richmond Cont

-	2.58	280.04	
1.34	281.38		
0+00	2.1	279.3	
+10	2.3	279.1	
+50	3.2	278.2	
1+00	4.4	277.0	
+50	6.5	274.9	
2+00	9.0	272.4	
2+25	9.58	271.8	
T.P.	9.58	271.80	
1022	282.02		
2+50	10.8	271.2	
3+00	9.5	272.5	
+50	6.6	275.4	
+90	4.5	277.5	
4+00	4.0	278.0	
+30	3.3	278.7	

So curb line Brooks Ave

No " " " " "

Richmond Cont

282.02

4+50 3.0 279.0

5+00 4.3 277.7

T.P. 6.92 275.10

0.58 275.68

5+50 1.7 274.0

6+00 6.5 269.2

+50 11.2 264.5

7+00 14.0 261.7

T.P. 13.29 262.39

7.56 269.95

7+50 9.2 260.8

8+00 8.5 261.5

+30 6.7 263.3

T.P. 7.52 262.43

12.78 275.21

T.P. 0.28 274.93

12.61 287.54

1.33 286.21

N/I of Cypress

Richmond Cont

10.67 296.88

4.81 292.07

6.43 298.50

4.45 294.05

299.05 S.W. B.P. Robinson & Richmond

11-9-54

Profile of Proposed Water Main
Franklin Ave Evans St to 25th St

		94.98	
0.64	95.62		
		12.85	82.77
0.86	83.63		
		12.60	71.03
6.55	77.58		
		2.50	
0+00		7.2	70.4
+10		7.9	69.7
+50		6.3	71.3
1+00		5.2	72.4
+50		3.9	73.7
2+00		2.8	74.8
+50		1.8	75.8
3+00		0.7	76.9
TR		0.05	77.53
8.22	85.75		

NE. BR. Ocean View & Evans

Set T.B.M. F.H. SE cor Franklin & Evans

W/L of Evans

W curb line

E curb & edge of 4" A.G.

Franklin Ave. Cont.

85.75

3+50	7.8	78.0
4+00	6.8	79.0
+50	5.9	79.9
5+00	5.1	80.7
+50	4.4	81.4
6+00	3.8	82.0
+50	3.6	82.2
6+60.35	3.6	82.2
+70.35	3.8	82.0
+90.35	3.4	82.4
7+00	3.5	82.3
7+10.35	3.7	82.1
+20.35	3.4	82.4
+50	3.0	82.8
T.P.	2.85	82.90

5.12 88.02

W/L of Sampson
 W curb line
 of Sampson
 E curb line
 E/L of Sampson

Franklin Ave Cont

88.02

8+00 5.0 83.0

+50 4.8 83.2

9+00 4.8 83.2

+50 4.7 83.3

10+00 4.9 83.1

+07 5.1 82.9

+07 4.4 83.6

T.P. 3.09 84.93

7.30 92.23

364 88.59

4.47 93.06

202 91.04

F gutter 28th St. & water produced

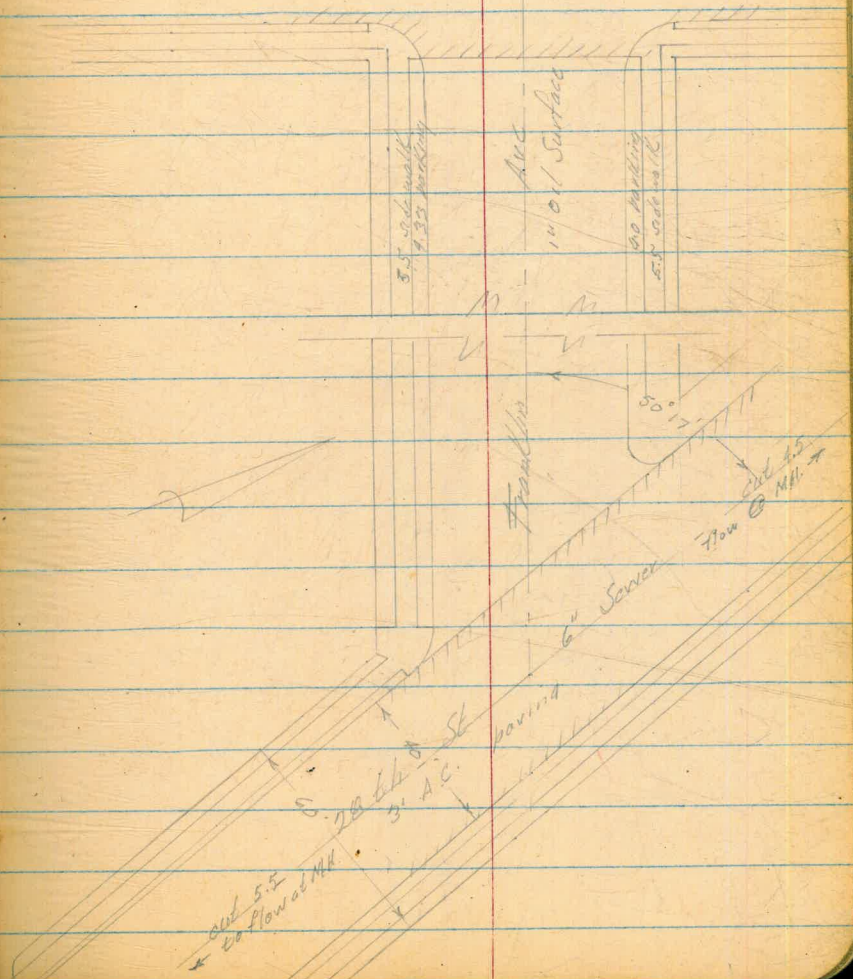
Top curb " " " " "

Sub T.B.M. Top F.H. 28th & Franklin

91.05 NE. B.P. 28th & Ocean View

Franklin Ave Cont.

Sampson - - - - - Ave.
6" con. paving

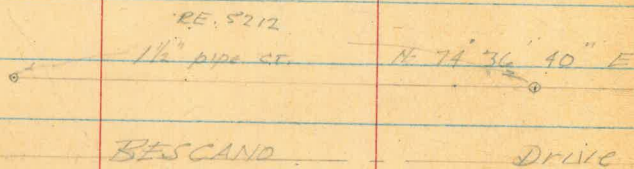


Mutlands 12" Feeder Line
La Jolla Scenic Dr to Bescano Dr

Wert
Kemp
Holahan

46

12-7-54



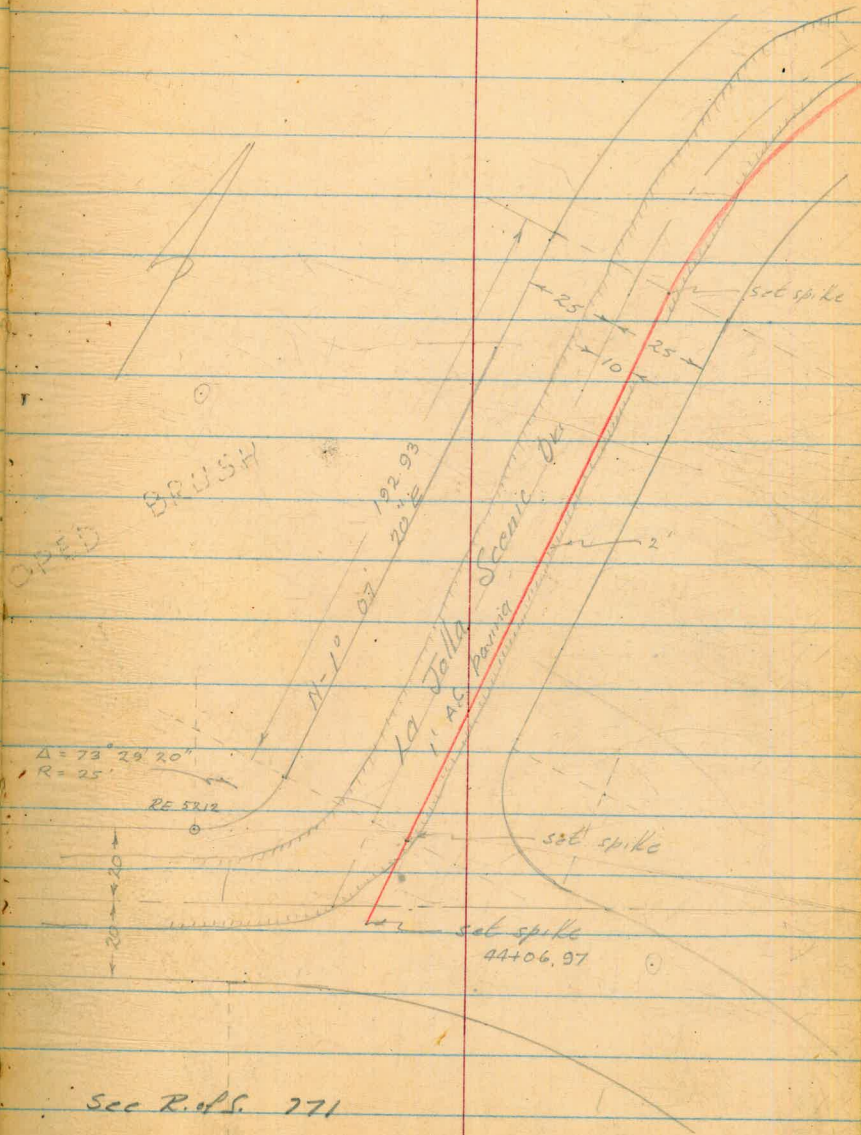
UNDEVELOPED BRUSH

$\Delta = 73^\circ 29' 20''$
 $R = 25'$

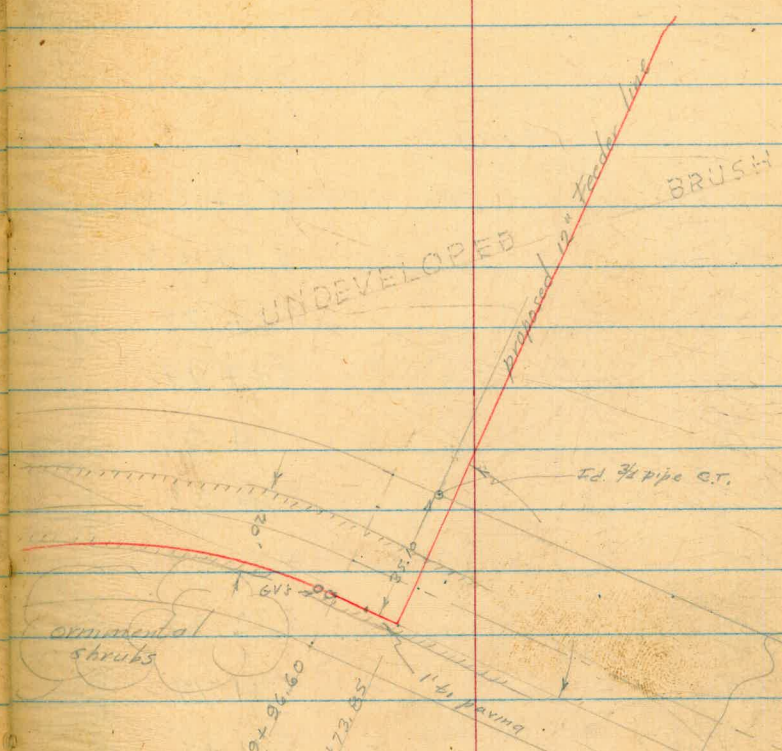
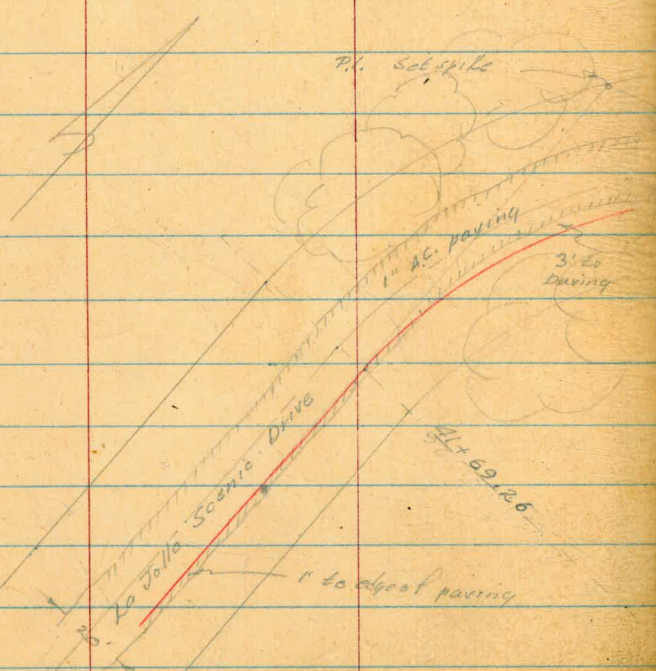
RE 5212

20'

See R.O.S. 771



Munklands 12" Feeder Line Cont



$A = 73.07$
 $ER = 150.10$
 $T = 103.82$
 $R = 140'$
 $L = 178.66$

$BC = 39 + 91.60$
 $CA = 39 + 73.85$

See Roll 221

Muirland 12" Feeder Line Cont.

535.43

TBM, 3/4" prop pipe 3.75 PL Sta 39+38.85

396 539.39

39+73.85 4.7 534.69

A point 90° 03' PL

+96.60 4.7 534.69

B.C.

40+00 4.6 534.79

+75 4.6 534.79

+50 5.0 534.39

+75 5.1 534.29

41+00 5.7 533.69

+25 6.6 532.79

+50 7.6 531.79

+69.26 7.9 531.49

TP 7.73 531.66

592 537.58

42+00 6.9 530.66

+50 8.4 529.16

43+00 9.8 527.76

Elev. Reduced By Palom 1770 12-15-58

E.C.

Muirlands Fender Line Cont.

	527.58	
43+50		11.4 526.18
+62.19		12.0 525.58
44+06.97		13.4 524.18
		9.98 527.60
		7.86 529.72
8.06	527.78	
		5.90 731.88
8.04	539.92	
		4.51 535.91

B.C.

P.L. water lines

(Marked 528.88)

Old T.B.M. NE. cor. Scenic Dr. & Bescano Dr

Set T.B.M. NW prop pipe " "

3/4" pipe 394 38.85

MUIRLANDS 12" FEEDER LINE
STR'S & GRD'S.
①

SHOREY
MARTEL
KELLHOPPER

3/31/55

50

TBM	3.25	538.68	535.43	
43+84. ⁰⁰ END OF WORK 3" B.O.	13.5	525.2	520.7	C45 ±
43+52 CORP. COCK	12.3	526.4	521.8	C46
43+50	12.3	526.4	521.8	C46
43+00	10.5	528.2	523.3	C42
42+50	9.0	529.17	524.9	C42
42+00	7.7	531.0	526.5	C45
41+69.26 AH, } E.C. 41+75.26 BK, } EQ.	6.8	531.9	526.9	C50
41+50	6.0	532.7	527.4	C53
41+25	5.3	533.4	527.8	C56
41+00	4.7	534.0	528.2	C58
40+75	4.2	534.5	528.7	C58
40+50	3.6	535.1	529.7	C60
40+25	3.4	535.3	529.8	C55
40+00	3.5	535.2	530.0	C52
39+96. ⁶⁰ B.C.	3.5	535.2	530.1	C51
39+91. ⁰⁰ AH, } Δ PT. 39+85. ³⁰ BK, }	4.0	534.7	530.2	C45
39+50	3.5	535.2	530.3	C42
TD 12.73 547.93	3.48	535.20		
39+25	11.5	536.4	530.5	C52
39+00	9.9	538.0	532.0	C60
38+50	7.3	540.6	535.1	C55

3/4" PROT PIPE 3.75 RT. STA. 39+38.85 (Pg. 48)

PLANS SHOW E.O. AT 43+62.¹² - IN ERROR; E.O. AT 43+89

Muir Lands 12" FEEDER LINE
(STK'S & GRD'S) CONT'D.

⑥

547.93

38+00			4.7	543.2	538.6	C4E
37+50 TP	10.61	557.07	1.47	546.46	541.8	C4Z
37+00			7.4	549.7	545.0	C4Z
36+60			5.4	551.7	547.3	C4T
36+58 ⁸⁰			5.5	551.6	547.3	C4Z
36+51 ⁸⁰			5.3	551.8	547.3	C4S
36+50			5.2	551.9	547.3	C4E
36+36 ³⁰ 12" 8 1/2" TEE			5.3	551.8	547.4	C4T
36+36 ³⁰ 90° BEND				552.5		C5L
36+00			3.0	552.1	547.5	C4E
CK.			4.9	552.2 = 552.2		
SET TBM	11.15	564.36	3.86	553.21		
35+72 ^{CA} 90° BEND			12.4	552.0	547.5	C4S
35+72 ^{CA}			12.4	552.0		C4Z
35+75			11.8	552.6	547.6	C5E
35+50			10.5	553.9	548.8	C5L
35+00			8.0	556.4	551.1	C5Z
34+50			5.9	558.5	553.4	C5L
34+00			3.8	560.6	555.8	C4E
33+50			1.7	562.7	556.2	C6S
33+00 TP	5.73	569.71	0.38	563.98	556.8	C7Z
32+50			5.1	564.6	557.2	C7E

SHOREY 9/21/55
MARTEL
KELLHOFFER

552.5

51.

& PROFILE STA. 35+79⁵⁴ (F.B. 825-34)

END CONC. BIK. WALL AT DRIVEWAY 25' LT. STA. 35+79⁵⁴

MURKLANDS 12" FEEDER MAIN

⑥ STR'S & Gnds. (CONT'D)

SHOREY 4/5/55
MARTEL
KELLHOFER.

52

569.71

22+00		51	564.6	557.1	C6 ⁸
31+50		5.3	564.4	558.3	C6 ¹
31+00		5.7	564.0	558.8	C5 ³
30+50		5.7	564.0	559.3	C4 ²
30+00		4.6	565.1	559.8	C5 ³
29+62 ³⁶ A	1 12" x 12" TREE	4.2	565.5	560.2	C5 ³
29+62 ³⁶		4.2	565.5		C5 ³
29+57	S.V. 12"	3.6	566.1	560.3	C5 ⁸
R	6.18 571.81	4.08	565.63		
29+50		6.0	565.8	560.4	C5 ⁴
29+00		4.9	566.9	560.8	C6 ¹
28+50		4.7	567.1	561.3	C5 ⁸
28+00		4.7	567.1	561.8	C5 ³
27+50		5.0	566.8	561.8	C5 ⁰
27+00		4.7	567.1	561.9	C5 ²
26+62	A.H. } EQ. 45° BEND.	4.5	567.3	562.0	C5 ³
26+55	B.K. }				
26+42	15° BEND	4.1	567.7	562.1	C5 ⁶
26+00		2.7	569.1	562.3	C6 ⁸
25+50		2.1	569.7	562.5	C7 ²
25+00		2.0	569.8	562.8	C7 ⁰
24+50		1.9	569.9	563.0	C6 ⁹

MUIRLANDS 12" FEEDER MAIN

① STR'S & GUD'S (CONT'D)

SHOREY 1/5/55
MARTEL
KELLHOFER

53

571.81

24+00			2.2	569.6	563.4	C ₆ ²
23+89 ³² P.O.C. OK.			2.1	569.7	563.5	C ₆ ²
TBM	5.38	575.44	1.8	570.0 = 569.9		
23+89 ³² P.O.C.			1.75	570.06		
23+75			5.9	569.5	563.5	C ₆ ²
23+50			5.9	569.5	562.5	C ₆ ²
23+31 ⁰³ (B.C.)			5.8	569.6	563.6	C ₆ ²
23+00			6.1	569.3	563.7	C ₅ ⁶
22+50			5.7	569.7	563.9	C ₅ ⁸
22+00			5.6	569.8	564.1	C ₅ ⁷
21+50			4.9	570.5	564.3	C ₆ ²
21+48 ¹⁴ EC			5.3	570.1	564.6	C ₅ ⁵
21+25			5.3	570.1	564.6	C ₅ ⁵
21+00			5.2	570.2	564.7	C ₅ ⁵
20+75			4.9	570.5	564.8	C ₅ ²
20+50			4.5	570.7	564.5	C ₆ ⁴
20+25			4.6	570.8	564.3	C ₆ ⁵
20+00			4.3	571.1	564.0	C ₇ ¹
19+75	4.76	575.62	4.6	570.8	563.8	C ₉ ²
19+50			4.58	570.86		
19+25			5.4	570.2	563.6	C ₆ ⁶
19+00			7.5	568.1	562.8	C ₅ ³

Made out cut sheets

23+89³² to 43+84² 1/5/55

E STA. AT 23+89³² P.O.C. (K.B. 895-32)

SET NAIL IN P.P. NO 6231 12' FROM 23+89³²

MUIRLANDS 12" FEEDER
(Cont'd)

4/19/55
4/20/55

54

575.62

19+38 ²⁷ B.C. OK.		8.5	567.1	562.0	C4 ²
TBM	1.97	574.86	7.1	568.5 = 568.4	ON STA 19+38 ²⁷ B.C.
			2.73	572.89	SET TBM ON IRON PIN 25' RT STA 19+38 ²⁷ B.C.
19+00		9.7	565.2	561.2	C4 ⁰
18+50		10.0	564.7	559.6	C4 ³
18+00		10.3	564.6	558.0	C6 ⁶
17+50		11.7	563.2	556.4	C6 ⁸
17+46 ⁴⁶ E.C.		11.8	563.1	556.4	C6 ²
17+25		12.4	562.5	555.6	C6 ²
TP	1.23	563.09	13.00	561.86	
17+00		1.9	561.2	554.8	C6 ⁴
16+75		2.6	560.5	554.0	C6 ⁵
16+50		3.2	559.7	553.2	C6 ²
16+25		3.7	559.4	552.8	C6 ⁶
15+99 ³⁸ B.C.		3.9	559.2	552.4	C6 ⁸
15+50		5.1	558.0	551.6	C6 ⁴
15+00		6.6	556.5	550.7	C5 ⁸
14+50 ²⁷ E.C.		7.9	555.2	549.9	C5 ³
OK. TBM		7.69	555.40 = 555.40		ON IRON PIN 25' RT. 14+50 ²⁷ E.C.
14+25		8.3	554.8	549.4	C5 ⁴
14+00		7.9	555.3	549.0	C6 ³
13+75		7.6	555.5	548.6	C6 ²

4/20/55

55

MUIRLANDS 12" FEEDER

(Cont. d.)

563.09

13+71 ⁵²	BC		2.6	555.5	548.4	C7 ¹
13+70 ¹¹	EC		7.7	555.4	548.4	C7 ²
13+50			8.2	554.9	547.6	C7 ³
TP	1.18	556.86	7.41	555.68		
13+25			3.0	553.9	546.5	C7 ⁴
13+00			4.4	552.5	545.5	C7 ²
12+75			5.8	551.1	544.4	C6 ²
12+50			7.3	549.6	543.4	C6 ³
12+25			8.7	548.2	542.0	C6 ³
12+00			10.0	546.9	540.5	C6 ⁴
11+82 ⁰⁵	B.C		10.8	546.1	539.5	C6 ⁶
11+50			12.3	544.6	537.6	C7 ²
TP	0.47	544.04	13.29	543.59		
11+00			1.2	542.8	534.7	C8 ¹
10+50			6.9	537.1	531.8	C5 ³
10+30 ⁹⁰	AH } EC		9.5	534.5	530.7	C3 ⁸
10+31 ⁸⁶	BK		10.4	533.6	530.6	C3 ⁶ C3 ⁰
10+25			10.5	533.5	529.0	C4 ⁵
10+00						
9+75			10.4	533.6	527.6	C6 ²
9+50			11.3	532.7	526.2	C6 ⁵
9+25	TP	2.58	13.21	530.83	524.8	C6 ²
9+00			4.3	529.1	523.3	C5 ⁸

✓

MURLANDS 12" FEEDER
Cont'd.

4/20/55

527.2

56

533.41

8+75		6.7	526.7	521.9	C48	
8+65	F.H. TEE	6.4	527.0	521.3	C52	
	⑤ F.H.	2.9	530.5	527.8	C9 ² to ell C27 to flange	
8+55.99	(Δ = 84°21' RT.) B.C. 12" TEE	6.6	526.8	520.8	C6° RT. ⑧	
		6.4	527.0		C6 ² LT. ⑥	
CK & STA. TBM		6.2	527.2 = 527.3		8 STA. 8+55 ²³ B.C.	
8+50	1.80 528.73	6.48	526.93	519.8	TBM SET ON 1/2" IRON PIPE NE. DRIVEWAY	
		2.3	526.4			
8+25		9.5	519.2	514.5	C47	⑥ LT C72
TD	0.06 516.16	12.63	516.10			⑥ LT C57
8+00		1.8	514.2	509.9	C43	⑥ LT C48
7+50		10.8	505.4	500.9	C45	⑥ LT C48
TD	0.24 503.53	12.87	503.29			
7+00		8.0	495.5	491.2	C43	
				491.8		
6+98.14	AH. EQUA (X PT)	8.1	495.4	491.0	C48 ⑧ LT	
		8.8	492.7	491.8	C29 C37 ⑥ RT	⑥ LT C47
6+92.39	BK. (Δ 37°39' LT)	11.21	492.12 = 492.93			
6+75	CK TBM	10.4	493.1	488.2	C47	
CK TD		8.61	494.92 = 495.01		(3/4" I.P. 5' 5/8")	
6+66.26	(X PT Δ = 22°36' RT)	11.8	491.7	486.4	C53	
6+62.5	0.98 491.76	12.75	490.78	486.0	C52 C48	
				485.6		
6+50		3.7	488.1	483.5	C64 C46	
				481.7		
6+37.5		5.7	486.1	481.0	C47 C51	
				477.2		
6+25		8.3	483.5	478.5	C47 C50	
				477.8		
6+12.5		10.8	481.0	476.0	C45 C50	
				471.5		
PL 00	0.26 479.10	12.92	478.84	474.0	C48	
				470.2		
5+87.5		2.8	476.3	472.2	C41	
				470.5		
5+75		3.9	475.2	470.5	C47	
				469.5		

NOTE: pipe moved 10' LT (new)
Sta. 6+12.5 to 5+87.5
4/24/55 DEATHY
As per instructions from
W.C. Brown & B. Huntington

MUIRLANDS 12" FEEDER
(Cont'd.)

4/26/55

57.

	279.10		(Rev. Grd)				
5+50		5.3	473.8	469.0	C18	473.8	
5+375		9.1	470.0	461.0	C90	469.5	5+42
IP	0.96	467.41	12.65	466.45		9.6	.6.0
5+328.1	P.I. Δ = 48°35' RT	3.6	463.8	458.1	C57	466.0	
5+25		10.2	457.2	453.0	C42	460.4	
		10.1	457.3		C43	7.0	
5+100		11.9	455.5	451.0	C45	455.6	
4+75	P.I. Δ = 45° LT	12.9	451.5	448.0	C65	459.5	
	4.61	459.15	12.87	451.52		12.9	
4+50		7.5	451.65	447.2	C45	451.9	
4+36.18						7.5	
4+36.30	P.I. Δ = 45° LT	8.0	451.2	447.0	C42	451.31	
CK. BM	0.30	452.37	7.08	452.07 = 452.83	BP End curb return	7.52	
4+25		2.04	450.33	445.8	C45	7.00	
				446.4			
4+00		3.81	448.56	444.5	C45	3.78	
				Rev. Grd			
3+50		7.30	445.07	440.6	C45	7.27	
3+00		10.80	441.57	437.1	C45	10.76	
IP	0.96	440.19	13.14	439.23			
2+50		2.14	438.05	433.6	C45	2.12	
CK. BM		2.94	437.25 = 438.00		Chis x (City)		
2+00		5.66	434.53	434.00	C45	5.68	
1+67.56	P.C.C.	7.88	432.31	427.8	C45	7.84	
1+50		9.48	430.71	426.2	C45	9.52	

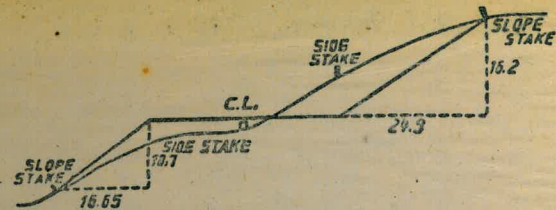
NOTE: E pipe
moved 15' LT.
from beginning
to 2 pt 4+36.18
4/27/55.

4/27/55

Muirlands 12" FEEDER

	240.19		
1+25		11.41	428.78
TP	0.36	427.47	1308 427.11
1+00		0.60	426.87
0+75		2.60	424.87
0+50		4.27	423.25
0+27.7	P.C.C	5.70	421.77
0+25		5.85	421.62
CK BM		9.30	418.17 = 418.33

c45	11.51
c45	
c45	0.74
c45	2.75
c45	4.41
c45	5.92
c45	6.07
DD. on Lamp Base	



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

THE NATIONAL BLANK BOOK COMPANY
 HOLYOKE MASSACHUSETTS
 NEW YORK CHICAGO BOSTON SAN FRANCISCO