

W 889

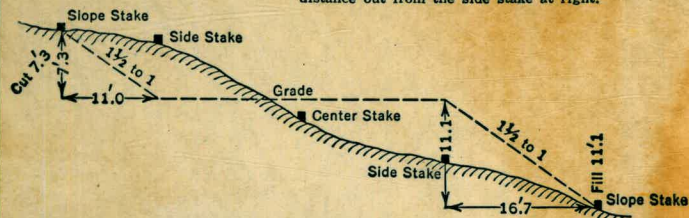
ARCH

DATA



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING**  
 Roadway of any Width. Side Slopes  $1\frac{1}{2}$  to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

ARCH RING X-SECTIONS

8-52  
HRS

ORIGINAL X-SECTION S

8-52

REPRODUCED FROM  
 U.S. GOVERNMENT PRINTING OFFICE  
 1917

The paper in this book No. F364A  
 is made of 50% high grade rag stock  
 with a WATER RESISTING surface sizing.

11.377-1. c. x. yk. chss.

## INDEX

PAGE					
1	ARCH	14-15	GRID		
2	"	15-16	REF.		
6		13-14	REF		
10		13-12	REF		
13		11-12	REF		
16	CONE	CUT OFF	TRAVERSE	11-12	
17	"	"	"	11-10	
18	ARCH	10-11	GRID		
19		11-12	GRID		
20		12-13	GRID		
21		13-14	GRID		
22		16-17	GRID		
23		1-2	GRID		
24		2-3	GRID		
25		3-4	GRID		
26		4-5	GRID		
27		5-6	GRID		
28		14-15	GRID		
29		6-7	GRID		
30		9-10	GRID		
31		8-9	GRID		
32		7-8	GRID		
	SEE CITY BOOK 798	15-16	(CITY'S NOTES FOR GRID LAYOUT)		

PAGE

33-38 - CHECK OF ARCH CUT OFFS

The right page of the notebook features a grid of 20 columns and 20 rows. A vertical red margin line is positioned on the right side of the grid, approximately one-fifth of the way from the right edge. The grid is drawn with light blue lines on a cream-colored background.

①

X-SECTION ARCH 14-15

D 1840

D 1850

D 1860

D 1870

D 1880

D 1890

D 1900

SOUTH

BASE

LINE

L 1075

(N &amp; SOUTH)

NORTH

H.I. 2013.60

$\frac{9.1}{26}$	$\frac{13.1}{8.7}$	$\frac{12.6}{4.5}$	$\frac{19.9}{1.0}$
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$\frac{9.1}{25.8}$	$\frac{10.2}{15.1}$	$\frac{17.4}{13.0}$	$\frac{17.8}{6.7}$	$\frac{15.2}{5}$	$\frac{10.4}{0}$	$\frac{9.9}{2.0}$	$\frac{10.5}{10}$
--------------------	---------------------	---------------------	--------------------	------------------	------------------	-------------------	-------------------

$\frac{6.0}{25.4}$	$\frac{6.0}{21.8}$	$\frac{5.0}{19}$	$\frac{16.3}{13.9}$	$\frac{12.8}{13.0}$	$\frac{4.4}{3.0}$	$\frac{4.3}{0}$	$\frac{3.4}{10}$
--------------------	--------------------	------------------	---------------------	---------------------	-------------------	-----------------	------------------

$\frac{2.0}{2.3}$	$\frac{12.4}{18}$	$\frac{12.9}{13.0}$	$\frac{15.4}{12.5}$	$\frac{7.4}{5}$	$\frac{6.8}{0}$	$\frac{0.5}{10}$
-------------------	-------------------	---------------------	---------------------	-----------------	-----------------	------------------

H.I. 2018.86

$\frac{6.7}{19.8}$	$\frac{15.9}{12.5}$	$\frac{16.0}{8.0}$	$\frac{12.0}{6.5}$	$\frac{6.3}{0}$	$\frac{5.5}{10}$
--------------------	---------------------	--------------------	--------------------	-----------------	------------------

$\frac{4.7}{13.5}$	$\frac{4.8}{9.0}$	$\frac{12.9}{5.3}$	$\frac{4.7}{13.5}$	$\frac{4.8}{9.0}$	$\frac{12.9}{5.3}$	$\frac{13.1}{4.0}$	$\frac{9.8}{6.0}$	$\frac{4.4}{15}$	$\frac{4.1}{20}$
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H.I. 2019.02

$\frac{0.5}{10}$
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Tbn 2018.99

0.37

H.I. 2018.86

-11.83

Tbn 2007.03

+6.57

H.I. 2013.60

-0.73

2012.99

6.05

H.I. 2019.02

(2)

X-SECTION

ARCH 15-16

TRANSIT  
@ D1930  
L1050

HORZ $\angle$	HORZ DIST	ROD	ELEV
115°	15'	5.4	
	21'	7.4	
	30.5'	16.9	
	26.0	16.6	
	30.0	17.6	
	31.0	16.0	
	35.0	17.0	
	38.0	19.2	
	41.0	20.6	
	42.0	19.8	
	47.0	17.0	
	54.0	14.0	
	58.0	14.8	
127°	8.0	3.9	
	13.0	4.7	
	20.0	6.7	
	25.0	13.5	
	26.0	22.5	
	28.0	41.0	
	28.0	17.0	
	32.0	11.2	
	38.0	11.6	
	42.5	12.1	
	39.0	11.4	2016.3

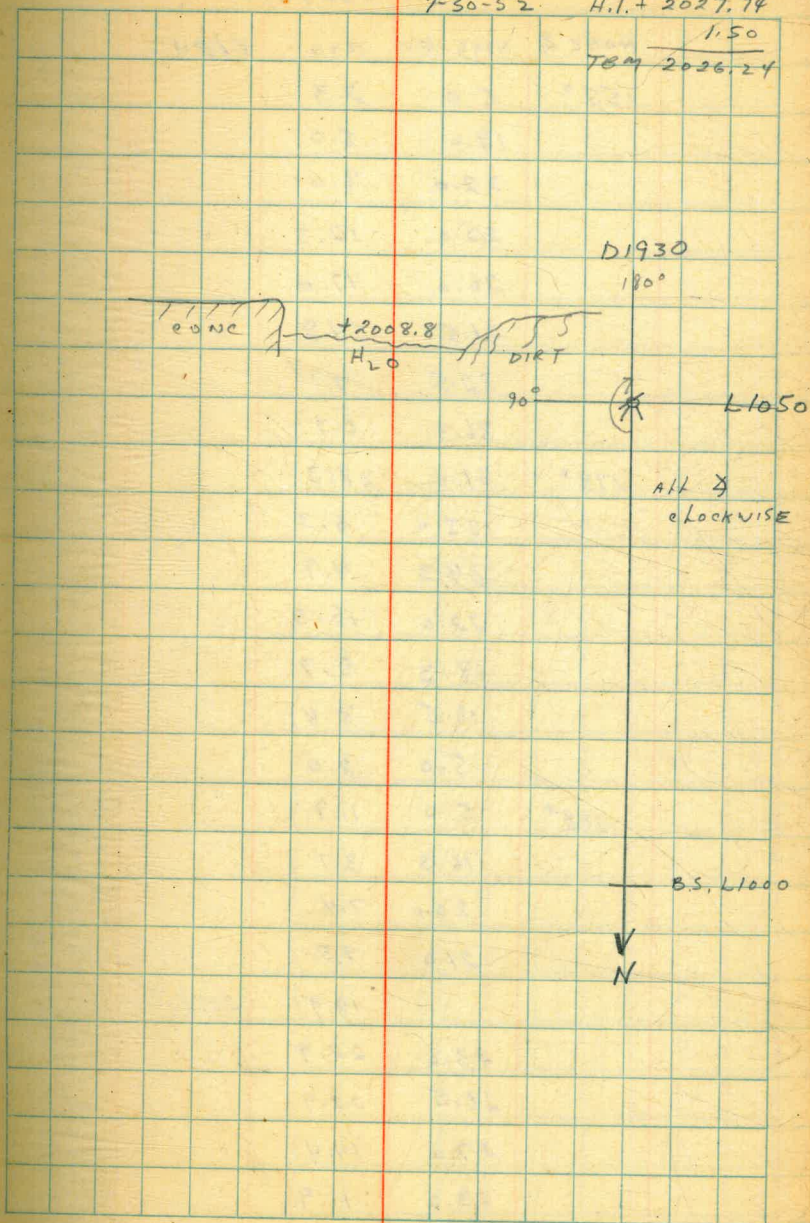
TBM 2026.20

+5 1.54

7-30-52 H.I. + 2027.74

1.50

TBM 2036.24



(3)

ARCN 15-12

H.1 2027.74

HORZ $\theta$	HORZ DIST	ROD	ELEV
155°	5.0	2.3	
	18.0	5.0	
	22.0	9.0	
	25.0	12.3	
	26.0	47.0	
	31.5	54.8	
	32.5	7.1	
	36.3	6.7	
178°	31.0	38.3	
	33.0	5.3	
	34.3	4.9	
	22.0	10.3	
	18.3	5.7	
	16.5	3.4	
	5.0	2.0	
188°	5.0	1.9	
	16.3	3.1	
	20.0	7.4	
	21.0	9.5	
		18.9	2008.8
	23.0	22.9	
	26.5	22.9	
	27.0	14.4	
	23.0	11.9	

④

ARCH 15-16

H.I. 2027.74

HORZ $\angle$	HORZ DIST	R.O.O	ELEV
214°	36.0	0.6	
	31.7	0.2	
	29.7	1.1	
	24.5	9.0	
	22.5	9.7	
	20	8.0	
	14.5	2.0	
	4.0	1.5	
	H.I. 2034.52		
244°	10.0	7.4	
	5.0	7.9	
	15.0	6.5	
	19.0	11.4	
	21.0	12.4	
	24	10.8	
	27.5	3.9	
	34.9	3.2	
	49.0	2.2	2032.3
257°	41.7	1.8	
	34.5	2.1	
	28.8	3.2	
	27.0	7.9	
	25	9.9	
	22	11.4	



⑤

ARCH 15-16

H.I. 2034.52

HORZ &	H. DIST	ROD	ELEV
257°	20	10.6	
	16	5.7	
	10	6.8	
	5	7.7	
270°	5	7.5	
	10	6.4	
	18	5.0	
	22	10.4	
	25	10.6	
	27.5	9.7	
	30	3.5	
	33.2	3.0	
	31	7.6	
	39	8.0	
	42	7.3	
	48	11.5	

⑥

ARCH 13-14.

HOKZ $\angle$	HOKZ DIST	ROD	ELEV
110°	13	+2.0	
	17	0.9	
	19	3.1	
	24.5	6.5	
	25.2	1.12	
	28.0	0.83	
	36.3	3.18	
133°	62.0	16.9	
	52.0	15.6	
	50.0	14.1	
	44.0	14.9	
	33.0	13.9	
	31.5	8.3	
	29.0	6.5	
	19.0	+1.0	
146°	25.0	+1.5	
	30.0	2.6	
	36.0	10.1	
	39.5	10.5	
	43.0	7.2	
	47.0	6.1	
	55.0	6.3	
180°	50.0	+2.1	
	43.0	+2.5	

H.I. 1991.36  
-5.01TBM 1997.14  
8.93

TBM 1991.35

H.I. 2006.07

D 1810

180

90 ~~X~~ L1069.60

B.S X L980

0°

V  
N

⑦

	ARC M	13-14	
	H.I.	1991.36	
Horz S	H. DIST	R.O.D	ELEV
180°	41.0	2.5	
	39.0	3.8	
	38.5	5.4	
	35.0	5.1	
	31.0	2.1	
	29.0	+4.7	
205°	29.5	1.0	
	31.5	1.7	
	H.I.	2006.07	
	34.0	14.0	
	36.0	14.3	
	40.8	6.5	
	43.6	5.5	
	22.0	7.5	
244°	19.0	5.3	
	25.0	11.7	
	26.0	13.0	
	29.0	13.5	
	31.9	5.5	
	39.0	4.1	
258°	22.0	4.9	
	26.5	12.0	
	31.5	12.0	
	38.0	10.6	
	40.0	7.1	

⑧

ARCH 13-14

H.I. 2006.07

HORZ $\angle$	H. DIST	R.O.	ELEV
270°	45.0	72.2	
	55.0	75.4	
	37.0	3.6	
	36.0	6.5	
	30.0	5.29	
	23.0	6.0	
258°	9.0	2.4	
	16.0	4.3	
	18.0	4.2	
	14.0	2.0	
	9.0	2.7	
	3.0	0.5	
244°	0.0	1.2	
	4.0	2.0	
	9.0	2.5	
	13.0	1.5	
205°	17.0	4.3	
	4.0	1.4	
	9.0	2.8	
	17.0	6.1	
180°	4.0	1.6	
	9.0	3.7	
	15.0	4.4	
	20.0	8.5	

(9)

ARCH 13-14  
H.I. 2006.07

HORZ $\angle$	H. DIST	ROD	ELEV
146°	8.0	5.7	
	16.0	10.6	
133°	12.0	9.3	
110°	10.0	9.4	

(10)

## X-SECTION ARCH 13-12

3 OYSTER  
LOCKED  
HADLEY  
ASH

		H.I. 1986.65		
1	HORZ &	H. DIST	POD	ELEV
	256°	15	2.9	
		23	3.1	
		24.2	4.5	
		26.8	3.36	
		34.5	3.96	
		36.0	5.4	
		38.8	2.9	
		42.0	1.7	
	237°	17.0	2.6	
		23.0	2.7	
		28.0	10.2	
		34.0	10.2	
		39.0	7.3	
		41.0	5.3	
		43.0	2.6	
		44.0	2.1	
		47.0	+0.4	
	220°	46.8	1.5	
		40.0	2.3	
		37.0	8.1	
		33.0	9.7	
		32.0	11.1	
		24.0	3.1	
		19.0	2.6	

7-31-52

BM 1988.29

-57.64

H.I. 1986.65

-5 11.46

1975.19

+5 0.66

H.I. -1975.85

180

01756

L. 1081.0090 ~~270~~\* 85.  
1980

V

N

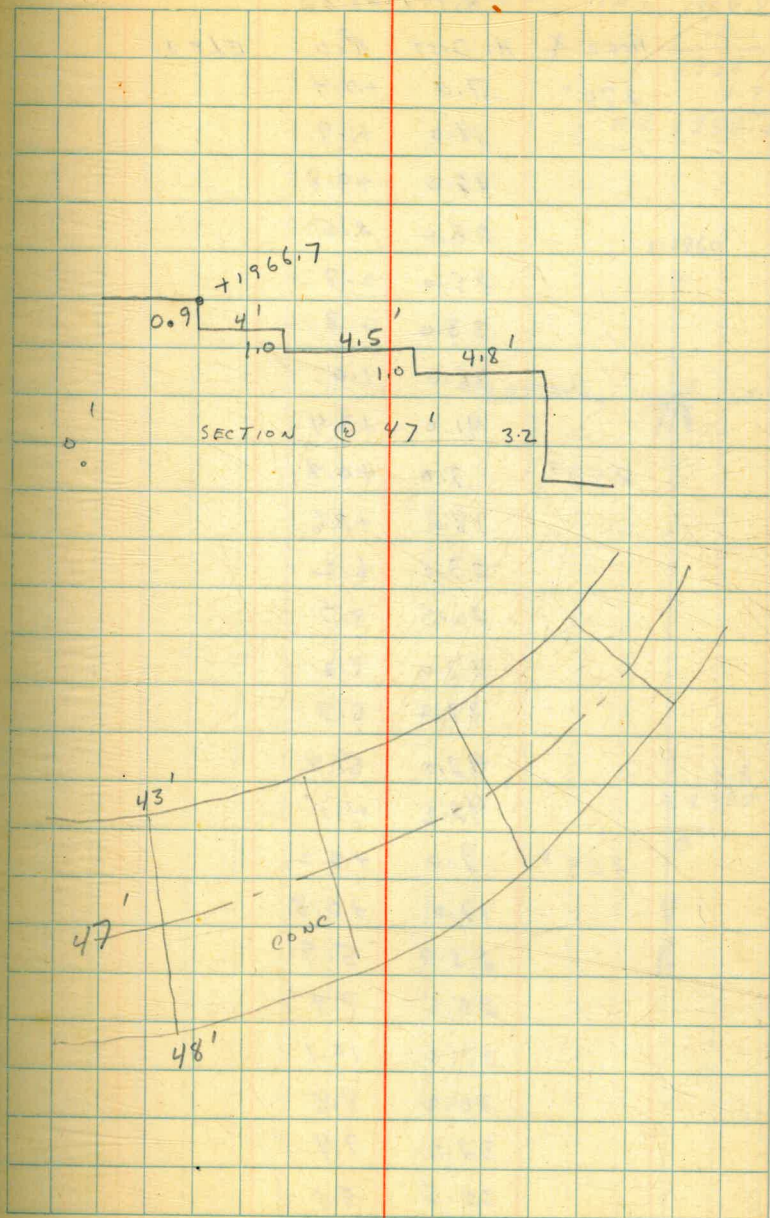
(11)

HORZ $\angle$	#	ARCH H.I. 1986.65 DIST R.O	ELEV
220°	14.0	3.1	
	0.0	5.0	
200°	16.0	3.6	
	26.5	4.7	
	34.0	13.4	
	38.0	12.8	
	39.0	9.8	
	47.0	3.8	
180°	52.0	2.3	
	55.8	8.8	
	49.7	9.2	
	41.0	16.6	
	30.0	7.0	
162°	20.0	5.3	
	20.0	7.5	
	25.0	7.8	
146°	31.0	10.3	
	27.0	10.7	
	16.0	8.6	
133°	27.0	10.8	
	17.0	9.2	
H.I. 1975.85			
162°	43.0	9.1	
	48.0	9.1	
	60.0	1.9	

(12)

 ARCH 13-12  
 H.I. 1975.85

H&RZ $\angle$	H. DIST	R.O.	ELEV
162°	67.0	1.6	
146°	37.0	7.6	
	38.0	10.9	
	41.0	12.3	
	48.0	12.5	
	53.0	12.0	
	61.6	4.3	
	68.0	4.8	
	76.0	5.1	
133°	32.0	9.4	
	38.0	11.7	
	44.0	15.0	
	49.5	15.6	
	49.6	16.3	
	53.0	16.3	





(13)

ARCH 11-12

H.I. 1968.83

HORZ $\times$	H. DIST	R.O.	ELEV
270°	7.0	+0.4	
	18.0	+1.9	
	22.0	+0.8	
	23.0	2.5	
	25.0	0.8	
	33.0	0.3	
	36.0	1.0	
	41.0	+3.4	
247°	7.0	+0.4	
	18.0	+1.6	
	23.0	6.2	
	26.5	8.7	
	37.0	8.2	
	37.2	5.3	
	42.0	5.2	
	42.2	4.1	
225°	9.0	+0.2	
	17.0	+0.8	
	23.0	5.9	
	25.5	7.9	
	27.0	10.1	
	30.0	8.8	
	32.0	7.4	
	32.5	5.1	

TBM 1968.30

0.53

7-31-52

H.I. 1968.83

12.12

1956.71

1.77

H.I. 1958.48

D1960

180

L1125.2490

270

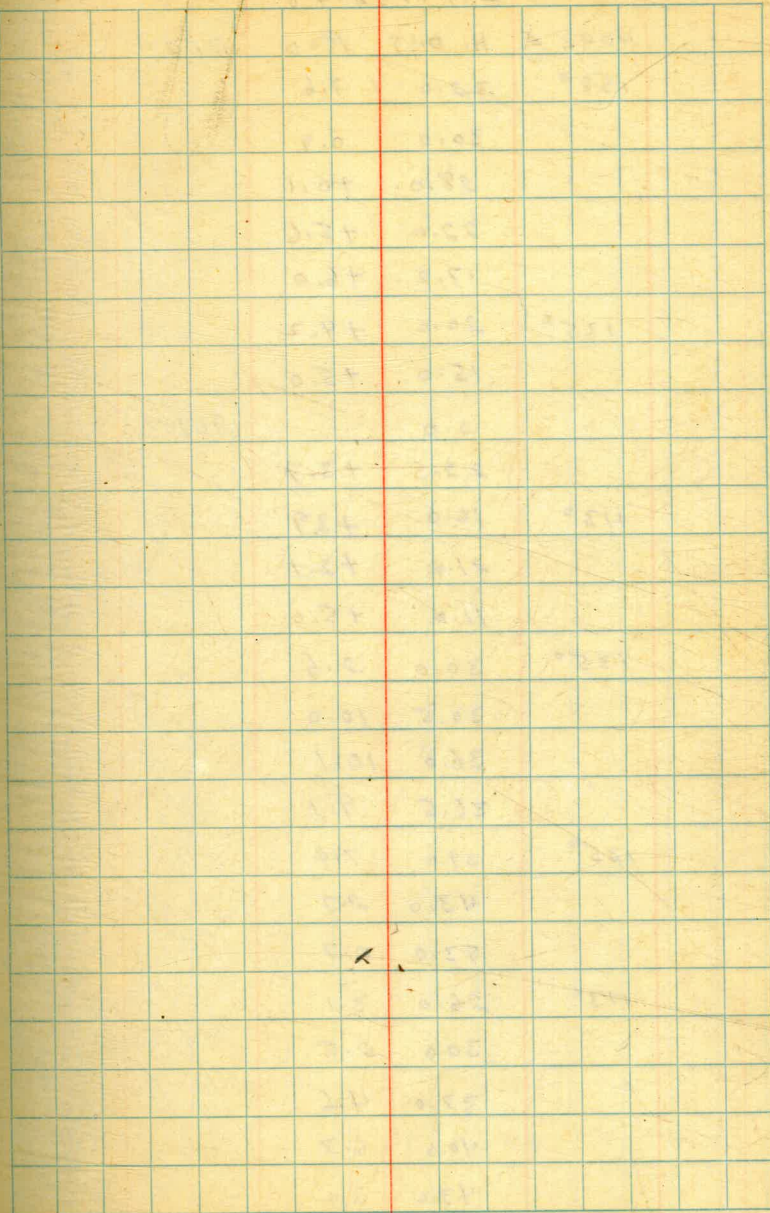
8.5  
X 1980

0°

V  
N

(14)

	ARCH 11-12		
	H.I. 1968.83		
HORZ $\angle$	H. DIST	R.O.D	ELEV
225°	39.6	+2.0	
	44.7	+4.5	
202°	43.8	+1.8	
	49.0	+2.2	
	42.2	+1.2	
	37.0	5.2	
	31.0	10.0	
	38.0	11.3	
	26.0	8.7	
	22.0	4.1	
	19.0	0.5	
	8.0	1.2	
180°	10.0	1.3	
	20.0	2.2	
	28.0	9.6	
	31.0	14.9	
	37.0	14.5	
	40.0	4.1	
	42.8	1.1	
	45.6	+0.7	
	51.0	+0.3	
158°	55.0	2.0	
	45.4	3.4	
	H.I. 1958.48		
	40.0	8.1	



(15)

ARCH 11-12

H.I. 1958.48

HORZ $\angle$	H. DIST	R.O.D	ELEV
158°	32.0	7.6	
	30.0	0.9	
	28.0	+0.1	
	22.0	+5.6	
	17.0	+6.0	
135°	20.0	+4.2	
	15.0	+5.0	
	0.0		1967.30
	22.5	+3.7	
113°	16.0	+3.9	
	21.0	+2.1	
	11.0	+5.0	
135°	30.0	2.6	
	30.5	10.0	
	36.0	10.1	
	36.5	9.1	
135°	39.0	7.4	
	43.0	2.7	
	53.0	0.7	
113°	26.0	3.1	
	30.0	2.5	
	37.0	4.6	
	40.0	6.3	
	43.0	3.1	
	48.0	3.6	

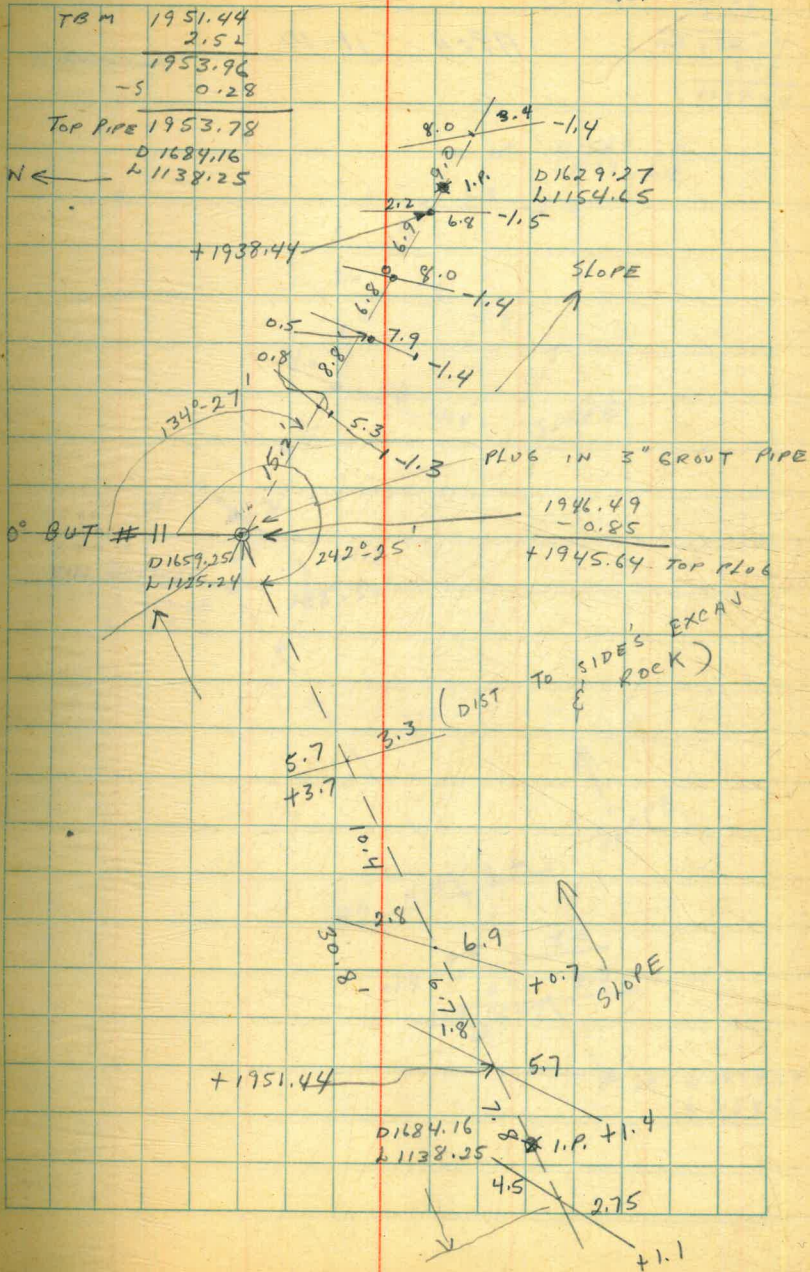
16

CONC CUT OFF LOCATIONS  
BY TRAVERSE

ARCH 11-12

JOYSTER  
LOCKER  
HARDLEY  
ASH

8-1-52



(17)

ARCH 11-10

BM Rock 1940.28

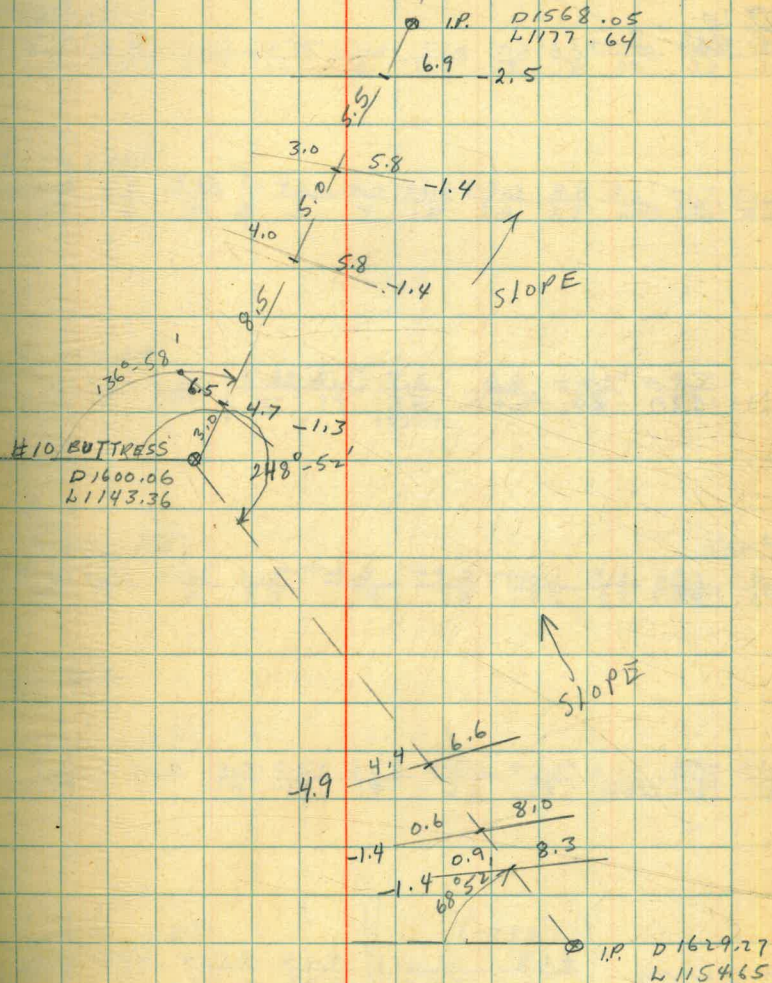
6.21

11.1 1946.47

8.05

1938.44

N ←



(18)

Arch Ring # 10 - # 11 - D-1600 - 1660

Sta.

+

+  $\Delta$  -

Elev.

D

3.20 1943.48

1940.28

D/G 10

D-1620

D-1630

D-1640

D-1650

D-1660

T.P.

11.56

1954.90

0.14

1943.24

T.P.

3.60

1958.10

0.40

1954.50

8 Aug. '52

X-Section of Arch Rings

(18)

South

Clyde Tape

Dallas -  
Stanley  
Dave

North

Base line = L-1154.65 @ 1 Pipe

L-1165

Bench on top of rock 5/8 Arch Ring 10-11 @ D-1620

(1943.48)

5.3	4.7	4.5	10.73	10.75	15.64	15.64	7.3	2.2	1.4	2.8	8.8
15	10	0	0.7	10	10	11.5	12	18	30	33	36

(1943.48)

7.6	6.5	4.9	9.22	9.21	4.0	+2.5	+3.0	8.8	8.2	+1.7	+1.5
30	18	8	5	3	7	15	24	27	44	46	50

(1943.48)

5.8	7.7	7.0	6.43	6.43	5.5	9.6	6.8	+4.5	+1.7
30	18	5	5	5	19	28	44.5	48	52

1933.9

(1943.48)

5.09	5.09	3.42	2.35	2.15	+4.0	+9.3	+10.1	0.1	+8.0	+8.0
4	3	3	7	10	14	20	26	37	49	52

5.09  
0.1

(1943.48)

+6.9	+2.0	2.00	2.0	0.57	0.57	+5.2	+11.5	+11.6	+9.0	+11.6
10	0	11	17	17	19	22	33	44	47	51

(1943.48)

+17.0	+16.5	+18.9	+7.3	+1.7	13.20	8.28
3	0	9	23.5	24.5	29.5	35

(1958.10)

① Arch Ring # 11-12. D-1660-1720

Sta. +  $\nabla$  - Elev.  
1958.10

D-1670  
T.P. 10.41 1968.44  $\frac{0.07}{0.03}$  1958.03

D-1680

D-1690

D-1700

D-1710

D-1720

8-Aug. '52 Same party as page 18

X-Sections (1958.10) North

Base line = 6-1154.65

(1968.44) (1958.10) (1968.44)  
 $\frac{2.1}{5} \frac{4.9}{13} \frac{8.5}{17} \frac{9.2}{19} \frac{9.2}{28} \frac{4.0}{28} \frac{8.7}{39}$

(1958.10)  
 $\frac{1.3}{7} \frac{2.0}{10} \frac{5.7}{12} \frac{6.8}{16} \frac{6.4}{20} \frac{3.3}{22} \frac{4.1}{32} \frac{4.5}{38}$

(1958.10)  
 $\frac{+0.6}{6} \frac{0.9}{9} \frac{3.7}{12} \frac{4.5}{20} \frac{0.0}{22} \frac{1.9}{31} \frac{1.9}{35}$

(1968.44)  
 $\frac{+1.5}{8} \frac{+1.2}{10} \frac{8.9}{17} \frac{10.6}{23} \frac{8.8}{27} \frac{1.8}{34} \frac{+0.6}{36}$

(1968.44)  
 $\frac{+2.4}{11} \frac{+2.0}{15} \frac{5.8}{25} \frac{9.7}{32} \frac{6.8}{39} \frac{+0.6}{50}$

(1968.44)  
 $\frac{+4.8}{12} \frac{+4.4}{21} \frac{4.9}{31.5} \frac{8.18}{31.5} \frac{8.26}{44} \frac{2.66}{50}$

Note all shots were taken North of Base line

$\frac{9.2}{1.2}$   
+7.8

(20) Arch. Ring # 12-13 = D-1720-1780  
 Sta. +  $\nabla$  - Elev.  
 1968.44

D-1730

T.B.M. 11.09 1978.87 0.66 1967.78  
 T.P.

D-1740

D-1750

D-1760

D-1770

D-1780

T.P. 11.26 1988.27 1.86 1977.01

T.B.M. 5.38 1982.89 (1982.87)

8-Aug '52 Same Party as page 18  
 X-Sections

Base line = L-115465 North

(1868.44)  
 $\begin{array}{r} +5.9 \\ 14 \end{array}$   $\begin{array}{r} +5.5 \\ 18 \end{array}$   $\begin{array}{r} 0.1 \\ 24 \end{array}$   $\begin{array}{r} 3.2 \\ 30 \end{array}$   $\begin{array}{r} 4.1 \\ 37 \end{array}$   $\begin{array}{r} 0.6 \\ 43 \end{array}$   $\begin{array}{r} +6.5 \\ 54 \end{array}$   $\begin{array}{r} +7.1 \\ 60 \end{array}$

Concrete on rock near Arch @ D-1741 = L-1121 + @ Iron pipe

(1868.44)  
 $\begin{array}{r} +7.3 \\ 76 \end{array}$   $\begin{array}{r} +7.0 \\ 20 \end{array}$   $\begin{array}{r} +2.4 \\ 24 \end{array}$   $\begin{array}{r} 1.0 \\ 29 \end{array}$   $\begin{array}{r} 1.2 \\ 33 \end{array}$   $\begin{array}{r} +7.6 \\ 44 \end{array}$   $\begin{array}{r} +9.2 \\ 49 \end{array}$

(1978.87)  
 $\begin{array}{r} 0.8 \\ 20 \end{array}$   $\begin{array}{r} 1.5 \\ 24 \end{array}$   $\begin{array}{r} 5.7 \\ 28 \end{array}$   $\begin{array}{r} 8.7 \\ 33 \end{array}$   $\begin{array}{r} +0.5 \\ 43 \end{array}$   $\begin{array}{r} +1.2 \\ 46 \end{array}$

(1978.87)  
 $\begin{array}{r} +1.5 \\ 23 \end{array}$   $\begin{array}{r} +1.0 \\ 28 \end{array}$   $\begin{array}{r} 2.9 \\ 32 \end{array}$   $\begin{array}{r} 6.2 \\ 38 \end{array}$   $\begin{array}{r} 5.3 \\ 39 \end{array}$   $\begin{array}{r} 0.0 \\ 45 \end{array}$   $\begin{array}{r} +3.1 \\ 49 \end{array}$   $\begin{array}{r} +3.6 \\ 51 \end{array}$

(1978.87)  
 $\begin{array}{r} +5.5 \\ 30 \end{array}$   $\begin{array}{r} +4.9 \\ 36 \end{array}$   $\begin{array}{r} 0.2 \\ 40 \end{array}$   $\begin{array}{r} 1.7 \\ 46 \end{array}$   $\begin{array}{r} 3.3 \\ 46 \end{array}$   $\begin{array}{r} 3.4 \\ 49 \end{array}$   $\begin{array}{r} +0.5 \\ 55 \end{array}$   $\begin{array}{r} +4.0 \\ 60 \end{array}$   $\begin{array}{r} +5.0 \\ 62 \end{array}$

(1978.87)  
 $\begin{array}{r} +6.9 \\ 40 \end{array}$   $\begin{array}{r} +6.6 \\ 46 \end{array}$   $\begin{array}{r} +0.8 \\ 50 \end{array}$   $\begin{array}{r} 1.9 \\ 55 \end{array}$   $\begin{array}{r} 2.5 \\ 60 \end{array}$   $\begin{array}{r} +4.80 \\ 67 \end{array}$

Top core pipe @ bottom buttress # 13

Top of pipe 10' ± S.W. of & bottom # 13.

+6.8 +9.0 +7.0 +9.9

Notes: All shots were taken North of Base line



(21) Arch Ring #13-14 = D-1780-1840

Sta. +  $\pi$  - Elev.

□ 11.33 1994.22 1982.89

1790

1800

1810

1820

1830

□ 11.33 1982.89

9-Aug. '52 same party as page 18  
X-Sections - Base line = L-1112.05

(21)

See bottom of page 20.

South					(1994.22)	North	
$\frac{6.5}{2}$	$\frac{6.8}{2}$	$\frac{12.2}{6.5}$	$\frac{12.5}{12.5}$	$\frac{7.2}{19}$	$\frac{7.0}{29}$		

$\frac{2.9}{3}$	$\frac{3.0}{0}$	$\frac{6.5}{1}$	$\frac{10.5}{5}$	$\frac{9.7}{10}$	$\frac{1.0}{17}$	$\frac{1.9}{27}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{0.2}{2}$	$\frac{0.1}{0}$	$\frac{5.4}{2}$	$\frac{6.0}{4}$	$\frac{7.8}{4.5}$	$\frac{7.6}{8}$	$\frac{3.2}{13}$	$\frac{2.1}{19}$	$\frac{5.2}{26}$
-----------------	-----------------	-----------------	-----------------	-------------------	-----------------	------------------	------------------	------------------

$\frac{2.7}{0}$	$\frac{2.6}{2.5}$	$\frac{1.3}{6}$	$\frac{4.8}{10}$	$\frac{4.5}{13}$	$\frac{1.1}{18}$	$\frac{5.1}{24}$	$\frac{5.9}{30}$
-----------------	-------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.5}{5}$	$\frac{6.1}{12}$	$\frac{0.4}{17}$	$\frac{2.1}{22.5}$	$\frac{2.8}{25.5}$	$\frac{1.0}{28}$	$\frac{2.1}{32}$	$\frac{7.0}{37}$	$\frac{7.1}{40}$
-----------------	------------------	------------------	--------------------	--------------------	------------------	------------------	------------------	------------------

see top of page

+9.0  
+7.0 -7.0

(21) Arch Ring X-Section of # 16-17

Sta. +  $\nabla$  - D-1960-2020 Elev.

T.B.M. 1.50 2044.01 2042.51

D-1960

D-1970

D-1980

D-1990

D-2000

D-2010

D-2020

F1

1.50 2042.51 2042.51

9-Aug. 1952 Same party as page 18

(22)

Base line = L-1073.13

Top of 2X2 hub on Axis line @ D-1980

(2044.01) North  
 $\frac{13.5}{0}$   $\frac{12.3}{17}$   $\frac{13.2}{23.5}$  Top Bank

$\frac{11.7}{0}$   $\frac{11.3}{14}$   $\frac{15.6}{15}$   $\frac{17.2}{20}$   $\frac{16.7}{24}$   $\frac{11.0}{29}$   $\frac{8.5}{39}$

$\frac{9.9}{0}$   $\frac{8.8}{11}$   $\frac{14.7}{12}$   $\frac{15.6}{17}$   $\frac{10.7}{19}$   $\frac{7.1}{23}$   $\frac{6.8}{29}$

$\frac{8.0}{0}$   $\frac{6.8}{10}$   $\frac{12.3}{12}$   $\frac{13.1}{15}$   $\frac{9.0}{18}$   $\frac{5.5}{21.5}$   $\frac{4.4}{31}$

$\frac{6.2}{0}$   $\frac{4.4}{14}$   $\frac{8.7}{15.5}$   $\frac{9.4}{20}$   $\times$   $\frac{2.5}{27}$   $\frac{0.4}{37}$

$\frac{2.5}{10}$   $\frac{0.8}{23}$   $\frac{6.2}{25}$   $\frac{5.6}{32}$   $\frac{13.5}{53}$   $\frac{+1.5}{42}$   $\frac{+3.5}{53}$

$\frac{0.3}{21}$   $\frac{+2.5}{42}$   $\frac{1.2}{50}$   $\frac{1.4}{59}$  ← North

+ 4.10

- 5.10

(23) Arch Ring # 1-2 X-Section  
 Sta. + — — — — —  
 D-1060-D-1120  
 Elev.

3.38 2053.98 2050.60

D-1060

D-1070

D-1080

D-1090

D-1100

T.P. 0.14 2042.87 11.25 2042.73

D-1110

D-1120

ASSUMED AS 1952  
 GRID LINE FWK.

Base line Going East & West = L-1090 = 0 (23)

13-Aug, 1952

Dallas - H  
 Stanley - K  
 Clyde - Tape & Axe  
 Curley - Tape & P

Top of 2x2 Hub @ D-1000 @ L-1000 ✓

(2053.98) North ←  
 $\begin{array}{r} 7.3 \\ 0 \end{array}$   $\begin{array}{r} 6.6 \\ 2.5 \end{array}$   $\begin{array}{r} 5.7 \\ 10 \end{array}$   $\begin{array}{r} 4.5 \\ 19 \end{array}$   $\begin{array}{r} 3.5 \\ 30 \end{array}$   $\begin{array}{r} 1.2 \\ 41.5 \end{array}$   $\begin{array}{r} 0.1 \\ 43 \end{array}$   
 46.6 47.3 48.2 49.4 50.4 52.7 53.8

✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 $\begin{array}{r} 8.7 \\ 0 \end{array}$   $\begin{array}{r} 7.8 \\ 4 \end{array}$   $\begin{array}{r} 5.8 \\ 12 \end{array}$   $\begin{array}{r} 4.5 \\ 21 \end{array}$   $\begin{array}{r} 3.6 \\ 30 \end{array}$   $\begin{array}{r} 2.2 \\ 41 \end{array}$   $\begin{array}{r} 1.0 \\ 42.5 \end{array}$   $\begin{array}{r} 0.0 \\ 45 \end{array}$   
 45.2 46.1 48.1 49.4 50.3 51.7 52.9 53.9

✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 $\begin{array}{r} 9.1 \\ 0 \end{array}$   $\begin{array}{r} 6.8 \\ 10 \end{array}$   $\begin{array}{r} 5.1 \\ 20 \end{array}$   $\begin{array}{r} 3.6 \\ 30 \end{array}$   $\begin{array}{r} 2.1 \\ 42 \end{array}$   $\begin{array}{r} 0.0 \\ 40 \end{array}$   
 44.8 47.1 48.8 50.3 51.8 53.9

✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 $\begin{array}{r} 9.4 \\ 0 \end{array}$   $\begin{array}{r} 6.9 \\ 12 \end{array}$   $\begin{array}{r} 5.3 \\ 23 \end{array}$   $\begin{array}{r} 4.0 \\ 30 \end{array}$   $\begin{array}{r} 3.2 \\ 36 \end{array}$   $\begin{array}{r} 1.4 \\ 44 \end{array}$   $\begin{array}{r} 2.5 \\ 44 \end{array}$   $\begin{array}{r} 0.0 \\ 50 \end{array}$   
 44.5 47.0 48.6 49.9 50.7 51.4 53.9

(2053.98) ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 $\begin{array}{r} 11.1 \\ 0 \end{array}$   $\begin{array}{r} 9.7 \\ 5 \end{array}$   $\begin{array}{r} 7.8 \\ 10 \end{array}$   $\begin{array}{r} 6.6 \\ 15 \end{array}$   $\begin{array}{r} 4.5 \\ 25 \end{array}$   $\begin{array}{r} 3.8 \\ 30 \end{array}$   $\begin{array}{r} 2.8 \\ 42 \end{array}$   $\begin{array}{r} 1.8 \\ 49 \end{array}$   
 42.8 44.2 46.1 47.3 49.4 50.1 51.1 52.1

(2042.87) ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 on Rock @ D-1105 @ L-1085  
 $\begin{array}{r} 2.5 \\ 0 \end{array}$   $\begin{array}{r} 0.4 \\ 7 \end{array}$   $\begin{array}{r} 1.9 \\ 17 \end{array}$   $\begin{array}{r} 3.5 \\ 24.5 \end{array}$   $\begin{array}{r} 4.6 \\ 30 \end{array}$   $\begin{array}{r} 6.0 \\ 35 \end{array}$   $\begin{array}{r} 7.7 \\ 39 \end{array}$   
 40.3 42.4 44.7 46.3 47.4 48.8 50.5

(2042.87) ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓  
 $\begin{array}{r} 5.2 \\ 0 \end{array}$   $\begin{array}{r} 3.3 \\ 7 \end{array}$   $\begin{array}{r} 1.8 \\ 15 \end{array}$   $\begin{array}{r} 0.1 \\ 22 \end{array}$   $\begin{array}{r} 1.1 \\ 30 \end{array}$   $\begin{array}{r} 3.0 \\ 44 \end{array}$   
 37.6 39.5 41.0 42.9 43.9 45.8

North ←

(24) Arch Ring # 2-3 D-1120-1180

Sta. +  $\Delta$  - Elev.

2042.87

T.P. 6.15 2047.85 1.17 2041.70

2.60 2045.25

T.P. 0.68 2036.69 11.84 2036.01

D-1130

D-1140

D-1150

D-1160

D-1170

T.P. 0.06 2024.66 <sup>09</sup> 12.88 2024.60

D-1180

Base line L-1090 = 0

(24)

13-Aug. 1952 Page 23 for party

Rock @ D-1127 & L-1062

Check elev. on Hub @ ~~1~~ Buttress #2 on Axis line

Rock @ D-1142 & L-1064

South (2036.69) North

$\frac{1.8}{0} + \frac{0.2}{9.5} + \frac{1.5}{18} + \frac{2.0}{25} + \frac{2.5}{30} + \frac{4.4}{37} + \frac{5.0}{42} + \frac{5.4}{58}$

24.9 36.5 35.2 33.4 33.2 32.9 31.7 31.3  
36.9 38.2 39.7 40.2 41.1 41.7 42.1

$\frac{4.6}{0} + \frac{3.1}{8} + \frac{1.7}{17} + \frac{0.6}{23} + \frac{0.7}{30} + \frac{1.6}{38} + \frac{1.5}{50}$

32.1 33.6 35.0 36.1 36.0 35.1 35.2

$\frac{7.8}{0} + \frac{6.0}{11} + \frac{4.4}{24} + \frac{3.4}{30} + \frac{2.6}{40} + \frac{2.0}{48}$

23.9 30.9 27.3 31.3 29.1 31.9

$\frac{13.2}{14} + \frac{11.9}{7} + \frac{10.5}{0} + \frac{9.1}{11} + \frac{7.9}{37} + \frac{6.7}{30} + \frac{6.1}{39} + \frac{5.5}{50}$

23.5 24.8 26.2 27.6 28.8 30.0 30.6 31.2

$\frac{13.8}{12} + \frac{12.9}{8.5} + \frac{12.3}{0} + \frac{12.4}{7} + \frac{10.6}{18} + \frac{10.1}{25} + \frac{9.8}{33.5} + \frac{11.7}{39}$

22.9 23.8 24.4 24.3 26.1 26.6 26.9 25.0

1 x 2 hub @ D-1170 & L-1085

South (2024.66) North

$\frac{13.2}{40} + \frac{11.5}{29} + \frac{9.7}{20} + \frac{5.8}{7.5} + \frac{5.0}{0} + \frac{2.6}{10} + \frac{1.8}{27} + \frac{3.7}{36}$

15.0 18.9 19.7 22.1 22.9 21.0

+7.0

(25) Arch Ring # 3-4 D-1180-1240  
Sta. +  $\uparrow$  — Elev.

D-1190 2024.66  
T.P. 0.12 2012.59 12.19 2012.47

D-1200

D-1210

D-1220

T.P. 1.86 2010.73 (2010.74)

D-1230

□ 11.79 2004.05 1992.26

D-1240

D-1230

D-1240

□ 4.09 1996.135 11.79 1992.26

ASSUMED AS 1952  
END LINE FULL

Base line L-1090 = 0

13-Aug. 1952 Page 23 for party (25)

South 2024.66 North  

16.3	13.9	13.3	12.6	10.6	7.6	5.8	4.0
4.0	3.7	2.8	2.0	1.8	5	1.5	3.1
08.3	10.2	11.3	12.0	14.0	17.0	18.8	20.6

 1x2 hub @ D-1201 & L-1090.5

(2012.59)  

7.2	6.1	3.3	1.9	0.0	+2.8	+4.0
4.0	3.6	2.0	1.9	0	1.8	3.4
05.3	06.4	09.2	10.6	0	15.3	16.5

10.9	8.4	5.6	3.0	1.5	-0.0
5.3	3.4	2.0	0	1.5	3.2
01.6	4.1	6.9	9.5	11.0	12.5

(2012.59)  

13.7	10.9	9.4	8.5	6.4	5.7	3.9	3.5	3.3
3.4	3.3	2.0	1.5	4	0	1.5	2.8	3.8
1998.8	1.6	3.1	4.0	6.1	6.8	8.6	9.0	9.2

Nail in Stump @ D-1215 ± & L-995

2x2 hub on Axis @ D-1273.48  
(2004.05)

South North  

8.2	6.1	5.0	3.9	2.8	1.0	0.2	+0.7	+1.5	-2.0
5.3	3.8	2.7	2.0	1.3	4	0	5.5	1.5	17.5
1995.8	1997.7	1999.0	0.1	1.2	3.0	3.8	4.7	5.5	2002.1

(2004.05)  

11.5	8.4	8.1	6.7	6.1	7.0	8.1	7.6	6.1	5.9	7.3
5.6	4.8	3.0	2.2	1.8	1.7	0	6	8.5	1.5	17
96.0	97.4	98.0	97.1	96.0	96.5	98.0	98.2			

2x2 hub on Axis @ D-1273.48

14-Aug. '52 D-1230 & D-1240 were taken same party as 13-Aug. See page 23

(20) Arch Ring #4-5 D-1240-1300

Sta. +  $\nabla$  - Elev.

1996.35

D-1250

D-1260

D-1270

D-1280

T.P. 2.27 1986.86 11.76 1984.59

D-1290

D-1300

T.P. 0.57 1975.69 11.74 1975.12  
6.00 1969.69 1969.69

ASSUMED AS 1952  
GND LINE F.W.K.

Base line = L-1125 = 0

14-Aug. '52 See page 23 for party. (20)

South						(1996.35)		North	
6.3	5.4	3.0	2.0	1.6	2.1	2.1	2.0		
23	19	12	8.5	0	15	35	45		
90.0	90.9	93.3	94.3	94.7	94.2	94.2	94.3		

9.2	6.0	4.5	4.3	3.7	2.4	2.0
25	18	12.5	0	15	35	47
87.1	90.3	91.8	92.0	92.6	93.9	94.3

10.7	5.1	3.0	3.6	4.4	3.3	2.8
19	9	0	9	15	2	35
85.6	91.2	93.3	92.7	91.9	93.0	93.5

(1996.35)								
8.6	5.3	6.9	10.4	10.4	8.8	4.5	1.9	1.5
7	0	8	11.5	13.5	10	21.5	25	35
87.7	91.0	89.4	85.9	85.9	87.5	91.8	94.4	94.8

Top rock D-1296 @ L-1112

(1986.86)								
5.9	1.8	+0.2	+1.0	1.7	2.5	2.2	+0.5	+1.6
12.5	5.5	0	3	8.5	13.5	20.5	28.5	35
80.9	85.0	87.0	87.8	85.1	84.3	84.6	87.3	88.4

11.7	10.0	4.7	0	4.2	5.5	4.4	9.6
17	12	2		6.5	7	18.5	22
75.2	76.9	82.2		82.7	81.4	82.5	77.3

Top of rock @ D-1312 @ L-1130

Check shot on Axis hub @ D-1332<sup>34</sup>

Arch Ring # 5-6 = D-1300 - 1360  
 Sta. +  $\uparrow$  - Elev.

Base line = L-1166.80 = 0  
 14-Aug. 52 see page 23 for party.

1975.69  
 D-1310

D-1320

D-1330

D-1340

T.P. 2.00 1965.51 12.18 1963.51

D-1350 ✓

D-1360

T.P. 0.75 1955.01 11.25 1954.26

E 7.32 1947.69 1947.68

South (1975.69) North  

0	$\frac{4.5}{16}$	$\frac{3.9}{25}$	$\frac{0.2}{31}$	$\frac{0.8}{36}$	$\frac{0.0}{42}$	$\frac{3.5}{49}$	$\frac{1.5}{56}$	$\frac{4.8}{73}$
	69.2	71.8	75.5	74.9	75.7	72.2	74.2	70.9

①  

$\frac{10.4}{11}$	$\frac{8.9}{20}$	$\frac{4.4}{27}$	$\frac{2.8}{30}$	$\frac{3.7}{37}$	$\frac{1.8}{42}$	$\frac{2.8}{50}$	$\frac{2.6}{60}$
65.3	66.8	71.3	72.9	72.0	73.9	72.9	73.1

②  

$\frac{13.1}{12}$	$\frac{7.3}{23}$	$\frac{8.2}{30}$	$\frac{9.8}{33}$	$\frac{9.5}{40}$	$\frac{3.5}{42}$	$\frac{5.2}{67}$
62.6	68.4	67.5	65.9	66.2	72.2	70.5

(1975.69)  

$\frac{19.1}{0}$	$\frac{16.5}{10}$	$\frac{11.2}{20}$	$\frac{10.2}{24.5}$	$\frac{8.6}{30.5}$	$\frac{11.8}{32}$	$\frac{12.7}{37}$	$\frac{11.3}{42}$	$\frac{5.1}{50}$	$\frac{6.0}{60}$
56.6	59.2	64.5	65.5	67.1	63.9	63.0	64.4	70.6	69.7

Rock @ D-1345 E L-1139

(1965.51)  

$\frac{7.4}{15}$	$\frac{6.8}{25.5}$	$\frac{3.1}{26.5}$	$\frac{3.0}{29}$	$\frac{7.3}{32.5}$	$\frac{9.6}{36.5}$	$\frac{12.6}{44}$	$\frac{13.3}{47}$	$\frac{8.5}{51}$
56.1	58.7	62.4	62.5	58.2	58.9	52.9	52.2	57.0

①  

$\frac{13.5}{18}$	$\frac{14.2}{27}$	$\frac{14.3}{37.5}$	$\frac{16.2}{40.5}$	$\frac{21.0}{43.5}$
52.0	51.3	51.2	49.3	44.5

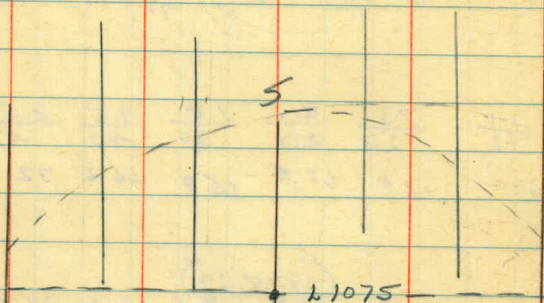
Rock @ D-1361 E L-1158

IX2 hvb on Axis @ D-1380 L

(28)

ARCH 14-15  
July 30, 1952

STA	+	H.I.	-	ELEV
	0.37	2018.86		2018.49
	6.57	2013.60	11.83	2007.03
	6.05	2019.02	0.73	2012.97
			0.43	2018.59


  
ARCHIT


  
V  
N
BASE LINE = 11075.0 FOR DISTANCES  
SOUTH     ~~S~~     NORTH

D 1840				H.I. 2013.60
9.1	13.1	17.6	19.9	
26	8.7	4.5	1.0	

D 1850							H.I. 2013.60
9.1	10.2	17.6	17.8	15.2	10.4	9.9	
25.8	15.1	13	6.1	5.0	0	2.0	10.5/10

D 1860							H.I. 2013.60
6.0	6.0	15.0	16.3	12.8	4.4	4.3	3.4
25.4	21.8	19	13.8	13	3	0	10

H.I. 2013.60			D 1870			H.I. 2018.86	
2.0	12.4	12.9	15.4	7.4	6.8	0.5	
23	18	13	12.5	5.0	0.0	10	H.I. 2013.60

H.I. 2018.86				D 1880		H.I. 2019.02	
6.7	15.9	16.0	12.0	6.3	5.5		
19.8	12.5	8	6.5	0.0	10		

D 1890								H.I. 2019.02	
4.7	4.8	12.9	13.1	9.8	4.4	4.1			
13.5	9.0	5.3	4.0	6.0	15	20			

D 1900

0.5	10
-----	----



(29)

ANCH 6-7 = D 1360-1420

STA	T	+	-	ELEV
T.P.	0.40	1954.66	/	1954.26
D-1370				
D-1380				
T.P.	0.55	1943.40	11.81	1942.85
D-1390				
D-1400				
T.P.	4.36	1935.64	12.12	1931.28
D-1410				
D-1420				
□		10.21	1925.43	(1925.43)

BASE LINE FOR 0' = L 1166 <sup>80</sup>

15 AUG 1952

DALLAS ID  
STAN  
DAVE  
CUREY  
CLYDE

SOUTH										NORTH																																												
Rock @ D-1361 / L-1158																																																						
(1954.66)																																																						
$\frac{4.1}{0}$					$\frac{3.7}{13}$					$\frac{5.4}{17}$					$\frac{4.2}{22}$					$\frac{7.8}{30.5}$					$\frac{7.3}{37.5}$					$\frac{5.1}{42}$					$\frac{4.4}{50}$																			
50.6					51.0					49.3					50.5					46.9					47.4					49.6					50.3																			
(1954.66)																																																						
$\frac{10.4}{0}$					$\frac{8.0}{10}$					$\frac{17.2}{14.5}$					$\frac{14.5}{30.5}$					$\frac{4.3}{27}$					$\frac{3.2}{33}$																													
44.3					46.7					37.4					40.2					50.3					51.4																													
Rock @ D-1386 / L-1164																																																						
(1943.40)																																																						
$\frac{4.4}{7}$					$\frac{3.5}{0}$					$\frac{3.5}{4}$					$\frac{5.0}{6.5}$					$\frac{12.8}{8}$					$\frac{8.3}{18}$					$\frac{2.8}{19.5}$					$\frac{1.3}{21.5}$					$\frac{1.4}{24.5}$					$\frac{1.8}{28}$									
39.2					39.2					39.2					38.2					30.2					35.2					40.2					44.2					47.2					50.2									
(1943.40)																																																						
$\frac{8.8}{34.6}$					$\frac{8.5}{24.9}$					$\frac{18.3}{25.3}$					$\frac{18.4}{25.2}$					$\frac{11.5}{31.2}$					$\frac{8.8}{34.6}$					$\frac{3.4}{40.2}$					$\frac{10.5}{43.2}$					$\frac{1.4}{44.2}$					$\frac{1.0}{47.2}$					$\frac{1.7}{41.5}$				
Rock @ D-1415 / L-1180																																																						
(1935.64)																																																						
$\frac{4.3}{9}$					$\frac{4.5}{0}$					$\frac{7.3}{6}$					$\frac{14.6}{8}$					$\frac{14.6}{17.5}$					$\frac{8.6}{17.5}$					$\frac{2.8}{28}$																								
31.2					31.2					28.2					21.2					21.2					27.2					32.2																								
(1935.64)																																																						
$\frac{6.3}{10}$					$\frac{6.6}{1}$					0					$\frac{11.3}{6}$																																							
CHECK ON I.P. IN RING 9-10 16 SE OF BUT # 10																																																						

(30)

ARCH RING 9-10

D 1600 - D 1540

STA +  $\pi$  - ELEVTBM 10.36 1935.79 ~~1925.43~~ IRON PIPE SE # 10

D-1600

D-1590

D-1580

TBM 1.63 1927.06 10.36 1925.43 I.P.

D 1570

D 1560

I.P. 6.15 1921.71 11.50 1915.56

D 1540

Aug 1-52

BASE LINE FOR 0' = L 1143.36

(1935.79)

SOUTH OR L5

NORTH OR R5

$\frac{39}{7.1}$	$\frac{31}{2.4}$	$\frac{23}{0.5}$	$\frac{17}{+1.5}$	$\frac{11.4}{+1.0}$	$\frac{11.4}{4.3}$	$\frac{10}{8.2}$	$\frac{0}{7.0}$	$\frac{6.7}{1.20}$	$\frac{8.2}{1.22}$
------------------	------------------	------------------	-------------------	---------------------	--------------------	------------------	-----------------	--------------------	--------------------

(1935.8)

$\frac{45}{8.5}$	$\frac{31}{10.1}$	$\frac{30}{7.6}$	$\frac{20}{7.7}$	$\frac{20}{12.9}$	$\frac{13.3}{12.5}$	$\frac{13.0}{10.95}$	$\frac{8}{10.7}$	$\frac{7}{7.3}$	$\frac{4}{7.8}$	$\frac{0}{7.5}$	$\frac{1}{5.2}$
------------------	-------------------	------------------	------------------	-------------------	---------------------	----------------------	------------------	-----------------	-----------------	-----------------	-----------------

$\frac{50}{12.2}$	$\frac{43}{13.1}$	$\frac{33}{14.0}$	$\frac{25}{14.8}$	$\frac{23}{1.8}$	$\frac{12}{0.3}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------

(1935.8)

$\frac{27}{+1.5}$	$\frac{20}{2.4}$	$\frac{3}{4.1}$	0	$\frac{20}{14.4}$
-------------------	------------------	-----------------	---	-------------------

(1927.1)

$\frac{55}{4.4}$	$\frac{46}{5.6}$	$\frac{38}{6.8}$	$\frac{28}{8.7}$	$\frac{21}{5.7}$	$\frac{17}{0.2}$	$\frac{6}{+1.5}$	$\frac{4}{+3.0}$	0	$\frac{2.5}{+3.5}$	$\frac{7}{1.8}$	$\frac{13}{1.3}$	$\frac{24}{+3.9}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	---	--------------------	-----------------	------------------	-------------------

(1927.1)

$\frac{55}{7.0}$	$\frac{50}{7.4}$	$\frac{37}{9.8}$	$\frac{28}{9.6}$	$\frac{16}{9.4}$	$\frac{0}{8.4}$	$\frac{12}{7.8}$	$\frac{25}{6.2}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------

(1927.1)

$\frac{55}{11.7}$	$\frac{46}{11.9}$	$\frac{33}{10.0}$	$\frac{18}{10.5}$	$\frac{4}{10.0}$	0	$\frac{4}{8.8}$	$\frac{14}{9.2}$	$\frac{26}{9.6}$
-------------------	-------------------	-------------------	-------------------	------------------	---	-----------------	------------------	------------------

BASE LINE FOR 0' = L 1156 58

1921.71

$\frac{50}{7.8}$	$\frac{4.5}{8.1}$	$\frac{37}{8.1}$	$\frac{25}{7.6}$	$\frac{10}{7.4}$	$\frac{1}{7.20}$	0	$\frac{5.4}{1.74}$
------------------	-------------------	------------------	------------------	------------------	------------------	---	--------------------

(31)

ARCH RING  
9-8 D1540-1480STA +  $\pi$  - ELEV

I.P. 1921.71

D-1530

D-1520

D-1510

D 1500

D 1490

1921.71

I.P. 12.17 1927.73 6.15 1915.56 1915.56

D 1480

Aug 1, 1952

BASE LINE FOR 0' = 11156.58

SOUTH

NORTH

(1921.7)

$\frac{50}{6.4}$	$\frac{42}{6.3}$	$\frac{37}{8.6}$	$\frac{27}{8.5}$	$\frac{17}{8.6}$	$\frac{9}{9.5}$	$\frac{4}{12.5}$	$\frac{0}{12.8}$	$\frac{20}{13.2}$	$\frac{39}{12.5}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	-------------------	-------------------

(1921.7)

$\frac{50}{6.6}$	$\frac{45}{7.6}$	$\frac{33}{7.8}$	$\frac{20}{8.5}$	$\frac{10}{8.3}$	$\frac{0}{7.3}$	$\frac{2}{7.9}$	$\frac{5}{11.7}$	$\frac{16}{11.7}$	$\frac{34}{12.2}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------	-------------------

(1921.7)

$\frac{50}{4.2}$	$\frac{44}{4.4}$	$\frac{36}{6.5}$	$\frac{27}{6.4}$	$\frac{20}{7.4}$	$\frac{8}{8.1}$	$\frac{0}{7.9}$	$\frac{7}{10.6}$	$\frac{12}{10.1}$	$\frac{13}{11.3}$	$\frac{30}{11.5}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------	-------------------	-------------------

(1921.7)

$\frac{52}{7.5}$	$\frac{46}{3.4}$	$\frac{38}{3.4}$	$\frac{27}{4.5}$	$\frac{19}{5.9}$	$\frac{11}{4.9}$	$\frac{9}{2.8}$	$\frac{0}{2.6}$	$\frac{8}{4.2}$	$\frac{12}{9.3}$	$\frac{18}{10.5}$	$\frac{31}{10.3}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

(1921.7)

$\frac{53}{7.2}$	$\frac{45}{2.7}$	$\frac{30}{2.0}$	$\frac{23}{2.7}$	$\frac{19}{3.9}$	$\frac{11}{4.6}$	$\frac{0}{5.2}$	$\frac{7}{8.0}$	$\frac{22}{8.2}$	$\frac{36}{8.6}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------

(1927.73) BASE LINE 11150

$\frac{0}{7.0}$	$\frac{5}{10.5}$	$\frac{10.5}{11.0}$	$\frac{13.5}{9.8}$	$\frac{29}{7.7}$	$\frac{42}{7.9}$
-----------------	------------------	---------------------	--------------------	------------------	------------------

(32)

ARCH RING

8-7 D1480 - D1420

STA +  $\pi$  - ELEV

I.P. 1927.73

D-1470

D-1460

D-1450

D-1440

D-1430

D-1420

AUG 1, 1952

BASE LINE FOR 0' = L 1150

NORTH

SOUTH

(1927.73)

$\frac{13.2}{3.3}$	$\frac{8.2}{0.5}$	0	$\frac{7.8}{2.5}$	$\frac{11.7}{4.5}$	$\frac{11.7}{6.5}$	$\frac{9.4}{15.5}$	$\frac{7.7}{26}$	$\frac{7.1}{35}$
74 <sup>5</sup>	14 <sup>5</sup>		19 <sup>2</sup>	16 <sup>2</sup>	16 <sup>2</sup>	18 <sup>3</sup>	20 <sup>2</sup>	20 <sup>2</sup>

NORTH

SOUTH

(1927.73)

$\frac{11.6}{8.0}$	0	$\frac{11.1}{1.5}$	$\frac{9.1}{1.0}$	$\frac{10.0}{3.0}$	$\frac{9.6}{4.5}$	$\frac{8.1}{6.5}$	$\frac{9.7}{12}$	$\frac{10.5}{14}$	$\frac{8.8}{23}$	$\frac{8.2}{34}$
16 <sup>2</sup>		16 <sup>6</sup>	18 <sup>2</sup>	17 <sup>2</sup>	18 <sup>2</sup>	19 <sup>2</sup>	18 <sup>2</sup>	19 <sup>2</sup>	18 <sup>2</sup>	19 <sup>5</sup>

SOUTH

NORTH

(1927.73)

$\frac{7.5}{11.7}$	$\frac{6.9}{7.0}$	$\frac{6.9}{0}$	$\frac{8.4}{3}$	$\frac{7.0}{10}$	$\frac{8.0}{13}$	$\frac{9.2}{18}$	$\frac{10.5}{21}$	$\frac{10.0}{31}$	$\frac{9.2}{33}$	$\frac{8.6}{36}$
20 <sup>2</sup>	20 <sup>8</sup>	20 <sup>8</sup>	19 <sup>3</sup>	20 <sup>2</sup>	19 <sup>2</sup>	18 <sup>5</sup>	17 <sup>2</sup>	17 <sup>2</sup>	18 <sup>5</sup>	19 <sup>1</sup>

$\frac{5.6}{11}$	$\frac{5.0}{4}$	$\frac{4.7}{0}$	$\frac{4.5}{3.6}$	$\frac{6.3}{12}$	$\frac{7.2}{18}$	$\frac{6.9}{26.6}$	$\frac{6.1}{34}$	$\frac{6.1}{38.8}$
28 <sup>1</sup>	22 <sup>2</sup>	23 <sup>2</sup>	23 <sup>2</sup>	21 <sup>4</sup>	20 <sup>5</sup>	20 <sup>8</sup>	21 <sup>6</sup>	21 <sup>6</sup>

$\frac{1.2}{15}$	$\frac{2.0}{5.3}$	$\frac{4.3}{2}$	0	$\frac{6.6}{4.4}$	$\frac{7.0}{14}$	$\frac{5.5}{21.7}$	$\frac{4.1}{29.5}$	$\frac{3.8}{36}$
26 <sup>5</sup>	25 <sup>7</sup>	23 <sup>4</sup>		21 <sup>1</sup>	20 <sup>7</sup>	22 <sup>2</sup>	23 <sup>6</sup>	23 <sup>9</sup>

$\frac{6.7}{14.4}$	$\frac{7.3}{5}$	$\frac{7.2}{7}$	$\frac{3.4}{7.7}$	$\frac{3.2}{13.5}$	$\frac{10.1}{18}$	$\frac{1.8}{19}$	$\frac{2.2}{34}$	$\frac{13.6}{59}$
21 <sup>2</sup>	20 <sup>2</sup>	20 <sup>5</sup>	24 <sup>1</sup>	24 <sup>5</sup>	27 <sup>8</sup>	29 <sup>5</sup>	29 <sup>2</sup>	31 <sup>3</sup>

NOTE: IF X-SECTION WAS NOT  
RUN SOUTH FAR ENOUGH  
ADDITIONAL POINTS WERE TAKEN FROM  
CITY'S BOOK FOR SAME  
SECTION WHEN NOTES WERE PLOTTED

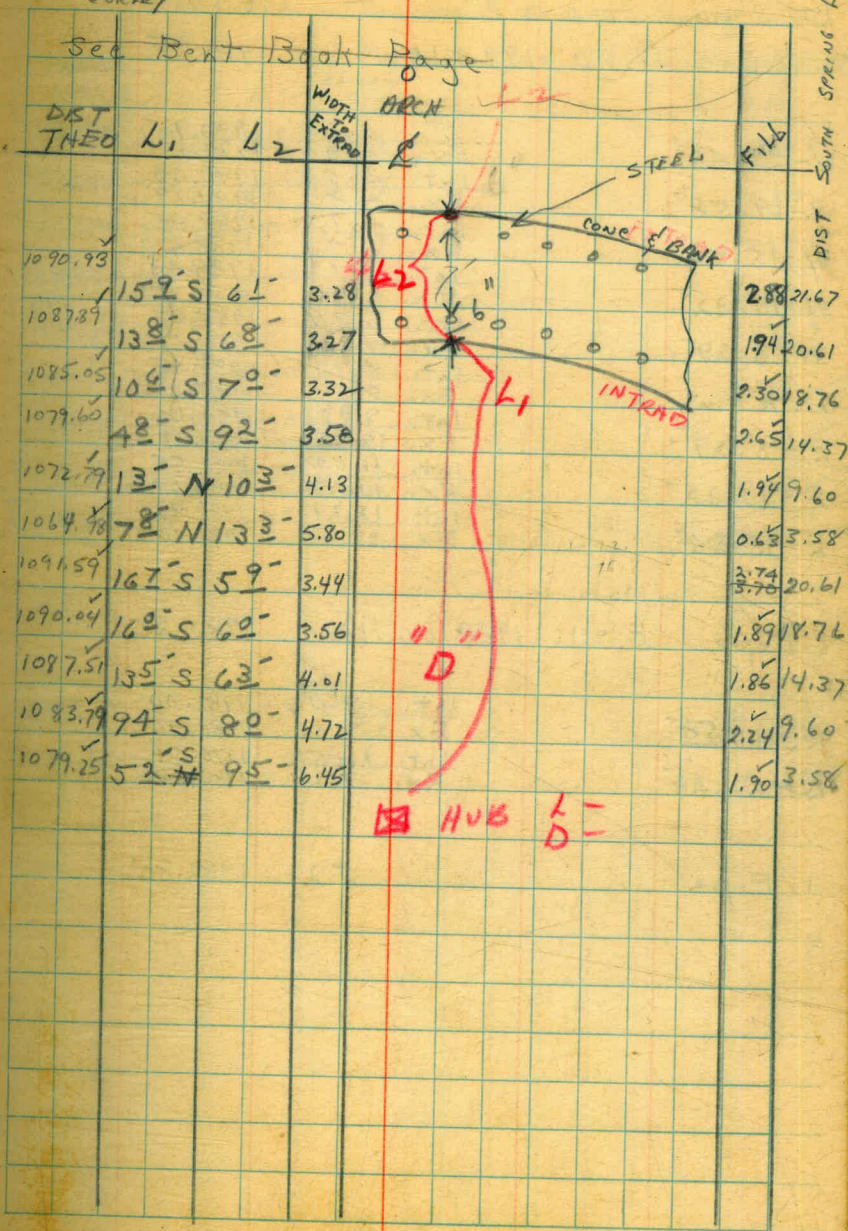
CHECK ARCH RING CUTOFF  
# 14-15 Arch Ring

BASE LINE HUB D-1870  
L-107215

STATION	+	H.I.	-	ELEV	INTRA DIST ACTUAL
1. Pipe @ # 14-15 Ring	8.15	2007.30		1999.15	
O= Ring			Int.	8.06	1999.24 1088.05
			Ex.	8.12	1999.18
W- 6.29			Int.	6.08	2001.22 1085.95
			Ex.	7.09	2000.21
W- 10.32			Int.	5.09	2002.21 1082.75
			Ex.	6.13	2001.17
W- 15.86			Int.	4.03	2003.27 1076.95
			Ex.	5.14	2002.16
W- 19.58			Int.	1.99	2005.31 1070.35
			Ex.	4.09	2003.21
W- 22.48			Int.	0.20	2007.10 1064.35
			Ex.	3.10	2004.20
E- 6.29			Int.	9.78	1997.52 1087.89
			Ex.	9.13	1998.17 1088.85
E- 10.32			Int.	10.08	1997.22 1088.15
			Ex.	10.13	1997.17
E- 15.86			Int.	11.94	1995.36 1085.65
			Ex.	11.10	1996.20
E- 19.58			Int.	9.24	1994.31 1081.55
			Ex.	8.30	1995.25
E- 22.48			Int.	10.72	1992.83 1077.35
			Ex.	9.04	1994.51
T.P.	4.40	2003.55	8.15	1999.15	
l. Pipe			4.40	1999.15	

SEPT 25-52 Elevations

DALLAS  
STAN  
CURLY



Continued on page 34

34 Check Arch Ring Cutoff # 13-14  
Continued from page 33.

"D" Station	+	-	Elev.	
L Pipe	11.30	1994.15	1982.85	INTRA ACTUAL
W-22.48	Int.	3.20	1990.95	1080.83 ✓
	Ex.	4.04	1990.11	
W-19.58	Int.	3.55	1990.60	1087.13 ✓
	Ex.	4.86	1989.29	
W-15.86	Int.	4.70	1989.45	1093.13 ✓
	Ex.	5.73	1988.42	
W-10.32	Int.	5.72	1988.43	1098.93 ✓
	Ex.	6.82	1987.33	
W-6.29	Int.	6.76	1987.39	1102.78 ✓
	Ex.	7.64	1986.51	
0 = Arch Ring	Int.	8.70	1985.45	1103.93 ✓
	Ex.	8.56	1985.59	
E-6.29	Int.	9.97	1984.18	1104.63 ✓
	Ex.	10.36	1983.79	
E-10.32	Int.	11.60	1982.55	1104.03 ✓
	Ex.	10.47	1983.68	
E-15.86	Int.	12.29	1981.86	1101.43 ✓
	Ex.	12.45	1981.70	

L Pipe 5.21 1988.06 11.30 1982.85

E-19.58	Int.	7.06	1981.00	1098.03 ✓
	Ex.	7.10	1980.96	
E-22.48	Int.	11.52	1976.54	1093.53 ✓
	Ex.	7.18	1980.88	

L Pipe 5.21 1982.85

26-Sept-52 page 33 for party  
Base line Hub = D-1816.24  
L-1084.03 Bent Book page 30  
D-1810 = Arch Ring

T.M.P.O DIST	L-1	L-2	EXTRA WIDTH	FILL
1081.13	32°N	90°	7.50	0.30 ✓
1087.50	35°S	95°	4.95	0.37 ✓
1093.46	91°S	78°	4.33	0.29 ✓
1098.83	149°S	62°	3.99	(C0.1) ✓
1101.72	180°S	63°	8.94	1.06 0.34?
1104.72	199°S	55°	3.91	0.79 ✓
1104.93	206°S	53°	4.07	0.30 ✓
1104.71	200°S	55°	4.29	0.68 ✓
1101.01	174°S	58°	4.77	(C0.42) ✓
1097.10	140°S	65°	5.57	(C0.93) ✓
1095.54	95°S	86°	7.62	F2.01 ✓

Continued on page 35

Check Arch Ring Cutoff # 12-13  
Continued from page 34

"D" Station	+	-	Elev.	
1. Pipe	3.06	1977.19	1974.13	INTRA ACTUAL
		Int. 1.67	1975.52	1097.06
W-22.48		Ex. 2.73	1974.46	
		Int. 2.31	1974.88	1102.96
W-19.58		Ex. 3.77	1973.42	
		Int. 3.74	1973.45	1108.56
W-15.86		Ex. 4.86	1972.33	
		Int. 4.89	1972.30	1114.46
W-10.32		Ex. 6.23	1970.96	
		Int. 6.10	1971.09	1117.96
W-6.29		Ex. 6.50	1970.69	
		Int. 7.60	1969.59	1120.16
O = Arch Ring		Ex. 7.80	1969.39	
		Int. 9.27	1967.92	1120.86
E-6.29		Ex. 9.31	1967.88	
		Int. 10.30	1966.89	1120.16
E-10.32		Ex. 10.27	1966.92	

1. Pipe	3.28	1969.00	11.47	1965.72	1965.72
		Int. 3.21	1965.79	1117.54	
E-15.86		Ex. 3.19	1965.81		
		Int. 5.22	1963.78	1114.26	
E-19.58		Ex. 4.19	1964.81		
		Int. 8.89	1960.11	1110.46	
E-22.48		Ex. 4.28	1964.72		

1. Pipe 3.28 1965.72

26-Sept. '52 page 33 for party  
Base line Hub = D-1750.31 Page 31 Bent Book  
L-1104.06

THEO DIST	L-1	L-2	WIDTH ARCH & CUTOFF	FILL
1096.50	7° N	9.2	7.72	0.50
1103.22	11° N	8.2	5.98	0.26
1109.42	45° S	7.5	5.27	0.86
1114.96	104° S	6.6	4.85	0.50
1118.02	139° S	5.5	4.75	0.05
1120.38	161° S	5.0	4.73	0.42
1121.19	168° S	4.6	4.92	0.33
1120.37	161° S	5.1	5.16	0.24

1. pipe 10" ± S.W. #12 Butt

1117.08	135° S	7.4	5.73	0.48
1114.32	102° S	8.2	6.71	0.06
1111.97	64° S	12.8	8.90	1.51

Continued on page 36

(36) Check Arch Ring Cutoff # 11-12  
 Continued from page 35  
 "B" Station +      -      Elev.

I. Pipe	8.52	1962.19	1953.67	INTRA ACTUAL
		Int. 1.90	1960.29	✓ 1109.28
		Ex. 4.52	1957.67	✓ 1118.38
W-22.48		Int. 4.62	1957.57	✓ 1125.28
		Ex. 4.48	1957.71	✓ 1130.68
W-19.58		Int. 4.44	1956.22	✓ 1132.98
		Ex. 5.97	1954.38	✓ 1136.48
W-15.86		Int. 5.81	1956.38	✓ 1136.48
		Ex. 6.07	1956.12	✓ 1135.88
W-10.32		Int. 7.39	1954.80	
		Ex. 7.81	1954.38	
W-6.29		Int. 9.31	1952.88	
		Ex. 9.27	1952.92	
O-# Ring		Int. 10.68	1951.51	
		Ex. 10.31	1951.88	
E-6.29		Int. 10.71	1951.48	
		Ex. 10.24	1951.95	

I. Pipe	3.40	1957.07	8.52	1953.67
		Int. 8.79	1948.28	✓ 1131.88
		Ex. 7.02	1950.05	✓ 1129.18
E-15.86		Int. 8.74	1948.33	✓ 1124.48
		Ex. 8.69	1948.38	
E-19.58		Int. 11.93	1945.14	
		Ex. 8.69	1948.38	

I. Pipe      3.40      1953.67

29-Sept. 1952 Page 33 for partu.  
 Base line Hub D-1690.02  
 T-1112.28  
 D-1690 = # Arch Ring

THEO DIST	L-1	L-2	I. Pipe In Arch Ring # 11-12	WIDTH ARCH @ CUTOFF	FULL
✓ 1111.79	3° N	156'	8.70		2.51 ✓
✓ 1120.53	6 L S	93'	7.15		2.15 ✓ 3.15 ✓
✓ 1125.12	13° S	74'	6.25		0.16 ✓
✓ 1130.88	18° S	72'	5.76		0.20 ✓
✓ 1134.31	20° S	69'	5.65		1.33 ✓
✓ 1137.29	24° S	63'	5.64		0.81 ✓
✓ 1137.60	24° S	57'	5.83		1.12 ✓
✓ 1135.78	23° S	58'	6.04		0.10 ✓
✓ 1134.59	18° S	78'	6.86		3.41 ✓
✓ 1129.77	15° S	92'	7.81		1.59 ✓
✓ 1126.94	12° S	100'	8.04		2.46 ✓

ok  
 10-16-5 ✓

Continued on page 37



(37)

Check Arch Ring Cutoff # 10-11  
Continued from page 36

D. Station + - Elev. INTRA ACTUAL

D. Station	+	-	Elev.	INTRA ACTUAL
L. Pipe	10.01	1945.17	1935.16	
W-22.48"		Int. 2.00 Ex. 3.75	1943.17 1941.42	1130.56 ✓
W-19.58"		Int. 2.22 Ex. 3.17	1942.95 1942.00	1135.76 ✓
W-15.86"		Int. 3.59 Ex. 4.89	1941.58 1940.28	1140.76 ✓
W-10.32"		Int. 4.85 Ex. 6.80	1940.32 1938.37	1146.56 ✓
W-6.29"		Int. 6.54 Ex. 6.79	1938.63 1938.38	1149.06 ✓
O = Ring		Int. 8.14 Ex. 8.15	1937.03 1937.02	1151.66 ✓
E-6.29"		Int. 9.49 Ex. 9.64	1935.68 1935.53	1151.26 ✓
E-10.32"		Int. 10.98 Ex. 11.06	1934.19 1934.11	1151.96 ✓

D. Station	+	-	Elev.	INTRA ACTUAL
L. Pipe	5.08	1940.24	10.01	1935.16
E-15.86"		Int. 7.56 Ex. 5.96	1932.68 1934.28	1148.56 ✓
E-19.58"		Int. 7.52 Ex. 7.49	1932.72 1932.75	1144.56 ✓
E-22.48"		Int. 12.30 Ex. 7.54	1927.94 1932.70	1140.56 ✓

L. Pipe 5.08 1935.16

29-Sept, 1952 Page 33 for party

Baseline Hub D-1625.78

L-1128.56

D-1630 = Arch Ring

(37)

THEO DIST L-1 L-2

THEO DIST	L-1	L-2	Width ARCH @ CUTOFF	Arch Ring # 10-11	FILL
✓ 1128.91	20° S	100°	10.30		✓ C 1.65 ✓
✓ 1135.15	72° S	99°	8.21		✓ C 0.61 ✓
✓ 1141.29	122° S	93°	7.29		✓ 0.53 ✓
✓ 1146.94	180° S	78°	6.70		✓ 0.38 ✓
✓ 1150.48	205° S	75°	6.56		✓ 1.42 ✓
✓ 1153.14	231° S	73°	6.51		✓ 1.48 ✓
✓ 1153.43	223° S	72°	6.75		✓ 2.17 ✓
✓ 1153.07	234° S	68°	7.06		✓ 1.11 ✓
✓ 1150.19	200° S	73°	8.13		✓ 7.63 ✓
✓ 1145.38	160° S	93°	9.68		✓ 0.82 ✓
✓ 1144.14	120° S	111°	12.38		✓ 3.58 ✓

ok  
10-16-5 ✓

Continued on page 38

(38)

Check Arch Ring Cutoff  
Continued from page 37

# 9-10

INTRA  
ACTUAL

"D" Station

+

A

-

Elev.

30-Sept. 1952 Page 33 for party.

Baseline Hub = D-1575-94

L-11571.39

D-1570 = R Ring FILL

INTRA  
THEOL<sub>1</sub>L<sub>2</sub>

L Pipe 1.57 1927.00 1925.43

W	INT	EXT	1926.78	1143.39
W-22.48	0.22	3.86	1923.14	1147.39
W-19.58	2.02	5.50	1922.98	1151.39
W-15.86	4.09	7.04	1922.91	1159.69
W-10.32	6.90	8.64	1920.10	1166.19
W-6.29	10.22	10.22	1916.78	1169.79
O.E. RING	10.17	10.15	1916.83	1172.89
E-6.29	11.57	11.65	1915.43	1173.19
E-10.32	12.95	12.95	1914.05	1172.29

L Pipe 0.84 1918.28 9.56 1917.44

E	INT	EXT	1912.44	1169.29
E-15.86'	5.84	4.47	1913.81	1164.19
E-19.58	5.69	5.91	1912.59	1157.39
E-22.48	6.26	5.89	1912.02	1157.39

L Pipe 0.84 1917.44

INTRA THEO	L <sub>1</sub>	L <sub>2</sub>	IRON PIPE IN RING #9-10	WIDTH ARCH CUTOFF
1146.30				2.91
1145.30	8° N	16 Z'	11.62	1.91
1153.12	0.0	13°	9.57	1.73
1159.96	8° S	10 Z'	8.54	0.27
1167.16	14° S	9 S'	7.94	0.97
1170.63	18° S	8 S'	7.77	0.84
1173.34	21° S	7 Z'	7.71	0.45
1173.68	21.8° S	6 Z'	7.96	0.49
1173.21	20 Z' S	7 Z'	8.34	0.92
				1917.45
1170.43	17° S	9 Z'	9.25	1.14
1165.51	12° S	11 Z'	10.45	1.32
1160.06	6° S	15°	12.85	2.67
				2.77
				1917.45

OK  
10-16-52

Continued on page 39

(39) Check Arch Ring Cutoff #8-9  
Continued from page 38

D' Station	+	π	-	Elev.	INTRA ACTUAL
L. Pipe	1.04	1918.49		1917.45	h
W-22.48'		Int. 7.01	1911.48	1162.72	
		Ex. 7.02	1911.47		
W-19.58'		Int. 7.16	1911.33	1165.72	
		Ex. 6.66	1911.83		
W-15.86'		Int. 6.66	1911.83	1170.02	
		Ex. 6.65	1911.84		
W-10.32'		Int. 6.44	1912.05	1174.52	
		Ex. 6.48	1912.01		
W-6.29'		Int. 6.43	1912.06	1176.12	
		Ex. 6.41	1911.88		
O = Arch Ring		Int. 6.66	1911.83	1177.42	
		Ex. 6.51	1911.98		
E-6.29'		Int. 6.59	1911.90	1175.32	
		Ex. 6.53	1911.96		
E-10.32'		Int. 6.62	1911.87	1176.32	
		Ex. 6.54	1911.95		
E-15.86'		Int. 6.59	1911.90	1170.22	
		Ex. 6.62	1911.87		
E-19.58'		Int. 6.70	1911.79	1164.32	
		Ex. 6.59	1911.90		
E-22.48'		Int. 6.65	1911.84	1157.82	
		Ex. 6.62	1911.87		

L. Pipe 4.51 1913.98

30-Sept. 1952 page 33 for party

Base Line Hub = D - 1509.22

h = 1180.82

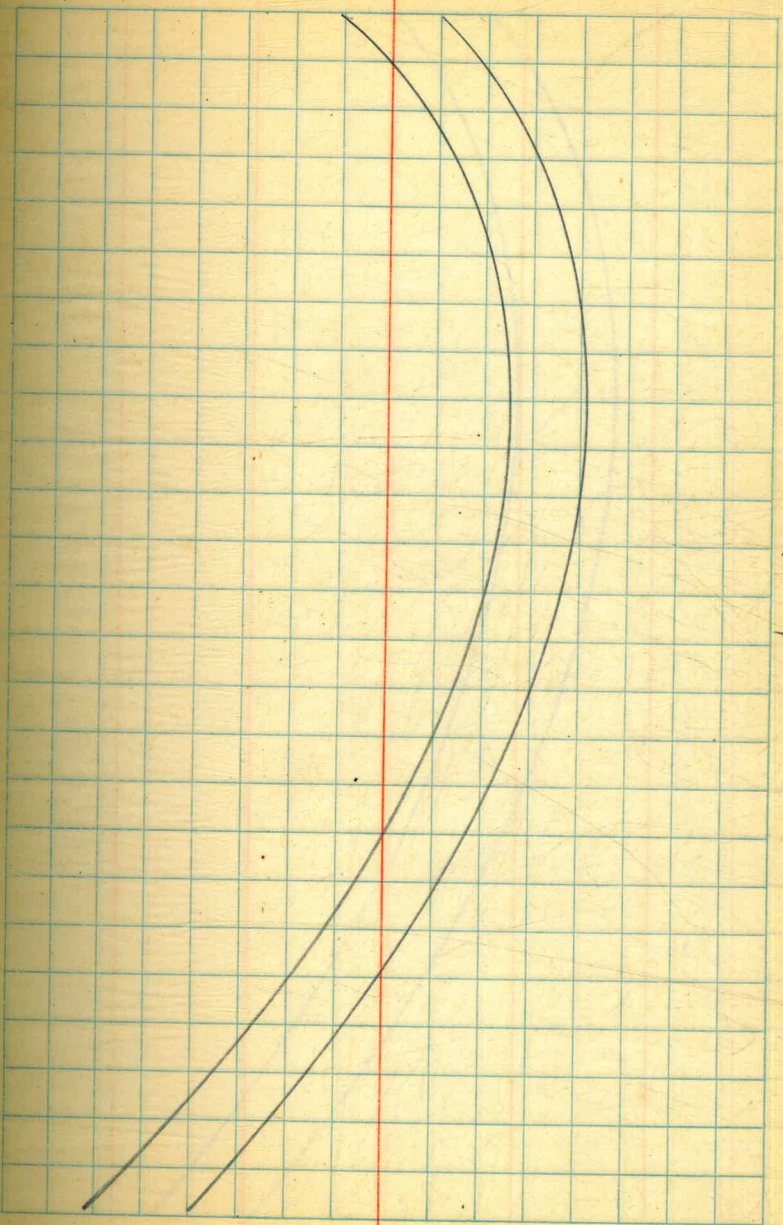
D = 1510 = Arch Ring

INTRA THRO	L-1	L-2	WIDTH ARCH CUTOFF	Iron pipe in ring #9-10	FILL
1160.60	18" N	90"	12.90	?	(2.12)
1166.77	15" N	96"	10.56		2.05
1171.04	10.8 N	111"	9.31		1.02
1175.21	6.3 N	81.9"	8.45		0.69
1177.05	4.7 N	87"	8.11		0.92
1178.34	3.4 N	81"	8.01		0.92
1177.21	3.5 N	68"	8.19	?	1.89
1175.39	4.5 N	70"	8.49	?	(0.93)
1170.97	10.6 N	96"	9.31		0.75
1166.31	16.5 N	125"	10.52		1.99
1153.08	28.0 N	144"	12.87		(4.74)

S/S # 9 Buttress elev. 1913.98

ok  
10-16-52

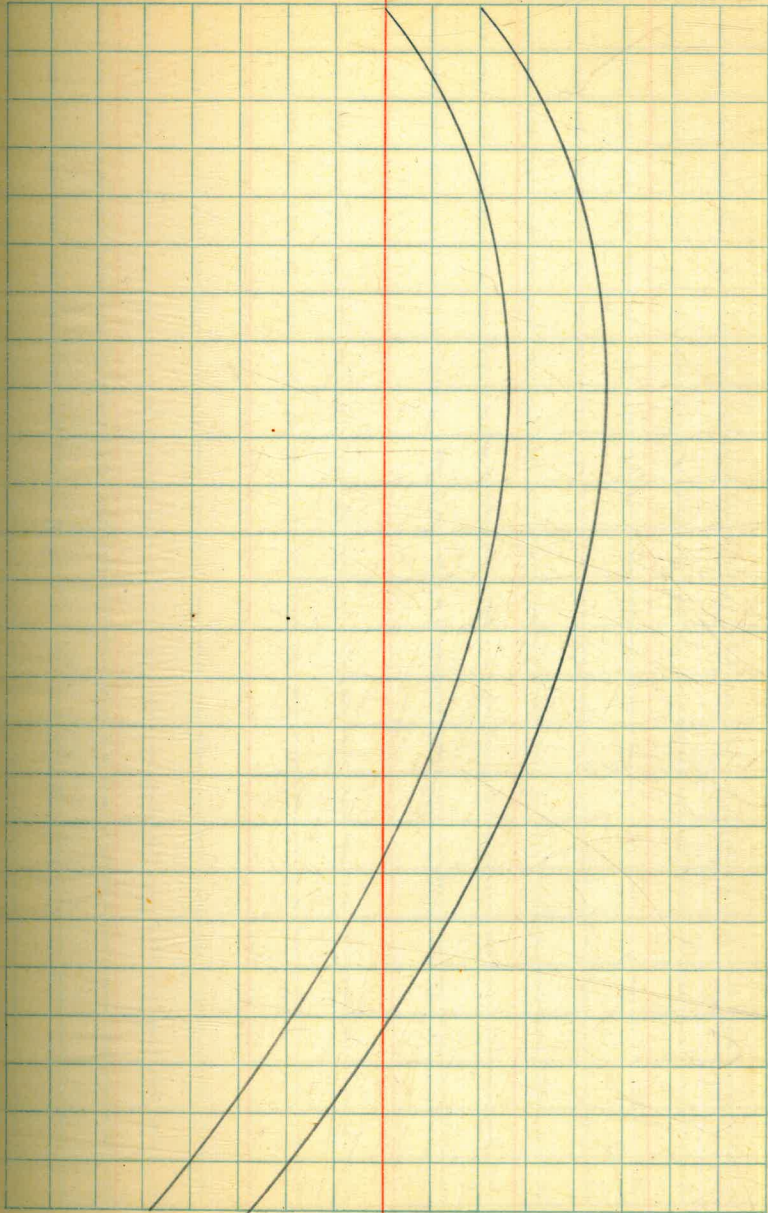
41

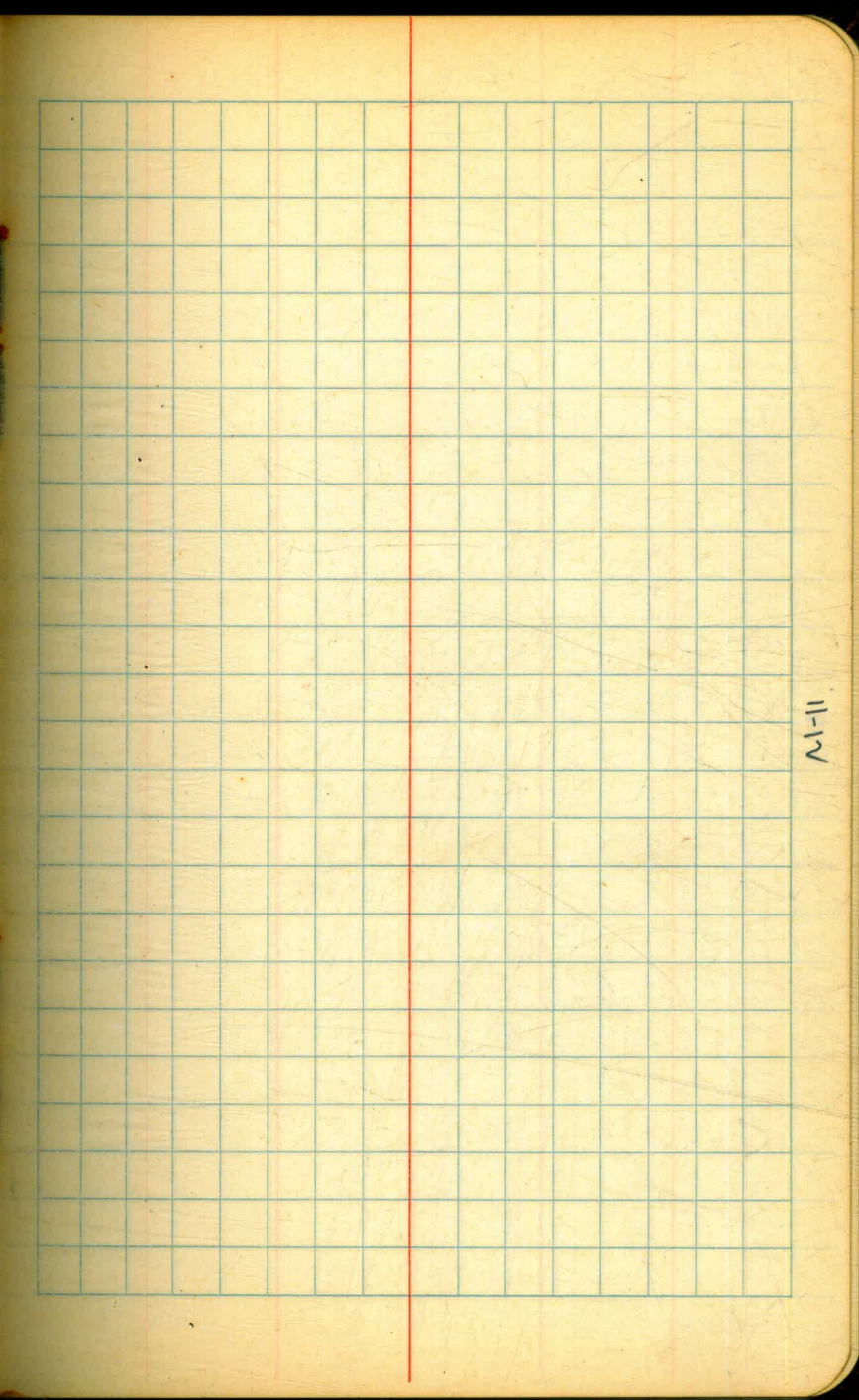
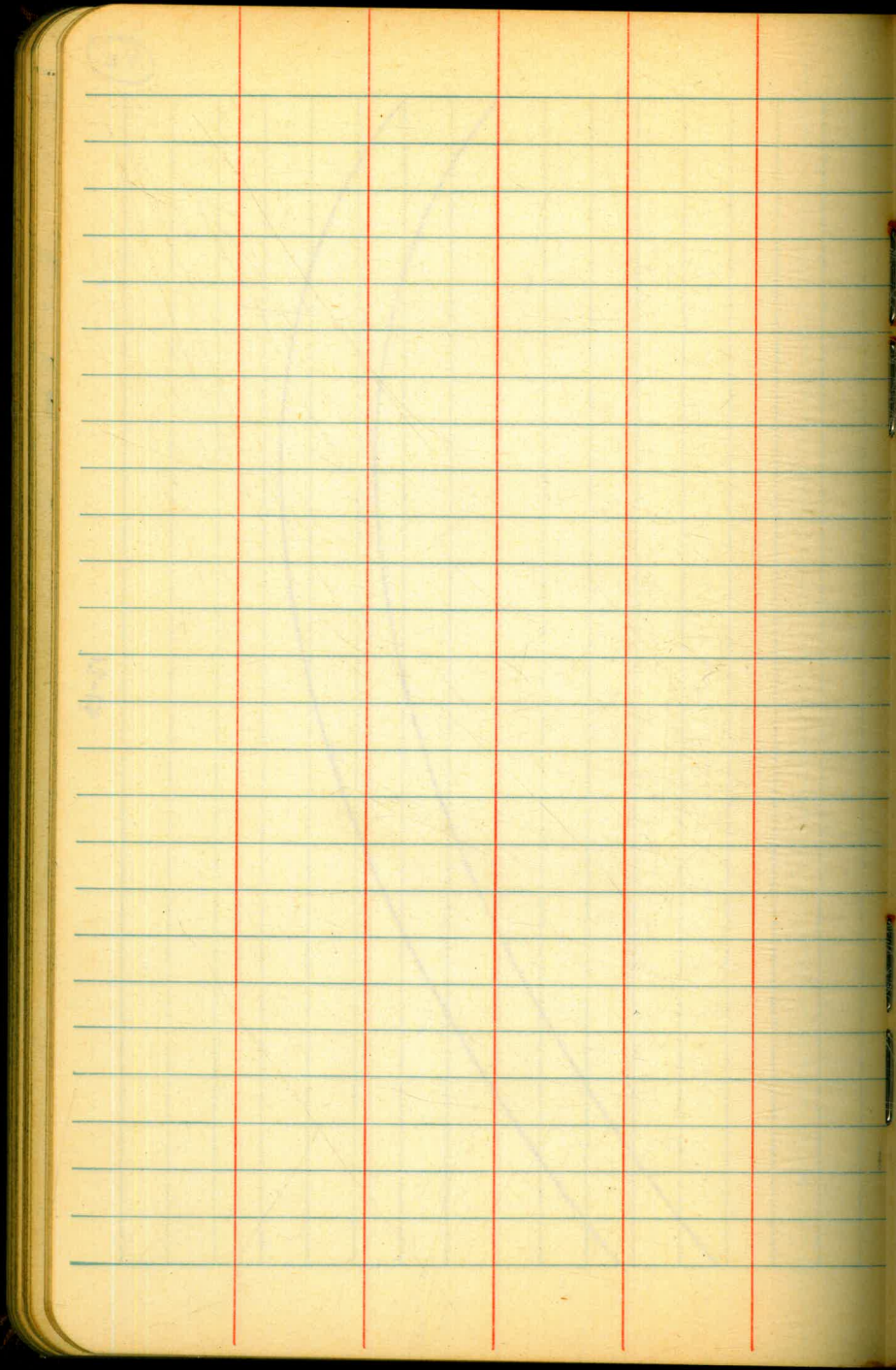


13-14

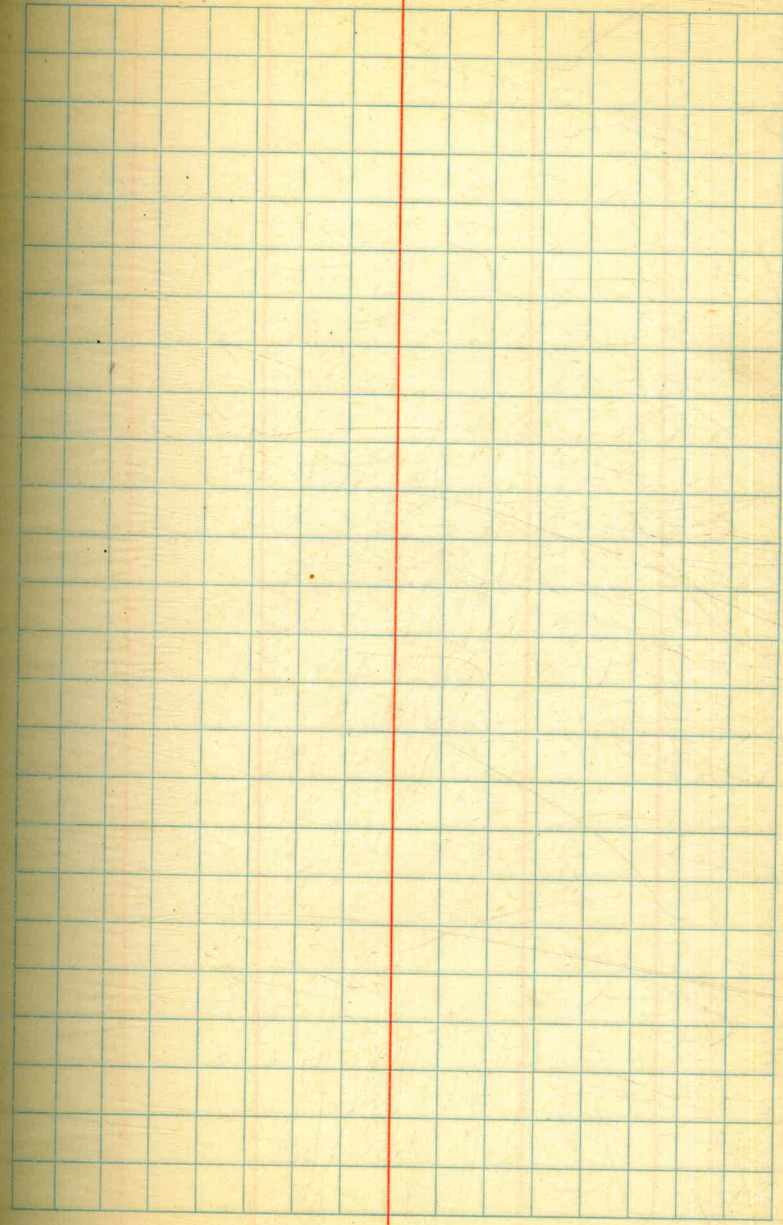
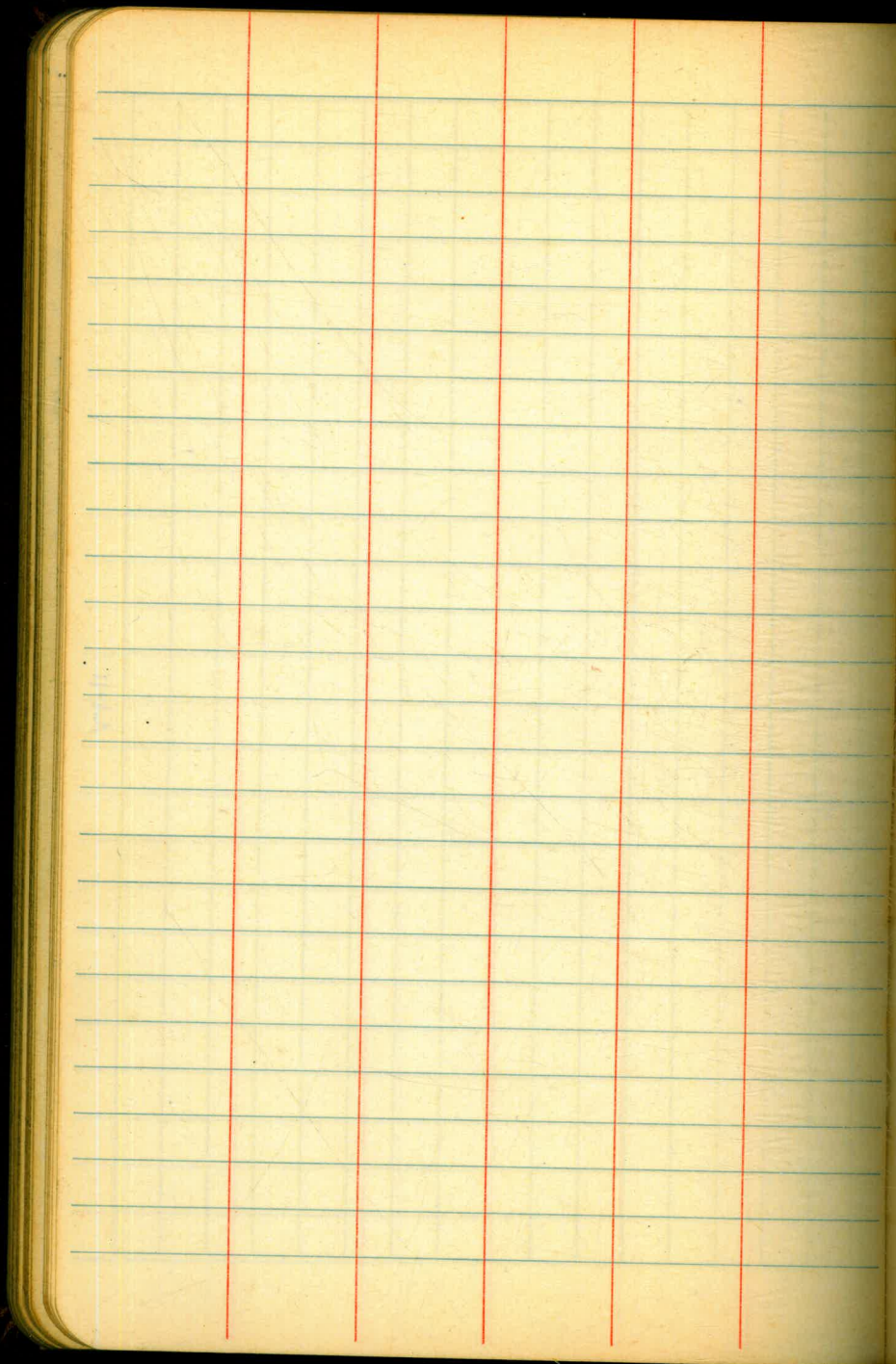
42

12-13

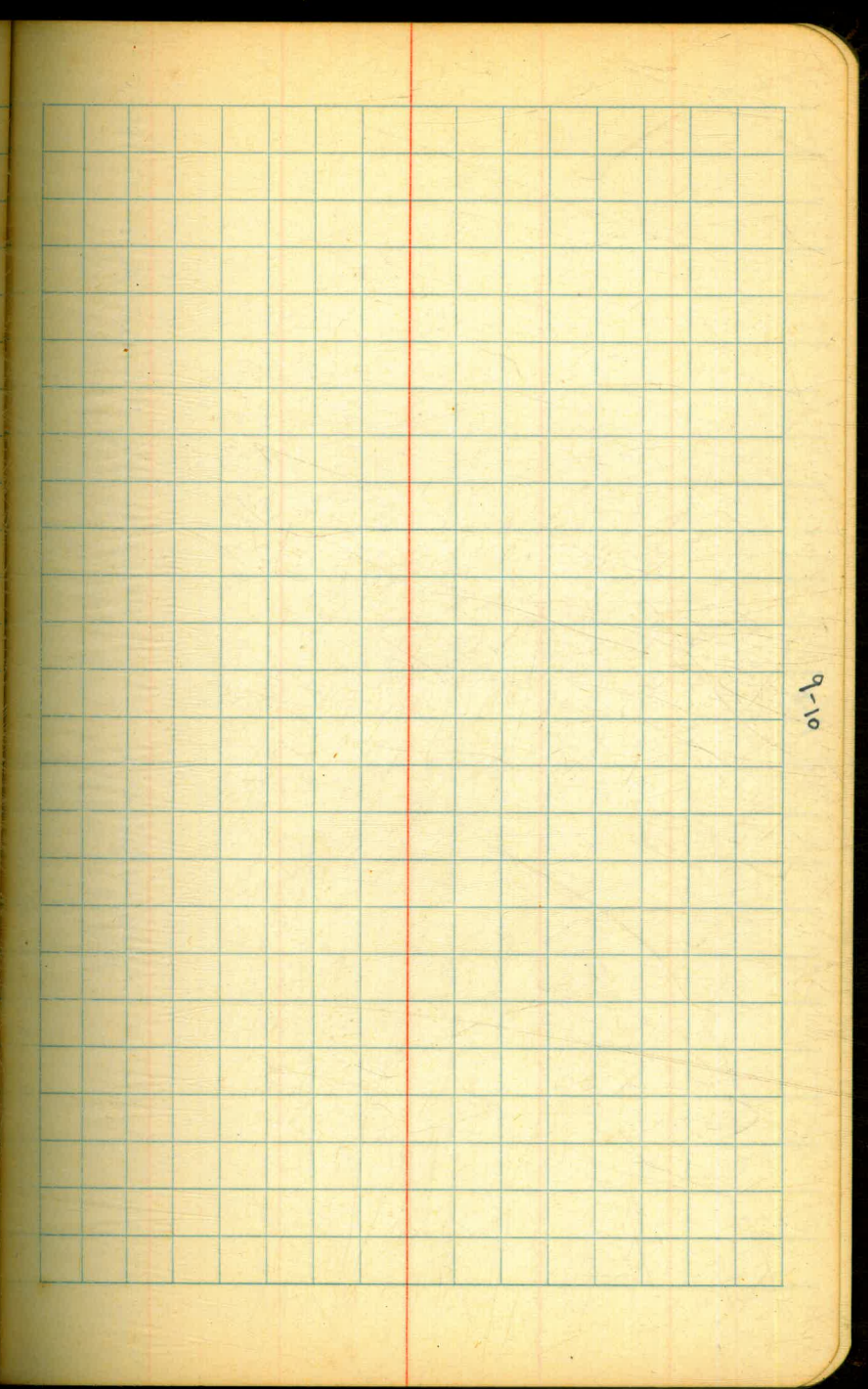
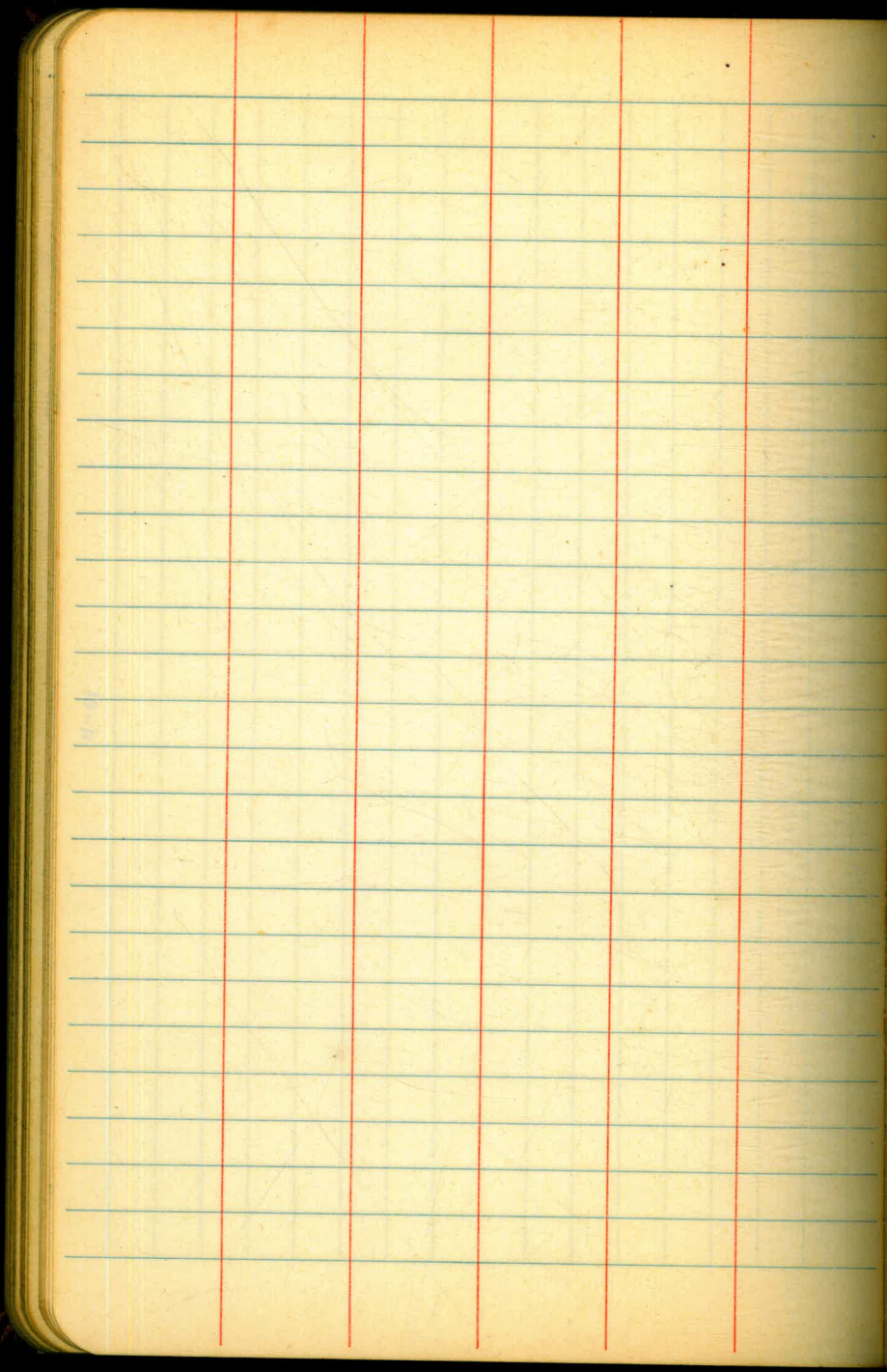




11-14

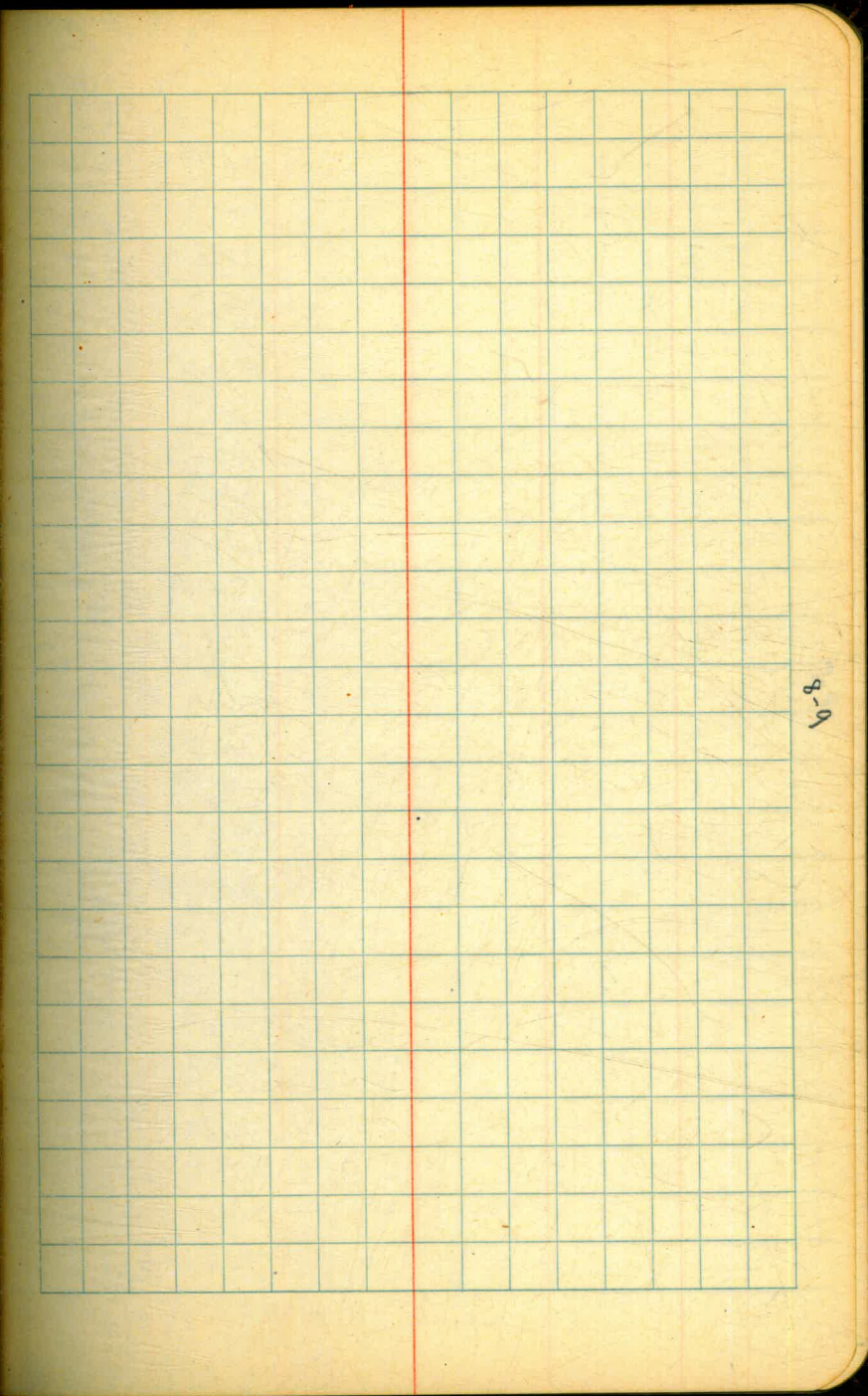
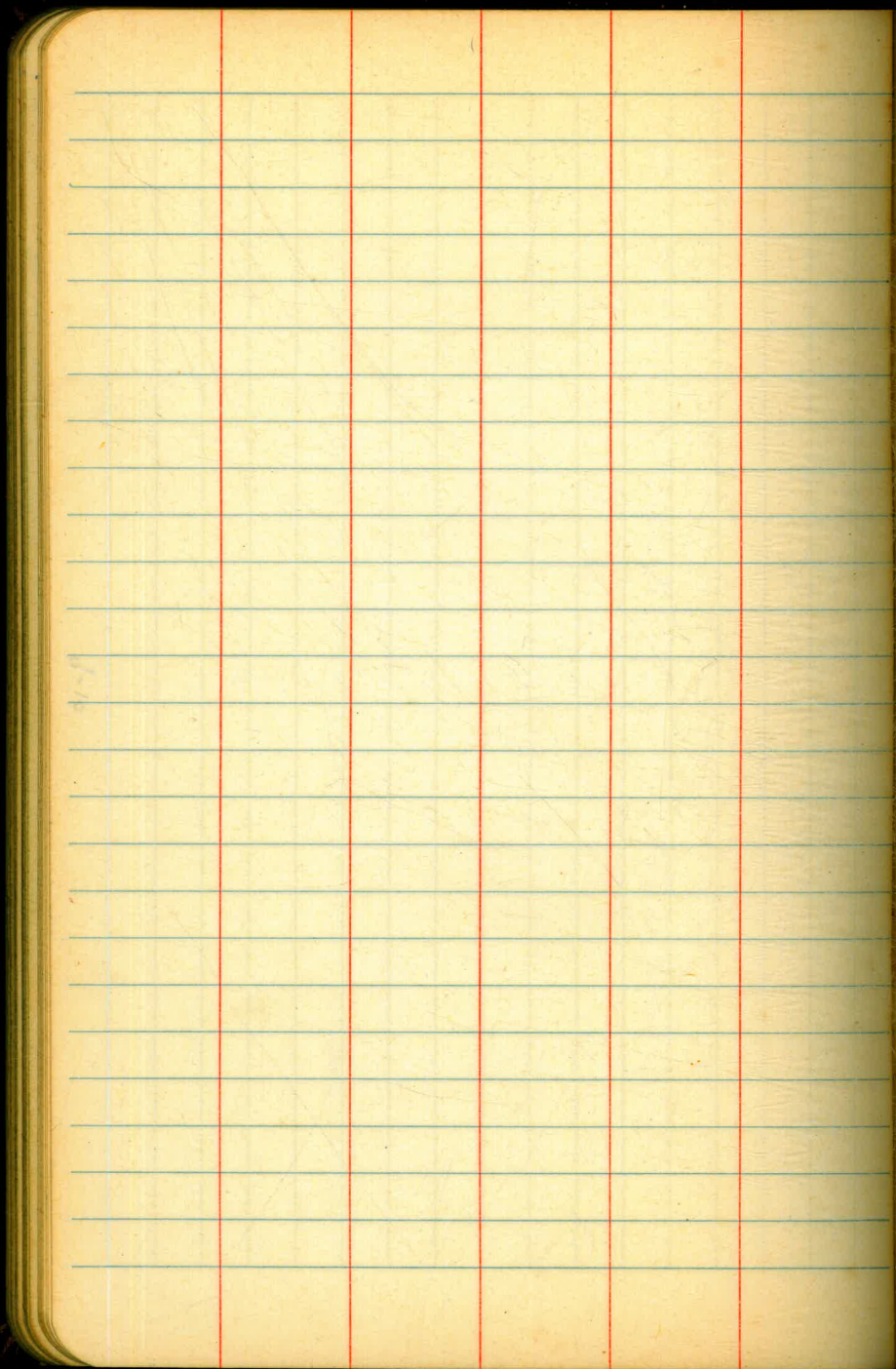


11-01

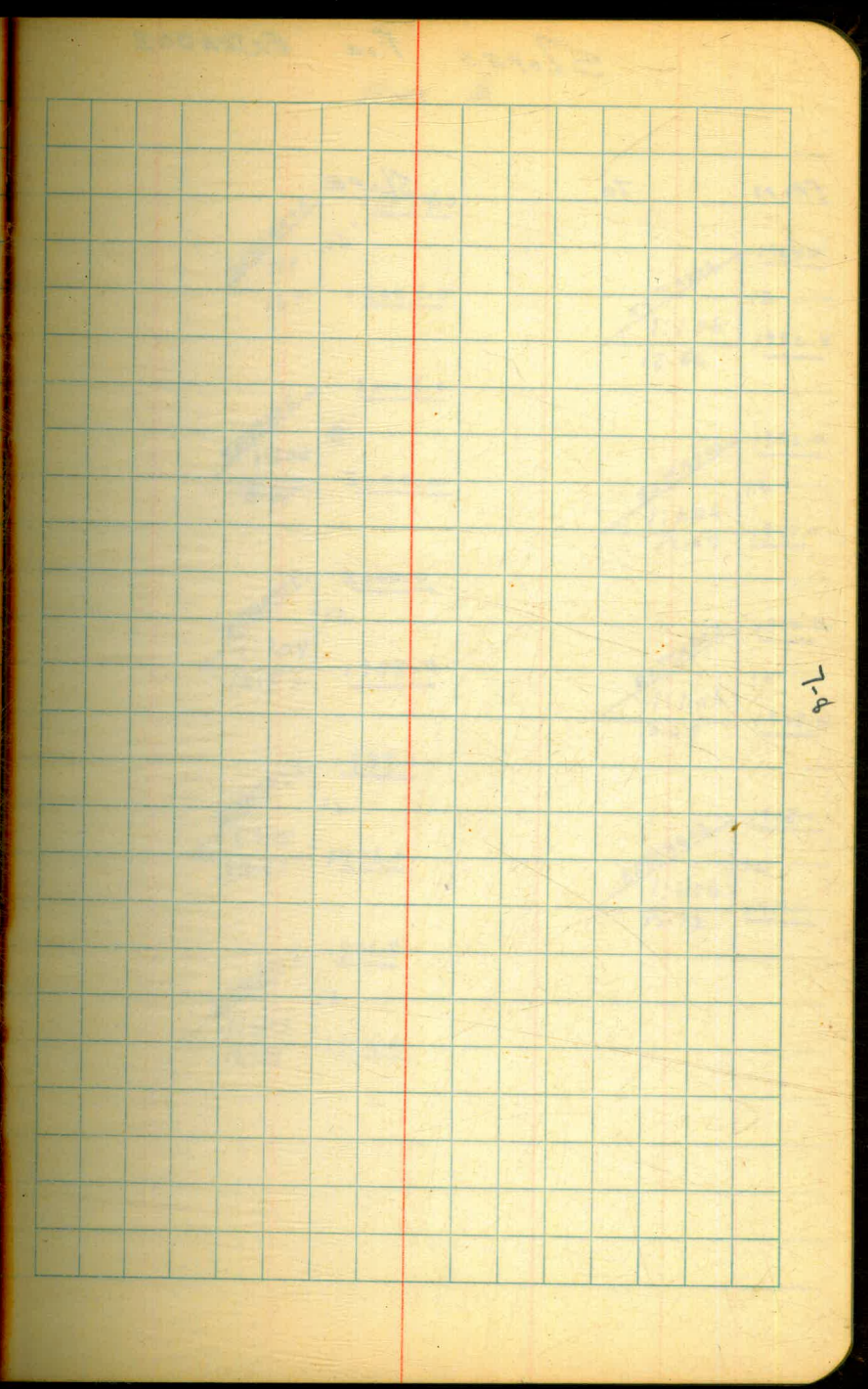
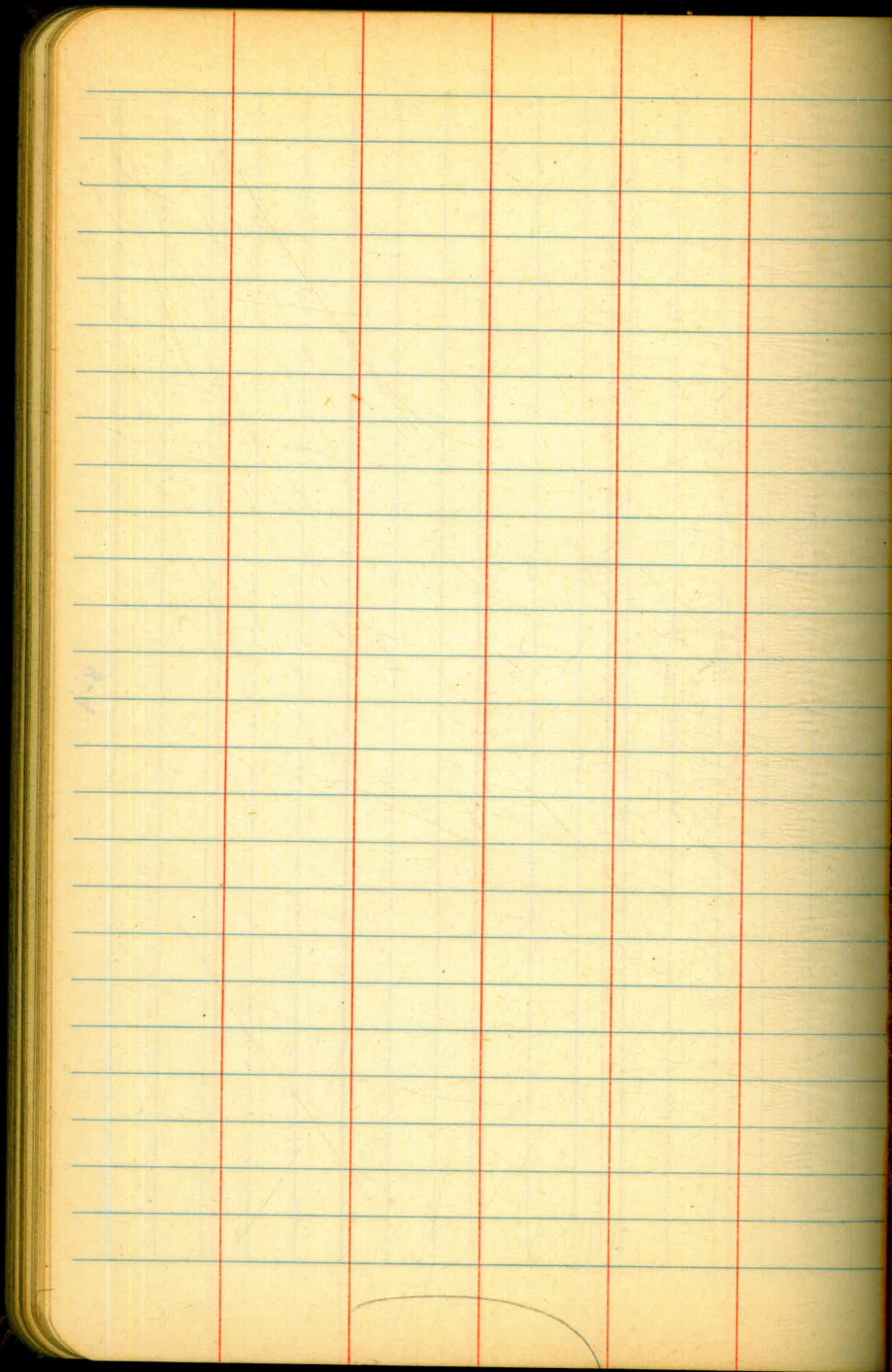


01-6





10-8

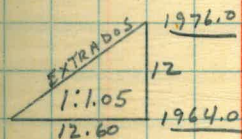
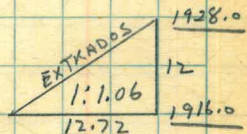
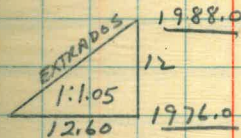
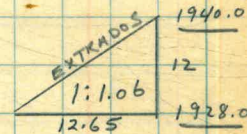
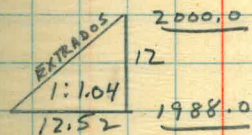
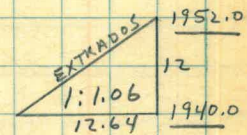
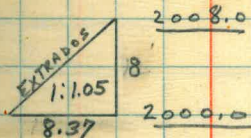
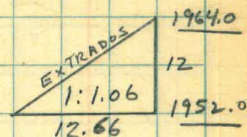
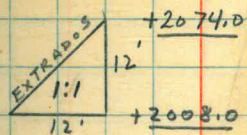


7-8

# SLOPES FOR EXTRADOS

FROM TO SLOPE

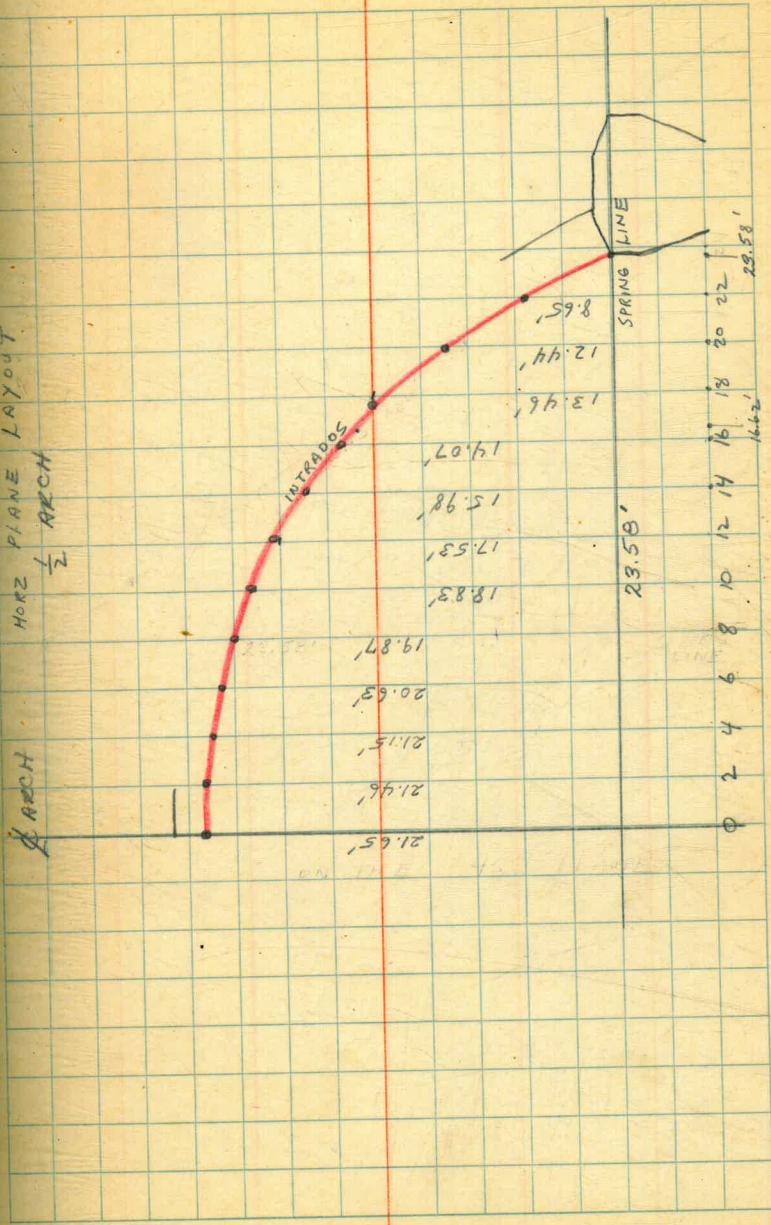
SLOPE  $\Delta$



HORIZ PLANE LAYOUT

ARCH

$\frac{1}{2}$  ARCH



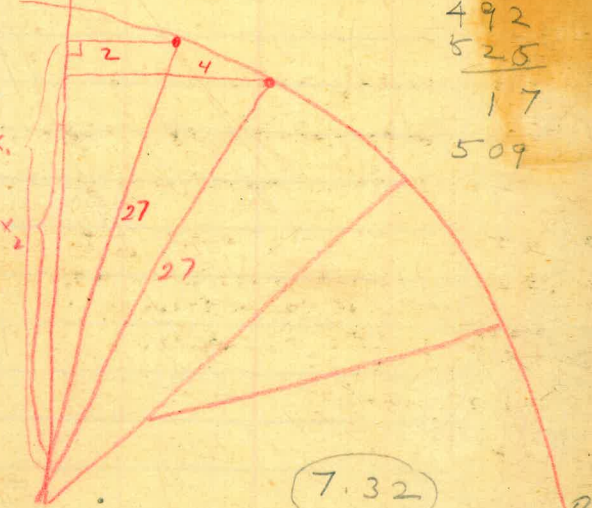
2068.50  
 90  
 2054  
 13.50

5.2  
 1.2  
 4.0

$x^2 + 2^2 = 27^2$   
 $x^2 = 27^2 - 2^2$

1978.00

4.3  
 1940.3  
 1944.6



492  
 525  
 17  
 509

7.32

190°

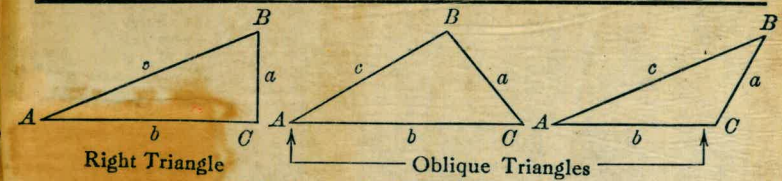
2068.50  
 1900  
 168

L1000

114032

TRIGONOMETRIC FORMULÆ

Aman Rod



Solution of Right Triangles

For Angle A.  $\sin = \frac{a}{c}$ ,  $\cos = \frac{b}{c}$ ,  $\tan = \frac{a}{b}$ ,  $\cot = \frac{b}{a}$ ,  $\sec = \frac{c}{b}$ ,  $\text{cosec} = \frac{c}{a}$

Given	Required	Formula
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$ , $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$ , $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$ , $b = a \cot A$ , $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$ , $a = b \tan A$ , $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$ , $a = c \sin A$ , $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formula
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$ , $C = 180^\circ - (A + B)$ , $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$ , $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$ , $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$ , $C = 180^\circ - (A + B)$
a, b, c	Area	$\text{area} = \frac{a + b + c}{2}$ , $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10'. From Table, Page IX.  $\cos 5^\circ 10' = .9959$ . Horizontal distance =  $319.4 \times .9959 = 318.09$  ft.  
 Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained.  $\text{Cosine } 5^\circ 10' = .9959$ .  $1 - .9959 = .0041$ .  $319.4 \times .0041 = 1.31$ .  $319.4 - 1.31 = 318.09$  ft.  
 When the rise is known, the horizontal distance is approximately: —the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance =  $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$  ft.