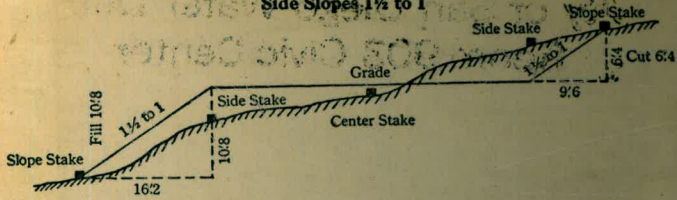


W



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 Roadway of any Width
 Side Slopes 1½ to 1



In the figure above: Opposite 6 under "Cut or Fill" and under .4 read 9/6 the distance from the side stake to the slope stake at right. Opposite 10 under "Cut or Fill" and under .8 read 16/2, the distance from the side stake to the slope stake at the left.

Cut or Fill	Distance out from Side or Shoulder Stake									Cut or Fill	
	0	.1	.2	.3	.4	.5	.6	.7	.8		.9
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

EUGENE DIETZGEN CO.

898-A

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

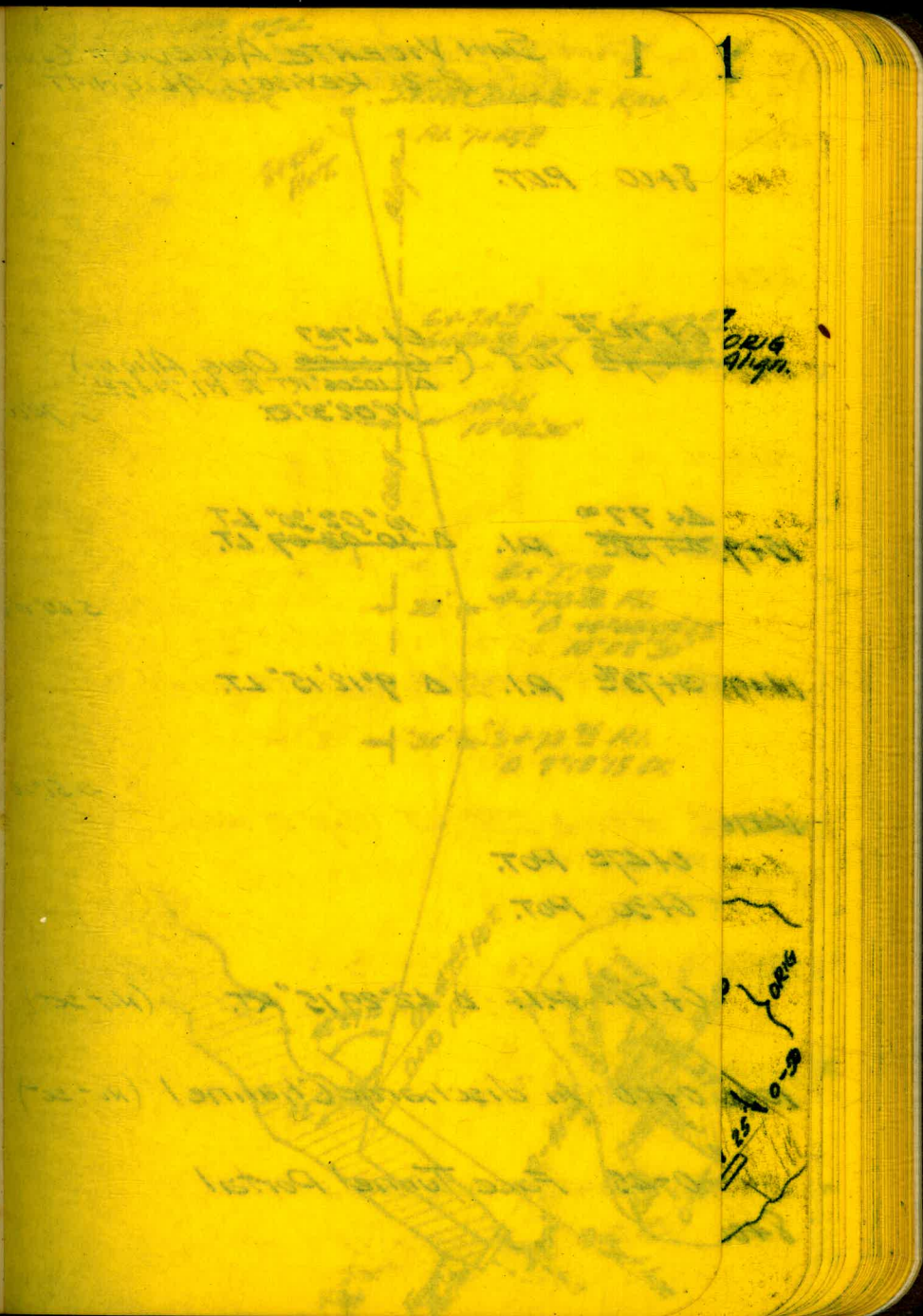
This Field Book is manufactured of a High
 Grade 50% Rag Paper having a WATER
 RESISTING SURFACE, and is sewed with
 Bing Special Enamel Waterproof thread.

Made in U. S. A.

INDEX

SAN VICENTE ARQUEDUCT CONN. REV. ALIGN. 1-6

" " " " ; & PROFILE 6-30
Alice



SAN VICENTE ARQUELUCT CONN.
R-2 REVISED ALIGNMT.

8+00 P.O.T.

~~6+72⁷⁵~~ POT (= ~~6+72⁷⁵~~ ORIG. ALIGN.)
6+47⁸⁷ P.O.T. ($\Delta 10^{\circ}02'30''$ RT R. PI. 7+45²)
10°02'30" RT

4+77⁰⁰ P.I. $\Delta 10^{\circ}02'30''$ LT
~~4+75⁰⁰~~ P.I. $\Delta 10^{\circ}02'30''$ LT

560' W E

3+73⁹⁶ P.I. $\Delta 9^{\circ}12'15''$ LT

551' W E

0+47⁰⁰ POT.

0+30 POT.

0+10 P.I. $\Delta 42^{\circ}29'15''$ RT. (N. + S. +)

0+00 in discharge Channel (N. + S. +)

0-45 Face Tunnel Portal

BEATTY
MURPHY
ALEXANDER

S.V.A. CONN. R-2 REV.

8+00 P.O.T. Align.

R.I. 7+45²

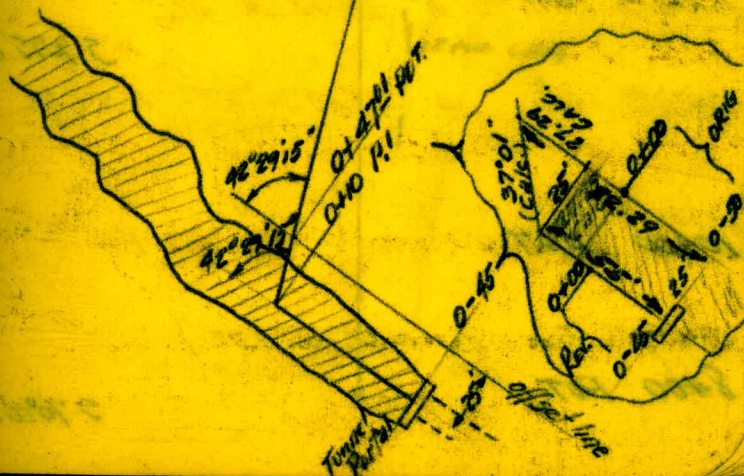
6+72⁷⁵ P.O.T. = 6+47⁸⁷ ORIG. ALIGN.

10°02'30" RT

ORIG.

4+77⁰⁰ P.I. $\Delta 10^{\circ}02'30''$ LT

3+73⁹⁶ P.I. $\Delta 9^{\circ}12'15''$ LT



2 SAN VICENTE AQUEDUCT CONN.
R-2 REVISED ALIGN'MT.

SEPT. 28, 1954
SAME PARTY

2
S.V.A. CONN. R-2 REV.

15+95.9 R.I. Δ (23'-90" LT 15780 ORIG)
385°00'E

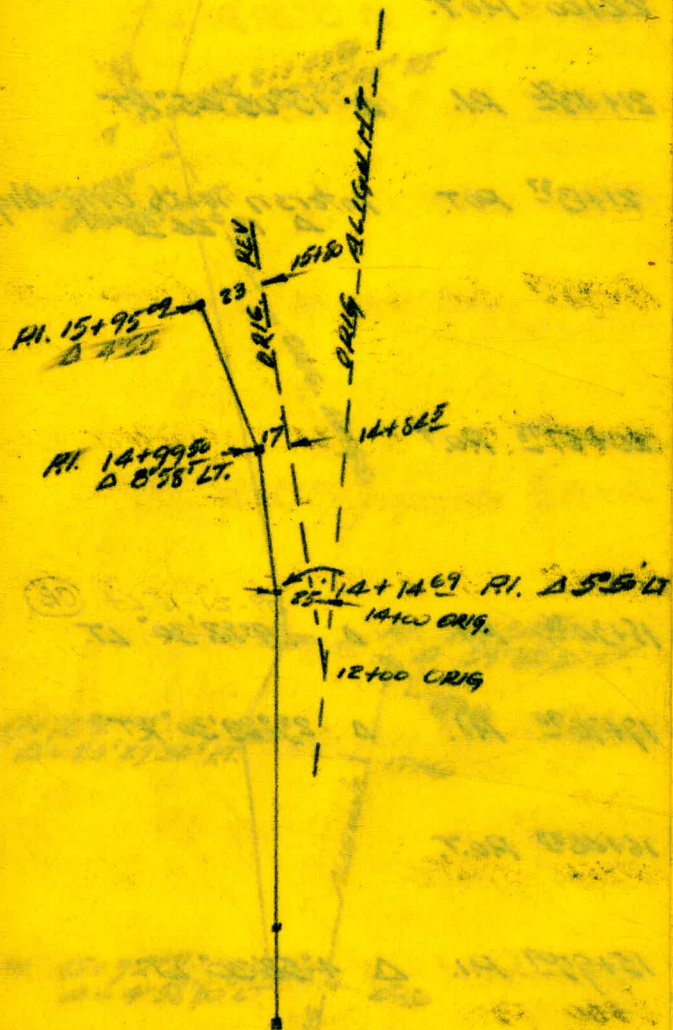
14+99.5 R.I. Δ 8'58" LT (17'-90" LT 14+84.5 ORIG)
376°00'E

14+14.9 R.I. Δ 5'30" LT (25'-90" LT 14+00 ORIG)
52°45'E

10+00 P.O.T.

8+00 P.O.T.

570°00'E



3

JAN VICENTE ARQUEDUCT CONN.
R-2 REV. ALIGNMT.

24+147²⁵ P.I.

22+100 P.O.T.

21+43²⁶ P.I. Δ 15°05'05" RT.21+13²⁷ P.O.T. Intersectn with Orig. Align.
 Δ 13°24'30"20+67²⁵ P.O.T.18+34²⁶ P.I. Δ 39°22'30" LT. (CB)17+76²⁶ P.I. Δ 23°29'30" RT.16+06²³ P.O.T.15+95²⁹ P.I. Δ 4°58'30" LT.SEPT 29, 1952
east of party

3

S.V. A CONN. R-2 REV.

P.I. 20+147²⁵P.I. 21+43²⁶
 Δ 15°05'05" RT.21+13²⁷

13°24'30"

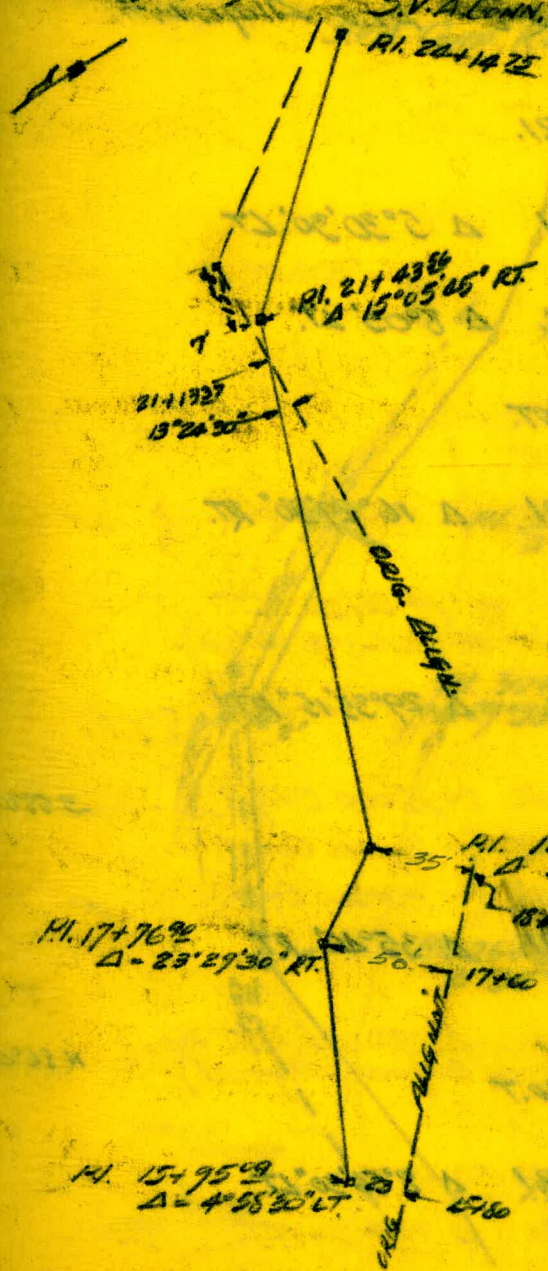
Orig. Alignmt.

P.I. 18+34²⁶
 Δ 39°22'30" LT.P.I. 17+76²⁶
 Δ 23°29'30" RT.

17+60

P.I. 15+95²⁹
 Δ 4°58'30" LT.

15+80



4

JAN VICENTE ARQUEDUCT CONN
R2 REV. Alignment

2.

37+97⁶⁶ P.I.2. 34+85²¹ P.I. $\Delta 5^{\circ}30'30''$ LT2. 34+36²¹ P.I. $\Delta 8^{\circ}03'$ LT.

2. 32+50 P.O.T.

31+92²² P.I. $\Delta 16^{\circ}29'30''$ RT.

2.

30+48²² P.I. $\Delta 29^{\circ}35'15''$ RT

13

11. 26+39⁴³ P.I. $\Delta 35^{\circ}46'$ RT.

16

25+65 P.O.T

1. 24+14⁷⁵ P.I. $\Delta 2^{\circ}26'30''$ LT.

S 58°00' E

N 56°45' E

4

Sept. 30, 1934
Same party

JVA. CONN. R2 REV.

P.I. 37+97⁶⁶P.I. 34+85²¹
 $\Delta 5^{\circ}30'30''$ LTP.I. 34+36²¹
 $\Delta 8^{\circ}03'$ LT.P.I. 31+92²²
 $\Delta 16^{\circ}29'30''$ RTP.I. 30+48²²
 $\Delta 29^{\circ}35'15''$ RT.P.I. 26+39⁴³
 $\Delta 35^{\circ}46'$ RT.P.I. 24+14⁷⁵
 $\Delta 2^{\circ}26'30''$ LT.

5 SAN VICENTE ARQUEDUCT CONN.
R-2 REV. ALIGN. MT.

2 55+25.72 P.I.

54+10 ROT.

52+92.91 P.I. Δ 19°26'30" LT.
(- 53+84.63 Orig. Align.)

52+18.83 ROT. (- 53+100 Orig.)

1 49+108.86 ROT. (- 50+100 Orig.)

42+58.83 ROT. (- 43+50 Orig.)

1 40+50 ROT.

1 39+108.72 P.I. Δ 19°01'30" RT.
(- 40+100 Original Alignment.)

37+96.72

37+97.12 P.I. Δ 9°04'30" RT.

5
SEPT
OCT. 1, 1952
SAME PARTY

5
S.V.A. CONN. R2 REV.

P.I. 55+25.72

ORIG 53+84.63

P.I. 52+92.91

Δ 19°26'30" LT

ORIG. 40+100

P.I. 39+108.72

Δ 19°01'30" RT

ORIG. P.I.
37+97.12

P.I. 37+96.72

Δ 9°04'30" RT

ORIG. 38+55

6 SAN VICENTE AQUEDUCT CONN.
R2 Rev. Alignment.

75+00⁹⁵ POT. Interon San Vicente #2

72+88²⁵ POT. Interon San Vicente #1.

69+69²⁵ P.I. $\Delta 1^{\circ}25'45''$ LT
(= 71400 ORIG.)

66+00 POT. (= 2nd Orig.)

64+08¹⁰ P.O.T. (= 2nd Orig.)

61+95²⁰ POT. (= 2nd Orig.)

58+84 P.O.T.

58+08²¹ P.I. $\Delta 16^{\circ}52'15''$
 $\Delta 17^{\circ}12'30''$ LT.

57+50 P.O.T.

55+25²² P.I. $\Delta 15^{\circ}49'15''$ LT.

OCT. 8, 1954

5

BEATTY
SHORR
MARTELL
ALEXANDER

SVA. CONN. R-2 REV.

SAN VICENTE #2 F 75+00⁹⁵

SAN VICENTE #1 F 72+88²⁵

See PD 849-
pp. 51-53
For Ties.

(71400 ORIG.)

P.I. 69+69²⁵ $\Delta -1^{\circ}25'45''$

P.I. 58+08²¹ $16^{\circ}52'15''$
 $\Delta 17^{\circ}12'30''$ LT.
ORIG. P.I. 59+01²⁵

P.I. 55+25²² $\Delta 15^{\circ}49'15''$ LT.

6

San Vicente Aqueduct Connection

Rev & Profile of X Sections

St. No.	Dist.	Elev.	St. No.	Dist.	Elev.
	0.89	766.55	10.11	756.44	
0+30					
	0.46	756.90	0.7		
0+47			3.2		
0+65			3.3		
0+74			12.49	744.41	
T.R.					
	0.17	744.58	1.3		
0+86			7.2		
1+00			13.7		
1+25			12.52	732.06	
T.R.					
	3.80	735.86	13.6		
1+50			12.96	722.90	
T.R.					
	4.32	727.22	12.27	714.95	
T.R.					
	1.82	716.77	4.8		
1+70			8.2		
1+75			6.3		
1+90					

9-28-54

West
Camp
Holdings

Et. Top So. postcard

0.00	00.95
20.00	20.95
40.00	40.95
60.00	60.95
80.00	80.95
100.00	100.95
120.00	120.95
140.00	140.95
160.00	160.95
180.00	180.95
200.00	200.95
220.00	220.95
240.00	240.95
260.00	260.95
280.00	280.95
300.00	300.95
320.00	320.95
340.00	340.95
360.00	360.95
380.00	380.95
400.00	400.95
420.00	420.95
440.00	440.95
460.00	460.95
480.00	480.95
500.00	500.95
520.00	520.95
540.00	540.95
560.00	560.95
580.00	580.95
600.00	600.95
620.00	620.95
640.00	640.95
660.00	660.95
680.00	680.95
700.00	700.95
720.00	720.95
740.00	740.95
760.00	760.95
780.00	780.95
800.00	800.95
820.00	820.95
840.00	840.95
860.00	860.95
880.00	880.95
900.00	900.95
920.00	920.95
940.00	940.95
960.00	960.95
980.00	980.95
1000.00	1000.95

	716.77	
2+00		7.0
2+05		9.8
2+20		1.8
T.P.	9.77 726.36	0.18 716.59
2+50		6.5
3+00		1.8
3+50		3.0
3+55		3.1
3+73	5.97 720.32	
	1.71 722.10	
4+00		2.0
4+15		1.3
4+22		16.7
4+28		14.7
4+33		9.8
4+50		3.5
T.P.	1.67 720.43	
	11.59 732.02	
T.P.	0.25 731.77	
	5.06 736.83	
4+77.0		2.51
5+00		3.5

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2+00				
2+05				
2+20				
T.P.				
2+50				
3+00				
3+50				
3+55				
3+73				
4+00				
4+15				
4+22				
4+28				
4+33				
4+50				
T.P.				
T.P.				
4+77.0				
5+00				

	716.77		
	736.88		
T.R.		0.14	736.80
	12.40		749.07
5107		19.5	768.57
5113		12.6	
5120		10.5	
5134		8.4	
5150		5.2	
5180		1.6	
T.R.		1.04	748.03
	721		755.24
5198.62		6.05	749.19
6118		3.6	
6150		4.4	
6174.75		5.4	
7100		1.4	
7107		3.1	
7150		5.7	
7175		5.2	
8100		7.56	747.68
		12.93	742.31
	0.20		742.51

7-28-54

4.4	16.		
$\frac{5.4}{0}$	$\frac{11.9}{75}$	$\frac{16.7}{28}$	
5.7	$\frac{12.9}{19}$	$\frac{15.6}{25}$	
$\frac{5.2}{0}$	$\frac{9.7}{70}$	$\frac{13.7}{20}$	$\frac{15.7}{25}$

	742.51	
8+50		7.0
8+60		10.0
8+75		13.0
T.P.		12.70 729.81
	0.71 730.52	
9+00		5.3
9+41		9.2
9+50		8.8
9+75		7.2
10+00		9.2
10+14		13.0
		717.69
		12.83 707.69
	1.18 718.87	
10+42		13.0
		12.64 706.03
	0.53 716.56	
10+50		4.1
10+60		7.8
10+72		12.5
		12.40 694.16
	1.34 695.52	

9-28-54

	742.51	
8+50		7.0
8+60		10.0
8+75		13.0
T.P.		12.70 729.81
	0.71 730.52	
9+00		5.3
9+41		9.2
9+50		8.8
9+75		7.2
10+00		9.2
10+14		13.0
		717.69
		12.83 707.69
	1.18 718.87	
10+42		13.0
		12.64 706.03
	0.53 716.56	
10+50		4.1
10+60		7.8
10+72		12.5
		12.40 694.16
	1.34 695.52	

625.52

10+92		10.7
11+00		12.3
T.P.		14.89 662.60
	0.40 669.09	17.70 717.81
11+40		12.5
		12.84 670.19
	1.79 671.98	
11+50		6.0
11+57		8.4
	0.95	8.95 663.03
	combine 9-29-54	
	0.85 663.88	
11+75		9.0
11+90		7.8
12+00		11.2
		12.57 651.31
	1.16 652.57	
11+15		5.8
12+27		11.2
		12.50 639.77
	6.59 646.51	

12.30

5.0	2.7	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
5.0	2.7	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
5.0	2.7	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
5.0	2.7	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
5.0	2.7	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31

left

9.0	6.2	3.6
0	18	26
11.2	16.5	11.3
0	18	27

646.51

12150	11.2
12175	11.4
12192	12.2
13100	9.6
13109	10.9
13115	8.2
13125	6.0
13150	3.1
13170	2.1
14100	3.6
Ri.	
14114.69	4.19 642.32
14132	3.0
14150	9.5
14151	12.0
14159	9.9
14160	9.2
14168	12.6
14172	12.5
14176	7.2

left

11.2	11.8	6.9	40.6
0	7	25	36
16.4	13.4	12.6	12.1
6	10	11	11
15.2			38
9.6	11.9	14.8	
0	10	18	
6.0	8.8	10.0	
0	10	11	
13150	3.1	7.4	
	0	25	
3.6	5.6	14.3	
0	11	28	

	643.24	
14799.50		0.87 642.37
	13.03 655.40	
		0.10 655.30
	12.85 668.15	
15150		11.3
		1.09 667.06
	13.16 680.22	
15195.09		9.49
16100		7.8 6.2
16105		6.7
16125		3.9
16147 46.23		2.83 677.79
	6.12 683.91	
16150		6.0
16175		7.0
17100		5.9
17150		4.2
17177.70		3.36 680.53
	4.15 684.68	
17177.70		4.2
17197		3.1

9-29-54

	680.5	
	678.1	
	675.2	
	671.5	
	669.2	

$$\begin{array}{r} 12 \\ 0 \end{array} \begin{array}{r} 4.6 \\ 7 \end{array} \begin{array}{r} 9.5 \\ 15 \end{array} \begin{array}{r} 13.2 \\ 22 \end{array} \begin{array}{r} 15.5 \\ 23 \end{array}$$

$$\begin{array}{r} 42 \\ 0 \end{array} \begin{array}{r} 6.1 \\ 3 \end{array} \begin{array}{r} 8.4 \\ 14 \end{array} \begin{array}{r} 12.6 \\ 26 \end{array}$$

$$\begin{array}{r} 10 \\ 0 \end{array} \begin{array}{r} 7.9 \\ 7 \end{array} \begin{array}{r} 11.4 \\ 19 \end{array} \begin{array}{r} 14.5 \\ 27 \end{array}$$

$$\begin{array}{r} 5.5 \\ 0 \end{array} \begin{array}{r} 8.6 \\ 10 \end{array} \begin{array}{r} 11.7 \\ 17 \end{array} \begin{array}{r} 14.5 \\ 21 \end{array} \begin{array}{r} 16.8 \\ 31 \end{array}$$

Red, 4-26-55
 Agling

18+00	684.68	3.3	
		8.93	676.25
	2.36		678.61
18+50		11.0	
		12.45	666.16
	3.80		669.96
18+61		10.5	
18+71		5.2	
18+82		0.2	
	12.73	681.90	0.19
	12.13	681.90	0.77
			0.77
	12.60	693.73	
18+90		12.6	
18+97		9.7	
19+00		0.9	
		0.23	693.50
	12.42	705.92	
19+25		11.3	
19+50		2.1	
		0.75	705.37

9-29-54

Left

~~spl. at angle~~ $\frac{3.3}{0}$ $\frac{5.3}{4}$ $\frac{7.5}{8}$ $\frac{16.2}{28}$

$\frac{11.0}{0}$ $\frac{15.0}{13}$ $\frac{17.4}{20}$ $\frac{20.4}{25}$

Set T.B.M. on rock 18+60, 20' Rb. creek bottom.

Right

Left

$\frac{4.0}{25}$ $\frac{4.8}{72}$ $\frac{8.9}{0}$ $\frac{11.2}{75}$ $\frac{12.6}{28}$

+4.1 +2.0 0.5 2.1 2.1 4.9 3.8
26 76 74 8 8 75 25

continue profiles

191 9-30-54

19150	12.94	705.17
19160	12.94	718.11
19173	12.94	718.11
19183	12.94	718.01
19191	12.16	730.17
20100	12.16	730.17
20111	12.16	730.17
20128	12.16	742.20
20150	12.16	742.20
20160	12.16	742.20
20180	12.13	754.27
21+67.78	12.13	754.27
20+84	12.13	754.27
21+00	12.13	754.27
21+19	12.13	754.27
21+50	12.13	754.27
5.71	759.11	

Right Left

+0.4	2.0	3.7	6.4	10.0	13.9	18.9
75	77	7	8	73	20	25

3.7	8.0	10.4	12.8
8	11	17	26

3.0	8.0	14.0
8	14	26

	742.32		
28+00		13.3	729.01
	12.39	13.31	729.01
28+10	3.77		732.78
28+11		6.4	
28+26		10.6	
28+50		4.7	
28+70		0.5	
		0.19	732.59
	12.55		745.14
29+00		5.0	
		0.22	744.92
	11.77		756.69
29+24		10.6	
		10.6	
29+50		6.8	
30+00		2.6	
30+19		2.4	
30+40.30		4.63	752.06
	6.57		758.63
30+80		4.6	
31+00		4.3	
31+50		4.1	
31+80		5.5	

	758.63		
31+92.93		6.28	752.35
	1.19	753.54	
32+00		1.1	
32+35		4.3	
32+50		8.1	
		12.82	740.72
	0.34	741.06	
32+73		4.2	
33+00		10.7	
		12.75	728.31
	0.38	728.69	
33+36		13.2	
		12.81	715.88
	0.94	716.32	
33+42		2.0	
33+50		6.5	
		12.14	704.18
	0.02	704.20	
33+68		3.1	
33+76		5.3	
		8.68	695.22
	0.13	695.44	

19/1/54

	740.72		
33+82		3.1	737.62
		1.8	735.82
33+88		6.2	729.62
		5.7	723.92
33+94		3.8	720.12
		12.08	708.04
		0.34	707.70
33+98		4.2	703.50
		10.7	692.80
		12.75	680.05
	0.38	680.43	
34+02		13.2	667.23
		12.81	654.42
	0.94	655.36	
34+12		2.0	653.36
34+20		6.5	646.86
		12.14	634.72
	0.02	634.74	
34+28		3.1	631.64
34+36		5.3	626.34
		8.68	617.66
	0.13	617.79	

Continue Profile

695.94

33+90

9.8

34+00

8.1

12.89 682.55

0.12 682.97

34+28

8.0

12.76 670.21

21.

0.93 671.14

34+36.21

2.56 668.56

34+50

9.8

34+53

11.0 658.31

34+59

11.4

34+61

10.6

12.05 671.09

21.

12.37 683.46

34+85.21

12.15 671.31

35+00

6.5

8.02 683.47

12.48 693.32

35+25

11.3

35+33

9.4

35+50

2.7

0.30 695.62

10.16 705.78

10-1-54

Handwritten notes at the top of page 22, including a date and possibly a location or project name.

705.78

35162

9.0

35183

3.9

0.13 705.65

10.84 716.49

36100

8.1

36122

2.1

0.31 716.18

12.58 728.76

36189

7.7

36150

4.2

0.19 728.57

2.68 738.25

37100

0.95 737.80

12.53 750.33

37120

8.5

37150

2.0

0.18 750.15

11.51 757.72

37180

6.0

P.L.

3719092

6.07

38100

6.6

38113

4.6

38150

4.2

10-1-54

21.50

2.1

22.61 23.8

2.1

2.1

2.1

2.1

2.1

2.1

22.61 23.8

2.1

2.1

2.1

22.61 23.8

2.1

2.1

2.1

22.61 23.8

2.1

2.1

2.1

2.1

22.61 23.8

2.1

21.50

757.72

39100
PI.
39108⁷²

7.5

8.50 749.22

0.90 750.12

39150

2.7

39179

6.0

40100

7.3

40117

9.0

40141

11.7

40159

12.70 737.42

40180

0.45 737.87

40150

1.2

41100

10.5

41120

12.59 725.28

41140

0.14 725.42

41130

2.9

41150

7.3

12.70 712.72

41187

0.71 713.43

42100

5.6

42100

7.7

42128

13.0

12.83 700.60

42150

0.40 701.00

10-1-54

39100	7.5	749.22
39150	2.7	
39179	6.0	
40100	7.3	
40117	9.0	
40141	11.7	
40159	12.70	737.42
40180	0.45	737.87
40150	1.2	
41100	10.5	
41120	12.59	725.28
41140	0.14	725.42
41130	2.9	
41150	7.3	
	12.70	712.72
41187	0.71	713.43
42100	5.6	
42100	7.7	
42128	13.0	
	12.83	700.60
42150	0.40	701.00

701.00

42134 2.9
 42150 7.3 693.7
 42150 11.89 689.11
 0.21 689.32
 43100 2.6
 43100 12.94 676.38
 0.62 677.00
 43130 4.0
 43150 9.6 672.12
 12.63 664.37
 0.21 664.58
 43171 2.6
 44100 9.9 651.96
 12.62 651.96
 0.30 652.26
 44129 4.7 647.29
 44150 8.6 638.69
 44170 17.9 620.79
 12.66 639.60
 0.54 640.14
 44185 5.5 634.65
 45100 10.7 629.0

10-1-54

Faint handwritten notes and numbers on the right page, including a date '10-1-54' at the top.

640.14

12.89 627.25

0.50 627.83

45+15 3.0

45+50 7.3

45+59 7.9

45+65 14.9

45+76 10.3

45+84 10.1

46+00 6.4

46+07 5.8

46+10 3.7

46+26 10.7

46+44 6.0

46+50 7.6 620.2

46+55 4.8

46+65 9.3

46+78 9.3

46+93 4.5

47+00 1.3

0.44 627.39

11.86 639.25

47+33 3.5

47+33 3.5
 47+34 3.5
 47+35 3.5
 47+36 3.5
 47+37 3.5
 47+38 3.5
 47+39 3.5
 47+40 3.5
 47+41 3.5
 47+42 3.5
 47+43 3.5
 47+44 3.5
 47+45 3.5
 47+46 3.5
 47+47 3.5
 47+48 3.5
 47+49 3.5
 47+50 3.5
 47+51 3.5
 47+52 3.5
 47+53 3.5
 47+54 3.5
 47+55 3.5
 47+56 3.5
 47+57 3.5
 47+58 3.5
 47+59 3.5
 47+60 3.5
 47+61 3.5
 47+62 3.5
 47+63 3.5
 47+64 3.5
 47+65 3.5
 47+66 3.5
 47+67 3.5
 47+68 3.5
 47+69 3.5
 47+70 3.5
 47+71 3.5
 47+72 3.5
 47+73 3.5
 47+74 3.5
 47+75 3.5
 47+76 3.5
 47+77 3.5
 47+78 3.5
 47+79 3.5
 47+80 3.5
 47+81 3.5
 47+82 3.5
 47+83 3.5
 47+84 3.5
 47+85 3.5
 47+86 3.5
 47+87 3.5
 47+88 3.5
 47+89 3.5
 47+90 3.5
 47+91 3.5
 47+92 3.5
 47+93 3.5
 47+94 3.5
 47+95 3.5
 47+96 3.5
 47+97 3.5
 47+98 3.5
 47+99 3.5
 48+00 3.5

	682.25	
47150		0.6
	17.91	0.04
	682.12	
48100		9.4
48118		8.3
48150		2.0
48170		0.6
		0.21
	12.75	664.66
48182		12.8
48198		8.8
49100		6.9
49105		5.2
49115		5.3
49140		0.3
		0.27
	13.06	677.45
49150		11.5
49178		8.1
49188		5.0
50100		3.2
50129		0.6

		677.45	
			0.55 676.90
	11.26	688.16	
50+30			9.2
50+77			3.8
			0.24 687.92
	12.40	700.32	
51+00			10.9
51+24			3.0
51+35			0.5
			0.44 699.88
	12.77	712.65	12.77
51+50			9.9
51+80			0.8
			0.30 712.35
	12.30	724.65	
52+00			4.6
			0.60 724.05
	11.06	736.01	
52+20			10.5
52+40			3.6
52+50			0.9 735.11
			0.36 735.68
	12.34	747.39	

10-9-54

	747.99	
52182		3.1
		0.11 747.88
	11.39 759.27	
53102		7.0 752.3
53121		5.5
53123		3.9
53136		1.4
		0.85 758.42
	9.80 768.22	
53150		8.4
53180		5.6
54100		2.9
		5.34 762.88
	1.33 ^{64.21} 717.57	
54113		2.7
54150		6.4
55100		11.0
55110		13.1
		12.86 ^{51.36} 758.35
	1.44 752.79	
P.I.		
55125.97		4.45 748.34
55150		7.1

base 10'x10'x10' rock

P.I.
52+92.91 P.I. Top rock 755.12 Elev.

base of rock

pile of 5 6'x6' rocks

base 6'x6' rock

752.79

12.92 752.87

55+07 - 0.33 740.20

56+00 3.3

56+06 5.7

56+21 9.9

56+50 13.6

12.42 722.78

0.92 726.86

56+62 3.4

56+65 4.8

57+00 5.0

57+08 7.8

12.98 716.32

1.89 721.35

57+15 9.5

57+23 12.9

57+33 9.3

57+50 7.5

57+69 12.6

57+80 12.56 711.59

1.73 713.32

57+89 6.1

10-9-54

Continued in F. 10-9-54
pp 22-23

	713.32	
57+91		12.91 713.32
58+00	0.33 710.26	11.9
58+100		12.02 701.30
58+200	0.90 702.20	
58+208.41		0.26
" " "		3.0
58+26		12.81 713.76
58+100	0.58 698.88	12.96 687.84
58+150	0.63 690.47	
58+150		0.7
58+162		4.7
58+184		16.7
		12.96 677.71
	0.26 677.97	
58+90		1.4
58+96		6.2
59+00		8.9
59+100		12.70 665.27
59+100	0.22 665.49	
59+111		4.4
59+133		9.2
59+136		13.3
	0.76 653.36	12.89 652.60

10-9-54

RAILROAD CURVE
AND
REVISION TABLES

© 1948 McGraw-Hill Book Co., New York City



Top 2x3x4' rock
Ground

CURVE FORMULAS

General Curve Formulas:
 $R = \frac{L^2}{8e}$
 $e = \frac{L^2}{8R}$
 $D = \frac{180}{\pi R}$
 $L = \frac{\pi R D}{180}$
 $\Delta = 2D \sin \frac{D}{2}$
 $M = R \left[1 - \cos \frac{D}{2} \right]$
 $T = R \tan \frac{D}{4}$
 $MA = M + AT = R \left[1 - \cos \frac{D}{4} \right] \tan \frac{D}{4}$
 $TA = AT + T = R \left[1 - \cos \frac{D}{4} \right] \tan \frac{D}{4} + T$
 $MA + TA = 2R \left[1 - \cos \frac{D}{4} \right] \tan \frac{D}{4} + T$
 $MA + TA = 2R \left[1 - \cos \frac{D}{4} \right] \tan \frac{D}{4} + T$
 ... (The text continues with detailed explanations of the formulas and their applications in railroad engineering.)

*Continued in F.B. 873
 pgs 55-62*

F.B. 898A

pp (1-6)

Final Stations (based
on Field Survey)

1

SAN VICENTE AQUEDUCT CONN.
R-2 REVISED ALIGNMT.

8+00 P.O.T.

6+74⁷⁵
~~6+71³⁸~~ P.O.T. (= 6+44²⁶ Orig. Align.)
6+47⁴⁷
 Δ 10°06' RT to P.I. 7+45³¹
10°02'30" RT. 5 70°00' E

4+77⁰⁰
~~4+73⁹⁶~~ P.I. Δ 10°02'30" LT
10°03'07" LT. 5 60°10' E

3+73⁹⁶ P.I. Δ 9°12'15" LT.
5 51°00' E

0+97⁰¹
~~0+47⁰²~~ P.O.T.
0+30 P.O.T.

0+10 P.I. Δ 42°29'15" RT. (Not set)

0+00 In discharge Channel (Not set)

0-45 Face Tunnel Portal

SEPT. 27, 1954

BEATTY
SHOREY
ALEXANDER
T. BERGER-29611

1

S.V.A. CONN. R-2 REV. ALIGN.

8+00
P.O.T.

P.I. 7+453

6+74.75

6+47.47

6+77.38 POT = 6+42.06 ORIG
ALIGN.

10°06'
10°02'30"

ORIG

4+77.00

4+73.96 P.I.

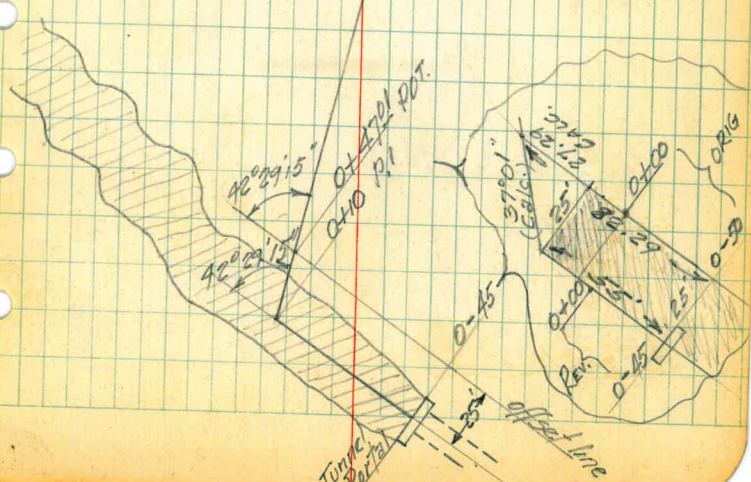
Δ 10°03'00" LT.
10°02'30"

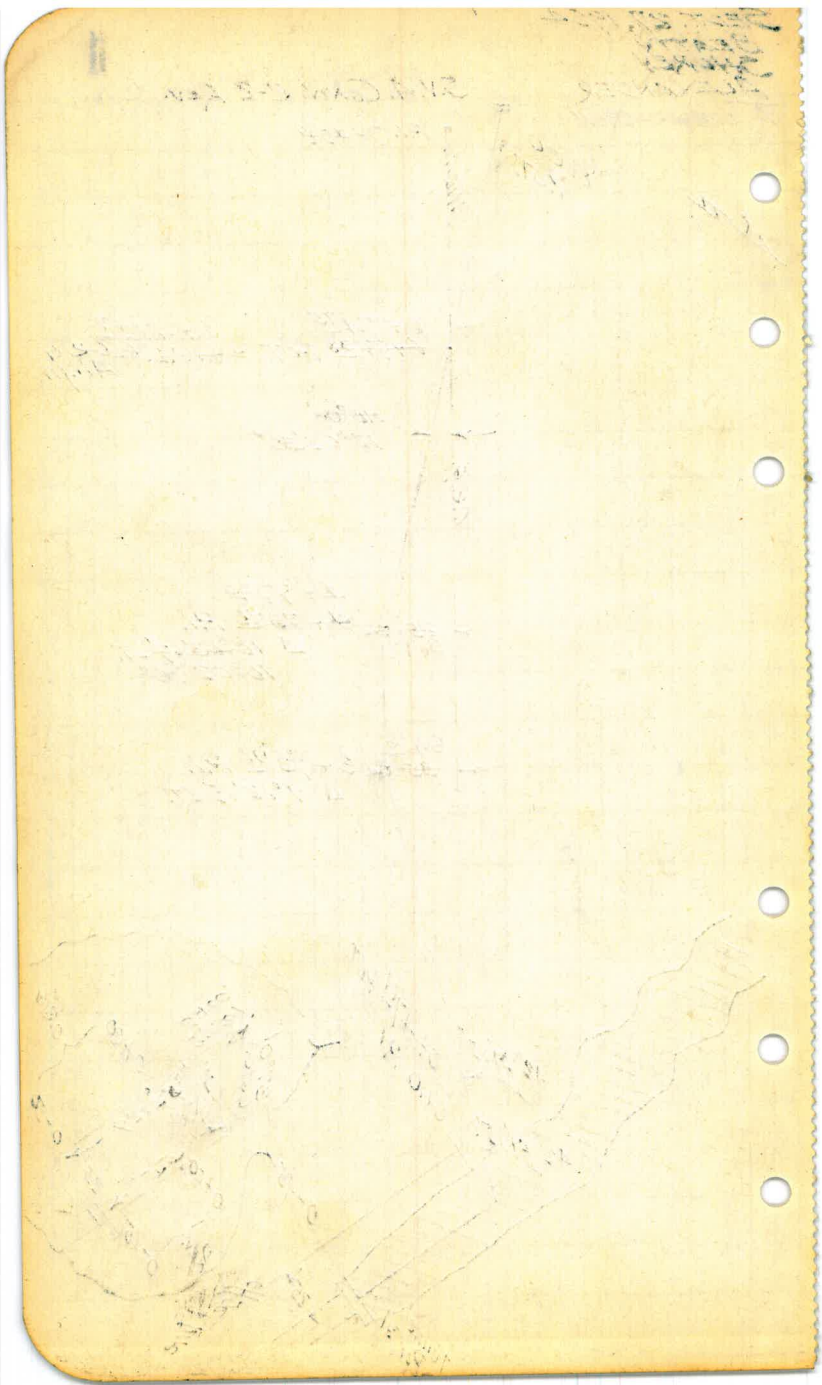
34.70

35

3+73.96 P.I.

Δ 9°12'15" LT.





21
The first thing I did
was to go to the
bank and get some
money out of the
machine. I was
lucky and got
the amount I
needed. I then
went to the
store and bought
some food. I
was very happy
to see the
manager and
the staff. They
were all very
friendly and
helpful. I
enjoyed my
visit very much.
I will be
back soon.

2

SAN VICENTE AQUEDUCT CONN.
R-2 REVISED ALIGN'MT.

15+95⁰⁹ P.I. Δ (23'-90" LT 15780 ORIG.)

S 85°00' E

14+99⁵⁰ P.I. Δ 8°58' LT (17'-90" LT 14+84⁵ ORIG.)

S 76°00' E

14+14⁸⁹ P.I. Δ 5°50' LT (25'-90" LT 14+100 ORIG.)

S 70°15' E

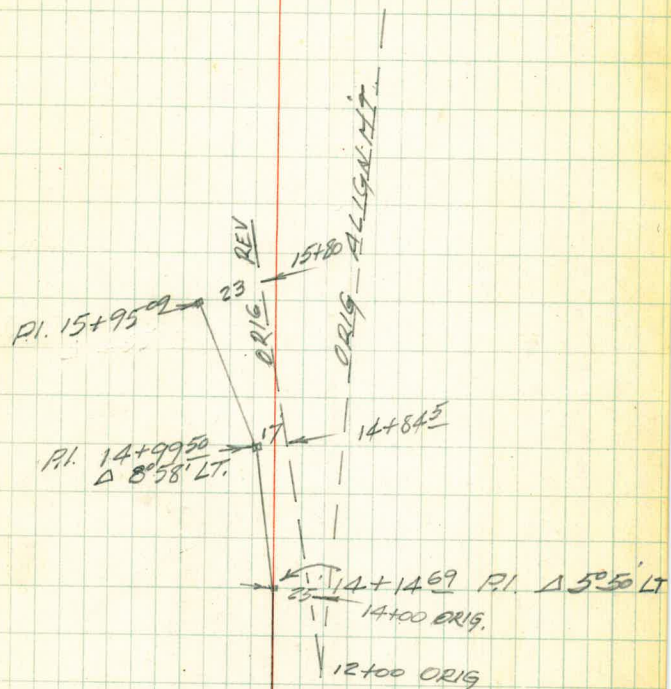
10+00 P.O.T.

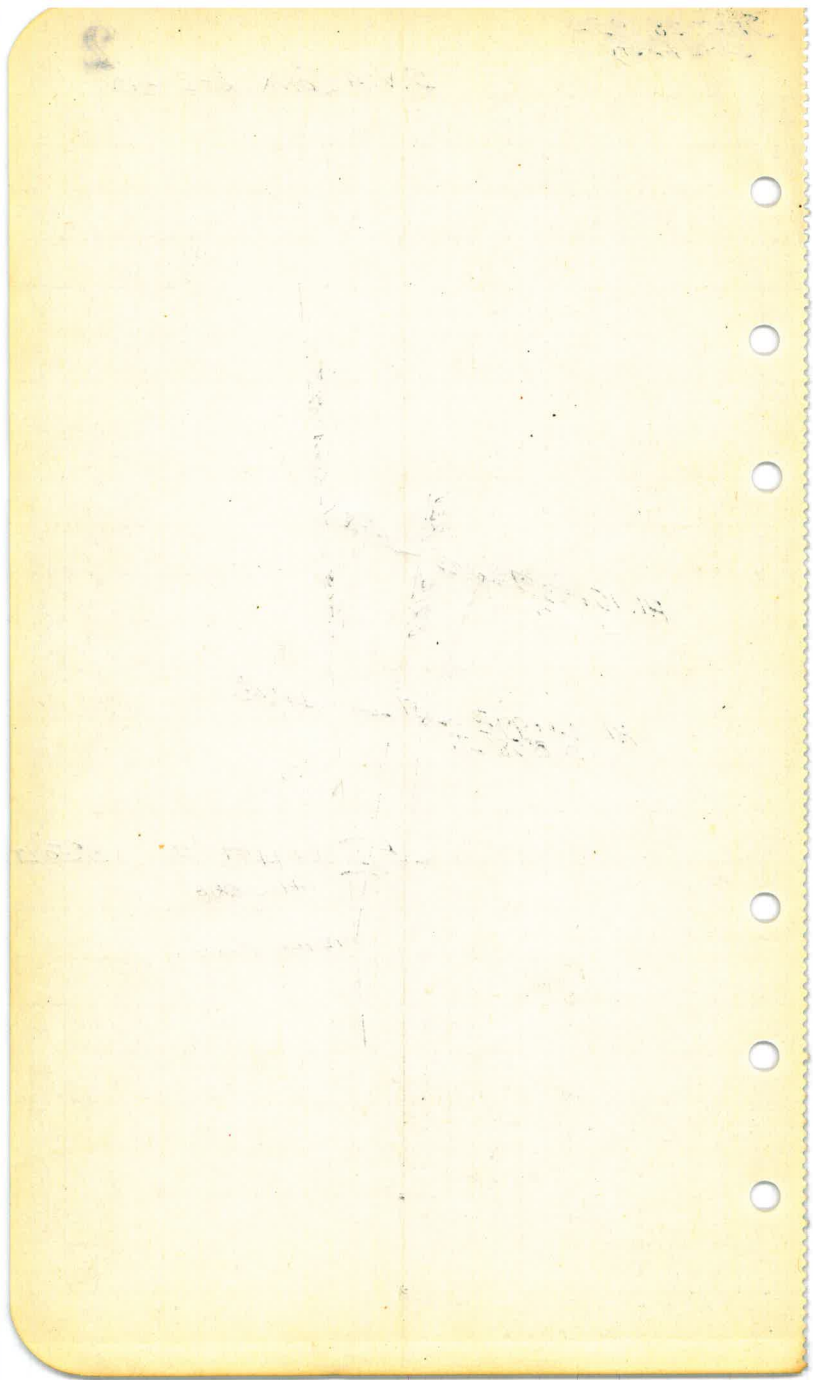
8+00 P.O.T.

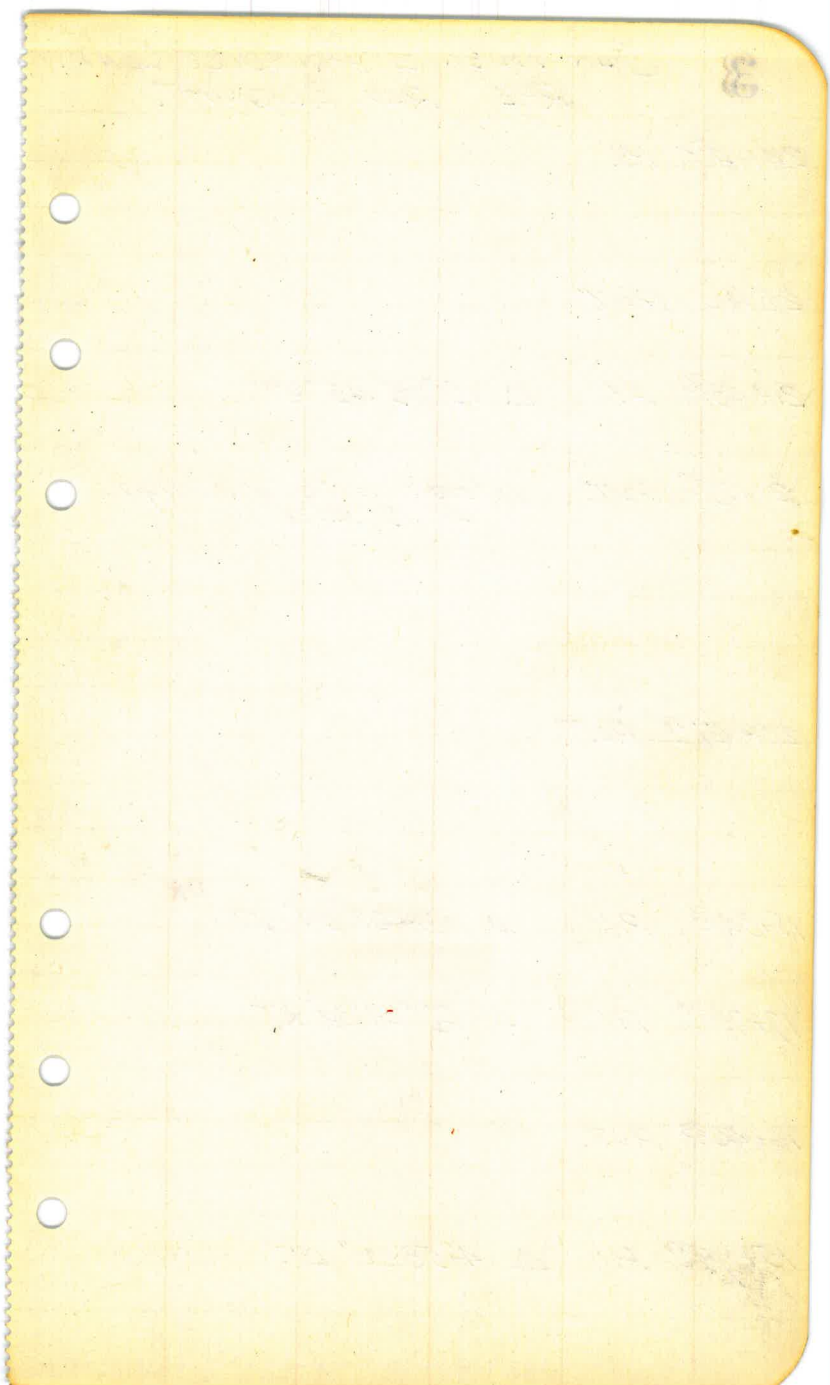
S 70°00' E

SEPT. 28, 1954
SAME PARTY

S.V.A CONN. R-2 REV. 2







3

SAN VICENTE AQUEDUCT CONN.
R-2 REV. ALIGNMT.

24+14⁷⁵ P.I.

22+00 P.O.T.

21+43⁵⁶ P.I. Δ 15°05'45" RT.

21+13³⁷ P.O.T. Intersn with Orig. Align.
 Δ 13°24'30"

20+67⁷⁸ P.O.T.

18+34⁸⁶ P.I. Δ ~~39°22'30"~~ LT. OK

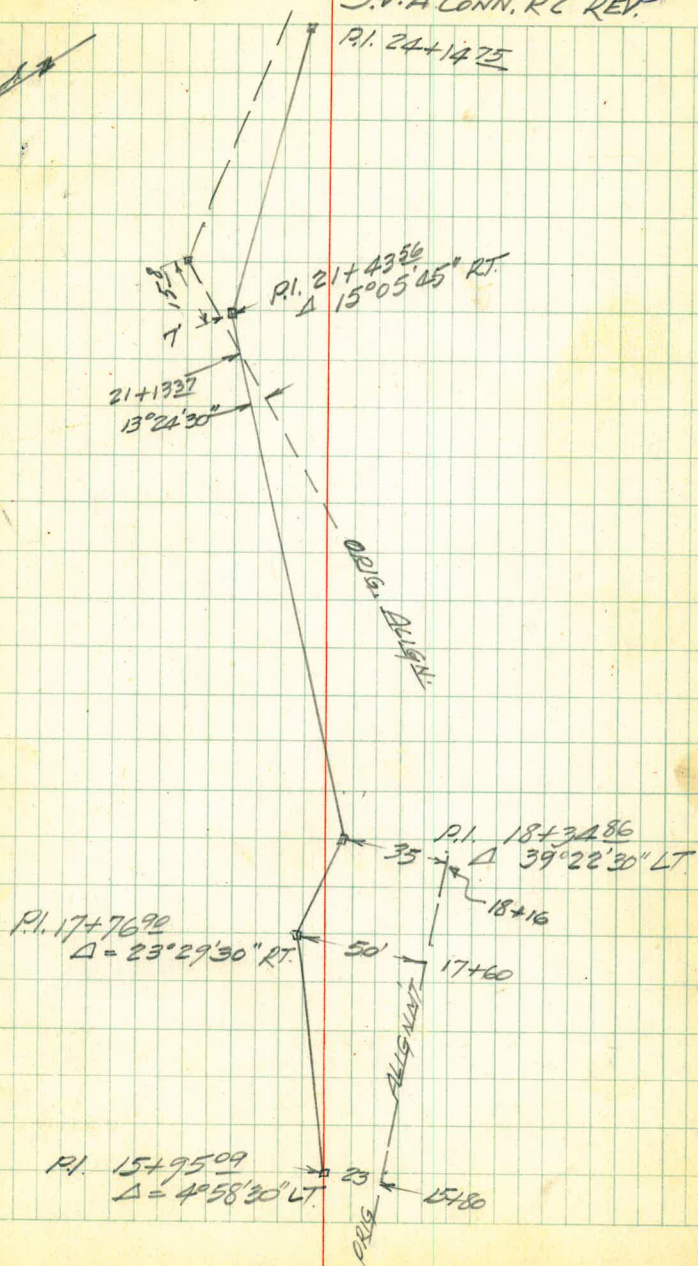
17+76⁹⁰ P.I. Δ 23°29'30" RT.

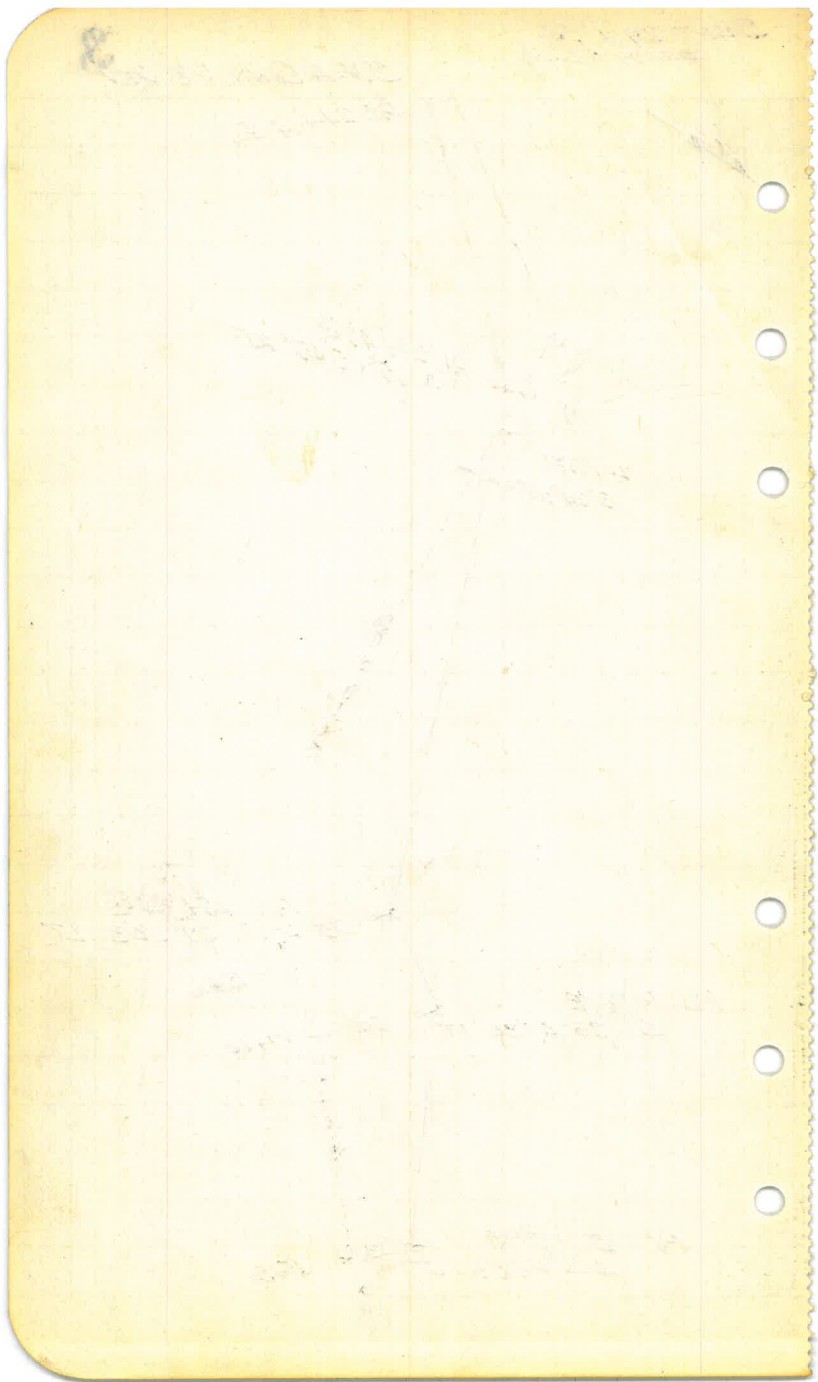
16+46⁹³ P.O.T.

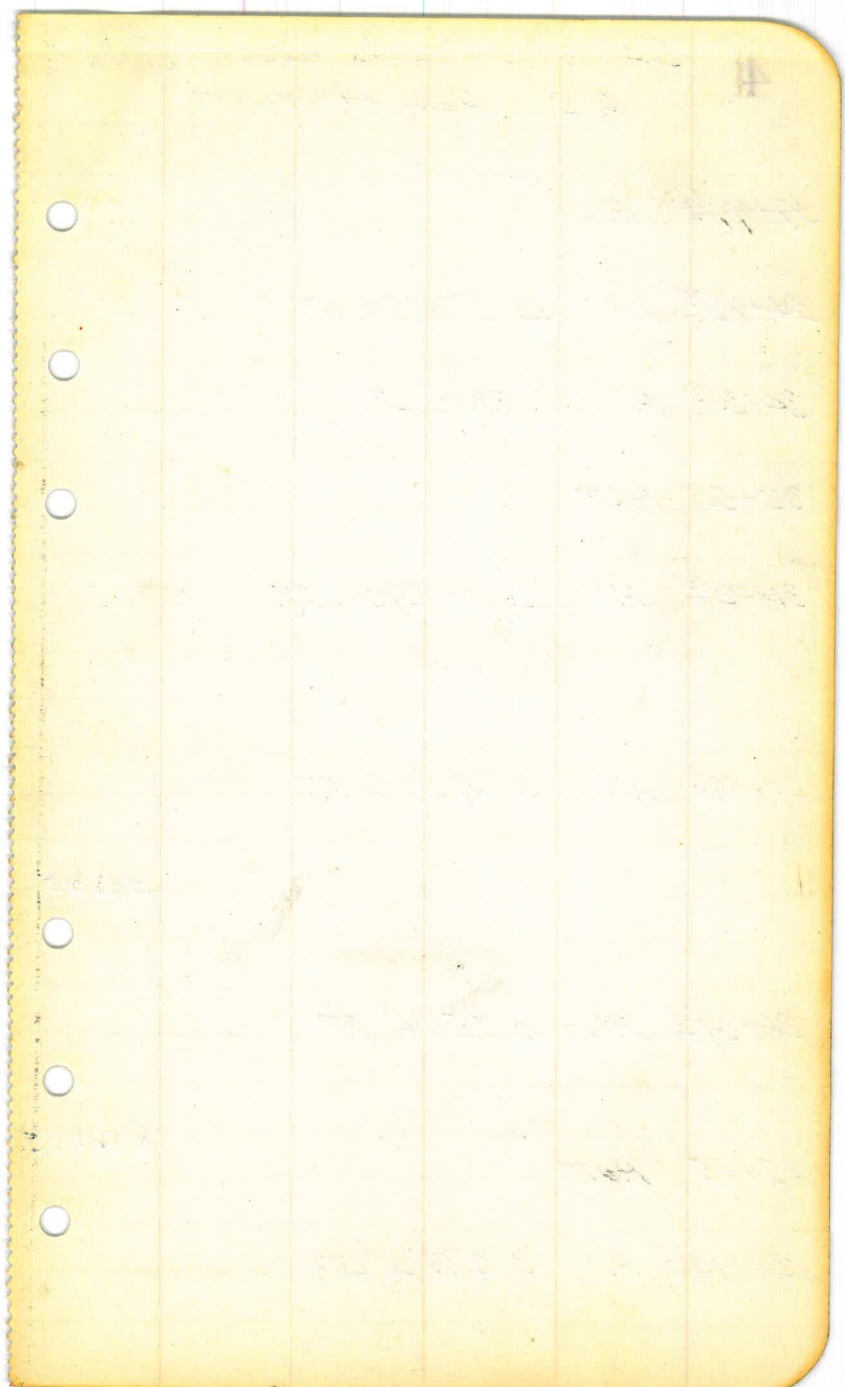
15+95⁹⁹ P.I. Δ 4°58'30" LT.

SEPT 29, 1954
BEATTY # party

S.V.A. CONN. R2 REV. 3







4

SAN VICENTE ARQUEDUCT CONN
R2 REV. Alignment~~37+97⁴⁶~~ P.I.34+85³¹ P.I. Δ 5°30'30" LT34+36²¹ P.I. Δ 8°03' LT

32+50 P.O.T.

31+92²⁹ P.I. Δ 16°29'30" RT30+48³⁰ P.I. Δ 29°35'15" RT

S 58°00' E

26+39⁴³ P.I. Δ 35°46' RT

N 86°45' E

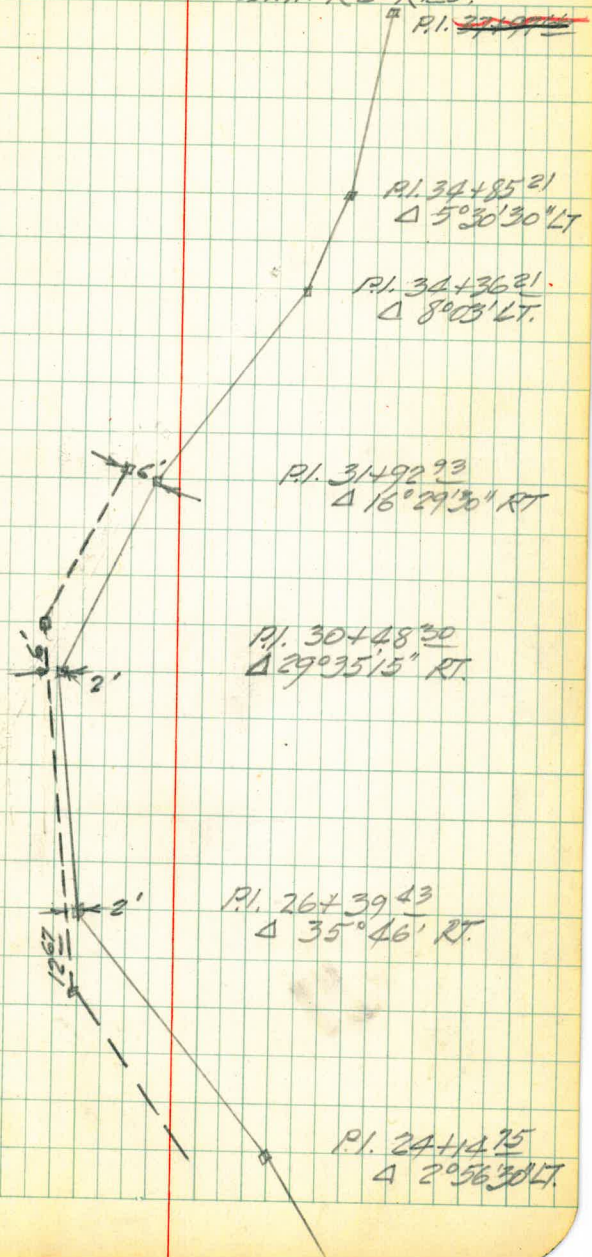
25+65 P.O.T.

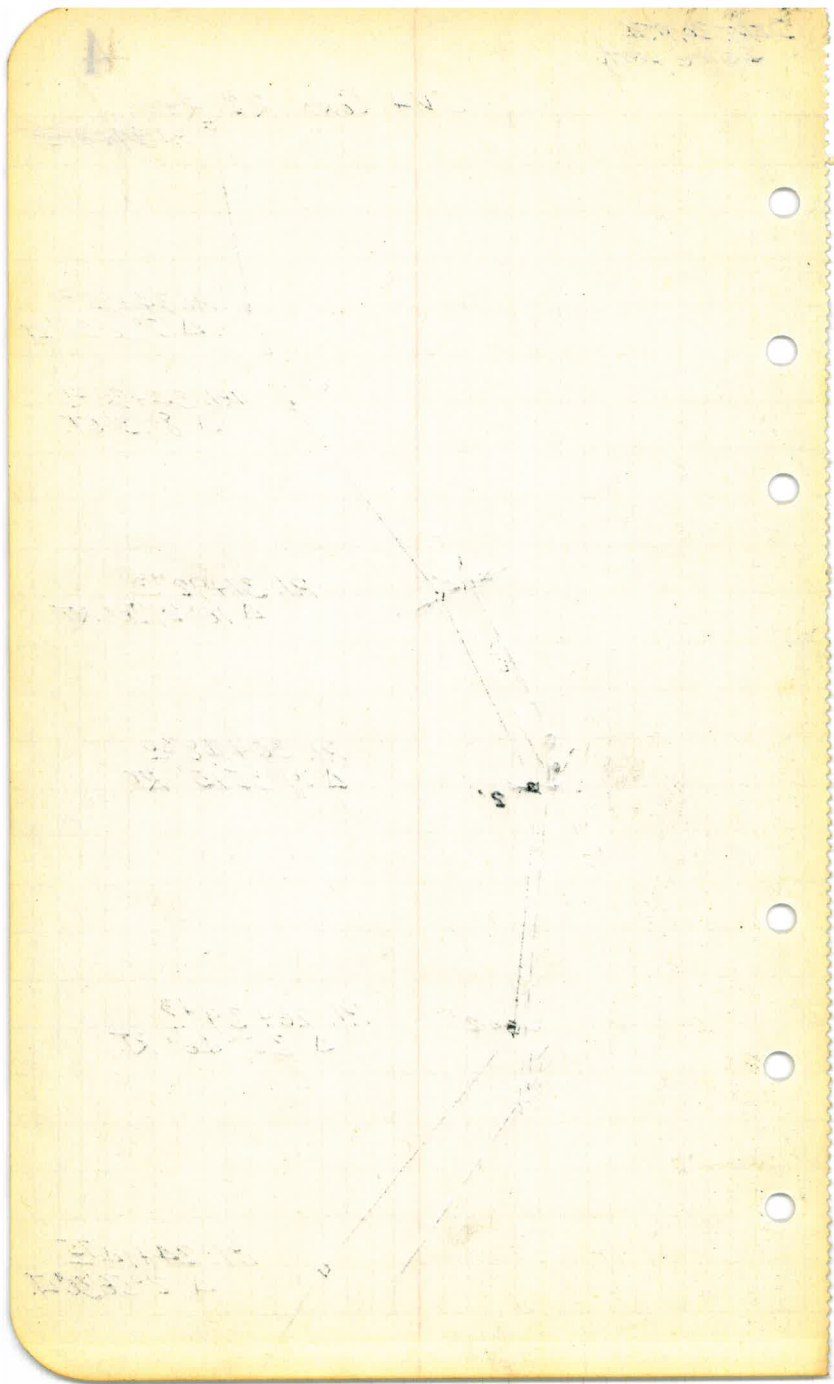
24+14⁷⁵ P.I. Δ 2°56'30" LT

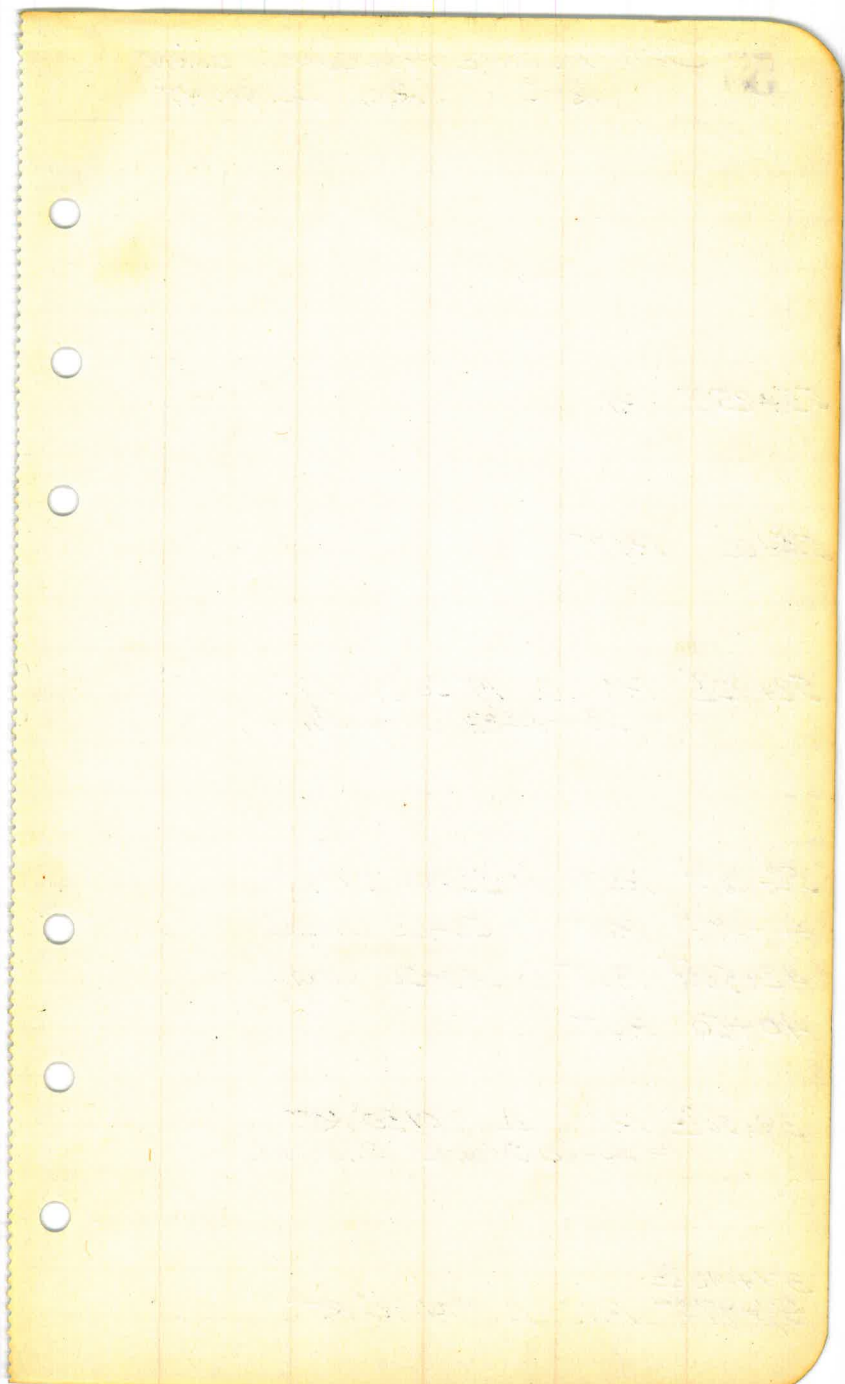
SEPT. 30, 1954
Same party

4

JVA. CONT. R2 REV.







5

SAN VICENTE AQUEDUCT CONN.
R-2 REV. ALIGN.'MT.

55+2597 P.I.

54+00 P.O.T.

52+929 P.I. Δ 19°26'30" LT.
(= 53+84.63 Orig. Align.)52+08⁸⁸ P.O.T. (= 53+00 Orig.)49+08⁸⁶ P.O.T. (= 50+00 Orig.)42+58⁵⁵ P.O.T. (= 43+50 Orig.)

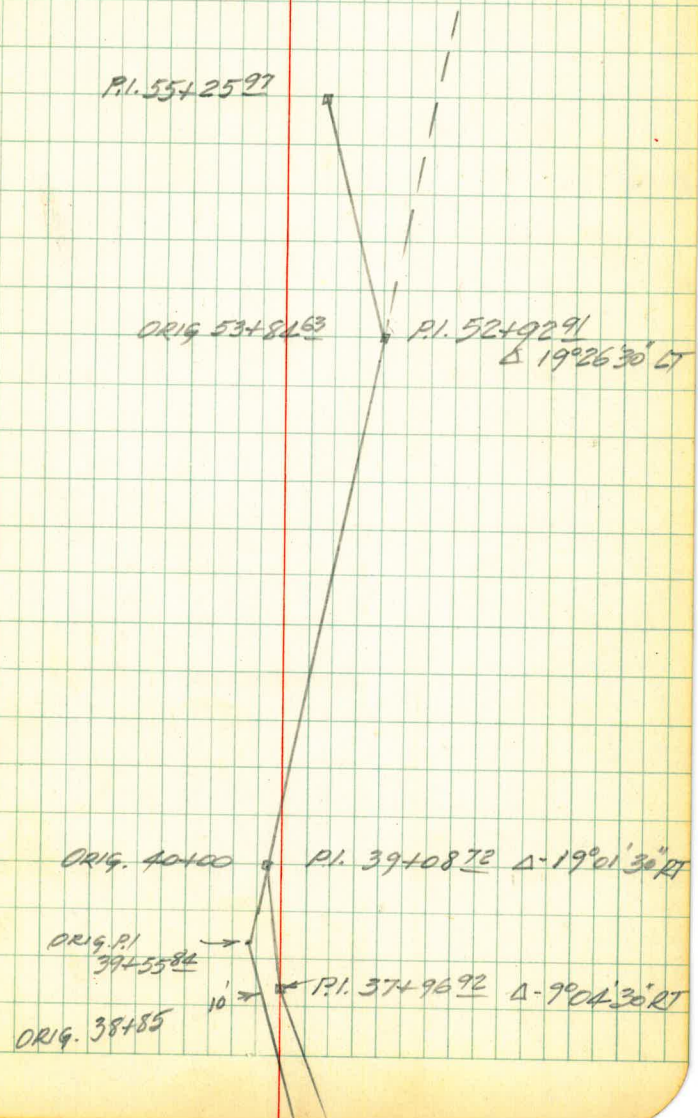
40+50 P.O.T.

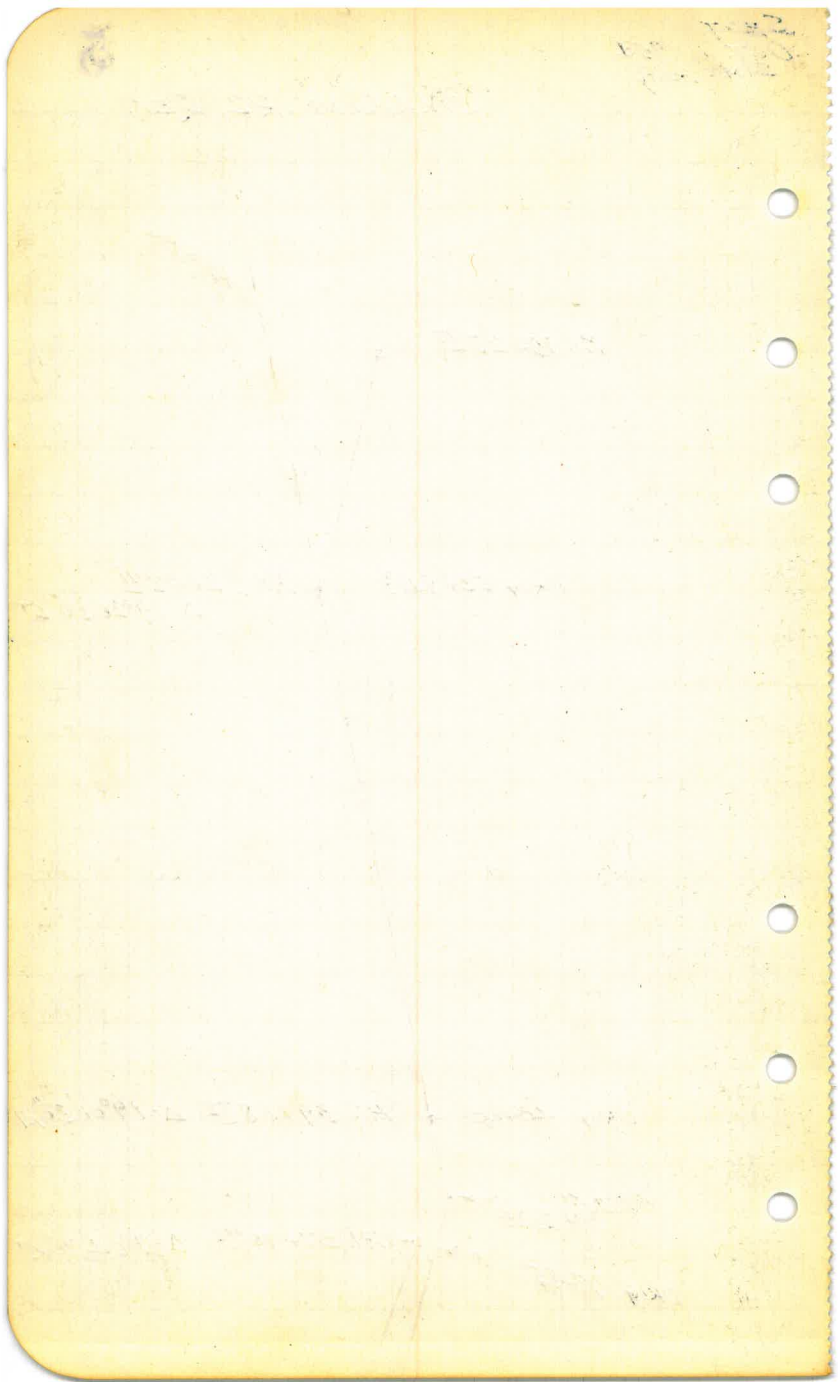
39+08³² P.I. Δ 19°01'30" RT.
(= 40+00 Original Align. mt.)37+96⁷²37+97⁶⁶ P.I. Δ 9°04'30" RT.

SEPT
OCT. 1, 1954
SAME Party

5

S.V.A. CONN. R2 REV.





[Faint, illegible handwriting on a yellowed, lined page with punch holes.]

6

SAN VICENTE AQUEDUCT CONN.
R2 REV. ALIGNMENT75+00⁹⁵ P.O.T. Intersect San Vicente #272+88⁵⁸ P.O.T. Intersect San Vicente #1.69+69⁵⁸ P.I. $\Delta 1^{\circ}25'45''$ LT
(= 71+00 ORIG.)

66+00 P.O.T.

64+08¹⁰ P.O.T.61+95²³ P.O.T.

58+84 P.O.T.

58+08⁴¹ P.I. $\Delta \begin{matrix} 16^{\circ}52'15'' \\ 17^{\circ}42'30'' \end{matrix}$ LT.

57+50 P.O.T.

55+25⁹⁷ P.I. $\Delta 15^{\circ}49'15''$ LT.

OCT. 4 1954

" 5

BEATTY
SHOREY
MARTELL
ALEXANDER

SVA CONN. R-2 REV.

6

SAN VICENTE #2 $\sqrt{7540075}$

SAN VICENTE #1 $\sqrt{72+8858}$

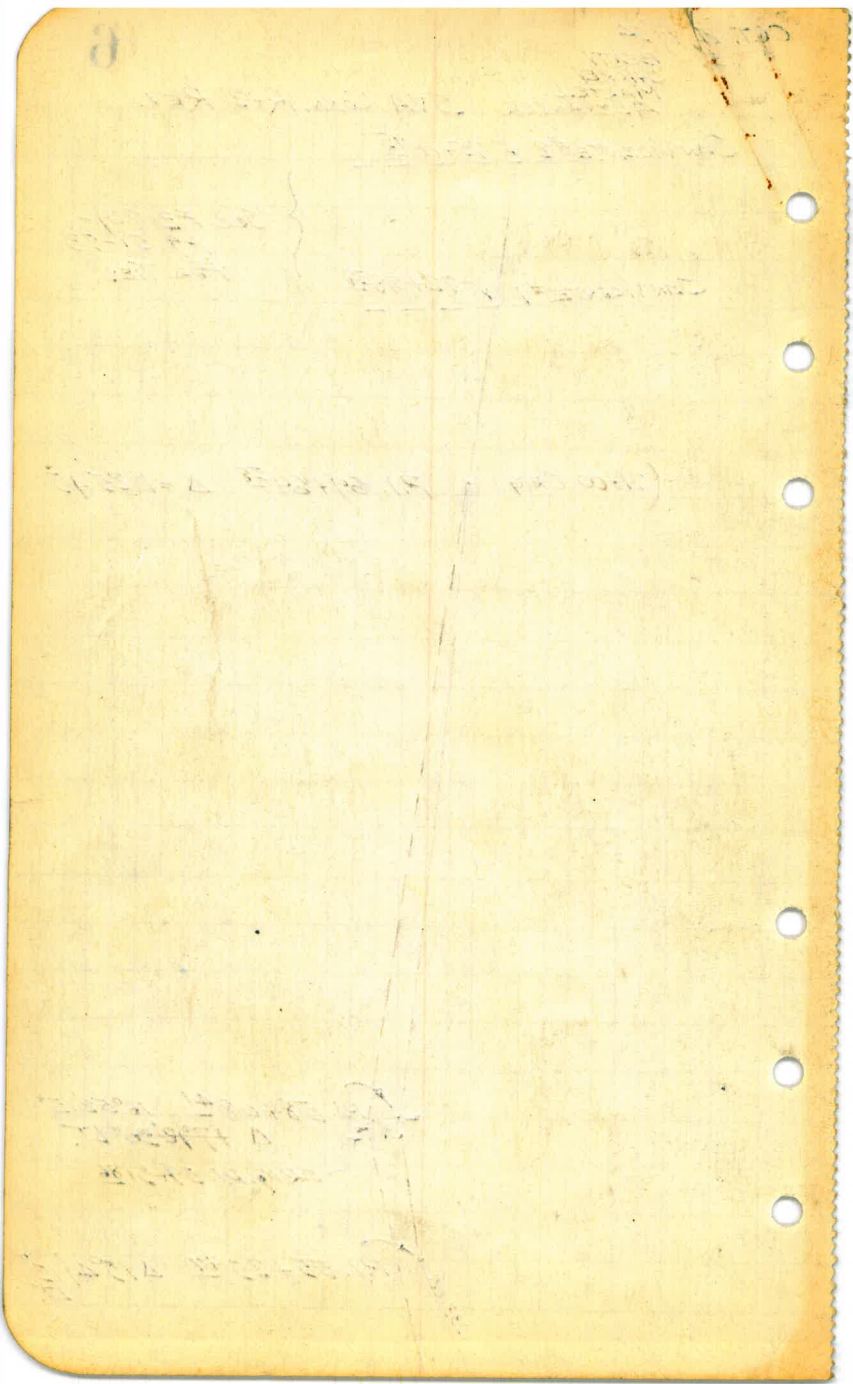
} Sec. FB 869-
Pg. 51-53
For TIES.

(71400 ORIG.) P.I. 69+69⁵⁸ $\Delta = 1^{\circ}25'45''$

P.I. 58+08⁴¹ $16^{\circ}52'15''$
 $\Delta 1790'30''$ LT.
ORIG. P.I. 59+3186

P.I. 55+25⁹⁷ $\Delta 15^{\circ}49'15''$
LT.

233.0



F.B. 898A

PP 7-30

Final Alignment Profile

(based on Field Survey)

Cont. F.B. 873
PPs. 55-62

Station	Profile	Profile	Profile
10+00	10+00	10+00	10+00
10+10	10+10	10+10	10+10
10+20	10+20	10+20	10+20
10+30	10+30	10+30	10+30
10+40	10+40	10+40	10+40
10+50	10+50	10+50	10+50
10+60	10+60	10+60	10+60
10+70	10+70	10+70	10+70
10+80	10+80	10+80	10+80
10+90	10+90	10+90	10+90
11+00	11+00	11+00	11+00
11+10	11+10	11+10	11+10
11+20	11+20	11+20	11+20
11+30	11+30	11+30	11+30
11+40	11+40	11+40	11+40
11+50	11+50	11+50	11+50
11+60	11+60	11+60	11+60
11+70	11+70	11+70	11+70
11+80	11+80	11+80	11+80
11+90	11+90	11+90	11+90
12+00	12+00	12+00	12+00
12+10	12+10	12+10	12+10
12+20	12+20	12+20	12+20
12+30	12+30	12+30	12+30
12+40	12+40	12+40	12+40
12+50	12+50	12+50	12+50
12+60	12+60	12+60	12+60
12+70	12+70	12+70	12+70
12+80	12+80	12+80	12+80
12+90	12+90	12+90	12+90
13+00	13+00	13+00	13+00
13+10	13+10	13+10	13+10
13+20	13+20	13+20	13+20
13+30	13+30	13+30	13+30
13+40	13+40	13+40	13+40
13+50	13+50	13+50	13+50
13+60	13+60	13+60	13+60
13+70	13+70	13+70	13+70
13+80	13+80	13+80	13+80
13+90	13+90	13+90	13+90
14+00	14+00	14+00	14+00
14+10	14+10	14+10	14+10
14+20	14+20	14+20	14+20
14+30	14+30	14+30	14+30
14+40	14+40	14+40	14+40
14+50	14+50	14+50	14+50
14+60	14+60	14+60	14+60
14+70	14+70	14+70	14+70
14+80	14+80	14+80	14+80
14+90	14+90	14+90	14+90
15+00	15+00	15+00	15+00
15+10	15+10	15+10	15+10
15+20	15+20	15+20	15+20
15+30	15+30	15+30	15+30
15+40	15+40	15+40	15+40
15+50	15+50	15+50	15+50
15+60	15+60	15+60	15+60
15+70	15+70	15+70	15+70
15+80	15+80	15+80	15+80
15+90	15+90	15+90	15+90
16+00	16+00	16+00	16+00
16+10	16+10	16+10	16+10
16+20	16+20	16+20	16+20
16+30	16+30	16+30	16+30
16+40	16+40	16+40	16+40
16+50	16+50	16+50	16+50
16+60	16+60	16+60	16+60
16+70	16+70	16+70	16+70
16+80	16+80	16+80	16+80
16+90	16+90	16+90	16+90
17+00	17+00	17+00	17+00
17+10	17+10	17+10	17+10
17+20	17+20	17+20	17+20
17+30	17+30	17+30	17+30
17+40	17+40	17+40	17+40
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17+60	17+60	17+60	17+60
17+70	17+70	17+70	17+70
17+80	17+80	17+80	17+80
17+90	17+90	17+90	17+90
18+00	18+00	18+00	18+00
18+10	18+10	18+10	18+10
18+20	18+20	18+20	18+20
18+30	18+30	18+30	18+30
18+40	18+40	18+40	18+40
18+50	18+50	18+50	18+50
18+60	18+60	18+60	18+60
18+70	18+70	18+70	18+70
18+80	18+80	18+80	18+80
18+90	18+90	18+90	18+90
19+00	19+00	19+00	19+00
19+10	19+10	19+10	19+10
19+20	19+20	19+20	19+20
19+30	19+30	19+30	19+30
19+40	19+40	19+40	19+40
19+50	19+50	19+50	19+50
19+60	19+60	19+60	19+60
19+70	19+70	19+70	19+70
19+80	19+80	19+80	19+80
19+90	19+90	19+90	19+90
20+00	20+00	20+00	20+00
20+10	20+10	20+10	20+10
20+20	20+20	20+20	20+20
20+30	20+30	20+30	20+30
20+40	20+40	20+40	20+40
20+50	20+50	20+50	20+50
20+60	20+60	20+60	20+60
20+70	20+70	20+70	20+70
20+80	20+80	20+80	20+80
20+90	20+90	20+90	20+90

7

San Vicente Aqueduct Connection

Rev. & Profile & X Sections

		765.66	
P.I.	0.89	766.55	
0+30			10.11 756.44
	0.46	756.90	
P.O.			0.7 756.2
0+47 ⁰¹			3.2 753.7
0+65			9.3 747.6
0+74			12.49 744.41
T.P.			
	0.17	744.58	
0+86			4.3 740.28
1+00			7.2 737.38
1+25			13.7 730.88
T.P.			12.52 732.06
	3.80	735.86	
1+50			13.6 722.26
T.P.			12.96 722.90
	4.32	727.22	
T.P.			12.27 714.95
	1.82	716.77	
1+70			4.8 711.97
1+75			8.2 708.57
1+90			6.3 710.47

7

9-28-54

Wert
Kemp
Holahan

El. top So. portal

2

18 12 18
18 12 18
18 12 18
18 12 18

18 12 18

8

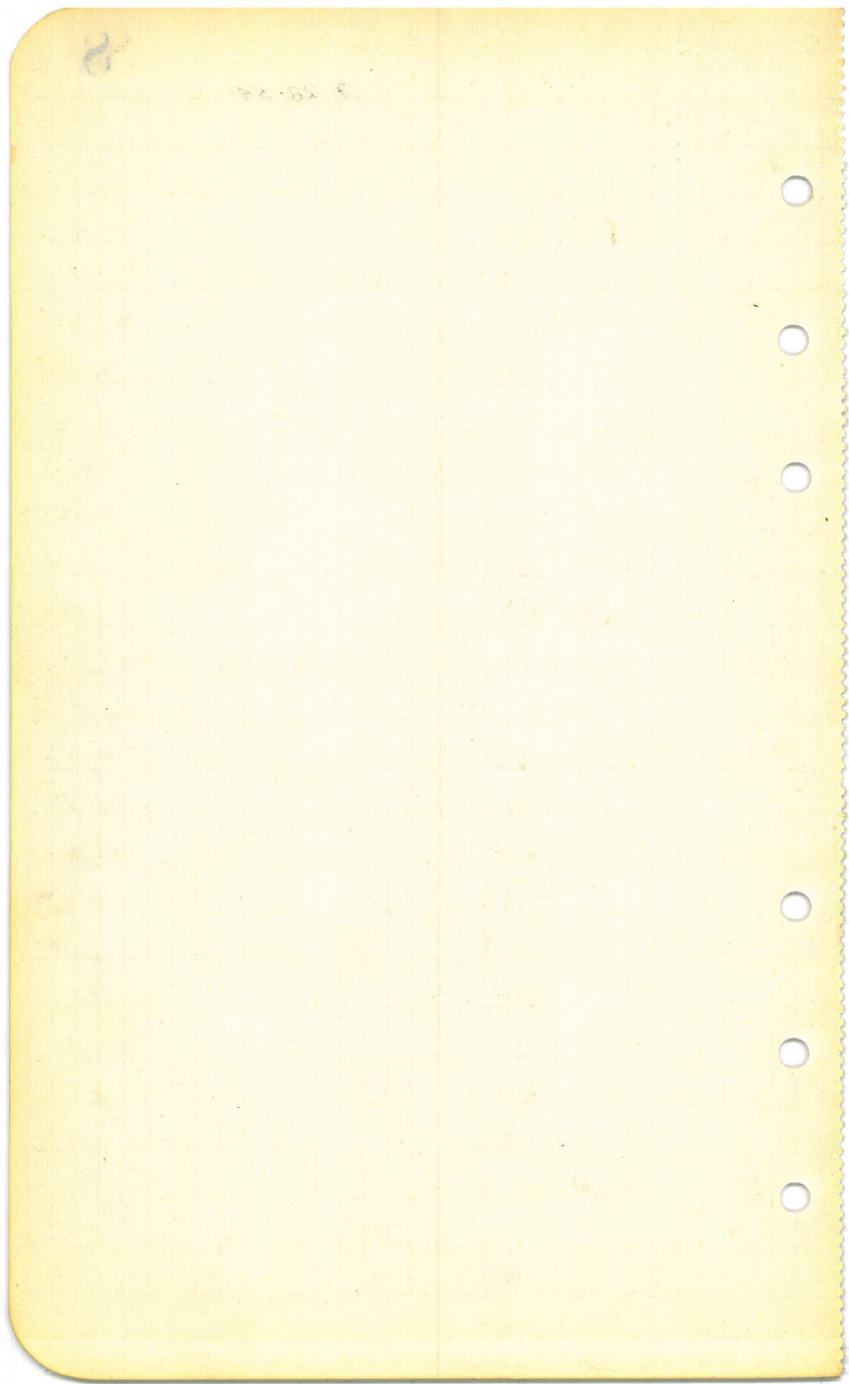
		77 317	
	20		2400
	28		2402
	18		2410
	25 22 24		24
		30 22 24	
	22		2420
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	20		2420
	21		2420
	20 22 24		2420
		31 22 24	
	20		2400
	18		2402
	22		2420
	21		2420
	20		2420
	22		2420
	21 22 24		24
		22 22 24	
	21 22 24		24
	22		2400

8

	716.77		
2+00		7.0	709.77
2+05		4.8	711.97
2+20		1.8	714.97
T.P.		0.18	716.59
	9.77	726.36	
2+50		6.5	719.86
3+00		1.8	724.56
3+50		3.0	723.36
3+55		3.1	723.26
3+73		5.97	720.39
	1.71	722.10	
4+00		9.0	713.10
4+15		11.3	710.80
4+22		16.7	705.40
4+28		14.7	707.40
4+33		2.8	712.30
4+50		3.5	718.60
T.P.		1.67	720.43
	11.59	732.02	
T.P.		0.25	731.77
	5.06	736.83	
3 4+77.0		2.51	727.32
5+00		3.5	733.33

9-28-54

8



Time	Location	Notes	Time	Location	Notes
23:00	23:00
23:05	23:05
23:10	23:10
23:15	23:15
23:20	23:20
23:25	23:25
23:30	23:30
23:35	23:35
23:40	23:40
23:45	23:45
23:50	23:50
23:55	23:55
00:00	00:00
00:05	00:05
00:10	00:10
00:15	00:15
00:20	00:20
00:25	00:25
00:30	00:30
00:35	00:35
00:40	00:40
00:45	00:45
00:50	00:50
00:55	00:55
01:00	01:00

		736.83		
T.P.			0.16	736.67
	12.10	749.07		
5+07			13.5	735.57
5+13			12.6	736.47
5+20			10.5	738.57
5+34			8.4	740.67
5+50			5.2	743.87
5+80			1.6	747.47
T.P.			1.04	748.03
	7.21	755.24		
P.O.T.				
5+98.62			6.05	749.19
6+18			3.6	751.64
6+50			4.4	750.84
6+74.75			5.4	749.84
7+00			4.4	750.84
7+07			3.1	752.14
7+50			5.7	749.54
7+75			5.2	750.04
8+00			7.56	747.68
			12.93	742.31
	0.20	742.51		

9-28-54

$$750.84 \quad 16.$$

$$\frac{4.4}{0}, \quad \frac{11.9}{75}, \quad \frac{16.2}{28}$$

$$749.84$$

$$\frac{5.7}{0}, \quad \frac{12.9}{9}, \quad \frac{15.5}{25}$$

$$750.04$$

$$\frac{5.2}{0}, \quad \frac{9.7}{70}, \quad \frac{13.7}{20}, \quad \frac{15.7}{25}$$

8

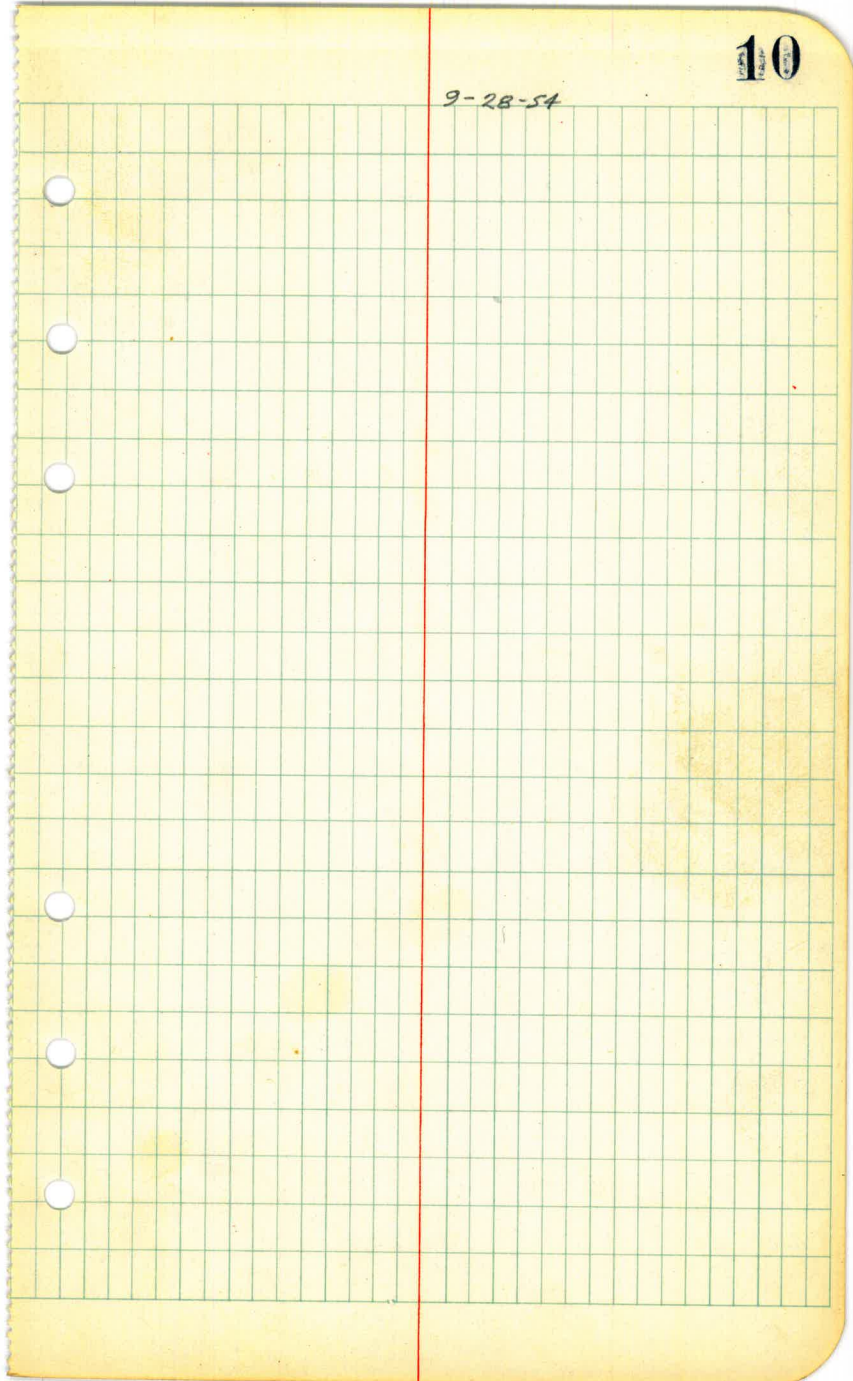
2-25-24

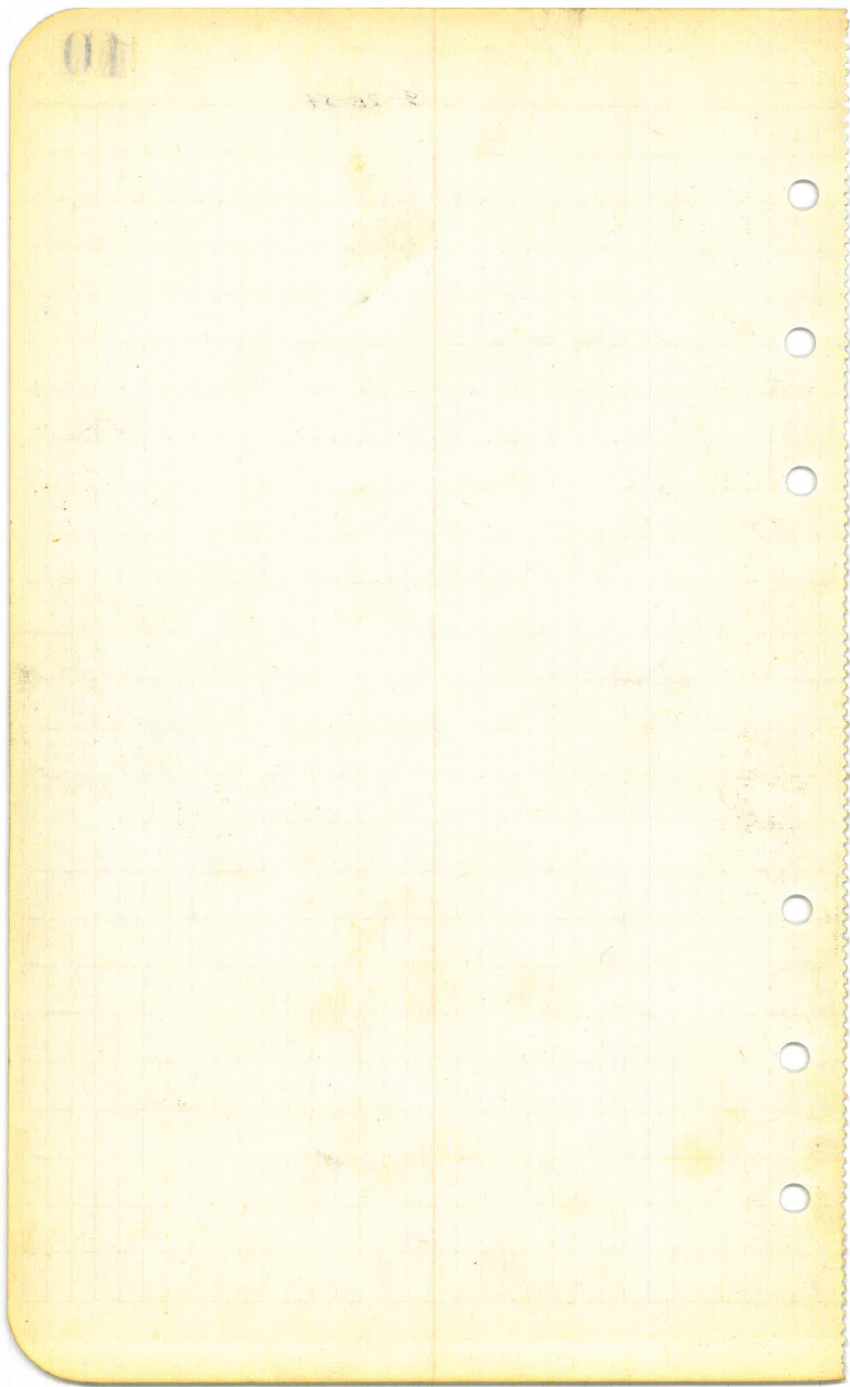
100	100	100	100
100	100	100	100
100	100	100	100
100	100	100	100

10	10	10	10	10
20	20	20	20	20
30	30	30	30	30
40	40	40	40	40
50	50	50	50	50
60	60	60	60	60
70	70	70	70	70
80	80	80	80	80
90	90	90	90	90
100	100	100	100	100
110	110	110	110	110
120	120	120	120	120
130	130	130	130	130
140	140	140	140	140
150	150	150	150	150
160	160	160	160	160
170	170	170	170	170
180	180	180	180	180
190	190	190	190	190
200	200	200	200	200

		742.51		
8+50			7.0	735.51
8+60			10.0	732.51
8+75			13.0	729.51
T.P.			12.70	729.81
	0.71	730.52		
9+00			5.3	725.22
9+41			9.2	721.92
9+50			8.8	721.72
9+75			7.2	723.32
10+00			9.2	721.32
10+14			13.0	717.52
			12.83	717.69
	1.18	718.87		
10+42			13.0	705.87
			12.84	706.03
	0.53	706.56		
10+50			4.1	702.46
10+60			7.8	698.76
10+72			12.5	694.06
			12.40	694.16
	1.36	695.52		

9-28-54





Year	Month	Day	Time	Location	Notes
1921	11	20	11:20		
1921	11	21	11:21		
1921	11	22	11:22		
1921	11	23	11:23		
1921	11	24	11:24		
1921	11	25	11:25		
1921	11	26	11:26		
1921	11	27	11:27		
1921	11	28	11:28		
1921	11	29	11:29		
1921	11	30	11:30		
1921	12	01	11:31		
1921	12	02	11:32		
1921	12	03	11:33		
1921	12	04	11:34		
1921	12	05	11:35		
1921	12	06	11:36		
1921	12	07	11:37		
1921	12	08	11:38		
1921	12	09	11:39		
1921	12	10	11:40		
1921	12	11	11:41		
1921	12	12	11:42		
1921	12	13	11:43		
1921	12	14	11:44		
1921	12	15	11:45		
1921	12	16	11:46		
1921	12	17	11:47		
1921	12	18	11:48		
1921	12	19	11:49		
1921	12	20	11:50		
1921	12	21	11:51		
1921	12	22	11:52		
1921	12	23	11:53		
1921	12	24	11:54		
1921	12	25	11:55		
1921	12	26	11:56		
1921	12	27	11:57		
1921	12	28	11:58		
1921	12	29	11:59		
1921	12	30	12:00		

11

695.52

10+92

10.7 684.82

11+00

12.3 683.22

T.P.

12.89 682.63

0.40 683.03

11+40

12.5 670.53

12.84 670.19

1.79 671.98

11+50

6.0 665.98

11+57

8.4 663.58

8.95 663.03

continue 9-29-54

0.85 663.88

11+75

4.0 659.88

11+90

7.8 656.08

12+00

11.2 652.68

12.57 651.31

1.16 652.47

12+15

5.8 646.67

12+27

11.2 641.27

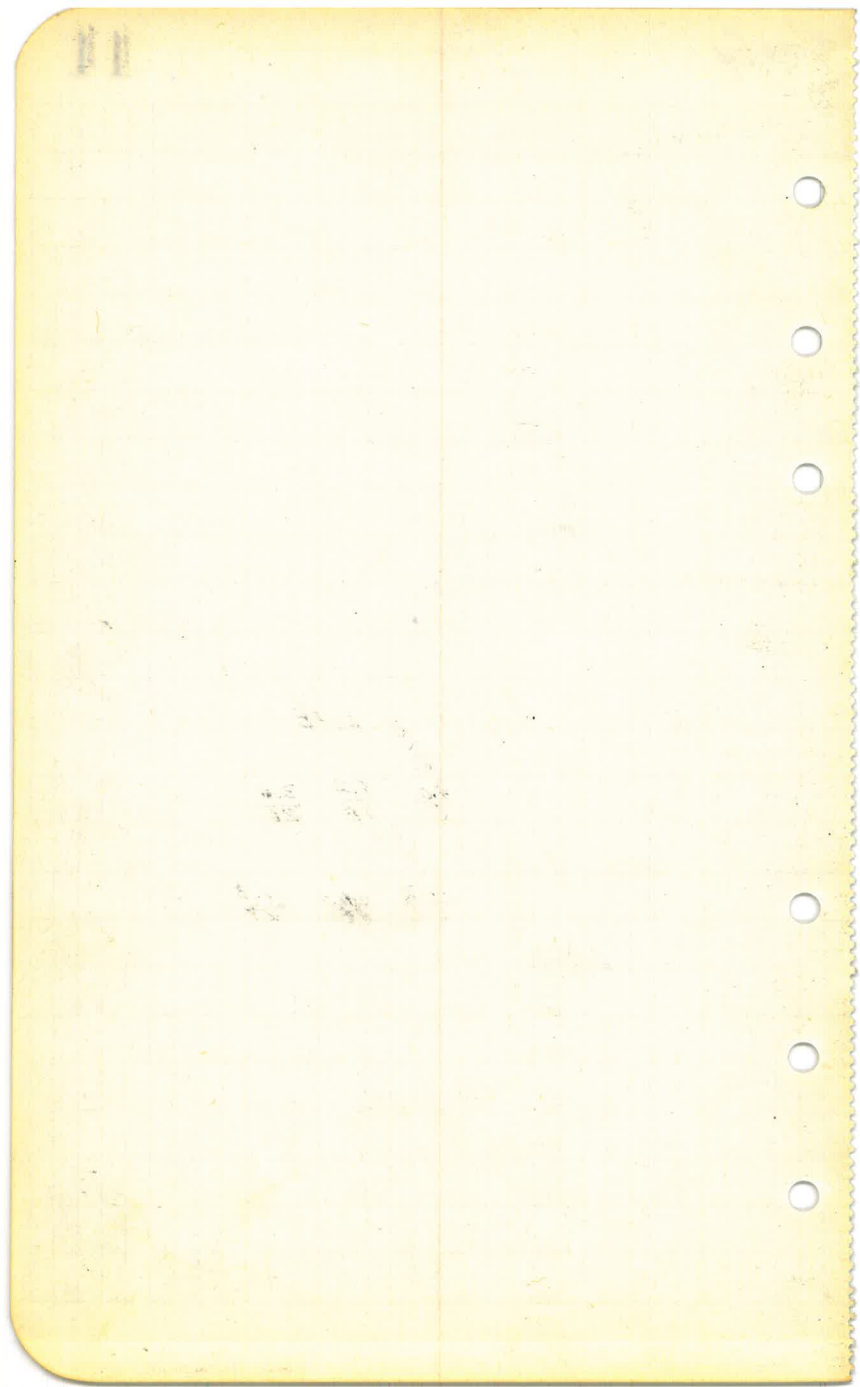
12.50 639.97

6.54 646.51

9/29/54

11

659.88 Left
 $\frac{10}{0}$ $\frac{6.2}{15}$ $\frac{3.6}{26}$
652.68
 $\frac{11.2}{0}$ $\frac{14.5}{18}$ $\frac{11.3}{27}$



51

100	100	100
200	200	200
300	300	300
400	400	400
500	500	500
600	600	600
700	700	700
800	800	800
900	900	900
1000	1000	1000
1100	1100	1100
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1400	1400	1400
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1600	1600	1600
1700	1700	1700
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4200	4200	4200
4300	4300	4300
4400	4400	4400
4500	4500	4500
4600	4600	4600
4700	4700	4700
4800	4800	4800
4900	4900	4900
5000	5000	5000

	646.51		
12+50		11.2	635.31
12+75		11.4	635.11
12+92		12.2	634.31
13+00		9.6	636.91
13+09		10.9	635.61
13+15		8.2	638.31
13+25		6.0	640.51
13+50		3.1	643.41
13+78		2.1	644.41
14+00		3.6	642.91
P.I.			
14+14.69		4.19	642.32
	0.92	643.24	
14+32		3.0	640.24
14+50		9.5	633.74
14+51		12.0	631.24
14+54		9.9	633.34
14+60		9.2	634.04
14+68		12.6	630.62
14+72		12.5	630.72
14+78		7.2	636.04

9/28/54

12

Left

635.31

$$\frac{11.2}{0} \quad \frac{11.8}{7} \quad \frac{8.4}{25} \quad \frac{10.6}{36}$$

635.11

$$\frac{11.4}{0} \quad \frac{13.4}{10} \quad \frac{12.6}{11} \quad \frac{13.1}{17} \quad \frac{15.2}{50}$$

636.91

$$\frac{9.6}{0} \quad \frac{11.9}{20} \quad \frac{14.8}{28}$$

640.61

$$\frac{6.0}{0} \quad \frac{8.8}{18} \quad \frac{10.0}{27}$$

643.41

$$\frac{3.1}{0} \quad \frac{7.4}{25}$$

13+50

642.91

$$\frac{3.6}{0} \quad \frac{5.6}{14} \quad \frac{11.3}{28}$$

[Faint, illegible handwriting on a yellowed, lined page with punch holes.]

181

1420.81

143.34

0.81 143.34

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

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13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

13.03 132.40

		643.24		
P.I.				
14+22.50			0.87	642.37
	13.03	655.40		
			0.10	655.30
	12.85	668.15		
15+50			11.3	656.85
			1.09	667.06
P.I.	13.16	680.22		
15+95.09			9.49	670.73
16+00			7.8	672.42
16+05			6.7	679.52
16+25			3.9	676.32
P.O.T.				
16+46.23			2.43	677.79
	6.12	683.91		
16+50			6.0	677.91
16+75			7.0	676.91
17+00			5.9	678.61
17+50			4.2	679.71
P.I.				
17+76.90			3.38	680.53
	4.15	684.68		
17+76.90			4.2	680.48
17+97			3.1	681.58

9-29-54

left

$$\begin{array}{r} 677.91 \\ 40 \\ 0 \end{array} \quad \begin{array}{r} 7.9 \\ 9 \end{array} \quad \begin{array}{r} 11.7 \\ 19 \end{array} \quad \begin{array}{r} 14.5 \\ 27 \end{array}$$

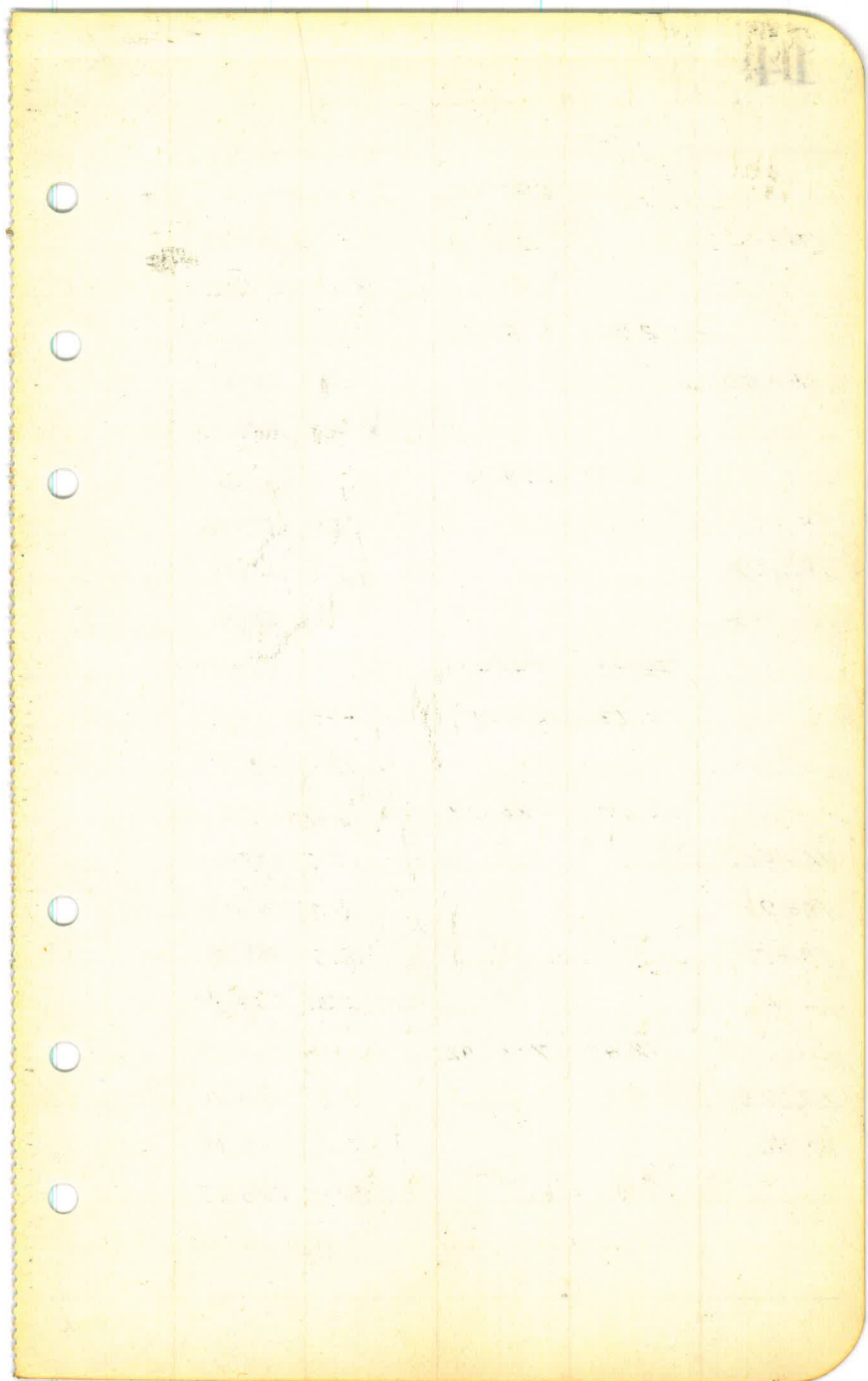
$$\begin{array}{r} 678.61 \\ 53 \\ 0 \end{array} \quad \begin{array}{r} 8.6 \\ 10 \end{array} \quad \begin{array}{r} 11.7 \\ 14 \end{array} \quad \begin{array}{r} 14.5 \\ 21 \end{array} \quad \begin{array}{r} 16.8 \\ 31 \end{array}$$

$$\begin{array}{r} 679.71 \\ 92 \\ 0 \end{array} \quad \begin{array}{r} 6.1 \\ 5 \end{array} \quad \begin{array}{r} 8.4 \\ 14 \end{array} \quad \begin{array}{r} 13.6 \\ 26 \end{array}$$

$$\begin{array}{r} 680.48 \\ 12 \\ 0 \end{array} \quad \begin{array}{r} 6.6 \\ 7 \end{array} \quad \begin{array}{r} 9.5 \\ 15 \end{array} \quad \begin{array}{r} 13.2 \\ 22 \end{array} \quad \begin{array}{r} 15.5 \\ 29 \end{array}$$

split angle

1. 11. 11. 11. 11. 11.
 2. 11. 11. 11. 11. 11.
 3. 11. 11. 11. 11. 11.
 4. 11. 11. 11. 11. 11.
 5. 11. 11. 11. 11. 11.



14

	684.68		
18+00		3.3	681.38
		8.43	676.25
	2.36	678.61	
18+50		11.0	667.61
		12.45	656.16
	3.80	669.96	
18+61		10.5	659.46
18+71		5.2	664.76
18+82		0.2	669.76
	12.13	681.90	0.19
	12.13	681.90	0.77
		0.77	681.13
	12.60	693.73	
18+90		12.6	681.13
18+97		9.7	684.03
19+00		8.9	684.83
		0.23	693.50
	12.42	705.92	
19+25		11.3	694.62
19+50		2.1	703.82
		0.75	705.17

x

9-29-54

Left

split sample

681.38				
3.3	5.3	7.5	16.2	
0	4	8	26	

667.61			
11.0	15.0	17.4	20.4
0	13	20	29

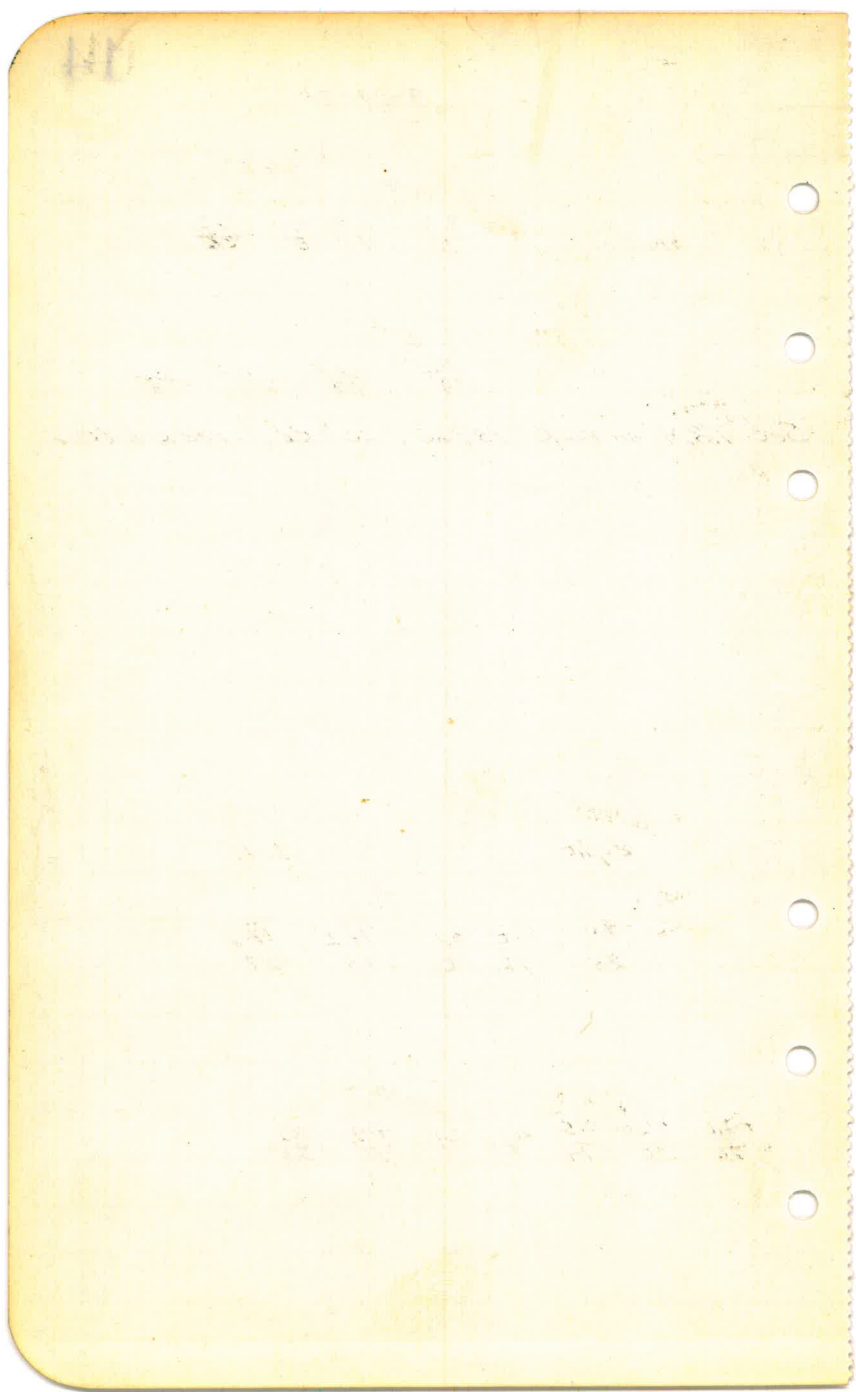
Set T.B.M. on rock 18+60, 20' Rb. creek bottom

Right

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684.83				
4.0	6.8	8.9	14.2	17.6
25	72	0	75	28

703.82				
+4.1	+2.0	0.5	2.1	2.1
26	20	19	9	0
			4.9	7.2
			15	25



Year	Month	Day	Time	Location	Notes
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1901	Jan	3	10:00
1901	Jan	4	10:00
1901	Jan	5	10:00
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1901	Jan	19	10:00
1901	Jan	20	10:00
1901	Jan	21	10:00
1901	Jan	22	10:00
1901	Jan	23	10:00
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1901	Jan	25	10:00
1901	Jan	26	10:00
1901	Jan	27	10:00
1901	Jan	28	10:00
1901	Jan	29	10:00
1901	Jan	30	10:00
1901	Jan	31	10:00

continue profiles

9-30-54

				705.17
	12.94	718.11		
19+60			9.2	708.91
19+73			4.2	713.91
19+83			0.1	718.01
			0.10	718.01
	12.16	730.17		
20+00			6.4	723.77
20+11			2.5	727.67
			0.25	729.92
	12+28	742.20		
20+50			3.7	738.50
20+60			0.3	741.90
			0.06	742.14
	12.13	754.27		
20+67.78			10.5	743.77
20+84			7.0	747.27
21+00			3.0	751.27
21+19			0.2	754.07
			0.57	753.70
	5.71	759.41		

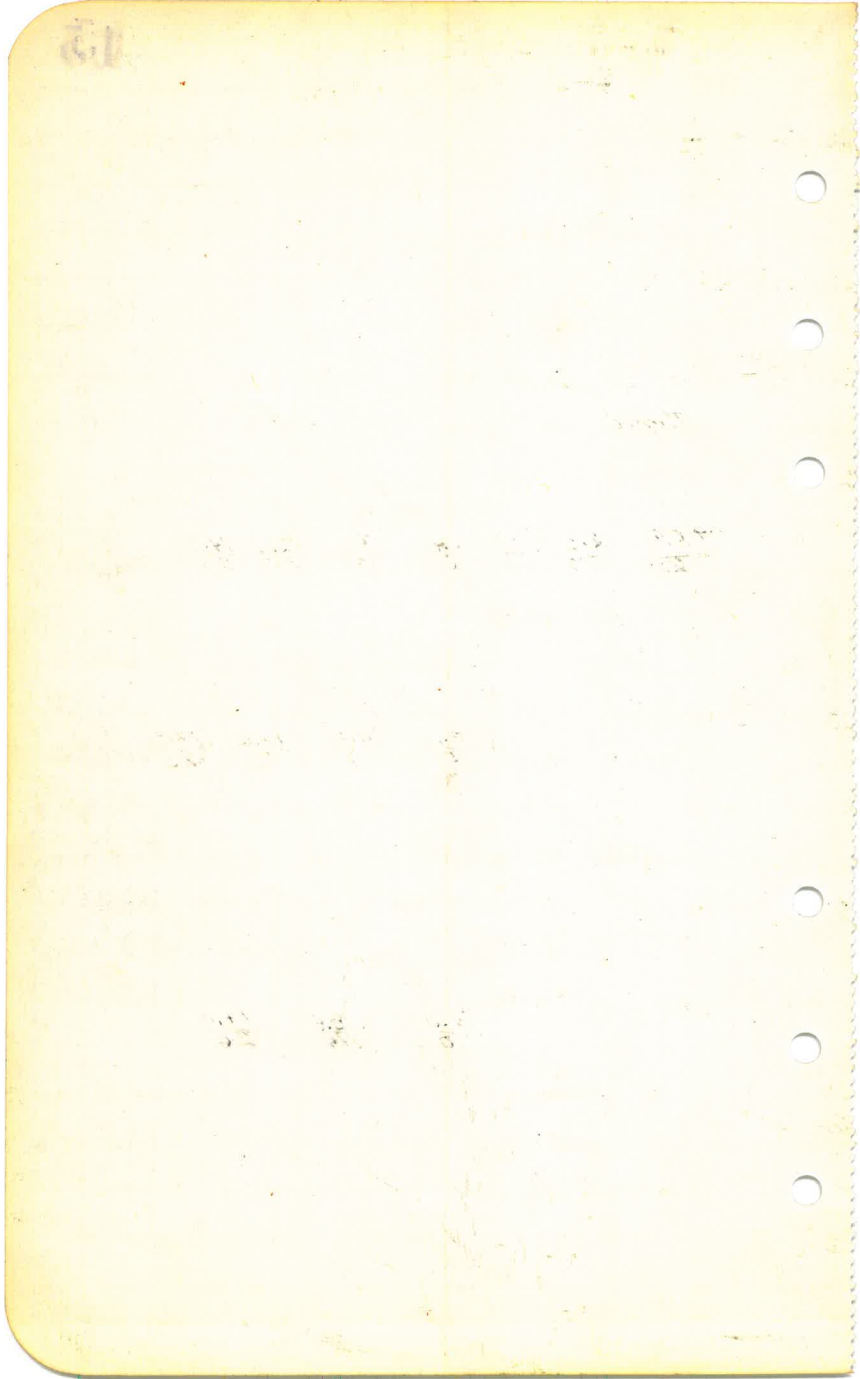
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Left

$$\begin{array}{ccccccc}
 & & & & 123.77 & & \\
 + 0.4 & 2.0 & 3.7 & 4.4 & 10.0 & 12.9 & 14.9 \\
 \hline
 25 & 77 & 7 & 0 & 13 & 20 & 25
 \end{array}$$

$$\begin{array}{cccc}
 & & & 138.50 \\
 3.7 & 8.0 & 10.4 & 12.8 \\
 \hline
 0 & 11 & 77 & 26
 \end{array}$$

$$\begin{array}{ccc}
 & & 1161.21 \\
 3.0 & 8.8 & 14.0 \\
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 0 & 14 & 26
 \end{array}$$



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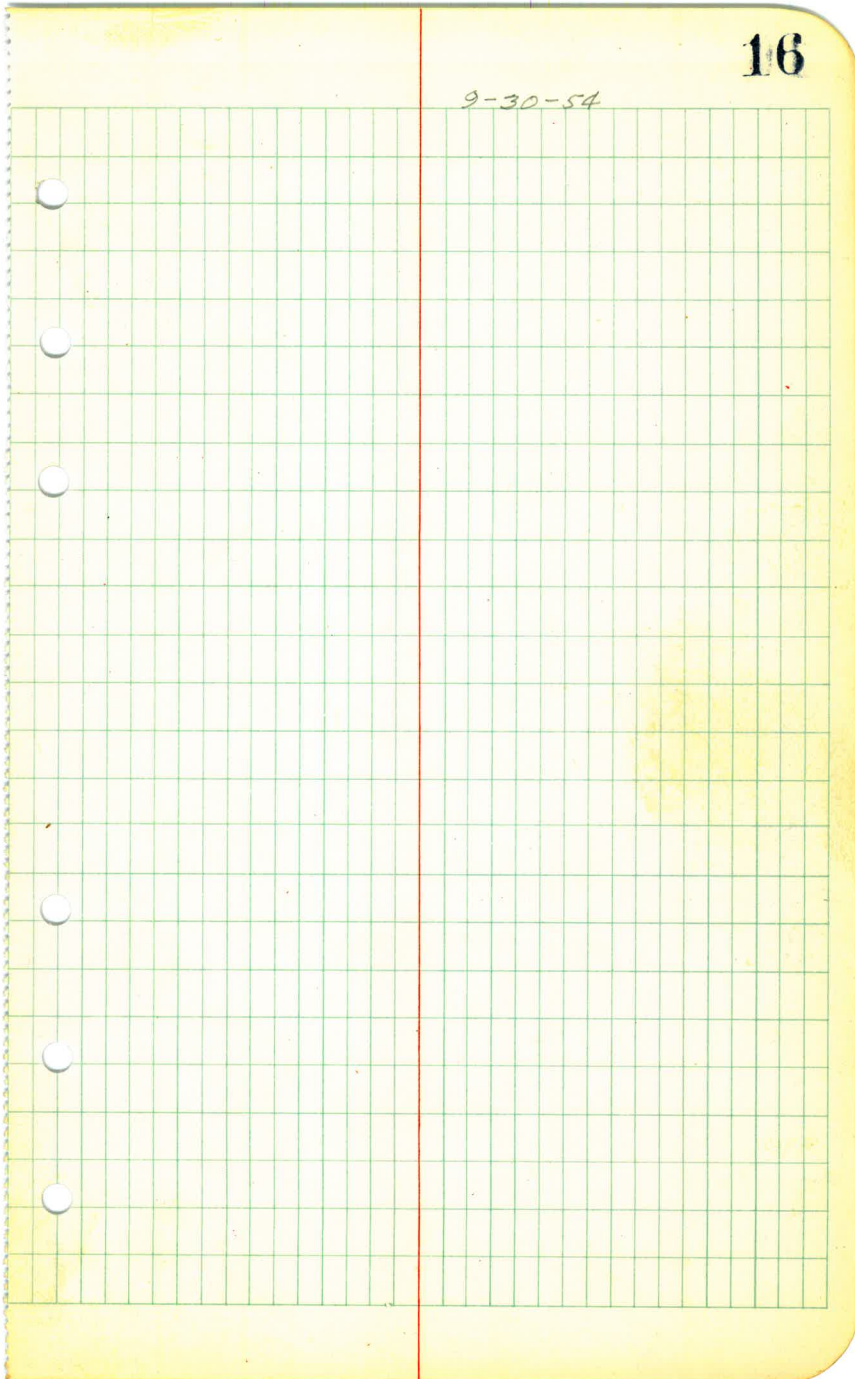
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		759.41		
P.I.				
21+43.56			2.45	756.96
21+50			2.0	757.41
21+81			2.7	756.71
22+00			7.2	752.21
22+13			12.0	747.41
			12.53	746.88
	0.77	747.65		
22+36			8.0	739.65
	0.54		12.78	734.87
	0.54	735.41		
22+50			1.2	734.21
22+60			5.5	729.91
22+70			9.0	726.41
			12.61	722.80
	0.16	722.96		
23+00			11.4	711.56
			12.70	710.26
	0.09	710.35		
23+11			3.0	707.35
23+25			11.3	699.05
			11.20	699.15

9-30-54



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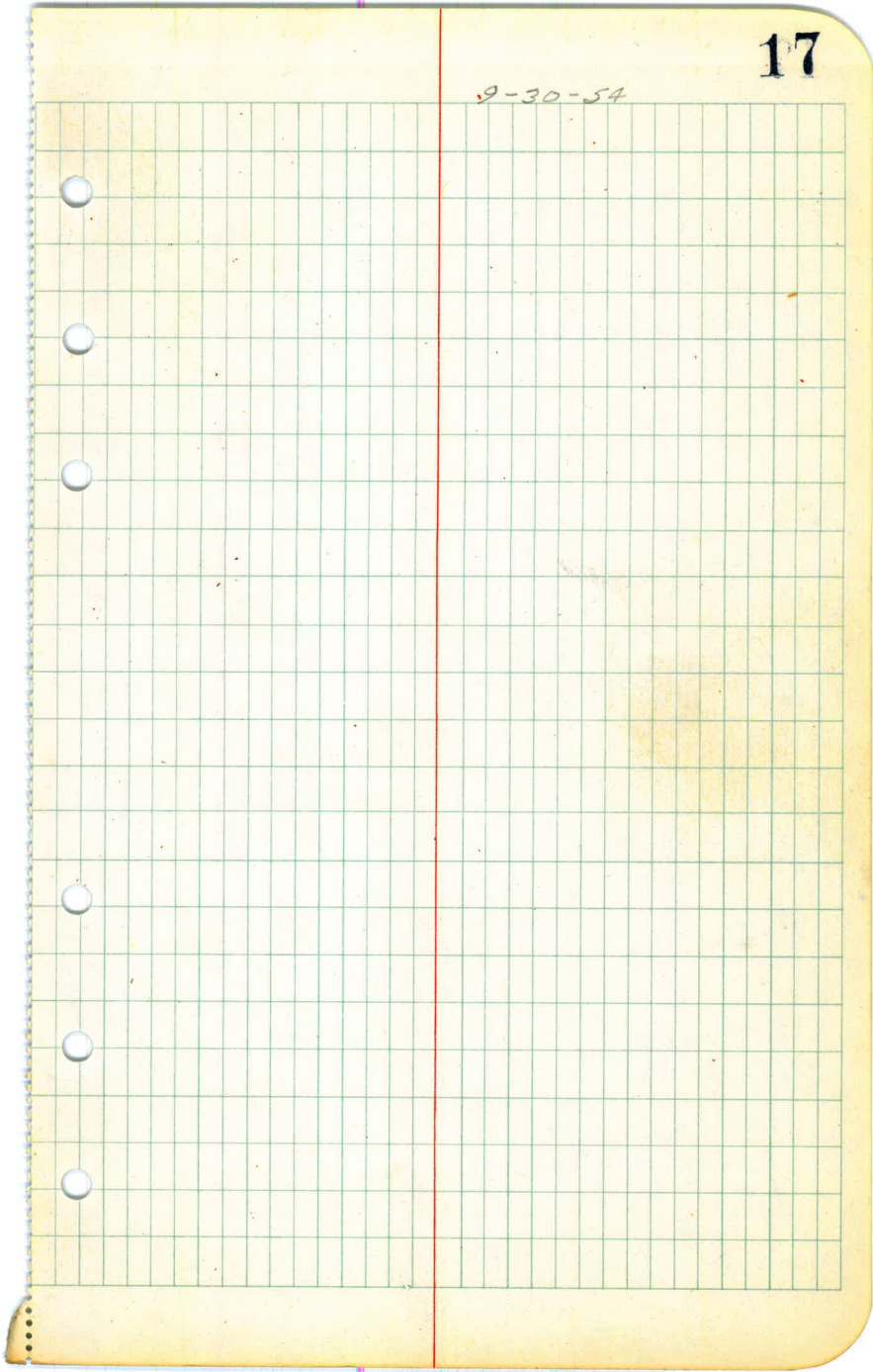


DATE	DESCRIPTION	AMOUNT
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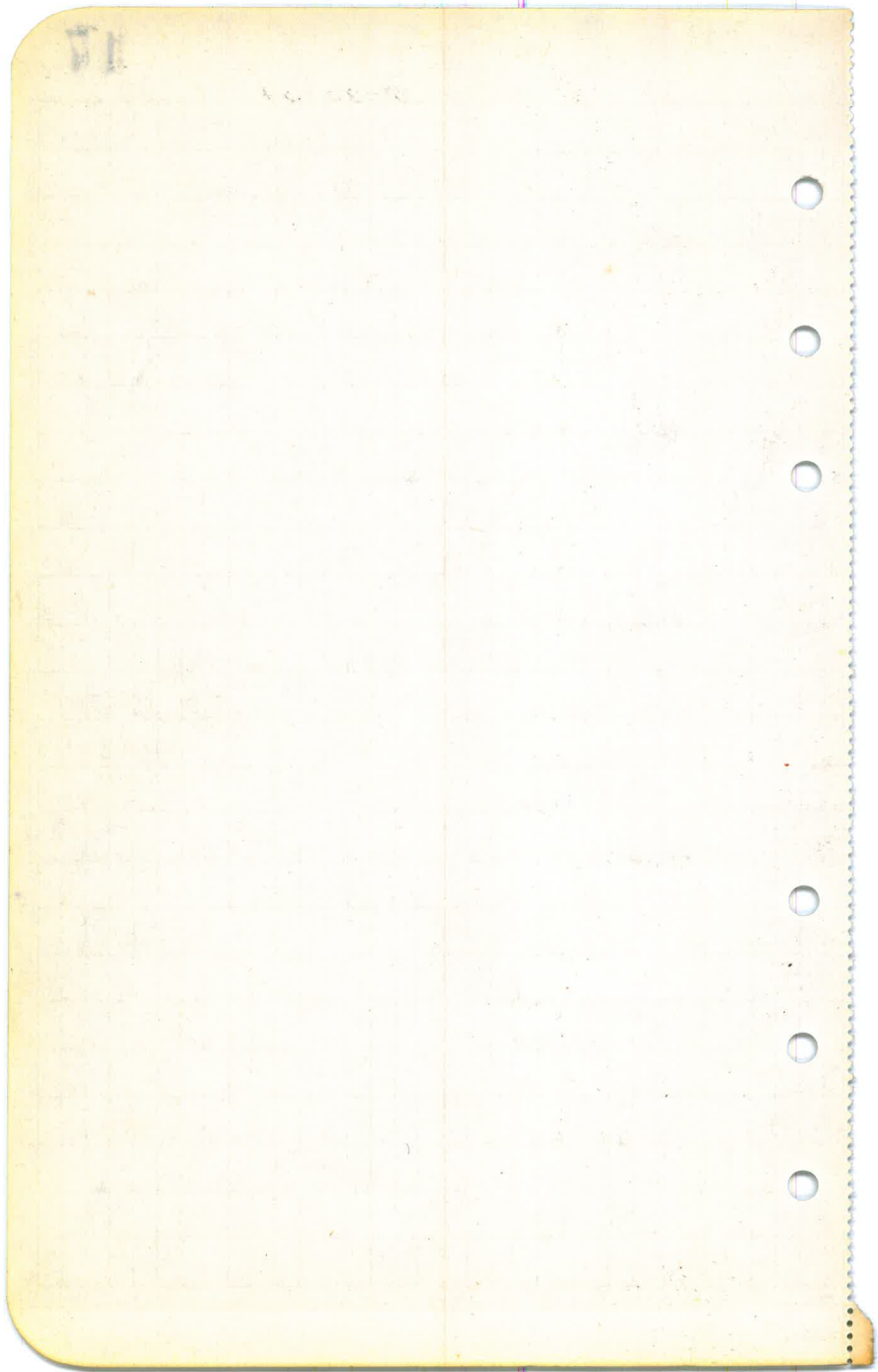
			699.15
	0.30	699.45	
23+43			5.5 693.95
23+50			7.8 691.65
23+54			11.7 687.75
			12.68 686.77
	6.42	693.19	
23+62			11.6 681.59
23+71			11.6 681.59
23+80			6.0 687.19
23+91			4.4 688.79
24+00			1.7 691.49
			0.90 692.79
	12.20	704.99	
P.I. 24+14.75			10.75 694.24
24+50			3.0 701.99
			0.51 704.48
	12.42	716.90	
24+76			0.6 716.30
			0.63 716.27
	13.00	729.27	
24+90			5.7 723.57
25+00			1.0 728.27

9-30-54



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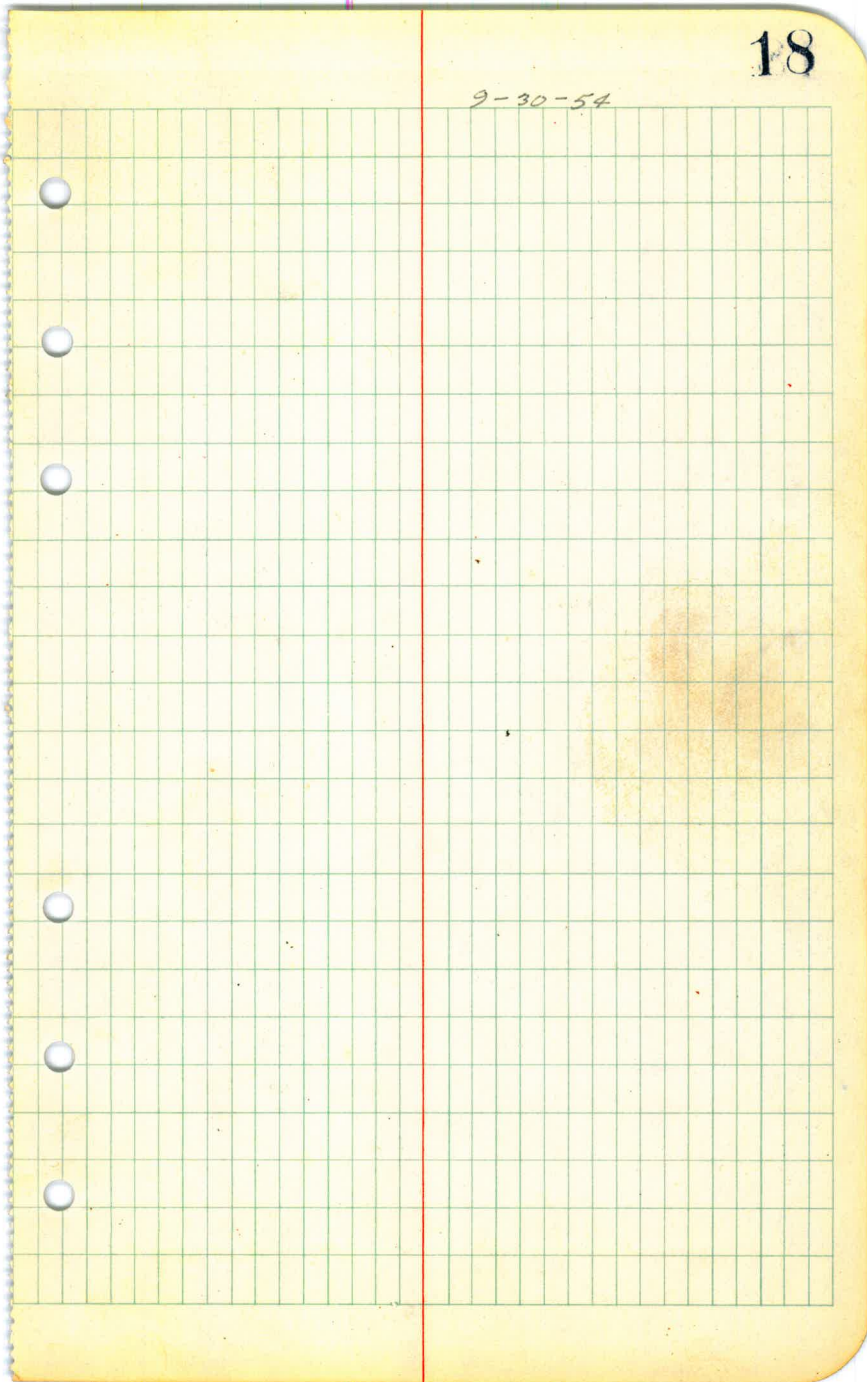
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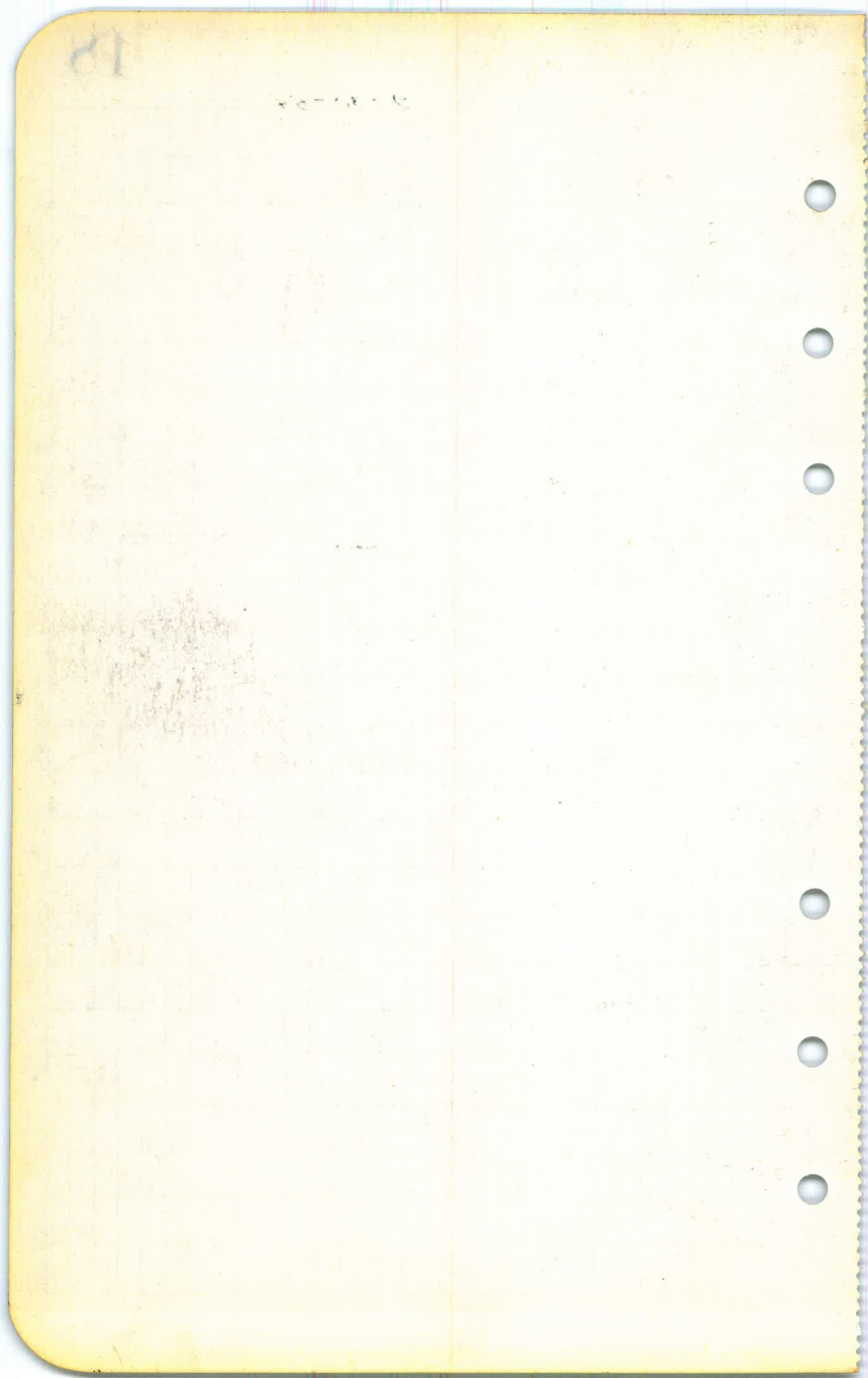
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		729.27		
			0.71	728.56
	12.38	740.94		
25+18			5.4	735.54
25+32			0.0	740.94
			0.03	740.91
	12.11	753.02		
25+50			6.2	746.82
25+60			3.1	749.92
			0.03	752.99
	6.29	759.28		
25+90			4.5	754.78
26+00			3.6	755.68
26+22			4.1	755.18
21. 26+39 ⁴³			5.76	753.52
	1.45	759.97		
26+50			1.2	753.77
26+71			1.6	753.37
27+00			4.8	750.17
27+25			10.0	744.97
			12.69	742.28
	0.04	742.32		
27+50			2.9	739.42

9-30-54

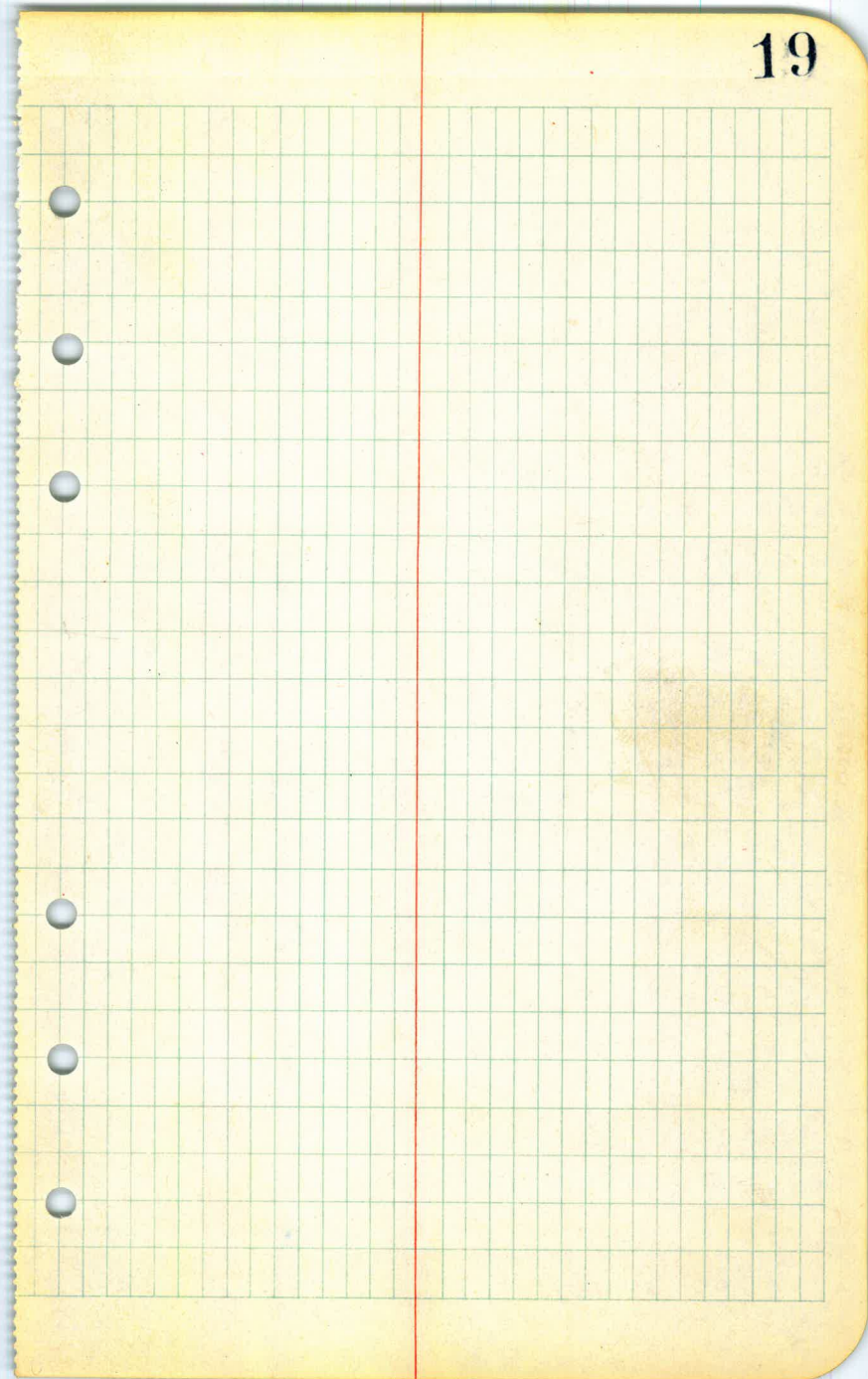


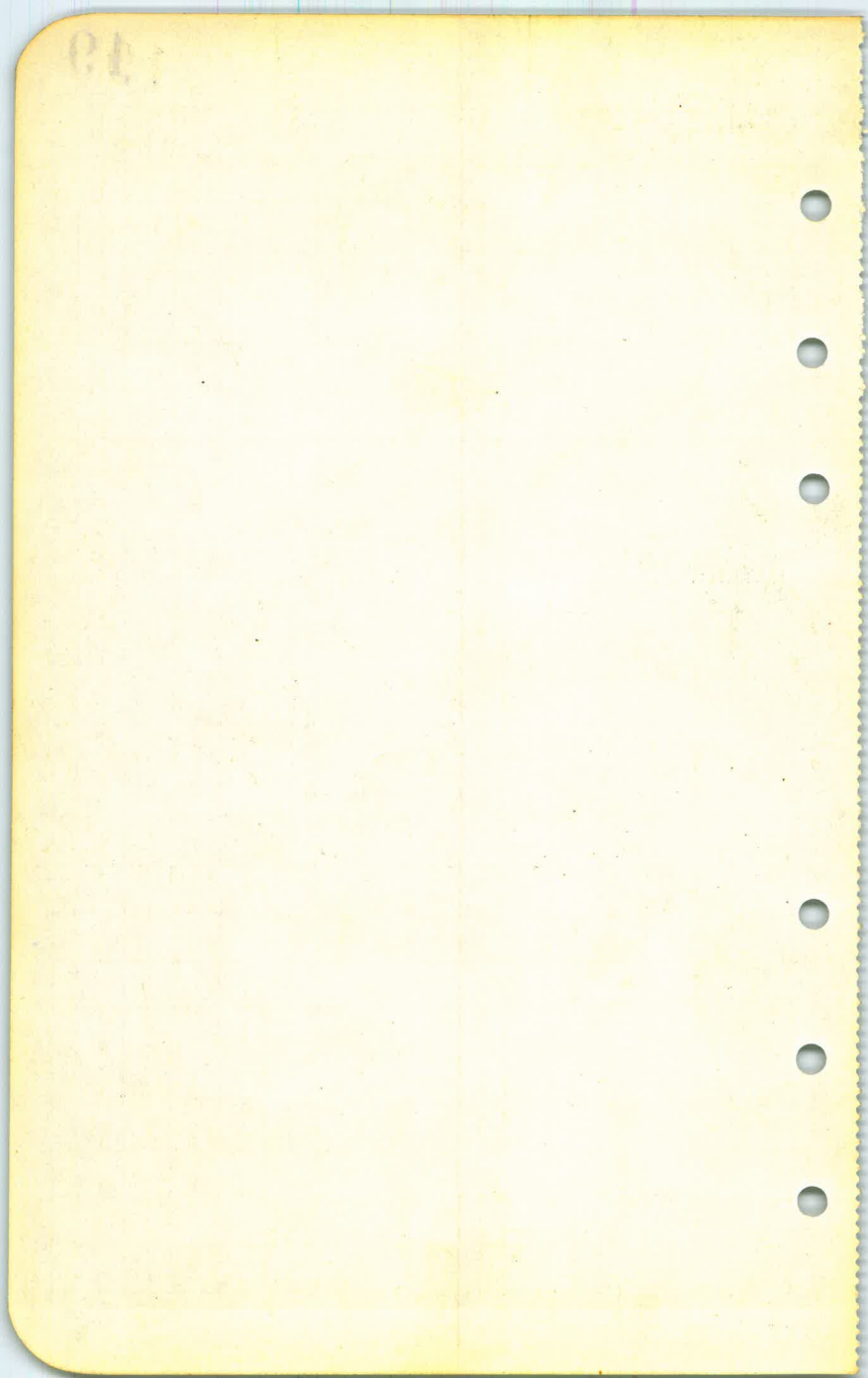


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	742.32		
28+00		13.3	729.02
		13.31	729.01
	3.77	732.78	
28+11		6.4	726.38
28+26		10.6	722.18
28+50		4.7	728.08
28+70		0.5	732.28
		0.19	732.59
	12.55	745.14	
29+00		5.0	740.14
		0.22	744.92
	11.77	756.69	
29+22		10.4	746.29
29+50		6.8	749.89
30+00		2.6	754.09
30+19		2.4	754.29
30+48.30		4.63	752.06
	6.57	758.63	
30+80		4.6	754.03
31+00		4.3	754.33
31+50		4.1	754.53
31+80		5.5	753.13





1995

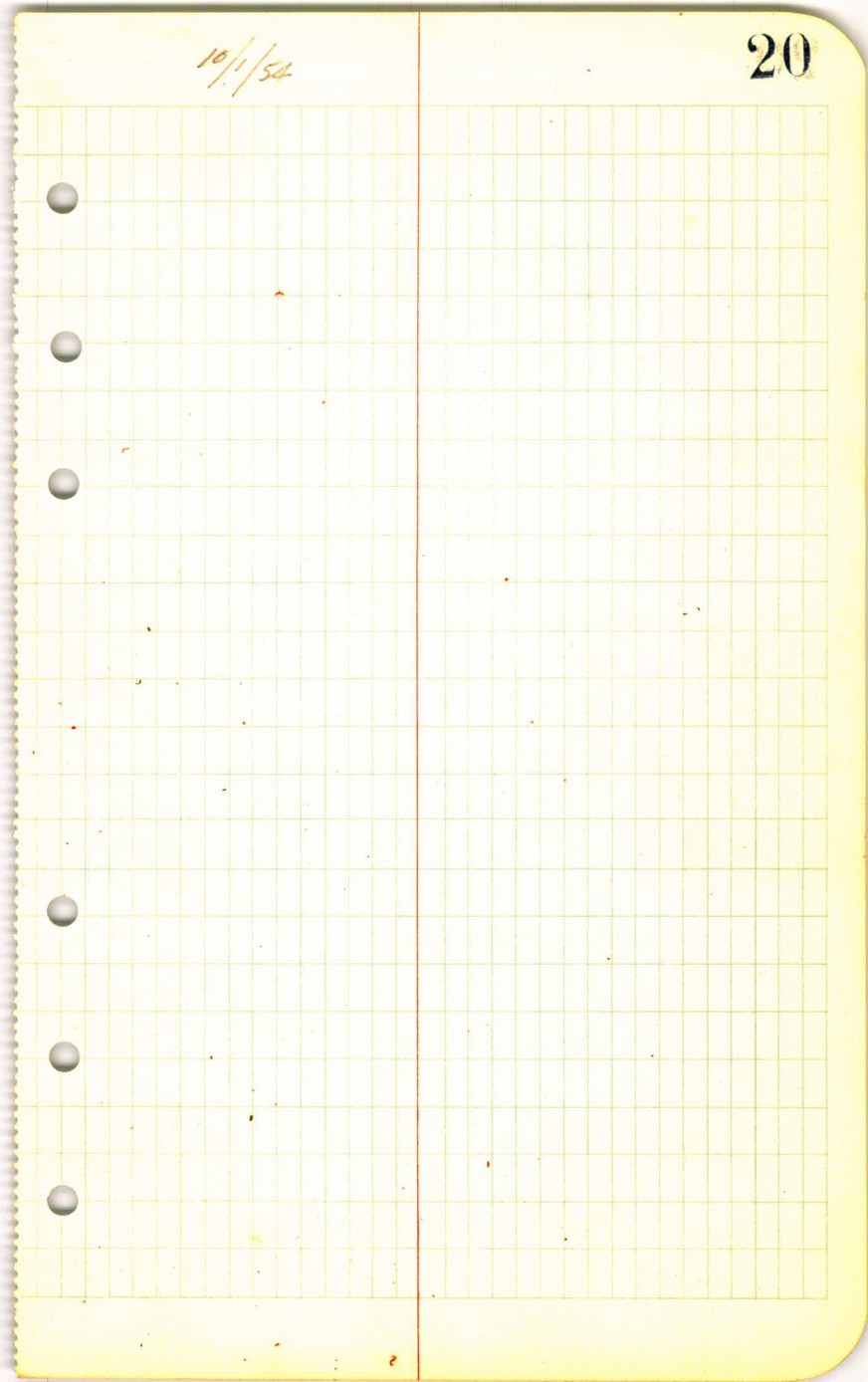
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1/4	1/4	1/4
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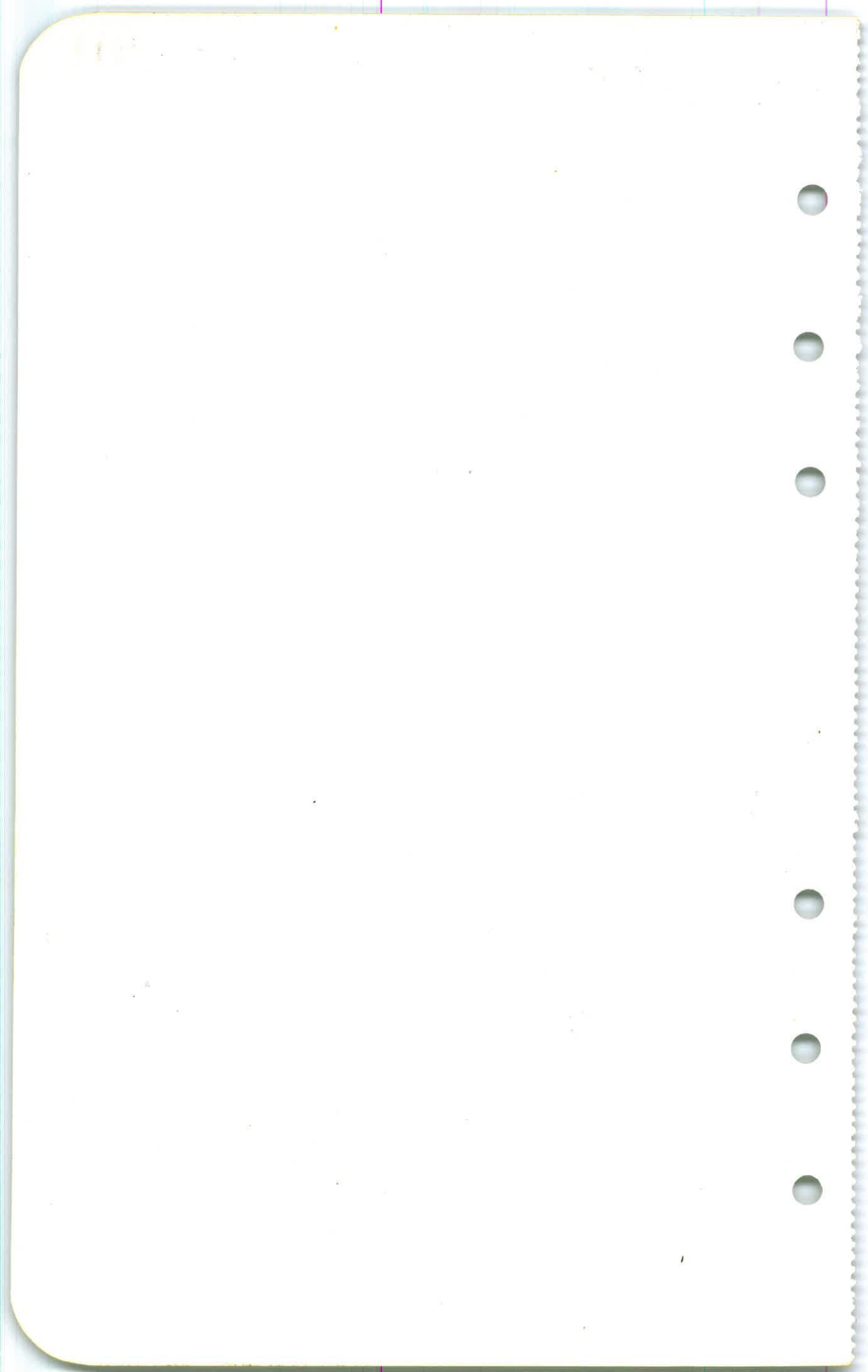
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		758.63		
31+92.93			6.28	752.35
	1.19	753.54		
32+00			1.1	752.44
32+35			4.3	749.24
32+50			8.1	745.44
			12.82	740.72
	0.34	741.06		
32+73			4.2	736.86
33+00			10.7	730.36
			12.75	728.31
	0.38	728.69		
33+36			13.2	715.49
			12.81	715.88
	0.44	716.32		
33+42			2.0	714.32
33+50			6.5	709.82
			12.14	704.18
	0.02	704.20		
33+68			3.1	701.10
33+76			5.3	698.90
			8.89	695.31
	0.13	695.44		

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1. Introduction
The purpose of this study is to investigate the effects of the independent variable on the dependent variable. The study is designed to explore the relationship between the two variables and to determine the extent to which the independent variable influences the dependent variable. The study is conducted in a controlled environment to ensure the validity of the results.

2. Methodology
The study uses a quantitative research design to collect data. The data is collected through a series of experiments and observations. The independent variable is manipulated, and the dependent variable is measured. The data is then analyzed using statistical methods to determine the significance of the results.

3. Results
The results of the study show a significant positive correlation between the independent variable and the dependent variable. The data indicates that as the independent variable increases, the dependent variable also increases. The results are supported by statistical analysis, which shows that the correlation is statistically significant.

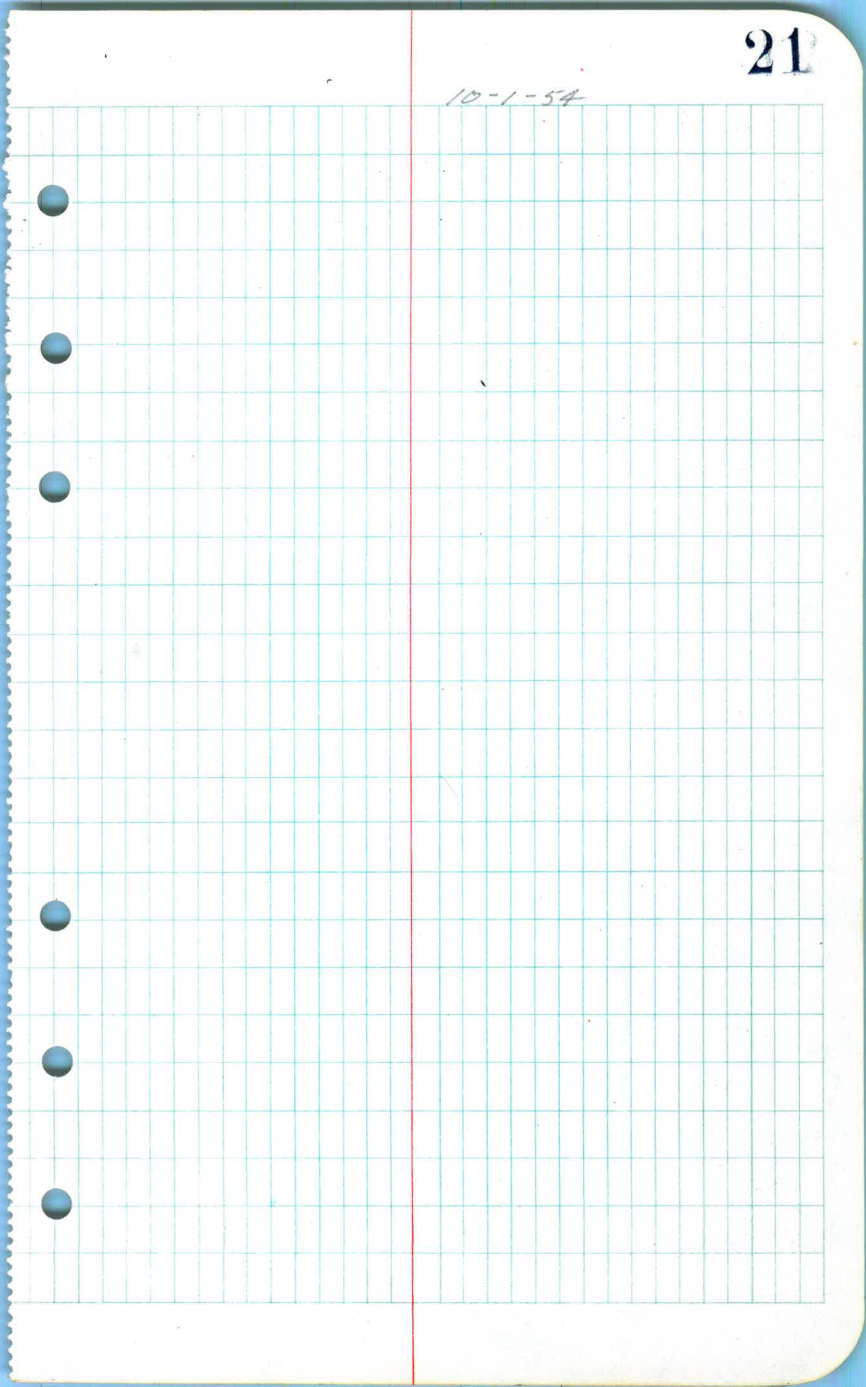
4. Conclusion
The study concludes that there is a significant positive relationship between the independent variable and the dependent variable. The results suggest that the independent variable has a positive influence on the dependent variable. The study provides valuable insights into the relationship between the two variables and has implications for future research.

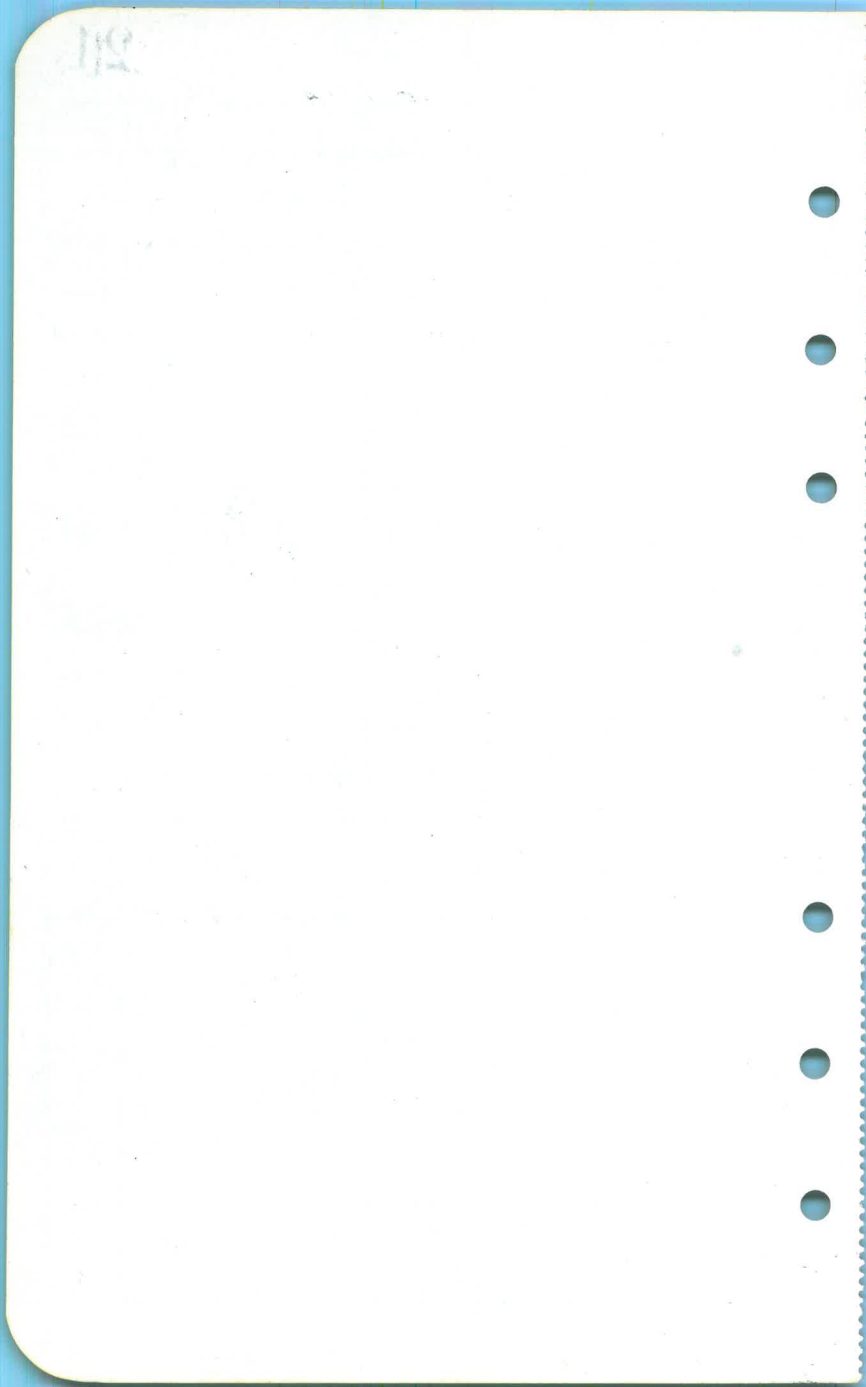
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Continue Profile

	695.44		
33+90		4.8	690.64
34+00		8.1	687.31
		12.89	682.55
	0.42	682.97	
34+28		8.0	674.97
		12.76	670.21
P.I.	0.93	671.14	
34+36.21		2.56	668.58
34+50		9.8	661.34
34+53		11.0	660.14
34+59		11.4	659.74
34+61		10.6	660.54
		0.05	671.09
P.I.	12.37	683.46	
34+85.21		12.15	671.31
35+00		6.5	676.96
		0.02	683.44
	12.48	695.92	
35+25		11.3	684.62
35+33		9.4	686.52
35+50		2.7	693.22
		0.30	695.62
	10.16	705.78	

10-1-54





1940

1. 10/10/40 - 10/11/40 - 10/12/40 - 10/13/40 - 10/14/40 - 10/15/40 - 10/16/40 - 10/17/40 - 10/18/40 - 10/19/40 - 10/20/40 - 10/21/40 - 10/22/40 - 10/23/40 - 10/24/40 - 10/25/40 - 10/26/40 - 10/27/40 - 10/28/40 - 10/29/40 - 10/30/40 - 10/31/40

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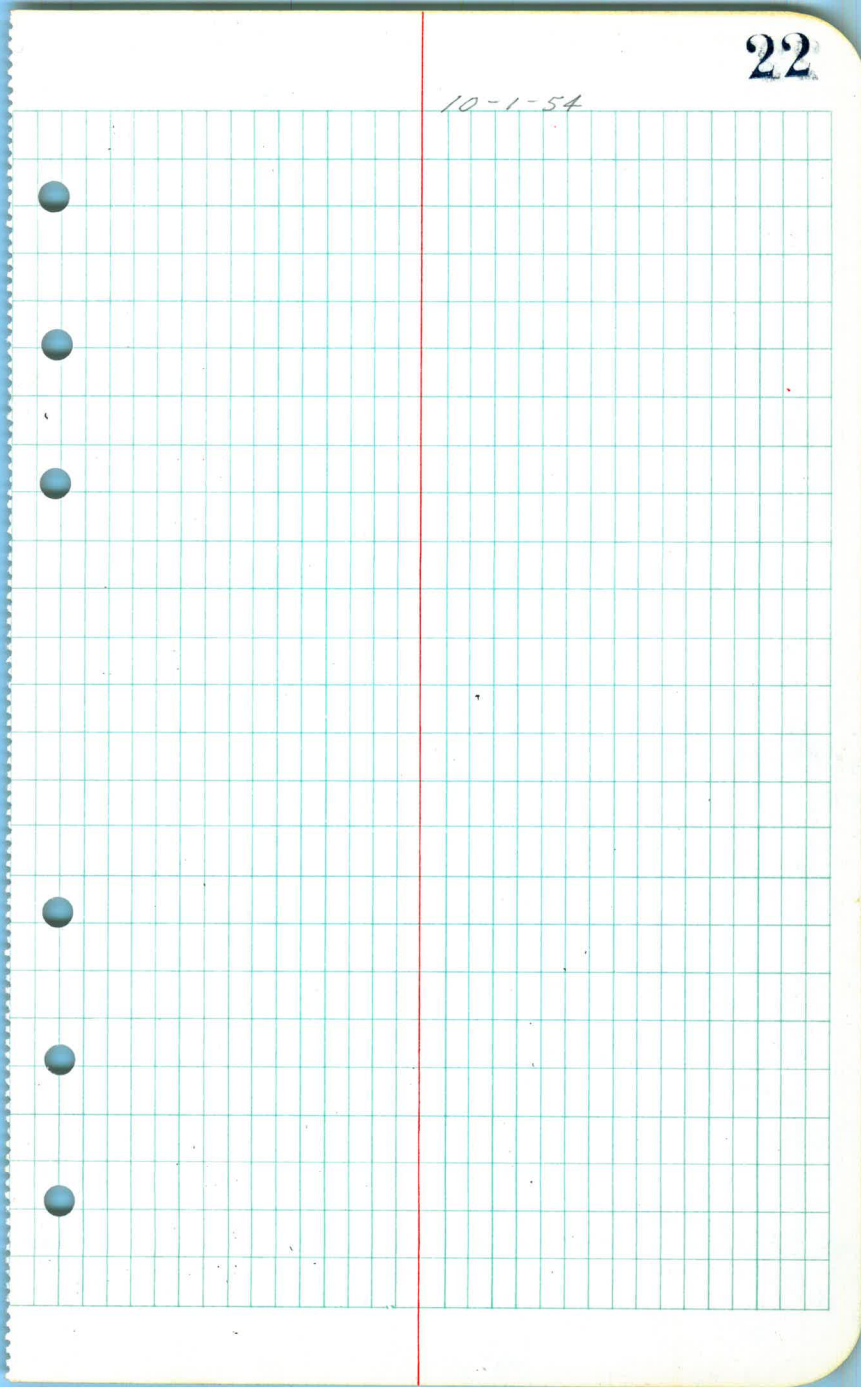
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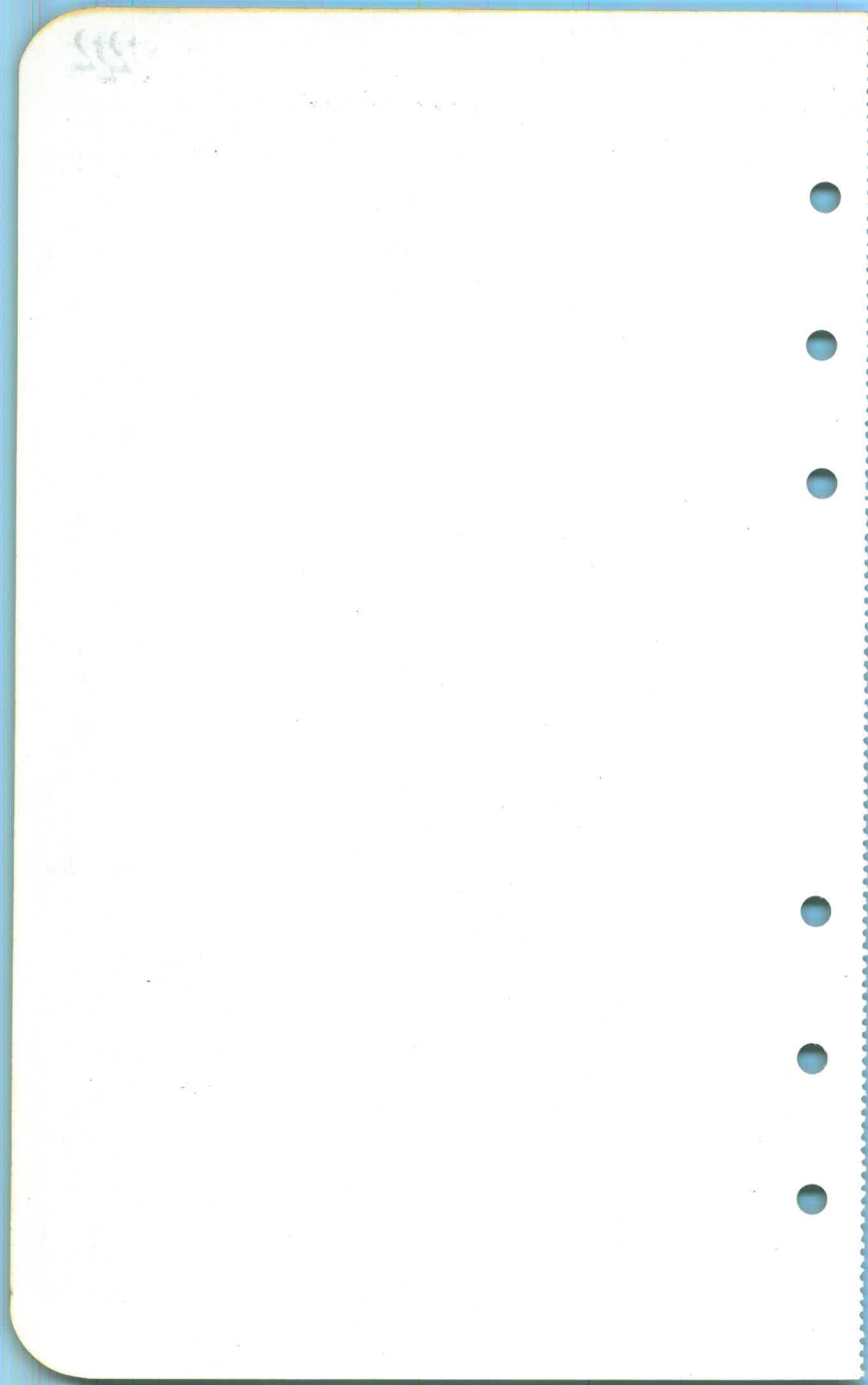
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		705.78		
35+62			9.0	696.78
35+83			3.9	701.88
			0.13	705.65
	10.84	716.49		
36+00			8.1	708.39
36+22			2.1	714.39
			0.31	716.18
	12.58	728.76		
36+39			7.7	721.06
36+50			4.2	724.56
			0.19	728.57
	9.68	738.25		
P.O.T. 37+00			0.95	737.80
	12.53	750.33		
37+20			8.5	741.83
37+50			2.0	748.33
			0.18	750.15
	7.57	757.72		
37+80			6.0	751.72
P.I. 37+96.92			6.07	751.65
38+00			6.6	751.12
38+13			4.6	753.12
38+50			4.2	753.52

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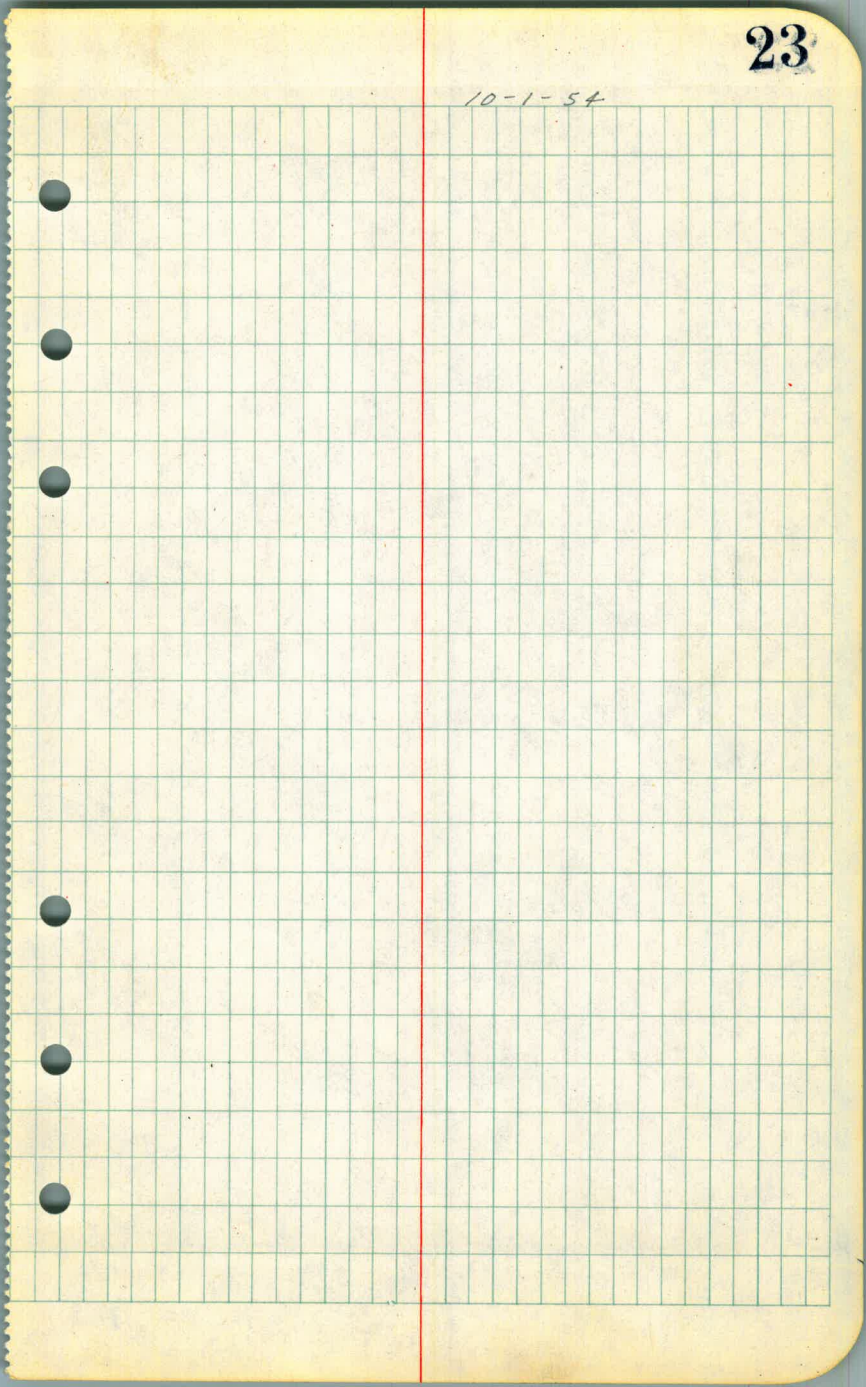


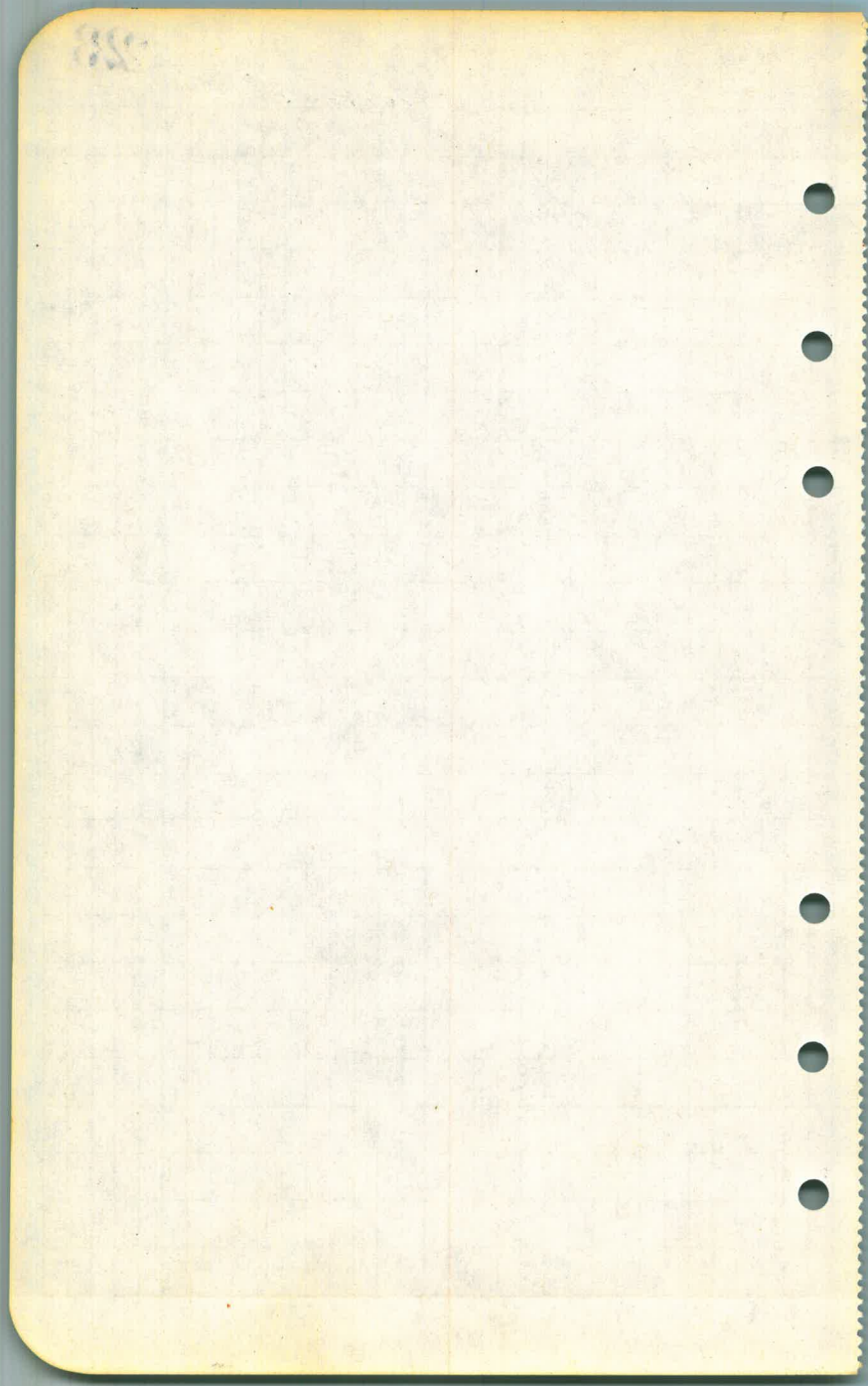
185

Handwritten notes on a lined page, organized into columns. The text is mostly illegible due to fading and bleed-through, but appears to be a list or ledger with several columns of entries.

		757.72		
39+00			7.5	750.22
<i>P.I.</i>				
39+08 ⁷²			8.50	749.22
	0.90	750.12		
39+50			2.7	747.42
39+79			6.0	744.12
40+00			7.3	742.82
40+17			9.0	741.12
40+41			11.7	738.42
			12.70	737.42
	0.45	737.87		
<i>P.O.T.</i>				
40+50			1.2	736.67
41+00			10.5	727.37
			12.59	725.28
	0.14	725.42		
41+30			2.9	722.52
41+50			7.3	718.12
			12.70	712.72
	0.71	713.43		
41+87			5.6	707.83
42+00			7.7	705.73
42+28			13.0	700.43
			12.83	700.60
	0.40	701.00		

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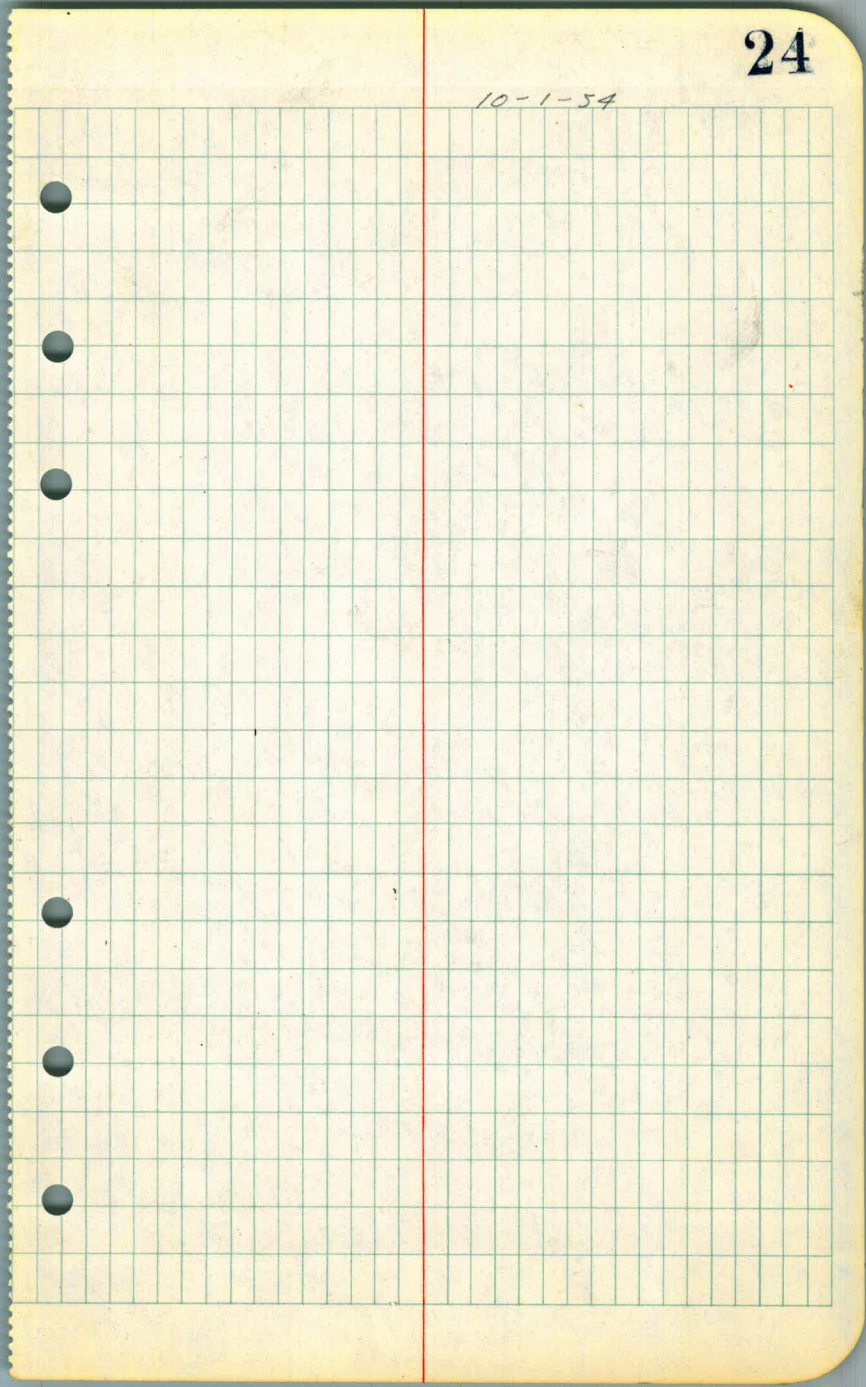


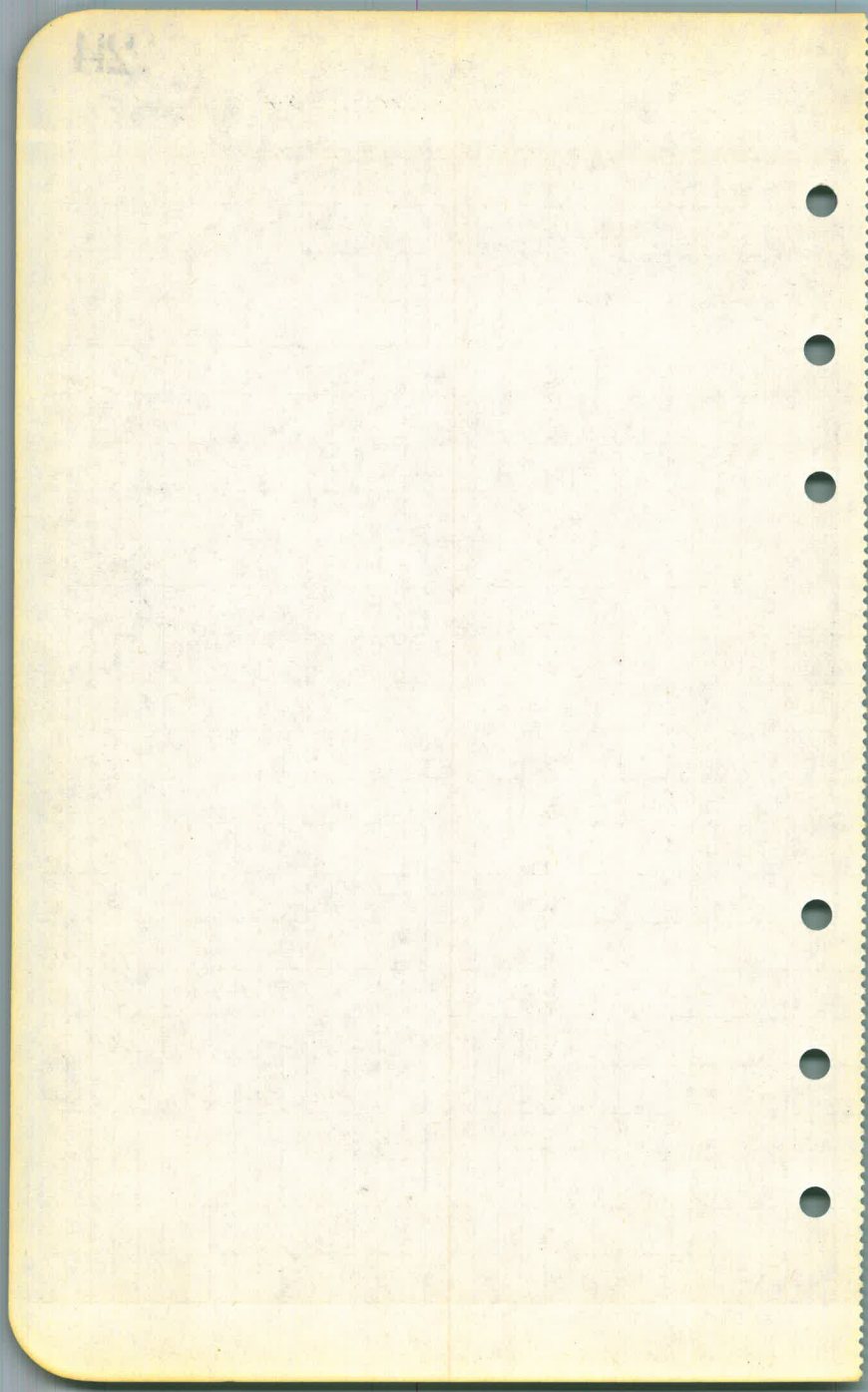
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Year	Month	Day	Time	Location	Remarks
1900	Jan	1	10:00
1900	Jan	2	11:00
1900	Jan	3	12:00
1900	Jan	4	13:00
1900	Jan	5	14:00
1900	Jan	6	15:00
1900	Jan	7	16:00
1900	Jan	8	17:00
1900	Jan	9	18:00
1900	Jan	10	19:00
1900	Jan	11	20:00
1900	Jan	12	21:00
1900	Jan	13	22:00
1900	Jan	14	23:00
1900	Jan	15	24:00
1900	Jan	16	25:00
1900	Jan	17	26:00
1900	Jan	18	27:00
1900	Jan	19	28:00
1900	Jan	20	29:00
1900	Jan	21	30:00
1900	Jan	22	31:00

	701.00		
42+39		2.9	698.10
42+50		7.3	693.70
		11.89	689.11
	0.21		689.32
43+00		7.6	681.72
		12.94	676.38
	0.62		677.00
43+30		4.0	673.00
43+50		9.6	667.40
		12.63	664.37
	0.21		664.58
43+71		2.6	661.98
44+00		9.9	654.68
		12.62	651.96
	0.30		652.26
44+29		4.7	647.56
44+50		0.6	643.66
44+70		12.9	639.36
		12.66	639.60
	0.54		640.14
44+85		5.5	634.64
45+00		10.7	629.44

10-1-54

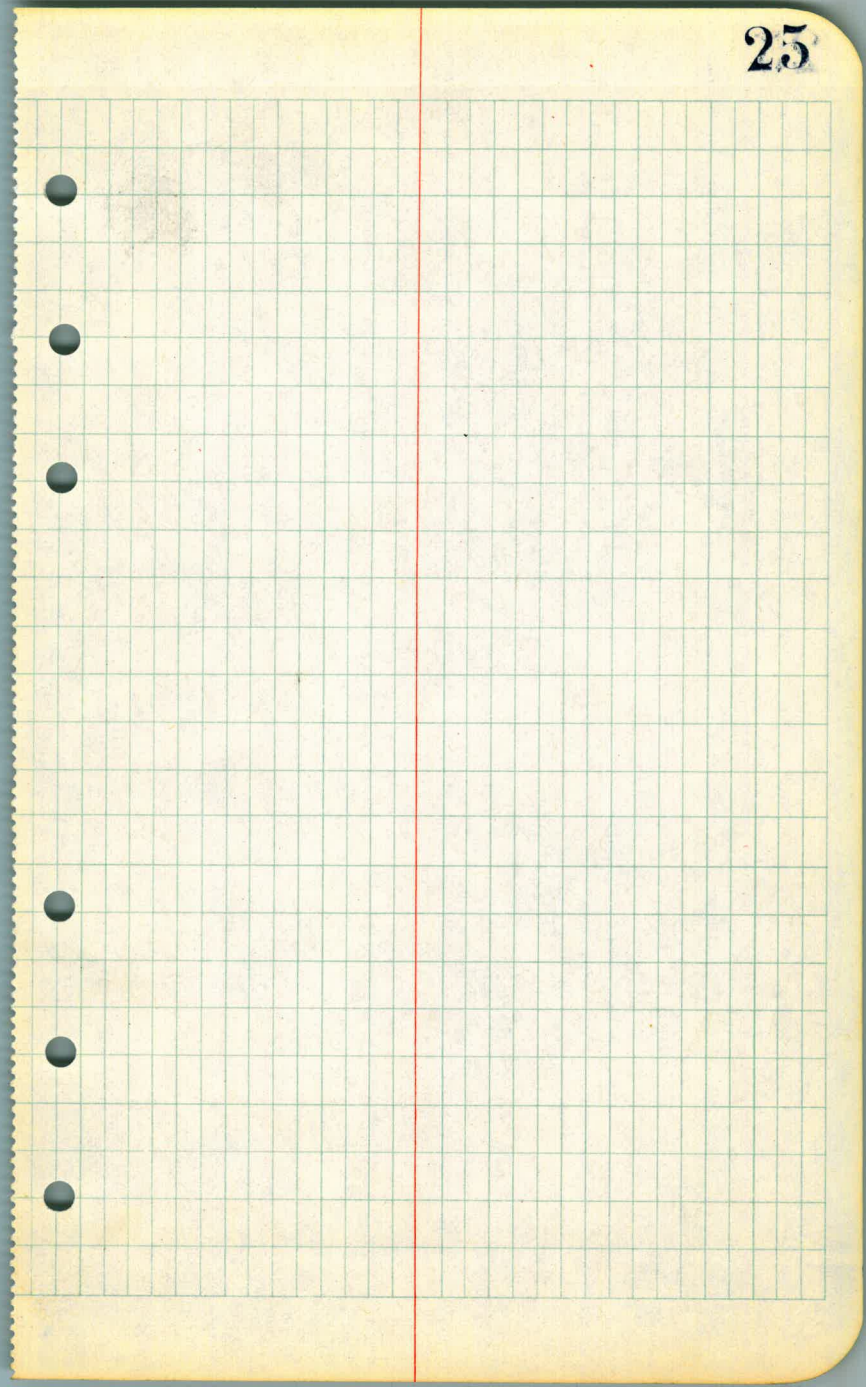


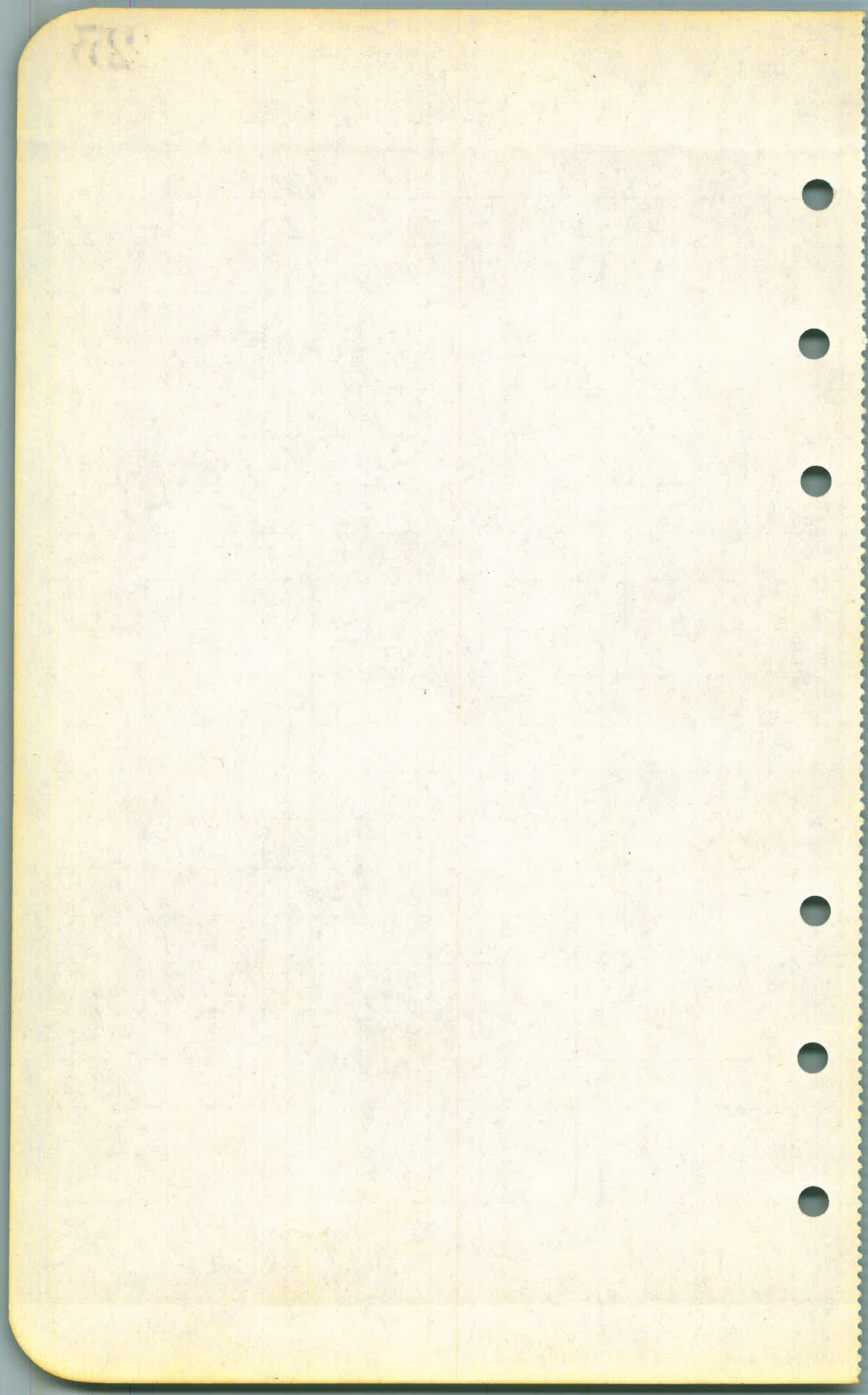


105

Time	Location	Notes
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10:20
10:30
10:40
10:50
11:00
11:10
11:20
11:30
11:40
11:50
12:00
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22:00
22:10
22:20
22:30
22:40
22:50
23:00
23:10
23:20
23:30
23:40
23:50
00:00

	640.14		
		12.89	627.25
	0.58	627.83	
45+15		3.0	624.83
45+50		7.3	620.53
45+59		7.9	619.93
45+65		12.9	614.93
45+76		10.3	617.53
45+84		10.1	617.73
46+00		6.4	621.43
46+07		5.8	622.03
46+10		3.7	624.13
46+26		10.7	617.13
46+44		8.8	619.03
46+50		7.6	620.23
46+55		4.8	623.03
46+65		9.3	618.53
46+78		9.3	618.53
46+93		4.5	623.33
47+00		1.3	626.53
		0.44	627.39
	11.86	639.25	
47+93		3.5	635.75



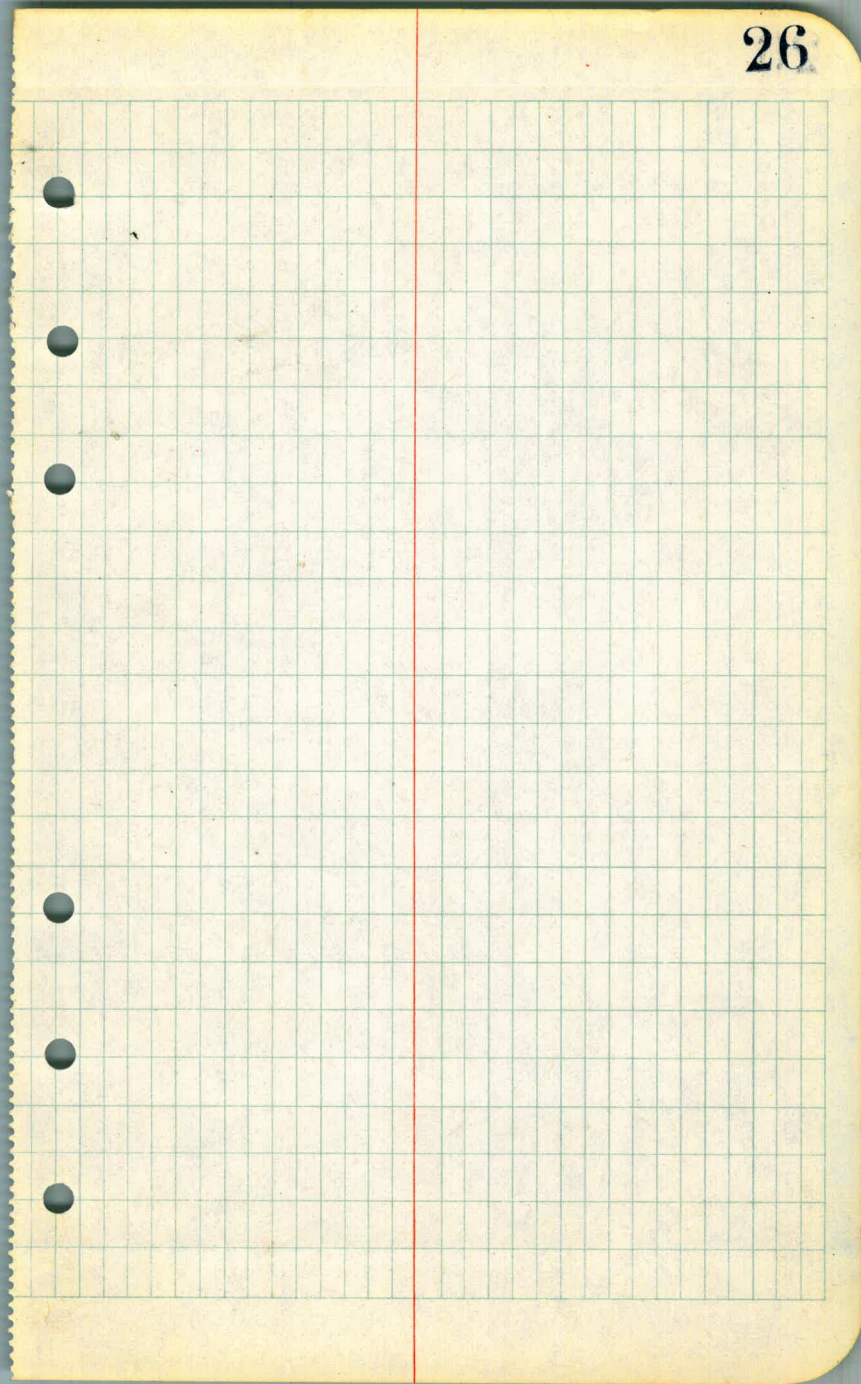


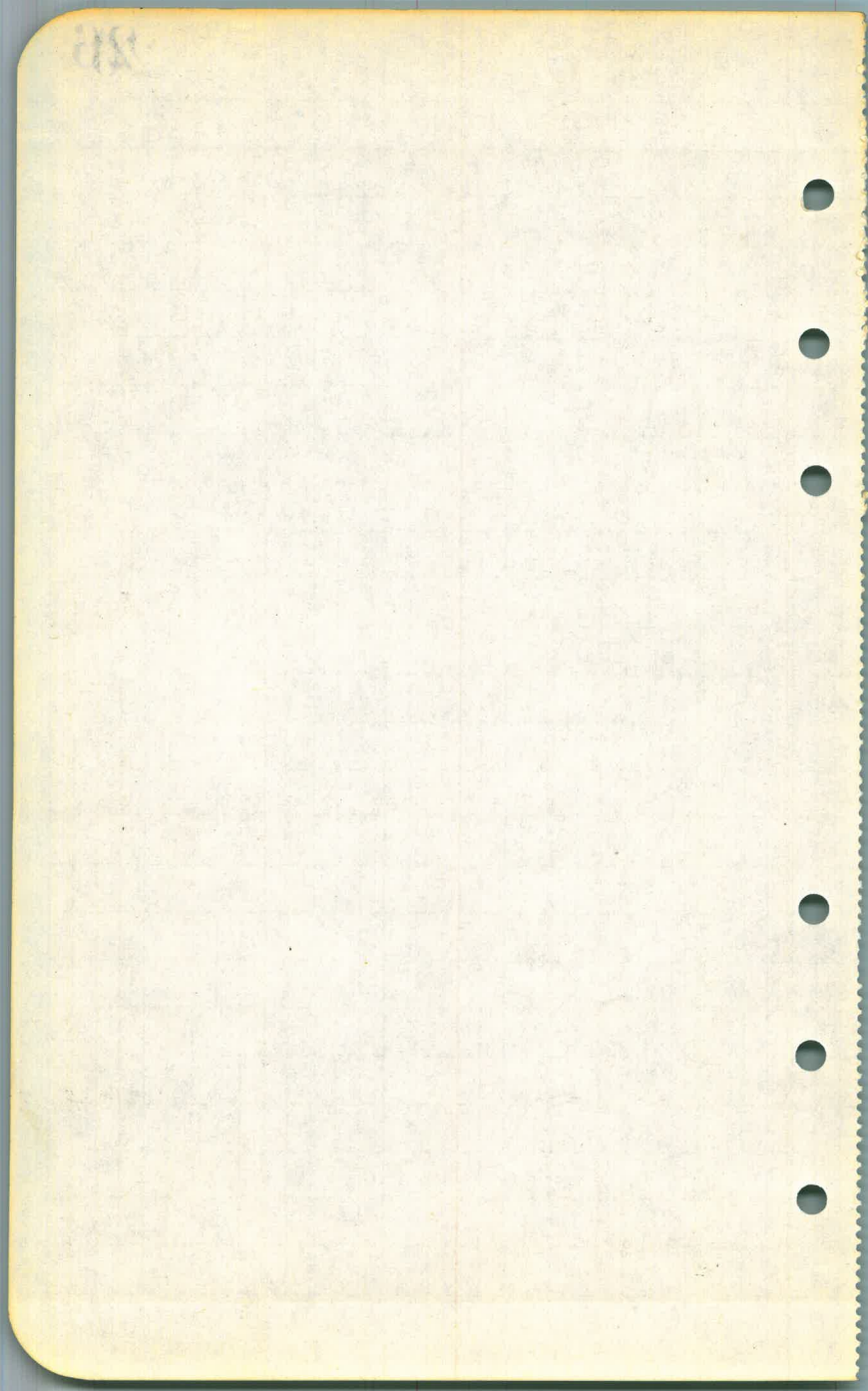
188

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93	93	93	93
94	94	94	94
95	95	95	95
96	96	96	96
97	97	97	97
98	98	98	98
99	99	99	99
100	100	100	100

		639.25		
47+50			0.6	638.7
	17		0.04	639.21 ✓
	12.91	652.12 ✓		
48+00			9.4	642.7
48+18			8.3	643.8
48+50			2.0	650.1
48+70			0.6	651.5
			0.21	651.91 ✓
	12.75	664.66 ✓		
48+82			12.8	651.9
48+98			8.8	655.9
49+00			6.9	657.8
49+05			5.2	659.5
49+15			5.3	659.4
49+40			0.3	664.4
			0.27	664.39 ✓
	13.06	677.45 ✓		
49+50			11.5	666.0
49+78			8.1	669.4
49+88			5.0	672.8
50+00			3.2	674.8
50+29			0.6	676.9

26



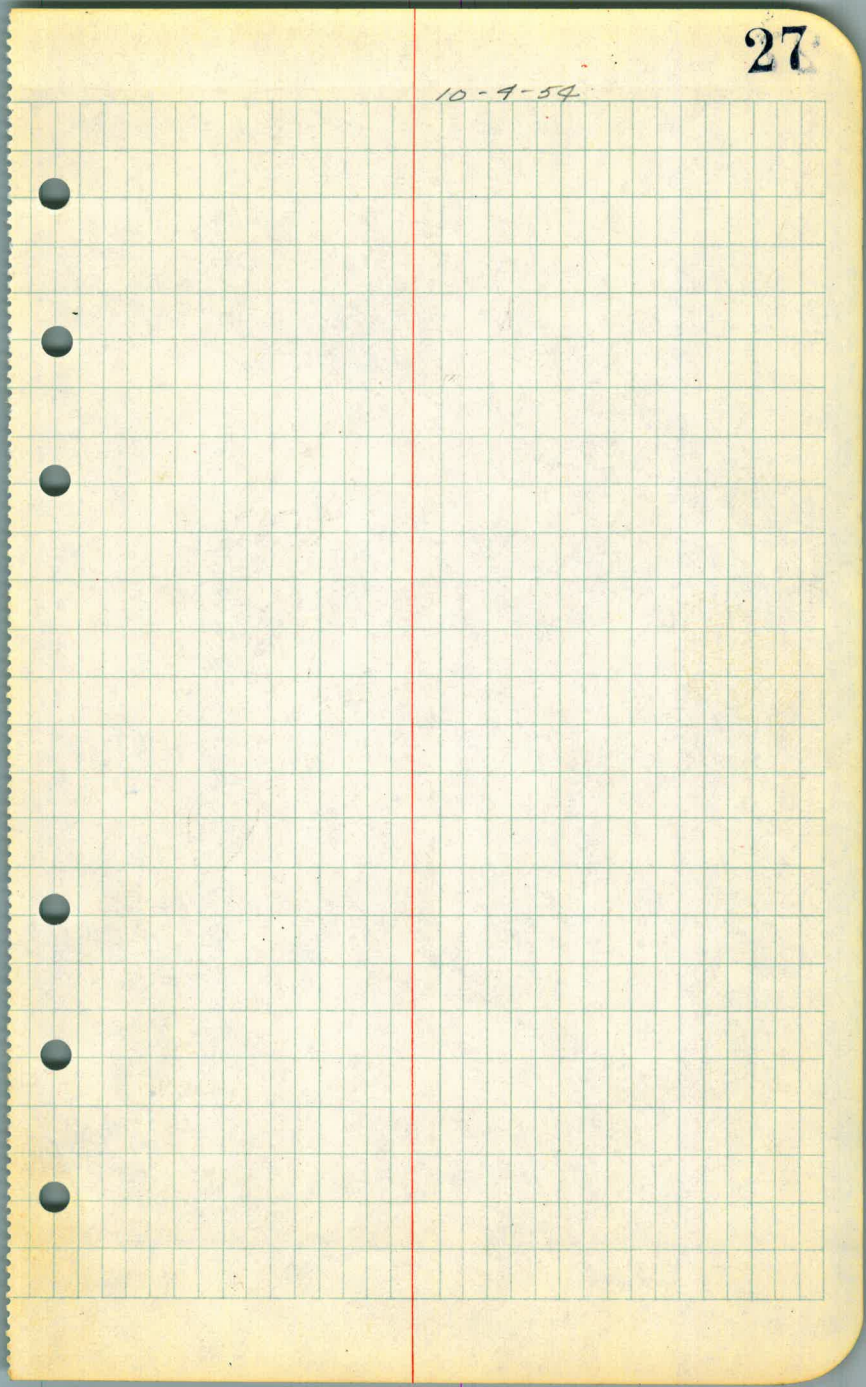


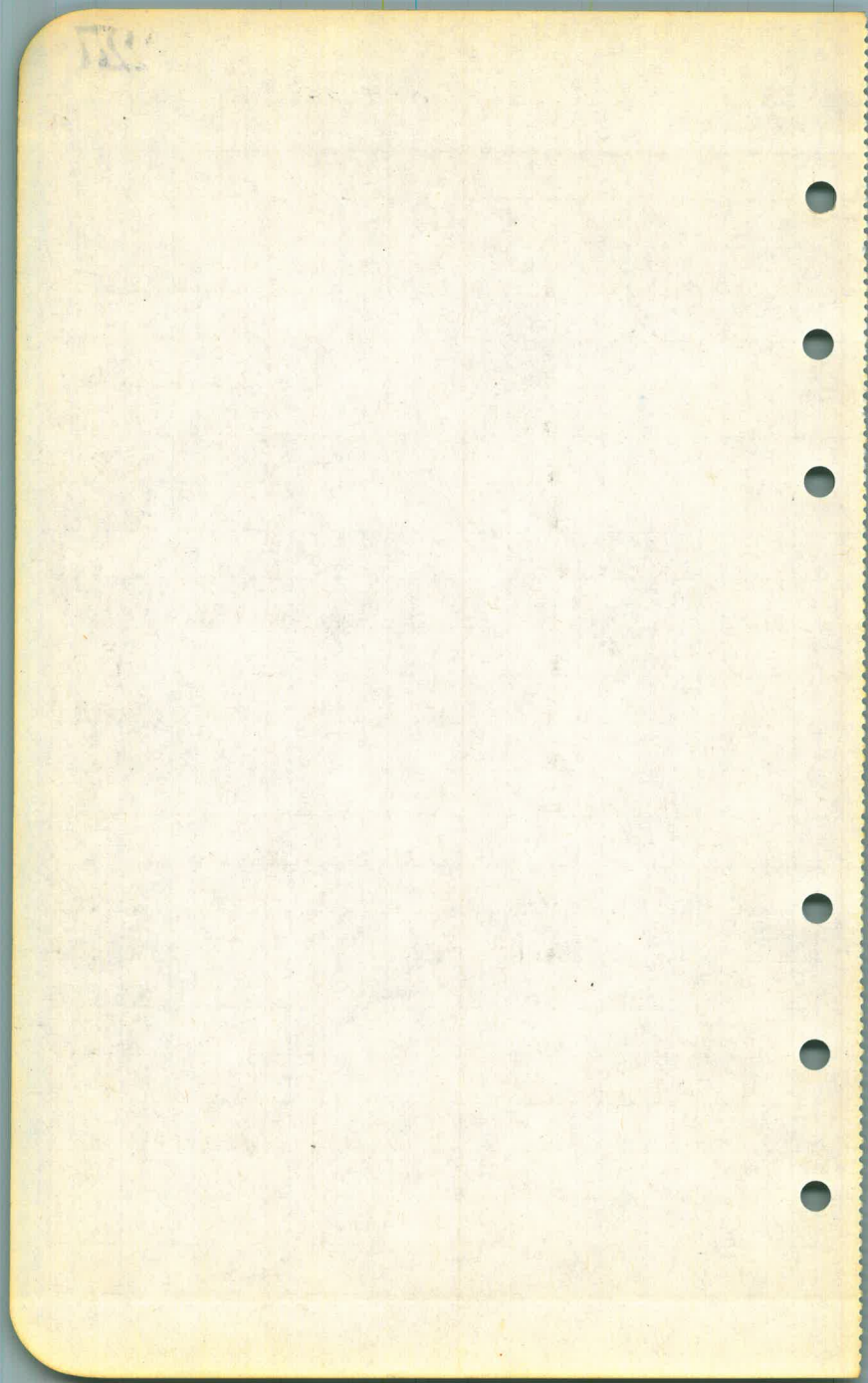
DATE	DESCRIPTION	AMOUNT
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1952-1-3
1952-1-4
1952-1-5
1952-1-6
1952-1-7
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1952-1-9
1952-1-10
1952-1-11
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1952-1-21
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1952-1-23
1952-1-24
1952-1-25
1952-1-26
1952-1-27
1952-1-28
1952-1-29
1952-1-30
1952-1-31

27

		677.45		
			0.55	676.90✓
	11.26	688.16✓		
50+50			2.2	679 ⁰
50+77			3.8	684 ⁴
			0.24	687.92✓
	12.40	700.32✓		
51+00			10.9	689 ⁴
51+24			3.0	697 ³
51+35			0.5	699 ⁸
			0.44	699.88✓
	12.77	712.65✓	12.77	
51+50			9.9	702 ⁸
51+80			0.8	711 ⁹
			0.30	712.35✓
	12.30	724.65✓		
52+00			4.6	719 ^L
			0.60	724.05✓
	11.96	736.01✓		
52+20			10.5	725 ^E
52+40			3.6	732 ⁴
52+50			0.9	735 ^L
			0.36	735.65✓
	12.34	747.99✓		

10-7-54





18

1	100	100
2	200	200
3	300	300
4	400	400
5	500	500
6	600	600
7	700	700
8	800	800
9	900	900
10	1000	1000
11	1100	1100
12	1200	1200
13	1300	1300
14	1400	1400
15	1500	1500
16	1600	1600
17	1700	1700
18	1800	1800
19	1900	1900
20	2000	2000

		747.99✓		
52+02			3.1	744 ⁹
			0.11	747.88✓
	11.39	759.27✓		
53+02			7.0	752 ³
53+21			3.5	753 ⁸
53+23			3.9	755 ⁴
53+36			1.4	757 ⁹
			0.85	758.42✓
	9.80	768.22✓		
53+50			8.4	759 ⁸
53+80			5.6	762 ⁶
54+00			2.9	765 ³
			5.34	762.88✓
	1.33	764.21✓		
54+13			2.7	761 ⁵
54+50			6.4	757 ⁸
55+00			11.0	753 ²
55+10			13.1	751 ⁻
			12.86	751.35✓
	7.1	752.79✓		
55+25.97			4.45	748 ³⁴
55+50			7.1	745 ¹

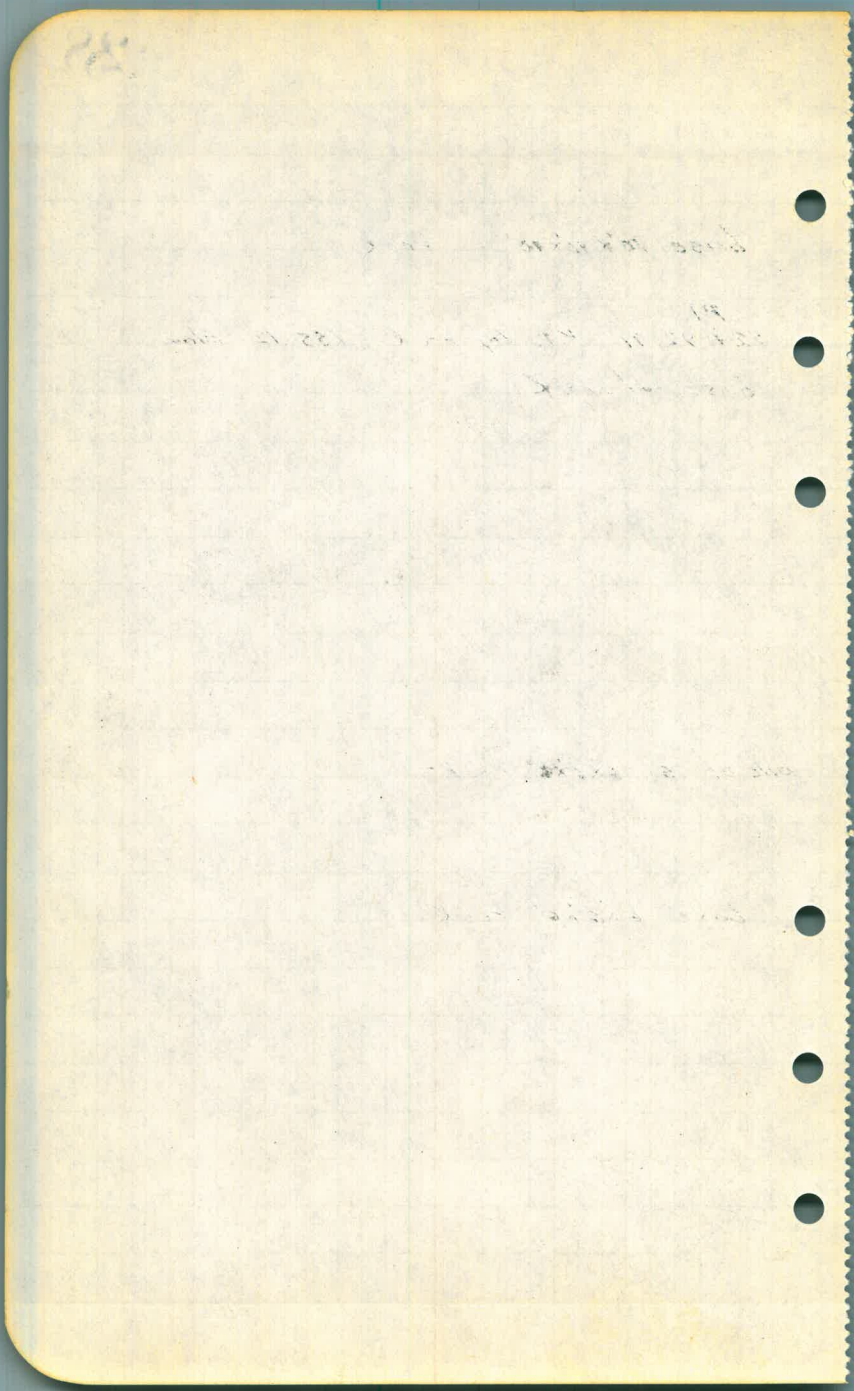
base 10' x 10' x 10' rock

P.I.
52 + 92.91 P.I. Top rock 755.12 Elev.

base of rock

pile of 5 6' x 6' rocks

base 6' x 6' rock



185

19.8.81 24.8

82

80

80

80

19.8.81 24.8

82

80

80

80

19.8.81 24.8

82

80

80

80

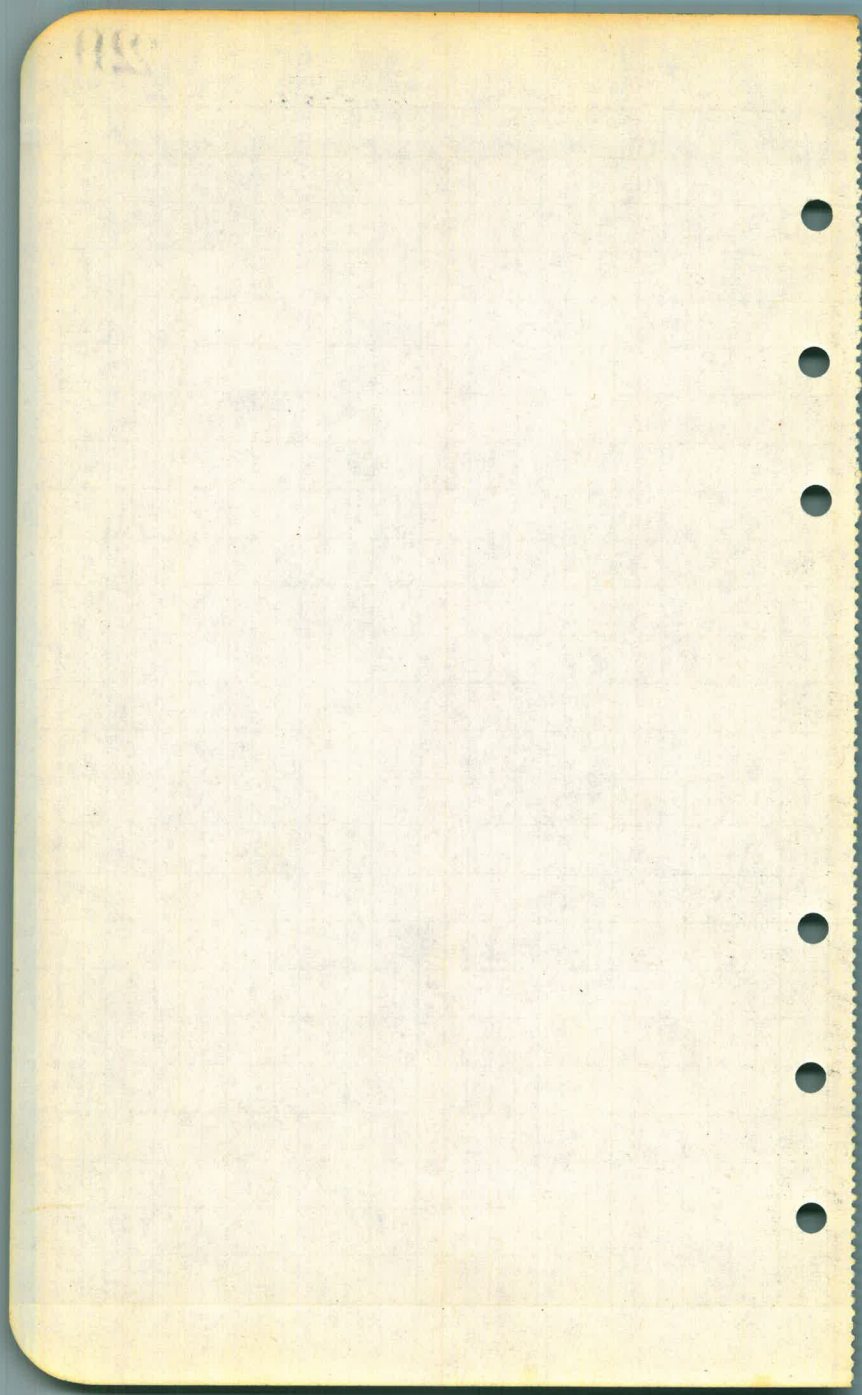
80

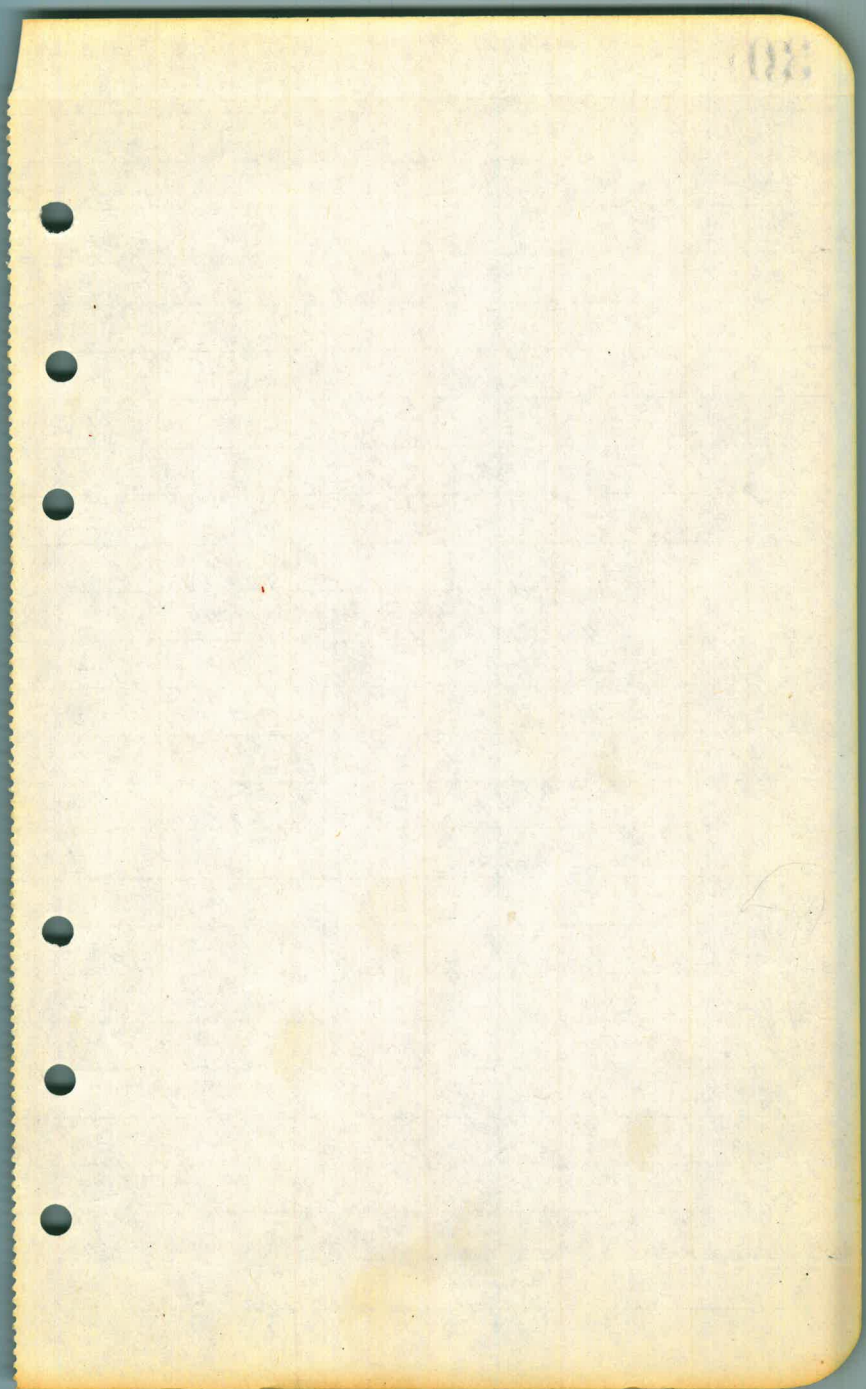
19.8.81 24.8

82

		752.79 ^v		
			12.92	739.87 ^v
54+97	0.33	740.20 ^v		
56+00			3.3	736 ⁹
56+06			5.7	734 ⁸
56+21			9.9	730 ³
56+50			13.6	726 ⁶
			12.42	727.78 ^v
	0.92	728.70 ^v		
56+62			3.4	725 ³
56+65			4.8	723 ⁹
57+00			5.0	723 ⁷
57+08			7.8	720 ⁹
			12.38	716.32 ^v
	7.83	724.15 ^v		
57+13			9.5	714 ¹
57+23			12.9	711 ³
57+33			9.3	714 ⁹
57+50			7.5	716 ¹
57+69			12.6	711 ⁶
57+80			12.56	711.59 ^v
	1.73	713.32 ^v		
57+89			6.1	707 ³

10-9-54

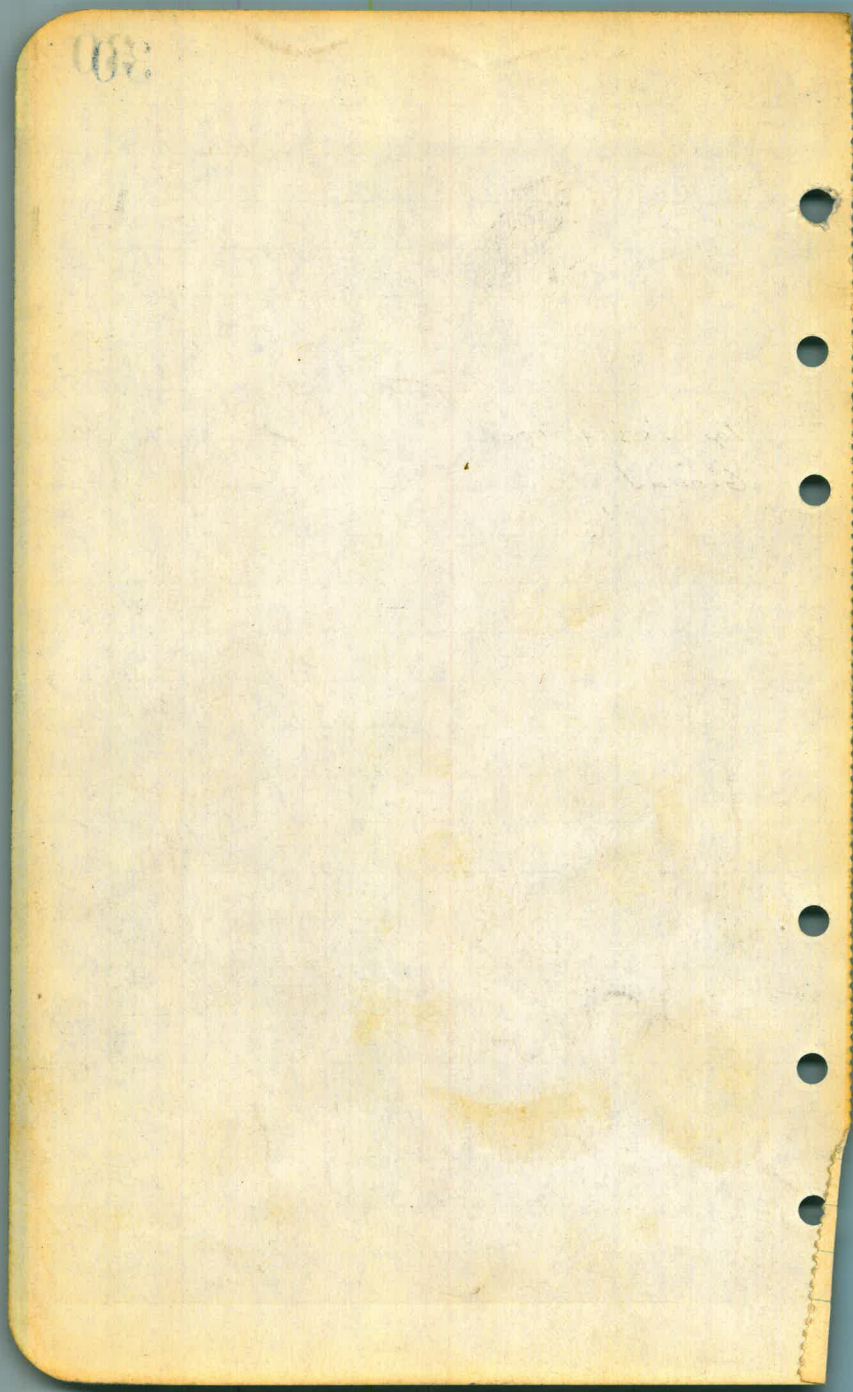




	713.321		
57+91		9.1	704 ²
58+00		11.9	701 ⁴
		12.02	701.30 [✓]
	0.90	702.20 [✓]	
58+08.41		0.26	701 ⁹
" " "		3.0	699 ³
58+26		8.1	694 ¹
		12.36	689.84 [✓]
	0.63	690.47	
58+50		0.7	689 ⁸
58+62		4.7	685 ⁸
58+84		11.7	678 ⁸
		12.76	677.71 [✓]
	0.26	677.97	
58+90		1.6	676 ⁴
58+96		8.2	668 ⁸
59+00		8.9	668 ¹
		12.70	665.27 [✓]
	0.22	665.49	
59+11		4.4	661 ¹
59+23		9.2	656 ³
59+36		13.3	652 ²
		12.89	652.60 [✓]
	0.76	653.36 [✓]	

10-9-54

Top 2x3x4' rock
Ground



Please Return to
City of San Diego Water Dept,
Room 903 Civic Center

758.63
7.76
750.87
66
21

750.66
750.54

JRO

59.41
53.32
6.09

759.41
53.32
6.09

20
9
11