

W907

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

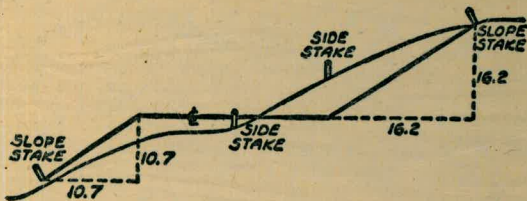
Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.41	1.51
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.054	.061	.068
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.887	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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 Alice ✓



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Delim Group 25

Knexville St Savannah to Morera 61-62 ✓
to Calle Del Cielo Stks for Meters

Calle Del Oro La Jolla Shores Dr 63 ✓
Stks for 6" AC Group 20

Ollie St Midway to Liberty 64 ✓
Stks for 6" AC Group 20

Liberty St Ollie St to Cumulas 65 ✓

~~VOID SEE PAGE 74~~

~~Linwood Pringle to Keating 67 ✓
STKS FOR 6" A.C. MAIN~~

WARDEN ST VOLTAIRE TO UDAL 68 ✓
Delim Group 26

32nd St Ast to 190' North 69-70 ✓

Delim Group 26
Dale St Redwood to 75' South 71-72 ✓
Hook Depth of Main

Quince St Vancouver to Haller 73 ✓
Stks for Meters

Linwood Pringle to Keating 74 ✓
Stks for Meters

Boundary St Laurel to Kalmia 75 ✓

Wet. SER.
Alley Blk 2, Nor El Cajon, E of Van Dyke 76-77
Alice

Worden St. Cont

86.75

Cen. mon. E side Wabaska Dr. W of Worden

2.56 89.31

6.82 82.49

T.B.M. ^S N.E. C. Udal & Worden

8.46 90.95

1.39 89.56

T.B.M. S.E. L.E.T. Vollaive & Worden

1.14 90.70

0+00	2.0	88.7
0+10	2.1	88.6
0+35	1.7	89.0
0+60	2.1	88.6
0+70	2.3	88.4
1+00	1.4	86.3
1+50	6.7	84.0
2+00	8.5	82.2
2+48	10.5	80.2
2+50	11.3	79.4
2+52	11.7	79.0

N.H. of Vollaive

N. curb

S. curb

S. curb

To edge 7" A.S. paving

Wordsen Cont.

90.70

3100	12.8	77.9	
3102.50	12.80	77.9	edge con. gutter
3106	13.09	77.6	" " "
3106	12.46	78.2	Top curb
3110	13.0	77.7	
3112	12.1	78.6	
3116	12.0	78.7	
3118	11.4	79.3	Top Slope
3132	18.2	72.5	
3136	18.8	71.9	Top Slope
3140	18.1	72.6	

7.56 83.14

6.20 89.34

2.57 86.77 = 86.75

Tourmaline Cont

		110.10	
0.95	111.05		
		10.90	100.15
0.86	101.01		
		9.26	91.75
2.02	93.77		
		2.20	91.57
0.26	91.93		
0+00		4.5	87.4
0+10		4.4	87.5
0+10		4.2	87.7
0+40		4.1	87.8
0+50		4.1	87.8
0+70		4.8	87.1
0+80		4.6	87.3
1+00		4.8	87.1
1+50		5.2	86.6

BP. SF. Tourmaline & Cass

TBM. N.E.H. Tourmaline & Mission

E/L

Storm Drain 6.5 to flow

f

w gutter

W/L

Tourmaline Cent

91.93

2+00	6.0	85.9
2+50	7.1	84.8
3+00	8.4	83.5
4+50	9.8	82.1
4+00	10.9	81.0
4+10	11.0	80.9
4+25	13.9	78.0
4+32.41	12.6	79.3
T.D.	9.33	82.60

TBM COO. Mon. 45 PL

Went
Kemp
Alexander

7

3-3-55

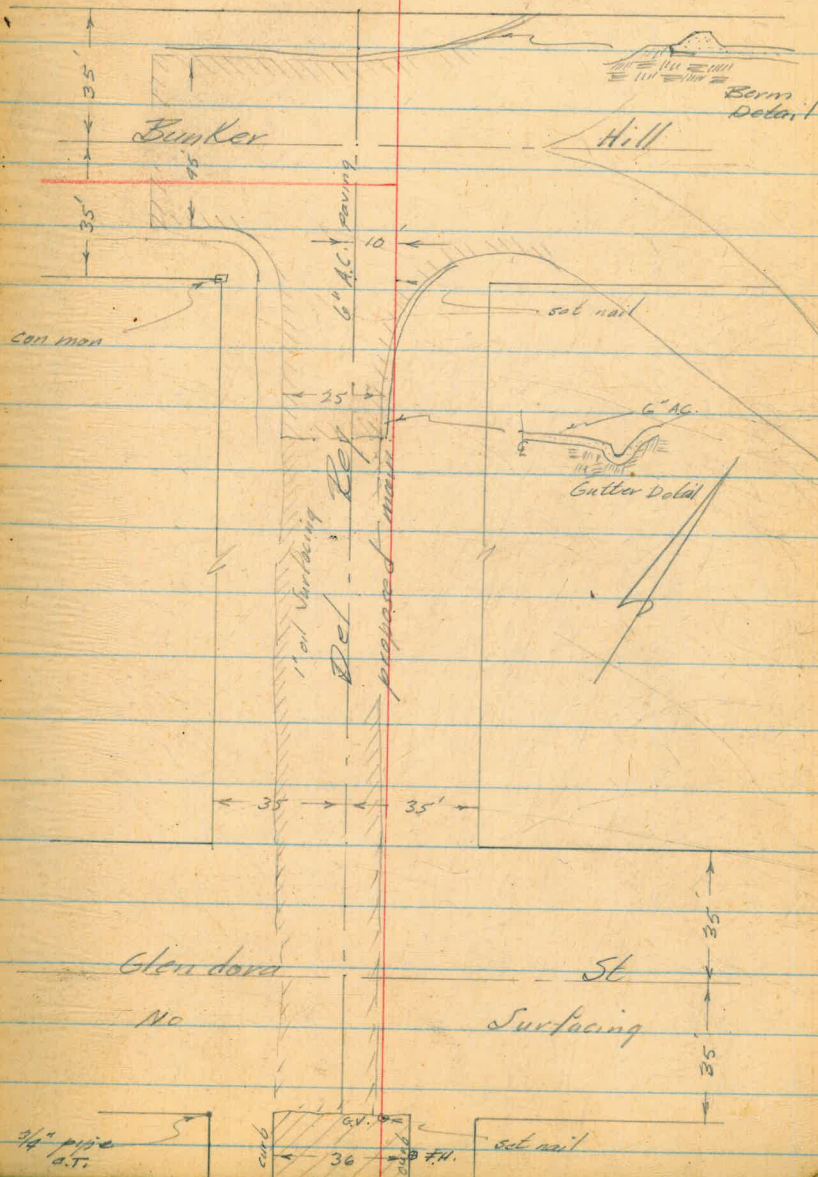
Profile of Proposed Water Line
Del Rey St., Bunker Hill to Glendora

0+00 N/H of Bunker Hill

0+70 S/H of Bunker Hill

5+70 N/H of Glendora

6+90 S/H of Glendora



Del Ray Cont.

33.48

SW. con. mon. Del Ray & Bunker Hill

2.46 35.94

0+00	1.2	31.74
+05	2.5	33.44
+13.5	2.1	33.84
+14	1.7	34.24
+15	2.1	33.84
+33	1.6	34.34
+45	1.6	34.34
+50	1.8	34.14
1+00	3.4	32.54
1+06	3.8	32.14
1+10	3.3	32.64
+50	3.9	32.04
2+00	5.3	30.64
+50	6.9	29.04
3+00	7.6	28.34

Reduced By Palomina 3-4-5

1/4 of Bunker Hill

Top AC. burm

crowm of 6" AC. road

Pl. proposed water lines

AC. gutter

Top AC. burm

Del Ray Cont.

35.94

3150 8.7 27.24

T.P. 6.39 29.55

0.55 30.10

4100 3.0 27.10

+50 3.6 26.50

5100 4.3 25.80

+50 4.9 25.20

6100 5.5 24.60

+40 6.7 23.40

7.47 22.63

Reduced by Delors. 1920
3-4-55

SE of Glendora, Cal., & Begin of 4" AC. pave.
3/4" prep con SW. cor. Del Ray & Glendora St.

Profile of Proposed Water Line
 Bunker Hill, Revere to Del Rey

3185

E/W of Del Rey

0170

E/W of Revere

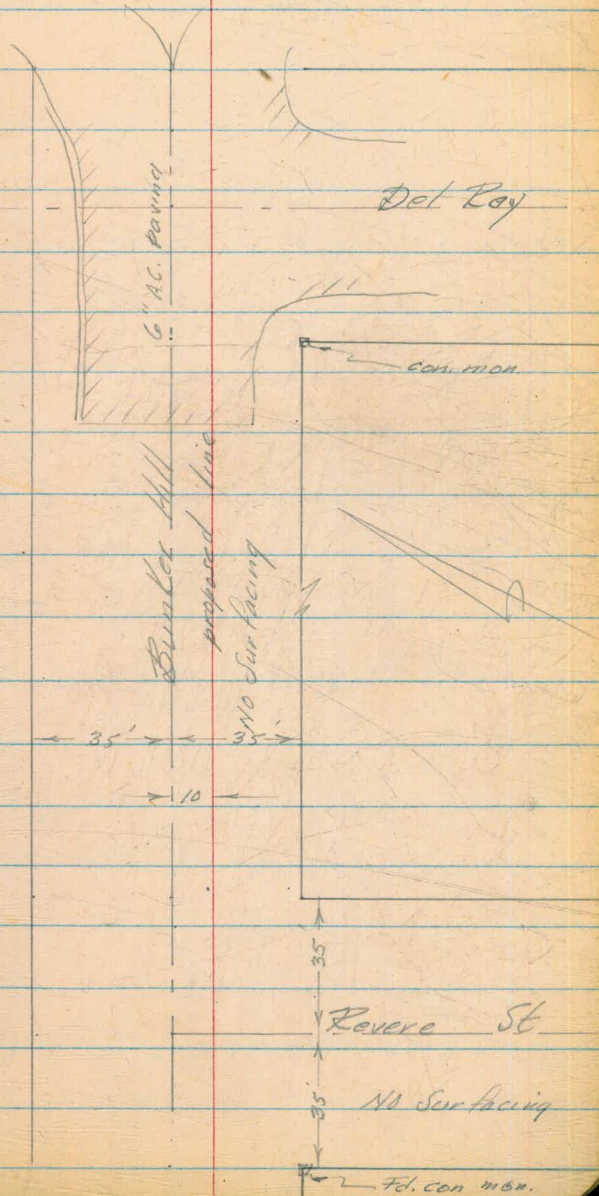
0100

W/W of Revere St

Wert
 Kemp
 Alexander

10

3-3-55



Bunker Hill Cont.

1634

SW. con mon. Revere & Bunker Hill

10.26 26.60

0100	9.7	16.9
45	8.5	18.1
50	8.4	18.2
1100	7.2	19.4
50	5.5	21.1
2100	3.3	23.3
T.P.	1.78	24.82

Reduced by J. Gray
3-4-55

W/H of Revere St.
Pl. of proposed water lines

11.01 35.83

2150	10.3	25.53
3100	7.0	28.83
20	5.3	30.53
50	3.3	32.53
85	1.5	34.33
4+10	0.2	35.63
	2.35	33.48

Begin 6" AC paving

Pl. of proposed water lines

E/H of Del Ray

SW. con mon Bunker Hill & Del Ray

Wert
Kemp
Alexander

3-3-55

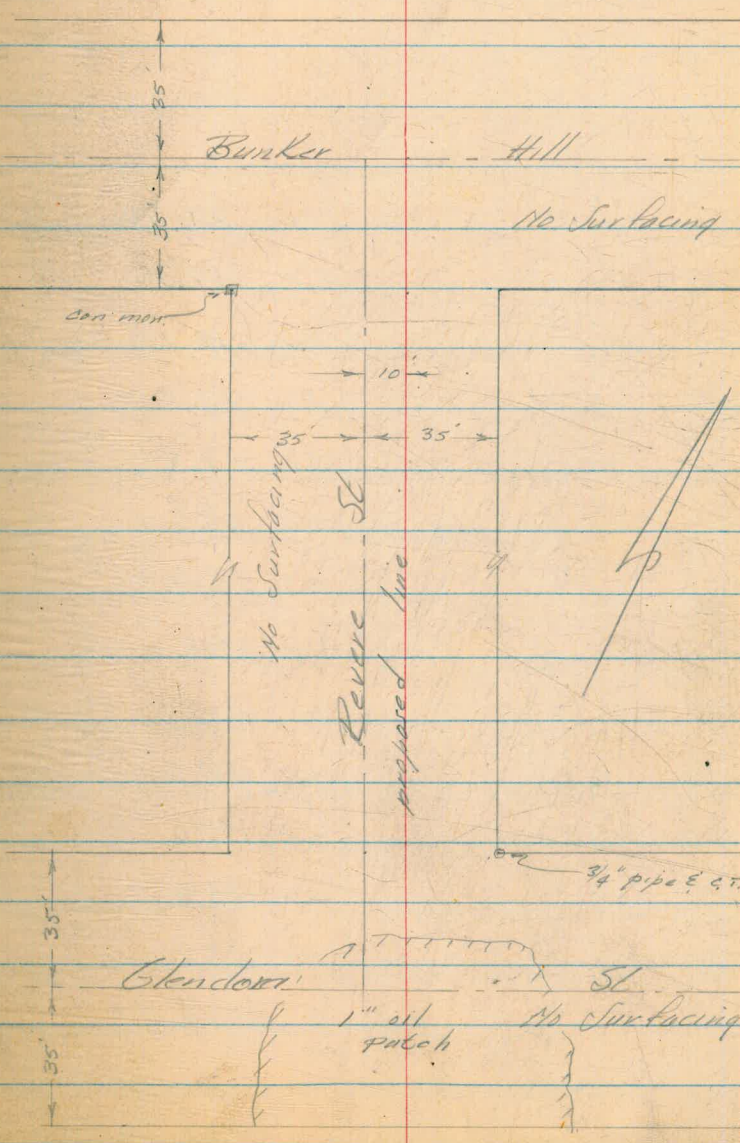
Profile & Proposed Water Line
Revere St, Bunker Hill to Glendora

0+00 N/H of Bunker Hill

0+70 S/H of Bunker Hill

5+70 N/H of Glendora

6+40 S/H of Glendora



Reverse Cont

16.34

396 20.30

0+00	+4.0	24.30
+09	7.0	19.30
+16	2.6	17.70
+25	2.1	18.20
+50	2.4	17.90
1+00	3.1	17.20
+50	2.9	17.40
2+00	1.5	18.80
2+50	3.6	16.70
+75	4.4	15.90
3+00	4.4	15.90
+50	4.5	15.80
4+00	4.6	15.70
+50	5.0	15.30

Reduced By Palomares

N/4 Bunker Hill & Top haul

bottom ditch

Revere Cont

20.30

5+00	5.2	15.10
+50	6.0	14.30
5+92	7.2	13.10
6+00	7.2	13.10
+25	7.3	13.00
6+40	7.1	13.20
5+99	7.1	14.81

Begin 1" AC paving

N.E. $3\frac{1}{2}$ " pipe & CT. Glendora & Revere

Proposed Water Line on Dalbergia St
 Yama St. to Osborne

0+00

Wk of Yama

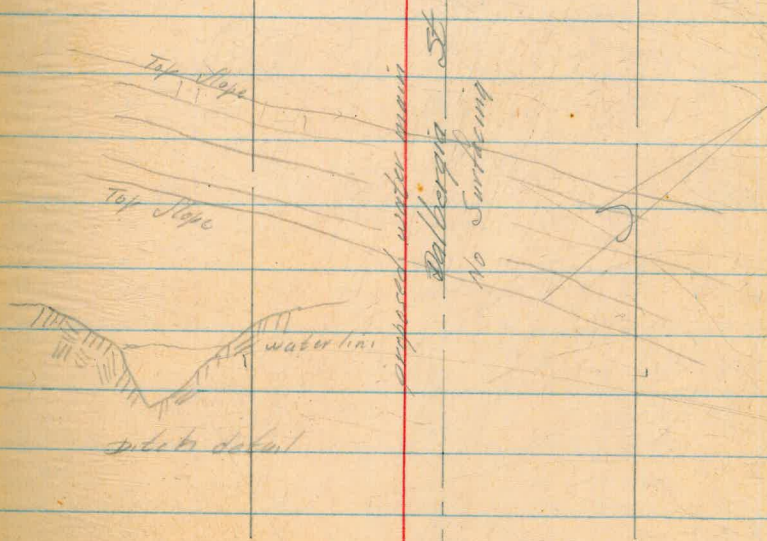
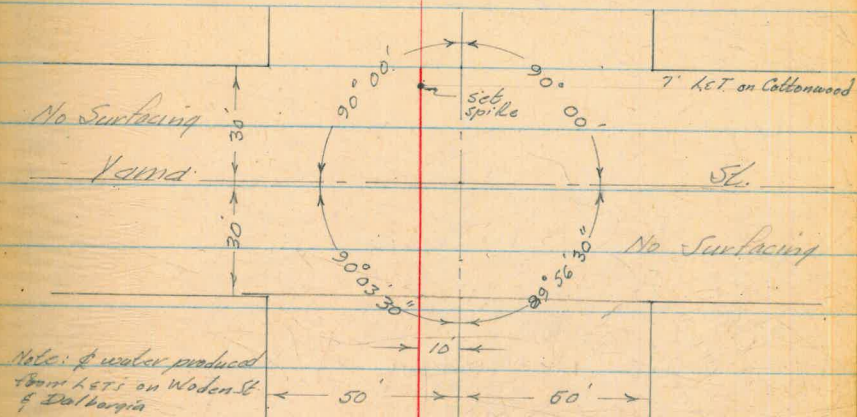
0+60

Wk of Yama

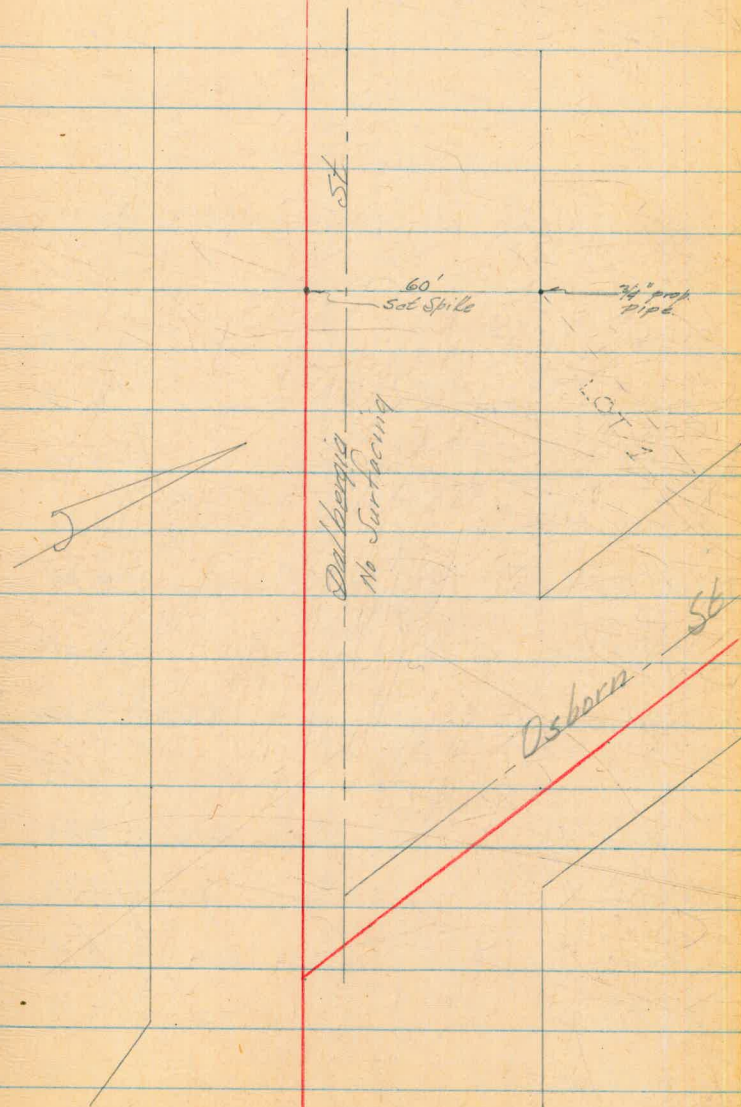
Wert
 Kemp
 Holdhan,
 Alexander

15

3-11-55



Dalbergia Cont



Dalbergia Cent

11.10

SE FH. Yama & Cottonwood

156 12.66

2.84 2.82

SE FH. Yama & Dalbergia

216 11.98

0+00	4.3	7.68
+43	5.8	6.18
+50	4.7	7.28
1+00	3.7	8.28
+30	3.6	8.38
+40	5.2	6.78
+44	2.2	4.78
+50	2.0	4.78
+56	2.3	4.68
+61	1.8	7.18
+69	3.6	8.38
2+00	1.8	7.18
+50	4.8	7.18

*Top ditch**Bottom " west side**" "**" " East side**Top " East side*

Dalbergia Cont.

11.98

3+00	5.2	6.78
+40	1.5	10.48
T.P.	0.04	11.94

13.21 25.15

3+50	11.0	14.15
+70	2.5	17.65
4+00	6.1	19.05
+50	4.3	20.85
T.P.	1.96	23.69

7.09 30.78

5+00	7.0	23.78
+50	6.3	24.48
5+93.17	5.9	24.88
6+00	5.8	24.98
* +50	5.5	25.23
T.P.	1.70	29.08

4.49 33.57

9.84 23.73

Pl. proposed water lines, Osborn & Dalbergia

NEFH. Osborn & Division

SEFH. 23.71 Marine View & Osborn

Dallergia Cont

~~30.78~~

6 + 88.92

.55 24.68

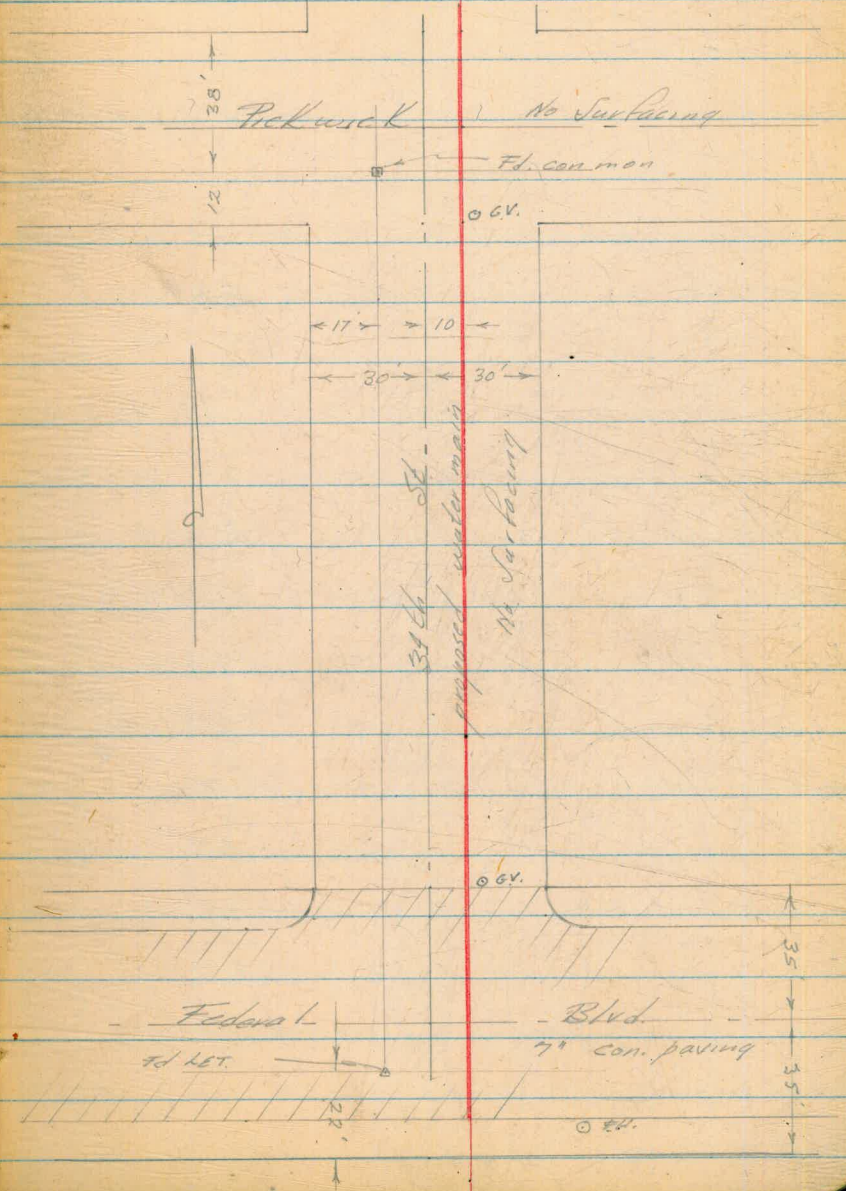
7 + 00

- .65 24.58

7 + 14

- .65 24.58

Profile & Proposed Water Main
 35th St. Federal Blvd to Pickwick



35th St. Cont

51.87

4.64 56.51

0+00	4.7	51.81
+04	4.56	51.95
+09		
+10	5.5	51.01
+25		
+35	4.7	51.81
+43.5	4.72	51.79
+50	4.9	51.61
+60	5.2	51.31
+70	4.7	51.81
1+00	4.3	52.21
+50	4.5	52.01
2+00	4.1	52.41
+50	3.8	52.71
2+89		
3+00	3.6	52.91

Reduced By Palomares 5-18-55

NWBR Federal # 35th

S/H of Federal

Sewer M.H. 8.5 ft. cut 12.0 to flow line
30' RL, F.H.

So. gutter of Federal

Water G.V. 44' RL

of Federal

10' LL G&E M.H. (not opened)

No gutter

Edge con. paving & Water G.V. 1.5 RL

Water G.V. 1' RL

35th St Cont

56.51

3420

3.5 53.01

4.12 52.09

4.41 56.50

4.64 51.86

N/H of Pickwick

Profile of Proposed Water Line
 "G" St. 26th St. to 27th St.

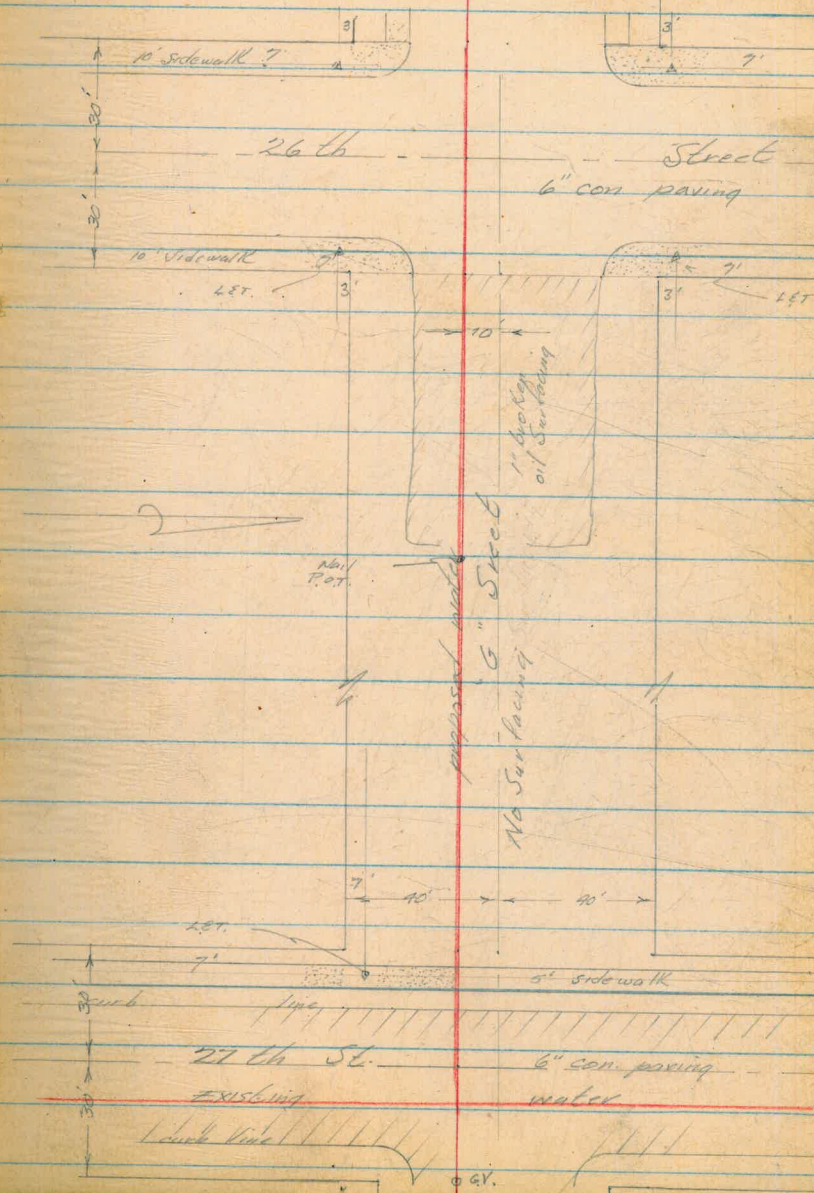
2100

End oil surfacing

Werb
 Kemp
 Holston

23

4-11-55



© A.V.

"G" St. Cont. Reduced Bk
5-2-55

171.99

SURF. 26th & "G" St

12.46 189.45 ✓

0+00	12.5	177.0	W of 26th St
0+10	12.2	172.3	W curb line
0+18	11.1	173.4	Gas crossing
0+30	9.9	174.6	E of 26th
0+40			Water gates 4' H & 4' Rl
0+42			Water gate 38' Rl
0+50	9.0	175.5	E curb line
0+51.5	8.5		E.H. 38' Rl
0+60	8.5	176.0	E/H of 26th, end on 4" compaving
1+00	5.2	179.3	
1+50	3.0	181.5	
2+00	3.1	181.4	end of 1" oil Surfacing
2+17			Street barricade
2+17	3.0	181.5	Top Slope
TP	8.13	176.32	

0.39 176.71 ✓

176.71

T.P.

12.40 164.31 ✓

79

0.48 164.76

3+90

5.7 159.1

3+00

7.6 157.2

3+07

8.3 156.5

3+16

10.7 154.1

T.P.

12.75 152.04 ✓

0.50 152.54 ✓

3+36

1.5 151.0

3+50

4.2 148.3

3+75

9.2 143.3

T.P.

13.24 139.30 ✓

0.34 139.64 ✓

4+00

0.5 139.1

4+07

1.4 138.2

4+15

3.3 136.3

139.64

4+50 7.8 131.8

4+56 9.0 130.6

T.P. 12.63 127.01 ✓

3.82 130.83 ✓

5+00 10.7 120.1

5+12 11.4 119.4

5+17 12.2 118.6

5+28 12.1 118.7

5+43 10.5 120.3

5+50 8.6 122.2

5+90 1.3 129.5

T.P. 0.78 130.55 ✓

12.54 143.07 ✓

6+00 10.3 132.8

T.P. 0.48 142.59 ✓

12.96 155.55 ✓

6+22 12.0 143.6

	155.55			
6+34		7.9	147.7	
+50		4.2	151.4	
+61		0.9	154.7	
* +65.7		1.1	154.5	edge of sidewalk
* +70.7		1.1	154.5	" " "
* +75.2		1.1	154.5	top curb
+75		1.8	153.8	gutter
T.P.		131	154.24 ✓	
	5.46	159.70 ✓		
6+91		5.2	154.5	sewer crossing
+91		5.03	154.67	" M.H. 10' H 3.8 to flow 150.9 FL.
7+02		5.0		Water gate 21' H
7+07		5.0	154.7	E curb line
7+08.5				TL 21' RB
* 7+19.7				G.N. on line
* 7+20.7		4.7	155.0	TL of walk
		4.71	154.99 ✓	B.M. SE 1st 10'

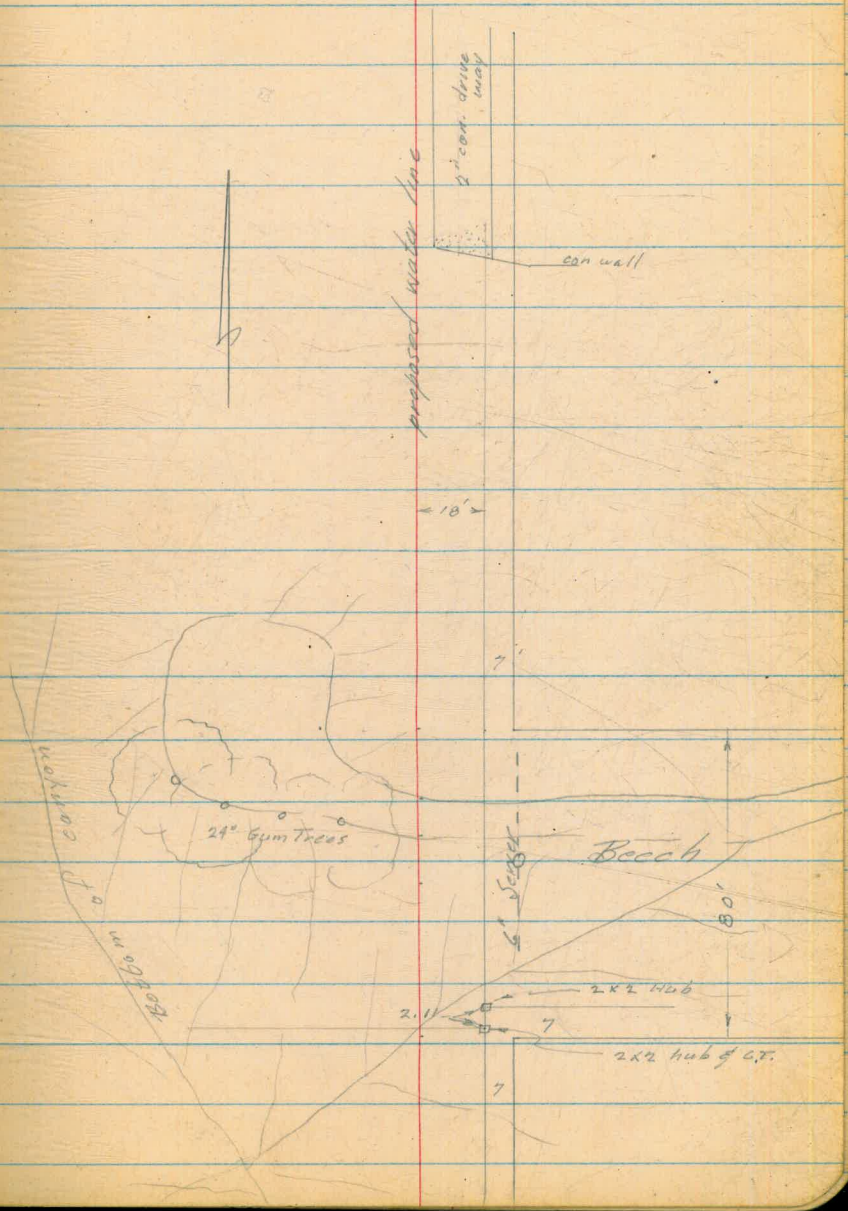
* = change in station

0+80

N 1/4 of Beech

0+00

S 1/4 of Beech St



32nd St cont.

178.61

RM. S/H in p.p., N/H of Beech, 40 ft waterline.

0.18 178.79

12.49 166.30

3.75 170.05

0+00

11.6

158.45

S/H of Beech St.

+15

4.4

165.65

T.P.

0.31

169.74

11.22 180.96

0+46

7.0

173.96

0+50

5.7

175.26

0+52

0.68

180.28

Sewer M.H. 25' Rt

cut 37 to flow

B+55

3.1

177.86

So. edge roadway

T.P.

2.36

178.6

12.24 190.84

0+66

12.9

177.94

No. edge roadway

+85

6.8

184.04

1+00

2.9

187.94

T.P.

0.61

190.23

12.34 202.57

202.57

1+32 6.0 196.57

+40 4.9 197.67

+50 1.5 201.07

T.P. 0.09 202.48

12.22 214.70

1+65 10.7 204.0

1+75 6.9 207.8

1+80 12" pepper tree 8' Rt

1+83 2.2 212.5

1+88 2.0 212.7

T.P. 0.56 214.14

12.96 227.10

1+91 5" pepper tree 5' Rt

1+98 10.8 216.3

2+03 5" pepper tree on line

2+14 2" " " " "

2+25 12" pepper tree 2' Rt

2+37 6" " " " "

227.10

2+50

8" pepper tree 4' H.

2+50

7.2

219.9

" " " "

2+60

3' " " " "

2+77

12" " " " "

2+85

22" pepper 6' H.

2+88

6" cactus on line

2+98

3" pepper tree 6' H.

3+00

2.4

224.7

6" " " 8' H.

3+06

cactus on line, (spinless type)

3+07

6" pepper tree 8' H.

3+15

15" " " 9' H.

3+15

cactus on line (century type)

T.P.

0.55 226.55

7.46 234.01

3+33

6" pepper tree 9' H.

3+39

9" " " 7' H.

3+46

6" " " 7' H.

3+50

5.1

228.91

234.01

3+52

6" pepper tree 7' 16

3+58

15" " " 9' 16

3+64

15" " " 14' 16

3+70

36" palm 17' 16

3+86.5

4.4

229.61

back sidewalk

3+92

4.4

229.61

Top curb

3+92

5.1

228.91

Gutter

4+00

4.6

229.41

4+37

3.4

230.61

curb to Lt. on Cedar

4+46

3.1

230.91

curb to Rt. on Cedar

4+57

water G.V. 4' 16

4+59.92

2.1

231.91

N/H of Cedar to Rt.

T.P.

2.56 231.45 = 231.47

NEBP, 32nd & Cedar

Wert
Kamp.
Hohlon

4-14-55

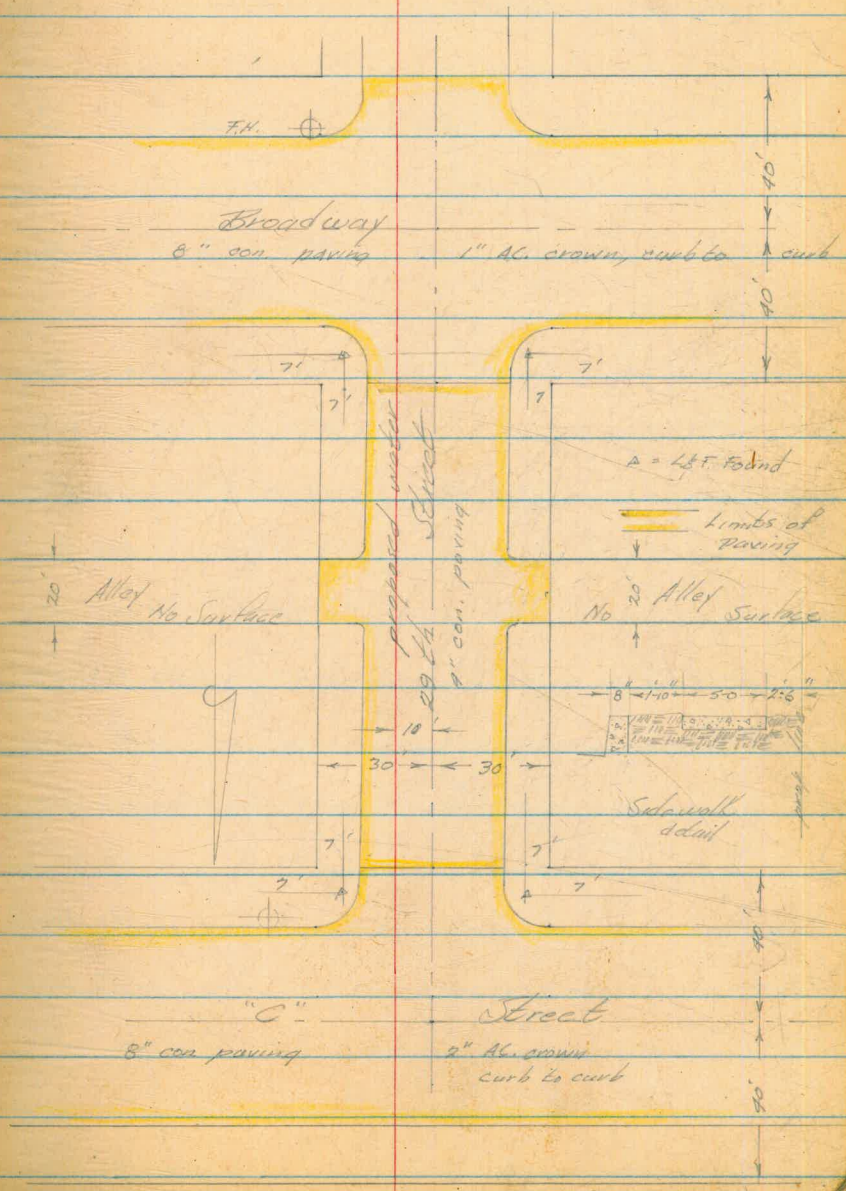
Profile & Proposed Water Line
29th St, "C" St. to Broadway

0+00 S/H of Broadway

0+80 N/H of Broadway

31+82.78 S/H of "C"

4+62.78 N/H of "C"



29th St. Cont

183.60

10.01 193.61

0+00 11.6 182.01

0+13 11.7 181.91

0+14 11.7 181.91

0+24.5 10.9 182.81

0+40 10.9 182.71

0+66 10.7 182.91

0+80 10.7 182.91

0+81 8.4 185.21

1+00 4.8 188.81

1+50 5.5 188.11

2+00 7.2 186.41

2+50 10.0 182.61

3+00 12.93 180.68

T.P. 3.51 184.19

SE. FH. 29th & Broadway

S/H of Broadway

FH. 30' RT

So curb line Broadway

Water GV. 3' RT

& Broadway

No curb Broadway

N/H of Broadway

Water GV. 1' RT

189.19

3+50	5.5	178.69	
3+82			Water Gk. 1' ft
3+82.78	9.3	174.89	S/E of "C" St
3+95			TH. 35' ft.
3+96.78	9.5	174.69	So. curb of "C"
4+00	9.3	174.89	
4+07			Water Gk. 35' ft
4+22	8.4	175.99	Gas crossing
4+48.78	8.7	175.99	No. curb of "C"
4+53	8.0	176.19	front sidewalk
4+58	7.9	176.39	back sidewalk
T.P.	7.92	176.77	SETH "C" & 20th.

Profile of Proposed Water Line
 Country Club Drive, Country Club
 Pump Sta. to Existing Line
 So. of Mumbulus Way

380.46

± Lgt. B.C. Sta. 1400 at Pump Sta.

0.30 380.76

0+00 11.7

0+50 6.0

1+00 B.C. 0.3

T.P. 0.12 380.64

13.00 393.64

1+25 10.3

1+50 7.4

1+75 4.6

2+00 1.7

T.P. 0.54 393.10

12.86 405.96

Went
 Camp
 Holohan
 Alexander

37

2-30-55

405.96

2+25	11.1	
2+50	8.2	
2+80.03 F.C.	4.8	
3+00	2.6	
T.P.	0.08	405.88

12.65 418.53

3+25.83 B.C.	12.1	
3+50	9.3	
3+75	6.4	
4+00	3.6	
4+11.66 P.R.C.	2.3	
T.P.	0.61	417.92

11.26 429.18

4+25	10.1	
4+50	9.3	

4+97

Left \$ Right

2.3	2.3	2.6
<u>9</u>	<u>9</u>	<u>9</u>

10.1

11.9

9 Tele crossing

9.2	9.1	9.3	10.2
<u>12</u>	<u>4</u>	<u>5</u>	<u>12</u>

SEE MH. 11.16.

129.18
5+00 5.8

5+01

5+50 3.7

5+84

5+89⁷ 2.9

5+97

6+00 2.0

6+10.65 EC 1.6

6+15 1.5

6+50 0.4

LE

$\frac{5.3}{9}$

$\frac{5.8}{0}$

$\frac{6.7}{12}$

gutter

$\frac{3.3}{9}$

$\frac{3.7}{0}$

$\frac{4.3}{12}$

gutter

Sewer
crossing $\frac{2.2}{9}$

$\frac{2.4}{0}$

Sewer crossing

Sewer MH 15' RL, 6.1 to flow

$\frac{1.8}{13}$

$\frac{2.0}{0}$

$\frac{2.5}{12}$

$\frac{1.8}{12}$

$\frac{1.6}{0}$

$\frac{2.4}{12}$

Storm Drain $\frac{\text{flow } 4.7}{12}$

$\frac{\text{grade } 1.2}{12}$

$\frac{1.5}{0}$

$\frac{\text{grade } 2.4}{12}$

$\frac{5.5 \text{ flow}}{12}$

$\frac{0.5}{12}$

$\frac{0.4}{0}$

$\frac{0.8}{12}$

	429.18		
T.P.		0.06	429.12
	11.25		440.37
7+00		10.1	
7+21		9.32	
7+26		9.22	
7+40		8.7	
7+50		8.2	
7+52		7.85	
7+97.77 B.C.		5.0	
8+50		0.3	

Left

+

Right

10.2
1210.1
010.5
12

G.E. MH. 7' L.

Sewer MH. 15' D., 11.6 ft. H.

8.7
0

Sewer crossing

8.0
128.2
08.4
12

Sewer MH. 12' L. 4.5 to flow

5.2
125.0
05.6
120.0
120.0
120.3
00.9
12

430.17

Left E Right

T.P. 008 440.29

12.74 453.03

8+57 Gas GV. 14' 16"

9+00 7.1 $\frac{5.1}{24}$ $\frac{6.3}{12}$ $\frac{7.1}{8}$ $\frac{8.0}{12}$

9+05 Telo. MH. 1.5 RE

9+10 Gas & Ele. MH. 1.5 RE

9+18 5.1 10" Sewer $\frac{5.1}{8}$ $\frac{5.9}{72}$
Crossing

9+18 Sewer MH. 19 ft. 5.3 to Pl.

9+50 2.0 $\frac{2.5}{12}$ $\frac{2.6}{8}$ $\frac{2.3}{72}$

T.P. 006 452.97

12.85 465.82

9+97.40 E.C. 10.4 $\frac{10.6}{72}$ $\frac{10.9}{8}$ $\frac{10.7}{72}$

10+50 5.2 $\frac{5.4}{12}$ $\frac{5.2}{8}$ $\frac{5.4}{72}$

465.82

1.02 464.80

11.81 476.61

10+84

10.58

Sewer M.H. 17" Lt (not opened)

11+00

10.8

 $\frac{11.1}{72}$ $\frac{10.8}{72}$ $\frac{11.1}{72}$

11+50

6.0

 $\frac{6.1}{72}$ $\frac{6.0}{72}$ $\frac{6.4}{72}$

12+00

3.6

 $\frac{3.6}{72}$ $\frac{3.6}{72}$ $\frac{4.0}{72}$

12+13

Water G.H. 6.5 Lt & F.H. 13.5 Lt

12+41

3.87

G&E M.H. 3' Rt.

12+46

4.18

T&L M.H. 5' Rt.

12+50

4.2

 $\frac{4.2}{72}$ $\frac{4.2}{72}$ $\frac{4.6}{72}$

13+02.30 B.G.

8.5

 $\frac{8.8}{72}$ $\frac{8.5}{72}$ $\frac{8.7}{72}$

10.19 466.42

0.48 466.90

466.90

Left

Right

13+25

1.4

 $\frac{1.7}{12}$ $\frac{1.4}{8}$ $\frac{1.6}{12}$

13+30

0.49

Sewer MH, 16' LL. (not opened)

13+50

4.2

 $\frac{4.6}{12}$ $\frac{4.2}{8}$ $\frac{4.5}{12}$

13+75

7.2

 $\frac{7.6}{12}$ $\frac{7.2}{8}$ $\frac{7.3}{12}$

14+00

10.0

 $\frac{10.4}{12}$ $\frac{10.0}{8}$ $\frac{10.5}{12}$

T.P.

12.19 454.71

0.06 454.77

14+25

0.9

 $\frac{1.1}{12}$ $\frac{0.9}{8}$ $\frac{1.1}{12}$

14+50

3.8

 $\frac{3.9}{12}$ $\frac{3.8}{8}$ $\frac{4.1}{12}$

14+65

5.80

Tele. MH, 6' RL

14+71

6.30

E.A.F. MH, 3' RL

14+75

6.6

 $\frac{6.6}{12}$ $\frac{6.6}{8}$ $\frac{7.6}{12}$

Left

£

Right

454.77

15+00

9.3

$\frac{9.5}{72}$

$\frac{9.3}{72}$

$\frac{10.4}{72}$

15+13.02 E.G.

10.7

$\frac{10.8}{72}$

$\frac{10.7}{72}$

$\frac{11.8}{72}$

T.P.

13.18 441.59

0.11 441.70

15+50

1.7

$\frac{1.6}{72}$

$\frac{1.7}{72}$

$\frac{2.4}{72}$

16+00

6.8

$\frac{6.9}{72}$

$\frac{6.8}{72}$

$\frac{7.6}{72}$

16+50

11.6

$\frac{11.8}{72}$

$\frac{11.6}{72}$

$\frac{12.3}{72}$

13.28 428.42

0.30 428.72

17+01.52 B.C.

3.7

$\frac{3.8}{72}$

$\frac{3.7}{72}$

$\frac{4.3}{72}$

17+20

5.32

G.F. M.H. 3.5 26

17+25

5.7

$\frac{5.7}{72}$

$\frac{5.7}{72}$

$\frac{6.6}{72}$

17+50

7.9

$\frac{7.7}{72}$

$\frac{7.9}{72}$

$\frac{8.7}{72}$

428.72

17+75

9.5

Left

Right

$\frac{9.0}{12}$

$\frac{9.5}{8}$

$\frac{10.5}{12}$

18+00

10.8

$\frac{10.1}{12}$

$\frac{10.8}{8}$

$\frac{12.1}{12}$

$\frac{12.7}{11}$

T.P.

12.26 416.46

9.88 426.34

18+25

8.9

$\frac{8.7}{12}$

$\frac{8.9}{8}$

$\frac{9.9}{12}$

$\frac{11.4}{25}$

18+40.88 P.C.C.

8.9

$\frac{8.4}{12}$

$\frac{8.9}{8}$

$\frac{9.8}{12}$

$\frac{11.2}{25}$

18+50

8.7

$\frac{8.7}{12}$

$\frac{8.7}{8}$

$\frac{9.7}{12}$

$\frac{11.1}{24}$

18+75

7.7

$\frac{7.1}{12}$

$\frac{7.7}{8}$

$\frac{8.9}{12}$

18+81

Water G.V. 8' H

18+83

F.H. 13' H

18+87

7.06

Tale M.H. 7' H

18+94

6.16

G.A.E M.H. 3.5' H

426.34

19+00

5.7

$\frac{5.2}{12}$

$\frac{5.7}{8}$

$\frac{6.6}{12}$

19+25

3.5

$\frac{3.1}{12}$

$\frac{3.5}{8}$

$\frac{4.6}{12}$

19+50

1.7

$\frac{1.2}{12}$

$\frac{1.7}{8}$

$\frac{2.6}{12}$

T.P.

1.30 425.04

745 432.49

19+75

6.2

$\frac{6.0}{12}$

$\frac{6.2}{8}$

$\frac{6.9}{12}$

20+05.15 E.C.

5.3

$\frac{5.3}{12}$

$\frac{5.3}{8}$

$\frac{5.7}{12}$

20+50

4.7

$\frac{4.9}{12}$

$\frac{4.7}{8}$

$\frac{5.5}{12}$

20+82.21

4.3

$\frac{4.5}{12}$

$\frac{4.3}{8}$

$\frac{4.4}{12}$

20+93

4.2

$\frac{4.3}{12}$

$\frac{4.2}{5}$

$\frac{4.2}{8}$

$\frac{4.4}{12}$

Existing
water line G.V.

Left

Right

432.49

21+05

4.14

Tele. MH. 7' RE

21+10

4.00

64E MH 3' RE

3.89 428.60

BM. End of curb, right side C.C. Drive

5-3-55

Profile of Proposed Water Line

"G" St 27th to 28th

Cont. From page 27

B.M.

SE 10' L&T

154.99

12.96 167.95 ✓

7+20.70 13.0 155.0

7+25 12.5 155.5

7+50 9.5 158.5

7+75 6.2 161.8

8+00 3.0 165.0

T.P. 2.45 167.50 ✓

11.67 179.17 ✓

8+25 11.0 168.2

8+50 7.9 171.3

8+75 5.8 173.4

9+00 4.6 174.6

9+25 4.3 174.9

9+50 4.8 175.1

"G" ST CONT

179.17

9+75 6.0 173.2

10+00 8.6 170.6

10+25 11.7 167.5

T.P. 12.89 166.28 ✓

0.59 166.82 ✓

10+50 3.4 163.4

10+75 7.7 159.1

11+00 12.0 154.8

T.P. 12.91 153.91 ✓

0.28 154.19 ✓

11+25 3.5 150.7

11+50 7.9 146.3

11+75 12.0 142.2

11+82.50 12.85 141.34

T.P. 12.98 141.21 ✓

0.60 141.81 ✓

12+00 3.7 138.1

SEWER M.H. 10' LT.

"G" ST CONT

141.81

12+25	8.0	133.8
12+50	12.0	129.8
T.P.	13.20	128.61 ✓

0.57 129.18 ✓

12+75	2.8	126.4
13+00	5.4	123.8
13+25	7.0	122.2
13+41	7.8	121.4
13+41	8.1	121.1
13+41	7.1	122.1
13+61.20	7.5	121.7
13+71	7.6	121.6
13+71	7.31	121.87
13+90	7.0	122.2
13+95 ±	6.8	122.4
14+00	6.7	122.5
14+06	6.7	122.5

STORM DRAIN CROSSING

TOP DRAIN GRATE 8' RT. 10.3 FLOW 36" PIPE

" " " 28' LT. 10.3 FLOW " "

END CON. PAVE & BEGIN A.C. PAVE 28TH ST

SEWER CROSSING

SEWER M.H. 10' LT. 13.7 FLOW

WATER GATE VALVE ON &

" " " " "

129.18

19.10

6.7 122.5

EAST EDGE A.C. PAVE 28TH ST.
T.B.M.

T.P.

7.52 121.66 ✓

SO. END S.W. CURB RETURN 28TH & "G" ST.

1.16 122.82 ✓

T.P.

13.02 109.80 ✓

1.52 111.32 ✓

T.P.

13.19 98.131 = 98.03

SWEEP 28TH & ISLAND

TOURMALINE ST.
MISSION BLVD TO R.R.
③ STR'S & GMS

7/18/58
SHOREY
KEMP
KELLHOFER
HOLEHAN

52

TBM.	1.97	23.54	91.57			
0+80			6.4	87.1	84.0	
1+00			6.6	86.9	83.8	
1+50			7.2	86.3	83.0	
2+00			7.9	85.6	82.1	
2+50			9.2	84.3	81.0	
TP	1.94	86.73	8.75	84.79		
3+00			3.6	83.1	79.6	
3+50			5.0	81.7	77.8	
3+75			5.28	81.45	76.8	
4+00			6.0	80.7	76.6	
4+10			5.9	80.8	76.5	
4+15			7.4	79.3	76.5	
			4.13	82.60	= 82.60	

N.E.F.H. TOURMALINE & MISSION BLVD. (Pg 5)

C3 ¹	6.2	X
C3 ¹	6.4	X
C3 ³	6.9	X
C3 ⁵		
C3 ³		
C3 ⁵	3.2	X
C3 ²	4.6	
C4 ¹	5.1	X
C4 ¹	5.7	X

TOP M.H.

TBM CONCL. MON. 45' RT. (Pg 6)

WATER METERS
93.54

0+81 S.			6.2	87.3	87.3
1+51 N.			5.3	88.2	87.3
1+56 S.			7.9	85.6	85.6
1+75 N.			5.5	88.0	86.8
2+35 N.			7.5	86.0	85.7
2+67 N.			8.5	85.0	85.1
2+90 S.	86.73		3.2	83.5	83.2
2+92 N.			2.5	84.2	84.5
4+04 N.			5.3	84.4	80.7

C0 ²	"783"
C0 ³	"778"
F0 ²	"762", "771"
C1 ²	"768", "770", "772", "774"
C0 ³	762, 764
F0 ²	758, 760
C0 ³	749, 751
F0 ³	754
C0 ³	768, 716, 712

SHASTA ST.
La Playa to -

TBM	2.80	32.34	29.54
0+52 ^E	G.V. BY CITY	4.4	27.9
		24.8	
0+75		3.7	28.6
		24.7	
1+00		3.9	28.4
		24.2	
1+50		4.9	27.4
		23.1	
2+00		6.7	25.6
		21.9	
2+50		7.9	24.4
		21.2	
2+80	86 } 11 1/4° BEND	8.0	24.3
CK. TBM	(END OF WORK	6.45	25.89 = 25.89
		20.7	

WATER METERS
32.34

1+65 W	5.5	26.8	26.5
1+78 W	5.0	27.3	26.1

7/18/55
SHOEEY
KEMP
KELLHOFER
HOLAHAN

53

TBM NAIL IN P.P.S.W. COR. SHASTA & LA PLAYA
(F.B. 904-2)

C3 ¹	4.4
C3 ²	4.4
C4 ²	4.7
C4 ³	5.7
C3 ²	6.9
C3 ²	7.8
C3 ⁶	

TOP STEP AT 3754 SHASTA (F.B. 904-9)

C0 ³	3778
C1 ²	3776

CROWN PT. DR.
 MORELAND ST. TO SHASTA ST.
 (B) STK'S & GRDS FOR U.A.C. MAIN

7/12/55
 SHORRY
 KEMP
 KELLHOFFER
 HOLMAN

54

BM.	7.72	29.40	21.68	S.W.B.P. MORELAND & CROWN PT. DR. (F.B. 904-9)			
0+15 ⁶⁵	25' (6"x4" TEE BY CITY)	7.8	21.6	18.0	C3 ⁶ ±	7.7	X
0+15 ⁶⁵		7.8	21.6	18.0	C3 ⁶	7.8	X
0+50		7.0	22.4	18.1	C4 ³	7.9	X
1+00		6.6	22.8	18.4	C4 ²	7.3	X
1+50		6.8	22.6	19.2	C3 ⁴	6.8	X
1+76 [±]	F.H. TEE	6.1	23.3	19.5	C3 ⁸	6.3	X
	(B)	5.8	23.6		C0 ² C4 ⁴		
2+00		5.9	23.5	19.8	C3 ⁷	6.0	X
2+50		5.8	23.6	20.0	C3 ⁶	5.9	X
3+00		5.7	23.7	20.0	C3 ⁷	5.6	X
3+50		5.7	23.7	20.2	C3 ⁵	5.6	X
3+75		5.7	23.7	20.2	C3 ⁵	5.6	X
4+00		5.7	23.7	20.4	C3 ³	5.6	X
4+50		5.3	24.1	20.6	C3 ⁵	5.3	X
5+00		5.0	24.4	20.6	C3 ⁶	5.3	X
5+39 ⁹⁵	END OF WORK	5.1	24.3	20.7	C3 ⁶	5.2	
		3.52	25.88	= 25.89			
				29.54			
	WATER METERS						
2+82	W.	29.40	5.3	24.1	24.0	C0 ¹ 3702	
3+26	W.		5.0	24.4	24.1	C0 ³ 3722	
3+77	W.		5.1	24.3	24.1	C0 ³ 3730	
5+28	W.		4.7	24.7	24.3	C0 ⁴ 3754	

TOP OF STEP AT 3754 SHASTA (F.B. 904-9)
 TBM NAIL IN P.P. S.W. COR. SHASTA & LA PLAYA (F.B. 904-9)

DEL REY ST

Bunker Hill to Glendora St
 STAs for 6" AC
 Meters set 10^W 30^E of PBL

	144	34.92	33.48
0+75		0.4	34.5 29.6
+50		0.5	34.9 29.5
+85 FH Tec		1.9	33.0 28.4
+85 (3) FH		+0.5	35.4 32.7
1+00		1.8	33.1 27.9
+50		2.1	32.8 26.3
+58 ME		1.8	33.1 30.5
2+00		3.8	31.1 24.8
+35 ME		4.8	30.1 28.8
+50		5.5	29.4 24.1
3+00		6.3	28.6 23.4
+28 ME		6.8	28.1 27.5
+43 MW		8.4	26.5 26.6
+50		7.3	27.6 23.1
+88 ME		7.0	27.9 26.8
4+00		7.5	27.4 22.8
+50		8.0	26.9 22.6
+53 MW		9.62	25.30 25.5

West
 Williams T.
 Varon Fokas
 Alexander J

YH 1944

7-20-55

56

sw Base Man Del Rey + Bunker Hill

C4	$\frac{9}{9}$	Begin work
C4	$\frac{9}{9}$	
C4	$\frac{6}{6}$	
C2	$\frac{7}{7}$	
C5	$\frac{2}{2}$	
C6	$\frac{5}{5}$	
C2	$\frac{6}{6}$	
C6	$\frac{3}{3}$	3567
C1	$\frac{3}{3}$	
C5	$\frac{3}{3}$	3545
C5	$\frac{2}{2}$	
C0	$\frac{6}{6}$	
F0	$\frac{1}{1}$	3535-37
C4	$\frac{5}{5}$	3538
C1	$\frac{1}{1}$	
C4	$\frac{6}{6}$	3531-33
C4	$\frac{3}{3}$	
F0	$\frac{1}{1}$	
		3518

Del Rey St Cont

57

5.63 30.93 25.30

477 ME	4.0	26.9	25.9
+97 MW	6.0	24.9	25.2
5+00	4.8	26.1	22.1
+19 ME	4.6	26.3	25.5
+46 ME	5.0	25.9	25.3
+50	5.2	25.7	21.6
+56 MW	6.7	24.2	24.6
+72 2 Motor West	7.1	23.8	24.3
6+00	6.2	24.7	20.5
+40	2.6	23.3	19.8
	8.30	22.63	=22.63

C1 ⁰	3517
F0 ³	3512
C4 ⁰	
C0 ⁸	3511
C0 ⁶	3509
C4 ¹	
F0 ⁴	3506
F0 ⁵	Blondora St
C4 ²	
C3 ⁵	

SW 3/4 1P prop Cor. T121T 200 page 9

Bunker Hill St

Revere Ave to Del Rey Ave

meters set 7 ERI no Mtg

10.53 26.87 16.34

0+45 9.0 17.9 13.2

1+00 7.0 19.9 14.8

+50 5.7 21.2 16.5

2+00 3.9 23.0 19.7

11.01 35.74 212 24.75

+50 10.5 25.3 21.9

3+00 7.4 28.4 25.4

+50 3.3 32.5 28.6

+85 1.6 34.2 29.6

228 3348

West
Williams T
Varonakis
Alexander &

58

sw corner Main Bunker Hill & Revere

C4 ¹ Begin work

C5 ¹

C4 ¹

C3 ³

C3 ⁸

C3 ⁰

C3 ⁹

C4 ⁶

= 33.48

Revere Avd

Bunker Hill to Glendora

5' x 9' for 6" AC

	7.58	73.92	16.34	
0+45			5.6	18.3 13.2
+80 FH Tee			6.4	17.5 13.0
+80 (6) FH			6.1	17.8 17.0
1+00			6.5	17.4 12.7
+50			6.7	17.7 12.4
2+00			5.0	18.9 12.1
+60			7.2	16.7 11.7
2+35 MW			6.2	17.7 15.5
+76 ME			7.7	16.2 16.0
3+00			7.9	16.0 11.4
+50			7.9	16.0 11.0
4+00			8.1	15.8 10.6
+42 MW	4.49	18.74	9.67	14.25 14.7
+50			3.2	15.5 10.1
5+00			3.5	15.2 9.6
+21 MW			5.4	13.3 13.1
+32 ME			3.8	14.9 13.6
+50			4.2	14.5 9.2

Wrest
Williams &
Varonfakis
Alexander &

59

7-20-57
See Page 11

	5' x 9' conc	man	Revere + Bunker Hill
C5	<u>1</u>		Begin work
C4	<u>5</u>		
C0	<u>8</u>		
C4	<u>7</u>		
C5	<u>3</u>		
	<u>8</u>		
C6	<u>0</u>		
C5	<u>0</u>		
	<u>2</u>		
C2	<u>2</u>		
C0	<u>2</u>		3545-57
	<u>6</u>		
C4	<u>0</u>		
C5	<u>0</u>		
	<u>2</u>		
C5	<u>4</u>		
F0	<u>4</u>		
C5	<u>4</u>		
	<u>6</u>		
C5	<u>2</u>		
	<u>2</u>		
C0	<u>3</u>		
C1	<u>3</u>		
	<u>3</u>		
C5	<u>3</u>		

REVERE CONT.

60.

18.74

7/20/55

+65 FH 20	4.4	14.3	9.0
+65 @ Q FH	4.2	14.5	13.3
6+00 S.	5.5	13.2	8.4
+15	5.6	13.1	8.2
	3.92	14.82	14.81

C5 ³

C1 ²

C4 ⁸

C4 ⁹

NE ³/₄ of REVERE + Glendora

Knoxville St Savannah St
to Morena

Pelims Group 25

3+21.30

Nly prop Line Morena St

0+07

POT

0+00

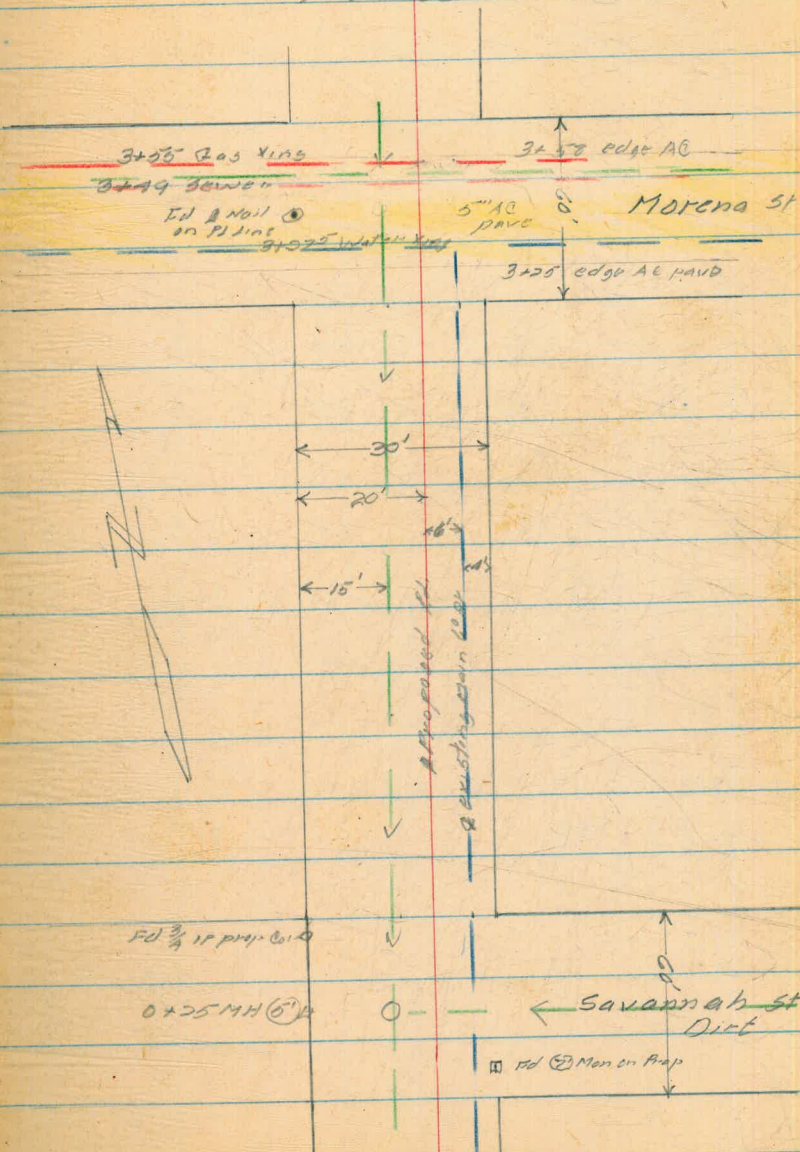
Sly prop Line Savannah

West
Williams
Varonakis
Alexander

3+25
16.30
3+41.30
30
3+71.30

61

7-22-55



Knoxville St
 & Profile

62

2.35 12.39 10.04

BR More enabled Tealote Crk
 or Top inlet

0+00

Sly prop line Savannah

0+00

8.4

$\frac{7.8}{20'RT}$ $\frac{8.9}{16'RT}$ $\frac{8.3}{5'RT}$

$\frac{8.0}{10'RT}$

+6.4 To Flow

+25

7.94

Top cost Rim sewer MH

$\frac{7.9}{20'RT}$ $\frac{7.9}{5'RT}$

$\frac{8.6}{10'RT}$

+50

7.9

$\frac{7.2}{20'RT}$ $\frac{8.5}{16'RT}$ $\frac{8.1}{5'RT}$

$\frac{8.7}{7'RT}$ $\frac{7.8}{10'RT}$

1+00

8.3

$\frac{7.3}{20'RT}$ $\frac{8.0}{5'RT}$

$\frac{8.2}{7'RT}$ $\frac{7.9}{10'RT}$

+50

8.0

$\frac{7.0}{20'RT}$ $\frac{7.2}{15'RT}$ $\frac{7.2}{5'RT}$

$\frac{7.8}{10'RT}$

2+00

7.8

$\frac{6.8}{20'RT}$ $\frac{7.7}{15'RT}$ $\frac{7.6}{5'RT}$

$\frac{7.4}{10'RT}$

+50

7.6

$\frac{5.8}{20'RT}$ $\frac{6.3}{17'RT}$ $\frac{6.1}{5'RT}$

$\frac{6.3}{10'RT}$

3+00

6.0

Begin to pave

$\frac{4.03}{20'RT}$ $\frac{4.09}{5'RT}$

$\frac{4.00}{10'RT}$

+25

3.96

+41³⁰ @ AC

3.27

+9.8 To Flow

Top North rim sewer MH 6'RT

$\frac{3.71}{20'RT}$ $\frac{3.86}{5'RT}$

$\frac{3.94}{10'RT}$

+58³

3.91

$\frac{3.8}{20'RT}$ $\frac{3.8}{5'RT}$

$\frac{3.3}{10'RT}$

+71³⁴

3.6

2.35 10.04 = 10.04

Colle Del Oro
La Jolla Shores Dr. to
Colle Del Cielo

Stks for Wat Mts

Meters Set 22° from Qst existing line ^{Pass} 0+00 east edge

10.23 37.92 22.69

1497 MN 31 34.8 39.0

1217 49.83 0.26 37.66

3704 MN 9.65 41.1 39.9

476 MN 4.5 45.9 43.8

A 418 MN 1.6 48.2 47.1

12.67 62.50 0.00 49.93

5747 MN 1.2 61.3 59.8

T.P. 0.31 49.71 13.10 49.40

T.P. 0.52 37.01 13.22 36.49

CHECK

B.M. 9.31 27.70 = 27.69

West
Williams +
Varonakis +
Alexander

63

7-22.55

B.M. SW Disc Camino Del Oro to La Jolla Shores Dr.

005 2330

012 2340

015 2354

014 2360

015 2385

118

Ollic St + Liberty St.
from midway to Cumulos
Stks for 6" AC

West +
Williams +
Varonfakis
Alexander

64

7-21-55

	209	5.47	338	+4.3
1+55		5.2	0.3	-4.0
1+55		5.0	0.5	-4.0
2+00		5.2	0.3	-3.3
+50		5.2	0.3	-3.2
2+63 WMDly		6.0	-0.5	2.8
3+00		5.0	0.5	-3.2
3+07.60 90' Road		4.8	0.7	-3.2

TBM nail in conc wall Set FB905 p26

Top existing 8" ci

C 4 ⁵ Begin Work

C 3 ⁶

C 3 ⁵

F 3 ³

C 3 ¹

C 3 ⁹

4120 Liberty

Liberty St

0+20		5.3	0.2	-3.4
0+45 smets SWly		5.0	0.5	3.0
0+50		6.2	-0.7	-4.2
0+60 FA Jec		6.2	-0.7	-4.2
0+60 @ R.F.H		5.4	0.1	3.1
0+67 SWly W.M		4.7	0.8	3.1
1+00		6.3	-0.8	-4.2
+50		6.4	-0.9	-4.2
+52 W.M SW		5.4	+0.1	3.2
2+00		6.3	-0.8	-4.3

C 3 ⁶

F 2 ⁵

C 3 ⁵

C 3 ⁵

F 3 ⁰

F 2 ³

C 3 ⁴

C 3 ³

F 3 ¹

C 3 ⁵

4133

4145

LIBERTY ST. CONT.

65.

5.47

2+00 W/M NELY	6.1	-0.6	3.6
+25 W/M SWLY	5.5	0.0	3.4
2+50	6.5	-1.0	-4.4
+58 W/M NELY	6.4	-0.9	3.8
+87 W/M SWLY	5.6	-0.1	3.6
3+00	6.4	-0.9	-4.4
+05 W/M NELY	6.6	-1.1	4.0
+36 W/M NELY	6.4	-0.9	4.1
+57	6.6	-1.1	-4.4
+76 W/M NELY	6.5	-1.0	4.2
4+00	6.3	-0.8	-4.5
+50	6.5	-1.0	-4.5
5+00	6.6	-1.1	-4.6
5.73	4.35	6.55	-1.08
+36 W/M SWLY	5.9	-1.0	3.0
+50	5.7	-1.3	-4.6
6+00	5.7	-1.3	-4.6
+25	5.7	-1.3	-4.7
+47 EHTC	5.7	-1.3	-5.0
7+47 (5) EHTC	5.8	-1.4	3.3

7/29/55

F4 ²	4190
F3 ⁴	4149
C3 ⁴	
F4 ⁷	4154
F3 ⁷	4159
C3 ⁵	
F5 ¹	
F5 ⁰	4202
C3 ³	4210
F5 ²	
C3 ⁷	
C3 ⁵	
C3 ⁵	
F4 ⁰	4227
C3 ³	
C3 ³	
C3 ⁴	
C3 ⁷	
F4 ⁷	

LIBERTY ST. CONT.

66.

1.35

6+50 ^{5 Wly}	5.7	-1.3	-5.1
+51 2 Mts	5.5	-1.1	2.8
+95	5.6	-1.2	-5.8
	5.39	-1.04	= 1.01

7/29/55

C3 ⁸F3 ⁹C4 ⁴

end of work

Top Fly Run Sewer MH @ Columbus + Liberty

Linwood St Check on

West 8-19-55
Meters see following page

7.89 172.21 164.32

= 1100

0+00 City Eng

3.1 168.80

C 120

Grade
167.60

1+07 Mt Nly

5.1 167.1

Top of Meter Box

1+80 M Nly

3.4 168.8 165.6

= C 32 = C 32

= 1485

1+35 City Eng Mt

4.9 167.3 165.6

100 62 in Stake 167.2

166.8

2+05 M Nly

5.8 166.4

= 2+05

1+55 City Eng

6.4 165.8 164.0

Cut 0³⁰ on Stake

7.89 164.32 = 164.32

Linwood St
Pringle to Keating

Stks for Meters

Reset	17' 85' Meters	Stk 22' from A St	7860 ft
	8.98	172.30	144.32
0+90	2 mts WM NY	2.4	170.9
			167.4
1+07	WM NY 108'	1.3	171.0
			167.1
1+51	WM NY 152'	6.1	167.2
			165.9
1+80	WM NY 148.5'	2.4	169.7
			166.7
1+90	WM NY 149.5'	6.8	170.7
			165.6
2+06	MM NY 2407	4.7	165.1
			164.7
2+15	MM NY 2416	7.9	165.4
			164.0
			163.3
	0.21	160.76	162.6
		12.75	160.55
2+86	WM NY 2427	6.5	150.8
			154.3
			150.6
	1.52	152.62	141.6
		12.66	148.10
3+23	WM NY	5.7	140.8
			146.9
			141.6
3+35	WM NY	10.4	138.5
			142.2
			138.0
	12.09	164.37	0.34
			152.28
	9.90	173.33	0.44
			162.43
			163.32 = 163.32
			9.01 164.32 = 164.32

West

Williams X
Varonakis +
Alexander
Kallbaker

8-3-55

BM 10 High

BM NW 1/4 Linwood + Pringle
0+00 15 N.W. PROP. PRINGLE

~~C 5.5 C 22 C 16~~

0 4.9 ~~C 32~~ C 11 1789

0 1.3 ~~C 03~~ C 08

0 5.1 ~~C 11~~ C 32 1776

0 1.8 ~~C 05~~ C 05 1775

0 4.6 ~~C 36~~ C 25 1770

0 2.8 ~~C 18~~ C 18 1767

0 3.7 ~~C 27~~ C 23 1762

0 5.3 ~~C 43~~ C 06

0 4.2 ~~C 32~~ 1752

67

169.7
168.8
165.6
03.2

164.0
22
166.5

WORDEN ST. VOLTAIRE TO UDAL

STKS. FOR 6" A.C. MAIN

WILLIAMS
ALEXANDER
VARONFAKIS †
KELLHOFER X

68.

8/10/55

T.B.M.

89.56

S.W. L&T VOLTAIRE + WORDEN

1.64 91.20

0+45 2.4 88.8

0+50 2.4 88.8 85.4

0+75 2.5 88.7 84.2

1+00 4.8 86.4 82.6

1+50 5.9 85.3 80.6

1+75 7.2 84.0 79.5

2+00 8.2 83.0 78.3

2+25 8.8 82.4 77.0

2+50 9.7 81.5 75.1

3+70 12.6 78.6 73.7

8.70 82.50 = 82.49

MEET EXISTING

C3 4

C4 5

C3 8

C4 7

C4 5

C4 7

C5 4

C6 4

MEET EXISTING

FH UDAL + WORDEN

CUT SHEET
MADE 8/11

32nd St Ast to 190' North

Proposed P2
Group 26

West
Williams
Vamvakis
Kellhofer

69

9-19-55

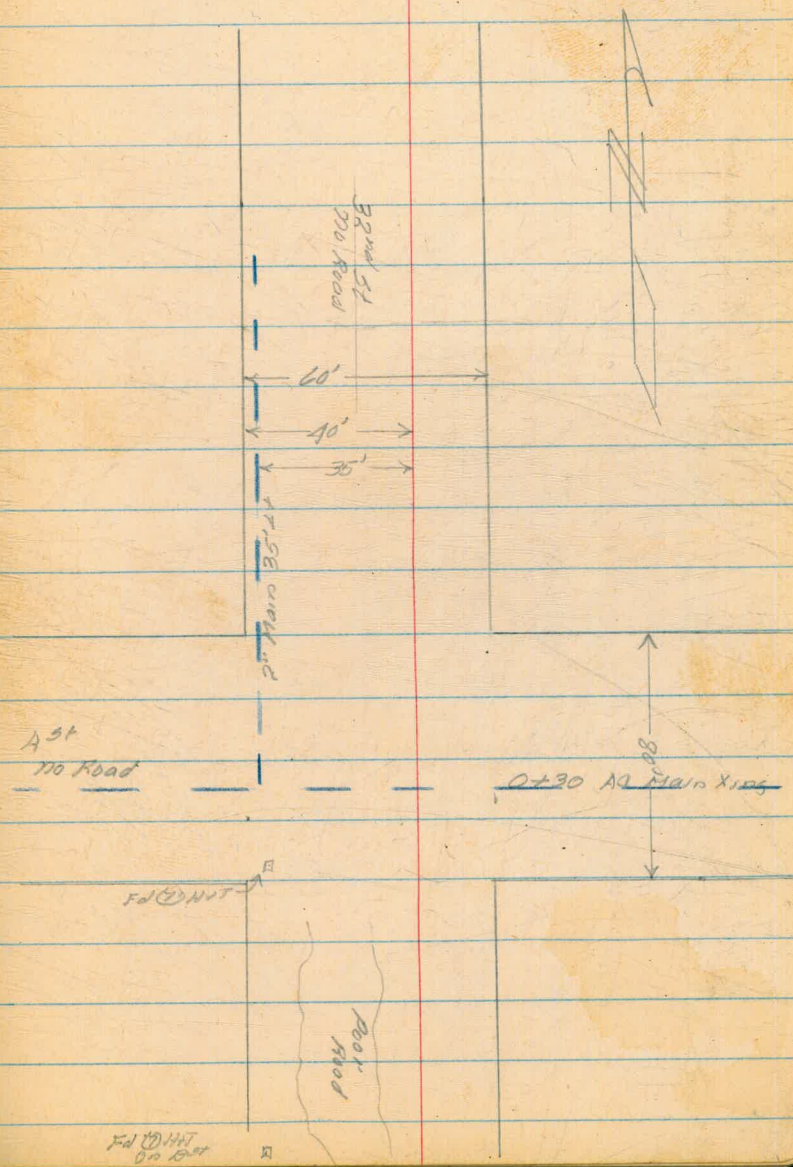
1+90±

End of work

0+07 POT

0+00

Sly Line Ast



32nd St

Q Profile

70

Sec. 4B
A⁵⁶
0+169.20

Sec. A⁵⁷

064 170.44 169.80

TBIS Nail in power pole 45' LL 0+00

0+00

slly prop line A⁵¹

0+00 7.0

$\frac{2.9}{21.1}$ $\frac{6.0}{18.1}$ $\frac{9.3}{25.1}$

0+21 8.6

Q

0+27 10.6

0+44 10.1

+46 9.0

0+50 10.5

$\frac{5.2}{10.1}$ $\frac{5.9}{8.1}$ $\frac{12.7}{7.1}$ $\frac{17.3}{20.1}$

0+

0+70 13.5

$\frac{5.5}{28.1}$ $\frac{7.5}{10.1}$ $\frac{18.4}{10.1}$

5.73 164.37 11.80 158.64

1+00 10.4

$\frac{6.2}{15.1}$ $\frac{14.1}{15.1}$

6.96 160.83 10.50 153.87

1+50 7.8

$\frac{1.9}{15.1}$ $\frac{12.5}{15.1}$

1+90 7.3

$\frac{2.3}{15.1}$ $\frac{3.7}{12.1}$ $\frac{4.2}{8.1}$ $\frac{11.9}{15.1}$

2.80 158.63

Dale St

Q Profile

72

5.59 317.41

311.82

0+00

5.2

+50

5.38

1+00

6.12

+32

6.53

5.59 311.82 = 311.82

SE BP Dale + Redwood

Top of Cover Nly Prop Line Redwood

Prod of Work

Quince St
Vancouver to Haller
Check Depth of existing 6" CI

1035 290.04 279.69

6.62 296.43 023 289.81

0+75 5.96 290.47 2932

1+32 6.14 290.29 2932

2+00 8.12 288.31 290.7

2+58 12.35 284.08 286.5

14.2 282.2

9.21 287.22 = 287.23 TBM PP SW Cor Quince + Haller

West
Williams T
Varonakis +
Kollhofer
120412 8-19-55

7.7
4.3
2.3
10.5
12.2

73

0+00 Fly Line Vancouver

BM NE BP Nite + Quince

Top existing 6" CI

NG. Rocks in casing

Top CV Vly Prop Line Haller

LINWOOD. PRINGLE TO KEATING

STKS for Meters

See page 67 New 1 Sheet
Meters Set 17th from # 4

West
Williams
Varonakis
Alexander

74

8-24-35

8.12	172.44		164.32		5th L+T Linwood + Pringle
0+90 M Nly		3.3	169.1	167.6	C1 ²
1+07 M Nly		3.8	168.6	167.4	C1 ³
1+57 M Sly		5.9	166.5	166.7	C0 ³
1+80 M Nly		3.8	168.6	166.7	C1 ⁹
1+90 M Sly		7.1	165.3	165.1	C0 ²
2+06 M Nly		6.6	165.8	165.4	C0 ⁴
2+15 M Sly		8.3	164.1	163.3	C0 ⁸
0.52	160.14	1282	159.62		
2+86 M Nly		7.7	152.4	150.8	C1 ⁶
0.53	147.68	1299	147.15		
3+23 N Sly		5.7	142.6	140.8	C1 ³
3+35 N Nly		7.1	140.6	138.5	C2 ¹
12.77	159.93	0.52	147.16		
12.65	172.43	0.15	159.78		
		8.10	164.33 = 164.32		

BOUNDARY ST

LAUREL TO KALMIA

STKS for Meters

Meters set 17³ from Q St 25' from FlyWest
Williams
Varonfakis
Alexander

75

line boundary st

8-25-55

0.92 295.54 295.12

BY SE Cor Boundary + Maple

0+26 M Wly 6.7 288.8 288.7

C0¹ 3547 Laurel

0+46 M Ely 7.7 287.8 287.2

C0⁶ 2443

0+76 M Wly 8.1 287.4 287.1

C0³ 2432

0+93 M Ely 9.0 286.5 285.8

C0⁷ 2429

1+19 M Wly 9.7 285.8 285.6

C0⁵ 2424

1+60 M Ely 11.0 284.5 283.6

C0² 2421

4.20 288.86 10.88 284.66

1+84 M Wly 5.1 283.8 283.6

C0³ 2410

2+14 M Ely 6.3 282.6 281.9

C0⁷

2+20 M Wly 5.8 283.1 282.4

C0³ 2404

2+43 M Ely 7.1 281.8 281.0

C0⁸ 2409

2+79 M Wly 7.5 281.4 280.5

C0² 2380

8.55 296.81 0.60 288.26

1.71 295.10 = 295.12

STAKES & Grades FOR
 WATER SERVICES
 ALLEY BLK 2 - Wilshire Terr
 El Cajon to Meade - Van Dyke to 43rd

Nov. 24 1956
 Beatty
 Paulson
 O'Brien

76.

BM	3.66	367.22		363.56	SWBP El Cajon & Van Dyke
0+12 W			4.1	363.1	362.8 C12 -0.9
0+59 E			4.2	363.0	362.7 C12
0+90 W			4.1	363.1	362.4 C16
0+99 E			5.0	362.3	361.8 C14
1+31 E			5.9	361.3	361.1 C11
1+55 W			6.6	360.6	360.5 C11
1+88 E			7.5	359.7	359.6 C11
2+09 E			8.2	359.0	359.0 C09
2+91 E	0.48	356.28	11.42	355.80	355.0 C17
3+21 W			0.4	355.9	353.9 C30
3+46 E			2.8	353.5	352.3 C21
3+59 W			3.4	352.9	351.8 C20
3+74 E			5.2	351.1	350.9 C11
4+06 W			6.3	350.0	350.8 C01
4+31 W			6.3	350.0	350.6 C03
4+35 E			6.5	349.8	350.4 C03
4+64 W			6.0	350.3	350.5 C07
4+77 E			6.7	349.6	350.2 C03

Alley Blk 2
(Cont'd.)

11/24/56

77

356.28

5+22 E 6.1 350.3 350.2 C10

5+39 W 5.5 350.8 350.8 C09

5+61 E 6.1 350.2 350.1 C10

5+93 W 5.3 351.0 351.0 C09

TP 11.02 367.14 0.56 355.72

OK BM 3.60 363.51 = 363.56

96

865

520

385

6+70.7

4.5

6+75.2

6+66.0

2.5

6+68.5

46

7

7+21.5

232

210.8

21.2

53
624.7

677.7

10

6+67.7

2.5

6+65.2

6+67.7

46

7+13.7

6

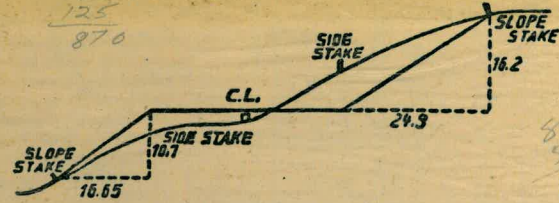
7+19.7

7+020

6+68.5

33.5

1.7
125 212.00
125
870



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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