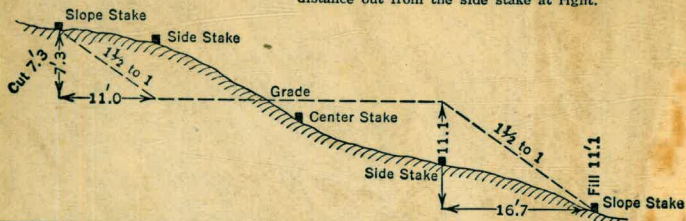


W 888

BUTTKES  
DATA

**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING**  
**Roadway of any Width. Side Slopes 1½ to 1.**

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



BUTTRESS X-SECTIONS  
 8-52  
 HRS

| Cut or Fill | Distance out from Side or Shoulder Stake |      |      |      |      |      |      |      |      |      |    | Cut or Fill |
|-------------|--|------|------|------|------|------|------|------|------|------|----|-------------|
|             | 0  | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | 0  |             |
| 0           | 0.0                                      | 0.2  | 0.3  | 0.5  | 0.6  | 0.8  | 0.9  | 1.1  | 1.2  | 1.4  | 0  |             |
| 1           | 1.5                                      | 1.7  | 1.8  | 2.0  | 2.1  | 2.3  | 2.4  | 2.6  | 2.7  | 2.9  | 1  |             |
| 2           | 3.0                                      | 3.2  | 3.3  | 3.5  | 3.6  | 3.8  | 3.9  | 4.1  | 4.2  | 4.4  | 2  |             |
| 3           | 4.5                                      | 4.7  | 4.8  | 5.0  | 5.1  | 5.3  | 5.4  | 5.6  | 5.7  | 5.9  | 3  |             |
| 4           | 6.0                                      | 6.2  | 6.3  | 6.5  | 6.6  | 6.8  | 6.9  | 7.1  | 7.2  | 7.4  | 4  |             |
| 5           | 7.5                                      | 7.7  | 7.8  | 8.0  | 8.1  | 8.3  | 8.4  | 8.6  | 8.7  | 8.9  | 5  |             |
| 6           | 9.0                                      | 9.2  | 9.3  | 9.5  | 9.6  | 9.8  | 9.9  | 10.1 | 10.2 | 10.4 | 6  |             |
| 7           | 10.5                                     | 10.7 | 10.8 | 11.0 | 11.1 | 11.3 | 11.4 | 11.6 | 11.7 | 11.9 | 7  |             |
| 8           | 12.0                                     | 12.2 | 12.3 | 12.5 | 12.6 | 12.8 | 12.9 | 13.1 | 13.2 | 13.4 | 8  |             |
| 9           | 13.5                                     | 13.7 | 13.8 | 14.0 | 14.1 | 14.3 | 14.4 | 14.6 | 14.7 | 14.9 | 9  |             |
| 10          | 15.0                                     | 15.2 | 15.3 | 15.5 | 15.6 | 15.8 | 15.9 | 16.1 | 16.2 | 16.4 | 10 |             |
| 11          | 16.5                                     | 16.7 | 16.8 | 17.0 | 17.1 | 17.3 | 17.4 | 17.6 | 17.7 | 17.9 | 11 |             |
| 12          | 18.0                                     | 18.2 | 18.3 | 18.5 | 18.6 | 18.8 | 18.9 | 19.1 | 19.2 | 19.4 | 12 |             |
| 13          | 19.5                                     | 19.7 | 19.8 | 20.0 | 20.1 | 20.3 | 20.4 | 20.6 | 20.7 | 20.9 | 13 |             |
| 14          | 21.0                                     | 21.2 | 21.3 | 21.5 | 21.6 | 21.8 | 21.9 | 22.1 | 22.2 | 22.4 | 14 |             |
| 15          | 22.5                                     | 22.7 | 22.8 | 23.0 | 23.1 | 23.3 | 23.4 | 23.6 | 23.7 | 23.9 | 15 |             |
| 16          | 24.0                                     | 24.2 | 24.3 | 24.5 | 24.6 | 24.8 | 24.9 | 25.1 | 25.2 | 25.4 | 16 |             |
| 17          | 25.5                                     | 25.7 | 25.8 | 26.0 | 26.1 | 26.3 | 26.4 | 26.6 | 26.7 | 26.9 | 17 |             |
| 18          | 27.0                                     | 27.2 | 27.3 | 27.5 | 27.6 | 27.8 | 27.9 | 28.1 | 28.2 | 28.4 | 18 |             |
| 19          | 28.5                                     | 28.7 | 28.8 | 29.0 | 29.1 | 29.3 | 29.4 | 29.6 | 29.7 | 29.9 | 19 |             |
| 20          | 30.0                                     | 30.2 | 30.3 | 30.5 | 30.6 | 30.8 | 30.9 | 31.1 | 31.2 | 31.4 | 20 |             |
| 21          | 31.5                                     | 31.7 | 31.8 | 32.0 | 32.1 | 32.3 | 32.4 | 32.6 | 32.7 | 32.9 | 21 |             |
| 22          | 33.0                                     | 33.2 | 33.3 | 33.5 | 33.6 | 33.8 | 33.9 | 34.1 | 34.2 | 34.4 | 22 |             |
| 23          | 34.5                                     | 34.7 | 34.8 | 35.0 | 35.1 | 35.3 | 35.4 | 35.6 | 35.7 | 35.9 | 23 |             |
| 24          | 36.0                                     | 36.2 | 36.3 | 36.5 | 36.6 | 36.8 | 36.9 | 37.1 | 37.2 | 37.4 | 24 |             |
| 25          | 37.5                                     | 37.7 | 37.8 | 38.0 | 38.1 | 38.3 | 38.4 | 38.6 | 38.7 | 38.9 | 25 |             |
| 26          | 39.0                                     | 39.2 | 39.3 | 39.5 | 39.6 | 39.8 | 39.9 | 40.1 | 40.2 | 40.4 | 26 |             |
| 27          | 40.5                                     | 40.7 | 40.8 | 41.0 | 41.1 | 41.3 | 41.4 | 41.6 | 41.7 | 41.9 | 27 |             |
| 28          | 42.0                                     | 42.2 | 42.3 | 42.5 | 42.6 | 42.8 | 42.9 | 43.1 | 43.2 | 43.4 | 28 |             |
| 29          | 43.5                                     | 43.7 | 43.8 | 44.0 | 44.1 | 44.3 | 44.4 | 44.6 | 44.7 | 44.9 | 29 |             |
| 30          | 45.0                                     | 45.2 | 45.3 | 45.5 | 45.6 | 45.8 | 45.9 | 46.1 | 46.2 | 46.4 | 30 |             |
| 31          | 46.5                                     | 46.7 | 46.8 | 47.0 | 47.1 | 47.3 | 47.4 | 47.6 | 47.7 | 47.9 | 31 |             |
| 32          | 48.0                                     | 48.2 | 48.3 | 48.5 | 48.6 | 48.8 | 48.9 | 49.1 | 49.2 | 49.4 | 32 |             |
| 33          | 49.5                                     | 49.7 | 49.8 | 50.0 | 50.1 | 50.3 | 50.4 | 50.6 | 50.7 | 50.9 | 33 |             |
| 34          | 51.0                                     | 51.2 | 51.3 | 51.5 | 51.6 | 51.8 | 51.9 | 52.1 | 52.2 | 52.4 | 34 |             |
| 35          | 52.5                                     | 52.7 | 52.8 | 53.0 | 53.1 | 53.3 | 53.4 | 53.6 | 53.7 | 53.9 | 35 |             |
| 36          | 54.0                                     | 54.2 | 54.3 | 54.5 | 54.6 | 54.8 | 54.9 | 55.1 | 55.2 | 55.4 | 36 |             |
| 37          | 55.5                                     | 55.7 | 55.8 | 56.0 | 56.1 | 56.3 | 56.4 | 56.6 | 56.7 | 56.9 | 37 |             |
| 38          | 57.0                                     | 57.2 | 57.3 | 57.5 | 57.6 | 57.8 | 57.9 | 58.1 | 58.2 | 58.4 | 38 |             |
| 39          | 58.5                                     | 58.7 | 58.8 | 59.0 | 59.1 | 59.3 | 59.4 | 59.6 | 59.7 | 59.9 | 39 |             |
| 40          | 60.0                                     | 60.2 | 60.3 | 60.5 | 60.6 | 60.8 | 60.9 | 61.1 | 61.2 | 61.4 | 40 |             |

MICROFILMED

The paper in this book No. F364A  
 is made of 50% high grade rag stock  
 with a WATER RESISTING surface sizing.

11,377-1. c, x, yk. chss.

KEUFFEL & ESSER CO., N. Y.  
 For Curve Tables see end of book.

# INDEX

| PAGE                               |   |
|------------------------------------|---|
| 1                                  | X-SECTION BUT # 15  |
| 4                                  | # 16  |
| 6                                  | # 17  |
| 8                                  | # 18  |
| 10 X-SECTION FROM D 2100 TO D 2130 |   |
| 11                                 | X-SECTION BUT # 3   |
| 13                                 | # 2   |
| 15                                 | # 1   |
| 17                                 | (CHECK CITY BOOK 798) SPILLWAY X-SECTIONS AT D 1000 S & N |
| 19                                 | ARCH RING X-SECT 6-7                                      |
| 20                                 | X-SECTION BUT # 7   |
| 23                                 | # 5   |
| 25                                 | # 4   |
| 27                                 | 6 36 # 6  |
| 28                                 | ARCH 14-15 ROUGH LOCATION                                 |
| 29                                 | " 13-14, 12-13 ROUGH LOCATION                             |
| 30                                 | " 11-12, 10-11, 9-10                                      |
| 31                                 | B.M. LEVELS BUT # 14 TO                                   |
| 33-32                              | B.M. LEVELS STUMP & ARCH 7-6                              |
| 34                                 | ARCH 9-8 ROUGH LOCATION                                   |
| 35                                 | B.M. LEVELS (CONT)  |
| 36                                 | BUT # 6 CONT  |
| 37-40                              | NEW TBM'S   |

Must be registered

MICROFILMED

Curtor

R

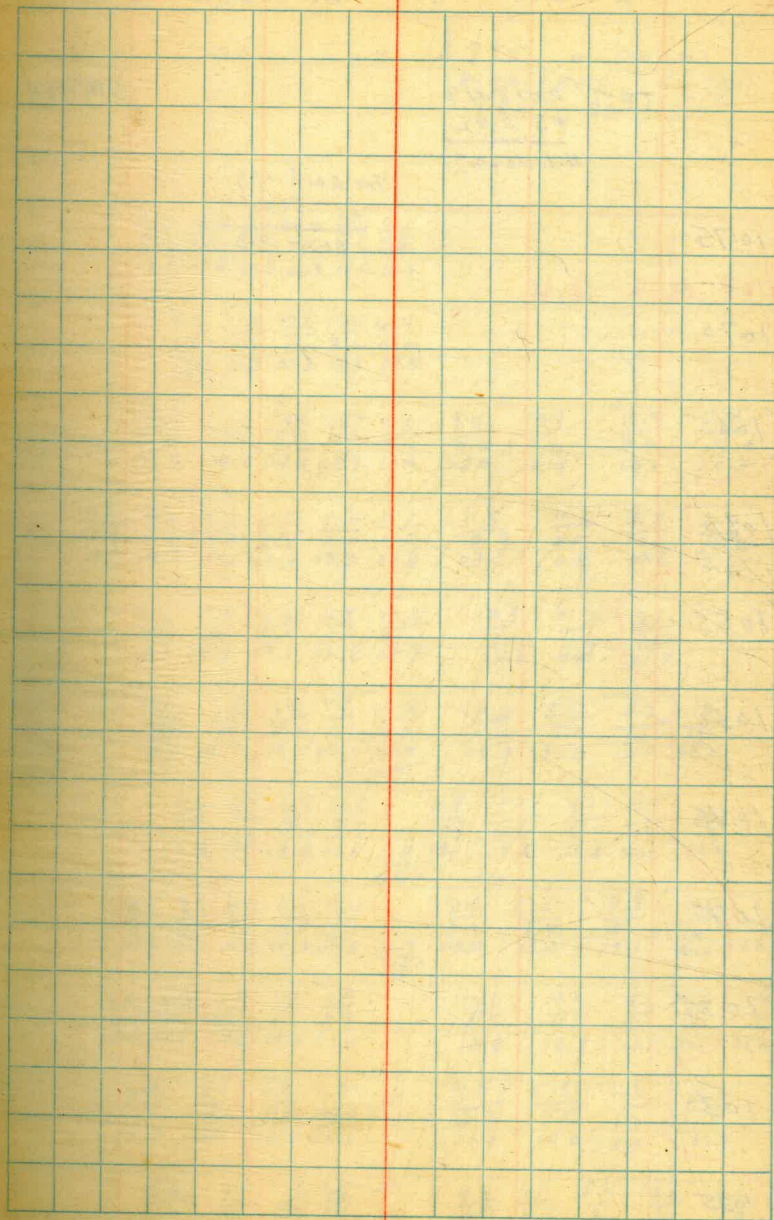
The paper in this book No. F284A  
 is made of 30% high grade rag stock  
 with a WATER-RESISTING surface sizing

40-44 FINAL X-SECTIONS TO L1016 #6

44-46 RE-X SECTION TO L1010 #6

46-47 TBM'S

49 Original Ground Butt #18





③

D 1900 #15

1020

40' 1015

35' 1010

30' 1005

25' 1000

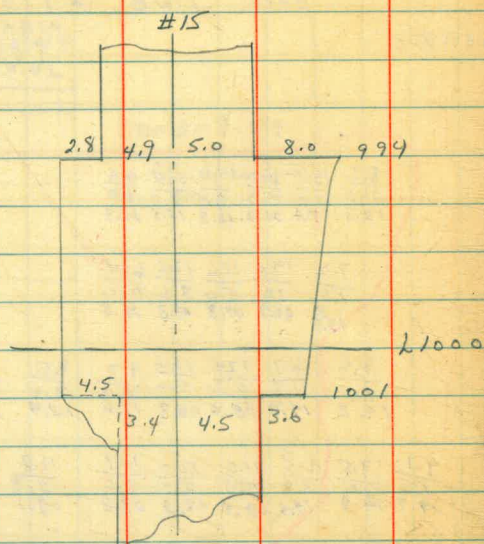
20' 995

15' 990

10' 985

5' 980

0' 975



EAST

#15

WEST

|                   |                   |                    |                    |                    |                    |                    |                    |                     |                    |
|-------------------|-------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|---------------------|--------------------|
| 6.5<br>15<br>17.3 | 7.9<br>10<br>15.9 | 5.6<br>5.0<br>15.3 | 9.3<br>3.5<br>11.6 | 9.0<br>2.6<br>11.9 | 5.1<br>5<br>15.8   | 2.6<br>1.6<br>18.3 | 1.2<br>1.5<br>22.6 |                     |                    |
| 7.5<br>15<br>16.3 | 7.9<br>10<br>15.9 | 5.7<br>5.0<br>15.2 | 8.5<br>3.4<br>11.7 | 9.2<br>1.5<br>11.7 | 8.7<br>2.9<br>12.2 | 5.7<br>3.7<br>15.2 | 4.9<br>5.0<br>16.0 | 2.8<br>1.0<br>18.1  | 1.3<br>1.5<br>22.5 |
| 7.3<br>15<br>16.5 | 7.2<br>10<br>16.1 | 5.1<br>5<br>15.8   | 5.1<br>4.5<br>15.8 | 8.5<br>2.0<br>12.4 | 8.3<br>3.5<br>12.6 | 5.0<br>4.2<br>15.9 | 4.5<br>5.0<br>16.4 | 2.8<br>1.0<br>18.1  | 2.1<br>1.5<br>21.7 |
| 5.5<br>15<br>18.3 | 6.7<br>10<br>17.1 | 4.4<br>5.0<br>16.5 | 7.1<br>3.0<br>13.8 | 8.3<br>1.5<br>12.6 | 8.2<br>2<br>12.7   | 4.4<br>5<br>16.5   | 2.8<br>1.0<br>18.1 | 1.9<br>1.5<br>21.9  |                    |
| 5.0<br>15<br>18.8 | 5.4<br>10<br>17.9 | 3.4<br>7.5<br>17.5 | 6.5<br>6.5<br>14.4 | 7.5<br>3.7<br>13.4 | 7.8<br>1.5<br>13.1 | 6.3<br>6.0<br>14.6 | 4.2<br>7.2<br>16.7 | 3.2<br>1.0<br>17.7  | 2.8<br>1.5<br>21.0 |
| 4.5<br>15<br>19.3 | 5.5<br>10<br>18.3 | 3.0<br>7.0<br>17.9 | 3.3<br>5.0<br>17.6 | 7.0<br>2.5<br>13.9 | 7.1<br>3.4<br>13.8 | 4.2<br>5.0<br>16.7 | 3.2<br>7.8<br>17.7 | 1.3<br>13.8<br>19.6 | 0.4<br>1.5<br>20.5 |
| 4.9<br>15<br>18.9 | 6.7<br>10<br>17.1 | 2.9<br>5.0<br>18.0 | 2.9<br>3.7<br>18.0 | 6.8<br>3.0<br>14.1 | 6.6<br>5.3<br>14.3 | 2.7<br>5<br>18.2   | 3.0<br>6.5<br>18.9 | 4.2<br>1.0<br>19.6  | 1.8<br>1.5<br>22.0 |
| 3.5<br>15<br>17.4 | 2.5<br>10<br>18.4 | 2.3<br>5.0<br>18.6 | 2.4<br>4.2<br>18.5 | 6.4<br>3.0<br>14.5 | 5.2<br>1.7<br>15.7 | 1.8<br>5<br>19.1   | 3.2<br>1.0<br>20.6 | 1.6<br>1.5<br>22.2  |                    |
| 4.7<br>15<br>16.2 | 3.3<br>10<br>17.6 | 2.5<br>5<br>18.4   | 1.4<br>0.0<br>19.5 | 3.5<br>5<br>20.3   | 3.5<br>5<br>20.3   | 2.2<br>10<br>21.6  | 0.5<br>1.5<br>22.3 |                     |                    |
| 7.5<br>15<br>18.4 | 7.1<br>10<br>13.8 | 5.3<br>5<br>15.6   | 4.1<br>0.0<br>19.7 | 2.6<br>5<br>21.2   | 1.7<br>10<br>22.1  | 0.4<br>1.5<br>23.4 |                    |                     |                    |

H.I. 2023.83

H.I. 2020.91

H.I. 2023.83

✓



5

995

990

0990

TSM STA 1980<sup>00</sup>  
 + 2042.51  
 + 5 2.63  
 H.I. 2045.14  
 - 10.72  
 2034.42  
 2.25  
 H.I. 2036.67

#16

01950

H.I. 2036.24

H.I. 2036.67

H.I. 2045.14

$$\begin{array}{r} 5.8 \\ 10 \\ \hline 30.9 \end{array}$$

$$\begin{array}{r} 2.5 \\ 0 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 0.4 \\ 6.0 \\ \hline 35.8 \end{array}$$

$$\begin{array}{r} 7.7 \\ 7.8 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 16.3 \\ 10.9 \\ \hline 25.9 \end{array}$$

$$\begin{array}{r} 10.5 \\ 9.2 \\ \hline 25.7 \end{array}$$

$$\begin{array}{r} +1.8 \\ 16 \\ \hline 38.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ 20 \\ \hline 39.7 \end{array}$$

$$\begin{array}{r} 2.6 \\ 30 \\ \hline 42.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ 10 \\ \hline 30.9 \end{array}$$

$$\begin{array}{r} 2.6 \\ 0 \\ \hline 34.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ 20 \\ \hline 40.5 \end{array}$$

$$\begin{array}{r} 2.0 \\ 30 \\ \hline 43.1 \end{array}$$



⑥ X-Section of Buttress #17 = D-2020  
 D-2020 = ~~2053.82~~ → = Base line for 0  
 Sta. + ~~11.31~~ - = Elev. 0

□ 11.31 ~~2053.82~~ 2042.51

□ 0.49 2050.30 2049.81

L-980 ✓

L-985 ✓

L-990 ✓

L-1000 ✓

L-1002 = Same as L-1000 ✓

L-1004 ✓

L-1010 ✓

L-1013 = Same as L-1010 ✓

□

3.99 ~~2049.83~~ (2049.81)

11-Aug. '52 Dallas - □ Dave - Tape # 4  
 Stanley - ~~11~~ Clyde Tape # 4 6  
 West East

Top Stk @ D-1980 on Axis line

Top Stk @ D-2010 on Axis line

$$\begin{array}{r} 4.6 \\ + 6.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} (2050.30) \\ + 4.9 \\ \hline 55.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ + 2.6 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 54.2 \\ + 3.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 52.3 \\ + 2.0 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 51.4 \\ + 1.1 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 51.3 \\ + 1.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 53.1 \\ + 2.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 50.0 \\ 0.3 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 50.1 \\ 0.1 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 50.3 \\ 0.0 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 50.1 \\ + 0.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 51.3 \\ + 1.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 49.8 \\ 0.6 \\ \hline 51.4 \end{array}$$

$$\begin{array}{r} 49.1 \\ 1.2 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 49.3 \\ 1.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 51.6 \\ + 1.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 49.6 \\ 0.7 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 48.4 \\ 1.9 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 42.4 \\ 7.9 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 42.4 \\ 7.9 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 42.4 \\ 7.9 \\ \hline 1.5 \end{array}$$

$$\begin{array}{r} 47.1 \\ 2.6 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 48.8 \\ 1.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 50.4 \\ 0.3 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 47.1 \\ 2.6 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 43.1 \\ 7.7 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 42.2 \\ 8.0 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 42.2 \\ 8.0 \\ \hline 1.5 \end{array}$$

$$\begin{array}{r} 47.1 \\ 2.6 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 48.4 \\ 7.9 \\ \hline 10 \end{array}$$

2x2 Hub @ 2010 on Axis line ✓

⑦ 11-Aug-52

Sta. +  $\pi$  - Elev

2057.30

L-1014 ✓

L-1020 ✓

L-1030 ✓

□

7.79 2042.51

Same party as page 6

⑦

|      | West |      | E         |      | Fog  |      | H    |
|------|------|------|-----------|------|------|------|------|
|      | 49.7 | 47.3 | (2050.30) |      | 43.5 | 47.2 | 48.5 |
|      | 10.6 | 10.9 | 7.7       | 7.9  | 6.7  | 5.5  | 2.2  |
|      | 0    | 4    | 22.5      | 0    | 2.5  | 5.5  | 10   |
| 50.7 | 48.8 | 47.8 | 45.3      | 43.2 | 43.0 | 47.3 | 47.5 |
| 0.2  | 1.5  | 2.5  | 5.0       | 7.1  | 7.3  | 3.0  | 2.7  |
| 10   | 7.5  | 4    | 2         | 0    | 6    | 7    | 10   |
|      | 48.5 | 46.5 | 44.4      | 41.3 | 41.3 | 41.3 | 45.9 |
|      | 1.7  | 3.0  | 3.9       | 9.0  | 9.0  | 9.0  | 4.4  |
|      | 10   | 4    | 0         | 1    | 5    | 10   | 10   |

Top of 2x2 @ D-1980 on Axis line

⑧ X-Section of #18 Buttress Excavation  
 @ D-2080 =  $\frac{+}{-}$   $\frac{\uparrow}{\downarrow}$  = Base line for Q

Sta. +       $\uparrow$       -      Elev.  
 1.83      2067.90      2066.07

L-985 ✓

L-990 ✓

L-997 ✓

L-999<sup>5</sup> ✓

L-1010 ✓

L-1011<sup>5</sup> ✓

L-1020 ✓

8.22      2059.68      (2059.68)

11-August 1952

Page 6 for party

| West                               |                    |                   | East               |                   |                    |                   |                  |
|------------------------------------|--------------------|-------------------|--------------------|-------------------|--------------------|-------------------|------------------|
| Top of 2x2 hub @ 2070 on Axis line |                    |                   |                    |                   |                    |                   |                  |
| (2067.90)                          |                    |                   |                    |                   |                    |                   |                  |
| $\frac{+6.5}{10}$                  | $\frac{+6.0}{5}$   | $\frac{+4.0}{0}$  | $\frac{+1.7}{4}$   | $\frac{+0.8}{10}$ |                    |                   |                  |
| 74 <sup>2</sup>                    | 73 <sup>2</sup>    | 71 <sup>2</sup>   | 69 <sup>4</sup>    | 68 <sup>7</sup>   |                    |                   |                  |
| $\frac{+6.3}{10}$                  | $\frac{+3.9}{6.5}$ | $\frac{+0.7}{0}$  | $\frac{0.7}{10}$   |                   |                    |                   |                  |
| 74 <sup>2</sup>                    | 71 <sup>2</sup>    | 68 <sup>6</sup>   | 67 <sup>2</sup>    |                   |                    |                   |                  |
| $\frac{+1.8}{10}$                  | $\frac{1.4}{3}$    | $\frac{2.2}{0}$   | $\frac{2.2}{5.5}$  | $\frac{2.2}{10}$  |                    |                   |                  |
| 69 <sup>2</sup>                    | 66 <sup>5</sup>    | 65 <sup>7</sup>   | 65 <sup>7</sup>    | 65 <sup>7</sup>   |                    |                   |                  |
| $\frac{+0.8}{10}$                  | $\frac{2.4}{3.7}$  | $\frac{4.1}{2.5}$ | $\frac{15.3}{2.2}$ | $\frac{15.4}{0}$  | $\frac{16.4}{1.8}$ | $\frac{2.7}{2.5}$ | $\frac{2.7}{10}$ |
| 68 <sup>2</sup>                    | 65 <sup>5</sup>    | 63 <sup>2</sup>   | 52 <sup>6</sup>    | 52 <sup>5</sup>   | 51 <sup>5</sup>    | 65 <sup>2</sup>   | 65 <sup>2</sup>  |
| $\frac{0.5}{10}$                   | $\frac{3.3}{5.5}$  | $\frac{4.1}{1.5}$ | $\frac{16.0}{1.5}$ | $\frac{15.7}{0}$  | $\frac{15.6}{2.5}$ | $\frac{4.3}{2.5}$ | $\frac{4.6}{10}$ |
| 67 <sup>2</sup>                    | 64 <sup>6</sup>    | 63 <sup>2</sup>   | 51 <sup>2</sup>    | 52 <sup>2</sup>   | 52 <sup>2</sup>    | 63 <sup>6</sup>   | 63 <sup>3</sup>  |
| $\frac{0.0}{10}$                   | $\frac{3.5}{5.5}$  |                   | $\frac{4.6}{0}$    |                   | $\frac{4.8}{10}$   |                   |                  |
| 67 <sup>2</sup>                    | 64 <sup>2</sup>    |                   | 63 <sup>3</sup>    |                   | 63 <sup>1</sup>    |                   |                  |
| $\frac{0.7}{10}$                   |                    | $\frac{4.8}{3}$   | $\frac{5.3}{0}$    |                   | $\frac{5.7}{5}$    | $\frac{5.6}{10}$  |                  |
| 67 <sup>2</sup>                    |                    | 63 <sup>1</sup>   | 62 <sup>6</sup>    |                   | 62 <sup>3</sup>    | 62 <sup>3</sup>   |                  |

Top of 2x2 @ D-2040 on Axis line

✓

⑨

11-Aug. 1952

Sta. +  $\pi$  - Elev.

2067.90

L-1030 ✓

L-1040 ✓

L-1050 ✓

Page 6 for party

⑨

West

(2067.90)

East

|                |                  |                 |                 |                 |                  |
|----------------|------------------|-----------------|-----------------|-----------------|------------------|
| <del>2.9</del> | $\frac{2.9}{10}$ | $\frac{6.7}{2}$ | $\frac{7.0}{0}$ | $\frac{7.3}{5}$ | $\frac{7.7}{10}$ |
|                | 65 <sup>0</sup>  | 61 <sup>2</sup> | 60 <sup>0</sup> | 60 <sup>6</sup> | 60 <sup>2</sup>  |

|                  |                 |                 |                 |                   |
|------------------|-----------------|-----------------|-----------------|-------------------|
| $\frac{5.3}{10}$ | $\frac{7.9}{4}$ | $\frac{8.5}{0}$ | $\frac{9.4}{5}$ | $\frac{10.0}{10}$ |
| 62 <sup>6</sup>  | 60 <sup>0</sup> | 59 <sup>1</sup> | 58 <sup>5</sup> | 57 <sup>2</sup>   |

|                  |                   |                  |                  |                   |
|------------------|-------------------|------------------|------------------|-------------------|
| $\frac{7.9}{10}$ | $\frac{9.4}{4.5}$ | $\frac{10.4}{0}$ | $\frac{11.6}{5}$ | $\frac{11.7}{10}$ |
| 60 <sup>0</sup>  | 58 <sup>5</sup>   | 57 <sup>5</sup>  | 56 <sup>3</sup>  | 56 <sup>2</sup>   |

✓

⑩ 11-August 1952 page 6 for party.

| Sta. | +    | ∩       | - | Elev.   |
|------|------|---------|---|---------|
| D    | 2101 | 2078.25 |   | 2076.24 |

D-2100

D-2110

D  
2120

D-2130

⑩ Non-excavated Sections between  
D-2100 & D-2130 & L-1000 = ~~L~~ = 0

2x2 hub on Axis line @ D-2100  
(2078.25)

| South             |                   |                  |                  |                 |                 |                  | North           |                  |
|-------------------|-------------------|------------------|------------------|-----------------|-----------------|------------------|-----------------|------------------|
| $\frac{16.7}{50}$ | $\frac{11.9}{34}$ | $\frac{8.6}{22}$ | $\frac{5.8}{12}$ | $\frac{4.3}{7}$ | $\frac{2.5}{3}$ | $\frac{-2.3}{0}$ | $\frac{2.0}{1}$ | $\frac{2.1}{15}$ |

|                   |                   |                  |                  |                  |                 |                  |                  |                   |
|-------------------|-------------------|------------------|------------------|------------------|-----------------|------------------|------------------|-------------------|
| $\frac{14.0}{50}$ | $\frac{11.8}{40}$ | $\frac{8.6}{30}$ | $\frac{5.5}{17}$ | $\frac{3.6}{12}$ | $\frac{1.7}{0}$ | $\frac{-1.0}{3}$ | $\frac{+1.7}{5}$ | $\frac{+5.7}{15}$ |
|-------------------|-------------------|------------------|------------------|------------------|-----------------|------------------|------------------|-------------------|

|                   |                  |                  |                  |                  |                          |                  |                   |                   |
|-------------------|------------------|------------------|------------------|------------------|--------------------------|------------------|-------------------|-------------------|
| $\frac{11.3}{50}$ | $\frac{9.1}{40}$ | $\frac{5.8}{30}$ | $\frac{4.8}{24}$ | $\frac{2.4}{20}$ | $\frac{1.8+1.8+3.9}{14}$ | $\frac{+3.9}{0}$ | $\frac{+7.7}{10}$ | $\frac{+7.8}{15}$ |
|-------------------|------------------|------------------|------------------|------------------|--------------------------|------------------|-------------------|-------------------|

|                  |                  |                  |                  |                  |                   |                  |                  |                  |                   |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|-------------------|
| $\frac{6.4}{50}$ | $\frac{5.7}{45}$ | $\frac{2.7}{37}$ | $\frac{1.9}{20}$ | $\frac{0.8}{12}$ | $\frac{+1.8}{10}$ | $\frac{+4.5}{4}$ | $\frac{+5.0}{0}$ | $\frac{+8.5}{8}$ | $\frac{+8.0}{15}$ |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|-------------------|

⑪ 11-Aug, 1952 Page 6 for party.

Sta. +  $\pi$  - Elev.

H 6.25 2025.76 2019.51

L-980

L-990

L-1000

L-1010

L-1020

L-1030

L-1035 same as L-1040

L-1040

6.26 2019.50 (2019.51)

X-Sections for #3 Buttress = D-1180 # ⑪  
R Buttress = 0

|   | West  |                           |                           | East                      |                           |                           |
|---|---|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
|   | T.B.M. Top of big rock @ D-1180 @ L 1000<br>(2025.76) |                           |                           |                           |                           |                           |
| ✓ | $\frac{8.5}{10}$<br>17.2                              | $\frac{7.6}{5.5}$<br>18.1 | $\frac{7.1}{0}$<br>18.6   | $\frac{5.6}{5}$<br>20.1   | $\frac{1.8}{12}$<br>23.9  |                           |
| ✓ | $\frac{8.0}{10}$<br>17.7                              | $\frac{7.9}{5}$<br>17.8   | $\frac{7.6}{0}$<br>18.2   | $\frac{6.4}{2.0}$<br>19.3 | $\frac{4.7}{8}$<br>21.0   | $\frac{+0.5}{14}$<br>26.2 |
| ✓ | $\frac{7.7}{10}$<br>18.1                              | $\frac{7.6}{5}$<br>18.2   | $\frac{7.7}{0}$<br>18.1   | $\frac{7.2}{4}$<br>18.6   | $\frac{3.3}{9.5}$<br>22.5 | $\frac{+1.8}{15}$<br>27.6 |
| ✓ | $\frac{6.7}{10}$<br>19.1                              | $\frac{7.4}{4}$<br>18.4   | $\frac{7.2}{0}$<br>18.6   | $\frac{6.7}{4}$<br>19.1   | $\frac{3.0}{10}$<br>22.8  | $\frac{1.8}{15}$<br>24.0  |
| ✓ |   | $\frac{5.4}{10}$<br>20.4  | $\frac{7.0}{3}$<br>18.8   | $\frac{7.1}{0}$<br>18.7   | $\frac{4.8}{6}$<br>21.0   | $\frac{+1.4}{14}$<br>25.8 |
| ✓ | $\frac{4.5}{10}$<br>21.3                              | $\frac{6.2}{5}$<br>19.6   | $\frac{7.7}{2.5}$<br>18.1 | $\frac{7.5}{0}$<br>18.3   | $\frac{5.5}{3.5}$<br>20.3 | $\frac{1.0}{10}$<br>24.8  |
| ✓ |   | $\frac{5.0}{10}$<br>20.8  | $\frac{4.7}{6}$<br>21.1   | $\frac{4.8}{0}$<br>21.0   | $\frac{3.5}{7}$<br>22.3   | $\frac{+4.0}{16}$<br>29.8 |

Continue to L-1090

Continued on page 12

⑫ 12 - Aug. 1952  
Sta. +      - Elev.

□ 6.29 2025.80 2019.51

L-1050

L-1060

L-1070

L-1080

L-1090

□ 6.29 2019.51 2019.51

Dallas - ~~□~~  
Stanley - ~~□~~  
Curley - ~~□~~ Tape  
Clyde - ~~□~~ Tape & Axe

Continued from page 11 ⑫

T.B.M. Top of big rock @ D-1180 & L-1000  
West East

(2025.80)

|                  |                 |                 |                 |                 |                   |
|------------------|-----------------|-----------------|-----------------|-----------------|-------------------|
| $\frac{5.0}{10}$ | $\frac{5.1}{5}$ | $\frac{5.0}{0}$ | $\frac{4.6}{3}$ | $\frac{2.2}{8}$ | $\frac{+3.5}{15}$ |
| 20.8             | 20.1            | 20.8            | 21.2            | 23.6            | 29.3              |

|                  |                 |                 |                 |                 |                  |                   |
|------------------|-----------------|-----------------|-----------------|-----------------|------------------|-------------------|
| $\frac{5.3}{10}$ | $\frac{4.4}{7}$ | $\frac{4.6}{4}$ | $\frac{4.1}{0}$ | $\frac{2.9}{4}$ | $\frac{+0.3}{8}$ | $\frac{+2.1}{14}$ |
| 20.5             | 21.4            | 21.2            | 21.7            | 22.9            | 26.1             | 27.9              |

|                  |                   |                   |                 |                   |                     |
|------------------|-------------------|-------------------|-----------------|-------------------|---------------------|
| $\frac{6.5}{10}$ | $\frac{5.0}{5.5}$ | $\frac{3.4}{2.5}$ | $\frac{2.9}{0}$ | $\frac{1.2}{6.5}$ | $\frac{+1.0}{12.5}$ |
| 19.3             | 20.8              | 22.4              | 22.9            | 24.6              | 26.8                |

|  |                  |                   |                 |                 |                   |                 |                  |
|--|------------------|-------------------|-----------------|-----------------|-------------------|-----------------|------------------|
| <del><math>\frac{3.8}{10}</math></del> | $\frac{7.8}{10}$ | $\frac{7.1}{6.5}$ | $\frac{5.0}{2}$ | $\frac{3.8}{0}$ | $\frac{2.0}{2.5}$ | $\frac{2.2}{2}$ | $\frac{1.1}{10}$ |
|  | 18.0             | 18.7              | 20.8            | 22.0            | 22.8              | 23.6            | 24.7             |

|                  |                 |                 |                 |                  |
|------------------|-----------------|-----------------|-----------------|------------------|
| $\frac{9.9}{10}$ | $\frac{8.5}{6}$ | $\frac{5.8}{0}$ | $\frac{2.0}{5}$ | $\frac{1.1}{11}$ |
| 15.9             | 17.3            | 20.0            | 23.2            | 24.7             |

Top of rock @ D-1180 & L-1000

⑬

12-Aug. 1952 Page 12 for party.

| Sta. | +    | -  | Elev.  |
|------|------|--|--|
| D    | 0.67 | 2063.41                                  | 2062.74  |
| T.P. | 1.51 | <del>2053.23</del><br><del>2053.09</del> | <del>11.59</del><br><del>2051.85</del><br><del>2052.03</del> |
| T.P. | 2.10 | <del>2047.63</del> <sup>37</sup>         | <del>8.07</del> <sup>06</sup><br><del>2045.52</del> 2045.27  |

L-980

L-990

L-1000

L-1005

L-1007 same as L-1010

L-1010

L-1013

X- Sections for #2 Buttress = D-1120 R  
R of Buttress = 0

⑬

| West  |                   |                 | East                    |                   |                   |
|---|-------------------|-----------------|-------------------------|-------------------|-------------------|
| T.B.M. Top of Sta. on Axis @ D-1071.41                      |                   |                 |                         |                   |                   |
| 1X2 Hub on Axis @ D-1100 ±                                  |                   |                 |                         |                   |                   |
| 2x2 Tack on Axis line @ R # Buttress = D-1120 <sup>00</sup> |                   |                 |                         |                   |                   |
| (2047.57) <sup>37</sup>                                     |                   |                 | (2053.59) <sup>37</sup> |                   |                   |
| $\frac{7.9}{10}$  | $\frac{11.9}{5}$  | $\frac{9.9}{0}$ | $\frac{8.2}{5}$         | $\frac{6.4}{10}$  |                   |
| 39.5  | 41.4              | 43.4            | 45.1                    | 46.9              |                   |
| $\frac{6.7}{10}$  | $\frac{4.8}{5}$   | $\frac{3.3}{0}$ | $\frac{6.6}{7}$         | $\frac{5.2}{10}$  |                   |
| 40.6  | 42.5              | 44.0            | 46.7                    | 48.1              |                   |
| $\frac{6.2}{10}$  | $\frac{5.0}{7.5}$ | $\frac{2.6}{0}$ | $\frac{6.7}{4}$         | $\frac{4.8}{10}$  |                   |
| 41.1  | 42.3              | 44.7            | 46.6                    | 48.5              |                   |
| $\frac{5.4}{10}$  |                   | $\frac{2.3}{0}$ | $\frac{6.4}{5}$         | $\frac{4.7}{10}$  |                   |
| 41.9  |                   | 45.0            | 46.9                    | 48.6              |                   |
|   | $\frac{4.2}{10}$  | $\frac{4.0}{0}$ | $\frac{8.8}{3.5}$       | $\frac{5.6}{6.5}$ | $\frac{4.4}{10}$  |
|   | 43.1              | 43.3            | 44.5                    | 47.7              | 48.9              |
| $\frac{4.1}{10}$  | $\frac{4.1}{3.5}$ | $\frac{8.9}{2}$ | $\frac{9.1}{0}$         | $\frac{6.4}{3.7}$ | $\frac{6.2}{5.2}$ |
| 43.2  | 43.2              | 38.4            | 38.2                    | 40.9              | 47.1              |
|   |                   |                 |                         |                   | $\frac{4.4}{10}$  |
|   |                   |                 |                         |                   | 48.9              |

33-44-3



(74) 12-Aug-'52 Page 13 for party  
Sta + \* - Elev.

L-1020

L-1022 = Same as L-1020

<sup>33</sup>  
2053.59

8.06 2045.53

L-1024

<sup>37</sup>  
2047.62 2.10 20

L-1028 = Same as L-1024

2.10 2045.53

Check

L-1030

L-1040

L-1050

L-1060

L-1070

11.08 <sup>33</sup>  
2053.59  
2062.91  
2063.17 1.50

2051.83  
2052.09

L-1080

0.1

0.17

2062.74 2062.74

(<sup>37</sup>  
2047.62)

West

|                  |                   |                  |                 |                 |
|------------------|-------------------|------------------|-----------------|-----------------|
| $\frac{4.2}{10}$ | $\frac{4.0}{3.5}$ | $\frac{10.4}{2}$ | $\frac{7.9}{0}$ | $\frac{9.3}{2}$ |
| 43.1             | 43.3              | 36.9             | 37.4            | 38.0            |

|                  |                 |                 |                   |
|------------------|-----------------|-----------------|-------------------|
| $\frac{4.3}{10}$ | $\frac{3.8}{5}$ | $\frac{3.8}{0}$ | $\frac{3.4}{2.3}$ |
| 43.0             | 43.5            | 43.5            | 43.9              |

(<sup>33</sup>  
2053.59) (~~2047.62~~)

|                     |                    |                    |                    |                    |
|---------------------|--------------------|--------------------|--------------------|--------------------|
| $\frac{42.1}{10.6}$ | $\frac{44.1}{9.2}$ | $\frac{45.9}{7.4}$ | $\frac{47.3}{6.0}$ | $\frac{48.8}{4.5}$ |
| 10                  | 4.7                | 0                  | 5                  | 10                 |

|                     |                    |                    |                    |                    |
|---------------------|--------------------|--------------------|--------------------|--------------------|
| $\frac{42.1}{11.2}$ | $\frac{43.8}{9.5}$ | $\frac{45.3}{8.0}$ | $\frac{47.3}{6.1}$ | $\frac{48.8}{3.5}$ |
| 10                  | 5                  | 0                  | 5                  | 10                 |

|                     |                    |                    |                    |                    |
|---------------------|--------------------|--------------------|--------------------|--------------------|
| $\frac{41.7}{11.6}$ | $\frac{43.8}{9.5}$ | $\frac{45.3}{7.9}$ | $\frac{47.3}{7.2}$ | $\frac{48.8}{5.5}$ |
| 10                  | 4.2                | 0                  | 2.2                | 5                  |

|                    |                    |                    |                    |                    |
|--------------------|--------------------|--------------------|--------------------|--------------------|
| $\frac{40.7}{6.7}$ | $\frac{42.2}{5.3}$ | $\frac{44.4}{2.9}$ | $\frac{46.2}{7.1}$ | $\frac{47.4}{5.9}$ |
| 10                 | 5                  | 0                  | 4.5                | 10                 |

|                    |                    |                     |                    |                    |
|--------------------|--------------------|---------------------|--------------------|--------------------|
| $\frac{39.1}{8.3}$ | $\frac{40.9}{6.5}$ | $\frac{42.5}{10.8}$ | $\frac{44.7}{8.6}$ | $\frac{45.5}{7.8}$ |
| 10                 | 4.5                | 0                   | 6                  | 10                 |

|                     |                    |                    |                    |                     |
|---------------------|--------------------|--------------------|--------------------|---------------------|
| $\frac{37.2}{10.1}$ | $\frac{38.7}{8.6}$ | $\frac{40.0}{7.3}$ | $\frac{41.3}{6.0}$ | $\frac{43.0}{10.3}$ |
| 10                  | 5                  | 0                  | 4                  | 10                  |

(<sup>33</sup>  
2053.59) (14)

East

|                   |                   |                  |
|-------------------|-------------------|------------------|
| $\frac{5.7}{6.3}$ | $\frac{5.2}{7.5}$ | $\frac{4.2}{10}$ |
| 43.6              | 42.1              | 43.1             |

|                 |                  |
|-----------------|------------------|
| $\frac{5.5}{6}$ | $\frac{4.3}{10}$ |
| 47.8            | 49.0             |

48.1 49.1

(15) 12-Aug. 1952 Page 13 for party

| Sta.  | +    | ⌈       | - | Elev.   |
|-------|------|---------|---|---------|
| III   | 3.27 | 2066.01 |   | 2062.74 |
| L-980 |      |         |   |         |

L-990

L-1000

L-1003

L-1010

L-1012.5 = same as L-1010

L-1014

L-1020

L-1022

X-Sections for #1 Buttress = D-1060 &

\* of Buttress = 0

West

East

| (2066.01)        |                   |                   |                   |                   |                   |                   |                   |                  |
|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|------------------|
| $\frac{6.1}{10}$ | $\frac{4.5}{5}$   | $\frac{2.8}{0}$   | $\frac{2.7}{1.4}$ | $\frac{11.5}{10}$ |                   |                   |                   |                  |
|                  |                   | 63.2              |                   |                   |                   |                   |                   |                  |
| $\frac{5.4}{10}$ | $\frac{4.1}{6.5}$ | $\frac{2.3}{0}$   | $\frac{2.9}{1}$   | $\frac{11.3}{10}$ |                   |                   |                   |                  |
| 60.6             | 61.9              | 63.7              | 63.1              | 54.7              |                   |                   |                   |                  |
| $\frac{3.4}{10}$ | $\frac{3.6}{8}$   | $\frac{5.2}{4}$   | $\frac{5.8}{0}$   | $\frac{5.7}{2}$   | $\frac{10.8}{10}$ |                   |                   |                  |
| 62.6             | 62.4              | 60.8              | 60.2              | 60.3              | 55.2              |                   |                   |                  |
| $\frac{3.0}{10}$ | $\frac{5.6}{3}$   | $\frac{8.3}{1.5}$ | $\frac{8.3}{0}$   | $\frac{8.3}{2}$   | $\frac{10.7}{10}$ |                   |                   |                  |
| 63.01            | 60.4              | 57.7              | 57.7              | 57.7              | 55.3              |                   |                   |                  |
| $\frac{3.3}{10}$ | $\frac{5.9}{5.5}$ | $\frac{8.4}{1.5}$ | $\frac{8.4}{0}$   | $\frac{8.4}{2}$   | $\frac{8.0}{3.5}$ | $\frac{5.6}{4.5}$ | $\frac{5.6}{5.5}$ | $\frac{9.2}{10}$ |
| 62.7             | 60.1              | 57.6              | 57.6              | 57.6              | 58.0              | 60.9              | 60.4              | 56.8             |
| $\frac{2.0}{10}$ | $\frac{3.5}{8.5}$ | $\frac{5.4}{6}$   | $\frac{5.6}{0}$   |                   | $\frac{5.1}{5}$   |                   | $\frac{9.2}{10}$  |                  |
| 63.01            | 62.5              | 60.6              | 60.9              |                   | 60.9              |                   | 56.8              |                  |
| $\frac{2.9}{10}$ | $\frac{3.0}{7.5}$ | $\frac{3.9}{6}$   | $\frac{3.9}{0}$   | $\frac{3.7}{5.5}$ | $\frac{8.6}{10}$  |                   |                   |                  |
| 63.1             | 63.               | 62.1              | 62.1              | 62.3              | 57.8              |                   |                   |                  |
| $\frac{2.9}{10}$ | $\frac{1.8}{4}$   | $\frac{1.2}{0}$   | $\frac{2.0}{4.5}$ | $\frac{8.6}{10}$  |                   |                   |                   |                  |
| 63.1             | 64.2              | 64.8              | 64.               | 57.4              |                   |                   |                   |                  |

⑩ 12-Aug. '52 Page 13 for party

| Sta    | + | +       | - | Elev |
|--------|---|---------|---|------|
| L-1030 |   | 2066.01 |   |      |

L-1038

|   |  |      |         |         |
|---|--|------|---------|---------|
| □ |  | 3.27 | 2062.74 | 2062.74 |
|---|--|------|---------|---------|

|   |      |         |         |  |
|---|------|---------|---------|--|
| □ | 5.61 | 2056.21 | 2050.60 |  |
|---|------|---------|---------|--|

L-1050

L-1060

⑩

West (2066.01)

| West             | West            | West            | West            | West            | East             |
|------------------|-----------------|-----------------|-----------------|-----------------|------------------|
| $\frac{3.8}{10}$ | $\frac{2.7}{7}$ | $\frac{1.3}{4}$ | $\frac{1.0}{0}$ | $\frac{1.0}{5}$ | $\frac{6.8}{10}$ |
| 62.2             | 63.9            | 64.7            | 2065.0          | 65.0            | 59.7             |

|                  |                 |                 |                 |                  |
|------------------|-----------------|-----------------|-----------------|------------------|
| $\frac{5.7}{10}$ | $\frac{4.7}{6}$ | $\frac{3.2}{0}$ | $\frac{2.7}{4}$ | $\frac{6.7}{10}$ |
| 60.3             | 61.8            | 62.8            | 63.8            | 59.3             |

2x2 @ D-1071  $\frac{1}{4}$  on Axis

2x2 Hub @ D-1000 on Axis

(2056.21)

|                  |                 |                  |
|------------------|-----------------|------------------|
| $\frac{4.5}{10}$ | $\frac{3.8}{0}$ | $\frac{3.1}{10}$ |
| 51.7             | 52.9            | 53.1             |

|                  |                 |                  |
|------------------|-----------------|------------------|
| $\frac{5.8}{10}$ | $\frac{5.7}{0}$ | $\frac{5.3}{10}$ |
| 50.4             | 50.5            | 50.9             |

(17) 12-Aug, 1952 Page 13 for party

| Sta.                   | +    | $\Delta$ | -     | Elev.   |
|------------------------|------|----------|-------|---------|
|                        |      | 2056.21  |       |         |
| 100 <sup>-</sup> South |      |          |       |         |
| 90 <sup>-</sup> S      |      |          | 10.9  |         |
| 90 <sup>-</sup> So     |      |          | 9.3   |         |
| 77 So                  |      |          | 6.7   |         |
| 42 So                  |      |          | 3.5   |         |
| 23 So                  |      |          | 4.8   |         |
| 0                      |      |          | 6.1   |         |
| 10 North               |      |          | 7.0   |         |
| 19 No.                 |      |          | 5.9   |         |
| 25 "                   |      |          | 8.0   |         |
| 38                     |      |          | 10.3  |         |
| 58                     |      |          | 11.6  |         |
| 74                     |      |          | 12.5  |         |
| T.P.                   | 0.65 | 2044.97  | 11.89 | 2044.32 |

|                        |      |         |       |         |
|------------------------|------|---------|-------|---------|
| 100 <sup>-</sup> South |      |         | 4.4   |         |
| 118 <sup>-</sup> "     |      |         | 6.2   |         |
| 136 "                  |      |         | 8.7   |         |
| 150 "                  |      |         | 9.5   |         |
| 175 "                  |      |         | 11.3  |         |
| T.P.                   | 1.05 | 2033.85 | 12.17 | 2032.80 |
| 200 No.                |      |         | 4.0   |         |
| 225 "                  |      |         | 7.3   |         |
| 250 "                  |      |         | 10.4  |         |
| 287 "                  |      |         | 11.0  |         |
| 300 North              |      |         | 10.8  |         |

Profile of D-1000 @ L-1000 = 0  
SPILLWAY

(17)

0 = D-1000 @ L-1000

Top of rock pile @ L-923<sup>±</sup> @ D-1000

Top of rock @ L-818 @ D-1000

(18)

12-Aug, 1952

| Sta  | +     | -    | Elev                  |
|------|-------|------|-----------------------|
|      |       |      | 2032.85               |
|      |       |      | <del>2045.82</del>    |
|      |       |      | <del>2044.02</del>    |
| T.P. | 12.52 | 0.35 | 2033.50               |
|      |       |      | 2045.79 <sup>89</sup> |
|      |       |      | <del>2048.79</del>    |
| T.P. | 10.60 | 0.23 | 2050.58               |
|      |       |      | <del>2048.78</del>    |
| □    |       | 5.61 | 2050.60               |

Page 13 for party.

(18)

Continued from page 1

Rock @ D-1003 &amp; L-822

Hub @ D-1000 &amp; L-1000

19

Ring # 6-7 = D 1360 - 1420  
X-Sections

Sta. +  $\Delta$  - Elev.

T.P. 0.40 1954.66 1954.26

D-1370

D-1380

T.P. 0.55 1943.40 11.81 1942.85

D-1390

D-1400

T.P. 4.36 1935.64 12.12 1931.28

D-1410

D-1420

10.21 1925.43 (1925.43)

Base line for 0 = L-1166.80

15-Aug, 1952

Dallas -  $\boxplus$   
Stanley -  $\boxtimes$   
Dave -  $\boxplus$  Tape  
Curley -  $\boxplus$  Tape  
Clyde -  $\boxplus$  Tape

South

Rock @ D-1361 @ L-1158

(1954.66)

$\frac{4.1}{0} \frac{3.7}{13} \frac{5.4}{17} \frac{4.2}{22} \frac{7.8}{30.5} \frac{7.3}{37.5} \frac{5.1}{42} \frac{4.4}{50}$

$\frac{10.4}{0} \frac{8.0}{10} \frac{17.2}{14.5} \frac{14.5}{20.5} \frac{4.3}{27} \frac{3.2}{33}$

Rock @ D-1386 @ L-1164

(1954.66)

$\frac{4.4}{7} \frac{3.5}{0} \frac{3.5}{4} \frac{5.0}{2.5} \frac{12.8}{8} \frac{8.3}{18} \frac{2.8}{19.5} \frac{+1.3}{21.5} \frac{+4.0}{24.5} \frac{+6.8}{32}$

(1943.40)

$\frac{8.8}{7} \frac{8.5}{0} \frac{18.3}{2.5} \frac{18.4}{8} \frac{11.5}{12} \frac{8.8}{17} \frac{3.4}{19} \frac{+0.5}{26} \frac{+1.4}{27} \frac{4.0}{33} \frac{4.0}{36} \frac{1.9}{41}$

Rock @ D-1415 @ L-1180

(1935.64)

$\frac{4.3}{9} \frac{4.5}{0} \frac{7.3}{6} \frac{14.6}{8} \frac{14.6}{17.5} \frac{8.6}{17.5} \frac{2.8}{28}$

(1935.64)

$\frac{6.3}{10} \frac{6.6}{1} \frac{0}{0} \frac{11.3}{6}$

Check on bar pipe in Ring #9-10 16' S.E. of Buttress #10

20

BOTTRESS # 7  
D-1420

| STA | +    | -       | ELEV    |
|-----|------|---------|---------|
| TBM | 3.37 | 1928.07 | 1924.70 |

L 1030

L 1020

L 1010

L 1006.4

L 1003

L 1000

L 992

L 990

L 980

L 970

L 960

8-4-52

#7

EAST

WEST

(1928.07)

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 8.0  | 9.6  | 9.4  | 8.1  | 7.1  | 4.6  | 3.0  | 2.8  |
| 2.7  | 4.3  | 0    | 9    | 12   | 7.4  | 17   | 20   |
| 20.1 | 18.5 | 18.7 | 20.0 | 21.0 | 23.5 | 25.1 | 25.3 |

(1928.07)

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 6.3  | 9.5  | 9.5  | 8.4  | 7.1  | 4.5  | 2.4  | 2.4  |
| 8    | 4.6  | 0    | 7    | 10   | 13.3 | 17   | 20   |
| 21.8 | 18.6 | 18.6 | 19.7 | 21.0 | 24.6 | 25.7 | 25.7 |

(1928.07)

|      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|
| 7.2  | 8.5  | 9.0  | 9.5  | 9.2  | 7.1  | 4.0  | 2.6  |
| 8.6  | 7    | 5    | 0    | 6    | 10   | 14   | 20   |
| 20.9 | 19.8 | 19.1 | 18.6 | 18.9 | 21.0 | 24.1 | 25.5 |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 4.4  | 9.0  | 9.4  | 9.4  | 9.5  | 9.3  | 8.9  | 5.6  | 2.8  |
| 9.2  | 6.0  | 5    | 0    | 4    | 4.5  | 7    | 13   | 20   |
| 23.7 | 19.1 | 18.5 | 18.7 | 18.5 | 18.8 | 19.2 | 22.5 | 27.3 |

|      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 9.5  | 10.2 | 11.4 | 11.3 | 10.8 | 11.0 | 10.2 | 8.6  | 5.7  | 4.2  | 3.1  | 3.1  |
| 8.6  | 6.1  | 3.7  | 2.1  | 0    | 5    | 8    | 9    | 14   | 18   | 18.5 | 20   |
| 18.6 | 17.9 | 16.7 | 16.8 | 17.3 | 17.1 | 17.9 | 19.5 | 22.4 | 23.9 | 25.0 | 25.0 |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 9.6  | 10.8 | 10.8 | 10.9 | 10.0 | 6.7  | 3.4  |
| 9.7  | 5    | 0    | 8    | 12   | 15   | 20   |
| 18.5 | 17.3 | 17.3 | 17.2 | 18.1 | 21.4 | 24.7 |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 9.3  | 11.0 | 10.7 | 10.5 | 10.0 | 8.3  | 3.9  |
| 9    | 4.4  | 0    | 6.5  | 10.5 | 13   | 20   |
| 18.8 | 17.1 | 17.4 | 17.6 | 18.1 | 19.8 | 24.2 |

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 9.0  | 11.1 | 10.6 | 10.5 | 5.7  | 3.9  |
| 6    | 4    | 0    | 5    | 13   | 20   |
| 19.1 | 17.0 | 17.5 | 17.6 | 22.4 | 24.2 |

|      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|
| 8.3  | 10.3 | 11.1 | 10.6 | 10.3 | 10.3 | 9.6  | 7.4  | 4.4  | 4.8  |
| 7.6  | 4.6  | 4    | 2    | 0    | 4    | 7    | 12   | 19   | 20   |
| 19.8 | 17.8 | 17.0 | 17.5 | 17.8 | 17.8 | 18.5 | 20.5 | 23.7 | 23.3 |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 9.3  | 11.1 | 11.3 | 10.1 | 10.5 | 10.2 | 8.1  | 5.5  | 6.7  |
| 5.8  | 4    | 3    | 0    | 2    | 5    | 12   | 18   | 20   |
| 18.8 | 17.0 | 16.8 | 18.0 | 17.6 | 17.9 | 20.0 | 22.6 | 21.4 |

|      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|
| 9.3  | 10.9 | 10.7 | 10.9 | 10.3 | 10.1 | 8.0  | 6.6  | 9.5  |
| 7.5  | 3    | 0    | 4    | 6    | 8    | 13   | 15   | 20   |
| 18.8 | 17.2 | 17.4 | 17.2 | 17.8 | 18.0 | 20.1 | 21.5 | 18.6 |

✓

(21)

## BUTTRESS # 7 (CONT)

L 950

L 940

L 1150

L 1140

L 1130

L 1120

L 1110

L 1100

L 1090

L 1080

L 1070

L 1065<sup>8</sup>

|                     | EAST                |  |                   |  |                    |  |                   |  |                   |  | (1928.07)          |  |                    |  |                    |  |      |  |      |  | WEST |  |      |  |      |  |      |  |      |  |      |  |      |  |      |  |      |  |
|---------------------|---------------------|--|-------------------|--|--------------------|--|-------------------|--|-------------------|--|--------------------|--|--------------------|--|--------------------|--|------|--|------|--|------|--|------|--|------|--|------|--|------|--|------|--|------|--|------|--|------|--|
| L 950               | $\frac{6.7}{10}$    |  | $\frac{9.0}{4.7}$ |  | $\frac{10.7}{0}$   |  | $\frac{10.8}{6}$  |  | $\frac{9.9}{8}$   |  | $\frac{10.1}{12}$  |  | $\frac{9.4}{15}$   |  | $\frac{9.6}{20}$   |  | 21.4 |  | 19.1 |  | 17.4 |  | 17.3 |  | 18.2 |  | 18.0 |  | 18.7 |  | 18.5 |  |      |  |      |  |      |  |
| L 940               |                     |  |                   |  | $\frac{8.7}{0}$    |  | $\frac{10.8}{10}$ |  | $\frac{11.3}{13}$ |  | $\frac{11.3}{20}$  |  |                    |  |                    |  | 19.4 |  | 17.3 |  | 16.8 |  | 16.8 |  |      |  |      |  |      |  |      |  |      |  |      |  |      |  |
| L 1150              | $\frac{7.3}{11.7}$  |  | $\frac{7.7}{5.5}$ |  | $\frac{7.9}{0}$    |  | $\frac{7.2}{6}$   |  | $\frac{6.4}{8}$   |  | $\frac{3.8}{10.5}$ |  | $\frac{4.1}{17.5}$ |  | $\frac{5.1}{20}$   |  | 20.8 |  | 20.2 |  | 20.2 |  | 20.9 |  | 21.7 |  | 24.3 |  | 24.8 |  | 23.0 |  |      |  |      |  |      |  |
| L 1140              | $\frac{6.2}{11}$    |  | $\frac{7.0}{6.3}$ |  | $\frac{7.3}{0}$    |  | $\frac{6.7}{5}$   |  | $\frac{2.1}{11}$  |  | $\frac{1.5}{15}$   |  | $\frac{5.9}{20}$   |  |                    |  | 21.9 |  | 21.1 |  | 20.8 |  | 21.4 |  | 26.0 |  | 26.6 |  | 22.2 |  |      |  |      |  |      |  |      |  |
| L 1130              | $\frac{1.4}{11.0}$  |  | $\frac{4.6}{7.3}$ |  | $\frac{6.9}{3.4}$  |  | $\frac{7.1}{0}$   |  | $\frac{7.1}{5}$   |  | $\frac{2.5}{8.5}$  |  | $\frac{2.0}{10}$   |  | $\frac{2.0}{16}$   |  | 26.7 |  | 23.5 |  | 21.2 |  | 21.0 |  | 21.0 |  | 25.6 |  | 26.1 |  | 26.1 |  | 22.7 |  |      |  |      |  |
| L 1120              | $\frac{+1.3}{13.6}$ |  | $\frac{0.0}{12}$  |  | $\frac{1.8}{70.5}$ |  | $\frac{4.1}{6.6}$ |  | $\frac{6.6}{6}$   |  | $\frac{6.8}{3.6}$  |  | $\frac{7.0}{0}$    |  | $\frac{1.6}{10.5}$ |  | 29.4 |  | 28.1 |  | 26.3 |  | 24.0 |  | 21.5 |  | 21.3 |  | 21.1 |  | 27.3 |  | 25.3 |  | 26.5 |  | 24.0 |  |
| L 1110              | $\frac{3.4}{10.6}$  |  | $\frac{3.5}{8.3}$ |  | $\frac{5.4}{7.7}$  |  | $\frac{6.8}{4}$   |  | $\frac{7.0}{0}$   |  | $\frac{7.1}{4.5}$  |  | $\frac{5.3}{10}$   |  | $\frac{3.5}{11.5}$ |  | 24.7 |  | 24.6 |  | 22.7 |  | 21.3 |  | 21.1 |  | 21.0 |  | 22.8 |  | 24.6 |  | 24.9 |  | 27.1 |  | 25.4 |  |
| L 1100              | $\frac{3.1}{10.2}$  |  | $\frac{5.1}{8.5}$ |  | $\frac{6.1}{5.7}$  |  | $\frac{6.6}{3.7}$ |  | $\frac{6.9}{0}$   |  | $\frac{7.1}{5}$    |  | $\frac{3.5}{9}$    |  | $\frac{3.4}{13}$   |  | 25.0 |  | 23.0 |  | 22.0 |  | 21.5 |  | 21.2 |  | 21.0 |  | 24.6 |  | 24.7 |  | 26.4 |  | 24.7 |  |      |  |
| L 1090              | $\frac{3.5}{10}$    |  | $\frac{5.1}{8.5}$ |  | $\frac{6.2}{6.8}$  |  | $\frac{7.0}{0}$   |  | $\frac{6.6}{6}$   |  | $\frac{4.2}{9}$    |  | $\frac{3.8}{11}$   |  | $\frac{3.1}{13}$   |  | 24.6 |  | 23.0 |  | 21.9 |  | 21.1 |  | 21.5 |  | 23.9 |  | 24.3 |  | 25.0 |  | 26.4 |  | 24.6 |  |      |  |
| L 1080              | $\frac{1.0}{10.2}$  |  | $\frac{3.2}{6}$   |  | $\frac{6.5}{4}$    |  | $\frac{7.1}{0}$   |  | $\frac{7.1}{4}$   |  | $\frac{6.1}{7}$    |  | $\frac{4.1}{11}$   |  | $\frac{3.9}{16}$   |  | 27.1 |  | 24.9 |  | 21.6 |  | 21.0 |  | 21.0 |  | 22.0 |  | 24.0 |  | 24.2 |  | 22.5 |  |      |  |      |  |
| L 1070              | $\frac{0.0}{11}$    |  | $\frac{1.4}{8.7}$ |  | $\frac{3.8}{6.7}$  |  | $\frac{5.5}{3.6}$ |  | $\frac{7.1}{3.5}$ |  | $\frac{7.0}{0}$    |  | $\frac{7.2}{5}$    |  | $\frac{4.5}{10}$   |  | 28.1 |  | 26.7 |  | 24.3 |  | 22.6 |  | 21.0 |  | 21.1 |  | 20.9 |  | 23.5 |  | 24.0 |  | 33.0 |  |      |  |
| L 1065 <sup>8</sup> | $\frac{0.5}{12.9}$  |  | $\frac{4.1}{8}$   |  | $\frac{7.3}{5}$    |  | $\frac{7.2}{0}$   |  | $\frac{7.2}{7}$   |  | $\frac{5.1}{9}$    |  | $\frac{2.8}{14}$   |  | $\frac{3.7}{20}$   |  | 27.6 |  | 24.0 |  | 20.8 |  | 20.9 |  | 20.9 |  | 23.0 |  | 25.3 |  | 24.4 |  |      |  |      |  |      |  |

✓



(22)

## BUTTRESS # 7 (CONT)

L1060

L1057

L1050

L1040

## ADDITIONAL SHOTS

|       |   |                     |            |
|-------|---|---------------------|------------|
| L1090 | x | $\frac{1.0}{11}$    | 1936.1     |
| L1080 | x | $\frac{3.6}{15}$    | 1937.5     |
| L1070 | x | $\frac{0.1}{18}$    | H1 1937.10 |
| L1060 | x | $\frac{2.7}{13.6}$  | 1937.0     |
| L1040 | x | $\frac{6.5}{11}$    | 1934.4     |
| L1030 | x | $\frac{6.8}{14.5}$  | 1931.7     |
| L1020 | x | $\frac{7.2}{13.5}$  | H1 1938.20 |
| L1010 | x | $\frac{1.7}{14.7}$  | 1931.84    |
| L1000 | x | $\frac{1.7}{14}$    | 1931.0     |
| L990  | x | $\frac{1.2}{14}$    | 1935.4     |
| L980  | x | $\frac{9.3}{15}$    | 1935.4     |
| L970  | x | $\frac{9.0}{18}$    | H1 1937.10 |
| L960  | x | $\frac{11.2}{11.5}$ | 1935.9     |
|       |   |                     | 1927.9     |
|       |   |                     | 1928.1     |
|       |   |                     | 1925.9     |

EAST

(1928.07)

WEST

|   |                    |                   |                   |                   |                 |                   |                   |                   |                   |                   |
|---|--------------------|-------------------|-------------------|-------------------|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| x | $\frac{3.7}{9}$    | $\frac{8.6}{6.4}$ | $\frac{9.5}{0}$   | $\frac{9.6}{4}$   | $\frac{9.0}{8}$ | $\frac{4.3}{1.3}$ | $\frac{4.0}{1.6}$ | $\frac{3.4}{1.8}$ | $\frac{3.5}{2.0}$ |                   |
|   | 24.4               | 19.5              | 18.6              | 18.5              | 19.1            | 23.8              | 24.1              | 24.7              | 24.6              |                   |
| x | $\frac{4.6}{10.6}$ | $\frac{9.7}{4.6}$ | same as           |                   | 1060            |                   |                   |                   |                   |                   |
|   | 23.5               | 18.4              |                   |                   |                 |                   |                   |                   |                   |                   |
| x | $\frac{5.5}{10.3}$ | $\frac{9.6}{3.8}$ | $\frac{9.3}{0}$   | $\frac{9.6}{8.5}$ | $\frac{8.9}{9}$ | $\frac{8.7}{11}$  | $\frac{6.2}{1.3}$ | $\frac{3.8}{1.9}$ | $\frac{3.6}{2.0}$ |                   |
|   | 22.6               | 18.5              | 18.8              | 18.5              | 19.2            | 19.4              | 21.9              | 24.3              | 24.5              |                   |
| x | $\frac{6.3}{7.7}$  | $\frac{8.9}{5.2}$ | $\frac{9.5}{3.6}$ | $\frac{9.6}{0}$   | $\frac{9.2}{3}$ | $\frac{7.1}{8}$   | $\frac{5.5}{1.2}$ | $\frac{4.0}{1.3}$ | $\frac{3.8}{1.9}$ | $\frac{4.3}{2.0}$ |
|   | 21.8               | 19.2              | 18.6              | 18.5              | 18.9            | 21.0              | 22.5              | 24.1              | 24.3              | 23.8              |

|       |   |                      |            |
|-------|---|----------------------|------------|
| L1130 | x | $\frac{3.6}{13}$     | 1937.3     |
| L1120 | x | $\frac{2.2}{17.6}$   | 1938.7     |
| L1110 | x | $\frac{3.3}{13.4}$   | H1 1940.90 |
| L1100 | x | $\frac{4.1}{11}$     | 1937.6     |
| L1050 | x | $\frac{1934.40}{16}$ | 1936.8     |

23

BUTTRESS #5  
D = 1300

| STATION | +    | ∧       | - | ELEV    |
|---------|------|---------|---|---------|
| □       | 4.93 | 1974.62 | — | 1969.69 |

L 950 ✓

L 960 ✓

L 970 ✓

L 980 ✓

L 990 ✓

|   |      |         |   |         |          |
|---|------|---------|---|---------|----------|
| □ | 4.21 | 1998.25 | — | 1994.04 | D 125143 |
|---|------|---------|---|---------|----------|

L 995

L 1002 ✓

L 1005

L 1010 ✓

L 1020 ✓

L 1030 ✓

WEST

EAST

| TBM | @ AXIS HUB                |                           | @ D 1332 34                |                            |
|-----|---------------------------|---------------------------|----------------------------|----------------------------|
|     | (1974.6)                  |                           |                            |                            |
|     | $\frac{5.0}{10}$<br>69.0  | $\frac{4.0}{10.6}$        | $\frac{4.5}{10.1}$<br>76.1 | $\frac{3.5}{10}$<br>71.1   |
|     |                           |                           |                            | $\frac{+1.5}{1.3}$<br>76.1 |
|     |                           |                           |                            | (1974.6) ✓                 |
|     | $\frac{5.0}{10}$<br>69.0  | $\frac{4.8}{4}$<br>69.8   | $\frac{6.7}{0}$<br>67.9    | $\frac{6.2}{4}$<br>68.4    |
|     |                           |                           |                            | $\frac{4.6}{4}$<br>70.0    |
|     |                           |                           |                            | $\frac{4.0}{10.6}$<br>70.6 |
|     |                           |                           |                            | $\frac{+2.0}{1.3}$<br>76.6 |
|     |                           |                           |                            | 1974.6                     |
|     | $\frac{5.0}{10}$<br>69.0  | $\frac{4.9}{6.5}$<br>69.7 | $\frac{8.8}{3}$<br>65.8    | $\frac{10.0}{0}$<br>64.0   |
|     |                           |                           |                            | $\frac{9.0}{3.5}$<br>65.6  |
|     |                           |                           |                            | $\frac{4.8}{5.5}$<br>69.8  |
|     |                           |                           |                            | $\frac{4.0}{10.6}$<br>70.6 |
|     |                           |                           |                            | $\frac{1.1}{12}$<br>73.5   |
|     |                           |                           |                            | $\frac{+4.5}{1.5}$<br>79.1 |
|     |                           |                           |                            | 1974.6                     |
|     | $\frac{4.9}{10}$<br>69.7  | $\frac{4.8}{5.5}$<br>69.8 | $\frac{9.8}{3.5}$<br>64.3  | $\frac{10.3}{0}$<br>64.3   |
|     |                           |                           |                            | $\frac{7.3}{4}$<br>67.3    |
|     |                           |                           |                            | $\frac{1.8}{9}$<br>72.8    |
|     |                           |                           |                            | $\frac{+5.5}{1.4}$<br>80.1 |
|     |                           |                           |                            | 1998.3                     |
|     | $\frac{4.7}{6.9}$<br>69.9 | $\frac{4.7}{6.9}$<br>69.9 | $\frac{9.7}{3.5}$<br>64.9  | $\frac{10.8}{0}$<br>63.8   |
|     |                           |                           |                            | $\frac{9.4}{2}$<br>65.2    |
|     |                           |                           |                            | $\frac{7.2}{5}$<br>67.4    |
|     |                           |                           |                            | $\frac{3.2}{8}$<br>71.4    |
|     |                           |                           |                            | $\frac{15.3}{7.6}$<br>83.0 |
|     |                           |                           |                            | $\frac{13.1}{20}$<br>85.2  |
|     |                           |                           |                            | 1998.3                     |
|     | $\frac{4.8}{10}$<br>69.8  | $\frac{8.0}{7.5}$<br>66.6 | $\frac{9.8}{3.5}$<br>64.8  | $\frac{10.0}{0}$<br>64.6   |
|     |                           |                           |                            | $\frac{10.3}{2}$<br>67.3   |
|     |                           |                           |                            | $\frac{7.8}{6}$<br>66.8    |
|     |                           |                           |                            | $\frac{3.2}{8}$<br>71.4    |
|     |                           |                           |                            | $\frac{14.2}{7.5}$<br>84.1 |
|     |                           |                           |                            | $\frac{10.2}{20}$<br>88.1  |
|     |                           |                           |                            | 1998.3                     |
|     | $\frac{4.8}{10}$<br>69.8  | $\frac{8.9}{7}$<br>65.7   | $\frac{9.5}{4}$<br>64.1    | $\frac{9.6}{0}$<br>65.0    |
|     |                           |                           |                            | $\frac{5.6}{6}$<br>69.0    |
|     |                           |                           |                            | $\frac{3.7}{9}$<br>70.9    |
|     |                           |                           |                            | $\frac{14.3}{8.4}$<br>84.0 |
|     |                           |                           |                            | $\frac{8.8}{20}$<br>89.5   |
|     |                           |                           |                            | 1998.3                     |
|     | $\frac{4.5}{10}$<br>70.1  | $\frac{4.8}{6}$<br>69.8   | $\frac{9.4}{5}$<br>65.2    | $\frac{9.0}{0}$<br>65.0    |
|     |                           |                           |                            | $\frac{5.6}{6}$<br>69.0    |
|     |                           |                           |                            | $\frac{3.7}{9}$<br>70.9    |
|     |                           |                           |                            | $\frac{14.3}{8.4}$<br>84.0 |
|     |                           |                           |                            | $\frac{8.8}{20}$<br>89.5   |
|     |                           |                           |                            | 1998.3                     |
|     | $\frac{4.2}{10}$<br>69.9  | $\frac{4.8}{6.9}$<br>69.8 | $\frac{9.5}{0}$<br>65.1    | $\frac{9.4}{4}$<br>65.0    |
|     |                           |                           |                            | $\frac{5.0}{5}$<br>69.6    |
|     |                           |                           |                            | $\frac{2.2}{7}$<br>72.4    |
|     |                           |                           |                            | $\frac{+0.5}{9}$<br>75.1   |
|     |                           |                           |                            | $\frac{8.3}{19}$<br>90.0   |
|     |                           |                           |                            | 1974.6                     |
|     | $\frac{5.0}{10}$<br>69.0  | $\frac{5.0}{6}$<br>69.6   | $\frac{8.0}{3.5}$<br>66.6  | $\frac{7.3}{0}$<br>67.3    |
|     |                           |                           |                            | $\frac{3.3}{7}$<br>71.3    |
|     |                           |                           |                            | $\frac{+1.0}{9}$<br>75.6   |
|     |                           |                           |                            | $\frac{5.5}{2.2}$<br>92.8  |
|     |                           |                           |                            | 1974.6                     |
|     | $\frac{5.2}{10}$<br>69.4  | $\frac{5.5}{6}$<br>69.1   | $\frac{6.9}{4}$<br>67.7    | $\frac{6.3}{0}$<br>68.3    |
|     |                           |                           |                            | $\frac{4.0}{6}$<br>70.0    |
|     |                           |                           |                            | $\frac{+1.4}{10}$<br>76.0  |
|     |                           |                           |                            | $\frac{5.0}{2.3}$<br>93.3  |

(24)

## BOTTRESS # 5 (CONT)

L1040 ✓

L1050 ✓

L1060 ✓

L1070 ✓

L1080 ✓

L1090 ✓

L1100

□

4.93 1969.69 1969.66

|                         |                    |                   |                   |                   |                                    |                                    |                                   |  |
|-------------------------|--------------------|-------------------|-------------------|-------------------|------------------------------------|------------------------------------|-----------------------------------|--|
| 1974.6                  |                    |                   |                   |                   |                                    |                                    | 1998.3 ←                          |  |
| $\frac{4.5}{10}$        | $\frac{4.6}{6.6}$  | $\frac{6.8}{3}$   | $\frac{6.8}{0}$   | $\frac{3.1}{5}$   | $\frac{+2.1}{10}$                  | $\left. \right\} \frac{4.7}{23}$   |                                   |  |
| 70.1                    | 70.0               | 67.8              | 67.8              | 71.5              | 76.7                               | 93.6                               |                                   |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    |                                   |  |
| $\frac{4.3}{10}$        | $\frac{5.8}{4.5}$  | $\frac{5.4}{0}$   | $\frac{4.5}{3.0}$ | $\frac{1.4}{6.5}$ | $\frac{+4.5}{11}$                  | $\left. \right\} \frac{4.3}{27}$   |                                   |  |
| 70.3                    | 68.8               | 69.2              | 70.1              | 73.2              | 79.1                               | 94.0                               |                                   |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    |                                   |  |
| $\frac{3.9}{10}$        | $\frac{3.9}{7}$    | $\frac{6.4}{5}$   | $\frac{5.4}{0}$   | $\frac{4.8}{1.5}$ | $\frac{2.7}{5}$                    | $\frac{+2.6}{7.5}$                 | $\left. \right\} \frac{9.5}{14}$  |  |
| 70.7                    | 70.7               | 68.2              | 69.2              | 69.8              | 71.9                               | 77.2                               | 88.8                              |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    | 94.4                              |  |
| $\frac{4.2}{10}$        | $\frac{4.4}{7}$    | $\frac{6.1}{4.3}$ | $\frac{5.3}{0}$   | $\frac{3.0}{3}$   | $\frac{0.2}{6.5}$                  | $\frac{+4.7}{9}$                   | $\left. \right\} \frac{9.4}{12}$  |  |
| 70.4                    | 70.2               | 68.5              | 69.3              | 71.6              | 74.4                               | 79.3                               | 88.9                              |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    | 93.7                              |  |
| $\frac{4.5}{10}$        | $\frac{5.0}{5.5}$  | $\frac{5.6}{2}$   | $\frac{2.5}{0}$   | $\frac{+2.0}{9}$  | $\left. \right\} \frac{9.0}{13.5}$ |                                    | $\frac{4.7}{18}$                  |  |
| 70.1                    | 69.6               | 69.0              | 72.1              | 76.6              | 89.3                               |                                    | 93.6                              |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    |                                   |  |
| $\frac{1.2}{14}$        | $\frac{4.3}{7}$    | $\frac{4.1}{2}$   | $\frac{0}{0}$     | $\frac{0.9}{5}$   | $\frac{+10.5}{7}$                  | $\left. \right\} \frac{12.9}{7.5}$ | $\frac{3.6}{19}$                  |  |
| 73.4                    | 70.3               | 70.5              | 73.7              | 85.1              | 85.4                               |                                    | 94.7                              |  |
| 1974.6                  |                    |                   |                   |                   |                                    |                                    |                                   |  |
| $\frac{0.9}{18.5}$      | $\frac{2.5}{15.5}$ | $\frac{3.4}{10}$  | $\frac{2.4}{3.5}$ | $\frac{1.0}{0}$   | $\frac{+0.8}{2}$                   | $\frac{+9.1}{5}$                   | $\left. \right\} \frac{12.0}{10}$ |  |
| 73.7                    | 72.0               | 71.2              | 72.2              | 73.6              | 75.4                               | 83.7                               | 86.3                              |  |
|                         |                    |                   |                   |                   |                                    |                                    | 94.4                              |  |
| TSM ON AXIS @ 0.1332 3x |                    |                   |                   |                   |                                    |                                    |                                   |  |

✓

(25)

X-SECTIONS

BUT #4

D = 1240

| STA    | + | ∩       | - | ELEV |
|--------|---|---------|---|------|
|        |   | 1998.25 |   |      |
| L 970  |   |         |   |      |
| L 975  |   |         |   |      |
| L 980  |   |         |   |      |
| L 990  |   |         |   |      |
| L 995  |   |         |   |      |
| L 1001 |   |         |   |      |
| L 1003 |   |         |   |      |
| L 1010 |   |         |   |      |
| L 1020 |   |         |   |      |
| L 1030 |   |         |   |      |
| L 1040 |   |         |   |      |
| L 1050 |   |         |   |      |

6 AUG 52

WEST.

EAST

|                  |                   |                    |                  |                    |                    |                     |   |
|------------------|-------------------|--------------------|------------------|--------------------|--------------------|---------------------|---|
| 1991.8           | 1992.1            | 1998.3             | 1998.7           | 1995.8             | 1999.8             | 2002.2              | 2012.9  |
| $\frac{6.5}{10}$ | $\frac{6.2}{4}$   | $\frac{6.5}{0}$    | $\frac{5.6}{4}$  | $\frac{2.5}{8}$    | $\frac{7.5}{11}$   | $\frac{10.7}{17}$   |   |
| 1992.2           | 1992.5            | 1988.0             | 1998.3           | 1987.9             | 1989.3             | 1994.5              | 2012.9  |
| $\frac{6.1}{10}$ | $\frac{5.8}{4}$   | $\frac{10.3}{2}$   | $\frac{10.8}{0}$ | $\frac{16.4}{2}$   | $\frac{9.0}{4}$    | $\frac{3.8}{8}$     | 2012.9<br>2001.3<br>2002.4                      |
| 1992.5           | 1993.0            | 1987.2             | 1987.0           | 1986.2             | 1993.7             | 2001.5              | 2002.5  |
| $\frac{5.8}{10}$ | $\frac{5.3}{5}$   | $\frac{11.1}{2}$   | $\frac{11.3}{0}$ | $\frac{10.1}{3.5}$ | $\frac{4.6}{7}$    | $\frac{11.4}{13}$   | $\frac{10.4}{16}$                               |
| 1993.1           | 1993.4            | 1987.7             | 1986.6           | 1987.3             | 1989.6             | 1994.5              | 2002.2  |
| $\frac{5.2}{10}$ | $\frac{4.9}{4.5}$ | $\frac{10.6}{3.5}$ | $\frac{11.7}{0}$ | $\frac{11.0}{2}$   | $\frac{8.7}{4.5}$  | $\frac{3.8}{7.5}$   | 2004.0<br>$\frac{10.7}{12}$<br>$\frac{8.9}{16}$ |
| 1993.5           | 1993.3            | 1987.9             | 1986.7           | 1986.6             | 1987.1             | 1988.9              | 1990.1  |
| $\frac{4.8}{10}$ | $\frac{5.0}{9}$   | $\frac{8.4}{6}$    | $\frac{11.6}{2}$ | $\frac{11.7}{0}$   | $\frac{11.2}{2.5}$ | $\frac{9.4}{5}$     | $\frac{8.2}{7}$                                 |
| 1993.8           | 1993.6            | 1990.3             | 1987.2           | 1986.8             | 1987.6             | 1988.8              | 1990.6  |
| $\frac{4.5}{10}$ | $\frac{4.7}{8}$   | $\frac{8.0}{7}$    | $\frac{11.1}{3}$ | $\frac{11.5}{0}$   | $\frac{10.7}{2}$   | $\frac{9.5}{4}$     | $\frac{7.7}{7}$                                 |
| 1994.0           | 1994.1            | 1987.0             | 1988.2           | 1990.3             | 1992.2             | 1995.7              | 2004.2  |
| $\frac{4.3}{10}$ | $\frac{4.2}{7}$   | $\frac{9.3}{4}$    | $\frac{11.2}{0}$ | $\frac{10.1}{3}$   | $\frac{8.0}{4}$    | $\frac{6.1}{6}$     | $\frac{2.4}{7.5}$                               |
| 1994.2           | 1994.3            | 1988.3             | 1987.4           | 1987.9             | 1994.2             | 2000.9              | 2004.7  |
| $\frac{4.1}{10}$ | $\frac{4.0}{5}$   | $\frac{10.0}{2}$   | $\frac{10.9}{0}$ | $\frac{10.4}{3}$   | $\frac{4.1}{5}$    | $\frac{12.0}{11}$   | $\frac{8.2}{12}$                                |
| 1994.7           | 1994.7            | 1989.4             | 1988.9           | 1990.3             | 1991.9             | 1995.1              | 2005.7  |
| $\frac{3.6}{10}$ | $\frac{3.6}{6}$   | $\frac{8.9}{3}$    | $\frac{9.4}{0}$  | $\frac{8.0}{3}$    | $\frac{6.4}{4.5}$  | $\frac{3.2}{6}$     | 2007.9<br>$\frac{7.2}{13}$<br>$\frac{5.0}{18}$  |
| 1995.2           | 1995.1            | 1990.8             | 1989.5           | 1991.4             | 1996.0             | 2006.9              | 2008.9  |
| $\frac{3.1}{10}$ | $\frac{3.2}{6}$   | $\frac{7.5}{3}$    | $\frac{8.0}{0}$  | $\frac{6.9}{4}$    | $\frac{2.3}{6.5}$  | $\frac{6.0}{14}$    | $\frac{4.0}{20}$                                |
| 1995.6           | 1995.1            | 1990.7             | 1989.8           | 1990.9             | 1995.1             | 2002.6              | 2008.0  |
| $\frac{2.7}{10}$ | $\frac{3.2}{5}$   | $\frac{7.6}{3}$    | $\frac{8.5}{0}$  | $\frac{7.4}{4.5}$  | $\frac{3.2}{4.7}$  | $\frac{10.3}{12.5}$ | $\frac{4.9}{15}$                                |
| 1995.1           | 1995.0            | 1991.9             | 1991.5           | 1992.2             | 1997.7             | 2007.4              | 2009.9  |
| $\frac{3.2}{10}$ | $\frac{3.3}{3}$   | $\frac{6.4}{2.5}$  | $\frac{6.8}{0}$  | $\frac{6.1}{4}$    | $\frac{0.6}{8}$    | $\frac{5.5}{12}$    | $\frac{3.0}{20}$                                |

26

Bot #4 (cont.)

L1060

|                  |                 |                 |                 |                   |                   |                   |                      |
|------------------|-----------------|-----------------|-----------------|-------------------|-------------------|-------------------|----------------------|
| 1995.6           | 1998.3          | 1993.2          | 1993.0          | 1993.1            | 1995.8            | 2007.3            | 2012.9               |
| $\frac{2.7}{10}$ | $\frac{3.5}{5}$ | $\frac{5.1}{2}$ | $\frac{5.3}{0}$ | $\frac{5.2}{3.5}$ | $\frac{2.5}{8.5}$ | $\frac{+9.0}{15}$ | $\frac{2009.5}{3.4}$ |
|                  |                 |                 |                 |                   |                   |                   | $\frac{20}{20}$      |

L1070

|                  |                 |                 |                 |                   |                   |                  |
|------------------|-----------------|-----------------|-----------------|-------------------|-------------------|------------------|
| 1995.1           | 1994.7          | 1994.4          | 1996.9          | 1999.5            | 2007.3            | 2009.4           |
| $\frac{3.2}{10}$ | $\frac{3.2}{3}$ | $\frac{3.9}{0}$ | $\frac{1.4}{5}$ | $\frac{+1.2}{10}$ | $\frac{+9.0}{15}$ | $\frac{3.5}{20}$ |

L1080

|                  |                 |                  |                  |                  |                   |                  |
|------------------|-----------------|------------------|------------------|------------------|-------------------|------------------|
| 1994.5           | 1995.3          | 1998.5           | 2000.8           | 2004.5           | 2007.1            | 2008.7           |
| $\frac{3.8}{10}$ | $\frac{3.0}{5}$ | $\frac{+0.2}{0}$ | $\frac{+2.5}{5}$ | $\frac{+6.2}{9}$ | $\frac{+8.8}{17}$ | $\frac{4.2}{20}$ |

L1090

5.39 1999.43 — 1994.04

|                  |                 |                 |                   |                  |                   |                  |
|------------------|-----------------|-----------------|-------------------|------------------|-------------------|------------------|
| 1994.3           | 1994.9          | 1995.9          | 1997.5            | 2003.2           | 2005.1            | 2007.1           |
| $\frac{4.0}{10}$ | $\frac{3.4}{4}$ | $\frac{2.4}{0}$ | $\frac{0.8}{3.5}$ | $\frac{+4.9}{8}$ | $\frac{+6.8}{15}$ | $\frac{5.8}{20}$ |

L1100

|                  |                 |                 |                    |                   |                  |
|------------------|-----------------|-----------------|--------------------|-------------------|------------------|
| 1994.4           | 1994.5          | 1999.4          | 2000.6             | 2002.1            | 2005.1           |
| $\frac{5.0}{10}$ | $\frac{4.7}{5}$ | $\frac{3.8}{0}$ | $\frac{+1.2}{5.5}$ | $\frac{+2.7}{12}$ | $\frac{7.8}{20}$ |



(27) X-SECTION BUTTRESS #6

| STA | +    | ∩       | - | ELEV    |
|-----|------|---------|---|---------|
| □   | 4.93 | 1974.62 |   | 1969.69 |
| □   | 5.00 | 1952.68 |   | 1947.68 |

L950

L956

L960

L970

|       |      |         |       |         |
|-------|------|---------|-------|---------|
| □     | 4.05 | 1951.73 |       | 1947.68 |
| T.P.  | 0.83 | 1940.58 | 11.98 | 1939.75 |
| L.980 |      |         |       |         |

L990

L991.5

L996

L1001

L1010

BASE LINE D1360 L #6  
5-6 AUG '52

STR ON AXIS D-1332<sup>34</sup>

| W                        | HI. 1952.7              |                           |                           |                             |                            |                             | E                           | 1974.6 |
|--------------------------|-------------------------|---------------------------|---------------------------|-----------------------------|----------------------------|-----------------------------|-----------------------------|--------|
| $\frac{6.2}{10}$<br>46.5 | $\frac{0.7}{0}$<br>52.0 | $\frac{2.3}{7}$<br>50.4   | $\frac{1.6}{10}$<br>51.1  | $\frac{0.0}{0}$<br>1952.7   | $\frac{16.6}{70}$<br>58.0  |                             |                             |        |
| $\frac{6.3}{10}$<br>46.4 | $\frac{5.9}{3}$<br>46.8 | $\frac{5.6}{0}$<br>1947.1 | $\frac{2.6}{9}$<br>1950.1 | $\frac{19.6}{12}$<br>1955.0 | $\frac{16.0}{17}$<br>58.6  |                             |                             |        |
| $\frac{6.1}{10}$<br>46.6 | $\frac{5.9}{6}$<br>46.8 | $\frac{10.3}{4}$<br>41.4  | $\frac{1.7}{0}$<br>1938.9 | $\frac{1.7}{3}$<br>38.3     | $\frac{4.0}{4.7}$<br>44.6  | $\frac{19.1}{10.5}$<br>55.5 | $\frac{14.2}{17.5}$<br>60.4 |        |
| $\frac{4.7}{10}$<br>5.6  | $\frac{4.6}{5}$<br>8.0  | $\frac{3.6}{4.5}$<br>8.0  | $\frac{3.4}{0}$<br>7.4    | $\frac{3.4}{5}$<br>6.2      | $\frac{18.1}{9}$<br>56.5   | $\frac{13.2}{14}$<br>61.9   |                             |        |
| $\frac{4.8}{10}$<br>3.0  | $\frac{5.0}{5}$<br>5.0  | $\frac{3.2}{9.4}$<br>3.5  | $\frac{1940.6}{0}$<br>9.4 | $\frac{33.2}{5}$<br>7.4     | $\frac{59.6}{13}$<br>15.0  | $\frac{62.1}{17}$<br>12.5   |                             |        |
| $\frac{3.1}{10}$<br>48.6 | $\frac{4.2}{4}$<br>47.5 | $\frac{5.0}{4}$<br>46.7   | $\frac{10.2}{4}$<br>38.4  | $\frac{10.2}{0}$<br>30.4    | $\frac{9.3}{31.3}$<br>31.3 | $\frac{7.4}{5.5}$<br>48.0   | $\frac{13.9}{14}$<br>60.7   |        |
| $\frac{3.4}{10}$<br>48.3 | $\frac{4.4}{7}$<br>47.3 | $\frac{5.1}{4}$<br>46.6   | $\frac{10.2}{4}$<br>38.4  | $\frac{10.2}{0}$<br>30.4    | $\frac{9.3}{31.3}$<br>31.3 | $\frac{7.4}{5.5}$<br>48.0   | $\frac{13.9}{14}$<br>60.7   |        |
| $\frac{5.0}{10}$<br>46.7 | $\frac{7.0}{6}$<br>39.6 | $\frac{7.6}{4}$<br>38.0   | $\frac{8.9}{0}$<br>31.7   | $\frac{8.4}{2}$<br>32.2     | $\frac{5.2}{5}$<br>35.4    | $\frac{2.8}{10}$<br>37.8    | $\frac{12.4}{15}$<br>62.2   |        |
| $\frac{4.6}{10}$<br>47.1 | $\frac{4.0}{7}$<br>36.6 | $\frac{4.0}{4}$<br>36.6   | $\frac{8.2}{0}$<br>32.4   | $\frac{8.1}{1}$<br>32.5     | $\frac{5.0}{5}$<br>35.6    | $\frac{1.7}{10}$<br>38.9    | $\frac{12.8}{14}$<br>61.8   |        |
| $\frac{2.3}{10}$<br>49.4 | $\frac{4.1}{5}$<br>47.6 | $\frac{7.1}{3.5}$<br>33.5 | $\frac{8.0}{0}$<br>32.6   | $\frac{7.1}{5.5}$<br>33.5   | $\frac{+5.7}{6}$<br>46.3   | $\frac{12.9}{13}$<br>61.7   | $\frac{9.3}{18.5}$<br>65.3  |        |

CONT PAGE (36) ✓

(28)

14-15

## ARCH RING LOCATION

| STATION   | +    | -       | ELEV    |
|-----------|------|---------|---------|
| B.M.      | 0.98 | 2015.18 | 2014.20 |
| L1071 98  |      |         |         |
| D 1893.58 |      | 7       |         |
| D 1885.86 |      | 11.84   | 2003.34 |
| D 1879.0  |      | 2003.33 | 1.09    |
| D 1870.0  |      | 4.02    | 1999.31 |
| D 1861.0  |      | 6.05    | 1997.28 |
| D 1854.14 |      | 7.87    | 1995.46 |
| D 1846.42 |      |         |         |
|           | 0.70 | 2003.33 | 12.55   |
|           |      |         | 2002.63 |

ARCH  
14-15

Aug 29, 1952

| TAPE<br>DIST FROM | BASE LINE                     | L1071 98 |           |       |
|-------------------|-------------------------------|----------|-----------|-------|
| P.K. IN           | WEST                          | SIDE     | # 14      | BUT   |
| DIST              | STATION OF<br>EXISTING INTRA. |          |           | INTRA |
| S-4.8             | L1076.78                      | F2.8     | 18.0 EXTR | 14.37 |
| S-11.3            | L1083.28                      | F2.5     | 22.9 EXTR | 19.47 |
| S-16              | L1087.98                      | F3.0     | 24.9 EXTR | 21.7  |
| S-16.4            | L1088.38                      | F2.3     | 22.0 EXTR | 19.47 |
| S-13.5            | L1085.03                      | F2.4     | 18.4 EXTR | 14.37 |
|                   |                               |          |           | 0     |

D 1870

2068.50

1999.31

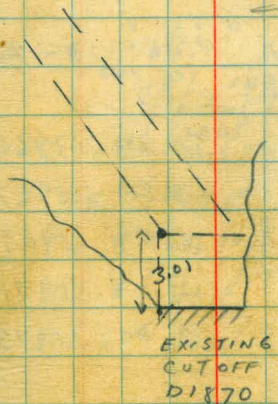
69.29 on road

- 21.7

90.99

87.98

F 3.01



01810 &  
ARCH KING 13-14  
BASE LINE L1084<sup>03</sup>

| STATION  | +    | ∧       | -     | ELEV   | DIST   |
|----------|------|---------|-------|--------|--------|
|          | 1.76 | 1992.84 | —     | ✓      |        |
| D 1794.2 |      |         | 10.66 | 1982.1 | 17.0 S |
| D 1801   |      |         | 9.07  | 1983.7 | 18.8 S |
| D 1810 ✓ |      |         | 6.8   | 1986.0 | 19.0 S |
| D 1819   |      |         | 4.5   | 1988.3 | 14.7 S |
| D 1825.9 |      |         | 2.3   | 1990.5 | 8.5 S  |

01750 &  
ARCH RING 13-12  
1976<sup>22</sup> ← (21) SEE PAGE ✓

|          |  |  |       |        |        |
|----------|--|--|-------|--------|--------|
| D 1734.2 |  |  | 10.23 | 1966.0 | 13.3 S |
| D 1741.0 |  |  | 8.50  | 1967.7 | 16.3 S |
| D 1750   |  |  | 6.59  | 1969.6 | 15.8 S |
| D 1759   |  |  | 4.28  | 1971.9 | 10.0 S |
| D 1766   |  |  | 2.60  | 1973.6 | 3.7 S  |

| calculated STATION | C OR F ABOVE EXISTING CONE | CALCULATIONS                         |                  | RADIUS |
|--------------------|----------------------------|--------------------------------------|------------------|--------|
| L 1101 ✓           | C 0.2 ✓                    | 2668.50<br>1982.1                    | 1101<br>1100.5   | 14.4   |
| L 1102.8 ✓         | F 1.5 ✓                    | EXTRADOS 86.40<br>19.13 ✓<br>1100.81 | 2068.5<br>1986.0 | 19.5   |
| L 1103 ✓           | F 1.2 ✓                    | 2668.5<br>1983.7                     | 825.7<br>21.7    | 21.7   |
| L 1098.7 ✓         | F 1.0 ✓                    | 84.8<br>19.5                         | 1104.2           | 19.5   |
| L 1092.5 ✓         | C 0.1 ✓                    | 1104.3                               | 2068.5<br>1988.3 | 14.4   |
|                    |                            | 2668.5<br>1990.5                     | 80.2<br>19.5     |        |
|                    |                            | 1078.0<br>14.4                       | 1099.7           |        |
|                    |                            | 1092.4                               |                  |        |

BASE LINE L1104<sup>96</sup>

|            |         |                                  |                   |        |
|------------|---------|----------------------------------|-------------------|--------|
| L 1117.3 ✓ | C 0.4 ✓ | 2068.50<br>1966                  | 2068.50<br>1967.7 |        |
| L 1120.3 ✓ | OK ✓    | EXTRADOS 102.50<br>20.05<br>20.5 | 100.80<br>19.5    | 120.30 |
| L 1117.8 ✓ | F 0.8 ✓ | 26.4 ✓<br>2068.50<br>1969.5      | 2068.50<br>1971.9 |        |
| L 1114.0 ✓ | F 2.1 ✓ | 24.3 ✓<br>98.9<br>21.7           | 96.60<br>19.5     |        |
| L 1107.7 ✓ | F 1.6 ✓ | 19.6 ✓<br>120.6<br>119.5         | 116.10<br>11.4    | 2.1    |
|            |         | 0.8                              |                   |        |
|            |         | 2068.50<br>1973.5                |                   |        |
|            |         | 94.90<br>14.4                    |                   |        |
|            |         | 109.3<br>107.7                   |                   |        |
|            |         | 12                               |                   |        |



(30)

£ D1690

| STATION   | +    | ARCH    | RINGS | 11-12 | ELEV    | DIST  |
|-----------|------|---------|-------|-------|---------|-------|
| IRON PIPE | 8.04 | 1961.71 |       |       | 1953.67 |       |
| D 1705.9  |      |         | 1.92  |       | 1959.79 | 1.5 N |
| D 1699    |      |         | 3.86  |       | 1957.85 | 3.5 S |
| D 1690    |      |         | 8.0   |       | 1953.71 | 8.0 S |
| D 1681    |      |         | 9.71  |       | 1952.00 | 7.8 S |
| D 1674.2  |      |         | 11.47 |       | 1950.24 | 5.8 S |

ARCH £ 1630 RINGS 10-11

| Rock     | +    | ARCH    | RINGS | 10-11 | ELEV    | DIST    |
|----------|------|---------|-------|-------|---------|---------|
| Rock     | 3.65 | 1943.93 |       |       | 1940.28 |         |
| D 1645.9 |      |         | 2.21  |       | 1941.72 | 13.3 S. |
| D 1639   |      |         | 4.47  |       | 1939.46 | 20.3 S  |
| D 1630   |      |         | 7.12  |       | 1936.81 | 24.2 S  |
| D 1621   |      |         | 8.17  |       | 1935.76 | 24.4 S  |
| D 1614.2 |      |         | 8.77  |       | 1935.16 | 21.4 S  |

ARCH £ D 1570 RINGS 9-10

| I.P.     | +    | ARCH    | RINGS | 9-10 | ELEV    | DIST   |
|----------|------|---------|-------|------|---------|--------|
| I.P.     | 2.96 | 1928.39 |       |      | 1925.43 |        |
| D 1585.9 |      |         | 6.87  |      | 1921.52 | 9.6 S  |
| D 1579   |      |         | 8.75  |      | 1919.64 | 17.5 S |
| D 1570   |      |         | 11.38 |      | 1917.01 | 20.8 S |
| D 1561   | 5.72 | 1923.18 | 12.65 |      | 1915.74 | 22.4 S |
| D 1554.2 |      |         | 10.04 |      | 1913.19 | 18.5 S |

1917.4  
5.72  
1923.18

SEPT 2, 1954

BASE LINE L 1128 63

| ROCK STATION | ROD  | SEE  | PAGE | (31) | 2068.5                                      | 2068.5                            | EXTRAD | INTEN |
|--------------|------|------|------|------|---|-----------------------------------|--------|-------|
| L 1127.13    | 5.9  | 24.0 | ✓    | ✓    | 127.1<br>1941.4<br>14.4                     | 132.1<br>1936.4<br>19.5           | 20.5   | 14.4  |
| L 1132.13    | 5.8  | 22.0 | ✓    | ✓    | 1955.8                                      | 1955.9                            | 25.1   | 19.5  |
| L 1136.63    | 8.1  | OK   | ✓    | ✓    | 2068.5<br>136.6<br>1931.9<br>21.7           | 2068.5<br>136.4<br>1932.1<br>19.5 | 27.3   | 21.7  |
| L 1136.43    | 10.1 | 20.4 | ✓    | ✓    | 1953.6                                      | 1951.6                            | 25.4   | 19.5  |
| L 1134.43    | 13.2 | 21.8 | ✓    | ✓    | 2068.5<br>134.4<br>1934.1<br>14.4<br>1948.5 | 2068.5<br>132.1<br>1936.4<br>19.5 | 21.1   | 14.4  |

BASE LINE L 1128 63

| Rock      | ROD  | SEE   | PAGE | 2068.50                           | 2068.50                           | 2068.50                  | EXTRAD               |
|-----------|------|-------|------|-----------------------------------|-----------------------------------|--------------------------|----------------------|
| L 1141.93 | 2.9  | 20.7  | ✓    | 148.9<br>1926.60<br>14.4          | 148.9<br>1919.60<br>19.5          | 152.8<br>1915.70<br>21.7 | 21.6<br>26.4<br>25.5 |
| L 1148.93 | 4.8  | 20.36 | ✓    | 1941.00                           | 1939.10                           | 1937.40                  | 28.2                 |
| L 1152.93 | 6.5  | F 0.6 | ✓    | 2068.50<br>176<br>1915.50<br>19.0 | 2068.50<br>150<br>1918.50<br>14.4 | 1935.8<br>1914.4<br>9.0  | 26.4<br>22.1         |
| L 1150.93 | 11.0 | 22.2  | ✓    | 1934.50                           | 1932                              |                          |                      |

BASE LINE L 1151 39

| SEE P.    | (32)             | 2068.50                   | 2068.50                  | 2068.50                  | EXTRAD |
|-----------|------------------|---------------------------|--------------------------|--------------------------|--------|
| L 1160.99 | F 0.57<br>(0.48) | 160.99<br>1907.69<br>14.4 | 168.9<br>1899.60<br>19.5 | 172.2<br>1896.30<br>21.7 | 23.0   |
| L 1168.89 | C 0.54           | 1922.09                   | 1919.10                  | 1918.00                  | 27.35  |
| L 1172.19 | F 1.0            | 2068.50<br>173.8          |                          | 2068.50<br>169.9         | 29.37  |
| L 1173.79 | C 1.5            | 1894.70<br>19.5           |                          | 1898.60<br>14.4          | 27.59  |
| L 1169.89 | C 0.7            | 1914.20                   |                          | 1913.00                  | 23.70  |

(31)

## B.M. LEVELS

| STATION   | +       | ⊖                      | ELEV   |
|-----------|---------|------------------------|--|
| PK #14    | -0.45   | 2013.75                | 2014.20  |
| T.P.      | 2.87    | 2006.00 <sup>OK</sup>  | 2003.13 <sup>5 5</sup> ± 1/2 ARCH 14-15 <sup>WOOD PL. 4</sup>    |
| IRON PIPE |         |                        | 6.85 1999.15   |
| T.P.      | 0.88    | 1993.88                | 1993.00 <sup>NOB. 2X L 1884 23 D 1816 29</sup>                   |
| IRON PIPE | 3.08    | 1985.93<br>1986.03     | 1982.85 <sup>1982.87</sup>                                       |
| IRON PIPE |         |                        | 8.36 1977.67 <sup>57</sup>                                       |
| IRON PIPE | 2.04    | 1976.27 <sup>17</sup>  | 1974.23 <sup>13</sup>  |
| IRON PIPE |         |                        | 7.33 1968.94 <sup>84</sup>                                       |
| IRON PIPE | 1.39    | 1967.27 <sup>11</sup>  | 1965.82 <sup>72</sup> (1967.78)<br><small>OLD B.M. WRONG</small> |
| T.P.      | 2.36    | 1959.48 <sup>38K</sup> | 1957.12 <sup>02</sup>  |
| BUT #11   |         |                        | 0.21 1967.0 <sup>1966.90</sup>                                   |
| IRON PIPE |         |                        | 5.71 1953.77 <sup>67</sup>                                       |
| T.P.      | 0.06    | 1947.32 <sup>22</sup>  | 1947.26 <sup>16</sup>  |
| IRON PIPE |         |                        | 12.08 1935.24 <sup>14</sup> 1935.16                              |
| Rock      |         |                        | 6.96 1940.36 <sup>26</sup> 1940.28                               |
| CHK       | +13.13  | -86.17                 |  |
|           | 0.45    | 45                     |  |
|           | +12.68  | -86.62                 |  |
|           | 2014.20 | +86.52                 |  |
|           | 1940.36 | ERROR .10              |  |
|           | 73.84   |                        |  |
|           | 12.68   |                        |  |
|           | 86.52   |                        |  |

SEPT. 2, 1952

|  |
|--|
| NAIL IN WEST SIDE #14 BUT 10' SOUTH L1000    |
| 3" PIPE CAP ARCH 15-14 -15' WEST of #14      |
| 3" PIPE CAP ± 10' WEST of #13 BUT ARCH 14-13 |
| 3" PIPE CAP of BUT #13                       |
| 3" PIPE CAP ARCH RING 12-13 ± D 1765         |
| 3" PIPE CAP ARCH RING 12-13 ± D 1740         |
| 3" " " 10' WEST of #12 BUT ARCH 13-12        |
| WEST WALL (CONC) BUT #11 (X)                 |
| 3" PIPE CAP (D 1684) ARCH 12-11<br>L 1138    |
| 3" PIPE CAP ARCH 11-10 ± D 1610              |
| B.M. Rock ± D 1612 Rock SOUTH ARCH. 11-10    |

(32)

## BM LEVELS

| STATION    | <sup>BS</sup><br>+ | +                     | <sup>FS</sup><br>- | ELEV                       |
|------------|--------------------|-----------------------|--------------------|----------------------------|
| IRON PIPE  | 2.20               | 1937.36               | —                  | 1935.16 BM                 |
| IRON PIPE  | 1.63               | 1927.06               | 11.93              | 1925.43 1925.43            |
| IRON PIPE  |                    |                       | 9.61               | 1917.45                    |
| IRON PIPE  | 9.96               | 1923.94               | 13.08              | 1913.98                    |
| IRON PIPE  |                    |                       | 8.39               | 1915.55                    |
| T.P.       | 11.95              | 1935.09               | 0.80               | 1923.14                    |
| TP         |                    |                       | 12.16              | 1922.93                    |
| 2X2 HUB    | 11.43              | 1942.30 <sup>OK</sup> | 4.22               | 1930.87 <sup>OK</sup>      |
| TREE STUMP |                    |                       | 1.40               | 1940.90 <sup>OK</sup>      |
| T.P.       | 3.91               | 1926.84               | —                  | 1922.93                    |
| 4" PIPE    |                    |                       | 5.68               | 1921.16                    |
| STUMP      | 12.92              | 1953.82 <sup>OK</sup> | —                  | 1940.90                    |
| 2X2 HUB    |                    |                       | 6.13               | 1947.69 1947 <sup>68</sup> |
| T.P.       | 11.89              | 1965.08 <sup>OK</sup> | 0.63               | 1953.19                    |
| T.P.       | 12.21              | 1975.54 <sup>OK</sup> | 1.75               | 1963.33                    |
| STUMP      | 3.95               | 1974.48 <sup>OK</sup> | 5.01               | 1970.53                    |
| 2X2 HUB    |                    |                       | 4.87               | 1969.61 1969 <sup>69</sup> |
| STUMP      |                    |                       | 9.97               | 1964.51                    |
| T.P.       | 11.93              | 1983.55 <sup>OK</sup> | 2.86               | 1971.62                    |
| T.P.       | 10.70              | 1993.45 <sup>OK</sup> | 0.80               | 1982.75                    |
| STUMP      |                    |                       | 5.34               | 1988.11                    |
| 2X2 HUB    |                    |                       | 1.26               | 1992.19 1992 <sup>26</sup> |

SEPT 2, 52

|                     |          |         |         |          |        |
|---------------------|----------|---------|---------|----------|--------|
| I.P.                | BM       | ARCH    | 11-10   | ±        | L 1155 |
| IRON PIPE           | CAP      | ARCH    | 9-10    | ±        | D 1590 |
| IRON PIPE           | CAP      | ARCH    | 9-10    | ±        | D 1570 |
| IRON PIPE           | CAP      | ARCH    | 9-10    | ±        | D 1550 |
| IRON PIPE           | CAP      | ARCH    | 8-9     | ±        | ∠ ARCH |
| IRON REINFORCING    | BAR      | BUT # 7 |         |          |        |
| L 1166              | ∠        | D 1415  |         |          |        |
| NAIL & SHINER       | IN STUMP | ±       | ∠ ARCH  |          | 7-6    |
| 4" OPEN END I. PIPE | ∠        | BUT # 7 | ±       | 70' S    | L 1000 |
| NAIL & SHINER       |          |         |         |          |        |
| D 1380              | ∠        | L 1000  |         |          |        |
| Rock                |          |         |         |          |        |
| Rock                |          |         |         |          |        |
| 18" STUMP           | 20' WEST | ∠       | BUT # 5 | ±        | L 1150 |
| D 1332              | ∠        | L 1000  |         |          |        |
| 15" STUMP           | ±        | L 1020  | ±       | D 1347.0 |        |
| Rock                |          |         |         |          |        |
| Rock                |          |         |         |          |        |
| 8" STUMP            | ±        | L 990   | D 1283  |          |        |
| D 1273              | ∠        | L 1000  |         |          |        |

## BM LEVELS

| STATION           | +     | -       | ELEV    |                    |
|-------------------|-------|---------|---------|--------------------|
| 2x2 HUB           | 11.05 | 2003.24 | 1992.19 | 1992 <sup>26</sup> |
| STUMP             | 12.21 | 2015.47 | 0.04    | 2003.20            |
| STUMP             |       |         | 4.36    | 2011.05            |
|                   |       |         |         | CHECKED & OKAY     |
| 800 <sup>00</sup> | 1.42  | 2085.46 |         | 2084.04            |
| T.P.              | 0.58  | 2078.05 | 7.99    | 2077.47            |
| T.P.              | 0.20  | 2065.26 | 12.99   | 2065.06            |
| T.P.              | 0.62  | 2055.72 | 10.16   | 2055.10            |
| T.P.              | 0.60  | 2043.65 | 12.67   | 2043.05            |
| STUMP             | 2.78  | 2036.17 | 10.26   | 2033.39            |
| STUMP             | 1.18  | 2031.47 | 5.88    | 2030.29            |
| T.P.              | 0.22  | 2018.88 | 12.81   | 2018.66            |
| STUMP             | 5.65  | 2015.58 | 8.95    | 2009.93            |
| STUMP             |       |         | 4.90    | 2010.68            |
| STUMP             |       |         | 8.56    | 2007.02            |
| STUMP             | 0.00  | 2002.90 | 12.68   | 2002.90            |
| 2x2 HUB           | 0.73  | 1992.99 | 10.66   | 1992.24            |
| STUMP             |       |         | 4.80    | 1988.19            |
| STUMP             | 0.68  | 1980.87 | 12.80   | 1980.19            |
| 2x2 HUB           |       |         | 11.16   | 1969.71            |
| STUMP             | 2.96  | 1974.46 | 9.37    | 1971.50            |
| STUMP             |       |         | 9.84    | 1964.62            |
| STUMP             |       |         | 3.88    | 1970.58            |
| T.P.              |       |         | 12.24   | 1962.22            |

CONT PAGE

(35)

SEPT 3, 1952

|  |  |  |  |  |
|--|--|--|--|--|
| D 1273 <sup>48</sup>                           |  |  |  |  |
| CLUSTER OF 3 (15" DIA) 20' EAST #4 BUT ± L 970 |  |  |  |  |
| D 1220 L 993 15" DIA                           |  |  |  |  |
| cone MONUMENT (NAIL IN TOP)                    |  |  |  |  |
| 18" STUMP ± L 900 20' WEST ♀ #2 BUT            |  |  |  |  |
| 18" STUMP ± L 980 20' EAST ♀ #3 BUT            |  |  |  |  |
| 10" STUMP ± L 950' 20' WEST ♀ #3 BUT           |  |  |  |  |
| 15" STUMP ± L 990 D 1220                       |  |  |  |  |
| 12" STUMP ± L 995 D 1230                       |  |  |  |  |
| CLUSTER OF 3 12" ONE ± L 950 20' WEST #4 BUT   |  |  |  |  |
| L 1000 D 1273 <sup>48</sup>                    |  |  |  |  |
| ± D 1280 ± L 988 15" STUMP                     |  |  |  |  |
| CLUSTER ± L 925 ± D 1290                       |  |  |  |  |
| D 1332 <sup>34</sup> L 1000                    |  |  |  |  |
| CLUSTER 8" 30' WEST ♀ #5 BUT ± L 1015          |  |  |  |  |
| 15" STUMP ± L 1020 ± D 1347                    |  |  |  |  |

(34)

D 1510  
ARCH RING 9-8

| STATION             | +    | π                  | —    | ELEV               | DIST  |
|---------------------|------|--------------------|------|--------------------|-------|
| IRON PIPE           | 2.50 | 1918 <sup>05</sup> | —    | 1915 <sup>55</sup> |       |
| D 1525 <sup>9</sup> |      |                    | 6.0  | 1912.1             | 9.3 N |
| D 1519              |      |                    | 5.7  | 1912.4             | 5.6 N |
| D 1510              |      |                    | 5.4  | 1912.7             | 3.3 N |
| D 1501              |      |                    | 5.25 | 1912.8             | 3.9 N |
| D 1494 <sup>2</sup> |      |                    | 5.25 | 1912.8             | 8.0 N |

BASE LINE L 1181<sup>45</sup>

| STATION CALCULATED   | COR F |                    |                    |
|----------------------|-------|--------------------|--------------------|
| ARCH RING 9-8        | ±     |                    |                    |
| L 1172 <sup>15</sup> | C 2.6 | 2068.50            | 2068.50            |
|                      |       | 172.2              | 175.9              |
|                      |       | 1896 <sup>30</sup> | 1872 <sup>60</sup> |
|                      |       | 14.4               | 195                |
|                      |       | 1910.7             | 1912 <sup>10</sup> |
| L 1175 <sup>85</sup> | F 0.6 | 2068.50            | 2068.50            |
|                      |       | 178.2              | 170.6              |
|                      |       | 1890 <sup>30</sup> | 1890 <sup>90</sup> |
|                      |       | 21.7               | 195                |
|                      |       | 1912 <sup>00</sup> | 1910 <sup>40</sup> |
| L 1178 <sup>15</sup> | C 0.7 | 2068.50            | 2068.50            |
|                      |       | 178.2              | 170.6              |
|                      |       | 1890 <sup>30</sup> | 1890 <sup>90</sup> |
|                      |       | 21.7               | 195                |
|                      |       | 1912 <sup>00</sup> | 1910 <sup>40</sup> |
| L 1177 <sup>55</sup> | C 2.4 | 2068.50            | 2068.50            |
|                      |       | 178.5              | 170.6              |
|                      |       | 1895 <sup>00</sup> | 1890 <sup>90</sup> |
|                      |       | 14.4               | 195                |
|                      |       | 1909 <sup>40</sup> | 1910 <sup>40</sup> |
| L 1173 <sup>45</sup> | C 3.4 | 2068.50            | 2068.50            |
|                      |       | 178.5              | 170.6              |
|                      |       | 1895 <sup>00</sup> | 1890 <sup>90</sup> |
|                      |       | 14.4               | 195                |
|                      |       | 1909 <sup>40</sup> | 1910 <sup>40</sup> |

(35)

BM LEVELS

| STATION | +                     | X                     | -                     | ELEV   |
|---------|-----------------------|-----------------------|-----------------------|--|
| TOP     | 0.13                  | 1962.35               | <del>          </del> | 1962.22  |
| T.P.    | 0.65                  | 1951.76               | 11.24                 | 1951.11  |
| STUMP   | 4.58                  | 1945.52 <sup>17</sup> | 10.82                 | 1940.94 <sup>18</sup> <del>1940.90</del>       |
| Rock BM | <del>          </del> | <del>          </del> | 5.19                  | 1940.33 1940.28                                |
| 2x2 HUB |                       |                       | 3.12                  | 1942.15 <small>CORRECTED FOR .05 ERROR</small> |

SEPT 3, 1952

20" STUMP ~~1/2~~ ARCH 7-6 SOUTH ARCH RING  
 Rock BM SEE PAGE (31) ERROR ~~45~~  
 #4 BUT HUB ON TARGET LINE SOUTH DAM

(36)

## BUTTRESS # 6 (CONT)

STATION +  $\Delta$  - ELEV

L1020

1951.73

L1030

T.P. 11.96 1951.71 0.83 1939.75

L1040

L1046

L1050

L1060

L1070 1951.73

□

4.2 1947.69 1947.68

L1080

L1090

L1100

L1110

L1120

W ← → E

|                    |                    |                     |                    |
|--------------------|--------------------|---------------------|--------------------|
| 1951.7             | 1940.6             | X                   | 1974.6             |
| $\frac{3.1}{10}$   | $\frac{4.2}{7}$    | $\frac{4.4}{4}$     | $\frac{4.8}{0}$    |
| 48.6               | 47.5               | 36.2                | 35.8               |
| 1951.7             | 1940.6             | 37.6                | 47.4               |
| $\frac{3.0}{10}$   | $\frac{+6.8}{6.5}$ | $\frac{13.8}{12.5}$ | $\frac{10.2}{19}$  |
| 48.6               | 47.5               | 60.8                | 64.4               |
| 1951.7             | 1940.6             | 47.4                |                    |
| $\frac{3.6}{10}$   | $\frac{4.2}{6}$    | $\frac{2.8}{3.5}$   | $\frac{2.1}{0}$    |
| 48.1               | 49.5               | 37.8                | 38.5               |
| 1951.7             | 1940.6             | 41.4                | 50.2               |
| $\frac{+0.8}{5}$   | $\frac{+9.6}{7.5}$ | $\frac{10.6}{17}$   | $\frac{7.3}{22}$   |
| 48.1               | 49.5               | 64.0                | 67.3               |
| 1951.7             | 1940.6             | 41.4                |                    |
| $\frac{3.3}{10}$   | $\frac{3.9}{6}$    | $\frac{13.0}{4}$    | $\frac{11.9}{0}$   |
| 48.4               | 47.8               | 38.7                | 39.8               |
| 1951.7             | 1940.6             | 39.9                | 52.4               |
| $\frac{+0.7}{6}$   | $\frac{9.9}{15}$   | $\frac{6.5}{20}$    |                    |
| 48.4               | 47.8               | 64.7                | 68.1               |
| 1951.7             | 1940.6             | 52.4                |                    |
| $\frac{2.7}{10}$   | $\frac{3.8}{6}$    | $\frac{10.6}{4.5}$  | $\frac{11.1}{0}$   |
| 49.0               | 47.9               | 41.1                | 40.6               |
| 1951.7             | 1940.6             | 42.2                | 50.6               |
| $\frac{9.5}{5}$    | $\frac{1.7}{5.5}$  | $\frac{8.7}{14}$    | $\frac{6.3}{20}$   |
| 49.0               | 47.9               | 65.9                | 68.3               |
| 1951.7             | 1940.6             | 50.6                |                    |
| $\frac{4.1}{10}$   | $\frac{8.4}{5}$    | $\frac{10.8}{3}$    | $\frac{10.3}{0}$   |
| 47.6               | 42.3               | 40.9                | 41.4               |
| 1951.7             | 1940.6             | 45.2                | 51.7               |
| $\frac{6.5}{6.5}$  | $\frac{0.0}{7.5}$  | $\frac{7.6}{16.5}$  | $\frac{5.7}{21}$   |
| 47.6               | 42.3               | 67.0                | 68.9               |
| 1951.7             | 1940.6             | 51.7                |                    |
| $\frac{2.4}{10}$   | $\frac{3.2}{7}$    | $\frac{9.4}{4.3}$   | $\frac{8.2}{0}$    |
| 49.3               | 40.5               | 42.3                | 43.5               |
| 1951.7             | 1940.6             | 46.8                | 50.1               |
| $\frac{1.6}{10.5}$ | $\frac{12.0}{19}$  | $\frac{1.8}{22}$    |                    |
| 49.3               | 40.5               | 62.6                | 72.8               |
| 1951.7             | 1940.6             | 50.1                |                    |
| $\frac{2.4}{10}$   | $\frac{2.6}{9}$    | $\frac{7.3}{6}$     | $\frac{10.3}{0}$   |
| 49.3               | 49.1               | 44.4                | 41.4               |
| 1951.7             | 1940.6             | 41.4                | 45.1               |
| $\frac{6.6}{5.5}$  | $\frac{3.4}{8.5}$  | $\frac{6.8}{21.5}$  | $\frac{2.0}{24}$   |
| 49.3               | 49.1               | 67.8                | 72.6               |
| 1951.7             | 1940.6             | 45.1                |                    |
| $\frac{2.3}{10}$   | $\frac{2.5}{8}$    | $\frac{9.5}{4}$     | $\frac{10.1}{0}$   |
| 49.4               | 49.2               | 42.2                | 41.6               |
| 1951.7             | 1940.6             | 47.7                | 41.7               |
| $\frac{10}{8.5}$   | $\frac{9.3}{16}$   | $\frac{3.4}{21}$    |                    |
| 49.4               | 49.2               | 65.3                | 71.2               |
| 1951.7             | 1940.6             | 41.7                |                    |
| $\frac{2.0}{10}$   | $\frac{2.9}{5}$    | $\frac{9.4}{4}$     | $\frac{7.6}{0}$    |
| 49.7               | 48.8               | 42.3                | 44.1               |
| 1951.7             | 1940.6             | 48.2                | 52.2               |
| $\frac{+0.5}{7}$   | $\frac{7.2}{17}$   | $\frac{4.3}{20}$    |                    |
| 49.7               | 48.8               | 67.4                | 70.3               |
| 1951.7             | 1940.6             | 52.2                |                    |
| $\frac{1.9}{10}$   | $\frac{2.0}{5}$    | $\frac{7.1}{4.5}$   | $\frac{4.9}{0.15}$ |
| 49.8               | 49.7               | 44.6                | 46.8               |
| 1951.7             | 1940.6             | 50.8                | 53.7               |
| $\frac{+2.0}{9.5}$ | $\frac{9.6}{15}$   | $\frac{5.2}{18}$    |                    |
| 49.8               | 49.7               | 65.0                | 69.9               |
| 1951.7             | 1940.6             | 53.7                |                    |
| $\frac{1.2}{10}$   | $\frac{2.2}{6}$    | $\frac{6.7}{4.5}$   | $\frac{6.4}{0}$    |
| 50.5               | 49.5               | 45.0                | 45.3               |
| 1951.7             | 1940.6             | 47.1                | 55.7               |
| $\frac{+4.0}{6}$   | $\frac{11.0}{13}$  | $\frac{5.7}{15}$    |                    |
| 50.5               | 49.5               | 63.6                | 68.9               |
| 1951.7             | 1940.6             | 55.7                |                    |
| $\frac{2.0}{10}$   | $\frac{2.1}{8}$    | $\frac{6.7}{6.5}$   | $\frac{7.1}{0}$    |
| 49.7               | 49.6               | 45.0                | 44.6               |
| 1951.7             | 1940.6             | 47.3                | 51.6               |
| $\frac{4.4}{7}$    | $\frac{0.1}{11.5}$ | $\frac{9.7}{16}$    | $\frac{6.8}{21}$   |
| 49.7               | 49.6               | 64.9                | 67.8               |
| 1951.7             | 1940.6             | 51.6                |                    |

| (37) Setting    | T     | B        | M's    | Elev      |
|-----------------|-------|----------|--------|-----------|
| □               | 3.94  | 2090.53  |        | 2086.59   |
| T.P.            | 0.565 | 2078.175 | 12.92  | 2077.61   |
| T.B.M.          | 0.88  | 2066.77  | 12.285 | 2065.890  |
| T.P.            | 1.51  | 2055.51  | 12.77  | 2054.00 ✓ |
| T.B.M.          | 3.18  | 2045.70  | 12.99  | 2042.52   |
| T.P.            | 1.02  | 2032.71  | 13.01  | 2032.69 ✓ |
| Check           |       |          |        |           |
| <del>T.P.</del> |       | 8.9      | 7.50   | 2026.21   |
| T.P.            | 0.04  | 2021.07  | 12.68  | 2021.03 ✓ |
| T.B.M.          | 0.54  | 2013.68  | 6.85   | 2014.22 ✓ |
| T.P.            | 0.25  | 2000.93  | 13.00  | 2000.68 ✓ |
| Check           |       |          | 1.77   | 1999.16   |
| T.B.M.          | 2.77  | 1998.16  | 0.00   | 2000.93 ✓ |
| T.P.            | 4.16  | 1989.62  | 12.70  | 1985.46 ✓ |
| T.B.M.          | 0.69  | 1978.27  | 12.04  | 1977.58 ✓ |
| Check           |       |          | 4.09   | 1974.18   |
| Check           |       |          | 12.53  | 1965.72   |
| T.B.M.          | 11.89 | 1980.76  | 9.40   | 1968.87 ✓ |
|                 |       |          | 0.00   | 1980.76   |
| T.B.M.          | 0.73  | 1969.60  |        | 1968.87 ✓ |
| T.B.M.          | 3.09  | 1966.51  | 0.00   | 1969.60 ✓ |
| T.B.M.          | 1.12  | 1954.79  | 12.84  | 1953.67 ✓ |
| T.B.M.          | 0.58  | 1942.37  | 13.00  | 1941.79 ✓ |
| □               |       |          | 2.08   | 1940.29   |

See page 38

Oct. 31 - 1952

Dick - Level  
Dallas - Notes  
Doane - φ

Nail in road  
2x2 @ Tack @ Axis # D-2074  
1x2 near 17 Butt  
2x2 Hub @ Axis # D-1980  
Nail 20" S.W. of #16 Butt.  
2x2 Hub @ D-1920 on Axis (2026.20)  
Nail 6" N.W. of #15 Butt.  
P.K. in West Wall of #14 Butt. (2019.20)  
2" Pipe in #14-15 Ring  
2" Pipe in #14-15 Ring (1999.15)  
Mark on W/S #13 Butt. South Pilaster  
1" Iron Bar in #13-14 Ring  
2" Iron Pipe @ S. Base of #13 Butt. (1977.87)  
2" Iron Pipe in 12-13 Ring (1974.13)  
2" Iron Pipe 10" S.W. of #12 Butt. (1965.72)  
2" Iron Pipe in #12-13 Ring (1968.84)  
Mark on West Wall #12 Butt. 15" S. of S. Pilaster  
  
Mark on West Face #11 Butt. 15" S. of S. Pilaster  
2" Iron Pipe in #11-12 Ring (1953.67)  
Marks on W. Face #10 Butt. 10" N. of S. Pilaster  
Big rock 30" South of #10 Buttress (1940.28)



(38) 31-Oct, 1952 Continued from page 37

Page 37 for party

|              | +               | ∓        | -     | Elev.    |
|--------------|-----------------|----------|-------|----------|
|              |                 | 1942.37  |       |          |
| T.B.M.       | 2.14            | 1937.32  | 7.19  | 1935.18  |
|              |                 |          | 7.89  | 1929.43  |
| T.B.M.       | 0.22            | 1925.66  | 11.88 | 1925.44  |
| check        |                 |          | 8.20  | 1917.46  |
| T.B.M.       | 5.00            | 1918.98  | 11.68 | 1913.98  |
|              |                 |          | 0.00  | 1918.98  |
| T.B.M.       | 12.50           | 1925.405 | 6.075 | 1912.905 |
|              |                 |          |       |          |
| T.P.         | 11.625          | 1936.47  | 0.56  | 1924.845 |
| T.B.M.       | 12.76           | 1948.46  | 0.77  | 1935.70  |
| T.B.M.       | 12.83           | 1960.19  | 1.10  | 1947.36  |
| T.P.         | 12.99           | 1972.28  | 0.90  | 1959.29  |
| T.B.M. Check |                 |          | 7.68  | 1964.60  |
| T.B.M.       |                 |          | 2.58  | 1969.70  |
|              |                 |          |       |          |
| T.B.M.       | 11.43           | 1976.03  |       | 1964.60  |
| T.P.         | 9.40            | 1983.92  | 1.51  | 1974.52  |
| T.P.         | 10.54           | 1994.43  | 0.03  | 1983.89  |
| side shot    | <del>0.75</del> |          | 4.33  | 1990.10  |
| T.P.         | 10.32           | 2004.00  | 0.75  | 1993.68  |

See page 39

2" Iron Pipe 20' S.W. of #10 Butt. (1935.16)  
 Mark on W. Face #9 Butt. 2' So. of S. Pilaster  
 2" Iron Pipe 15' S.E. of #10 Butt. (1925.43)  
 2" Iron Pipe in #9-10 ring  
 2" Iron Pipe 15' S.W. #9 Butt  
 Mark on W. Wall #8 Butt. 20' S. of S. Pilaster  
 6" Eyelet @ Entrados near #8-9 Arch Ring

3-Oct, 1952

Stanley - ∓  
Dallas - ∓

5/8" Bolt on valve @ 4" pipe 50'± S.W. of #7 Butt.  
 Big rock on #7 Butt. @ L-1200±  
 Big rock in G-7 ring D-1395± @ L-1105±  
 1x2 hub #6 Butt @ L-900±  
 16" stump L-1020 @ D-1347 page 32 elev. 1964.51  
 2x2 Hub @ Tack L-1000 @ D-1332<sup>34</sup> page 32 el 1969.69

4-OCT, 1952

Dick - ∓  
Dallas - ∓

1x2 hub @ L-900± @ D-1300±  
 1x2 hub @ L-850± @ D-1250±  
 L-1000 @ D-1272<sup>36</sup> 2x2 Hub @ Tack  
 Big rock @ L-825± @ D-1215±

(39)

Continued from page 38

|                        | +    | ⌈       | -     | Elev.     |
|------------------------|------|---------|-------|-----------|
|                        |      | 2004.00 |       |           |
| T.B.M. 12.86           |      | 2013.99 | 2.87  | 2001.13   |
| T.B.M.<br>Stump        |      |         | 3.28  | 2010.71 ← |
| Stump                  |      |         | 6.94  | 2007.05 ← |
| Stump                  |      |         | 11.06 | 2002.93   |
| T.B.M. 3.10            |      | 2013.81 |       | 2010.71 ← |
| Check                  |      |         | 6.76  | 2007.05 ← |
| T.B.M. 12.84           |      | 2026.56 | 0.09  | 2013.72   |
| T.P.<br>T.B.M.<br>Rock | 6.07 | 2032.42 | 0.21  | 2026.35   |
|                        |      |         | 1.44  | 2030.98   |

4-Oct. 1952

Dick - ⌈  
Dallas - Notes of ⌘

(39)

2031.02

40 penny nail in  
8" Stump @ D-1225 ± & L-920 ±  
12" Stump @ D-1220 & L-990  
Nail in 12" Stump @ D-1222 & L-996  
Nail in 12" Stump @ D-1222 & L-950

6-Oct. 1952

Dallas - ⌈ & Notes  
Curley - ⌘

Boulder @ L-800 ± &amp; D-1140 ±

Big rock @ L-725 ± &amp; D-1080 ±







Final X-Sections #6 Buttress

| Sta.       | + | -      | Elev. |
|------------|---|--------|-------|
| L-1016.4   |   | 1934.0 |       |
| Bulkhead ↑ |   |        |       |

22-Dec.'52. # 5↑ (44)

| (1951.8) | East |      |      |      | West |      |      |      |
|----------|------|------|------|------|------|------|------|------|
| 6.3      | 4.7  | 3.8  | 3.2  | 0    | 1    | 1.2  | 3.6  | 4.4  |
| 4.4      | 6.2  | 7.9  | 9.4  | 9.7  | 9.4  | 8.3  | 8.0  | 4.3  |
| 47.4     | 27.8 | 26.1 | 24.6 | 24.3 | 24.6 | 25.5 | 26.0 | 29.5 |

(1951.8)  
4.7  
4.4  
47.4



12-31-52

| Sta | +   | -    | Elev. |
|-----|-----|------|-------|
| □   | 0.0 | 1940 | 1940  |

L-959

L-960.3

L-961

L-962.2

|     |        |        |
|-----|--------|--------|
| 4.0 | 1932.0 | 1928.0 |
|-----|--------|--------|

~~L-992.3~~  
~~L-992.3~~

L-1000

# 6 Buttress Excavation

(45)

(RE-XSECTION) West

Dick  
Dallas  
Ben  
Curley

Zero Section

(1940.0)

|       |      |      |
|-------|------|------|
| 0     | 1.2  | 4    |
| 2.5   | 0.1  | +0.5 |
| 937.5 | 39.9 | 40.5 |

(1940.0)

|      |        |      |      |
|------|--------|------|------|
| 3.0  | 0      | 1.6  | 4    |
| 3.5  | 5.4    | 5.9  | +0.5 |
| 34.6 | 1934.1 | 40.5 |      |

(1940.0)

|      |      |      |      |
|------|------|------|------|
| X 0  | 0.6  | 0.8  | 4    |
| 7.1  | 7.1  | 6.1  | 6.7  |
| 32.9 | 32.9 | 33.9 | 33.3 |

(1932.0)

|      |      |
|------|------|
| 0    | 4    |
| 10.7 | 10.2 |
| 21.3 | 21.8 |

(1932.0)

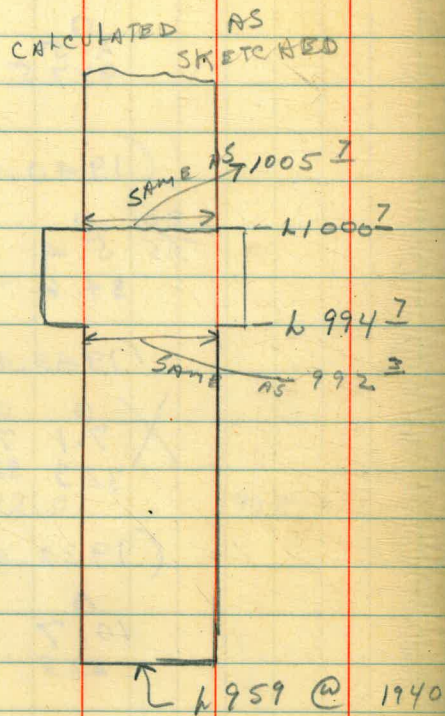
|      |      |
|------|------|
| 0    | 4    |
| 11.9 | 11.6 |
| 20.1 | 20.4 |

Cont'd page 46

12-31-'52

| Sta     | + $\pi$ | - Elev |
|---------|---------|--------|
| L-1005Z |         | 1932.0 |

L-1010



⊕ (1932.0) West

|      |      |
|------|------|
| 0    | 4.1  |
| 11.3 | 11.3 |
| 20.7 | 20.7 |

(1932.0)

|        |        |
|--------|--------|
| 0      | 4.1    |
| 6.6    | 8.5    |
| 1925.4 | 1923.5 |

102.54      102.54  
1923.5

46

✓



Sta. +  $\nabla$  — Elev.

□ 1.25 1965.85 1964.60

T.P. 0.44 1953.66 12.63 1953.22

T.B.M. 2.25 1951.41

T.B.M. 5.42 1952.32 6.76 1946.90

12.32 1940.00

Check 0.90 1951.42

T.P. 3.03 1942.76 12.59 1939.73

T.B.M. 2.45 1940.31

1940<sup>28</sup>

1-27-53

Dallas - Notes

Curley -  $\nabla$   
Ben -  $\nabla$

(47)

T.B.M. on #6 Butt.  $\nabla$  set elev. 1940 @ #6

See page 58

Nail & Tin in 16" stump @ L-1020 $\pm$  #D-1347 $\pm$

Small rock @ L-944 $\pm$  #D-1360 $\pm$

L & T #6 Butt. @ L-947 $\pm$  #D-1360

Big rock 7' West of #6 Butt. @ L-967 $\pm$

Mark on Bullhead @ L-1068 in Butt. #6 for Archie

Rock 25' $\pm$  S.E. of #7 Buttress form @ L-1108

Big Rock @ 10-11 Arch Ring Elev. 1940<sup>28</sup>



ADDITIONAL SECTIONS

SOUTH OF AXIS FROM D 1840 - D 2080  
FOR ORIGINAL GROUND TO PO.

| STA  | +                | π                 | -   | ELEV  |
|------|------------------|-------------------|---|---|
| □    | 6.6              | (2058.0)          | -   | 2051.4  |
| L    | 48.4             | 33                |   |   |
| 1070 | $\frac{0}{1.6}$  | $\frac{1.5}{6.7}$ | $\frac{30}{9.8}$  | $\frac{45}{13.3}$ } $\frac{82}{12.0}$                                     |
| L    |                  | (2058.0)          |   | (2050.0)  |
| 1090 | $\frac{0}{2.6}$  | $\frac{14}{5.0}$  | $\frac{25}{10.0}$   | $\frac{35}{12.4}$ $\frac{46}{16.9}$ } $\frac{72}{12.6}$ $\frac{91}{16.2}$ |
| L    |                  | (2058.0)          |   | (2050.0)  |
| 1110 | $\frac{0}{4.3}$  | $\frac{10}{7.2}$  | $\frac{22}{14.5}$ } $\frac{40}{12.2}$ $\frac{65}{16.1}$ } |   |
| L    | 4.0              | (2050.0)          | 12.0  | 2046.0 (2039.6)   |
| 1130 | $\frac{0}{4.3}$  | $\frac{10}{9.8}$  | $\frac{22}{12.7}$   | $\frac{25}{13.3}$ $\frac{62}{17.9}$ } $\frac{72}{11.1}$ $\frac{84}{12.0}$ |
| +    | (2050.0)         |                   | (2039.6)  |   |
| 1150 | $\frac{0}{11.2}$ | $\frac{35}{6.3}$  | $\frac{62}{12.4}$ $\frac{68}{13.8}$ } $\frac{113}{5.6}$   |   |
|      | 38 <sup>3</sup>  | 33 <sup>3</sup>   | 27.2 25 <sup>3</sup>                                      |   |
| +    | π                | -                 | ELEV  |   |
|      | 0.8              | 2039.6            | 11.2  | 2038.8  |
|      | 0.2              | 2027.4            | 12.4  | 2027.2  |
|      | 3.4              | 2017.8            | 13.0  | 2014.4  |
|      | 1.8              | 2009.1            | 10.5  | 2007.3  |
|      | 3.8              | 2011.7            | 1.2   | 2007.9  |
|      |                  |                   | 0.0   | 2011.7 (2012.0)   |

LOCKER π  
MAYSTED π  
WELLS π  
SOYSTER π

2-18-53 (49)

D 2080 = 0 = # 18 BUTTRESS

|  |          |  |  |
|--|----------|--|--|
| (2050.0)   | 2027.4   | THIS SHOT SHOULD BE<br>ALMOST THE SAME AS<br>D 1950 L 1070 TOPO<br>IN JULY '52 |  |
| $\frac{94}{144}$ $\frac{102}{15.8}$ } $\frac{130}{1.1}$  |          |  |  |
| (2027.4)   |          |  | SHOULD BE<br>SAME AS<br>D-1890<br>L 1070<br>(2009) |
| $\frac{115}{15.3}$ } $\frac{140}{2.7}$ $\frac{155}{6.4}$ $\frac{80}{10.3}$ $\frac{190}{14.4}$ }                  |          |  |  |
| (2039.6)   | (2027.4) |  |  |
| $\frac{82}{8.2}$ $\frac{97}{11.5}$ $\frac{107}{12.0}$ } $\frac{135}{4.2}$ $\frac{157}{8.4}$ $\frac{180}{12.7}$ } |          |  | $\frac{220}{1.1}$ $\frac{240}{6.0}$                |
| (2027.4)   | (2009.1) |  |  |
| $\frac{90}{13.0}$ } $\frac{120}{4.5}$ $\frac{150}{8.5}$ $\frac{180}{17.0}$ }                                     |          |  | $\frac{240}{11.0}$                                 |
| (2027.4)   | (2009.1) |  |  |
| $\frac{144}{10.7}$ $\frac{176}{16.0}$ }  |          |  | $\frac{240}{11.0}$                                 |



Blank lined page with four vertical red margin lines.

Blank grid page with a vertical red margin line on the left side.

Natural Trigonometrical Functions

Angle. Sin. Tan. Sec. Cosec. Cotg. Cosin.

|    |       |       |        |       |       |        |
|----|-------|-------|--------|-------|-------|--------|
| 0  |       |       |        |       |       | 0      |
| 32 | .5299 | .6249 | 1.1792 | 1.887 | 1.600 | .84805 |
| 10 | .5324 | .6289 | 1.1813 | 1.878 | 1.590 | .84650 |
| 20 | .5348 | .6330 | 1.1835 | 1.870 | 1.580 | .84495 |
| 30 | .5373 | .6371 | 1.1857 | 1.861 | 1.570 | .84339 |
| 40 | .5398 | .6412 | 1.1879 | 1.853 | 1.560 | .84182 |
| 50 | .5422 | .6453 | 1.1901 | 1.844 | 1.550 | .84025 |
| 33 | .5446 | .6494 | 1.1924 | 1.836 | 1.540 | .83867 |
| 10 | .5471 | .6536 | 1.1946 | 1.828 | 1.530 | .83708 |
| 20 | .5495 | .6577 | 1.1969 | 1.820 | 1.520 | .83549 |
| 30 | .5519 | .6619 | 1.1992 | 1.812 | 1.511 | .83389 |
| 40 | .5544 | .6661 | 1.2015 | 1.804 | 1.501 | .83228 |
| 50 | .5568 | .6703 | 1.2039 | 1.796 | 1.492 | .83066 |
| 34 | .5592 | .6745 | 1.2062 | 1.788 | 1.483 | .82904 |
| 10 | .5616 | .6787 | 1.2086 | 1.781 | 1.473 | .82741 |
| 20 | .5640 | .6830 | 1.2110 | 1.773 | 1.464 | .82577 |
| 30 | .5664 | .6873 | 1.2134 | 1.766 | 1.455 | .82413 |
| 40 | .5688 | .6916 | 1.2158 | 1.758 | 1.446 | .82248 |
| 50 | .5712 | .6959 | 1.2183 | 1.751 | 1.437 | .82082 |
| 35 | .5736 | .7002 | 1.2208 | 1.743 | 1.428 | .81915 |
| 10 | .5760 | .7046 | 1.2233 | 1.736 | 1.419 | .81748 |
| 20 | .5783 | .7089 | 1.2258 | 1.729 | 1.411 | .81580 |
| 30 | .5807 | .7133 | 1.2283 | 1.722 | 1.402 | .81412 |
| 40 | .5831 | .7177 | 1.2309 | 1.715 | 1.393 | .81242 |
| 50 | .5854 | .7221 | 1.2335 | 1.708 | 1.385 | .81072 |
| 36 | .5878 | .7265 | 1.2361 | 1.701 | 1.376 | .80902 |
| 10 | .5901 | .7310 | 1.2387 | 1.695 | 1.368 | .80730 |
| 20 | .5925 | .7355 | 1.2413 | 1.688 | 1.360 | .80558 |
| 30 | .5948 | .7400 | 1.2440 | 1.681 | 1.351 | .80386 |
| 40 | .5972 | .7445 | 1.2466 | 1.675 | 1.343 | .80212 |
| 50 | .5995 | .7490 | 1.2494 | 1.668 | 1.335 | .80038 |
| 37 | .6018 | .7536 | 1.2521 | 1.662 | 1.327 | .79864 |
| 10 | .6041 | .7581 | 1.2549 | 1.655 | 1.319 | .79688 |
| 20 | .6065 | .7627 | 1.2577 | 1.649 | 1.311 | .79512 |
| 30 | .6088 | .7673 | 1.2605 | 1.643 | 1.303 | .79335 |
| 40 | .6111 | .7720 | 1.2633 | 1.636 | 1.295 | .79158 |
| 50 | .6134 | .7766 | 1.2661 | 1.630 | 1.288 | .78980 |
| 38 | .6157 | .7813 | 1.2690 | 1.624 | 1.280 | .78801 |
| 10 | .6180 | .7860 | 1.2719 | 1.618 | 1.272 | .78622 |
| 20 | .6202 | .7907 | 1.2748 | 1.612 | 1.265 | .78442 |
| 30 | .6225 | .7954 | 1.2778 | 1.606 | 1.257 | .78261 |
| 40 | .6248 | .8002 | 1.2808 | 1.601 | 1.250 | .78079 |
| 50 | .6271 | .8050 | 1.2838 | 1.595 | 1.242 | .77897 |

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

Angle. Sin. Tan. Sec. Cosec. Cotg. Cosin.

|    |       |       |        |       |       |        |
|----|-------|-------|--------|-------|-------|--------|
| 0  |       |       |        |       |       | 0      |
| 39 | .6293 | .8098 | 1.2868 | 1.589 | 1.235 | .77715 |
| 10 | .6316 | .8146 | 1.2898 | 1.583 | 1.228 | .77531 |
| 20 | .6338 | .8195 | 1.2929 | 1.578 | 1.220 | .77347 |
| 30 | .6361 | .8243 | 1.2959 | 1.572 | 1.213 | .77162 |
| 40 | .6383 | .8292 | 1.2991 | 1.567 | 1.206 | .76977 |
| 50 | .6406 | .8342 | 1.3022 | 1.561 | 1.199 | .76791 |
| 39 | .6428 | .8391 | 1.3054 | 1.556 | 1.192 | .76604 |
| 10 | .6450 | .8441 | 1.3086 | 1.550 | 1.185 | .76417 |
| 20 | .6472 | .8491 | 1.3118 | 1.545 | 1.178 | .76229 |
| 30 | .6494 | .8541 | 1.3151 | 1.540 | 1.171 | .76041 |
| 40 | .6517 | .8591 | 1.3184 | 1.535 | 1.164 | .75851 |
| 50 | .6539 | .8642 | 1.3217 | 1.529 | 1.157 | .75661 |
| 41 | .6561 | .8693 | 1.3251 | 1.524 | 1.150 | .75471 |
| 10 | .6583 | .8744 | 1.3284 | 1.519 | 1.144 | .75280 |
| 20 | .6604 | .8796 | 1.3318 | 1.514 | 1.137 | .75088 |
| 30 | .6626 | .8847 | 1.3352 | 1.509 | 1.130 | .74896 |
| 40 | .6648 | .8899 | 1.3386 | 1.504 | 1.124 | .74703 |
| 50 | .6670 | .8952 | 1.3421 | 1.499 | 1.117 | .74509 |
| 42 | .6691 | .9004 | 1.3456 | 1.494 | 1.111 | .74314 |
| 10 | .6713 | .9057 | 1.3492 | 1.490 | 1.104 | .74120 |
| 20 | .6734 | .9110 | 1.3527 | 1.485 | 1.098 | .73924 |
| 30 | .6756 | .9163 | 1.3563 | 1.480 | 1.091 | .73728 |
| 40 | .6777 | .9217 | 1.3600 | 1.476 | 1.085 | .73531 |
| 50 | .6799 | .9271 | 1.3636 | 1.471 | 1.079 | .73333 |
| 43 | .6820 | .9325 | 1.3673 | 1.466 | 1.072 | .73135 |
| 10 | .6841 | .9380 | 1.3711 | 1.462 | 1.066 | .72937 |
| 20 | .6862 | .9435 | 1.3748 | 1.457 | 1.060 | .72737 |
| 30 | .6884 | .9490 | 1.3786 | 1.453 | 1.054 | .72537 |
| 40 | .6905 | .9545 | 1.3824 | 1.448 | 1.048 | .72337 |
| 50 | .6926 | .9601 | 1.3863 | 1.444 | 1.042 | .72136 |
| 44 | .6947 | .9657 | 1.3902 | 1.440 | 1.036 | .71934 |
| 10 | .6967 | .9713 | 1.3941 | 1.435 | 1.030 | .71732 |
| 20 | .6988 | .9770 | 1.3980 | 1.431 | 1.024 | .71529 |
| 30 | .7009 | .9827 | 1.4020 | 1.427 | 1.018 | .71325 |
| 40 | .7030 | .9884 | 1.4061 | 1.422 | 1.012 | .71121 |
| 50 | .7050 | .9942 | 1.4101 | 1.418 | 1.006 | .70916 |
|    | .7071 | 1.    | 1.414  | 1.414 | 1.    | .70711 |

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

NORTH FACE

2068.50 = L996.0

S = .125

2002.32 = L987.73

S = 0.40

1976.27  
5.43

1970.84

1.28  
1.16  
2.44

1.53

2096.2  
1943.00  
157.20  
163.20

174  
163

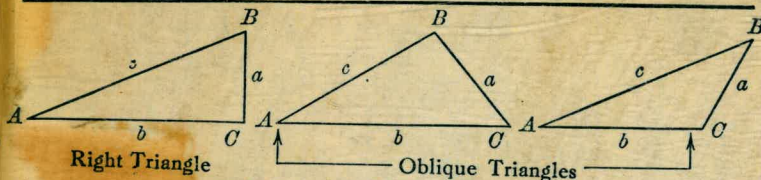
14  
60  
1840 840  
120 1120  
2020 1960  
120.01  
118.85  
1.16

1951.6  
975.3  
2 5  
5  
1968.94  
1967.78  
2.0  
1.16

2070

2070  
2070  
2070  
2070  
2070  
2070  
2070  
2070

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

For Angle A.  $\sin = \frac{a}{c}$ ,  $\cos = \frac{b}{c}$ ,  $\tan = \frac{a}{b}$ ,  $\cot = \frac{b}{a}$ ,  $\sec = \frac{c}{a}$ ,  $\operatorname{cosec} = \frac{c}{b}$

| Given | Required | Formulas  |
|-------|----------|---|
| a, b  | A, B, c  | $\tan A = \frac{a}{b} = \cot B$ , $c = \sqrt{a^2 + b^2} = a\sqrt{1 + \frac{b^2}{a^2}}$  |
| a, c  | A, B, b  | $\sin A = \frac{a}{c} = \cos B$ , $b = \sqrt{(c+a)(c-a)} = c\sqrt{1 - \frac{a^2}{c^2}}$ |
| A, a  | B, b, c  | $B = 90^\circ - A$ , $b = a \cot A$ , $c = \frac{a}{\sin A}$                            |
| A, b  | B, a, c  | $B = 90^\circ - A$ , $a = b \tan A$ , $c = \frac{b}{\cos A}$                            |
| A, c  | B, a, b  | $B = 90^\circ - A$ , $a = c \sin A$ , $b = c \cos A$                                    |

Solution of Oblique Triangles

| Given      | Required | Formulas   |
|------------|----------|--|
| A, B, a    | b, c, C  | $b = \frac{a \sin B}{\sin A}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$  |
| A, a, b    | B, c, C  | $\sin B = \frac{b \sin A}{a}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$  |
| a, b, C    | A, B, c  | $A + B = 180^\circ - C$ , $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$<br>$c = \frac{a \sin C}{\sin A}$                                     |
| a, b, c    | A, B, C  | $s = \frac{a + b + c}{2}$ , $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$<br>$\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$ , $C = 180^\circ - (A + B)$ |
| a, b, c    | Area     | $s = \frac{a + b + c}{2}$ , $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$  |
| A, b, c    | Area     | $\text{area} = \frac{bc \sin A}{2}$  |
| A, B, C, a | Area     | $\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$   |

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle =  $5^\circ 10'$ . From Table, Page IX.  $\cos 5^\circ 10' = .9959$ . Horizontal distance =  $319.4 \times .9959 = 318.09$  ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained.  $\text{Cosine } 5^\circ 10' = .9959$ .  $1 - .9959 = .0041$ .  $319.4 \times .0041 = 1.31$ .  $319.4 - 1.31 = 318.09$  ft.

When the rise is known, the horizontal distance is approximately: - the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance =  $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$  ft.