

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

ROLLMEP  
MAY 1965

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut, subtract if fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

88

Please Return to  
City of San Diego Water Dept.  
Room 903 Civic Center

(15)

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.21	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.12	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.890	.987	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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alicia

Alley BIK 61  
 N of Madison E of 33rd  
 Proposed PL

11-2-53

7+26 06 + North prop line - Alley

7+19 Sewer MH 301+

Water Meters

0+94 9' RT  
 1+05 9' RT  
 1+09 9' RT  
 1+33 10' RT  
 1+60 10' RT  
 2+22 10' RT  
 2+66 10' RT  
 3+39 10' RT  
 3+80 10' RT  
 4+30 10' RT  
 4+62 10' RT  
 5+30 10' RT  
 6+79 10' RT  
 6+39 9' RT

Water Meters

0+78 3' RT  
 0+83 3' RT  
 1+25 6' RT  
 1+78 3' RT  
 2+34 3' RT  
 2+96 3' RT  
 3+41 5' RT  
 3+79 5' RT  
 4+37 5' RT  
 4+87 3' RT  
 5+51 3' RT  
 5+89 3' RT  
 6+38 3' RT

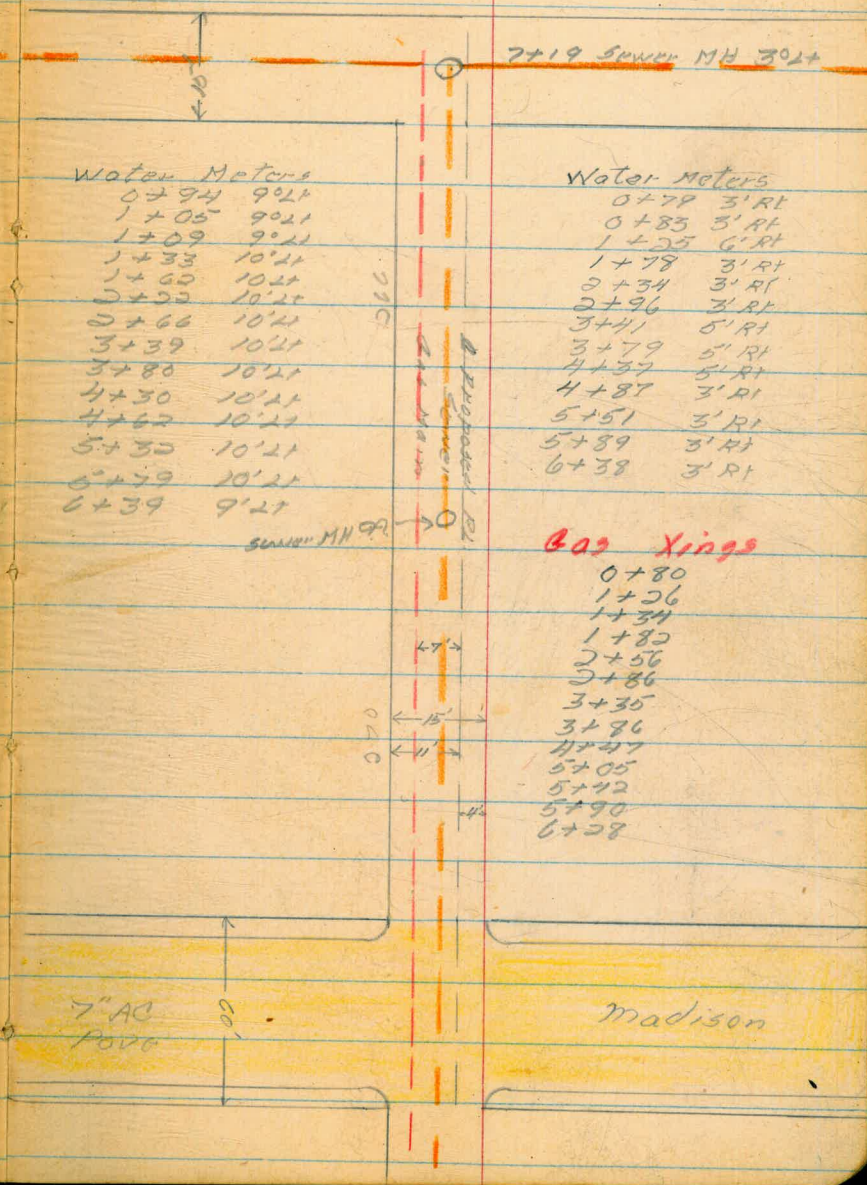
Gas Xings

0+80  
 1+26  
 1+34  
 1+80  
 2+56  
 3+86  
 3+35  
 3+96  
 4+47  
 5+05  
 5+42  
 5+90  
 6+28

7" AC  
 1000

Madison

0+00 South prop line Madison



10-30-53

West  
Williams  
Voronofokis  
Kemp

	641	387.42	381.01
0	7.36	391.33	345 383.97
0+00		7.74	383.59
+13		7.96	383.37
+47		7.65	383.68
0+50		7.64	383.69
+60		7.25	384.08
1+00		6.8	384.53
+50		6.4	384.93
2+00		6.3	385.03
+50		5.8	385.53
3+00		5.7	385.63
+50		5.0	386.33
4+00		4.7	386.63
+50		4.4	386.93
5+00		3.6	387.73
+50		4.1	387.23
6+00		4.0	387.33
+50		3.9	387.43

S-E BP Madison + Bancroft

South prop line madison

Cutter line

Cutter line

edge of

391.33

7+00  
7+19 ok  
126

3.2 388.13  
3.7 387.63 + 4.5 to flow  
3.1 388.23

383.13

TOP SEWB MH 30H

2.26 390.41

3.18 388.15

3.34 387.49

6.26 384.15

6.46 381.03 = 381.03

Alley BIK A E of 35<sup>th</sup>  
N of Meade

West  
Williams  
Varontakis  
Kemp

4

7+42 + North Prop Line Meade

8" AC

Water Meters  
6+72 10' RT

Meade

Water Meters

1+47 3' RT  
1+98 2' RT  
2+32 2' RT  
2+64 2' RT  
2+88 3' RT  
3+32 1' RT  
3+73 1' RT  
4+15 2' RT  
4+58 2' RT  
5+09 3' RT  
5+54 3' RT  
5+57 3' RT  
6+18 3' RT  
6+64 3' RT

3+00 end 2" O.I.

Gas Xings

1+44 5+16  
1+86 6+47  
2+19 5+64  
2+50 6+24  
3+04 6+45  
3+36 6+45  
3+66 6+45  
4+23  
4+61

Sewer MH 0+82 3' RT

8" AC PVC

FD 2+136

0+50 Gas Xing

Meade

0+18 Gas Xing

0+31 Water Xing

0+00

South Prop Line Meade

Wilson St

Profile Alley B1k A

West  
Williams  
Varon Fokus  
Kemp

11-3-53

5

	5.56	392.37	386.81
0+00		4.82	387.9
+50		4.64	387.7
+67		5.1	387.3
+81		4.53	+4.5 To Flow
1+00		3.58	388.8
+50		2.35	390.0
2+00		1.82	390.5
+50		1.68	390.7
3+00		1.26	391.1
+50		0.7	391.7
	5.17	397.02	0.55 391.85
4+00		5.2	391.8
+50		5.4	391.6
5+00		5.2	391.8
+50		4.8	392.2
6+00		4.2	392.8
+50		4.5	392.5
		5.40	

BM NW BP 35<sup>th</sup> + Meade

Crater Line north side

Top Foot Run Sewer NH 3<sup>rd</sup> Lt

edge AC pave



292.02

7+42

5.49

391.5

142 392.53 5.91 391.11

5.65 386.89 = 386.89

6

Alley BIK C N of Meade  
Alley BIK E E of 36th

West  
Williams  
Varonakis  
Kemp

11-4-53

Monroe  
8"  
AC Pave

Water Meters

1+47 11' 21"  
2+04 11' 21"  
2+34 11' 21"  
2+58 11' 21"  
3+42 11' 21"  
3+99 11' 21"  
3+33 11' 21"  
4+71 11' 21"  
5+05 11' 21"  
5+09 11' 21"  
5+44 11' 21"  
5+80 11' 21"  
6+40 11' 21"

Water Meters

FD 1/2" 10  
5' 00"

1+45 10' RI  
1+46 10' RI  
1+93 10' RI  
2+10 10' RI  
2+77 10' RI  
3+01 5' RI  
3+59 10' RI  
4+03 10' RI  
4+54 10' RI  
5+05 30' RI  
5+14 5' RI  
5+51 10' RI  
5+90 10' RI  
6+40 10' RI

Gas Xings

1+42  
1+93  
2+20  
2+49  
2+76  
3+10  
3+46  
4+19  
4+63  
4+92  
5+07  
5+72  
5+95

Gas Main 80"

0+50 Gas Xing

0+30 Water Xing

Meade

8" AC Pave

0+00

South prop Line Meade

Monroe

Alley BIK C + F Cont'd

8

14+43

N Prop Line Madison

~~14+24 No Xing~~

~~14+07 Water Xing~~

Madison St

6" Ac Pipe

2 Gas 6" LT

Water Meters

8+38 11' LT  
 8+81 11' LT  
 9+16 11' LT  
 10+02 11' LT  
 10+62 11' LT  
 11+15 11' LT  
 11+54 11' LT  
 12+03 11' LT  
 12+53 11' LT  
 12+89 11' LT  
 13+93 11' LT  
 13+31 11' LT  
 13+95 11' LT

2 Water Main 10" LT

Water Meters

8+04 2' RT  
 8+56 2' RT  
 8+59 2' RT  
 9+15 2' RT  
 9+58 3' RT  
 10+15 2' RT  
 10+61 1' RT  
 11+17 1' RT  
 11+63 1' RT  
 11+99 1' RT  
 12+31 1' RT  
 12+65 1' RT  
 12+87 10' RT  
 13+18 1' RT  
 13+37 1' RT  
 13+63 1' RT

Gas Xings

7+77  
 8+14  
 8+45  
 8+81  
 9+07  
 9+54  
 10+04  
 10+75  
 11+00  
 11+54  
 11+98  
 12+36  
 13+60  
 13+60  
 13+27  
 13+43

11-4-53

6.23 392.91 386.68

BM SE BP Monroe + Cherokee

4.28 391.84 5.35 387.56

0+00 2.17 384.7

South prop line made

+50 6.97 384.9

+67 7.46

Butter line north side

0+80 7.2 384.6

6.9 384.9  
11.21 385.3  
5.4 386.4 edge of road

1+00 5.7 386.1

5.8 386.0  
11.21 386.3  
4.9 386.9

+50 5.3 386.5

5.5 386.5  
11.21 386.5  
4.9 386.6

2+00 5.2 386.6

5.3 386.5  
11.21 386.5  
4.9 386.6

+50 5.2 386.6

5.3 386.5  
11.21 386.5  
4.9 386.6

3+00 5.1 386.7

5.0 386.8  
11.21 386.8  
5.1 386.7

+50 4.6 387.2

4.5 386.8  
11.21 386.8  
4.5 387.3

3+83 5.28

Top SWMP 11.1 3.5 2.1

3+87 3.62

4.0 13.5 RT Begin Cone

4+00 4.2 387.6

3.6 387.2  
11.21 387.2  
4.0 387.8

4+04 3.04

13.5 RT End Cone

5.64 393.47 4.01 387.83

3.6 387.2  
11.21 387.2  
4.0 387.8

4+50 5.6 387.9

3.6 387.2  
11.21 387.2  
4.0 387.8

+58 5.08

14.5 RT Basin cone Garage Floor

393.47

4+77		5.02	
4+81		5.11	
4+93		5.09	
4+93		4.74	
5+02		4.72	
5+00		5.2	388.3
5+21		5.32	
5+30		5.06	
+50		4.9	388.6
6+00		4.3	389.2
+50		4.1	389.4
+62		5.41	
6+82		5.68	387.79
+93		5.89	387.58
7+00	5.10	392.99	5.58 387.89
+32		5.34	387.65
+50		4.3	388.7
8+00		3.3	389.7
+50		3.4	389.6

End cone Garage Slab

9° RT Begin cone Single Garage

9° RT End cone " "

16.2 RT Begin cone Single Garage Slab

" " End " " "

5.0  
11.2  
5.2  
4.81

7.5 RT Begin Cone Slab Garage Floor

8.5 RT End " " "

4.2  
11.2  
5.3  
4.81

4.1  
11.2  
4.2  
4.81

4.1  
11.2  
4.4  
4.81

Top Sewer MH 3.5 RT

5.41  
11.2  
5.42  
4.81

Cutter line South side Monroe

Cutter line North side

392.99

9+00 3.3 389.7

+50 3.8 389.2

10+00 4.2 388.8

+50 3.7 389.3  
389.4

11+00 6.27 395.65 3.61 389.38

+50 5.9 389.8

12+00 5.5 390.2

+50 5.1 390.6

13+00 5.0 390.7

+50 5.5 390.2

14+00 8.91 386.7

+43 8.7 387.0

3.66 392.94 6.37 389.28

6.24 386.70 = 386.68

Alley BIK 197 N of University  
E of Swift

7+19<sup>52</sup>

North prop line Polk

West  
Williams  
Varonakis  
Kemp

12

Polk

6+95 Gas Xing

6" AC PAVE

6+99 Sewer Xing

Water Meters

1+16 15' LT  
1+85 15' LT  
2+79 11' LT  
3+28 13' LT  
3+67 13' LT  
4+13 13' LT  
4+66 13' LT  
5+09 12' LT  
5+47 12' LT  
5+88 12' LT  
6+06 12' LT  
6+88 12' LT  
6+41 10' LT

Water Meters

1+12 4' RT  
1+30 4' RT  
2+23 4' RT  
2+91 4' RT  
2+34 4' RT  
3+75 3' RT  
4+28 3' RT  
4+20 4' RT  
5+04 4' RT  
5+36 3' RT  
6+02 4' RT  
6+23 4' RT  
6+55 4' RT

Telc Poles

0+87 Deadman 4' RT  
1+08 PP # D1201 3' RT  
1+30 PP No 4  
1+49 PP # 409931 4' RT  
3+30 PP # 406932 4' RT  
4+30 PP # 406933 4' RT  
5+30 PP # 406934 4' RT  
6+30 PP # 406935 3.5 RT  
4+80 PP # 469137 3.5 RT

Gas Xings

3+03  
2+38  
2+75  
3+25  
3+70  
4+15  
4+05  
5+11  
5+46  
5+31  
6+41

5" AC over 9" Cond

University Ave

0+27 Gas Xing

0+87 30  
0+32 30

0+00

South prop line University

Q Profile Alley Dik  
197

6.58	365.40	358.82
0+00	5.28	360.1
+12	5.41	359.8
+50	4.78	360.6
+67	5.36	360.0
1+00	3.9	361.5
250	2.0	363.4
2+00	1.0	364.4
7.59	372.04	0.95 364.45
+50	7.0	365.0
3+00	6.3	365.7
+50	5.7	366.3
4+00	5.2	366.8
+50	4.4	367.6
5+00	3.6	368.4
+50	3.2	368.8
6+00	2.7	369.3
+50	2.0	370.0
+86	2.70	369.3

11-5-53

Rain

13

BM BP NW Cor. Swift University

South Line University

South Cutter Line

N

North Cutter

Cutter South Side



372.04

6+99.5

2.21 + 2.3 To Flowton

Top E rim Sewer MH 5011

7+00

2.30 369.7

7+12.6

2.45 369.6

Bottom cb

7+12.8

1.82 370.2

Top cb

7+19.52

1.3 370.7

0.95 365.40

7.59 364.45

6.57 358.83 = 358.83

Mission St Madison  
to Texas St

11-6-53

15

69.37  
340.65  
409.02

Gas + water  
in same location

5+20.32 3 End AD pave

15° 59' 30 RT

84° 48' 30 RT 1+08 to Texas St

4+27.07 on 2" main to Texas St

parallel to Ob.

4+10.46 EO 35° 55 RT Δ = 45° 31'

4+09.02 Long chord dist

L = 340.65

Δ = 40°

Dist Per. 4.0085667

R = 100'

L = 69.81

R = 421.80

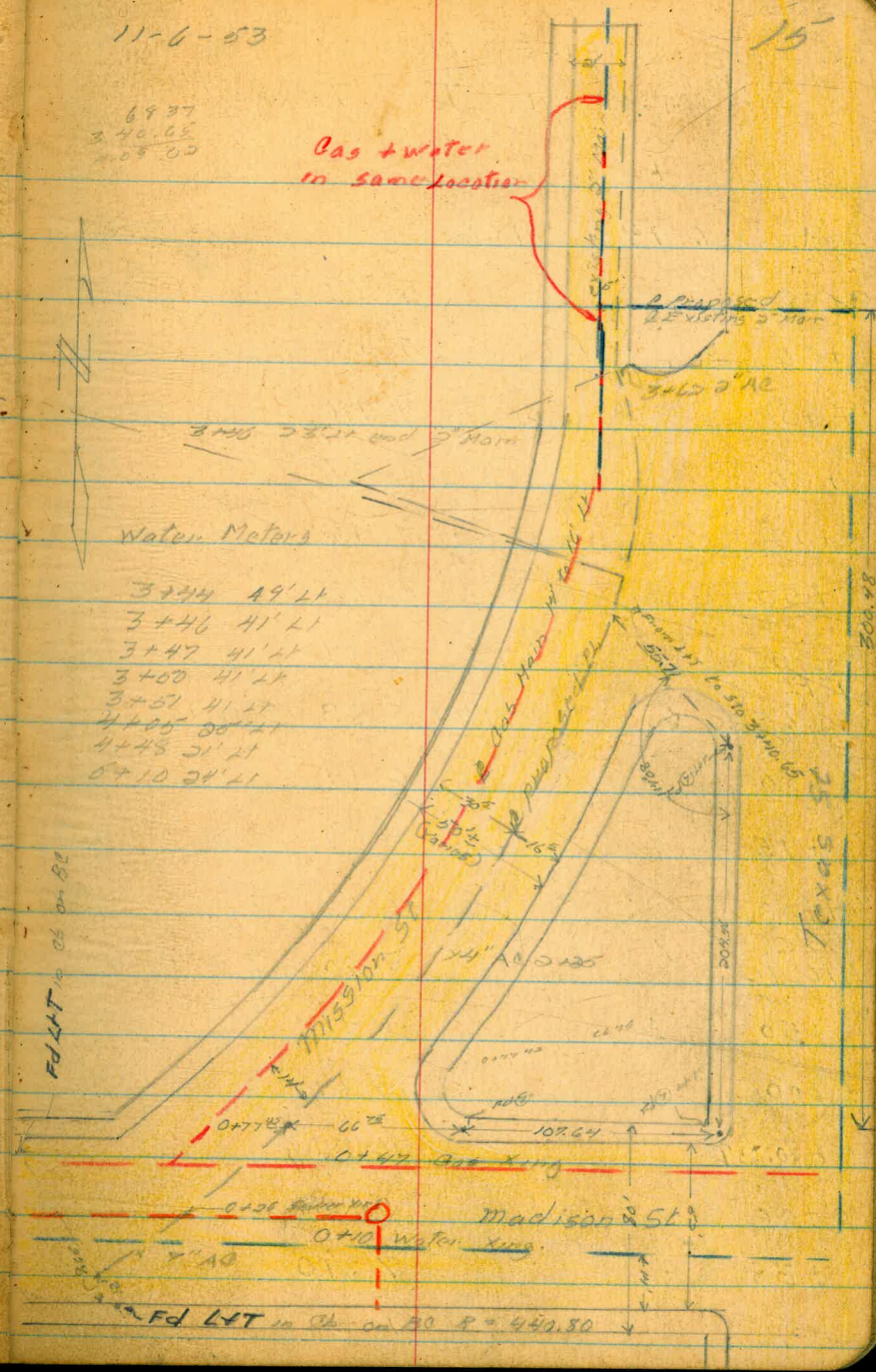
3+40.65 PCC

Δ = 45° 31'

R = 428.80

L = 341.15

0+00 80 15' off South of Madison



♀ PROFILE MISSION  
MADISON TO TEXAS

WEST  
WILLIAMS  
VARON FAKIS X  
KEMP †

11/6/53

348.90  
343.97  
4.93

16

	+	HI	-	EL.
B.M.	6.44	348.72		342.28
B.C.				343.23 AR
0+00			5.49	342.72
+26			4.80	343.92
+50			5.08	343.64
1+00			4.74	343.98
+50			4.37	344.35
2+00			4.46	344.26
+50			4.73	343.99
3+00			4.94	343.78
T.P.				
340.65 EC	6.00	349.49	5.23	343.49
3+50			6.14	343.35
+75			6.59	342.90
4+00			5.63	343.86
E.C.				
410.46			5.30	344.19
+50			5.47	344.02
5+00			5.99	343.50
5+20.39			6.21	343.28
0+00			5.25	344.24
+38			7.40	342.09
+50			10.25	339.24

MADISON + LOUISIANA S.E.B.P.

to top of line 337.82 Top Sewer MH 552 RT

END A.C. PAVE

MAIN TO TEXAS ST.  
EAST FROM STA. 4+27.07

7.4	7.7
10' LT.	10' RT.
9.4	10.1
10' LT.	10' RT.

♀ PROFILE MISSION  
MADISON TO TEXAS

WEST  
WILLIAMS  
VARONFAKIS X  
KEMP †

11/6/53

17

+ 349.49 - E1

0+68			12.5	336.99 A.R.	13.7	11.5
				<del>337.24</del>	10 LT	10 RT
1+80			12.20	337.29	TEXAS ST	
1+08			12.36	337.13	TEXAS ST MAIN	
T.P.	4.93	348.97	5.45	344.04		
CK. TO						
B.M.			6.62	342.35 = 342.28		

Alley BIK 2 N of Polk  
E of Menlo

West  
Williams  
Varonakis  
Kemp

(Susan) 18  
11-12-53

6+97.45

North prop Line Orange

71  
23  
71

6+71.2 Gas Xing

Orange

5" Teejet 5" DI

6+43 CV or D

6" AC pave

6" Full Lat (6" DI)

Water Meters

0+75 15" DI  
1+30 15" DI  
1+78 15" DI  
2+50 15" DI  
2+85 15" DI  
3+50 15" DI  
3+75 15" DI  
4+44 15" DI  
4+98 15" DI  
5+39 15" DI  
5+48 15" DI

Water Meters

0+60 3" RI  
0+70 3" RI  
0+73 3" RI  
1+16 3" RI  
1+61 4" RI  
1+91 3" RI  
2+44 4" RI  
2+87 4" RI  
3+38 1" RI  
3+38 3" RI  
4+48 3" RI  
4+86 3" RI

Gas Xing's

0+46  
0+90  
1+61  
1+90  
2+48  
3+11  
3+30  
3+79  
4+44  
5+15  
5+90

Full Lat on 4" DI

6" AC pave

0+00

South prop Line Polk

0+30 MH 5" DI

Storm Drain Xing 0+13

Polk

0+00 CV on 4"

Alley BIK 2  
Profile

West  
Williams  
Varonfakis  
Kemp

Warm  
11-16-53

19

6.30 349.39 343.09

BM NW 130 University + Menlo

0.07 349.39 0.57 348.80

Turn Top FH NE cor. Menlo + Polk

0+00 6.12

+07 6.52

+20 6.09 + 5.3 To Flow

Top east side Sewer MH

+40 6.02

North edge AD pave

6.37 349.68 6.08 343.31

+50 6.0

1+00 5.3

+50 5.0

2+00 4.6

+50 4.2

3+00 3.1

+50 2.1

4+00 1.0

+27 6.23 355.58 0.33 349.35

+6.5 To Flow Top E edge Sewer MH

+50 5.9

5+00 5.3

+50 4.5

355.58

6700 4.3

+17<sup>5</sup> 4.47

+32<sup>5</sup> 4.58

+50 4.04

+97<sup>1/2</sup> 3.82

edge AC pave

Outer south side

edge cone pave North <sup>2 in.</sup> prep

242 349.08 892 346.66

0.66 349.48 0.26 348.82

6.38 343.10 = 342.09 TBM

Sand Rock Grade  
(Texas St)

7+69<sup>34</sup> 50

$\Delta = 13^{\circ} 01' 46''$  LT  
Transit line R = 980

1753952

6+55 end bridge

6+25 Begin Bridge

Water Meters

0+55 27' LT

5+15 27' LT

7+47 31' LT

Gas Xing

6+02

6+23 end Bridge

6+12 Begin Bridge

6" WD 3" Pipe Line Xing

4+91 end Gas Well

4+77 Begin Gas

4" WD 2" Pipe

8" Main 30' LT

BM-

Gene Helwell Sta 6+00

See FB 2245 P 10

2+11 26.40' Lt. Full Sand Meter

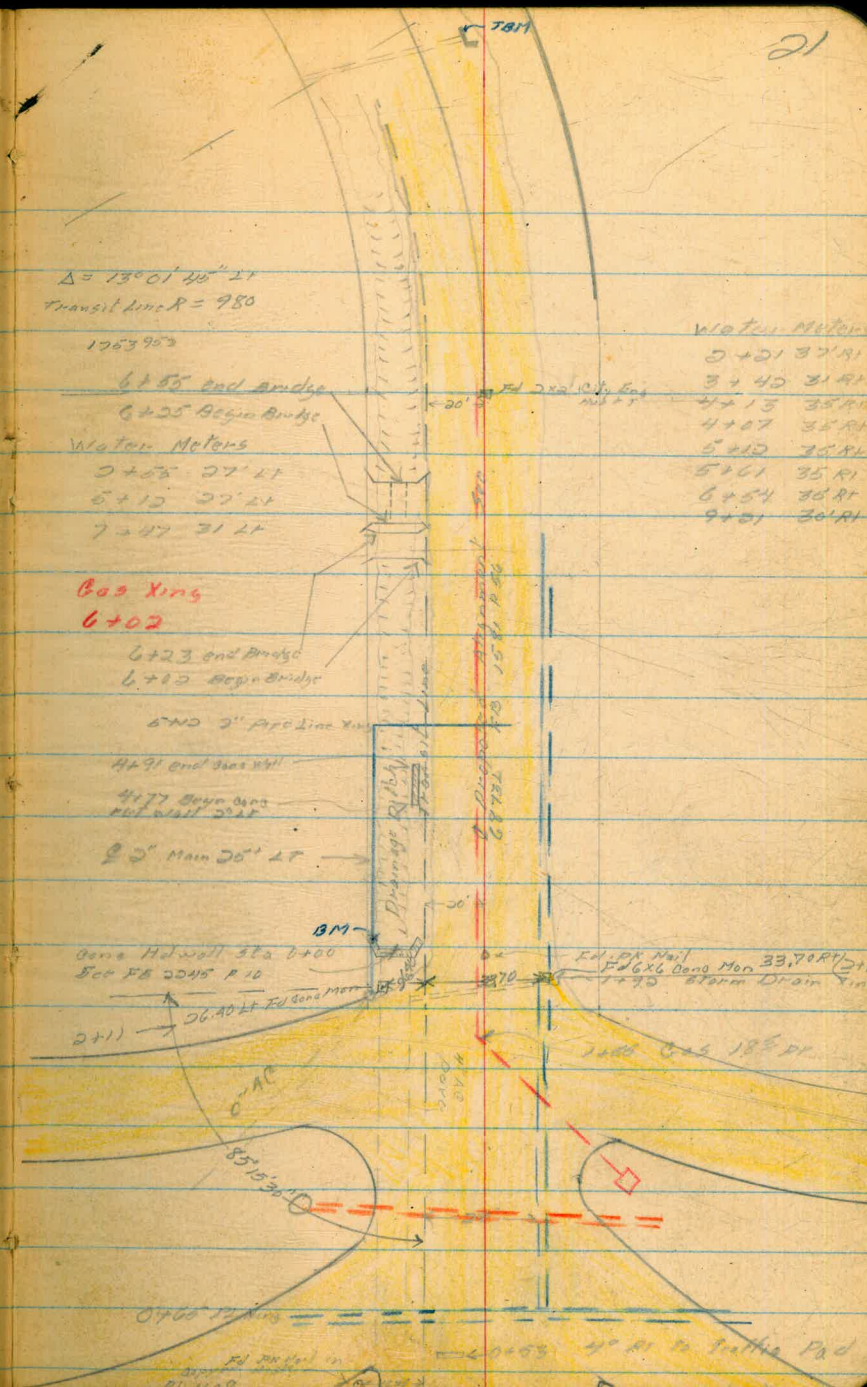
Ed. PK No. 1  
FD 626 Gene Mon 33.70' RT (2+11)  
1+75 Storm Drain Xing

1+40 Gas 18" DI

2+30<sup>26</sup> = 0+00 Drain Line Survey See FB 2245 P 10

0+00<sup>40</sup>

16.35' Lt. to 14' over 1108



7811

21



Profile Transit Line  
Sand Rock Grade (Texas)

12-1-53

West 22  
Williams  
Vorenfakis  
Kemp

2+

RT

0.13 56.97 56.84

0+00 12.64 44.3

0+50 9.84 47.1

1+00 7.05 49.9

1+00 7.66 ± 20' to Flow

+50 4.20 52.8

2+00 1.23 55.7

11.95 68.79 0.13 56.84

+50 9.70 59.1

3+00 5.0 63.8

12.10 80.40 0.49 68.30

+50 12.15 68.3

BM on cone Headwall

10.85	11.90	12.05
20	20	20
844	9.16	9.89
20	30	50

2+30 17.11

12.69	11.87
30 RT	31 Top Beam
9.20	11.37
9.10	4.8

8.62  
31 RT

6.97  
10 RT

7.57  
34 RT

6.83  
35 RT

9.3 RT Top West edge sewer Mt

5.3  
20 RT

4.00  
10 RT

4.45  
30 RT

1.70  
16 RT

1.85  
15 RT

1.14  
10 RT

1.44  
30 RT

0.77  
36

11.8  
5 RT

9.20  
10 RT

9.00  
31 RT edge oil

6.7  
5

5.00  
4 RT edge oil

4.45  
10 RT

4.7  
30 RT

14.6  
3 RT

12.27  
5 RT

12.00  
10 RT

11.91  
30 RT

edge oil

12-5-53

80.410

11+00

7.05

73.4<sup>✓</sup>

$$\frac{11.8}{9.1} \quad \frac{8.0}{6.2}$$

$$\frac{7.74}{5.1} \quad \frac{7.30}{7.0} \quad \frac{7.14}{3.0}$$

edge oil

+50

2.55

77.9

$$\frac{8.0}{8.1} \quad \frac{2.7}{4.1}$$

$$\frac{3.02}{5.1} \quad \frac{2.60}{10.1} \quad \frac{2.63}{2.9}$$

edge oil

11 62

90.36<sup>✓</sup>

1.66

78.74<sup>✓</sup>

Turn on rock rubble wall

5+00

10.02

80.3<sup>✓</sup>

$$\frac{13.3}{4.1}$$

$$\frac{8.2}{2.1} \quad \frac{8.30}{5.1} \quad \frac{7.87}{7.1} \quad \frac{7.79}{2.9}$$

edge oil

+50

2.8

87.6<sup>✓</sup>

$$\frac{4.8}{5.1}$$

$$\frac{3.25}{3.1} \quad \frac{3.21}{1.1} \quad \frac{3.71}{2.1}$$

edge oil

12 36

10 3.00

0.22

90.14<sup>✓</sup>

6+00

11.2

91.8<sup>✓</sup>

$$\frac{13.3}{7.1} \quad \frac{10.8}{4.1}$$

$$\frac{11.67}{3.1} \quad \frac{11.27}{7.1} \quad \frac{11.54}{2.1}$$

edge oil

+50

6.93

96.1<sup>✓</sup>

$$\frac{6.60}{13.1}$$

on Bridge

$$\frac{6.99}{1.1} \quad \frac{6.63}{1.1} \quad \frac{7.37}{2.1}$$

edge oil

7+00

2.56

100.4<sup>✓</sup>

$$\frac{3.96}{9.1} \quad \frac{1.49}{6.1}$$

$$\frac{2.25}{7.1} \quad \frac{3.04}{2.1}$$

edge oil

12 36

11 5.26

0.10

102.90<sup>✓</sup>

+50

10.32

104.8<sup>✓</sup>

$$\frac{13.00}{1.1} \quad \frac{10.15}{1.1} \quad \frac{10.46}{2.1}$$

$$\frac{9.91}{10.1} \quad \frac{10.14}{19.1}$$

edge oil

115.26

7+69 34 80 9.56 106.7

9.86 8.09 8.65 8.37 8.57  
12RT 8RT 8RT 10RT 17RT  
← edge oil →

8+00 5.83 109.4

10.25 5.46 6.06 6.50 5.53  
13RT 8RT 4RT 10RT 15RT  
← edge oil →

7.50 1.50 113.7

5.08 0.34 1.70 1.45 1.35  
7 12RT 7RT 10RT 16RT  
← edge oil →

13.10 128.31 0.05 115.21

9+00 10.34 118.0

1.30 9.38 10.69 10.20 10.38  
22RT 20LT 7RT 10RT 16RT  
← edge oil →

4.50 6.18 122.1

8.82 5.79 6.57 6.13 6.32  
26RT 23RT 8RT 10RT 15RT  
← edge oil →

1.22 128.53 1.00 127.31

□ in cone in south end  
Turn on Cone Hdwall on west side of road

0.21 116.04 1.20 115.83

0.10 103.63 1.25 103.53

9.57 94.06 =

94.10 Nail in Power Pole 275310

48.9

Flow Line  
2.5 Storm drain  
1+99

56.84  
10  
56.89  
0.50  
59.39  
59.85  
61.84  
3.05  
48.9

Amberst St 67<sup>th</sup> to 68<sup>th</sup>

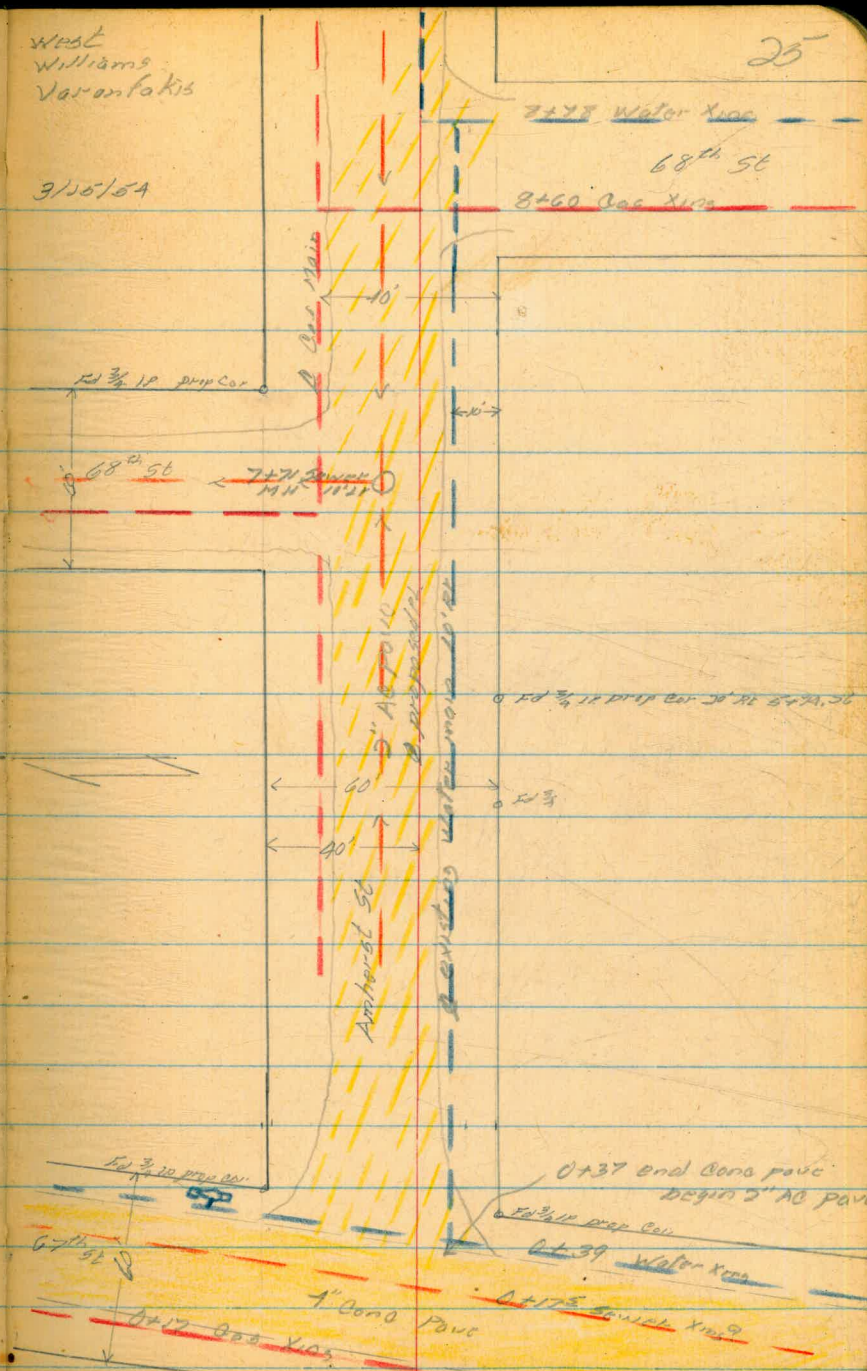
West  
Williams  
Varonakis

25

3/15/64

7+60<sup>el</sup> Amberst = 2+11.05 67<sup>th</sup> Tee

5+77.26 POT



0+60 POT east line of 67<sup>th</sup>

7+77 Water Line

68<sup>th</sup> St

8+60 Gas Line

2+11.05 67<sup>th</sup> Tee

68<sup>th</sup> St

7+77 Sewer Manhole

Amberst St

2+11.05 67<sup>th</sup> Tee

0+37 end Cond pipe  
begin 1" AC Pave

0+39 Water Line

0+17 Cond Pipe

67<sup>th</sup> St

Profile Amherst St.

2.05	159.95	
1.11	155.09	8.17 150.98
0+00		7.37
+15		10.57
+20		10.67
+37		10.62
+50		10.25
1+00		8.11
+50		6.97
2+00		6.57
+50		5.95
3+00		5.46
+50		5.17
4+00		5.00
+50		4.80
5+00		4.90
+50		4.25
6+00		4.20
+50		4.14

457.40	BM SW BP	68 <sup>th</sup>	+ E1 Cajon	
	West prop line 67 <sup>th</sup>			
	10.40 TOTL		11.03 TOTL	
10.38 TOTL	West edge	asph pave	11.00 TOTL	
10.27 TOTL	East	" " "	11.15 TOTL	
	16' LT edge	Asph pave	6' RT edge	Asph pave
	14' " " "	" " "	8' RT " " "	" " "
	14' " " "	" " "	8' RT " " "	" " "
	14' " " "	" " "	8 <sup>2</sup> ' RT edge	Asph pave
			8	
	14' LT edge	Asph pave	8' RT edge	Asph pave
	13' LT edge	Asph pave	7' RT edge	Asph pave
	15' LT edge	Asph pave	7' RT edge	Asph pave

455.09

7+00	4.04	
+50	4.16	
+71	4.10	+9.1 To Flow
+60 <sup>06</sup> Tee	4.22	

15'20 edge AC pave	6 RT edge AC pave
Top South edge sewer 11' 10' 21	

9+00	4.99	
+50	4.40	
9+00	4.06	

18'21 edge AC pave	4 RT edge AC pave
17'21 edge AC pave	5 RT edge AC pave

8.51 459.49 7.11 450.98

210 457.39 = 457.40

68th St Alley South  
of El Cajon to Amherst St

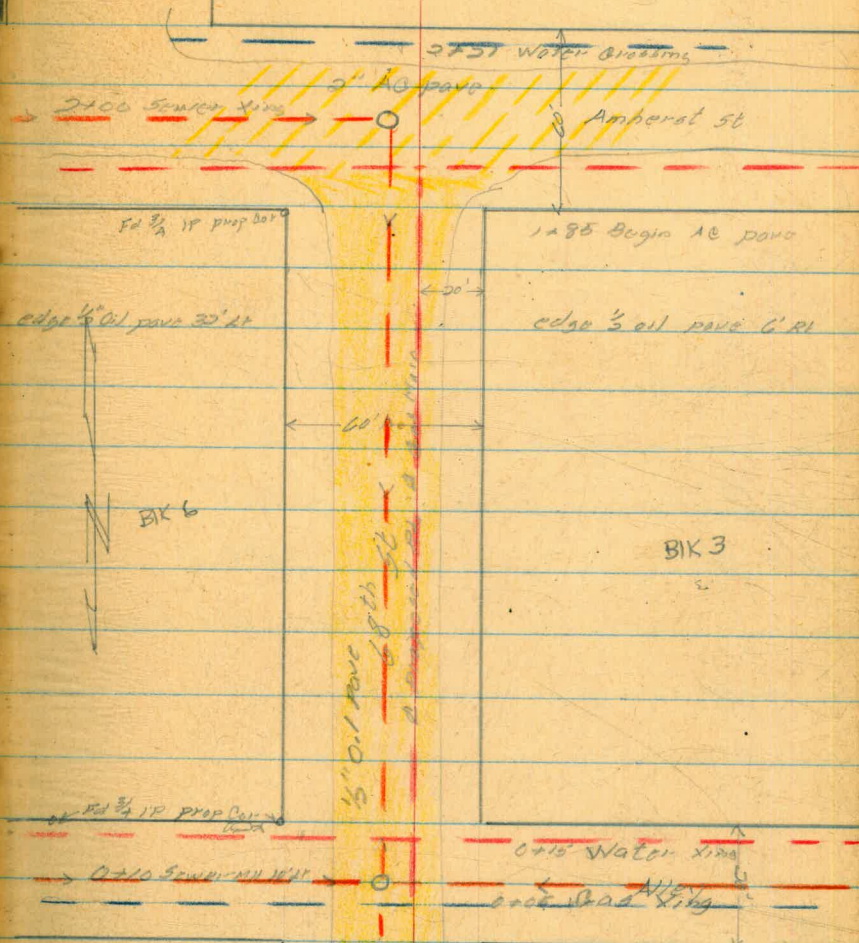
2+31.05

South prop line Amherst

2+11.05 68th = 7+60.06 Amherst (Top)

0+00

North Line Alley



68<sup>th</sup> St  
Alley South of El Cajon  
to Amhurst

West  
Williams  
Varonfakis

29

3/15/54

210	459.50	457.90
0+00	5.12	454.4
		+13.5
0+10	4.88	454.6
+50	5.96	453.54
1+00	6.90	452.6
+50	7.94	451.6
2+00	8.96	451.0
+11 <sup>05</sup> Tot	8.60	451.0
2+31 <sup>05</sup>	8.64	450.9
210	457.40	-

BMWOP 68<sup>th</sup> + El Cajon

To Flow line

Top West edge sewer MH 10'11"

South prop line Amhurst St

457.40



68th St Amberst  
to Tower

5+88.60 x

2° 02' 30" RT

16  
15  
23  
1

0+40 = 8+65<sup>03</sup> Amberst St

0+00

North prop line Amberst

8+65 Sewer DE 5' LL  
West  
Williams  
Vorontakis

30

3/19/54

7+50 Sewer MII 5' LL

Ed 1" iron pipe

6+44 Sewer Deadend  
5' LL

Ed 3/4" pipe

0+60 Sewer

0+48 Water Xing

6+20 RT

7+61 Water Xing  
Kasefield Dr

Ed 1 1/2" 10' 15' RT 5+22.60

12" C.I. 10' 10' RT  
10' 10' RT  
10' 10' RT

15" Bell Drain pipe  
2+73

Amberst St

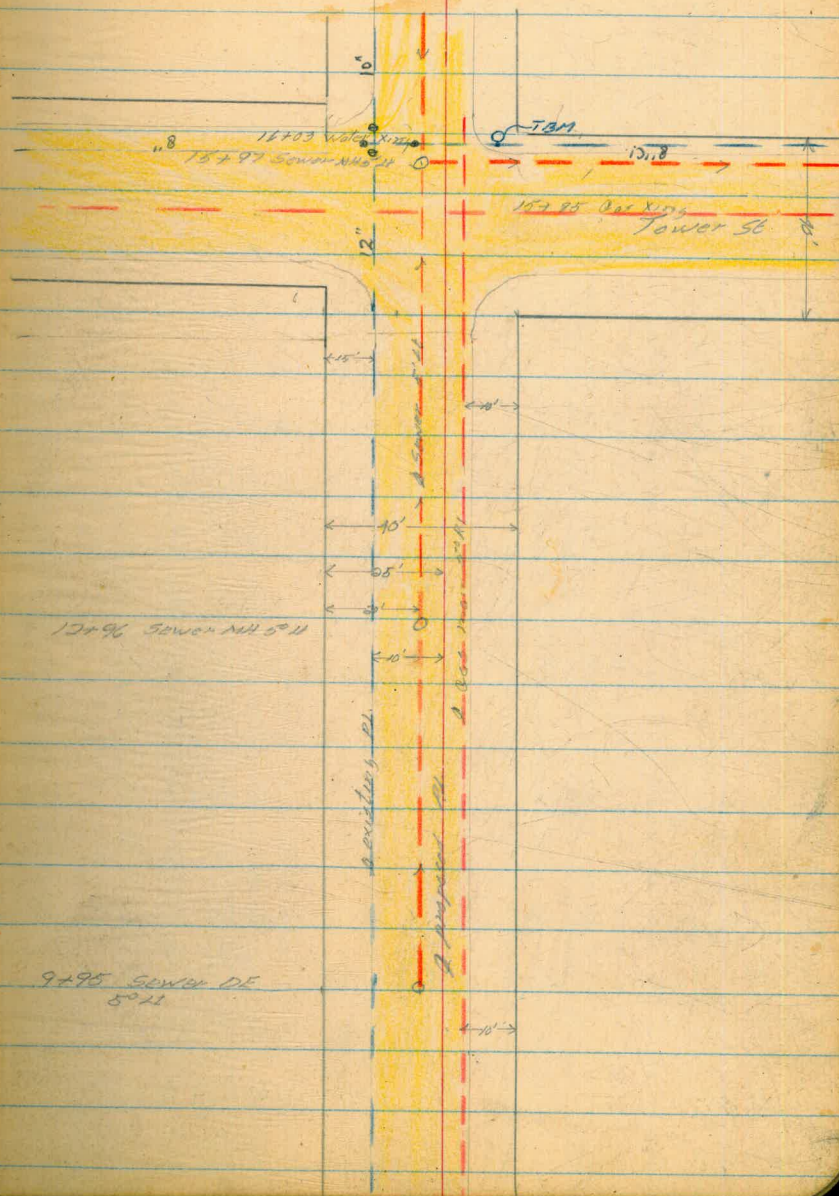
0+29 Sewer Xing

0+20 3/4" Xing

16+06 <sup>05</sup> South prop line Tower

15+81 <sup>05</sup> Tel

16+06 05



Q Profile 68th SE  
Amherst to Tower

1.26	458.46 ✓	457.10
136	452.41 ✓	451.05 ✓
0+00	0.9	451.5 ✓
+21	1.93	451.0 ✓
148 Tee	1.27	451.1 ✓
+50	1.40	451.0 ✓
1+00	3.17	449.3 ✓
+50	4.88	447.5 ✓
2+00	6.56	445.9 ✓
+50	7.15	445.8 <sup>3</sup> ✓ crw ✓
+739	7.35	445.1 ✓
3+00	6.90	445.5 ✓
+50	5.29	446.7 ✓
4+00	3.36	449.0 ✓
+50	2.16	451.3 ✓
5+00	0.27	452.14 ✓ 252.14 ✓
T.P. 11.01	463.15 ✓	
+50	9.91	453.24 ✓
5+88.60 ✓	8.47	454.68 ✓
1+00	8.15	455.0 ✓

West  
Williams  
Varonakis

3/19/54

BM SWBP 68th + E2 Dejon

North prop line Amherst

Begin oil pave

14.2t edge oil	6' RT edge oil
16.2t edge oil	4.8t edge oil
- 8.3 Top 10" Drain 9.9 2t	- 9.7 Top 10" Drain 17' RT
16 <sup>2</sup> 2t edge oil	5' RT edge oil
13' 2t edge oil	5' RT edge oil
14' 2t edge oil	6' RT edge oil
14 2t edge oil	8' RT edge oil

46315<sup>W</sup>

6+50	7.36	455.8	✓		
7+00	6.78	456.4	✓	11' LT edge oil	11' RT edge oil
1+50	5.96	457.1	✓		
1+50	5.83	457.32	✓	Top West edge sewer MH	
8+00	5.38	457.8	✓	11' LT edge oil	7' RT edge oil
1+50	4.98	458.7	✓		
9+00	3.16	460.0	✓	12' LT edge oil	8' RT edge oil
1+50	2.59	460.6	✓		
10+00	2.70	460.9	✓	12' LT edge oil	6' RT edge oil
1+50	3.73	459.4	✓		
11+00	4.98	458.3 <sup>2</sup>	✓	13' LT edge oil	6' RT edge oil
1+50	0.75	457.56 <sup>W</sup>	✓		
12+00	2.01	455.5	✓	12' LT edge oil	6' RT edge oil
1+50	3.06	454.5	✓		
1+96	3.05	454.5 <sup>CFW</sup>	✓	Top West edge sewer MH 5' LT	
13+00	3.71	453.8	✓	12' LT edge oil	5' RT edge oil
1+50	3.98	453.6	✓		
14+00	4.58	453.0	✓	12' LT edge oil	6' RT edge oil
1+50	5.33	452.2	✓		

+72 to Flow

CFW

+6.5 to Flow

CFW 453.94

Profile 68<sup>th</sup> 34

Cont

06

457.56 ✓

15+00 5.96 451.6 ✓

+50 6.99 450.6 ✓

+81<sup>05</sup> Tee 7.38 450.2 ✓  
+13° to Flow

+97 7.76 449.8 ✓

11+00 7.23 449.8 ✓

+06<sup>05</sup> 7.92 449.6 ✓

6.01 457.78<sup>v</sup> 6.39 451.17 ✓

6.20 463.02<sup>w</sup> 0.96 456.82 ✓

2.22 464.13<sup>v</sup> 11.72 451.30 ✓

6.94 460.83<sup>v</sup> 0.21 453.89 ✓

3.37 457.46 ✓

34

3/19/54

13' at edge oil 6' RT edge oil

Top west edge sewer MH 5' at

South prop line Tower

TBM Nail in PP 12/19/52 SW corner  
6' Tower

457.40

REDUCED BY C.F.W. 15 DEC '54

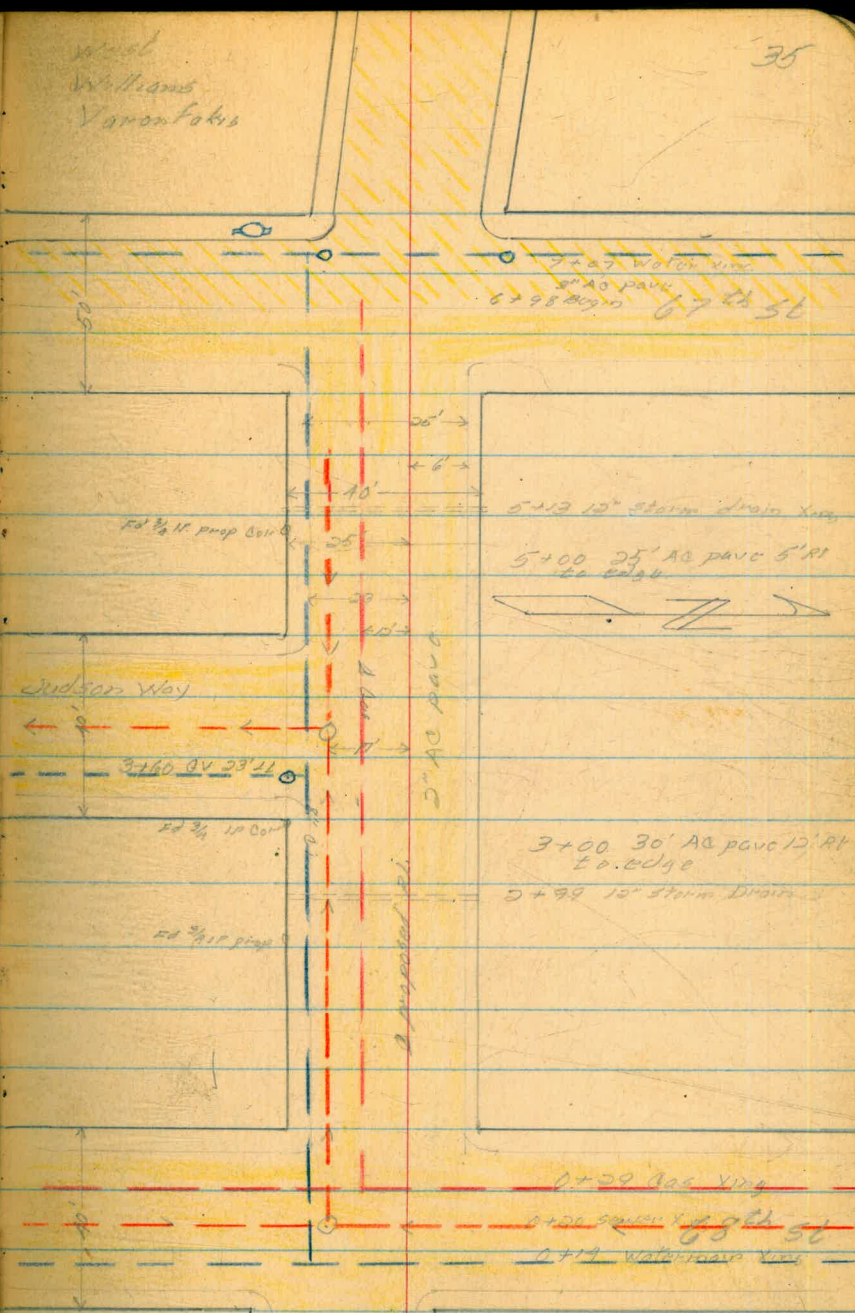
Tower 55 68<sup>th</sup> to 67<sup>th</sup>

West  
Williams  
Varonakis

35

7+24<sup>A</sup> ±

West prop line 67<sup>th</sup>



0+24 AN

0+00

East line 67<sup>th</sup>

Q Profile Tower 56  
68<sup>th</sup> to 67<sup>th</sup>

	529 456.46 <sup>W</sup>	451.17
0+00	6.93	449.6 ✓
+50	6.28	450.2 ✓
1+00	6.26	450.2 ✓
+50	6.51	450.0 ✓
2+00	7.02	449.44 ✓
+50	7.67	448.8 ✓
2+99	10.2	446.3 ✓
3+00	8.29	448.2 ✓
+50	7.57	448.9 ✓
+69	6.99	449.5 ✓
4+00	6.58	449.9 ✓
+50	5.92	450.75 C.F.W.
	7.29 458.13 <sup>W</sup>	5.62 450.84 ✓
5+00	7.04	451.1 ✓
	9.19	449.0 <del>2</del>
+13	8.51	449.6 ✓
+50	6.60	451.5 ✓
6+00	5.82	452.3 ✓
+50	4.85	453.3 ✓

West  
Williams  
Varonakis  
Kellhofer

36

3/23/54

TB19 nail in power pole  
east prop line 68<sup>th</sup>

9° RT <sup>12  
88  
102</sup> Flow line 12' Culvert

Top North run sewer 112 17'±

12' RT 12' storm drain  
27' Lt 12' storm drain  
Flow line 15' RT 12' storm drain

458.13 N

7+00

1.99 453.7 ✓

+292

1.24 453.9 ✓

1.57 457.95 N 1.75 456.38 ✓

8.22 456.47 ✓ 9.70 448.25 ✓

5.28 451.19 N

= 451.17

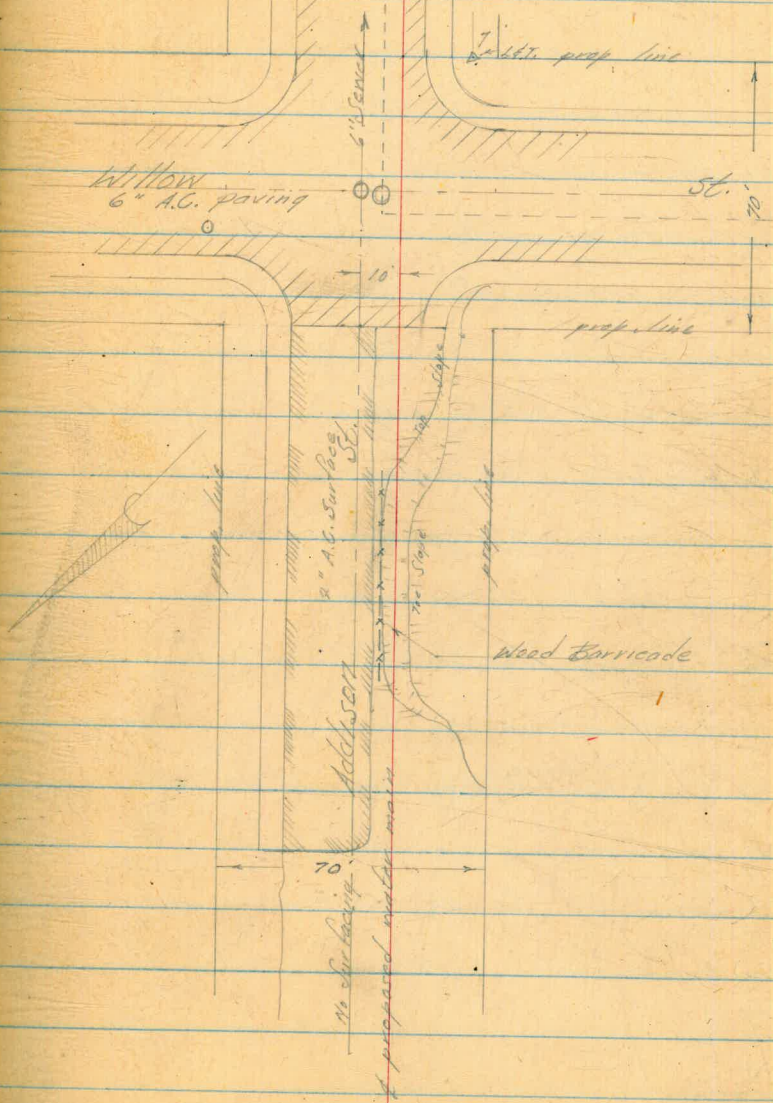
West prop line 67<sup>m</sup>Top FH SW Cor. 67<sup>m</sup> + TowerREDUCED 17 DEC '54  
C.M.W.



Profile & Pro. Water on Addison St. 44

0+00	E. prop line of Willow, 64.
+18	E. curb line
+35	Power M.H. 10' RL
+36	Water 5' RL
+40	angle point 14" Water line
+45	Gas M.H. 39' RL
+52	W. curb line
+70	Edge 6" A.C. paving

Willow St. to Flynn St.



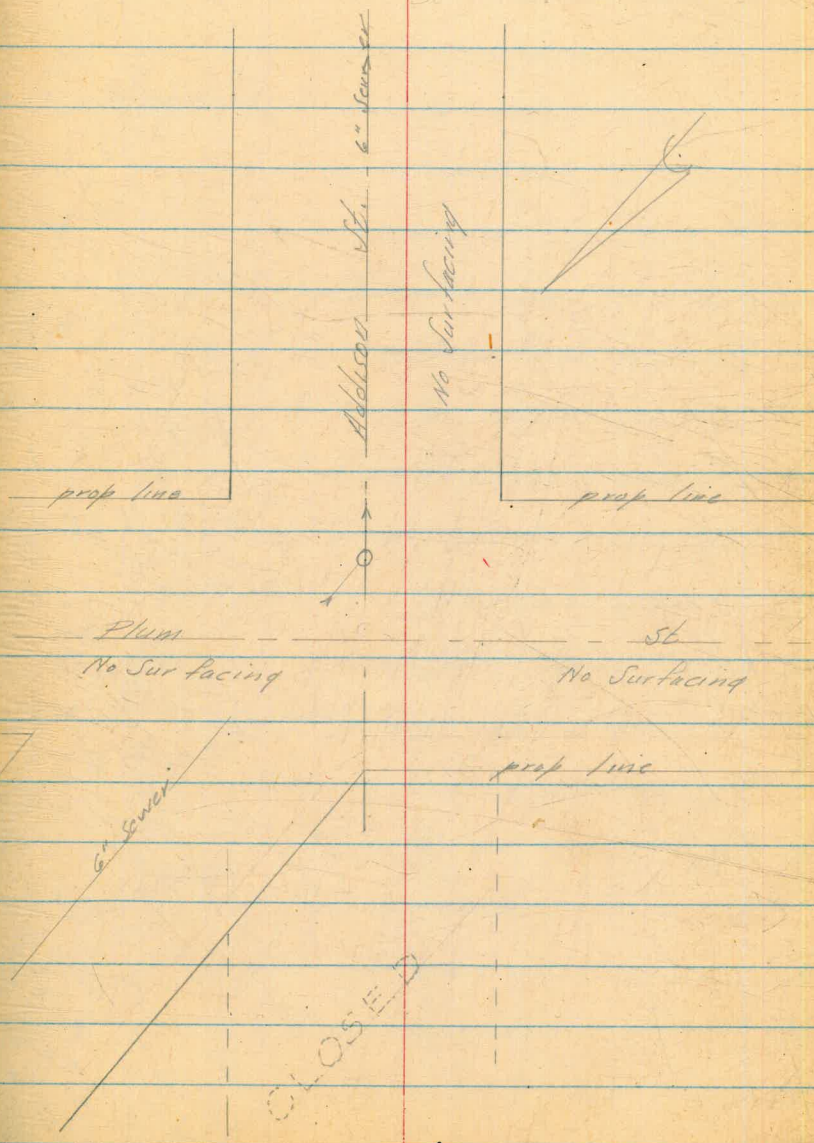
Profile of Addison Cont.

3182

Sewer M.H.

4190

W prop line Plum St.



Profile & Proposed Water on Addison St

Willow St to Plum St.

66.20

N.W. B.P. Cañon & Willow St.

11.06 72.26

0+00	2.2	70.06
+18	1.4	70.86
+35	0.42	71.84
+36	0.59	71.67
+50	0.3	71.96
+52	0.2	72.06
T.P.	0.94	71.32

E. curb line Willow

Sewer M.H. 6.0' red to th.

Water M.H. A.A.V.

W. Curb line Willow

N.W. B.P. Addison Willow

9.56 80.88

+70	8.3	72.58
+100	6.0	74.88
+50	3.4	77.48
2+00	6.7	74.18

West edge 6" A.C. paving

1.8	5.6	2.6	0.9	0.8	1.4
6.7	5	2.6	5.0	10	15
10					

+10	4.3	76.58
-----	-----	-------

Profile Addition Cont.

80.88

T.P. 0.40 80.98

14.81 92.29

2+50 16.3 75.99

22.					
16.3	16.0	14.2	RE		
70	5	0	13.4	10.6	11.0
			5	70	75

3+00 7.9 84.39

7.7	7.5	7.0
5	0	5

T.P. 0.27 92.02

12.49 109.51

+50 12.0 92.51

+82 4.50 100.01

Sewer M.H.

4+00 3.0 101.51

T.P. 0.94 113.57

8.57 112.14

+40 3.6 108.54

Work prop. line Plum. St.

T.P. 13.08 99.06

1.02 100.08

T.P. 12.78 87.30

0.30 87.60

## Profile Addison Comb.

87.60

T.P.

8.50 79.10

0.71 79.81

8.48 71.33

0.58 71.91

10.71 61.20

61.20

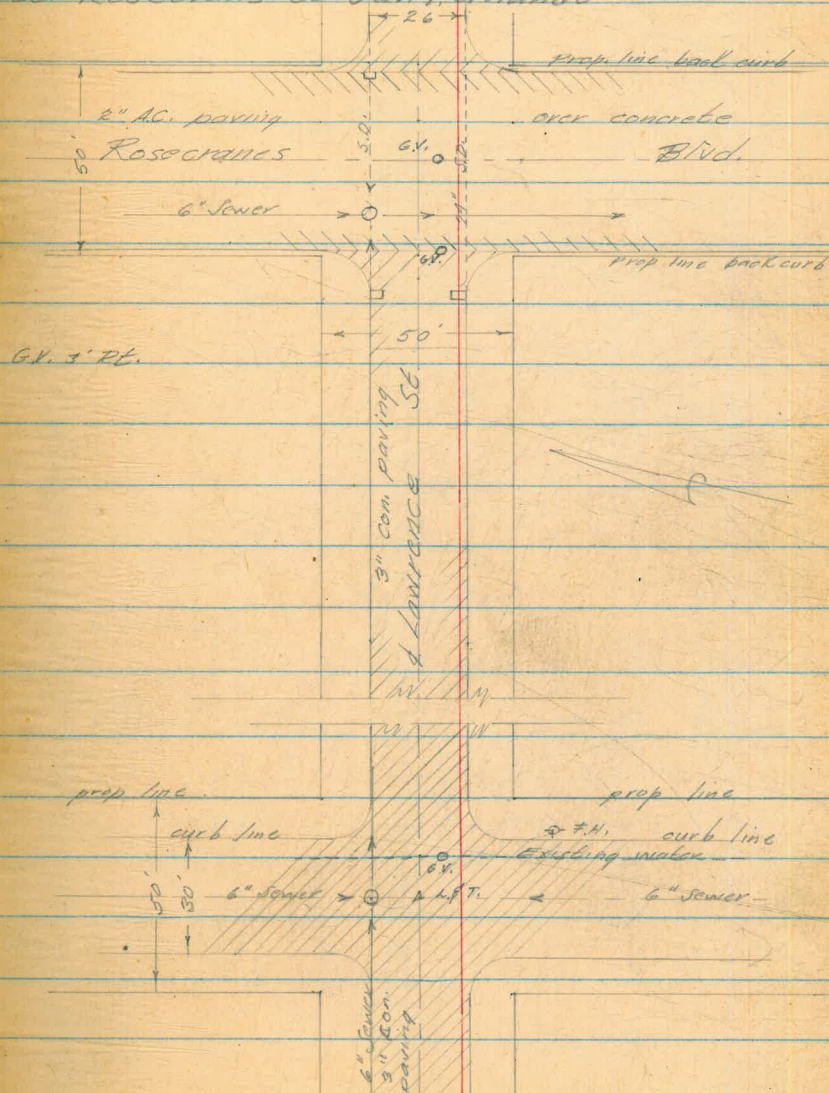
BP. Cañon &amp; Willow

5-20-54

Profile & Proposed Water on Lawrence St. Rosecrans to San Fernando

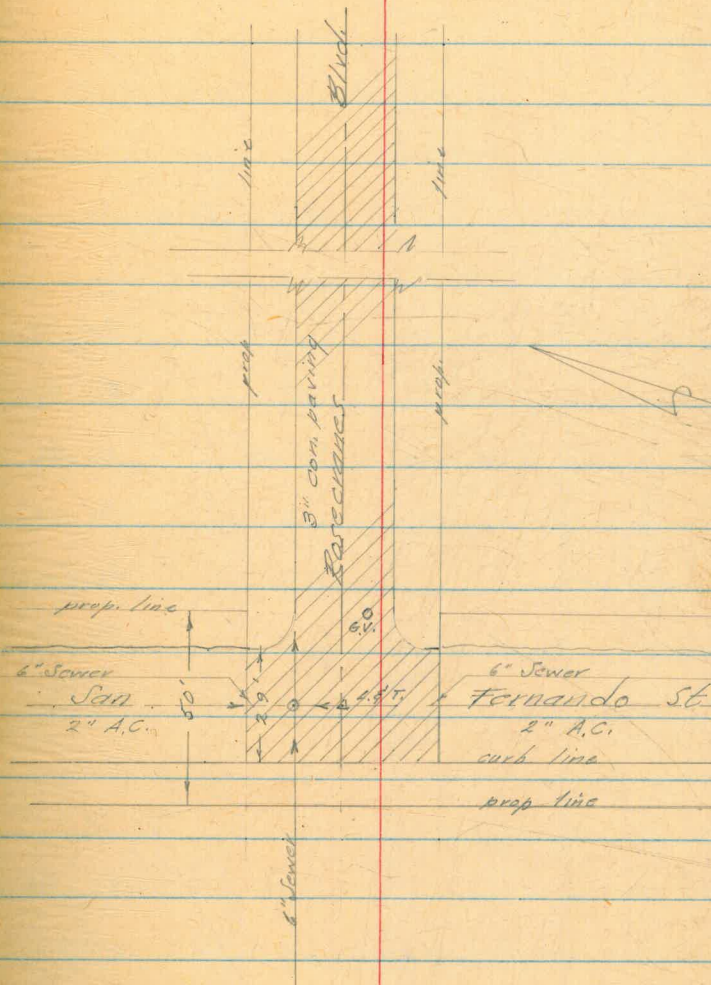
0+00 East prop. Rosecrans, back curb  
 +01 Clean out for 24x24" con. Storm Drain  
 +25 E. Rosecrans G.V. 3' RB  
 +37 Sewer M.H. 27' RB.  
 +50 West prop. Rosecrans, back curb G.V. 3' RB.  
 +60 E. edge 3x3" catch basin. Prop. line runs into storm drain 1" from No edge

3+49.81 E. prop line of San Elijo  
 +53 F.H. 15' 11"  
 +64 G.V. 6' RB  
 3+74.81 E. San Elijo  
 +89.5 West curb line



Lawrence St Cont.

- 6+99.86 E. prop. line San Fernando
- 7+00 G.V. 2.5' R.L.
- 7+24.86  $\Delta$  San Fernando
- +25 Sewer M.H. 25' R.L.
- +39 W. curb line
- 7+49.86 W. prop. line



## Profile of Water on Lawrence,

## Rosecranes to San Fernando

			33.60		NE to P. Rosecranes & Kellogg
	6.26	39.86			
			5.15	34.71	
	13.25	47.96			
0+00			13.2	34.76	13.1 E. prop Rosecranes
+25			12.1	35.86	12.2 & Rosecranes
+37			11.95	36.01	Sewer M.H. 17.75 red lat. l.
+50			11.9	36.06	11.9
+60			11.0	36.96	11.0
+100			8.3	39.66	8.0
+50			4.2	43.76	3.9
70			11.9	46.77	
	18.76	59.53			
+100			11.7	47.83	11.4
+105			11.0	48.53	10.9 E. edge con. drive way
+115			10.4	49.13	10.3 W " " " "
+50			7.5	52.03	7.3 E. edge con. " "



## Profile Lawrence St.

Cont.

59.53

2+60	6.7	52.83	6.4	W. edge cen. drive way
3+00	3.5	56.03	3.2	
T.P.	0.49	59.04		

12.19 71.23

3+50	11.2	60.03	10.9	
+59	11.0	60.23	10.6	E. curb line San Elijo
+74	10.33	60.96		Sewer M.H. 15.83 rad latth.
+89	10.3	60.03	10.0	W. curb line San Elijo
4+00	10.0	61.23	9.6	
+50	5.6	65.63	5.3	
T.P.	2.38	68.85		

13.00 81.85

5+00	11.9	69.95	11.6	
+50	7.5	74.35	7.2	
6+00	3.1	78.75	2.8	
T.P.	0.45	81.90		

14.60 93.00

## Profile of Lawrence St

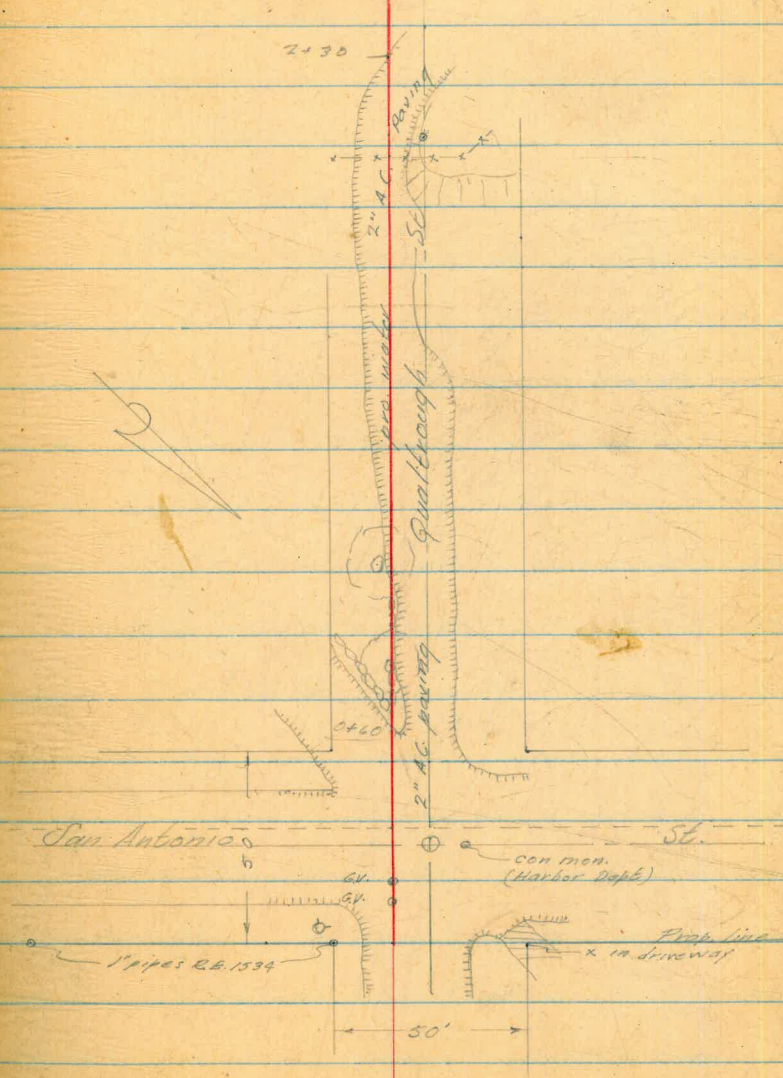
Cont.

	93.00				
6150		9.8	83.20	9.4	
7100		5.4	87.6	5.1	
+25		4.1	88.9	4.1	∩ San Fernando
+25		4.45	88.55		Sewer M.H. 8.95 road to the
7439		4.0	89.0	3.7	W. curb line
+50		2.8	90.2	2.7	W. prop. San Fernando
T.P.		4.04	88.96		∩ L.E.T. Lawrence & San Fern
	0.86		89.82		
T.P.		8.90	80.92		
	1.23		82.15		
		11.62	70.53		
	0.35		70.88		
		10.27	60.61		
	3.45		64.06		
		4.42	59.64		
			59.65		B.P. cor Kellogg & San Eligo

Werb  
Kemp  
Holahan 5-21-54 4B

Profile of Qualtrough, Reservoir to San Antonio

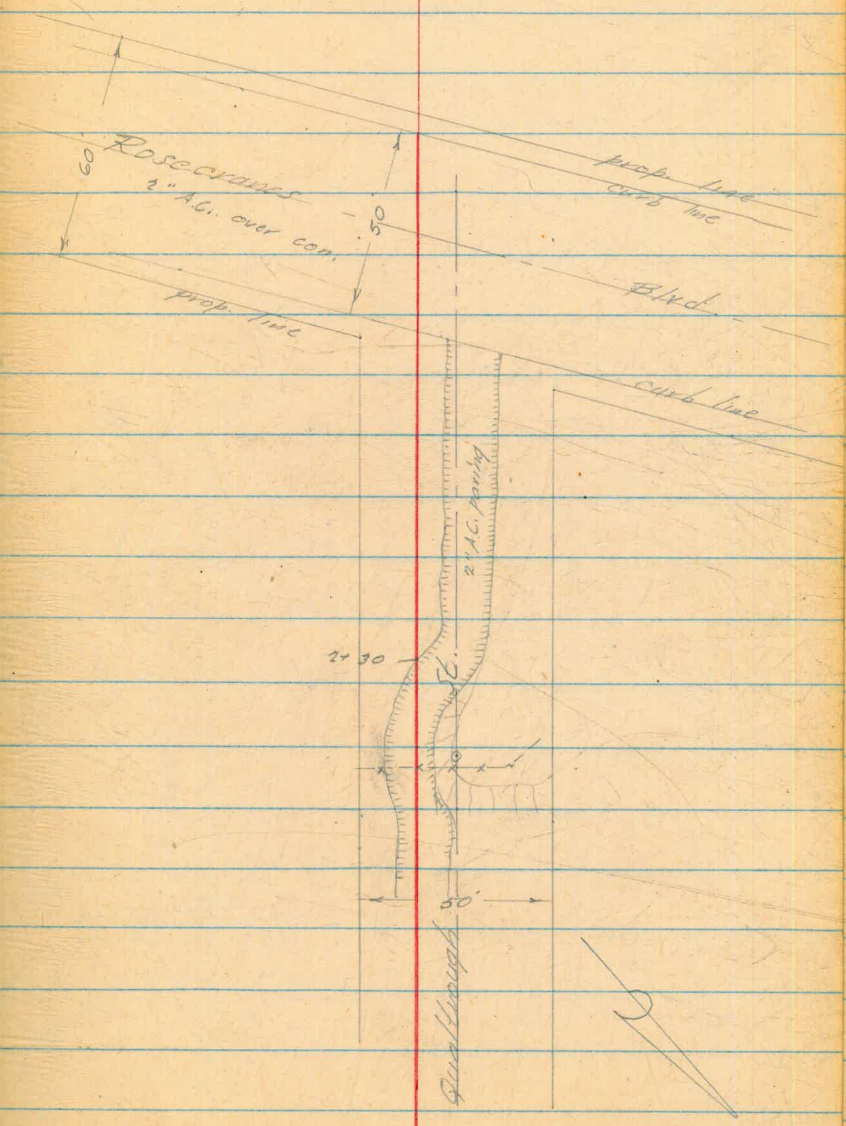
- 2+30 2" AC paving crosses & water
- 2+08 Need barricade
- 1+00 12" tree 7' lb.
- +70 10" tree on line
- +60 rock lower bed on line
- +40 W. curb line
- +29 2' 2" trench, 3' con. covering
- +25 Sewer M.H.
- +16 G.V. Existing line on San Antonio
- +10 E. curb line & G.V.
- 0+08 F.H. 30' lb.
- 0+00 East prop. line of San Antonio



# Profile of Gualtrough Cant

- 3+63 W. prop. line
- 3+53 W. curb face
- 3+03 E. curb face

- 2+30 A.C. paving crosses water line
- 2+11 P.O.T. of Gualtrough



Profile & Proposed Water Main

		11.17	
	2.86	14.03	
T.P.		11.00	3.03
	3.51	6.54	
T.P.		5.72	0.82
	13.34	14.16	
0+00		13.7	.46
+10		14.3	-1.4
+23		13.3	-2.6
+25		13.26	.90
+29		13.3	.86
+40		12.9	1.26
+50		12.0	2.16
+60		11.2	2.96
+100		0.9	13.26
T.P.		0.50	13.66
	13.18	26.84	

Quantrough, Rosecrans to San Antonio

S.W. & P. San Antonio & Owens St.

Harbor Dept Brass Men 3' No 4 of San Antonio

- E. prop line San Antonio
- E. curb line " "
- San Antonio
- Sewer M.H.
- 3" con. filled 24" ditch assumed H.P. Navy fuel line
- W. curb line

## Profile of Quantrough

Cont.

	26.84		
1+42		5.4	21.44
+50		4.3	22.54
T.P.		0.11	26.73
	12.93		39.66
1+75		2.9	29.76
2+00		1.9	37.76
T.P.		0.23	39.43
	13.14		52.57
2+17		10.3	42.27
+50		4.2	48.37
T.P.		0.29	52.28
	13.27		65.55
2+75		10.4	55.15
3+00		4.1	61.45
+03		4.1	61.45
+30		3.2	62.35

E. curb Rosecranes Blvd.

High point in crown, Rosecranes

## Profile of Quantrough

65.55

T.P.

2.36

63.19

5.44 68.63

T.P.

4.64

63.99

0.62 64.61

T.P.

12.28

52.33

2.30 54.63

T.P.

6.64

47.99

Cont.

S.W. T.S. tag 2201. Top of curb

S.E. B.P. Rosecranes &amp; Owens El 48.07

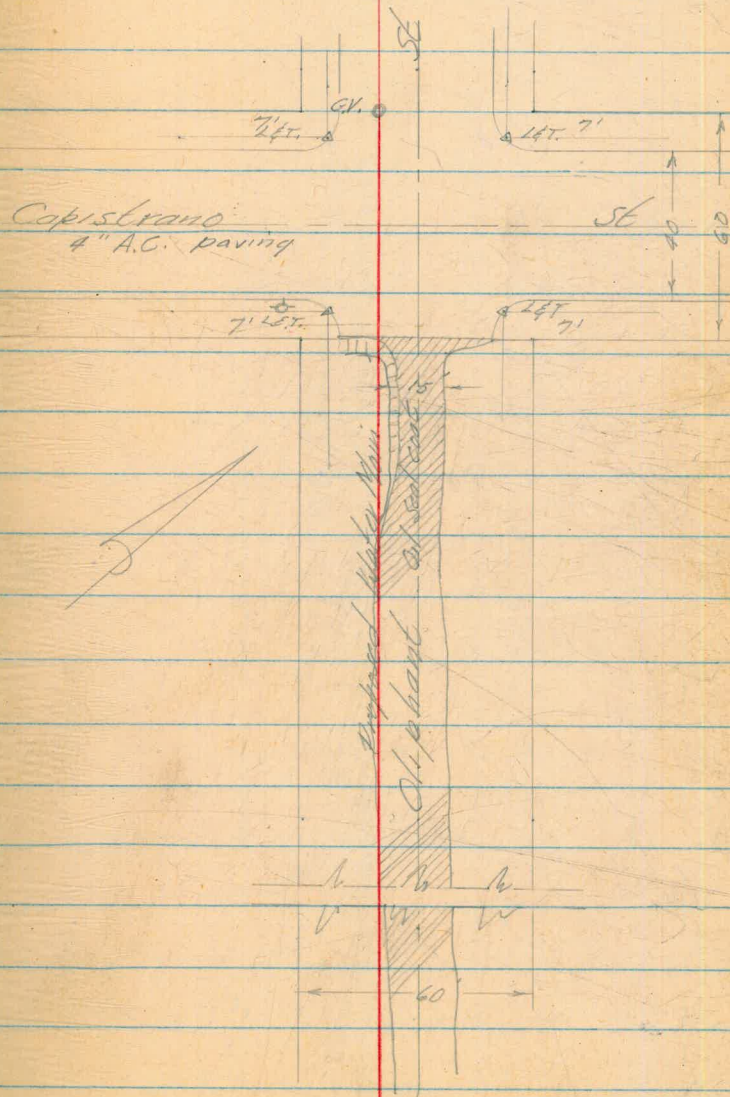
Went  
Camp  
Holahan

5-24-54

## Profile of Water Elephant St.

0+00	W. prop line of Capistrano
+10	W. curb line
+50	F. " "
+60	E. edge 4" A.C. paving
+66	Toe of 4" sand (flower bed)
+77	Top of " " "

## Capistrano to Clove





## Profile of Elephant Curb

3127 W. curb line Tustin St.

3145 &amp; Tustin

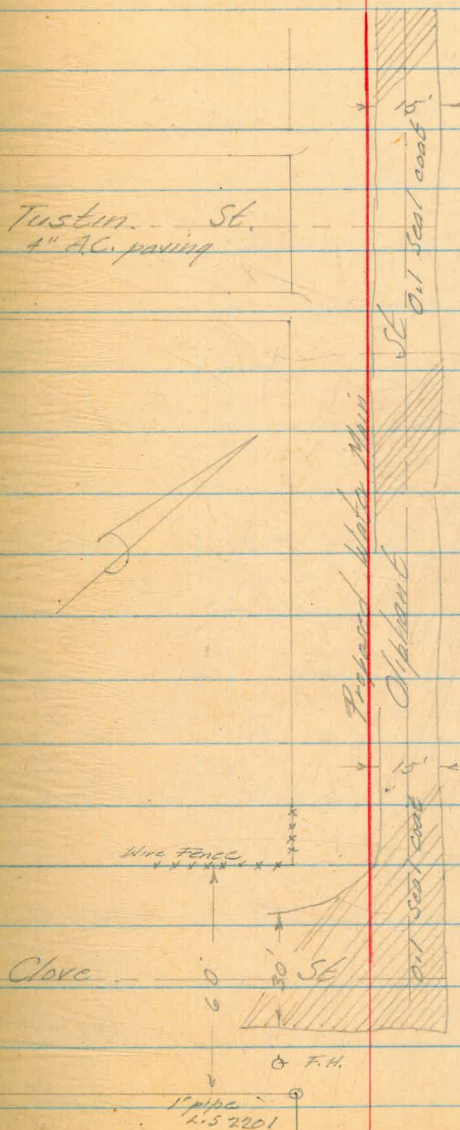
3163 E. curb line

Tustin St.  
1" A.C. paving

6127 Wire fence line W. prop. Clove

6180 F.H. 10' So. of Prop. Elephant

6187 E. prop. line Clove



Profile of Proposed Water on

Elephant, Capistrano to Clove

		129.21	
	0.16	129.37	
		12.10	117.27
	3.42	120.69	
0+00		6.7	113.99
+10		6.4	114.29
+50		4.9	115.79
+60		4.6	116.09
+66			
+70			
T.P.		0.84	119.85
	2.87	122.72	
1400		0.5	122.22
+50		+ 0.3	123.02
2400		1.7	121.02
+50		6.7	116.02

N.W. B.P. Capistrano & Macaully

W. prop. Capistrano

W. curb line Capistrano

E. " " "

E. edge 4" A.C. paving

$\frac{4.3}{10}$	$\frac{4.3}{5}$	$\frac{5.8}{8}$	$\frac{0.4}{5}$ <sup>Rb</sup>
------------------	-----------------	-----------------	-------------------------------

$\frac{3.9}{5}$	$\frac{3.9}{2}$	$\frac{0.5}{6}$	$\frac{0.0}{8}$
-----------------	-----------------	-----------------	-----------------

Hand level

## Profile of Oliphant Cont.

	122.72		
T.P.		12.36	110.36
	0.67		111.03
3100		2.2	108.83
+50		9.0	102.03
T.P.		12.89	98.14
	0.90		98.54
4100		0.3	98.24
+50		6.0	92.54
5100		8.8	89.74
+50		9.3	89.24
6100		8.3	90.24
T.P.		10.94	87.60
	7.82		95.42
6150		8.2	87.22
+80		6.8	88.62
+87		7.8	87.62

E. prop. line of Oliphant

Oliphant, Capistrano to

Clove Cont.

95.42

T.P. 2.17 93.25

12.91 106.16

T.P. 0.11 106.05

12.81 118.86

T.P. 0.21 118.65

13.22 131.87

T.P. 0.13 131.74

12.38 144.12

T.P. 0.13 143.99

4.35 148.34

T.P. 11.94 136.40

0.12 136.52

7.35 129.17

129.21

N.W. B.P. Capistrano & Macaulay

Top S.W. F.H. Oliphant & Clove

5-20-54

Profile & Proposed Water, Evergreen

Lowell to Newell

25.30

S.W. B.P. Lowell & Evergreen

6.19 31.49

0+00	5.3	26.19	No prop Lowell
+18	5.3	26.19	No curb line Lowell
+30	4.9	26.59	& Lowell
+50	5.3	26.19	
+51	5.3	26.19	No curb line Lowell
+91	5.03	26.46	Telephone M.H.
1+00	5.1	26.39	
+50	5.0	26.49	
2+00	4.8	26.69	
+50	4.2	27.29	
+84	3.7	27.79	No edge paving Macaully
+95	3.5	27.99	& Macaully
3+00	3.6	27.89	
+06	3.8	27.69	No edge paving Macaully
T.P.	3.26	28.23	

5.15 33.38

## Profile of Evergreen Cont.

33.38

3+15 4.99 28.39

Gas M.H.

+21 5.8 27.58

No. curb line Macaully

+25 5.8 27.58

E 4' Storm Drain &amp; Prop. Water

+25 8.52 24.86

Top R.C. 4' Storm Drain

+50 5.5 27.88

4+00 4.4 28.98

+40 2.6 30.78

End pavement 2" A.C. Evergreen St.

+50 1.9 31.58

T.P. 0.11 33.27

11.97 45.24

5+00 10.2 35.04

+50 3.3 41.94

+57 2.6 42.64

So curb line Newell St

+91 0.9 44.34

No. " " " "

6+00 0.5 44.74

+10 0.2 45.04

No. prop. Newell

4.65 40.59

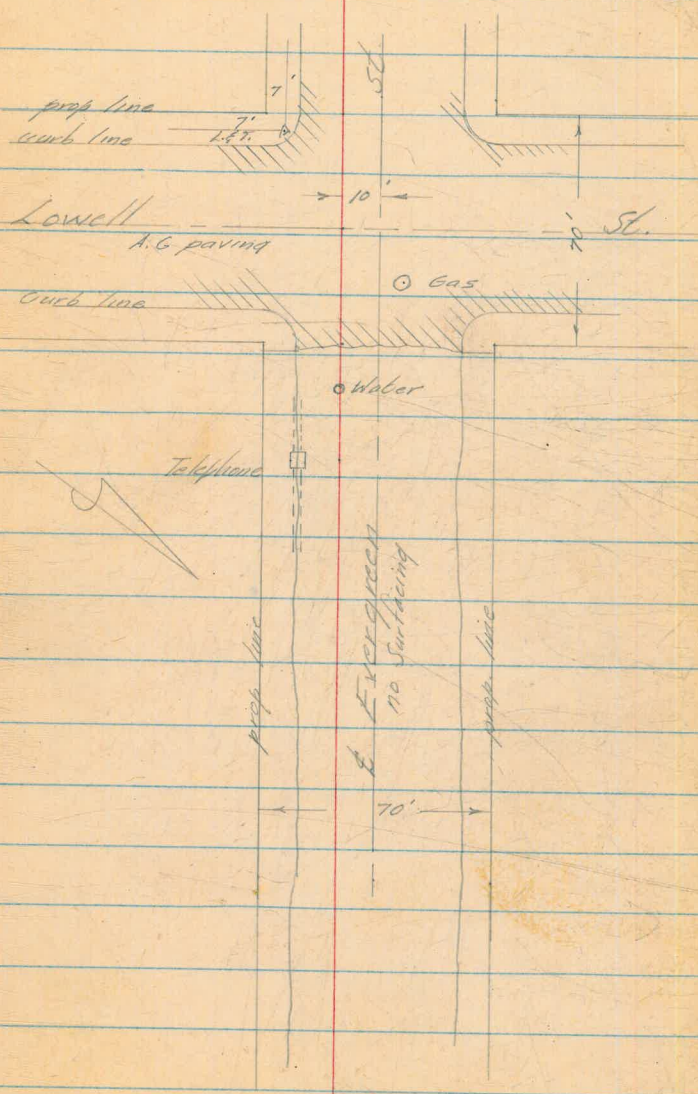
40.67

SE. Lft Newell &amp; Evergreen

# Profile of Evergreen Lowell to Newell

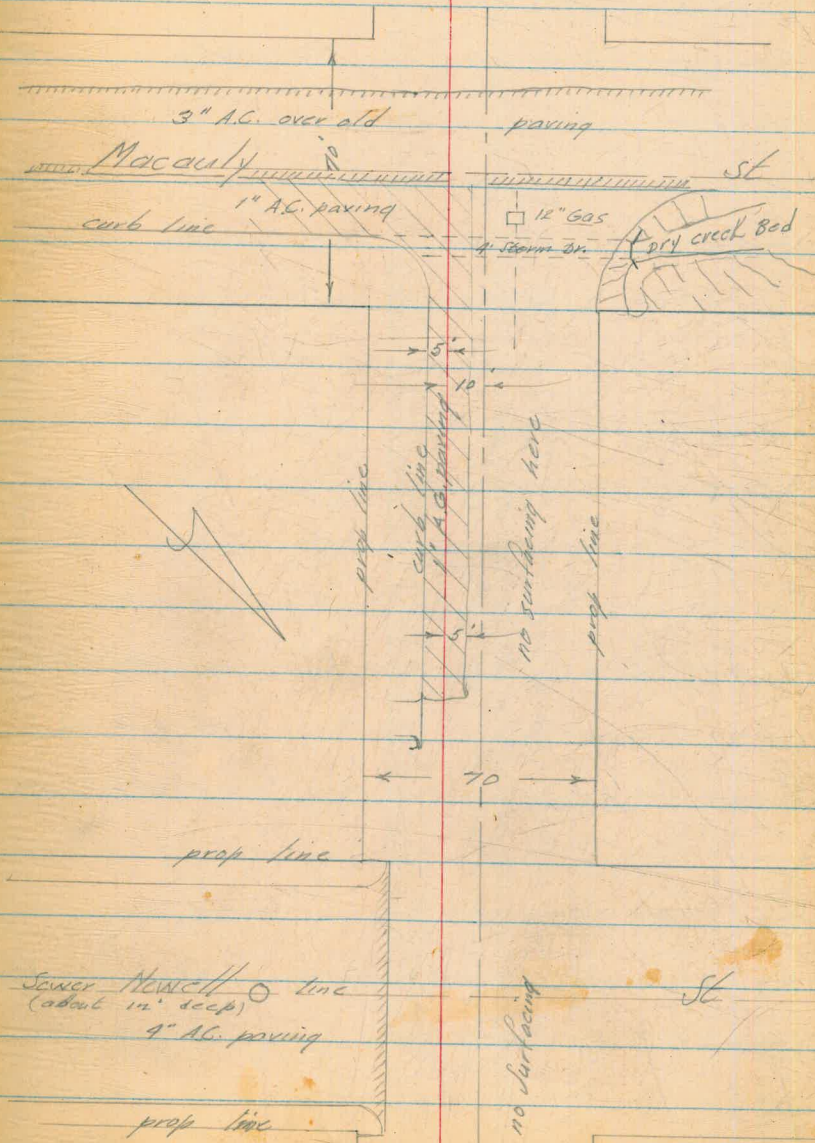
- 0+00 W. prop line of Lowell St.
- +18 W. curb line " "
- +35 E Lowell St.
- +45 Gas M.H. 15' lb.
- +51 E. curb line Lowell St.
- +72 G.L., existing 7" line
- +91 Telephone M.H. 13.5 lb. No cables cross street at M.H.

No curbs or surfacing from Sta 0+55 on Evergreen to Sta 7+84 Macaulay



Profile of Evergreen Court

- 2+89 W. edge of paving, 3" new over old
- 3+05 E. of P. Macaully
- 3+06 E. edge of paving
- 3+15 Gas M.H. 17' 14" line parall to St.
- 3+22 E. curb line, no curb on W. side
- 3+25 E. 4' Storm Drain
  
- 4+90 End of old 1" paving
  
- 5+90 W. prop. Newell St.
- 157 W. curb line
- 159 G.V. 22' H.
- 91 E. curb line
- 6+10 E. prop. line







## Profile Proposed Water La Salle St. Nashville So. 450'

	252	4.29	1.77		N.W. F.H. Nashville & La Salle	LE side		RE side		
					top curb	curb	street	water	curbline	top curb
0400			3.8	+ .49		$\frac{4.3}{25}$	$\frac{3.9}{10}$	$\frac{3.8}{0}$	$\frac{4.1}{5}$	$\frac{3.6}{5}$
+10			3.7	+ .59		$\frac{4.6}{25}$	$\frac{4.0}{10}$	$\frac{3.2}{0}$	$\frac{4.0}{5}$	
+25			3.88	+ .41	8" Sewer M.H.		7.9 to flow			
+40			4.4	- .11		$\frac{4.8}{25}$	$\frac{4.6}{10}$	$\frac{4.4}{0}$	$\frac{4.8}{5}$	
+50			4.7	- .41		$\frac{4.5}{25}$	$\frac{5.0}{25}$	$\frac{4.9}{10}$	$\frac{4.7}{0}$	$\frac{5.3}{5}$
+100			4.6	- .31		$\frac{4.5}{25}$	$\frac{5.1}{25}$	$\frac{4.7}{10}$	$\frac{4.6}{0}$	$\frac{4.9}{5}$
+150			4.7	- .41		$\frac{4.4}{25}$	$\frac{5.0}{25}$	$\frac{4.9}{10}$	$\frac{4.7}{0}$	$\frac{5.0}{5}$
+200			4.6	- .31		$\frac{4.4}{25}$	$\frac{4.5}{25}$	$\frac{4.8}{10}$	$\frac{4.6}{0}$	$\frac{4.3}{5}$

4.29

top curb curb street water curb top curb

2+50

4.4

- .11

 $\frac{4.3}{25}$  $\frac{4.8}{25}$  $\frac{4.5}{10}$  $\frac{4.4}{8}$  $\frac{4.5}{5}$  $\frac{4.2}{5}$ 

3+00

4.2

+ .09

 $\frac{4.0}{25}$  $\frac{4.6}{25}$  $\frac{4.3}{10}$  $\frac{4.2}{8}$  $\frac{4.2}{5}$  $\frac{4.0}{5}$ 

+25

3.88

8" Sewer M.H. 6.5 to flow

+50

4.1

+ .19

 $\frac{3.9}{25}$  $\frac{4.4}{25}$  $\frac{4.1}{10}$  $\frac{4.1}{8}$  $\frac{4.5}{5}$  $\frac{4.0}{5}$ 

4+00

4.2

+ .09

 $\frac{3.8}{25}$  $\frac{4.3}{25}$  $\frac{4.3}{10}$  $\frac{4.2}{8}$  $\frac{4.7}{5}$  $\frac{3.9}{5}$ 

+53

3.5

+ .79

 $\frac{3.2}{25}$  $\frac{3.7}{10}$  $\frac{3.5}{8}$  $\frac{3.6}{5}$  $\frac{3}{5}$ 

T.P.

2.52

1.77

B.M. on T.H.

BK 2  
 Alley E of Menlo  
 Mt Polk  
 5K5 for 6' 40' Main + Motors

West  
 Williams  
 Varanfokis  
 Kellhofer

65

2/2/57

0.55 349.37 348.82

TAM Top FH NE cor. Menlo + Polk

8.20 354.76 281 346.56

0+80	3.2	351.0	347.6	C4 $\frac{0}{}$	Begin work
1+00	3.3	351.5	347.2	C4 $\frac{3}{}$	
+50	3.7	351.1	346.5	C4 $\frac{6}{}$	
+49	3.9	350.9	350.4	C0 $\frac{5}{}$	WM W
+59	3.9	350.9	350.3	C0 $\frac{6}{}$	WM W
2+00	4.3	350.5	346.0	C4 $\frac{5}{}$	
2+00	4.7	350.1	349.8	C0 $\frac{3}{}$	WMW
+11	4.5	350.3	349.9	C0 $\frac{4}{}$	WME
+48	4.9	349.9	349.2	C0 $\frac{7}{}$	WME
2+50	4.9	349.9	345.4	C4 $\frac{5}{}$	
+50	5.2	349.6	349.0	C0 $\frac{6}{}$	WMW
3+00	6.0	348.9	344.6	C4 $\frac{2}{}$	
+08	6.2	348.6	348.2	C0 $\frac{4}{}$	WME
+21	6.8	348.0	347.6	C0 $\frac{4}{}$	WMW
+41	7.0	347.8	347.3	C0 $\frac{5}{}$	WMW
+08	6.3	348.5	343.7	C4 $\frac{8}{}$	

BLK 2

E. OF MENLO  
N. OF POLK

354.76

3+58 6.4 348.4 347.0

4+00 8.0 346.8 342.8

+04 8.1 346.7 346.2

+08 8.1 346.7 346.0

+47 9.5 345.3 345.3

9.21 349.76 9.21 345.55

4+50 3.9 345.9 342.0

+52 4.0 345.8 345.3

5+00 4.4 345.4 341.0

+05 4.5 345.3 344.8

+19 4.4 345.4 344.7

+36 4.7 345.1 344.7

+50 4.6 345.2 340.6

+64 5.2 344.6 344.6

+87 5.3 344.5 344.4

6+00 5.2 344.6 340.4

+21 5.1 344.7 344.3

+37 5.4 344.4 344.0

+50 5.6 344.2 340.0

+55 6.0 443.9 340.0

6.52 349.90

6.38 343.38

104 348.86 = 348.82

WEST  
WILLIAMS  
VARONFAKIS  
KELLHOFER

66.

7/7/54

C1  $\frac{4}{1}$ 

WME

C4  $\frac{0}{1}$ C0  $\frac{5}{1}$ 

WME

C0  $\frac{1}{1}$ 

WMW

C0  $\frac{0}{1}$ 

WMW

C3  $\frac{9}{1}$ C0  $\frac{5}{1}$ 

WME

C4  $\frac{4}{1}$ C0  $\frac{5}{1}$ 

WME

C0  $\frac{1}{1}$ 

WMW

C0  $\frac{4}{1}$ C0  $\frac{0}{1}$  → 4  $\frac{6}{1}$ 

WME

C0  $\frac{1}{1}$ 

WMW

C0  $\frac{1}{1}$ 

WME

C4  $\frac{2}{1}$ C0  $\frac{4}{1}$ 

WMW

C0  $\frac{4}{1}$ 

WME

C4  $\frac{2}{1}$ C3  $\frac{8}{1}$ 

End of work

Mission St  
Madison to Texas

WEST  
WILLIAMS  
VARONFAKIS  
KELLHOFER

67.

9/20/54  
HOT

687	349.15	342.78	
0+10		5.8 343.4	339.4
+50		5.4 343.8	339.6
1+00		5.1 344.1	340.0
+50		4.8 344.4	340.4
+57 wnw		5.0 344.2	
2+00		5.0 344.2	340.8
+08 wnw		4.5 344.7	
+50		5.3 343.9	340.4
+50 wnw		4.3 344.9	
+90 wnw		4.2 345.0	
3+00		5.5 343.7	340.2

SEBP Madison + Louisiana

C4 <sup>0</sup> Begin work

C4 <sup>2</sup>

C4 <sup>1</sup>

C4 <sup>0</sup>

C4 <sup>4</sup>

C3 <sup>4</sup>

C3 <sup>5</sup>

C3 <sup>5</sup>

C3 <sup>5</sup>

C3 <sup>5</sup>

C3 <sup>5</sup>

334	347.27	522	343.93
+30		3.8 343.5	340.1
+40 <sup>65</sup> Ect		3.9 343.4	340.0
+50		3.9 343.4	340.0
+75		4.2 343.1	339.4
4+00		3.3 344.0	340.6
+09 <sup>02</sup> x		3.3 344.0	340.5

C3 <sup>4</sup>

C3 <sup>4</sup>

C3 <sup>4</sup>

C3 <sup>1</sup>

C3 <sup>4</sup>

C3 <sup>5</sup>

347.27

4+27.07 Tee

3.3 344.0340.4

C3  $\frac{6}{}$ 

+50

3.4 343.9340.2

C3  $\frac{7}{}$ 

5+00

3.9 343.4339.8

C3  $\frac{6}{}$ +23<sup>5</sup> <sup>Work</sup> End of.

4.1 343.2339.6

C3  $\frac{6}{}$ 

0+05

3.2 344.1340.2

C3  $\frac{9}{}$ +37<sup>2</sup>

5.3 342.0338.6

C3  $\frac{4}{}$ +62<sup>2</sup>

9.1 338.2333.4

C4  $\frac{8}{}$ 

1+04

9.5 337.8333.2

C4  $\frac{6}{}$ 

3.48 348.31 2.44 344.83

6.01 342.30 = 342.58





49th & Imperial  
 & Profile proposed DRAIN  
 From SAND TRAP

9/23/52

70

BM	0.44	185.30	184.86		
TD	0.79	172.86	13.23	172.07	
TD	0.12	159.72	13.26	159.60	
TD	3.63	150.82	12.53	147.19	
SET TBM			4.59	146.23	
0+00		& IMPERIAL AVE on A.C. Pavt.	4.58	146.24	
0+17		Edge A.C. Pavt	5.09	145.74	
0+33		Edge Conc. Val Cham.	5.33	145.49	
0+38.5		Edge " " "	5.25	145.54	
0+41			4.5	146.3	
0+48			4.5	146.3	
0+56			8.7	142.1	
0+67.5 0+68		on Conc Curb	11.91	138.91	
0+68		Curb	13.33	137.49	
TD	3.67	142.34	12.15	138.67	
0+83		Edge Conc ditch	5.05	145.77	137.3
0+84		Bottom " " "	5.50	145	136.8
1+08.23		" " " "	5.98		136.4

NW Cor Val Cham 0+39

138.3  
 4.01 5.47 5.98 5.47 5.27 4.03 4.03 4.03  
 0.85 0.85 0 0.8 1.2 1.4 1.4 1.4  
 136.9  
 136.4  
 136.9  
 138.3  
 138.3  
 138.3

49th & Imperial  
Drain Line  
(Cont'd.)

9/23/54

71

142.34  
1+50 5.8 136.5

1+82 5.2 137.1

2+00 8.7 133.6

2+12 9.1 133.2

2+30<sup>40</sup> P1 5.5 136.8

2+50 8.2 134.1

2+54 8.1 134.2

2+67 10.3 132.0

2+80 9.6 132.7

2+90 6.6 135.7

3+00 8.0 134.3

3+00 2.26 131.67 130.3 129.31

3+33 4.9 126.8

Left

Right  
139.0 137.0 136.5 136.2 136.8 134.0  
3.3 5.3 5.8 6.1 5.5 8.2  
10 4 2 6 15 20

140.2 137.9 137.1 135.3 135.5 138.7  
2.1 4.4 5.2 7.0 6.8 3.6  
10 7 8 5 15 19

135.9 133.6 133.6 134.2 134.8 138.3  
6.2 8.7 8.7 8.1 7.5 4.0  
10 5 8 10 15 25

6.2 9.6 9.1 6.1  
15 10 8 10

Split of 7

7.6 10.1 10.2 8.4 5.5 3.8  
35 30 20 10 2 10

7.3 10.6 9.2 8.2 7.3  
35 20 10 2 10

Slope of  
Solid fill dump 0.0 6.6 9.7 9.7 8.4  
10 6 8 15

dito. 0.0 8.0 4.1 4.1 9.3  
12 5 7 15

49<sup>th</sup> Imperial

(Cont.d.)

131.67

3+50 6.6 125.1

3+96 8.6 123.1

4+00 7.3 124.4

4+18 7.5 124.2

4+50 10.9 120.8

① 2.64 120.96 13.35 118.32

4+68 2.9 118.1

4+90 3.1 117.9

5+00 4.4 116.6

5+15 5.9 115.1

5+35 5.9 115.1

5+50 7.8 113.2

5+67 7.8 113.2

6+00 11.4 109.6

① 3.92 111.77 13.11 107.85

6+32 3.2 108.6

6+46 5.1 106.7

6+50 4.6 107.2

6+60 3.7 108.1

9/23/50

72.

Slope of Solid  
Fill Dump2.7 5.8 6.6 6.6 4.0  
16 10 4 5 10

gully

6.7 7.3 8.3 9.2 8.4 6.0  
10 5 4 12 15 209.0 10.9 13.9 13.4 10.0  
10 5 15 25 301.5 3.1 4.4 6.1 6.0 1.9  
15 10 5 10 15 254.6 6.3 7.8 8.6 8.4 4.1  
15 10 5 6 12 259.9 11.4 11.4 10.9 8.1  
10 5 5 10 252.7 4.6 5.1 5.0 2.4  
10 5 5 6 15

49<sup>TH</sup> & IMPERIAL  
(Cont'd.)

9/23/50

73

111.77

6+72 5.5 106.3

6+91 8.0 103.8

6+93 8.4 103.4

6+95 8.4 103.4

7+00 8.0 103.8

7+15 8.5 103.3

7+20 9.8 102.0

7+25 10.4 101.4

7+32 8.5 103.3

7+50 8.0 103.8

7+80 8.3 103.5

8+00 10.4 101.4

8+15 edge of gully 12.6 99.2

8+35 " " " 13.0 98.8

8+43 11.3 100.5

8+50 10.9 100.9

8+72 10.3 101.5

8+85 8.1 103.7

9+00 8.8 103.0

5.7 8.5 8.7 8.0 4.8  
15 8 4 2 10

6.2 8.0 8.3 11.6 11.4 7.9  
10 2 4 12 15 20

8.8 10.1 10.4 10.7 13.1 12.8 10.3  
20 10 2 5 10 15 20

9.0 10.0 10.9 13.0 12.6 12.4  
20 10 8 12 25 35

to gully 65' left

49th &amp; Imperial

9/23/54

74

111.77

9+17 9.9 101.9

9+29<sup>5/4</sup> Edge oiled road 12.15 99.62

9+43 &amp; " " 12.91 98.86

TP 3.83 102.55 13.05 98.72

9+50 on oiled road 4.49 98.06

9+57<sup>NW</sup> Edge oiled road 5.50 97.05

9+63 5.7 96.9

9+64 5.1 97.5

9+81<sup>10</sup> Pl. 6.9 95.7Rim 6.98 95.57  
Inv. 13.81 88.74

10+00 5.5 97.1

10+50 4.5 98.1

11+00 4.1 98.5

11+50 1.9 101.3

TP 6.96 106.32 3.19 99.36

6.2 57 39 00  
10 4 2 15(RT & FWD Tang) 8.1 6.9 6.4 3.6  
10 4 10 13

(5' LT &amp; to 1/2 mile)

Run of Sew. M.H. { 33' LT 9+43<sup>5</sup> 11 & ST  
20' LT 9+63 at RT 45 to 47.5 7.2 6.7 5.5 4.1 0.0  
10 7 6 4 8 156.5 4.5 2.5  
10 4 86.9 4.1 1.0  
10 4 104.5 4 4.5  
10 4 10

49<sup>TH</sup> & IMPERIAL  
(Cont.d.)

9/23/54

75

106.32

11+65		3.3	103.0
11+70		3.3	103.0
11+78		4.5	101.8
11+80		5.4	100.9
11+88		-9.0 14.4	91.9
11+94		-8.0 22.4	83.9
12+06		29.2	77.1
12+14		31.7	74.6
12+45	Sly edge Cholla's channel & Flow line	34.3	72.0
Set TBM.	11.83	106.39	11.76 94.56
P	13.06	119.45	0.00 106.39
	Rim	5.60	113.85
	Inn.	11.64	107.81
P	12.88	131.38	0.95 118.50
P	11.38	142.62	0.14 131.24
P	10.25	152.07	0.80 141.82
CK TBM	7.65	153.89	5.83 146.24 = 146.23
P	3.73	149.99	7.63 146.26
CK P (WEST)		5.76	144.23 = 144.35

335 LT  
2150 RT  
2

Nail in pole 16' LT 10+89

Rim JEW MH 215' LT along H & St  
9+432

NW Cor. Val Chamber 0439

L400 Gloria & Franklin

MANZANITA DRIVE

ELY End Poppy PLACE TO WLY TERMINUS  
 ⑤ STKS & GRDS FOR 8" A.C. WATER

SEPT. 24, 1954

DEATY  
 SHOREY  
 MARTELL  
 ALEXANDER

76.

TBM							
	6.09	289.61		283.52			
1+22	8x6 TEE		5.5	284.1	280.2	C39	52
1+47	BC		5.4	284.2	279.9	C43	53
1+50			5.0	284.2	279.9	C43	53
1+75			5.5	284.1	279.6	C45	55
2+00			5.2	284.4	279.4	C50	58
2+05	EC (also Rduy EC)		5.1	284.5	279.3	C52	58
2+50			4.5	285.1	278.9	C62	66
2+85	45° BEND (Δ = 41° 1' LT)		5.1	284.5	278.5	C60	51
3+00					278.3		
3+07.70 BK							
3+13	45° BEND (Δ = 41° 08' LT)		5.6	284.0	278.2	C58	56
3+10.33 AH							
3+25			5.5	284.1	278.0	C61	61
3+75			7.0	282.6	277.0	C56	75
4+25			9.2	280.4	274.8	C56	
4+50			9.8	279.8	273.1	C62	4+50 11.1 8
4+76	End Work		12.3	277.3	271.4	C59	12.3
4+78							
4+88	11) 0.75	278.39	11.97	277.64	= 277.63		
4+80	Begin Work		1.3	277.1	271.2	C59	19
5+00			1.7	276.7	270.4	C63	23
5+50			4.9	273.5	268.4	C51	47
5+66 BC			6.4	272.0	267.5	C45	56

Nail in Po Pole

MANZANITA DR.  
(Cont'd.)

9/24/54

208.3

72

9

12

207.4

37

25

5+75	278.39	6.8	271.6	267.0	C46	5+75 $\frac{60}{2}$	
6+00		8.2	270.2	265.7	C45		72
6+25		8.8	269.6	264.3	C53	6+25 $\frac{83}{2}$	72
6+50		10.1	268.3	263.0	C53		94
6+75		10.5	267.9	261.7	C62	6+75 10.2	111
7+00		11.0	267.4	260.4	C70		114
7+05 <sup>82</sup> EC (Also Rdwy DC)		11.0	267.4	261.1	C63		133
7+50		12.7	265.7	257.5	C82		29
TD	0.62	265.69	13.32	265.07			55
7+75		2.7	263.0	256.0	C70		102
8+00		5.4	260.3	254.2	C61		120
8+50		9.7	256.0	250.6	C54		127
TD	8.28	261.30	12.67	259.02			
9+00		9.8	251.5	247.0	C45		
9+12	12"x8" TEE	10.5	250.8	245.6	C52		
CK TOM Nail IN P. PINE		0.22	261.08	261.07			

WATER METERS

1+47 Nly.	289.6	4.4	285.2	284.6	C06	✓	4028 Manzanita
2+875 Nwly	"	4.5	285.1	282.9	C22		4018
3+70 Nwly		7.7	281.9	281.4	C05		4008
3+79 SEly		7.1	282.5	281.1	C14		4007
4+10 Nwly		9.2	280.4	279.5	C09	✓	4004
4+25 SEly	No EXIST MET	9.1	280.5	278.2	C23		? Poppy Drive
4+47		10.7	278.9	277.3	<del>C45</del> C14		3978



9/24/54

650 4.0

78

WAT.

4+96 NWly	278.39	1.0	277.4	275.3	C21	3970 Mangawita
5+95 NWly		6.2	272.2	270.4	C18	3948
				265.3	C20	
6+75 SELy		11.1	267.3	263.6	C32	3945
<del>6+95</del>						
7+68 NWly		10.1	268.3	264.8	C35	3944
7+73						
7+71 NWly	265.69	2.4	263.3	260.8	C25	3934
8+17 NWly		6.2	259.5	258.0	C15	3928
8+53 NWly		9.9	255.8	255.5	C03	3912
8+76 SELy		12.5	253.2	253.3	F01	No Address

Catalina Standpipe  
Drain line  
Elevs of M.H

4+96 BM 3.78 38694 383.16

5+95

6+75 ♀ Bottom of Manhole 9.60

6+95

7+68

Lip of Bell of C.I. Drain 9.50

7+73

7+71

♂ of

8+17

8+53

8+76

269.80		LT	RT
109+50	4.6	4.8 10	5.6 2
+57	5.9	4.0 2	17 10
+67	7.7		
+75	8.7		
+90	11.2		
110+00	12.7	12.4 10	13.6 1
		11.4 4	10.4 10
0.33	256.88 ✓	13.25	256.55
110+11	1.9		
+18	3.0		
0.57	244.53 ✓	12.92	243.96 ✓
0.28	231.97 ✓	12.84	231.69 ✓
0.18	218.83 ✓	13.32	218.65 ✓
0.03	205.71 ✓	13.15	205.68 ✓
0.08	192.86 ✓	12.93	192.78 ✓
0.36	180.12 ✓	13.10	179.76 ✓
0.31	167.23 ✓	13.20	166.92 ✓
0.71	154.76 ✓	13.18	154.25 ✓
0.14	142.34 ✓	12.56	142.20 ✓
0.52	129.61 ✓	13.25	129.09 ✓
0.85	117.50 ✓	12.96	116.65 ✓
8.64	116.80 ✓	9.34	108.16 ✓
4.92	120.91 ✓	0.81	115.99 ✓
1.82	113.67	9.04	111.87 ✓
			112.13 ✓
			108.26 ✓
		5.43	108.52 ✓

420.57  
13.40  
407.19  
7.26  
415.15

SEBP

32nd  
of Adams

385.80

34th on SW1/4

385.35

319.29		LT	RT
104	307.36 ✓	12.97	306.32 ✓
105+00	4.2	4.4 10	3.3 10
+20	5.5		
+50	7.3	7.6 10	7.7 5
+75	8.5		6.4 10
106+00	10.0	10.3 10	10.7 4
+25	11.5		9.2 10
+50	12.7	13.1 10	11.9 10
108	295.21 ✓	12.23	294.13 ✓
107+00	3.1	3.2 10	2.2 10
+18	4.0		
+50	6.0	6.2 10	4.9 10
+83	8.2		
108+00	9.4	9.5 10	9.7 2
+17	10.3		8.8 2
108+43 <sup>21</sup> Δ PT.	12.9		8.1 10
0.35	282.61 ✓	12.95	282.26 ✓
108+50	0.9	2.0 10	2.4 3
+70	2.9		0.5 2
+90	6.2		0.8 10
109+00	7.7	9.1 10	9.2 3
+20	12.0		7.4 1
0.24	267.80 ✓	13.05	267.56 ✓

(CONT'D. OVER)

5.90

3.25

9.15

TBM S.E. COR.

Gas Co, M.H.

0.28 440.26 ✓ 439.98 ✓

TP 0.00 428.06 12.20 428.06 ✓

S. EDGE M.H. 3.40 424.66  
68493

TP 4.57 420.59 12.04 416.02 ✓

7.91 415.15 13.35 407.24 ✓

OK. TBM ONAVA, M.H. 4.20 410.95 =  
411.19

381.04				
2.06	369.86 ✓	13.24	367.80 ✓	
100+40	0.8	LT	RT	
+50	2.3	3.7 10	3.2 3	0.2 10
101+00	10.1	11.8 10	11.5 5	7.7 10
0.87	357.39 ✓	13.34	356.52 ✓	
101+17	0.6	LT	RT	
+50	6.4	8.0 10	7.6 6	4.1 10
+63	8.4			
0.72	345.01 ✓	13.10	344.29 ✓	
102+00	2.0	LT 3.4 10	3.0 4	RT 0.1 10
+10	3.3			
+50	9.7	11.0 10	11.5 3	8.3 10
+71	12.1			
0.23	332.00 ✓	13.24	331.77 ✓	
102+70	2.6	LT	RT	
103+00	4.3	5.1 10	2.8 10	
+13	6.5			
+50	11.6	12.4 10	11.8 3	10.0 10
0.57	319.29 ✓	13.28	318.72 ✓	
103+75	2.4	LT	RT	
+20	4.1			
104+00	5.4	6.3 10	6.0 3	4.4 3
+15	7.5			
+50	11.3	12.0 10	11.8	9.6 10

### PROFILE OF PROPOSED MURRAY PIPELINE

2.97	414.15		411.18 ✓
5.57	406.71	13.03	401.12 ✓
OK. BM	M.H. 96+50	3.24	403.47 ✓
			403.52
2.46	405.93 ✓		403.47
96+77.45	P.O.T	4.7	LT
97+00		4.3	RT
+50		6.0	6.2 10
+70		8.3	5.7 7
98+00		9.4	4.9 10
98+19.66	P.O.T	11.0	9.4 10
98+37		12.2	7.3 6
			8.6 10
0.91	393.86 ✓	12.98	392.95 ✓
98+50	1.6	LT 2.0 10	RT 1.4 5
+85	4.8		10.5 10
99+00	6.8	7.3 10	6.3 4
+35	11.1		4.4 10
+50	13.1		
		13.7 10	10.7 10
0.53	381.04 ✓	13.35	380.51 ✓
99+60	1.0	LT	RT
100+00	6.5	7.3	5.4 4
			4.5 10

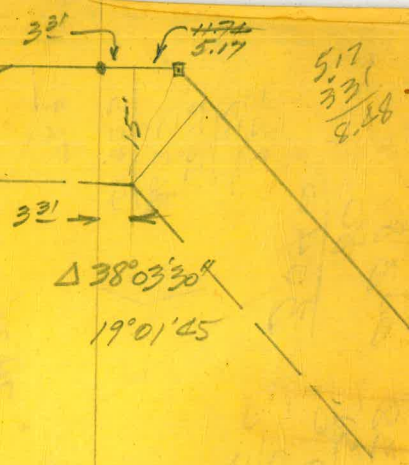
(CONT'D OVER)

$\begin{array}{r} .0038 \\ \underline{55} \\ 190 \\ \underline{190} \\ 7090 \end{array}$	$\begin{array}{r} .0038 \\ \underline{80} \\ 3040 \end{array}$
	$\begin{array}{r} 725 \\ \underline{0057} \\ 5075 \\ \underline{3625} \\ 41325 \end{array}$
$\begin{array}{r} 74.26 \\ \underline{0057} \\ 51982 \\ \underline{37130} \\ 423282 \end{array}$	$\begin{array}{r} 74.26 \\ \underline{42} \\ 73.84 \text{ from} \end{array}$
$\begin{array}{r} 35^{\circ}02' \\ 17-31 \end{array}$	$\begin{array}{r} 949290 \\ \underline{7384} \\ 8499.05 \end{array}$
$\begin{array}{r} 1.048625 \\ \underline{55} \\ 5243125 \\ \underline{5243125} \\ 57.674375 = 57.67 \end{array}$	$\begin{array}{r} 180- \\ \underline{35-02} \\ 215-02 \\ \underline{107-31} \\ 98-00 \\ \underline{9-31} \end{array}$

~~7831611~~  
~~7826919~~  
~~4892~~  
~~2326~~

Proposed  $\Delta$

EXIST. 42" WATER



~~5.17~~  
~~3.31~~  
~~9.48~~

~~Tan 7829265~~  
~~15~~  
~~39146325~~  
~~7829265~~  
~~117438975~~  
~~3156186~~  
~~15~~  
~~15780930~~  
~~3156186~~  
~~47342790 = 4.73~~

~~3449785~~  
~~3446530~~  
~~3255~~  
~~814~~  
~~3448971~~  
~~15~~  
~~17244855~~  
~~3228971~~  
~~51734565~~

~~15780930~~  
~~15780930~~  
~~173590230~~

Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center

390.89  
 0.30  
 386.89

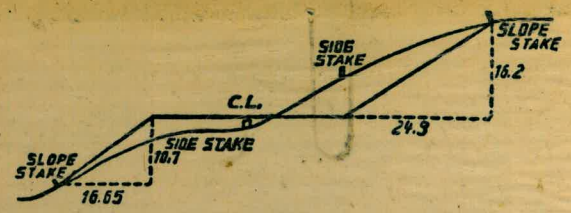
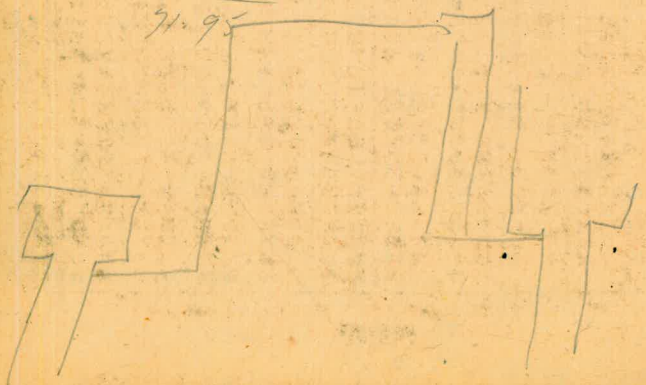
6.30  
 13.01

Glenn & Franklin

4400 - 144.35

71.20 W of cap tk  
 79

71.95



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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