

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

ROD FENCE
JAN 1940

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table is located by the side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

3.8
35
373.
43
416

Cuts

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	10	19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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C.J.
 Shedd
 Made
 2/11
 Pickwick St 34th to 35th
 Stks for 6" AC Main

B.M.	0.21	78.10	72.89
0+40		1.6	76.5 71.8
+50		2.1	76.0 71.5
+65		2.8	75.3 71.2
+65		2.8	75.3 74.5
+91 M.N.		1.8	76.3 73.9
1+00		4.2	73.9 69.4
+33 M.N.		3.4	74.7 72.2
+50		6.4	71.7 67.4
+92 M.N.		6.3	71.8 69.7
2+00		8.3	69.8 65.2
+37 M.N.		7.2	70.9 68.2
+50		9.4	68.7 64.1
+62 M.S.		10.1	68.0 67.0
+90 M.S.		9.8	68.3 66.5
3+00		9.9	68.2 62.9
+16 M.N.		8.9	69.2 66.4
+50		11.4	66.7 61.8
T.P.	0.46	67.54	11.02 67.08

West
 Williams
 Vavontakos T
 Kellhoffer &
 Clear + warm

2/11/65

Sec FB 877 Page 42

Top South run sewer MH 9' 2" 0+30
 C4 ⁷
 C4 ⁵
 C4 ¹
 F.H TEE
 C0 ⁸
 FH (5)
 C2 ⁴
 C4 ⁵
 C2 ⁵
 C4 ³
 C2 ¹
 C2 ⁶
 C4 ¹
 C2 ¹
 C4 ⁶
 C1 ⁰
 C1 ⁸
 C1 ³
 C5 ⁸
 C2 ⁹
 C4 ⁹

PICKWICK ST. CONT.

2.

67.54

3+95 M.S. 1.7 65.8 64.2

4+00 2.0 65.5 60.6

+06 M.N. 0.4 67.1 64.4

+50 2.6 64.9 59.4

+58 M.S. 2.9 64.6 62.8

5+00 4.0 63.5 58.2

+05 M.S. 4.0 63.5 61.6

+02 M.N. 3.1 64.4 62.2

+50 6.0 61.5 55.8

+65 M.N. 5.2 62.3 60.2

6+00 9.2 58.3 53.2

+24 M.N. 11.3 56.2 56.4

+50 13.2 54.3 49.8

T.P. 9.79 14.74 12.59 54.95

7+00 11.5 53.2 48.6

T.P. 10.55 74.75 0.54 64.20

CHECK 7.67 67.08 = 67.04

C₁ 6C₄ 9C₂ 1C₅ 5C₁ 8C₅ 3C₁ 9C₂ 2C₅ 1C₂ 1C₅ 1F₀ 5C₄ 6

2/11/55

FB 877 PAGE 42 S.RIM M.H 3+60

C V X
check
N 400
2/17

Island SE 32nd to Bancroft
stks for 6" AC main

	7.39	89.41	82.02
0+10		6.9	82.5 78.4
+625'		7.0	82.4 78.4
1+00		6.6	82.8 78.7
+105 mn		6.4	83.0 82.4
+112 mn		6.5	82.9 82.5
+130 mn		6.5	82.9 82.6
+150		6.1	83.3 79.1
+165 mn		6.0	83.4 82.9
+190 mn		5.9	84.0 83.2
2+00		5.3	84.1 79.6
+106 mn		5.3	84.1 83.3
+25'		5.0	84.4 79.8
+50 mn		5.1	84.3 83.1
+50		4.9	84.5 79.5
+75'		5.2	84.2 78.2
3+00		6.1	83.3 76.2
	2.27	81.08	10.60 78.81
+31 mn		0.6	80.5 76.4

West
Williams &
Varonakis
Kellhofer ♀

3

2/11/55

BM NW ② KAT 32 nd + Island	
C4 ¹	begin work
C4 ⁰	
C4 ¹	
C4 ⁶	
C0 ⁴	32089
C0 ³	3210
C0 ² <small>Wash. Ginnery</small>	3211
C4 ²	3212
C0 ⁵	3216
C0 ⁸	3217
C0 ⁸	3221
C4 ⁵	
C0 ⁶	
C4 ²	3225
C1 ⁰	
C5 ⁰	
C6 ¹	
C7 ¹	
C4 ¹	

151 and St Cont.

1

81.08

+65.50

2.6 78.5 69.3

C9 $\frac{2}{8}$

+65 m.s

4.7 76.1 71.6

C4 $\frac{1}{8}$

+62 MN

3.9 77.2 72.1

C5 $\frac{1}{2}$

+79 MN

6.1 75.0 69.8

C5 $\frac{2}{2}$

+87.5

7.9 73.2 64.0

C9 $\frac{2}{2}$

+100

9.6 71.5 63.4

C8 $\frac{1}{2}$

+13

11.0 70.1 62.9

C7 $\frac{2}{2}$

9.29 89.17 0.90 80.18

2/11/55

3239

3236

32

end of work

7.92 82.02 - 82.02

CUX
Shoe
Made
2/11

Logan Ave 35th to Wabash & W.
Stks for CAC Main

	11.45	55.64		14.19	
0+60	0.93	53.10	3.17	52.47	48.0
1+00			2.1	51.3	46.6
+27 ms			3.5	49.9	49.5
+50			1.6	48.8	44.9
+73 ms			5.1	48.0	48.0
+91 ms			6.5	46.9	47.3
2+00			6.6	46.8	43.0
+25 mn			7.1	46.0	46.0
+33 ms			7.9	45.4	46.0
+50			8.7	44.7	40.9
+75 mn			9.8	43.6	42.8
+83 ms			10.2	43.2	43.3
3+00			11.0	42.4	38.6
+23 ms	0.63	41.53	12.50	40.90	40.7
+27 mn			1.4	40.1	40.4
+50			2.8	38.7	34.0
+62 mn			4.7	36.8	37.5
+87 ms			6.1	35.9	35.0

West
Williams &
Varonfakis &

5

2/19/55 SUNNY & WARM

55 Top FH 35th + National

C4	5	
C4	7	
C0	4	
C3	9	
C0	0	
F0	4	
C3	8	
C0	0	
F0	6	
C3	8	
C0	8	
F0	1	
C3	8	
C0	2	
C0	3	
F0	7	
C4	7	
F0	7	
C0	4	

LOGAN AVE. CONT.

AI.53.

4+00	0.66	7.7	33.8	29.4	C4	<u>4</u>
+32 MN		29.75	12.44	29.09	F0	<u>1</u>
+50		1.9	27.9	23.7	C4	<u>2</u>
+75 MN		6.2	23.6	25.0	F1	<u>4</u>
+89 MN		6.3	23.5	24.0	F0	<u>5</u>
+99 MN		8.4	21.4	22.0	F0	<u>6</u>
5+00		8.0	21.8	18.0	C3	<u>8</u>
+19 MN		10.0	19.8	19.7	C0	<u>1</u>
+38 MN		12.5	17.3	17.5	F0	<u>2</u>
+50 FH TEE		13.3	16.5	12.0	C4	<u>5</u>
+50 (5°) CTH		13.3	16.5	16.0	C0	<u>5</u>
		7.81	21.91			= 21.88 Turn on 18 Prep Cor

12.48 19.96 36.98

3.51 52.59 0.38 19.08

7.91 44.68 = 44.19 Top FH SF Cor 25th + National

0.83 50.12 33.0 19.29

6.19 43.51 12.70 37.32

6.52 36.99 = 36.99

2/14/55

6

SE BP 36th + National.

CUT
SHEET 2/17
MADE

151 and 5t 36th to 300' west
stks for 6" ACMam

	5.01	125.93	120.92
0+09		4.4	121.5 117.8
+11 FH TEE		4.2	121.7 117.4
+41 (5) FH		5.7	120.2 120.6
+50		4.1	121.8 117.2
1+00		5.1	120.8 116.4
+50		5.6	120.3 115.7
+68 m9		7.2	128.7 118.7
2+00		7.8	118.1 115.0
+18 mN		9.8	121.1 119.0
+50		8.2	117.7 114.2
+90 mN		5.2	120.7 117.5
+95		7.9	118.0 113.4
	5.01	120.92	= 120.92

West
Williams π
Varontakis φ

7

2/15/03 - HAZY + WARM
sec 892 page 13

on cone men 27 North of south prop line

C₃ ¹₃
Begin work
C₄ ⁴
F₀ ⁴
C₄ ⁴
C₄ ⁴
C₄ ⁶
C₀ ⁹
C₃ ¹
C₂ ¹
C₃ ⁵
C₃ ²
C₄ ⁶

Spec
Work
2/17

Maple Court + 30th St
Stks for A" AC Main

	1.92	288.78	286.85
30 th St	6.63		
630+00 North	286.99	8.92 279.86	276.2
630+00 East		17.0 279.15	276.2
+50		5.9 280.6	276.5
+100		5.2 281.3	277.0
+150		3.7 282.8	278.2
+195		2.3 284.2	280.3
Maple Court	11.79	291.60	6.68 279.81
0+75-		10.0 281.6	277.6
291 miv		8.6 283.0	283.0
+100		8.0 283.6	279.3
+10 ms		7.1 284.5	284.3
+25		6.3 285.3	281.0
+29 ms		6.1 285.5	285.5
+33 mn		5.9 285.7	285.5
+50		5.0 286.6	283.0
+66 ms	4.3	287.3	287.1
+100	3.5	288.1	284.0
+13 ms	3.5	289.1	288.2
+91	2.8	288.8	284.9
	4.72	286.88	= 286.85

West
Williams &
Varonfokis ♀

8

2/16/55 RAIN 4:00 P.M.
See FB 877 Page 10

Top South edge Sower MH

C3	7	290.79
C3	3	280.86
C4	1	277.0 C3
C4	3	278.0 C3
C4	6	279.2 C3
C3	9	End of 30 th St Line

C4	0
C0	0
C4	3
C0	2
C4	3
C0	0
C0	2
C3	6
C0	2
C4	1
FO	1
C3	9

end of work

out shoot
made

Alley BIK 3
So. of Lewis East of Fourth
5th St. for 6" AC Main

West
Williams &
Varonokakis

9

2/18/55 PARTLY CLOUDY

	1.92	285.09	283.12	SW OP. Fourth & Lewis
6	0+39		5.3 279.7 275.7	C4 <u>0</u> Begin Work
15	+50		5.1 279.9 276.3	C3 <u>6</u> <u>3</u>
	+76 mw		3.1 281.9 281.6	C0 <u>8</u>
	+100		2.5 282.5 278.7	C3 <u>2</u>
	+109 mw		1.8 283.2 283.0	C0 <u>1</u>
	+150		1.0 284.0 279.9	C4 <u>1</u>
	+154 mw		0.8 284.2 284.3	F0 <u>1</u>
6	5.91	290.73	0.25 284.79	
	+199 mw		5.5 285.2 285.0	C0 <u>2</u>
1	2+00		5.9 284.8 281.0	C3 <u>8</u>
	+34 mw		5.3 285.4 285.4	C0 <u>0</u>
	+50		5.9 285.3 281.4	C3 <u>9</u>
	+55 me		5.1 285.6 285.4	C0 <u>2</u>
	+75 mw		5.0 285.7 285.8	F0 <u>1</u>
3	1+00		5.2 285.5 281.8	C3 <u>8</u>
	+106 3 285.21		5.2 285.5 281.7	C3 <u>1</u>
	+115 mw		5.0 285.7 285.8	F0 <u>1</u>
	+29 3 30° 11		5.3 285.4 281.3	C4 <u>1</u>
	+50		5.9 284.8 280.9	C3 <u>9</u>

Alley BIK 3 cont

10

290.23

3+79

3+80

61 284.62 80.3

C4³

2/18/55

End of work

1.20 284.98 6.95 283.78

1.87 283.11 = 283.12

Cut shot
+14 Je

Neale SE Pringle to Keating

West
Williams &
Varon Falsist

110

11.06 248.15 237.99

10.41 258.23 0.63 217.82

0-07 FH Tce 42254 0 250.0

0+00 40 254.2 250.1

+50 4.2 254.0 250.0

1+00 94 248.8 244.7

0.29 242.65 1287295.36

+50 1.1 244.6 239.6

+70 4.0 241.7 236.2

2+00 104 235.3 230.8

0.28 233.02 1291232.74

+25 1.0 229.0 224.2

+50 10.3 222.7 218.0

0.85 221.81 1206220.96

0.17 210.18 1210209.71

3+00 2.1 208.1 202.3

+125 5.9 204.3 197.5

0.14 197.27 1305197.13

+43 FH Tce 1.9 195.4 191.4

+43 ② FH + 1.1 198.4 195.4

2/21/55 CLEAR - WINDY
500 PB 980 P 27

SW FH Tce + Pringle

C4 ⁰
₁

C4 ⁰

C4 ⁰

C4 ¹

C4 ⁰

C5 ⁰

C5 ⁵

C4 ⁵

C4 ⁸

C4 ¹

C5 ⁸

C6 ⁸

C4 ⁰

C3 ⁰

Neals St Cont

12

197.27

3+50

3.1 194.2 190.0

C4 $\frac{2}{1}$

+80 Tree
East

4.2 193.1 187.8

C5 $\frac{3}{1}$

+80 Tree(6)

4.6 192.7 187.8

C4 $\frac{9}{1}$

4+00

6.8 190.5 186.4

C4 $\frac{1}{1}$

+16

8.3 189.0 185.3

C3 $\frac{1}{1}$

2/21/55

End of Work

276 194.51 = 194.94 TOM SW city eng hub

Our show
Made

Torrence St Pringle to 230' Wood
STKS for 6" AC Main (A)

West
Williams &
Varonfakis &

13.

2/21/65 CLEAR WINDY

7.28	244.67	237.39			
0+00		7.9 236.8 232.8	C4	0	SW EH Torrence + Pringle
+50		6.6 238.1 233.7	C4	4	Begin Work
1+00		2.2 242.5 237.9	C4	6	
+25		0.7 244.0 239.2	C4	8	
+50		0.6 244.1 239.8	C4	3	
+75		1.1 243.6 239.0	C4	4	
+78 mws		1.7 243.0 242.8	C0	2	
2+00		2.6 242.1 237.0	C5	1	
+03 mE		2.7 242.0 241.4	C0	6	
+27 mE		5.4 239.3 239.2	C0	1	
+22 mW		6.1 238.6 238.8	F0	2	
+30		5.5 239.2 234.7	C4	5	End of Work
	7.28	237.39			237.39

out shoot
Made

Guy 56 Pringle to Roating
stks for 6" AC Main

West &
Williams
Varonakis &

14

1.92	200.38	198.46	
0+35'	38	196.6 193.4	
+50	41	196.3 193.0	
1+00	5.4	195.0 191.4	
+09 mw	6.0	194.4 194.3	
+50	8.3	192.1 186.0	
0.17	187.92	186.3 187.75	
P.G.T.			
1+75'	1.1	186.8 181.0	
+75' ME		186.5 187.5	
2+00	9.9	178.0 174.0	
1.14	176.78	1228 175.61	
+125	2.8	174.0 161.0	
+11 ME	1.2	175.6 165.0	
+17 mw	3.8	172.0 164.0	
+50 0.95	164.92	12.81 163.97	153.2
2+72 mw	7.2	157.7 152.9	
+75	7.3	157.6 148.0	
0.36	152.84	12.44 152.18	
3+00	1.3	151.5 143.0	
+25	3.8	149.0	
		137.2	C11

2/21/95
See FB 857 P54

Top FH SW Cor Guy + Pringle

2 C3 Begin Work

C3 3

C3 6

C3 1

C0 1

C6 1

C5 8

C4 0 F10 186.8
4.9 141.7

C13 0

C10 6 moved to 1+75'

C9 0

C4 8

C9 6

C8 5

C11 8

GUY ST CONT

15

152.84

1.91 191.90 12.35 140.99

3+00

5.1 136.8 131.6 C5²

4.78 137.12 = 137.09

136.8

2/21/55

end of work

500 FB 807 1400 02

Car Boni Stop 1st up 95 ± 18 3291

Linwood St

MISSION HILLS Blvd to
KootenayStks for 6" AC Main
169.87
0.46 109.50163.41
163.04WEST
WILLIAMS X
VARONFAKIS ♀

16

2/28/55

1+03

16.6 153.3 151.0

147 NW Cor Pringle + Linwood

C2 3

Begin work

+50

8.1 161.8 155.0

C6 8

+64 MW

8.8 161.1 160.1

C1 0

+64 ME

5.3 164.6 161.0

C3 4

164.32

5.11

169.73

6.37

163.34

2+00

7.2 162.7 157.4

C5 3

+50

7.8 162.1 159.3

C2 7

+52 MW

7.8 162.1 163.8

F1 5

+96 ME

3.1 166.8 166.3

C6 5

3+00

6.6 163.3 159.8

C3 5

+07 ME

2.5 167.9 166.6

C0 8

+42 MW

5.6 161.3 165.0

F0 7

+60

6.5 163.4 160.0

C3 4

end of work

4+00

5.2 164.7 160.2

C4 5

Begin work

1

6.08 173.71
~~173.34~~ 2.29 167.63
~~167.66~~C3 7

+41 ME

2.0 171.1 167.4

C8 1

+50

5.5 168.2 160.1

C4 1

+57 ME

2.1 171.6 167.5

C8 0

5+00

5.7 168.0 160.0

LINWOOD ST. CONT.

17

173.71
173.79

+701 m.w.		6.3	167.4	166.1
+74 m.E		5.2	168.5	166.4
+75		6.6	167.1	160.0
+91 m.w.		7.5	165.2	165.1
+50		7.9	165.8	158.8
+53 m.E		6.3	167.4	165.5
+65 m.w.	162.66	9.0	164.7	163.2
6+00	1.22	162.29	122.7	161.07
			161.44	153.4
+23 m.w.		4.9	157.8	153.7
+25		6.7	156.0	147.7
+37 m.E		9.2	153.5	150.3
TP	0.56	153.92	9.30	153.36
		153.55		2.99
+50		1.3	152.6	142.0
+73 M.W.		6.5	147.4	141.4
+75		8.1	145.8	136.3
TP		141.75		141.29
+86 M.E.	0.46	144.38	12.63	140.92
				137.8
7+00		7.1	134.7	131.0
TP		139.30		132.50
		6.80	138.93	9.25
				132.13
				137.16 = 137.09
				= .07
		2.14	136.79	= 137.09
				= .30 (PAGE 15) (SEE PAGE 18 FOR CHECK LEVELS)

2/28/55

C1 3C1 9C7 1C1 1C7 0C1 9C1 5C8 0C4 1C8 3C3 2in back of 6+00 m.E
Turn on Top Cobble Wall

CHECK LEVELS GUY + PRINGLE TO
KEATING + PRINGLE

B.M.	0.91	199.37		198.46
TP	1.07	188.07	12.37	187.00
TP	0.96	176.31	12.72	175.35
TP	4.35	172.38	8.28	168.03
CHECK T.B.M.		8.97	163.41 =	163.04

WEST
WILLIAMS X
VARONFAKIS ♀

18

F.B. 857 - P. 54

TOP FH S.W COR GUY + PRINGLE

L + T N.W COR. PRINGLE + LINWOOD

CUT SHEET
MADE 3/1 Longbranch St Abbott to Spray
Spray St Longbranch to W PT Longbranch
57ks for 6" AC Main

B.	3.59	6.85	3.31
T.	0+20	3.1	3.8 -0.3
T.	+50	3.8	3.1 -0.5
T.	+100	4.8	2.1 -0.8
CH.	+15 mn	4.4	2.5 2.8
T.	+27 mn	4.0	2.9 3.6
	+50	5.1	1.8 -1.0
	+71 mn	4.5	2.4 2.8
	+69 mn	4.3	2.6 3.3
	2+00	5.0	1.9 -1.2
	+108 mn	4.8	2.1 2.9
	+130 mn	4.5	2.1 2.9
	+37 mn	4.6	2.3 3.1
	+50	4.9	2.0 -1.4
	+72 mn	4.6	2.3 3.2
	+94 mn	3.4	3.5 3.2
	3+00	4.4	2.5 -0.9
	+16 mn	1.9	5.0 3.6
	+16 mn	1.6	5.3 3.3

West.
Williams X
Varonfakis

19

3/2/55

BM NE BP Longbranch + Abbott

C 4 $\frac{1}{1}$
Begin Work
C 3 $\frac{6}{6}$
C 2 $\frac{9}{3}$
Fo $\frac{1}{1}$
Fo $\frac{1}{1}$
C 2 $\frac{8}{4}$
Fo $\frac{4}{4}$
Fo $\frac{1}{1}$
C 3 $\frac{1}{8}$
Fo $\frac{5}{5}$
Fo $\frac{8}{8}$
Fo $\frac{4}{4}$
Fo $\frac{9}{9}$
C 0 $\frac{3}{3}$
C 3 $\frac{4}{4}$
C 1 $\frac{4}{0}$
C 2 $\frac{0}{0}$

Longbranch Cont.

20

6.85

+149 mn	1.5	5.9	3.4
+45 ms	3.9	3.5	3.8
+50	3.8	3.1	-0.2
+86 ms	1.1	0.8	4.2
+92 mn	1.4	5.5	3.5
	4.38	7.59	364 3.81

+100	4.05	3.57	-0.4
+50	4.2	3.4	-0.7
+64 ms	2.9	4.7	3.8
+73 mn	5.1	2.5	3.1
5+00	4.8	2.8	-1.0
+50	5.7	1.9	-1.1
6+00	7.4	0.2	-3.2
+50	7.2	0.4	-3.2
+80 ♂	7.8	-0.2	-3.2
0+25	7.3	0.3	-3.2
+50	7.4	0.2	-3.2
+63 FH 100	7.5	0.7	-2.8
+63 (57 ± 0H)	7.5	0.1	2.2
1+00	5.7	1.9	-1.6
+34	5.9	1.7	-2.0
	4.28	3.31	= 3.31

3/2/55

C₂ ⁰
F₀ ³
C₃ ³
C₁ ⁶
C₂ ⁰

C₃ ⁹
C₄ ¹
C₀ ⁹
F₀ ⁵ NOT 54
C₃ ⁸
C₃ ⁰
C₃ ⁴
C₃ ⁶
C₃ ⁰
C₃ ⁵
C₃ ⁴
C₂ ⁹
F₂ ¹
C₃ ⁵
C₃ ⁷

Quinn St 30th to 31st

54K5 for 6" AC Main

Stn 3+75 to 5+25 replace

10.53 312.59

302.06

1.93. 311.99 2.53 310.06

0.58 304.29 8.28 303.71

3+75

1.7 302.6 299.0

C³ ⁶

4+00 0.37 291.88 12.78 291.51 287.5

C⁴ ⁰

4+25

11.6 280.3 276.0

C⁴ ³

0.73 280.12 12.49 279.39

4+50 0.16 268.00 11.98 268.14 263.0

C⁵ ¹

4+75

11.3 257.3 254.8

C² ⁵

1.80 259.00 11.10 257.20

C⁷ ²

5+00

4.8 259.2 247.0

C⁵ ²

5+25

6.8 252.2 247.0

247.1

West
Williams &
VaronFokis &

21

3/3/55

SWBP 30th & Redwood St

Cut sheet
made 3/4/55

33rd 54 Date to Elm
54ks for 6" AC Main

22

West

Williams X

Varonفاتیج 3/4/55 Cloudy

491	231.91	226.03	NW 13° Barcroft + Elm
9.89	240.67	066 230.78	
0+80	7.0	233.7 230.0	C3 2 begin work
1+00	4.3	236.4 229.1	C3 0
+46 mE	6.6	234.1 230.3	C3 ⁸
+50	6.4	234.3 227.2	C3 1
+63 mW	7.1	233.3 229.6	C3 ⁷
+75	8.4	232.3 226.0	C3 3
2+00	131 229.83	125228.52 221)	C4 1
+01 mE	2.1	227.7 226.2	C1 ⁵
+40 mE	4.3	225.5 221.8	C3 ⁷ ??
+50	5.1	224.7 220.1	C4 3
+62.5	6.5	223.3 219.4	C3 9
+98 mW	11.2	218.6 213.0	C5 ⁶
10.27	238.22	1.88 227.95	
1.43	231.61	8.04 230.18	
0.95	228.90	6.07 226.59 = 226.53	

2+75 059 217.91 12.08 216.82 213.9 C31

1719 NW 011
Turn on one block house

33RD ST CONT.

23

217.41

510
200.7
110

3+00	0.71	205.78	10.7	206.7	204.0	C 2 ²
+25	1.09	193.03	6.7	198.8	193.6	C 3 ⁻²
+50			12.03	192.93		
+62.5			9.7	190.3	189.1	C 6 ⁻²
+75			7.0	187.0	180.0	C 7 ⁰
4+09			7.9	186.1	180.0	C 6 ⁻¹
			6.2	187.8	185.0	C 2 ⁻⁸
			12.61	205.88	0.76	193.27
			12.79	218.42	0.25	205.63
			12.00	230.06	0.31	218.11
			3.61	226.55	-	226.53

End of work

Dudley St
Silvergate to Catalina

west
Williams
Varon Park

24

12.70	30 7.92	295.22
+20	12.7	295.2
+20	11. ³ 4	296.5
+21 FH Tee	10.1	297.8
+21 (D) FH	8.3	299.6
+20	8.0	299.9
+20	4.3	303.6
+26 m3	2.0	305.9
+200	1.9	306.0
+50 304 3/10.27	0.19	307.73
192 m5	1.8	309.0
+200	—2.2	308.6
+100 mN	(1.7)	309.1
+50	2.8	308.0
+100	1.5	306.3
+12 m5	1.5	306.3
+16 mN	0.3	305.5
+50	6.8	304.0
+70 m3	7.5	303.3

321/55- prolonged eastly
L+T on east cb of Silvergate + D Dudley
Begin work

DUDLEY ST. CONT.

25

310.77

5+00	9.3	301.5
+13 mn	10.7	300.1
2.67	300.85	12.59 298.18
150	1.7	299.2
166 50 100	2.8	298.1
+66 @ EII	2.1	298.8
1400	1.8	296.1
+31 ms	5.7	295.2
+31 mn	8.0	292.9
+50	8.2	292.7
7+00	11.8	289.1
+23 m.s	12.8	288.1
0.95	289.67	12.13 288.72
+31 M.N	3.8	285.9
+50	3.9	285.8
+78 M.S.	5.0	284.7
8+00	7.6	282.1
+50	10.1	279.6
T.P.	2.04	279.25 12.46 277.21

3/4/55

DUDLEY ST. CONT.

279.25

9+00
T.P.
+50

3.2 276.1

6.32 272.93

200

26

3/4/55

CUT
SHEET MADE
3/7

Dudley St
Silvergate to Catalina

STKS FOR 6" A.C. MAIN

	12.99	308.21	295.22	
D+20		12.9	295.3291.6	C ₃ ¹ ₆
+50		11.6	296.6292.0	C ₄ ⁵
+71 FH Tee		10.3	297.9293.4	C ₄ ⁰
+71 (6) FH		9.5	299.7296.7	C ₃ ⁸
1+00		8.1	300.1295.3	C ₄ ⁹
+50		4.7	303.5298.6	C ₄ ⁸
+86 m.s		2.4	305.8305.0	C ₀
2+00		2.3	305.9301.8	C ₄ ¹
+50 3.44	311.02	0.63	307.58303.8	C ₃ ⁸
+92 m.s		2.2	308.8308.4	C ₀ ⁴
3+00		2.7	308.3304.4	C ₃ ⁹
+00 m.s		2.1	308.9308.7	C ₀ ²
+50		3.2	307.8303.2	C ₄ ⁶
4+00		4.9	306.1302.0	C ₄ ¹
+12 m.s		4.8	306.2305.5	C ₀ ⁷
+16 m.s		5.7	305.3305.2	C ₀ ¹
+50		7.2	303.8299.6	C ₄ ²
+70 m.s		7.9	303.1302.9	C ₀ ²

West
Williams &
Varonakis +

27

3/7/55 SUNNY + WARM
Dudley Prob
Silvergate + L

LFT on east ch Silvergate + L
Begin work

Dudley St Cont

28

311.02

5+00 9.7 3013 297.2

+13 MN 11.1 299.9 300.2

1.90 300.57 12.35 298.67

250 1.5 299.1 294.6

766 FH 700 2.7 297.9 293.6

461(6) FH 2.0 298.6 297.9

6+00 4.7 295.9 291.3

+31 ms 5.6 295.0 293.5

+31 MN 7.8 292.8 292.6

+50 8.1 292.5 287.8

7+00 11.6 289.0 284.4

+73 ms 12.6 288.0 287.2

0.92 288.89 12.60 287.97

+31 MN 3.1 285.8 285.7

+50 3.3 285.6 281.1

+78 ms 7.3 284.6 283.5

8+00 6.9 282.0 277.6

+50 9.5 279.4 274.3

1.9.4 278.65 1218 276.71

317/55

C4 1
3

FO

C4 5C4 3CO 1C4 4C1 5CO 2C4 2C4 6C1 8

CO

CO 1C4 5C1 1C4 4C5 1

Dudley St
Cont

278.65

+100

+25

+50

10.89

2.8
4.9

275.9271.7
2738 269.0

C4
C4 8
C3 8

11.71 295.05 0.31 283.31

12.78 307.71 0.09 294.96

1.77 309.10 0.41 307.33

5.39 302.27 12.82296.88

7.04 295.23 = 295.22

29

3/7/55

BEECH ST. FELTON TO
GREGORY.
STKS FOR METERS

WEST
WILLIAMS &
VARONFAKIS +

30

T.B.M. 6.89 220.82 213.93

2+21 M.S. 8.5 212.3 211.8

C O 5

3+40 M.E.
CHECK
T.B.M.

C 6 $\frac{1}{2}$ ON GREGORY

6.89 213.93 = 213.93

3/9/55 SUNNY + WARM

BEECH

F.B. 892 PAGE 7 (7'L&T S.E. FELTON)

29TH ST IMPERIAL To COMMERCIAL

B.M. 4.76 76.81 72.05

S.W.B.P. 29TH IMPERIAL

T.P. 5.98 75.27 7.52 69.29

C O $\frac{7}{2}$ FH (5)

3+75 5.4 69.9 69.2

T.P. 5.37 76.69 3.95 71.32

CHECK
B.M. 4.63 72.06 = 72.05

GREENE ST + SOTO

LOWERING OF MAIN ON GREENE

B.M. 1.47 35.15 33.68

T.P. 12.24 44.39 3.00 32.15

T.P. 12.53 56.84 0.08 44.31

T.P. 7.72 62.83 1.73 55.11

0-14 8.0 54.8 53.3
55.2

0+34 4.1 58.7 55.6
55.1

+39 3.7 59.1 55.6
55.1

+46 3.3 59.5 55.7
55.2

+55 2.55 60.2 55.7
55.7

+67 1.8 61.0 56.6

T.P. 1.09 51.73 12.19 50.64

T.P. 1.46 40.17 13.02 38.71

T.P. 4.94 35.58 9.53 30.64

CHECK
B.M.

$$1.90 \quad 33.68 = 33.68$$

T.B.M. 8.23 63.34 55.11

0+46 8.28 55.06

$$8.23 \quad 55.11 = 55.11$$

WEST
WILLIAMS π
VARONFAKIS φ

31

3/9/55

S.W.B.P ETIWANDA + CASTELAR ST

O+00.15 W. PROP. LINE SOTO
(RADIUS HUB N.W.COR) ON TOP PIPE

C 1 ^{5'} 9.79 53.04

C 3 ^{5'} C 3 ^{5'} 6.24 56.59

C 3 ^{8'} C 4 ^{0'} 6.02 56.81 TEE

C 3 ^{8'} C 4 ^{4'} 5.65 57.18 TEE

C 4 ^{8'} C 5 ^{0'} 5.10 57.73

C 4 ^{4'} C 5 ^{3'} 4.40 58.43

RADIUS HUB NW COR GREENE + SOTO

10' LT. TOP A.C. MAIN ON SOTO

CUT SHEET
MADE 3/15

GALVESTON. GARDENA TO ORTEN
STKS. FOR 6" A.C. MAIN

WEST
WILLIAMS
VARONFAKIS†
MARTEL T.
KELLHOFER

32

3/15/55 CLOUDY

B.M.	11.69	62.94	51.25	N.W.I.P. GARDENA AVE + GALVESTON ST.
0+40		14.2	48.7	452 C3 5
+75		13.0	49.9	46.0 C3 9
+100		12.2	50.7	46.6 C4 1
+105		12.0	50.9	46.7 C4 2
+105		11.7	51.2	50.4 C0 8 F.H. TEE
+136 M.W.		9.5	53.4	52.1 C1 3
+150		10.7	52.2	48.5 C3 7
2+00		8.5	54.4	51.2 C3 3
+50		5.6	57.3	54.2 C3 1
+53 M.W.		5.0	57.9	58.5 F0 6
3+00		2.0	60.9	57.5 C3 4
T.P. 12.68				
+19 M.W.	75.19	0.43	62.51	63.0 F0 5
+50		10.7	64.5	60.8 C3 7
+70 M.W.		8.6	66.6	66.6 C0 0
4+00		6.8	68.4	64.1 C4 3
+50		2.8	72.4	67.6 C4 8
+68 M.W.		1.35	73.8	73.4 C0 4
T.P. 12.90	87.72	0.37	74.82	

GALVESTON CONT.

33

87.72

5+00	12.3	75.4	71.0	C4 ²
+25	11.3	76.4	72.1	C4 ³
+50	10.1	77.6	73.3	C4 ³
6+00	8.0	79.7	74.8	C4 ⁹
+00	8.8	78.9	78.8	FH TEE
+25	6.8	80.9	75.4	C0 ¹
+50	6.2	81.5	75.8	C5 ⁵
+70 M.E.	4.8	82.9	80.4	C2 ⁵
+84 M.W.	6.7	81.0	80.7	C0 ³
7+00	4.0	83.7	77.3	C6 ²
+41 M.W.	4.2	83.5	82.0	C1 ⁵
+50 T.P.	1.7	86.0	78.0	C8 ⁰
8+00	3.21	90.02	0.91	C7 ⁹
+20 M.W.	5.3	84.7	82.9	C1 ⁸
+50	3.5	86.5	78.8	C7 ¹
+76 M.W.	6.5	83.5	82.8	C0 ⁷
9+00	4.4	85.6	78.9	C6 ¹
+41 M.W.	8.4	81.6	82.2	F0 ⁶
+50	6.4	83.6	78.2	C5 ⁴

3/15/55

GALVESTON CONT.

34

90.02

10+00	6.8	83.2	77.0	C5 $\frac{5}{6}$
+35 M.W.	9.5	80.5	81.0	F0 $\frac{5}{6}$
+50	7.4	82.6	77.0	C5 $\frac{5}{6}$
11+00	8.5	81.5	76.4	C5 $\frac{1}{6}$
+50	10.3	79.7	75.9	C3 $\frac{8}{9}$
+84 M.W.	11.7	78.3	79.6	F1 $\frac{3}{8}$
12+00	11.5	78.5	75.7	C2 $\frac{8}{9}$
+35 M.W.	12.7	77.3	79.4	F2 $\frac{1}{6}$
+50	12.1	77.9	75.6	C2 $\frac{3}{8}$
+75	11.5	78.5	75.5	C3 $\frac{0}{9}$
+80	79.4	79.5		
+83 M.W.	12.2	77.8	79.0	F1 $\frac{2}{3} = F0 \frac{1}{2}$
13+00	10.1	79.9	75.9	C4 $\frac{0}{9}$
+16	8.4	81.6	76.2	C5 $\frac{4}{9}$

T.P. 2.03 83.89 8.16 81.86

T.P. 1.47 72.66 12.70 71.19

T.P. 1.48 61.30 12.84 59.82

CHECK
B.M. 10.09 51.21 = 51.253/15/55 WINDY +
CLOUDY12+00 77.9
+ 9.0
8.6.9
79.5
79.986.9
7.1
79.878.9 ⑥ 7H 6+00
+ 6.76
85.66 Top Projec

7+82 6.56 79.1

10+72 8.47 77.19

722 83.44

LA SALLE ST NASHVILLE TO EAST
TERMINUS. STKS FOR 6" A.C.MAIN

WEST X
WILLIAMS
VARONFAKIS ♀

35

N.W.E.H. NASHVILLE + LA SALLE ST

3/16/55 SUNNY + COOL

B.M.	2.62	4.39	1.77	
0+35			4.8 - 0.4 - 4.2	C 3 $\frac{8}{8}$
+50			4.9 - 0.5 - 4.3	C 3 $\frac{8}{8}$
1+00			4.6 - 0.2 - 4.3	C 4 $\frac{3}{3}$
+50			4.5 - 0.1 - 4.4	C 4 $\frac{3}{3}$
2+00			4.5 - 0.1 - 4.4	C 4 $\frac{3}{3}$
+50			4.4 - 0.0 - 4.3	C 4 $\frac{3}{3}$
3+00			4.1 0.3 - 4.2	C 4 $\frac{5}{5}$
+50			4.0 0.4 - 4.2	C 4 $\frac{6}{6}$
4+00			3.8 0.6 - 4.1	C 4 $\frac{7}{7}$
+50			3.8 0.6 - 4.0	C 4 $\frac{5}{5}$
CHECK B.M.			2.62 + 1.77 = 4.39	

WATER METERS STKD.

PAC. BEACH DR LAMONT To
MORRELL

WEST ♀
WILLIAMS
VARONFAKIS X

36

B.M.	2.83	37.93	35.10
0+67 M.N.	4.2	33.7	34.1
1+01 M.S.	5.6	32.3	33.0
+25 M.S.	5.7	32.2	32.8
+37 M.N.	4.2	33.7	33.4
+81 M.N.	4.6	33.3	33.0
2+54 M.N.	5.5	32.4	32.2
3+37 M.N.	6.6	31.3	30.8
+60 M.N.	7.7	30.2	30.2
+91 M.S.	8.4	29.5	29.2
4+25 M.N.	9.8	28.1	27.9
+37 M.S.	9.8	28.1	27.5
+84 M.N.	12.6	25.3	24.9
CHECK B.M.	2.83	35.10	$= 35.10$

N.E. L+T (7) LAMONT + PACIFIC BEACH DR.

Fo 4
Fo 1
Fo 4
Co 3
Co 3
Co 2
Co 5
Co 0
Co 3
Co 2
Co 4
Co 4

3/21/55 CLEAR + WARM

Cox Shad
Nov 18
3/2/46

Titus St
Pringle to Keating

	2.12	143.41	141.29	
	6.56	139.29	10.73	132.68
0+35		6.2	133.0	128.6
+50		6.3	132.9	128.8
1+00		5.6	133.6	129.5
+50		4.1	135.1	130.2
2+00		2.9	134.3	130.0
+50		5.1	134.1	129.7
3+00		6.3	133.9	128.9
+97 ^c FN TEE		6.0	133.2	128.3
+97 ^b (5-)		5.8	133.4	133.2
+80		6.8	137.4	126.8
	11.10	143.78	6.56	132.68
	2.48	141.30	=	141.29

West
Williams &
Varonfakis &
Clear & Warm

37

3/29/55 Sunny & Warm

TP water Met East 6+86 sec Dago 17

Turn on end of east cb Titus & Keating
begin work

C4 4
C4 1
C4 1
C4 9
C4 3
C4 4
C4 0
C5 9
C4 2
C0 6

End of work

Cr. Fisher made
3/29/56

San Clemente

Tennyson to Voltoira

5tks for 6" AC

	166	128.30	126.69
0+20		2.2	126.1 122.6
+50		2.7	125.6 122.0
1+00		6.0	122.3 118.6
+50		9.1	119.2 114.0
	112	116.56	128.6 115.94
2+00		1.9	114.7 109.6
+97 ME		5.9	110.7 109.3
+50		5.9	110.7 105.2
3+00		10.0	106.6 100.9
	0.90	109.92	12.51 104.05
+50 TEE		1.95	103.5 96.5
+65 ME		0.5	99.5 98.9
4+00		6.1	98.9 92.0
+25		11.6	93.4 89.4
	0.77	93.15	12.57 92.38
4+00		2.8	90.7 86.8
+92 ME		6.7	86.5 87.8
5+00		7.6	85.6 77.0

West
Williams &
Varonfakis &

Clear + Warm

38

3/29/56

Burn 1059 + 91035 West of 89950
Copper disk

Pennyson

City engr copper disk 5' south prep line

C3

C3

C3

C5

C5

C1

C5

C5

C7

C6

C6

C4

C3

F1

C8

C4

93.4

26

90.8

Toys of old dual 4+17

85.6

-3.6

4+91 ± 82.0

93.15'

0.77 81.80 1212 81.03

5+00

1.9 79.9 76.4

C3 5

6+00

7.9 76.9 74.0
72.5C2 9 C4 4

7+00

8.3 73.5 68.8

C4 7

L70

10.2 71.6 68.4

C3 2

end of work

91.135

8.34 73.46 =

73.33 SW Top FH San Clemente + Volante

San Clemente Check depth of main under elekt conduit

0.56 99.16 88.9

Sta 4+00

3+90 6.96 92.5

Top of existing 6" Transite

4+10 9.80 89.7

" " " " "

4+18 11.25 88.2

" " " " "

4+20^E 11.5 88.0

" " " " "

4+30 11.8 87.7

" " " " "

4+40 11.85 87.6

" " " " "

4+50 13.02 86.5

" " " " "

9.08 90.38

= 90.4 4+50 Binney

at abs
Ductedge duct
at North

out sheet
made

Whittier 57
Catalina Blvd to 107' SLY

12.99	57.51	44.57
0+70		10.0 47.5 43.4
+75 FH Toc		9.9 47.6 43.6
+75 (6) FH		9.9 47.6 47.8
1+00		7.8 49.7 45.3
+39 ms		1.6 55.9 54.0
+50		2.2 55.3 50.5
11.01	67.26	126 56.25
+70 ms		9.3 58.0 56.3
+87 mn		9.5 57.8 56.8
+92 mn		9.5 57.8 56.9
2+00		9.4 57.9 53.0
+25		8.9 58.1 54.3
+34 ms		8.7 58.6 58.6
+50		8.7 58.6 54.5
+55 ms	^{2mots}	8.5 58.8 58.8
3+00		7.9 59.1 55.1
+25		7.0 60.3 55.5
+50		5.5 61.8 55.0

West
Williams &
Varonokist

Clear & Warm

40

3/28/55

C4	<u>1</u>	Top run sewer H 0+35 See FB 878
C4	<u>0</u>	Begin work
F0	<u>2</u>	
C4	<u>4</u>	
C1	<u>9</u>	
C4	<u>8</u>	
=	56.22	2' RT 1+10
		TBM Nail in Top stab pole
C1	<u>7</u>	
C1	<u>0</u>	
C0	<u>9</u>	
C4	<u>9</u>	
C4	<u>1</u>	
C0	<u>0</u>	
C4	<u>1</u>	
C0	<u>0</u>	
C4	<u>3</u>	
C4	<u>8</u>	
C6	<u>8</u>	

Whittier Cont

41

67.26

3+76 ms

4.5 62.8 58.5

C4 $\frac{3}{8}$

4+00

3.3 61.0 54.2

C9 $\frac{0}{8}$

4+16 ms

2.7 64.6 56.6

C8 $\frac{6}{0}$

4+50

3.1 63.9 52.3

C11 $\frac{6}{9}$

4+77

4.1 63.2 51.3

C11 $\frac{9}{0}$

3.44 63.82

3/28/55

end of work

15-873460

= 63.88 TBM Nail in Tel stub rock

Toronto St.

Check on Depth of Main

1.84 35.52 33.68

2.94 26.14 12.32 23.20

3.56 29.57 5.13 21.01

7.06 30.13 1.50 23.07

1.71 27.14 4.70 25.43

5.49 20.05 7.57 19.57

5.71 26.06 1.71 20.35

5.64 29.25 2.45 23.61

1.15 27.92 2.48 26.77

4.67 26.06 6.53 21.39

10.76 36.58 0.29 25.82

2.90 33.68 = 33.68

10.73 31.08 20.35

Top Cone Butter

2+73

Top Cb

2+73

Top of 6" Ci Pipe

2+15 1

Top Cb

2+15

9.92 40.69 0.31 30.77

Top Cb

1+15

Top of Pipe

1+15

West
Williams
Varonfakis

42

3/30/55

SW BM BP Castellair + Flawanda

Top Cb cretaceous + w. ordona

6' from FA Toronto
TBM Sta 2+79 ± yellow □ end of Cb

SW BM BP Castellair + Flawanda

TBM

Temeocula Cont

13

40.69

3.44 32.10 12.03 28.66

2+14 2

1.81 30.29

Cut Stake C 5' 3 30.3
5.3
25.0

2+14 2 Top Cb

7.22 29.88

11.76 20.34 = 20.30

end of Cb 3.00 23.30

20.30

2+80

3.71 19.64

on Cut Stake X 0 3 19.64
.7
20.39.

3.00 20.35

Rialto WPT Loma
Check depth of Pipe for Lowering

West
Williams &
Varon Sotis &

44

9/31/53

7.29	13.15	586
Top Ob		
4+32	2.42	10.73
4+32 Top pipe	5.10	7.75
4+55 Top Ob	4.42	8.73 5.2
4+55 Top Ob pipe	6.80	6.35
4+82	6.91	6.24 2.7
4+82	8.37	4.78
4+97	9.14	3.97
5+10	9.99	3.16
5+29	10.65	2.50
	8.54	4.61
7.29	5.86	= 586

Top stem AV no stem

4+86.31 end of Ob BC

8.7
3.5
6.2

C 3 2

C 3 5

Top of Ob at Fire Hydrant

Top of Cone Kick Block

Top of pipe

..

..

edge of Blacktop WPT Loma Blvd

Durant St
33rd to Wabash
Set Motors South Side

Set back of Meter 22.67 from 2.4

20590

2.05	24.71	22.66	
1+35	5.64	19.1	
1+35 NS	5.72	19.0	18.9
1+80	5.82	18.9	
1+80 (8) OVS	5.90	18.8	18.7
1+80	5.91	18.8	
	2.05	22.66	= 22.66

West
Williams
Varenfakis

45

7-7-55

0+00 EY Prop Line Gregory

BM SF EH 33rd + Steel St

Top of Ch N Side St

003

Top Ch N Side St

003

Top Ch N Side St

Alloy Blk 1 Wiltshire Pl

E of A3 N of El Cajon

Banks of Meters set 225 from \$ 110612

BN 1.72 365.28 363.56

P 2.86 355.41 12.73 352.55

0+26 E. 3.8 351.6 352.3 FO²

0+78 E. 4.2 351.2 351.3 FO¹

1+36 W 5.6 319.8 309.7 CO¹

1+49 E 6.0 319.4 349.2 CO²

1+59 E 6.4 349.0 348.9 CO¹

1+67 W 6.8 348.6 348.7 FO¹

2+40 W 6.8 348.6 328.1 CO⁵

2+48 E 6.6 348.8 348.3 CO⁵

2+81 W 6.7 348.7 328.0 CO²

3+06 E 6.5 348.9 328.1 CO⁵

3+21 W 7.1 348.3 328.8 FO⁵

3+51 E 6.10 355.96 5.55 349.86 349.9 CO²

3+76 W 5.5 349.5 350.5 CO²

3+78 E 5.1 350.9 350.7 CO²

3+92 E 4.9 351.1 351.3 FO²

CK 393 352.06 351.7 CO⁴ = CO⁴³

4+19 W 3.9 352.1 351.9 CO²

4+74 W 3.9 352.1 352.2 FO¹

West
Williams
Varenfisks
Kesthater

7-8-55

0+00 NY prop El Cajon

BT SWP Van Dyke + El Cajon 363.50

46

7-8-55

ALLEY
(Cont'd.)

355.96

4+96 E

37 352.3 352.6 FO3

5+09 W

3.9 352.1 352.3 FO2

5+30 E

3.9 352.1 352.2 FO1

5+35 E

3.7 352.3 352.1 CO2

5+75 W

3.6 352.6 350.6 CO1

5+80 W

3.22 352.70 350.6 C2.14 = C2.25

6+07 (5) GV.

6.03 349.93 349.0 CO9

OK TBM. 5.23 355.38 5.81 350.15 = 50.28

P 3.06 355.64 3.20 352.18

OK BM 3.32 352.32 = 352.60 BP NW. Cor ad & Heade

OK. in pole NW cor of Alley (Meade)

47

A1 + 4M 352.60 352.50

DELTA ST 41ST TO 300'
E. OF 42ND

Book of Meters Set 27' From A.S.T 28340

B.M.	811	71.43	63.29		
	1041	81.11	0.73	70.70	
0+00	M N Y		9.3	71.8	71.9
+05	(3) FH		9.8	71.3	72.1
+27	M N Y		1.6	79.5	72.7
+87	M S Y		11.2	69.9	71.3
+75	M N Y		9.6	71.5	71.4
+76	M S Y		11.1	70.0	70.6
+106	M N Y		9.9	71.2	71.2
+227	M S Y		10.5	70.6	70.1
+76	M S Y		9.8	71.3	69.7
+85	M N Y		9.5	71.6	70.6
+106	M S Y		10.9	70.2	69.5
+45	M N Y A.T.R.		10.2	70.9	70.0
+69	M M Y	75.55	10.28	70.83	69.8
+70	M S Y		8.2	67.4	69.9
+24	M S Y		7.1	68.5	68.5
+27	M N Y		3.6	72.0	69.3
+28	M N Y		3.6	72.0	68.9

WEST
WILLIAMS X
VARON FAKIST

48

7/15/55

N.W.B.P. 40TH + DELTA ST

0+00 S.E PROB. LINE 41ST

F0 $\frac{1}{8}$ 1103-05

F0 $\frac{8}{8}$ 2 F.H 28' + From S

C6 $\frac{1}{4}$ 4108

F1 $\frac{4}{1}$ 4111

C0 $\frac{1}{6}$ 4128

F0 $\frac{6}{0}$ 4129

C0 $\frac{0}{5}$ 4138

C0 $\frac{5}{6}$ 4127

C1 $\frac{6}{0}$ 4143

C1 $\frac{0}{7}$ 4144

C0 $\frac{1}{9}$ 4151

C0 $\frac{9}{0}$ 4152

C1 $\frac{0}{5}$ 4162

F2 $\frac{5}{5}$ 4159

C0 $\frac{0}{7}$ 4165

C2 $\frac{7}{1}$ 4168

C3 $\frac{1}{1}$ 4178

Delta Cont

49

	75.55				
5+26 M.SL.Y.	8.0	67.6	67.7	FO ^L	4185
5+33 MN.L.Y.	5.2	70.4	68.3	C2 ^I	4188
+79 M.SL.Y.	6.6	69.0	67.3	C1 ^I	4191
6+85 M.SL.Y.	4.1	71.5	66.4	C5 ^L	4205
7+33 M.SL.Y.	4.4	71.2	65.6	C5 ^G	4211
+87 M.SL.Y.	6.7	68.9	63.9	C5 ^O	4223
	559	69.96	= 69.94		

See Fig 2179 Page 67

West rim Sauer-MH 6730

75.55

5+9

69.96

Grand Ave Lee St
Check on Water Meter Vault

West
Williams
Varonakis
Alexander

50

7-26-55

7.68 12.97

7.85

city end PK nail to PP East side bridge

Top Ob NW opp West side box 6.97 6.00

Top Meter-Vault NW cor 5.97 6.50

" " SE " 6.12 6.35

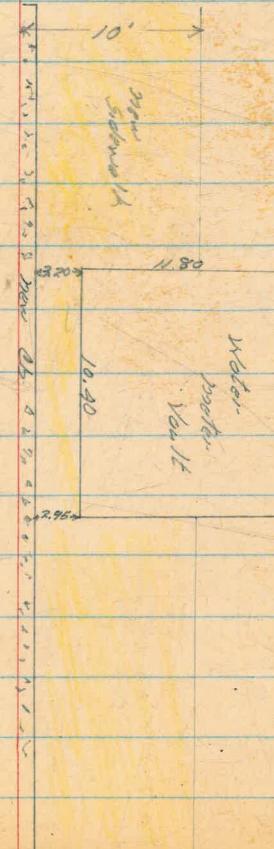
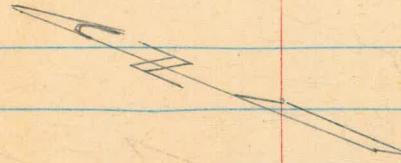
" " SW " 6.10 6.37

" " NE " 6.09 6.38

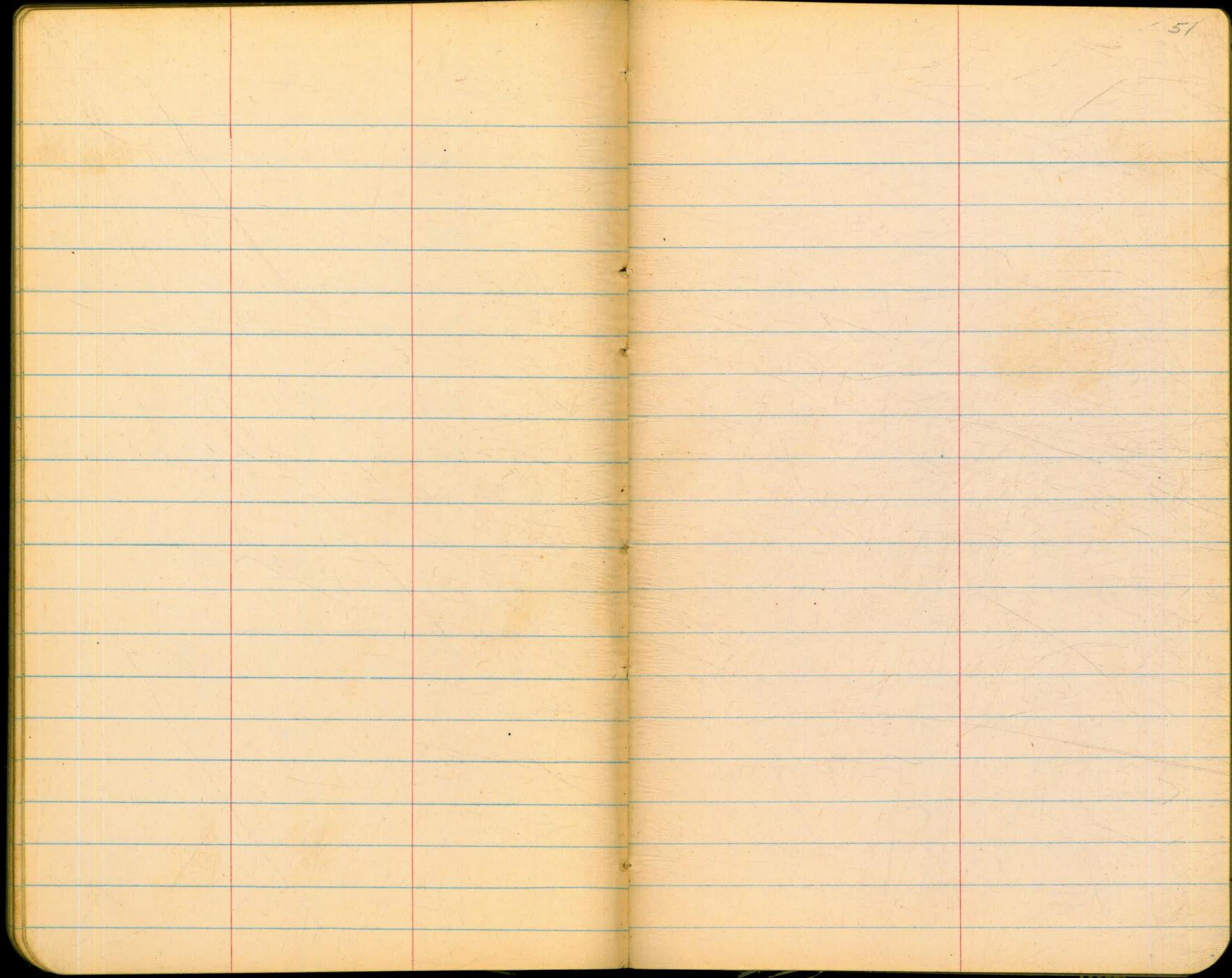
Top Ob opp E side box 6.16 6.01

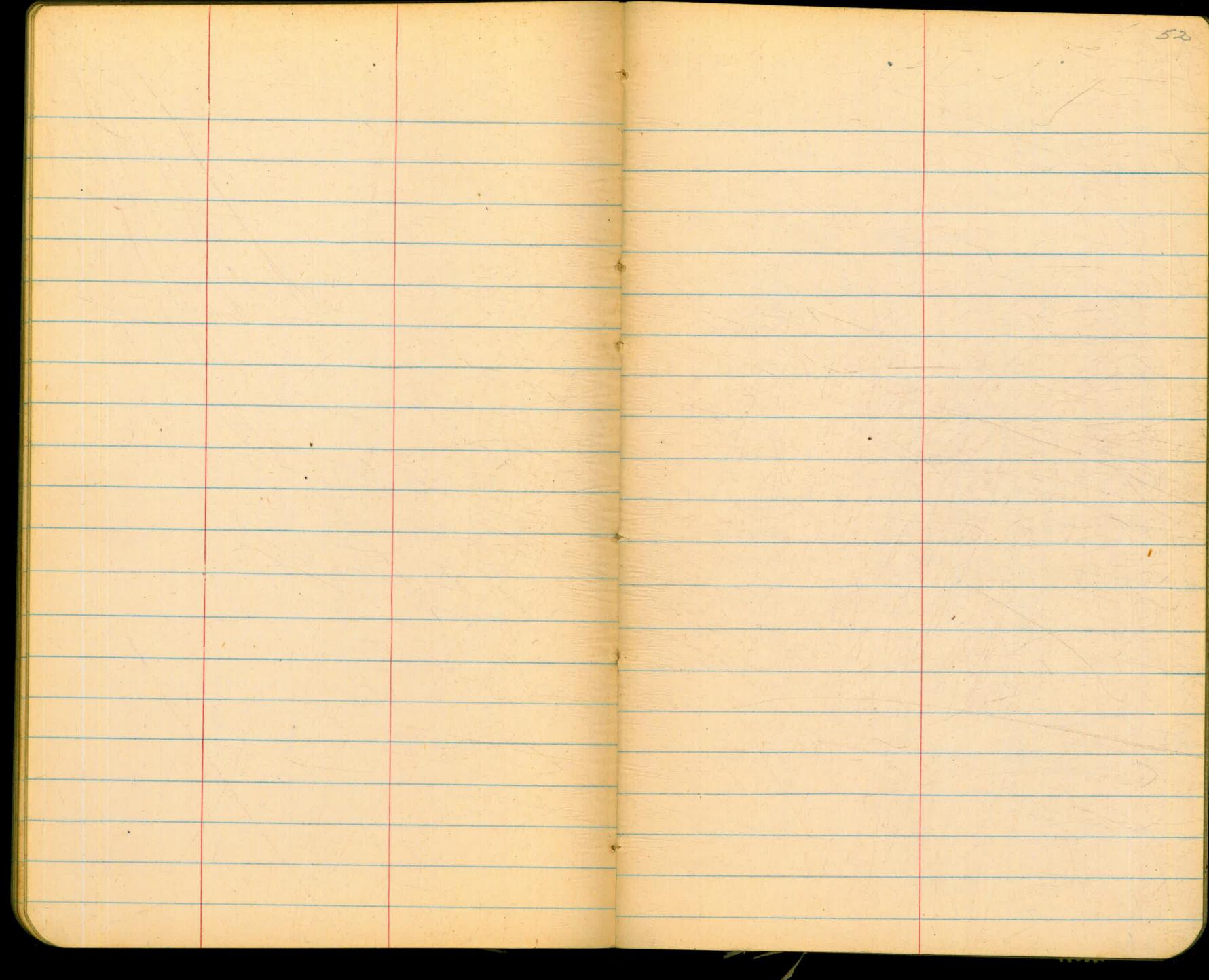
5.28 7.19 = 7.18

Xo end cl 1-cf



4"



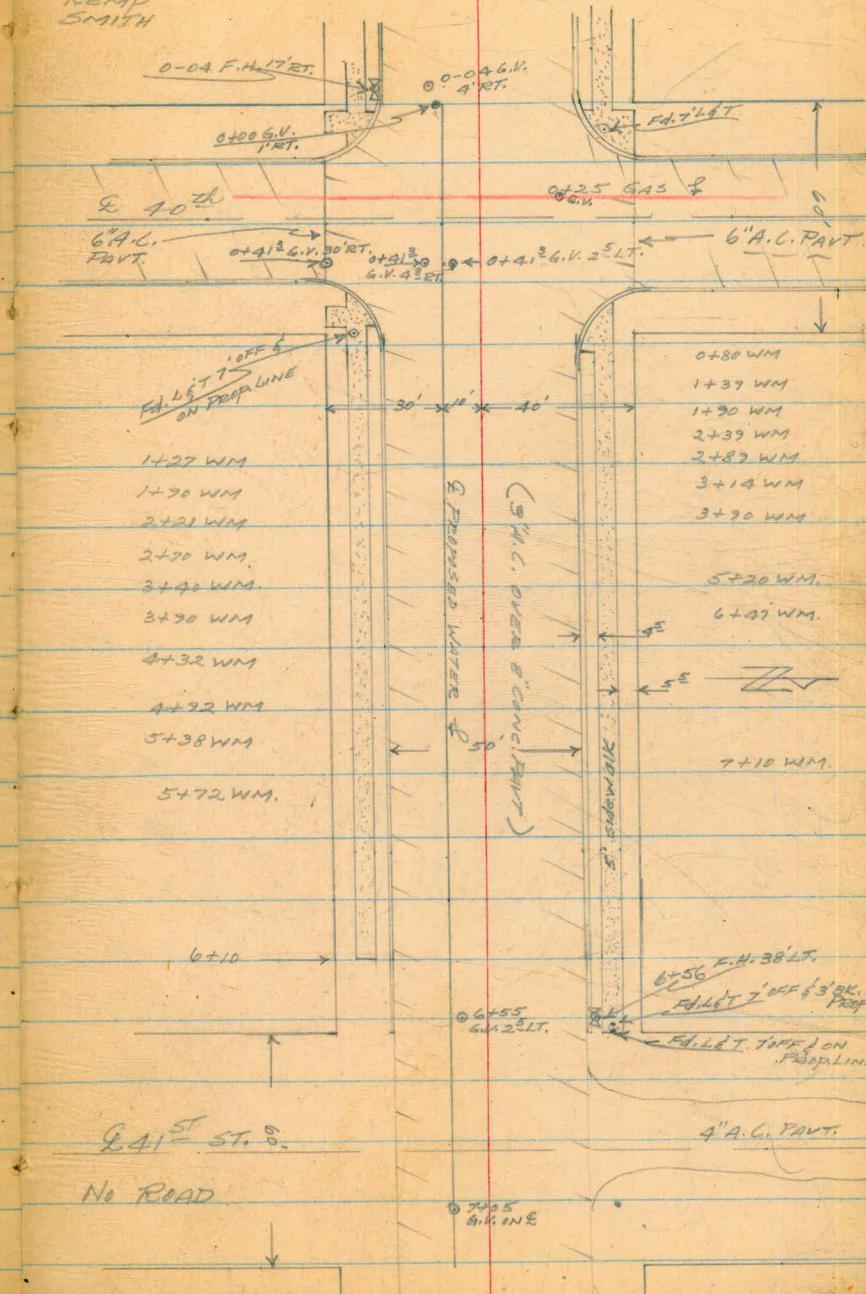


NATIONAL AVE.
40th TO 41st ST.
& PROFILE PROPOSED WATER MAIN
PRELIMINARY

0+00 = W/L 40th ST.

2/20/56
SHOREY
MARTELL
KEMP
SMITH

53



7+20 = E/L 41st ST.

NATIONAL AVE
(CONT'D)

54

BM 10.66 45.91 35.25

TP 11.31 56.92 0.30 45.61

D 10.71 67.45 0.18 56.74

SET TBM 1.00 66.51 1.94 65.51

NWBP 41ST NATIONAL

0+00 3.7 63.81

0+50 7.3 62.21

1+00 6.4 60.11

1+50 8.7 57.81

2+00 11.1 55.91

TP 1.78 55.44 12.85 53.66

2+50 2.5 52.94

3+00 4.7 50.94

3+50 7.0 48.44

4+00 9.3 46.14

4+50 11.6 43.84

TP 2.14 44.72 12.86 42.58

5+00 3.3 41.42

5+50 5.6 39.12

6+00 7.8 36.92

6+50 10.2 34.52

7+00 12.0 32.72

7+20 12.7 32.02

CK, B.M. 9.48 35.24 = 35.25

SWFH 40TH NATIONAL

ROANOKE ST.
F.H.'S RELOCATED & STAKED

P	1.02	201.82	200.80	
⑤ F.H.	SW Cor Hopkins & Roanoke	3.42	198.39	192.70
GV.		8.97	192.85	192.3
CK BM		1.02	200.80	
P	0.61	200.82	200.21	(10+25 C7E)
⑤ F.H.	SE Cor Desuville St & Roanoke	1.58	199.24	192.2
GV		10.35	190.47	192.2
BM	13.35	160.39	147.09	BP NE Cor Winchester & Rachael
	8.12	168.49	0.02	160.37
CK P		4.02	164.47	- 164.45
⑤ F.H.	SE Cor Rachael & Roanoke	8.10	160.39	160.7
GV.		7.71	160.78	160.0
P	2.72	219.57	216.85	
	6.2	213.37	210.9	C 2 ⁴⁷ to flange (F.H. 55 out from PL)

July 9 1956
Bessie
Smith.

55

Roanoke St
F.H. Contd.

TP

1.14 213.61

212.47

⑤ F.H. NE Cor Roanoke 4.26 209.35 209.2
B Morningside

CK P

CK 19+00.88

1.14 212.47

4.05 209.56 = 208.29

Top exist F.H. NE Cor Morningside & Roanoke
C O $\frac{5}{8}$ to flange $\frac{5}{8}$ out from P/L

C12

MORENA BLVD.
16" Horiz GV at STA 9+55.95
Morena @ LEHIGH ST.

8/6/56

BEATTY
SHOREY
Kemp
Smith.

57.

CE.
DISC
FB 2154
CITY Engr.

1.71 14.73 Tocojote Creek
End of stub (4)
WH, (4) GV Box
EL., (5)
4.0 10.7 6.9 C 4³
5.5 9.2 10.7 F 1.
7.3 7.4 10.7 F 3
4.71 10.03 - 10.02

Per
Harry Horn
City Engr.s

← 17.5 →
55 ← → 37.5

Shrub Hedge
EXIST CONC
CHAMBER
(BROKEN)
NOTE: F. Gentiliani
Wet Dist. 32x5
he needs 7'
from 6 pipe for
proposed chamber

CE
DISC
LEHIGH
← 17.5 →
55 ← → 37.5
EVAL (16" Horiz)
9+55.95

BLVD.

On New & KNOXVILLE

← 37.5 →
← 17.5 →

← 37.5 →
← 17.5 →

ALLEY BLKS 210-213

NORTH OF SUNSET CT., E. OF STRANDWAY

4.41 10.80

6.39

11-9-56

KEMP
SMITH
O'BRIEN

FAIR & WARM
58.

SPK. IN P.P. 0452 2nd RT ALLEY BLK 221

0+05 { BEGIN WORK
2" B.O. ASSEM.

4.5 6.3 2.6 C3 7

0+50

4.5 6.3 2.6 C3 7

0+75

4.4 6.4 2.5 C3 9

1+00

6.1 4.7 1.1 C3 6

1+50

8.3 2.5 -1.7 C4 2

1+87 IP 4.90 4.60

11.10 -0.30 -3.9 C3 6

2+00

4.6 0.0 -3.9 C3 9

2+24 6" TAP. CROSS

4.7 -0.1 -3.9 C3 9 + CUT TO EXIST. MAIN.

2+50

4.9 -0.3 -4.3 C4 0

3+00

4.2 0.4 -4.4 C4 8

3+50

5.0 -0.4 -4.5 C4 L

4+00

5.5 -0.9 -4.6 C3 7

4+25

5.8 -1.2 -4.7 C3 5

4+50

5.3 -0.7 -4.4 C3 3

4+82 { END WORK
2" B.O. ASSEM.

4.8 -0.2 -4.0 C3 8

CK. BM

4.34 0.26 = 0.28

NAIL IN P.P. 4+44 4' RT.

ALLEY BLKS 210 TO 213
(CONT.)

59

WATER METERS

10.80

0+095.	4.6	6.2	5.4	C08
00+135	4.8	6.0	5.4	C08
0+13N	4.9	5.9	5.4	C05
00+24N	5.1	5.7	5.4	C03
0+95N	5.3	5.5	4.2	C13
00+96S	5.8	5.0	4.0	C19
1+11N	6.6	4.2	3.0	C12
1+19S	6.8	4.0	2.6	C14
2+77N.	4.6	0.0	-1.6	C18
1 3+28N	4.6	0.0	-1.7	C17
3+31S.	4.6	0.0	-1.7	C12
1 3+56S	5.1	-0.5	-1.7	C12
3+68N	5.2	-0.6	-1.8	C12
2 3+89N	5.3	-0.7	-1.8	C12
4+07S.	5.5	-0.9	-1.9	C19
2 4+09S.	5.5	-0.9	-1.9	C19
4+43S.	5.5	-0.9	-1.9	C19
2 4+48S.	5.4	-0.8	-1.8	C19
4+76N.	4.8	-0.2	-1.4	C12
3 4+77S.	4.9	-0.3	-1.4	C12

3

4

4

4

6

ALLEY BLK. 148
NORTH OF MONTEREY CT., E. OF STROADWAY
@ STRK'S & GRD. 6" A.C. MAIN

11/13/56

SHOREY

KEMP

SMITH

60

TBM 2.67 8.09 5.42

0+05 6" TEE & PLUG 5.1

3.0 3⁰

1.8

C3 3⁺

CUT TO EXIST. MAIN

0+25 4.8

3.3 3³

1.2

C3 6

0+50 2.7

5.4 5⁴

-0.8

C3 5

0+88 0.5

7.6 7⁶

-3.7

C4 2

1+00 7.3 0.8

-3.6

C4 9

1+28 8" X 6" TAPP. CROSS 7.4 0.7

-3.9

C4 1⁺

CUT TO EXIST. MAIN

5' C.Y. TO CONN. TO
1+57 END WORK 2" C.I. MAIN 7.5 0.6

-3.2

C3 8⁺

OK. TBM 2.67 5.42 = 5.42

NOTE: METERS IN THIS
ALLEY ALREADY STRKD. FROM
IMPROVEMENT SHEET

ALLEY BLK'S. 208 & 209 MISSION BEACH
NORTH OF SEAGIRT CT., E. OF MISSION BLVD.
@ STR'S & GED. 6' A.C. MAIN

11/15/56
SAOREY
KEMP
SMITH

61

TBM 3.98 4.10 0.12

0+00 BEGIN WORK	3.9	0.2	-3.0
0+12	4.5	-0.4	-4.0
0+50 10"X6" CROSS	4.3	-0.2	-4.0
0+75	4.5	-0.4	-4.4
1+00	3.9	0.2	-4.5
1+50	4.6	-0.5	-4.6
2+00	4.8	-0.7	-4.7
2+50	5.2	-1.1	-4.9
2+75	5.1	-1.0	-5.0
3+00	5.0	-0.9	-4.9
3425 END WORK - 2" B.O.ASSY	4.9	-0.8	-4.8
CK.TBM	3.98	0.12	= 0.12

S. EDGE SEW. M.H. 0-01

C38⁺ CUT TO EXIST. MAIN

C36

C38⁺ CUT TO EXIST. MAIN

C4⁰

C4⁷

C5¹

C4⁰

C3²

C4⁰

C4⁰

C4⁰

C4⁰

WATER METER

4.10

0+825.	4.5	-0.4	-1.7
1+00N. 1+06N.	4.3	-0.2	-1.7
1+31N.	4.4	-0.3	-1.7
1+595.	4.6	-0.5	-1.8
1+66N.	4.6	-0.5	-1.9
1+665.	4.4	-0.3	-1.9
1+88N.	4.6	-0.5	-1.9
1+915.	4.5	-0.4	-2.0
2+17N.	4.8	-0.7	-2.0
2+335.	5.0	-0.9	-2.1
2+33N.	4.8	-0.7	-2.2
2+745.	5.0	-0.9	-2.2
2+75N	5.3	-1.2	-2.3
34245.	5.3	-1.2	-2.3
3427N.	5.1	-1.0	-2.2
	4.7	-0.6	-2.2

GUY ST.
PRINGLE TO LINWOOD
⑤ STK'S FOR LOWERING MAIN
0+95 TO 1455 (0+00 = SELBY LINE PRINGLE)

TBM 10.63 197.04 186.41

12/17/56
SHOREY
KEMP
SMITH

62

2" X 2" H418 MK'D P.O.T. 1464⁰⁰ E

0+95	4.4	192.6	185.4	C7 ²
1400	5.1	191.9	184.5	C7 ¹
1425 TP	0.02	183.69	183.67	C9 ¹
1455 TP	9.96	193.14	183.18	C7 ³
CK TBM		6.71	186.43	= 186.41

WATER METER'S
197.04

0+60 S.	2.5	194.5	194.0	C0 ⁵
1+26 N.	9.6	187.4	182.6	C4 ⁸
1+69 S.	10.5	173.2	169.4	C3 ⁸
2+20 S.	25.0	158.7	156.3	C2 ⁴

TROJAN AVE
VALLEY WAY TO SHARRON PLACE

B.M.	12.56	373.57		361.01
	10.47	383.54	0.50	373.07
	3.02	384.57	1.99	381.55
0+96 CONN TO EXIST. 8" P. 1400			378.8	+
	1.9	382.7	378.5	04 ² CUT TO EXIST. PIPE
1+25	2.3	382.3	377.2	05 ¹
1+50	0.9	383.7	376.6	07 ¹
2+00	3.4	381.2	375.4	05 ⁸
2+50			374.2	
2+53 64 8" X 6" TEE	4.9	379.7	374.8	04 ²
3+00			374.1	
3+08 - B.C.	4.1	380.5	374.0	06 ⁵
3+31 7 F.H. TEE ⑤	5.0	379.6	373.0	06 ⁶
	5.1	379.5		06 ⁵ C2 ⁵ FLANGE
3+50	5.3	379.3	372.0	07 ³
3+71 16 P.R.C.	5.4	379.2	371.5	07 ⁷
4+00	5.7	378.9	370.5	08 ¹
4+25	6.7	377.9	369.7	08 ²
4+46 23 E.C.	6.5	378.1	369.0	09 ¹
4+50			368.6	
5+00	7.8	376.8	366.8	010 ⁰
5+50 TP 0.38	374.87	10.08	374.49	365.0 09 ⁵

TROJAN AVE
(CONT'D)

64

374.87

6+00	2.9	372.0	363.4	C8 ^b
6+50	4.8	370.1	361.6	C8 ^c
6+88	5.3	369.6	360.2	C9 ^d
7+00	5.5	369.4	360.0	C9 ^d
7+50	7.3	367.6	359.0	C8 ^b
7+75	8.7	366.2	358.4	C7 ^e
8+02	3			
8+07 ^f	EXIST TEE			
TP	4.63	369.77	365.14	
OK. BM	8.80	360.97	-361.01	

56th ST.
MEADE TO TROJAN AVE.
⑥ STK'S & GRD. 6" A.C. MAIN

4/8/57
SHOREY
KEMP
SMITH

65

BM	0.38	428.15	437.77
TP	3.53	428.54	13.14 425.01

0+60 ODN. TO EXIST. 6" C.L.

	5.5	423.0	418.20
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NEBP EL CAJON 56th

NOTE: RESTAKED 3/12/57
IN RED

0+75		4.3	424.2	417.6
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1+25		4.8	423.7	417.0
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1+62 TP	0.07	421.64	6.97	421.57	415.6
RESTAKE TP	1.42	422.99	7.4	421.57	415.6
2+00			3.6	418.0	412.3

2+50		11.3	411.7	8.8	412.8
TP	0.18	409.87	13.30	409.69	407.9
3+00 TP	6.59	409.19	3.8	407.1	403.3

3+50		8.2	401.7	5.5	413.7
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4+00 TP	0.79	397.86	12.80	397.07	398.5
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4+25 TP	0.26	396.17	13.28	395.91	391.4
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4+50		5.4	392.5	2.3	393.9
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5+00		9.2	388.7	6.0	390.2
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5+50 TP 2.04	387.38	12.52	385.34	9.0	387.2
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6+00	TP 4.5	386.04	4.9	382.5	378.9
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6+50		11.88	384.3	11.88	384.29
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7+00 END WORK		3.16	380.3	3.16	381.2
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CK.		8.4	379.0	6.4	379.6
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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		7.7	379.7	7.7	379.7
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		6.3	379.7	7.7	379.7
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RADIO DRIVE 8" A.C. MAIN
SPRINGFIELD TO PARADISE
⑤ STR'S & GRD.
BM 112 466.29 465.17

CONN. TO EXIST. G.C.I.
0+72. 6" G.V. 2 1/2" X 6" RED. 8.6 457.7 449.8
0+75 8.9 457.4 449.4
1+00 10.2 456.1 447.8
+50 P 0.35 453.81 12.83 453.46 449.5
2~ 4.8 449.0 441.3
+50 8.9 444.9 438.0
3~ 13.8 440.0 434.7
P 0.13 440.81 13.13 440.68
+50 5.2 435.6 431.5
4~ 10.7 430.1 428.2
4+33 86 22 1/2° BEND A.P.T. 11.9 428.9 426.2
+50 P 0.10 427.89 13.6 427.2 425.3
5~ 3.0 424.9 422.3
+19 F.H.TEE 4.1 423.8 421.1
⑤ 6.3 421.6
+50 5.1 422.8 419.2
5+38 44 2 A.P.T. 22 1/2° BEND 7.9 420.0 416.2
6~ (OMIT) 416.0
+50 8.9 419.0 418.9

1/9/57
SHOREY
BEND
SMITH
CONC. MON. N.E. COR. 69th & MALLARD
C7² ± CNT TO EXIST. MAIN
C8⁰
C8³
C9²
C9³
C6⁹
C5³
C4^L
C1⁹
C2² C5⁶
C1⁸ C7⁸
C2⁶ C8²
C2² C8⁴
F1⁹ To PLANGE 60⁵ To BOTTOM
C3⁶ C8⁶
C3⁸ C6⁸
C5^L C9²

RESET @ RT. 1/18/57

RADIO ROAD

⑥ STKS
(CONT'D)

427.89

7+00		11.3	416.6	411.7
+50		14.0	413.9	409.5
P	0.49	415.06	13.32	414.57
8~		4.5	410.6	407.2
+50		5.9	409.2	405.0
9~		8.1	407.0	402.7
+50		11.8	403.3	400.5
11~	TP 1.58 403.65	13.6	401.5	398.1
11+49	24 APT. 11 $\frac{1}{4}$ ° BEND	12.99	402.07	
10+98	F.H. TEE	2.7	401.0	396.2
	⑤	0.3	403.4	394.2
11~		6.4	397.3	394.1
+50		9.3	394.4	392.1
12~		10.9	392.8	390.0
+50		9.6	394.1	388.6
13~	TP 2.70 393.07	11.6	392.1	387.2
13+49	46 APT. 11 $\frac{1}{4}$ ° BEND	13.28	390.37	
		5.2	387.9	385.8
14~		6.3	386.8	384.4
+50		8.3	384.8	381.6
15~		8.6	384.5	380.3
+50		10.6	382.5	378.8
15+52	44 APT. 11 $\frac{1}{4}$ ° BEND	11.0	382.1	378.7

1/9/58
SHOREY,
REMP,
SMITH

67

(D) RT.

c4 ²	c8 ²
c4 ²	c8 ²
c3 ⁴	c8 ⁶
c4 ²	c8 ⁸
c4 ³	c9 ³
c2 ⁸	c8 ⁴
c3 ⁴	c7 ⁵
c4 ⁸	c7 ⁹
c9 ²	c1 ³ TO BOT. F4 ¹ TO FLANGE
c3 ²	c9 ² 403.3
c2 ³	c9 ²
c2 ⁸	c9 ⁹
c5 ⁵	c10 ⁴
c4 ²	c10 ⁵
c2 ⁴	c7 ⁴
c2 ⁴	c9 ²
c3 ²	c11 ²
c4 ²	c10 ²
c3 ²	c6 ²
c3 ⁴	c5 ³

RADIO RAAD
② STK'S
(CONT'D)

393.07

16+00	12.6	380.5	377.9	C2 ⁶	
+50	13.9	379.2	377.0	C2 ³	
TP 2.83	382.56	13.34	379.73	C7 ³	
17~~	5.2	377.4	375.4	C2 ⁹	
+15 F.H.TEE	5.4	377.2	374.9	C2 ³	
②	6.3	376.3		F3 ³ TO FLANGE C1 ⁴ TO BOTTOM	
+50	4.9	377.7	373.7	C0 ⁶	
18~~	5.0	377.6	372.1	C4 ⁵	
+50	5.9	376.7	370.5	C6 ²	
18+52 ⁰⁷ APT. 1 1/4 ⁰ BEND ③ RT.	6.0	376.6	370.4	C6 ²	
19~~	6.8	375.8	368.9	C6 ²	
+25 ② RT.	7.0	375.6	368.0	C7 ⁶	
+50	7.2	375.4	367.3	C8 ¹	
20~~	8.1	374.5	365.8	C8 ²	
+50 TP 1.74	<u>375.25</u>	9.05	373.51	364.6	C8 ²
21~~	2.4	372.9	363.5	C9 ⁴	
+50	3.7	372.6	362.4	C10 ³	
22~~	3.1	372.2	360.9	C11 ³	
+50	4.0	371.3	359.5	C11 ⁸	
23~~	5.3	370.0	358.0	C12 ⁰	

1/9/57
SHOREY
KEMP
SMITH

⑩ RT.

68

C9³

C7³

C6²

C5⁶

C5³

RADIO ROAD
② STK'S
(CONT'D)

375.25

1/9/57
SHOREY
LEMP
SMITH

69

23+24 F.H. TEE

⑤

6.3 369.0 357.3

C11²

11.8 368.5

C1² TO FLANGE C6² TO BOTTOM

+50

7.4 367.9 356.6

C12³

24-

9.4 365.9 355.1

C10⁸

+50

11.5 363.8 353.6

C10²

25-

13.4 361.9 353.2

C9⁷

PP

0.42 362.97

12.70 362.55

C9⁵

+50

3.1 359.9 358.4

C9³

26-

5.0 358.0 349.3

C8⁷

+25

348.6

1. +50

7.3 355.7 348.5

C7²

END WORK-CONN TO

26+92± EXIST. 8" C.1.8" X 8" TEE

9.3 353.7 348.4

C5³ ±

CUT TO EXIST. MAIN

PP

2.11 352.31 12.77 350.20

OK. BM

5.95 346.36 = 346.32

Top F.H. ATTIX & Radio (F.B. 909-56)

WATER METERS
382.56

2 16+80 SLY

4.2 378.4 372.6

F1²

17+82 NLY

+0.8 383.4 376.5

C6⁹

3 21+49 SLY

9.1 366.2 366.4

F0³

ELEV. TOP OF MAIN &
 SERVICES
 ROSECROFT LANE
 (CATALINA TO SILVERGATE)
 0+00 = E/L CATALINA
 BM 3.77 310.27 306.50

1/16/57
 SHOREY
 KEMD
 SMITH

70

SPIKE E. CATALINA & ROSECROFT LANE

1+00 S.	6.7	303.6	302.4	C ₁ ²	W.M. SERVICE LATERAL "3749"
1+05 ⁵ Top Main	7.6	302.7	305.2	C ₂ ⁵	
1+12 N.	7.2	303.1	302.0	C ₁ ¹	" " "3744"
2+02 S.	7.2	303.1	303.1	C ₀ ⁰	" " "3739"
2+20 N.	6.4	303.9	302.9	C ₁ ⁰	" " "3734"
2+38 Top Main	7.2	303.1	306.3	C ₃ ²	
2+98 ⁵ Top Main	5.8	304.5	302.4	C ₂ ²	
3+49 Top Main	4.1	306.2	309.2	C ₃ ²	
3+49 S. TP 11.40 321.54	3.2	307.1	306.0	C ₁ ⁰	" " "3715"
3+69 N.	14.7	306.8	306.8	C ₀ ⁰	" " "3714"
4+75 S.	8.4	313.1	312.6	C ₀ ⁵	" " "3651"
5+28 Top Main	6.4	315.1	318.7	C ₃ ⁶	
5+45 S.	4.2	317.3	316.4	C ₀ ⁹	" " "3641"
5+88 N. TP 13.17 334.51	2.3	319.2	318.7	C ₀ ⁵	" " "3646"
6+87 Top Main	10.6	323.9	327.3	C ₃ ⁴	
7+18 S.	8.5	326.0	325.8	C ₀ ²	" " "3631"
8+08 Top Main TP 0.48 321.87	6.1	328.4	331.6	C ₃ ²	NOTE: GRD'S FOR LATERALS ARE CURB GRD'S MINUS 3.15
TP 0.63 310.73	13.12	321.39			
CK.BM	4.24	306.49	= 306.50		

WATER METERS
ROSECROFT LANE
CATALINA BLVD TO SILVERGATE
0400 = E/L CATALINA BLVD

1/22/57
SHOREY
KEMPF
SMITH

71

				SPIKE & CATALINA & ROSECROFT
BM	7.99	314.49	306.50	
0+17 F.H.		8.2	306.3	FOL
1+00 S.		8.7	305.8	C1 ²
				"3749"
1+12 N.		9.0	305.5	C1 ²
				"3744"
2+02 S.		8.0	306.5	C1 ²
				"3739"
2+20 N.		8.8	305.7	C0 ²
				"3734"
3+49 S.		5.2	309.3	C1 ⁰
				"3715"
3+69 N.		4.4	310.1	C1 ²
TP	13.07	327.20	309.1	"3714"
4+75 S.		0.36	314.13	
		11.7	315.5	C0 ²
				"3651"
5+45 S.		7.9	319.3	C0 ²
				"3641"
5+88 N.		5.7	321.5	C0 ²
				"3646"
7+18 S.		+ 1.6	328.8	C0 ²
				"3631"
TP	0.22	315.32	12.10	315.10
CK.B.M.		8.82	306.50	= 306.50

"L" ST.

32ND ST. TO 245 EAST

⑤ STK'S FOR 4'A.C. MAIN

BM 6.08 83.13 77.05

0+40 5.8 77.3 73.7

1/25/57

SHOREY

KEMP

SMITH

PAULSON

S.W.B.P. "L" ST. & 32ND

C₃⁶ + CUT TO EXIST. MAIN

0+45 4" 6.V. 5.9 77.2 73.7

C₃⁵

0+62 6.0 77.1 73.7

C₃⁴

1+00 5.5 77.6 73.8

C₃⁸

1+50 5.3 77.8 74.1

C₃⁷

2+00 5.0 78.1 74.3

C₃⁸

2+50 4.8 78.3 74.5

C₃⁸

2+62 4.8 78.3 74.6

C₃⁷

3+00 5.5 77.6 73.4

C₄³

3+11 ± 3" B.O. Assy. 5.9 77.2 73.1

C₄¹

CK. BM 6.08 77.05 = 77.05

72

WATER METERS
EMERALD ST.; OLNEY TO PENDLETON

1/31/57
SHOREY
KEMP
SMITH

73

S.W.B.P. DIAMOND & PENDLETON

BM	060 83.71	83.11	
	1.76 73.29	12.18 71.53	
0+14 F.H.	3.8 69.5	70.9	F1 4
0+15 S.	3.6 69.7	69.8	F0 1
0+59 S.	5.1 68.2	68.1	C0 1
0+88 S.	5.7 67.6	67.4	C0 2
1+19 S.	6.3 67.0	67.2	F0 2
1+73 S.	5.9 67.4	66.9	C0 5
2+04 S.	6.2 67.1	66.8	C0 3
2+11 N. F.H.	4.7 68.6	68.6	C0 2
2+55 S.	6.4 66.9	66.7	C0 2
2+96 S.	6.0 67.3	66.6	C0 7
3+40 S.	5.8 67.5	66.5	C1 0
3+79 S.	5.8 67.5	66.4	C1 1
T.P.	1130.84.22	0.37 72.92	S.W.B.P. DIAMOND & PENDLETON
CK BM	1.10 83.12	= 83.11	

COVINGTON ROAD

496' WLY. BOUNDARY ST. TO TERMINUS
 @ 5TK'S 4" A.C. MAIN

2/1/57
 SHOREY
 KEMP
 SMITH

74

B.M. 6.66 301.78 295.12

P 0.84 290.48 12.14 289.64

S.E.B.P. MAPLE & BOUNDARY

4+96 5.8 284.7 281.6 C₃¹ ± CUT TO EXIST. MAIN

5+00 5.9 284.6 281.3 C₃³

5+50 7.9 282.6 279.1 C₃⁵

6+00 10.3 280.2 276.8 C₃⁴

6+20 11 1/4° BEND 11.2 279.3 275.9 C₃⁴

6+69 13.3 277.2 273.5 C₃⁷

P 11.75 301.60 0.63 289.85

CK. B.M. 6.49 295.11 = 295.12

KEW TERRACE

NUTMEG TO TERMINUS

(5) STK'S 4" A.C. MAIN

BM 6.26 301.38 295.12

PP 0.46 297.43 4.41 296.97

PP 6.59 294.37 9.65 287.78

BEGIN WORK

0436 6"X4" REDUCER 8.6 285.8 282.4 C₃⁴ + CUT TO EXIST. MAIN0450 8.9 285.5 282.1 C₃⁴1+00 10.0 284.4 280.6 C₃⁸1+50 11.5 282.9 279.1 C₃⁸2+00 13.3 281.1 277.5 C₃⁶2+09 END. 4" CAP. 13.0 281.4 277.2 C₄²

PP 8.37 302.52 0.22 294.15

CK.B.M. 7.42 295.10 = 295.12

2/1/57
SHOREY
KEMP
SMITH

S.E.B.P. MAPLE & BOUNDARY

75

OLIPHANT ST.
WILLOW TO EVERGREEN
⑧ STK'S & GRD. 6" A.C. MAIN

BM.	0.28	153.09	152.81
0+45	8"X6" TAPP. SLEEVE	2.4	150.7 147.1
0+75		3.5	149.6 146.7
0+80	F.H. TEE	4.0	149.1 146.2
⑧		4.3	148.8
0+90	APT. 5° 42'38" RT.	5.1	148.0 144.9
1+00		6.2	146.9 143.6
1+40	25° APT. 5° 42'38" LT.	10.7	142.4 138.7
1+50	TP 0.16 140.01	11.8	141.3 137.4
1+75		0.9	139.1 134.3
2+00		1.5	138.5 130.0
2+25	TP 0.58 127.30	9.8	130.2 123.2
2+50	TP 0.22 114.54	5.7	121.6 116.2
3+00	TP 0.11 101.68	7.1	107.4 103.3
3+38	TP 0.28 89.04	5.1	96.6 91.2
3+88		6.0	83.0 76.4
4+16	CONN. TO EXIST. MAIN 9.6	79.4	76.6
CK.TBM		4.62	84.42 = 84.42

2/8/57
SHADY
KEMP
SMITH

N.W.B.P. OLIPHANT & WILLOW

C₃ ⁸ ± CUT TO EXIST. MAIN

C₂ ⁸

C₂ ⁹

C₂ ⁶ TO BOTTOM F1" TO FLANGE

C₃ ¹

C₃ ³

C₃ ⁷

C₃ ⁹

C₄ ⁸

C₉ ²

C₈ ⁵

C₇ ⁰

C₆ ²

C₅ ⁴

C₄ ⁷

C₅ ³

C₅ ¹

C₅ ⁴

C₄ ²

C₆ ⁶

C₂ ⁸ ±

4+16

EXIST.

7.3

79.5

76.6

C₂ ⁹ ±

2.34

84.47 = 84.42

76

WATER METERS

153.09

1425 SLY 8.7 184.4 143.3 C₁

1485 SLY 1.3 138.7 135.8 C₂

2+00 NLY 1.3 138.7 133.4 C₃

RESTARTED 3/25/57

⑧ 2+50

0.20 121.80 121.60
TP 0.15 107.88 12.07 107.73

3+00 4.3 105.6 102.2 C₃ ⁴

TP 0.04 97.10 12.82 97.06

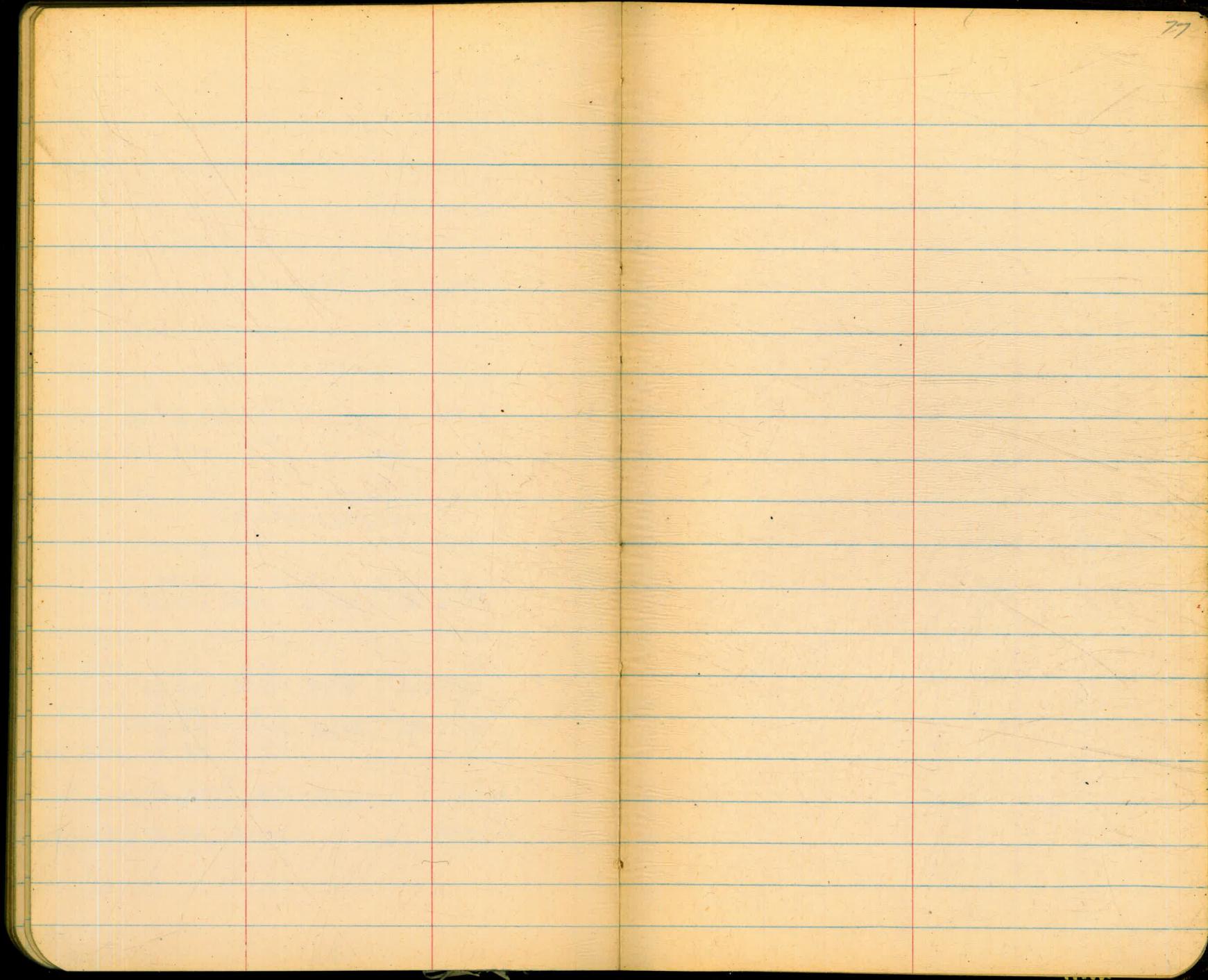
3+38 2.9 94.2 91.2 C₃ ⁰

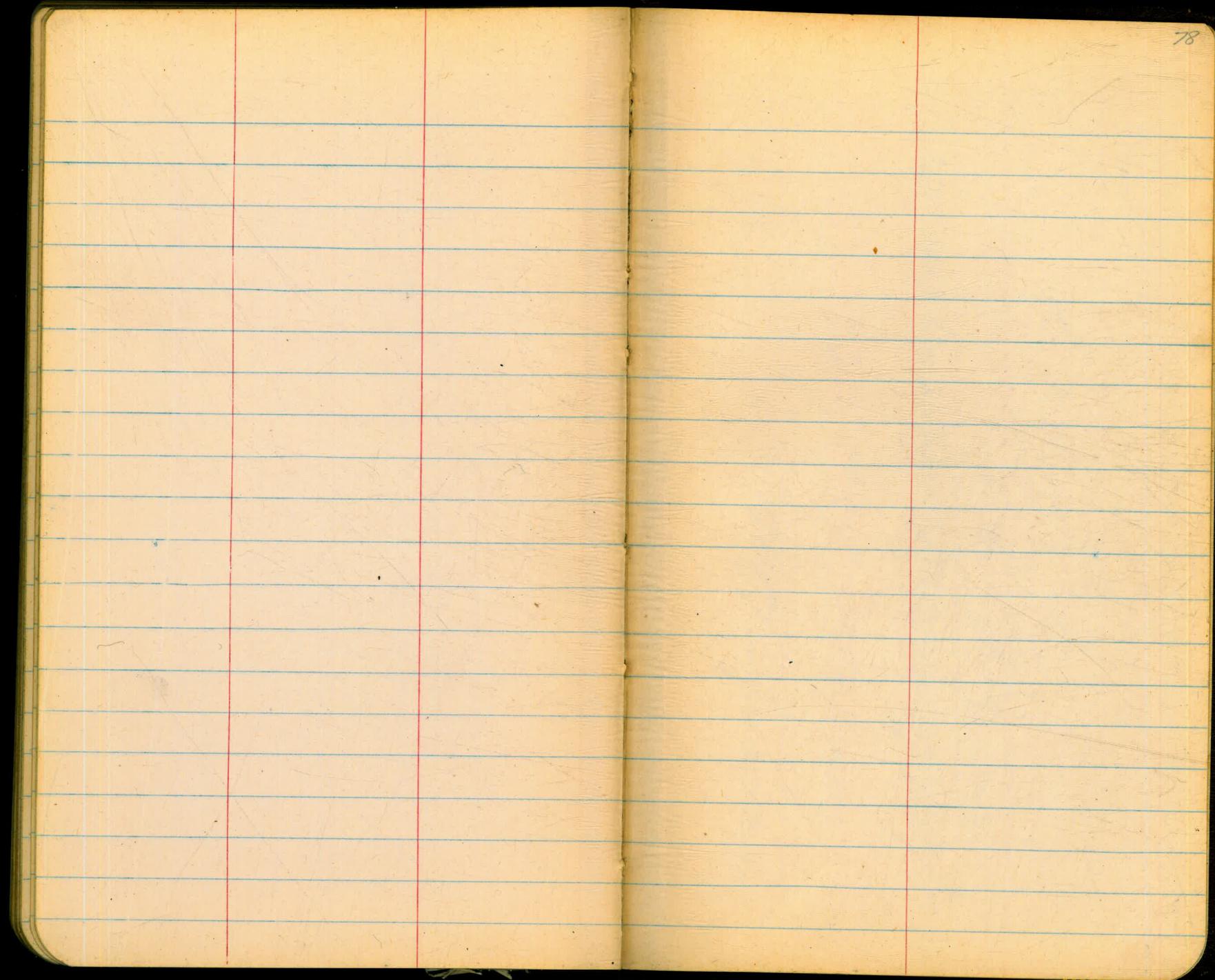
TP 2.76 86.81 13.05 84.05

3+88 7.9 78.9 76.4 C₂ ⁵

4+16 7.3 79.5 76.6 C₂ ⁹ ±

CK.TBM 2.34 84.47 = 84.42





~~Howard~~ - Bob:-

4/30/57

Could you boys stake
Kew Terrace & Corning ton st
on Grp. 27

RCP

0+05

0+50

+75

1+00

1+87

2+00

+24

+50

3+00

+50

4+00

+25

+50

+82

^w
¹¹

0+095

0+135

0+13N

0+24 N✓

0+95N✓

0+985✓

1+11 N✓

1+95✓

2+77N✓

3+28N✓

3+315✓

3+565✓

3+6881✓

3+89N✓

4+075✓

4+095✓

4+4733

4+485

4+76N

4+775

Howard Bob:-

4/30/57

Could you boys stake
Kew Terrace & Corrington St.
on Gr. 27

RCP

W
N

0+05
0+50
+75
1+00
1+87
2+00
+24
+50
3+00
+50
4+00
+25
+50
+82

0+095
0+135
0+13N
0+24N✓
0+95N✓
0+905✓
1+11N✓
1+195✓
2+77N✓
3+28N✓
3+315✓
3+565✓
3+688N✓
3+89N✓
4+075✓
4+095✓
4+433
4+48S
4+76N
4+77S

102
 30
30.60
 84.5
715.1

1033
21
 033
66
693 = 0.7

12345678910

11
10.8
.3

86.4
80.5
5.9

102
29
91.8
204
293.8
84.5
714.08

12.18
6.93
5.54

80.5
5.9
7.02
12.49 0.15
28
25
790
56
700

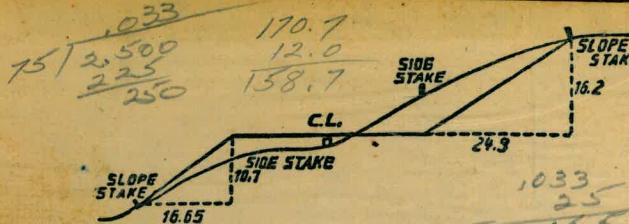
12.2
91.2
32.0

7.18
+ 5.28
12.46
5.24

281 7.22 = 713

113 32.000
32.0
940
924
160
 12.46
5.58
6.88 = 0.98
9.8

12.46
5.87
- 6.39 = 0.78
69



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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