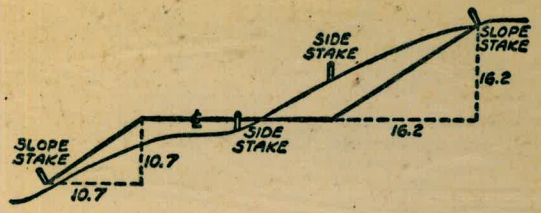

Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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Stks For 6" AC Main
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Date St 29th St to 25 East of Dale St 29-30
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Quince St Haller to Nile 31
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Cut sheet made

Upshur + Shafter St
Scott to Cañon St
stks for 6" Main

	3.51	14.66	11.15		
0+45					
+50			2.9	11.8	7.5
+77 FH Tee			3.1	11.6	6.7
+77 ⑤ ℄ FH			3.2	11.5	~~9.4~~ 9.6
1+00			4.4	10.3	6.2
+50			5.8	8.9	5.0
2+00			6.8	7.9	3.8
+50			7.8	6.9	2.5
3+00			9.0	5.7	1.3
+15-04 BC			9.7	5.0	0.8
+25			10.4	4.3	0.6
+50			10.7	4.0	-0.3
+75			11.5	3.2	-1.2
4+00			11.8	2.9	-2.4
+25			12.1	2.6	-2.4
+50	4.77	7.29	12.14	2.52	-1.7
+75			4.6	2.7	-1.2
+80.10 EC			4.6	2.7	-1.0

West
Williams ⊼
Varontakis ⌽

3/28/55

See FB893 Page 32

Turn on SW ⑦ Mon Scott + Upshur St

Begin Work

C4 3
C4 9
C1 9
C4 1
C3 9
C4 1
C4 4
C4 4
C4 2
C3 7
C4 3
C4 4
C5 3
C5 0
C4 2
C3 9
C3 7

Upshur + Shafter Cont

7.29

5+00 End of = 1+87	4.4	2.9	-0.6
+67 ME	4.3	3.0	3.0
+50	3.8	3.5	-0.7
1+00	4.0	3.3	-1.0
0+45	6.1	1.2	-1.8
	4.70	2.59	=

3/28/55

C 3 5 5+00 end of work Upshur
C 0 0 = 1+87 " " " Shafter
C 4 2
C 4 3
C 3 0

7.57 BM BD SW cor Cañon + Shafter

Cutsheet made

Talbot St
Scott to Rosecrans
stks for 6" ℄

	2.20	13.35		11.15	
0+27			4.4	9.0	5.0
+50			3.6	9.8	5.8
1+00			2.4	11.0	7.5
+50	12.03	24.70	0.68	12.67	9.3
2+00			10.4	14.3	10.9
+50			8.4	16.3	12.7
3+00			6.5	18.2	14.7
+50			4.2	20.5	16.9
+70			3.6	21.1	18.0
			6.26	18.44	=18.43

West
Williams π
Varontokis ¢

3/28/55

See FB 893 Page 32

Turn on (T) mon Scott + Upshur St

C4 $\frac{0}{}$	Begin work
C4 $\frac{0}{}$	
C3 $\frac{5}{}$	
C3 $\frac{4}{}$	
C3 $\frac{4}{}$	
C3 $\frac{6}{}$	
C3 $\frac{5}{}$	
C3 $\frac{6}{}$	
C3 $\frac{1}{}$	End of work

3+00 ℄ nail see FB 893 page 30

Cut sheet made

Oliver St

Olney to Lamont

Stks for 6" AC Main

	8.42	9.33		0.91	
0+80 ms			7.0	1.4 2.3	5.0
0+80			5.7	3.7 3.6	0.2
1+00			6.0	3.3	-0.2
+08 mN			6.0	3.3	1.6
+50			7.0	2.3	-1.0
2+00			7.3	2.0	-1.4
+04 mN			7.2	2.1	3.8
+32 mN			7.5	1.8	3.8
+50			6.8	2.5	-1.6
+75 MN			8.4	0.9	3.6
3+00	6.07	7.21	8.19	1.14	-2.0
+50 M.N.			5.7	1.5	3.4
+50			6.0	1.2	-2.0
4+00			5.5	1.7	-2.0
+00 MN			5.9	1.3	3.2
+50 MN			6.0	1.2	3.1
+50			5.4	1.8	-2.0
+93 MN			5.8	1.4	3.0
5+00			6.2	2.0	-2.0
+50			4.9	2.3	-2.0

West

Williams ↗

Varonfakis ↓

3/29/05 CLEAR + WINDY

See FB 897

TBM Nail in Guy pole 60' South 1+00

F2 7/ F3 1/

C3 4/ 32

Begin work by city

C3 5

C3 3 F1 3

C3 4

F1 7

F2 0

C4 1

F2 7

C3 1

C3 2

C3 7

F1 9

F1 9

C3 8

F1 6

C4 0

C4 3

3.3
5.2
8.5 HI
4.8
3.7
8.5
6.9
1.6

2160

2158 4.5 1.3

9.2

2154

F1 9

2128

2120

2114

Oliver Cont

3/29/55

	T.E.					
5+60 EH Tee		5.3	1.9	-2.0	C3 9	
+60 (5)		5.0	2.8	2.6	FO 4	
6+00		5.9	1.3	-2.0	C3 3	
+50		4.6	2.6	-1.8	C4 4	
+69 MN		3.4	3.8	4.4	FO 6	
7+00		1.9	5.3	1.6	C3 1	2074 end of work By City Begin work by Contractor
	10.51	16.91	0.81	6.10		
7+20 MN		9.6	7.3	6.9	CO 4	2068
+50		9.3	7.6	3.8	C3 8	
+71 MN		7.8	9.1	9.0	CO 1	2061
8+00		7.7	9.2	5.2	C4 0	
+50		6.9	10.0	6.4	C3 6	
9+00		5.8	11.1	7.4	C3 1	
+08 MN		5.1	11.8	12.2	FO 4	2040
+50		4.7	12.2	8.6	C3 6	
+78 MN		3.6	13.3	13.7	FO 4	2032
10+00		3.4	13.5	9.8	C3 1	
+28 MN		2.2	14.7	14.9	FO 2	2026
+50		2.8	14.1	10.1	C4 0	

	16.91					3/29/55	
10+87 MN		1.7	15.2	15.8	F0 6		
11+00		2.7	14.2	10.4	C3 8	2014	6.28 4.88 1.40 14.20 15.60
+50 FH Tee		2.4	14.5	10.6	C3 9		15.3
+50 ⑤ & FH		~~1.6~~	~~15.3~~	16.1	~~F0~~ 8	Replaced ⑩ F0 5 4/5/55	F.H. set at 1160 From RP. 5/13/55 ~~15~~
+75		2.2	14.7	9.8	C4 9	6"x6" vert Tee	
+88		2.1	14.8	9.4	C5 4		
12+00		1.7	15.2	9.4	C5 8		
+50 1288	29.15	0.64	16.27	12.6	C3 1		
13+00		9.5	19.7	16.0	C3 1		
+17 MN		9.5	19.7	20.9	F1 2	1968	
+27 MS		6.9	22.3	23.2	F0 9	1965	
+35 MN		7.7	21.5	22.5	F1 0	1964	
+50		4.8	24.4	20.8	C3 6		
+86 MS 1291	41.12	0.94	28.21	28.7	F0 5	1957	
14+00		11.9	29.2	25.6	C3 6		
14+00 WM Nor.		11.1	30.0	28.7			
+30 MS		9.7	31.4	32.6	F1 2 C/3	WM std 4/8/55 1951	
+48 MN		7.9	33.2	32.9	C0 3	1946	
+50		8.3	32.8	29.6	C3 2		
+78 MS		6.4	34.7	35.7	F1 0	1945	

Oliver Cont

		41.12						3/29/55
15+00			5.3	35.8	32.6	C3	2	
+25			4.4	36.7	33.4	C3	3	
+50			3.8	37.3	33.9	C3	4	
+52	MN		3.4	37.7	37.6	Co	1	1936
+75			3.4	37.7	34.4	C3	3	
+85	MS		2.6	38.5	38.5	Co	0	1927
+92	MS		2.6	38.5	38.6	Fo	1	1921
+95	MN		2.7	38.4	38.2	Co	2	1926
16+00			3.1	38.0	34.6	C3	4	
+36	MS		2.3	38.8	38.9	Fo	1	1917-19
+36	MN		2.0	39.1	38.7	Co	4	1920
+46	MS		2.3	38.8	39.1	Fo	3	1911
+50			3.0	38.1	35.2	C2	9	
	5.70	44.42	2.40	38.72				
17+00			5.8	38.6	35.7	C2	9	
+31	FH Tee		5.3	39.1	36.1	C3	0	
	(6) ℄ FH		~~4.7~~	~~39.7~~	39.7	~~Co~~	0	~~Replaced (7) Co 2 4/5/55 B~~
+50			4.9	39.5	36.3	C3	2	
+70			4.6	39.8	36.4	C3	4	end of work
			4.29	40.13	=	40.12		NE HT (7) Oliver + Lamont

FB 870

Winona
Orange Ave to 300' south
Stks for 6"

	1.45 334.40		332.95	
0+50		6.8	327.6	324.0
1+00		7.4	327.0	324.2
+50		7.2	327.2	324.4
2+00		7.0	327.4	324.7
+50		6.3	328.1	325.5
3+00		3.2	331.2	328.3
2+93		6.40	328.0	
		1.45	332.95 = 332.95	

West
Williams &
Varonfakis

3/30/55

BM SE BP Orange + 49th

C3 6
C2 8
C2 8
C2 7
C2 6
C2 9

Top end of existing 6" AC

April 5 1955
BEATTY
WILLIAMS
VARONFAKIS

ALCOTT ST.

CLOVE 315' NWly
Construction Stks & GROS
FOR 6" A.C.

4/5/55

TBM.	11.13	159.25		148.12	water faucet 15' So & Alcott
0+70	Begin Work		11.5	147.8	144.8
0+95	FH. TEE		10.8	148.5	145.6
	⑩ FH.		10.8	148.5	149.00
1+00			10.5	148.8	145.8
1+50			8.7	150.6	147.9
2+00			6.1	153.2	150.4
TP 2+50	6.83	164.84	1.24	158.01	153.2
3+00			4.1	160.7	156.0
3+15	2" B.O.		3.6	161.2	156.8
TP	1.35	155.62	10.57	154.27	
CK TBM			7.49	148.13 = 148.12	
1+21 NE			6.7	152.6	151.5
1+53 NE		" 159.25	5.5	153.8	153.3
2+12 NE		"	2.7	156.6	156.8
2+54 NE		164.84	5.3	159.5	159.3
3+03 NE			2.5	162.3	161.8

C30 (not marked)		
C29		
FO5		
C30		
C27		
C28		
C48		
C47		
C44		
C11		
CO5	(WAT MET.S. 25 from ℄ ST.)	2456 CLOVE 3510 ALCOTT
FO2		3520 "
CO2		3530 "
CO5		3540 "

CLOVE ST.
ZOLA TO ALCOTT
Construction Grds & Strs for 6" A.C.

4/5/55

BM	2.32	163.82		161.50	B.P. ZOLA & CHATSWORTH
TP	1.71	153.69	11.84	151.98	
0+25	6" GV.	CITY	8.0	145.7	
0+30	6" GV.	CITY	8.0	145.7	
0+50			8.9	144.8	141.4 C3L
1+00			8.7	145.0	141.6 C3L
1+50			8.5	145.2	141.8 C3L
2+00			8.0	145.7	142.3 C3L
2+50			7.7	146.0	142.8 C3L
2+95	EXIST.	6" TEE	6.3	147.4	
CK TBM			5.57	148.11 = 148.12	Wat. Fauc at School Fence

ADDISON ST.
WILLOW TO PLUM
Construct Stks & Grds.
FOR 6" AC. MAIN

BM.	12.81	74.01		61.20	
CK BM.			2.70	71.31 =	
0+70	Begin Work		1.6	72.4	69.0
TP	11.89	85.83	0.07	73.94	
1+00			10.4	75.4	69.4
1+50			10.1	75.7	70.0
2+00			10.5	75.3	70.6
2+50			9.6	76.2	72.4
2+75			4.6	81.2	75.3
3+00	12.55	97.19	1.19	84.64	80.8
3+12.5			9.8	87.4	82.3
3+50			4.7	92.5	84.3
3+63	F.H. TEE		3.0	94.2	84.9
	(7) F.H.		4.9	92.3	88.5
3+70	Plug & Cap		1.9	95.3	85.3
TP	10.32	105.62	1.89	93.30	
CK TP		WAT MET	5.57	100.07 = 100.01	
1+02 NE	Hy	85.8	10.8	75.9	74.9
1+37 NE	(EXIST in CURB)				
1+42 SW			14.0	71.8	76.6
1+79 NE	(EXIST. in curb)				
2+03 SW			12.0	73.8	79.7
2+41 NE			3.4	82.4	82.4
2+50 SW			11.2	74.6	82.2
2+95 NE			1.3	84.5	85.4
3+20 SW	H.	97.19	8.6	88.6	86.2
3+24 NE			10.8	86.4	86.9

April 12 1955
BEATTY
WILLIAMS
ALEXANDER

11

BP NWly Cor CANON & WILLOW ST.
BP SWly Cor Addison & WILLOW. ST

C34 (not marked)
C60
C57
C47
C38
C59
C38
C51
C82
C93
C74 C38
C100
C01
F48
F59
C00
F76
F09
C24
F05

3304 Addison
3312 "
3312 Canon
3320 Add.
3324 Canon
3330 Add.
3332 Canon
3340 Add.
3344 Canon
3350 Addison

4/12/55
Beatty
Williams
Alexander

QUAL TROUGH ST
SAN ANTONIO TO ROSECRANS.
Construct Stks & Grds For 6" A.C. MAIN

B.M	2.59	13.76		11.17	SW B.P. San Antonio & Owens St	FB 881 pg. 50
	4.13	06.05	11.82	01.92		
0+17	Begin Work Existing GV.		5.7	00.4	C	
0+50			3.9	02.2	-01.6	C38
TP	13.03	17.82	1.26	04.79		
1+00			4.5	13.3	06.6	C67
TP	13.08	30.09	0.41	17.41		
1+50			7.7	22.8	19.3	C35
TP	12.89	42.51	0.87	29.62	25.7	C39
1+75						
2+00			4.6	37.9	29.0	C89
TP	12.89	54.56	0.84	41.67		
2+25			11.5	43.1	38.7	C44
2+52			4.7	49.9	45.1	C48
TP	12.35	66.82	0.09	54.27		
3+00			5.2	61.6	57.6	C60
3+02	F.H. TEE		5.1	61.7	57.8	C39
	(6) F.H.		5.0	61.8	61.9	FO- C40
3+04	End Work Existing 6"C.I.		5.1	61.7	58.0	
CK BM			5.13	61.69 =	61.80	B.P. SE Cor Qualtrough & Rosecrans.
CK TP			3.66	63.16 =	63.19	4.5 220l Disc. SW " " " FB. 881 pg. 52
		WAT. MET.S.				
1+05	N/y	4 17.82	6.1	11.7	12.6	FO 9/4 650 San Antonio
1+17	S/y		2.1	15.7	15.3	CO 646 "
1+36 1+37	N/y	2-Mets. 30.09 14	8.3	22.2	20.4	C1 8 2922 Qualtrough.
2+14	S/y	4 42.51	1.7	40.8	40.0	CO 8 2921 "

April 13 1955
Beatty
Williams
Alexander

Lawrence St.
Rosecrans To San Fernando
Construct. Stks & Grds For 6" A.C. Main.
(3 on curb)

BM	9.38	42.98		33.60	B.P. Nely Cor Rosecrans & Kellog
0+50			6.9	36.1	
0+67	F.H. Tee		6.1	36.9	33.0 C3?
TP	11.37	50.24	4.11	38.87	
1+00			10.0	40.2	36.1 C4'
1+50			6.0	44.2	40.2 C4?
2+00			1.9	48.3	44.3 C4?
TP	12.98	62.40	0.82	49.42	
2+50			10.1	52.3	48.3 C4?
3+00			5.9	56.5	52.4 C4'
3+50			2.0	60.4	56.4 C4?
3+59	6" G.V.		2.5	59.9	56.4 C3.5
3+69	6" G.V.		2.1	60.3	56.4 C3?
3+87.5			1.65	60.75	56.4 C4'
4+00			0.75	61.65	57.3 C4'
TP	12.64	74.51	0.53	61.87	
4+25			10.7	63.8	59.3 C4.5
4+30			8.5	66.0	61.5 C4.5
5+00			4.1	70.4	66.0 C4'
TP	12.68	87.02	0.17	74.34	

LAWRENCE ST.
(Cont.d.)

87.02

5+50		12.2	74.8	70.6	C4 2
6+00		7.8	79.2	75.2	C4 0
6+50		3.4	83.6	79.5	C4 1
T.P.	8.88 94.19	1.71	85.31		
6+95 (S)	F.H. TEE F.H.	6.5 6.4	87.7 87.8	83.5	C4 3 CO 0 To Flange F.H. Set 8' out from main. 5' from P.L.
7+00		6.1	88.1	83.9	C4 2
7+15	End Work	5.9	88.3		
CK TBM.		5.24	88.95	= 88.96	E.L.&T. San Fernando F.B. 881 pg. 47

WAT. MET.S EXISTING BK. of Curb.

1+87 N'ly
2+00 S'ly
2+01 S'ly
2+76 S'ly
3+47 N'ly
4+72.5 S'ly
5+49 N'ly
5+64 S'ly
6+62 N'ly

GUIZOT ST.

PT. LOMA TO DEVONSHIRE
Construct. Grds & Stks for
8" A.C. MAIN

BM		2.08	122.23	120.15	BP SE Cor. PT. LOMA & GUIZOT
0+~~30~~ ~~25~~	Beginning of work	2.41	119.82	16.0±	— NOTE: PT LOMA AVE 15 80' instead of 70'
0+50		2.58	119.65	115.8	C38
0+75		3.60	118.63	114.8	C38
1+00		3.2	119.0	114.6	C44
1+50		3.9	118.3	114.2	C41
1+75		4.2	118.0	114.0	C40
2+00		5.4	116.8	113.1 ±	—
2+015	8x6 TEE (City)	5.4	116.8	1130±	—
2+25		5.8	116.4	112.2	C42
2+50		7.1	115.1	110.5	C46
3+00		10.7	111.5	107.3	C42
P		12.26	109.97		
3+25	1.50 111.47	2.82	108.65	105.3	C33
3+50		3.63	107.84	104.4	C34
4+00		4.2	107.3	103.2	C41
4+50		5.5	106.0	101.8	C42
4+75		6.2	105.3	101.1	C42
5+00		7.45	104.0	101.0±	—
5+07	8x6 TEE (City)	7.6	103.9	100.8±	—
5+12	8" GV. (City)	7.7	103.8	100.6±	—
5+25		7.45	102.0	99.6	C24
5+50		8.2	103.3	99.0	C43
6+00		9.5	102.0	97.4	C46

✓

GUIZOT ST (Cont.d.)

			111.47				
6+25				11.1	100.4	96.8	C36
6+50				11.1	100.4	96.4	C40
6+75				11.6	99.9	96.4	C35
P 7+00		5.95	107.03	10.39	101.08	97.5	C36
7+50				4.2	102.8	98.4	C44
7+75				4.0	103.0	98.8	C42
8+00				4.0	103.0	98.8	C42
8+12	8"×6" TEE			4.9	102.1	98.8±	— 4.6 C
8+25				4.4	102.6	98.8	C38
8+50				5.1	101.9	98.3	C36
9+00				5.4	101.6	97.4	C42
9+25				6.66	100.4	96.6	C38
9+50				6.94	100.1	96.4	C37
10+00				4.68	102.4	98.8	C36
P 10+50		11.52	118.33	0.22	106.81		
				11.9	106.4	102.0	C44
11+00				8.8	109.5	105.2	C43
11+17	8"×6" TEE City			8.55	109.78	106.0±	— 8.8 C
11+22	8" G.V. City			8.22	110.11	106.2±	— 8.14 C
11+50				6.5	111.8	107.4	44
12+00				5.1	113.2	109.0	C42

GUIZOT ST. (Cont'd)

		118.33			
12+50			5.34	113.0	109.5
13+00			4.06	114.27	110.8
13+50			3.3	115.0	110.8
14+00			3.6	114.7	110.4
14+22.5	8"x6" TEE (City)		4.50	113.83	110.2±
14+27.5	8" GV (City)		4.90	113.43	110.2±
14+50			4.0	114.33	110.0
15+00			4.4	113.9	109.8
FP	2.46	117.34	3.45	114.88	
15+50			4.81	112.5	108.8
15+75			5.46	111.88	108.0 ~~106.4~~
16+00			6.54	110.8	107.0
16+50			6.8	110.5	106.4
17+00			7.8	109.5	105.2
17+27.5	8"x6" TEE		8.94	108.40	104.6±
17+50			9.2	108.1	104.0
18+00			11.3	106.0	101.8
FP	0.84	105.75	12.43	104.91	99.0
18+50			12.92	102.83	~~99.5~~
19+00			4.50	101.25	97.6

C35	
C35	
C42	
C43	
—	4.26 C
—	4.24 C
C43	
C41	
C38	
C39	
C38	
C41	
C43	
—	8.70 C
C41	
C42	
C38	102.45 3.3 C
C37	DIP 18+61

✓

GUIZOT ST. (Cont'd) & DEVONSHIRE DRIVE

			105.75				
19+50			5.0	100.75	96.4	C44	
20+00			8.1	97.7	93.7	C40	
20+50			12.7	93.1	89.5	C36	93.11 12.64 C
PI	0.60	93.20	13.15	92.60			
21+00			3.7	89.5	85.6	C39	
21+50			6.4	86.8	82.6	C42	
21+90	8"x6" Tee C.I.		8.13	85.1	81.5+	—	85.37 7.87 C
21+95	8" G.V.		7.8	85.4	81.4+	—	8.20 8.00 C
22+00			7.9	85.3	81.0	C43	
22+50			9.3	83.9	79.6	C43	
23+00			10.7	82.5	78.3	C42	
23+50			12.9	80.3	76.5 ~~77.0~~	C38	
TI	12.55	93.27	12.48	80.72			
23+75			13.8	79.5	75.8 ~~76.0~~	C37	
24+00			13.12	80.15	76.2	C40	
24+16 18	45° Bend		12.95	80.32	76.5	C38	
24+19 46	BK (B.C)		11.50	81.77	78.0 ~~77.0~~	C40 C38	11.16 C
24+50 92	AH.						
25+00			9.00	84.27	80.7	C36	8.70 C
25+50			6.36	86.91	83.0	C39	6.08 C
26+00			3.58	89.69	86.1	C36	3.33 C
26+50			1.32	91.95	88.1	C39	1.08 C
TI	8.62	101.75	0.14	93.13			
27+00			7.9	93.9	90.2	C37	7.62 C
ck rim Sew MH.			7.68	94.07 = 94.07	—	pg. 19 FB. 867	
27+50			6.75	95.0	91.6	C34	6.50 C
28+00			6.00	95.75	92.7	C36	5.70 C

GUIZOT ST. & DEVONSHIRE DR. (Cont.d.)

			101.75				
1	28+50			5.83	95.92	92.3	
2	29+00			6.16	95.59	92.0	
3	29+50			6.64	95.11	91.3	
4	29+55.58	E.C.				91.2	
5	30+00			7.36	94.39	90.6	
6	30+50			7.90	93.85	90.1	
7	31+00			8.47	93.28	89.6	
P	31+50.		3.73	97.26	8.22 / 4.60	93.53 / 92.66	89.2
8	32+00				5.88	91.38	87.9
9	32+40				7.22	90.04	86.4
10	32+50				7.72	89.54	86.0
11	32+83	END WORK			8.00	89.26	85.07
	ck. Rim Sew				7.08	90.18 = 90.11	
P	Top F.H.				0.29	96.97	

	Elev. ℄ of pipe
C36	96.23 / 5.52 C
C36	93.89 / 5.86 C
C38	93.45 / 6.30 C
C38	94.67 / 7.08 C
C38	94.14 / 7.61 C
C37	93.53 / 8.22 C
C35	92.94 / 2.32 C
C35	91.90 / 3.36 C
C36	90.35 / 6.91 C
C35	89.84 / 7.42 C
	89.60 / 7.66 C
Pg. 18 FB. 867	

✓

GUIZOT ST. (Cont.d)

6" A.C MAIN ALLEY BLK 1 to ALLEY BLK 5

122.23 (From Pg 15)

2+01.5	90° Bend (City)	4.5					
2+25		4.8	117.4	113.2 ~~112.4~~			
2+50		6.1	116.1	111.9 ~~110.7~~			
3+00		9.7	112.5	108.3 ~~107.5~~			
3+25	111.47	10.2	110.2	106.8 ~~105.9~~			
3+50		11.23	110.24	106.5 ~~104.6~~			
4+00		3.3	108.2	104.2 ~~103.0~~			
4+50		4.6	106.9	102.7 ~~102.0~~			
4+75		5.3	106.2	102.0 ~~101.3~~			
5+00		6.55	104.92				
5+07	90° BEND City End work	6.75	104.72	—			

—

C 42	(0.7 curb) 3.5 42	117.10 5.13	℄
C 42		115.70 6.50	℄
C 42		112.23 10.00	℄
C 36		110.2 1.20	℄
C 37		109.85 1.57	℄
C 40		107.75 3.77	℄
C 42		105.2 6.3	℄
C 42	104.82 6.03 ℄	105.5 6.0	℄
		104.63 6.84	℄

—

✓

GUIZOT ST
(Cont'd)
6" AC. MAIN
Alley BLK 8 to ALLEY BLK 12.

107.03 (from pg. 16)

8+12	90° Bend Cty	3.95			—	103.05 3.98 C	
8+25		3.4	103.6	99.4 ~~99.0~~	C42	102.9 4.10 C	
8+50		3.8	103.2	99.0 ~~98.5~~	C42	103.5 4.5 C	
9+00		4.45	102.6	98.3 ~~97.6~~	C43	101.85 5.18	
9+25		5.40	101.6	97.9 ~~97.0~~	C37	101.43 5.60 C	
9+50		4.88	102.2	98.0 ~~96.8~~	C42	101.71 5.32 C	
10+00		3.37	103.7	99.9 ~~99.0~~	C38	103.53 3.50 C	
10+50	118.33	10.9	107.4	103.1 ~~102.2~~	C43	106.63 11.72 C	
11+00		7.9	110.4	106.1 ~~105.6~~	C43	109.65 8.68 C	
11+17	90° Bend Cty.	7.73	110.60		✓	110.55 7.78 C	

Guizot St Cont'd

6" A.C Main Alley Blk 15 to Alley Blk 18

		118.33 (from pg 17)				
12+~~22~~ 22.5		90° Bend (C.L.) 3.55		—	—	114.73 ✓ Elev. ℄ pipe.
						3.60 C
14+50		3.0	115.3	111.0 ~~110.2~~	C43	114.53 3.80 C
15+00		3.4	114.9	110.7 ~~110.1~~	C42	114.23 4.10 C
15+50	117.34	3.28	114.06	110.2 ~~109.7~~	C39	113.73 3.61 C
15+75		3.35	114.0	110.0 ~~109.7~~	C40	113.50 3.84 C
16+00		4.80	112.54	108.7 ~~107.3~~	C38	113.20 5.14 C
16+50		5.7	111.6	107.6 ~~106.7~~	C40	111.12 6.20 C
17+00		6.7	110.6	106.5 ~~105.5~~	C41	110.0 7.35
17+~~88~~ 27.5		90° Bend (C.L.) 8.00	109.34	—	—	109.38 7.96 C

✓

OZARK St

Imperial North

meters set 17E. from Q St

Stks For Water Meters 28302

B.M.	9.34	148.22		138.88
T.P.	12.13	160.33	0.02	148.20
0+29 M.W.			0.7	159.6 159.3
1+49 M.W.			2.3	158.0 157.5
2+49 M.W.			3.9	156.4 156.0
+63 M.E.			4.0	156.3 156.4
3+03 M.W.			4.5	155.8 155.6
+39 M.E.			4.1	156.2 155.8
+88 M.E.			4.5	155.8 155.4
4+05 M.W.			4.8	155.5 154.8
+61 M.E.			4.6	155.7 154.8
+78 M.W.			5.2	155.1 154.2
5+04 M.E.			6.2	154.1 154.2
+79 M.W.			8.8	151.5 151.1
T.P.	2.12	150.38	12.07	148.26
6+22			2.0	148.4 148.6
+22			0.5	149.9 149.1
7+12 M.W.			9.1	141.3 143.1
+80 M.E.			9.1	141.3 141.2

West
Williams
Vamvakakis
Alexander

7-28-55

L&T Top Con. Pilaster W'ly of 12" x 12" Con. Post Sta. 10+68.08 Ozark St

Co	3	0+00 15 10' S. of N. Prop. on Imperial
Co	5	
Co	4	122-24
Fo	1	202
Co	2	205
Co	4	209
Co	4	215
Co	1	212
Co	9	217
Co	9	218
Fo	1	219
Co	4	222
Fo	1	(5) G.V. (13.7' E. of ℄)
Co	8	(5') F.H. (19.5' E. of ℄)
Fi	8	
Co	1	

7/28/55

	150.38					
T.P. 4.55	145.76	9.17	141.21			
9+42 M.E.		3.0	141.8	139.2	C3 6	323
10+04 M.W.		8.1	137.7	138.5	FO 8	
+32 M.E.		4.6	141.2	138.4	C2 8	335
+34		5.8	140.0	137.5	C2 5 (5') G.V. (7' E OF ℄)	
CHECK B.M.		6.87	138.89=138.88			

Boston St

38th to 39th

Stks For Water Meters

Meters set 22.5 From ℄ St 2640 — 190.

B.M.	2.82	79.40		76.58	
T.P.	0.46	73.79	6.07	73.33	
0+24 M.S.			1.2	72.6	72.9
1+15 M.S.			2.2	71.6	70.8
+20 M.N.			3.7	70.1	70.0
+75 M.S.			3.4	70.4	67.0
+76 M.N.			5.4	68.4	66.5
+82 M.S.			3.7	70.1	66.6
2+22 M.N.			7.4	66.4	63.4
+26 M.S.			7.3	66.5	63.5
+73 M.S.			10.9	62.9	60.4
T.P.	0.02	60.84	12.97	60.82	
3+32 M.N.			6.3	54.5	56.4
+75 M.N.			10.1	50.7	53.6
4+06 M.N.			9.2	51.6	51.6
T.P.	1.87	49.84	12.87	47.97	
+22 M.S.			4.2	45.6	50.4
+60 M.S.			2.6	47.2	48.0
5+27 M.S.			6.1	43.7	43.2

West ⊼
Williams
Varonfakis &
Alexander

7-28-55

S.E.B.P. 38TH + NATIONAL

0+00 IS E. PROP. 38TH ST.

$F0 \frac{3}{}$	
$C0 \frac{8}{}$	3821
$C0 \frac{1}{}$	3820 -24
$C3 \frac{4}{}$	3827
$C1 \frac{9}{}$	3830
$C3 \frac{5}{}$	3831
$C3 \frac{0}{}$	3836
$C3 \frac{0}{}$	3837
$C2 \frac{5}{}$	3843
$F1 \frac{9}{}$	3852
$F2 \frac{9}{}$	
$C0 \frac{0}{}$	3866
$F4 \frac{8}{}$	3867
$F0 \frac{8}{}$	3875
$C0 \frac{5}{}$	38.85

BOSTON ST. CONT.

		49.84			
5+72 M.S.			14.7	35.1	40.0
T.P.	0.25	39.17	10.92	38.92	
T.P.	3.60	30.37	12.40	26.77	
CHECK T.B.M.			10.02	20.35 = 20.31	

7/28/55

F 4 9

3891

P.P. S.W. Cor. 39 & Z. St.

"Z" St.
37th To 38th.
(2) Wat Mets

BM		6.31	45.16	38.85	
6+56	F.H.	G.V.	8.84	36.32	36.70
6+56	F.H.		8.6	36.6	37.2
6+50	So.		8.9	36.3	37.1
4+27	So.		3.1	42.1	36.9
3+57	So.		10.4	34.8	31.2
P		0.56	33.52	12.20 32.96	
2+33	N.		8.2	25.3	29.3
2+10	N.		8.1	25.4	28.3
1+48	So.		6.3	27.2	26.4
Ck BM				7.60	26.12 = 26.20

Aug. 1 1955
West
& party

See FB 901 P68
TBM Top SW FH 38th & Z

FO4
FO6 Mets std 75 Bk 20' curb
FO8 (Orig Mets are located 275 from E St)
C52
C06
F10
F29
C08
NW Cor

Z ST
37TH To 38TH
② WAT. MET.S

8/1/55
WEST
E party

25

BM	0.21	39.06		38.85	
2+73 S			11.3	27.8	31.3
2+90 N			0.0	39.1	3.16
D 3+15 S	5.30	31.71	12.71	26.35	30.1
3+36 S			5.7	26.0	29.5
3+87 S			6.3	25.4	28.2
4+02 S			6.6	25.1	27.8
4+23 N			1.4	30.3	28.1
4+75 S			7.0	24.7	25.8
6+42 N			7.0	24.7	22.3
6+45 F.H.			10.4	21.3	21.5
" F.H. G.V.			10.20	21.51	21.4
CK BM			11.38	20.33	=20.31

F35
C75
F32
F35
F28
F27
C22
F1'
C24
F02
C01
Nail in pole

DATE St 33rd to Felton
Felton St Date to 100' South
Proposed PL.

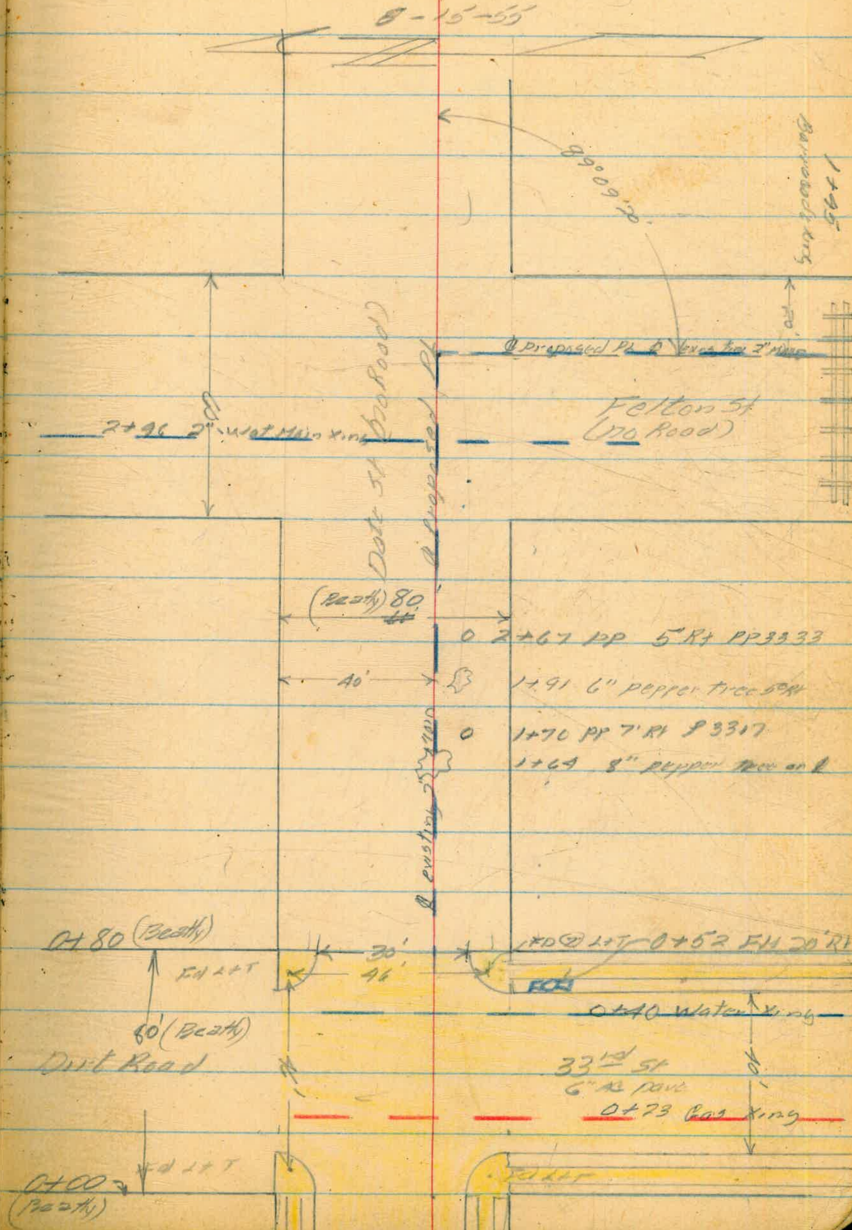
(Beatty)
3+30.29
~~3+20.29~~ Date = 0+40 Felton ℄ 89°09'20" Rt

2+35
~~2+25~~ POT

1+90
~~1+80~~ POT

0+00 Wly prop Line 33rd St

West
Williams
Varontakis
Alexander



Date St
℄ Profile

	4.53	231.06		226.53
	8.42	239.33	0.15	230.91
0+10 ~~0+00~~			5.15	234.1
+60 ~~+50~~			5.00	234.3
+80 ~~+70~~			4.85	234.4
+93 ~~+83~~			1.5	237.8
1+10 ~~1+00~~ } etc.			2.2	237.1
+50			5.2	234.1
	0.33	231.21	8.45	230.88
2+00			3.1	228.1
+25			6.9	224.3
	4.09	222.79	12.51	218.70
+50			11.2	211.6
	3.97	213.66	13.10	209.69
2+81			18.1	195.6

Note: Add 10' to all stations

Reduced by A.E. Mathison 8-23-55

6.5 / 40'Lt

NW BP [illegible] 225.39

NW BP Bancroft & Elm

Wly prop Line 33

℄

end AC pave

2.5/35'Lt 2.8/28 3.6/25 3.3/14 1.4/11'Lt 1.8/20'Rt

3.0/35'Lt Conc Rock Wall 2.2/20'Rt

5.6/30' 2.8/26 4.3/16'Lt 5.6/20'Rt

4.0/40'Lt 2.4/6'Rt 3.0/20'Rt

8.2/40'Lt 7.7/23 5.5/16'Lt 7.9/20'Rt

6.7/40' 6.8/30' 8.1/13.5 14.4/12'Rt 11.1/20'Rt

10.7/40'Lt 17.9/6'Rt 8.2/20'Rt

	213.66		
0.21	200.95	12.92	200.74
3+00		8.1	192.9
1.21	195.84	6.32	194.63
3+20 =0+40 Fulton Date		11.3	184.5
Fulton			
0+10			
+50		10.1	185.7
13.07	198.65	10.26	185.58
+75		9.5	189.2
12.41	210.98	0.08	198.57
1+00		13.2	197.8
12.48	222.44	1.02	209.96
6.44	228.47	0.41	222.03
1+44		5.7	222.8
+50		6.08	222.4
13.03	232.59	8.91	219.56
7.06	239.53	0.12	232.47
2.74	229.35	12.42	227.11

3.3 / 10' | 3.9 / 35'Lt | 12.2 / 10'Lt | 2.8 / 8'Rt | 0.9 / 20'Rt

2×2 Hub & Tack 2+97 3'Rt

8.3 / 40'Lt | 11.6 / 22' | 8.6 / 20'Rt

6.7 | 17.0 / 20'Lt | +2.7 / 28Rt | +8.3 / 40'Rt

7.7 / 20'Lt | 10.6 / 10'Lt | 6.1 / 9Rt | +15 / 21 | +1.1 / 40'Rt

10.9 / 20'Lt | +12.4 / 40'Rt

+0.4 / 20'Lt | 14.2 / 7'Rt | 12.6 / 15'Rt | 9.7 / 25' | 2.2 / 40'Rt

5.6 / 20'Lt | 5.0 / 40'Rt

Begin AC pave
Turn on South rim sewer mh Cedar & Fulton

-2.80 226.55 = 226.53

DATE ST

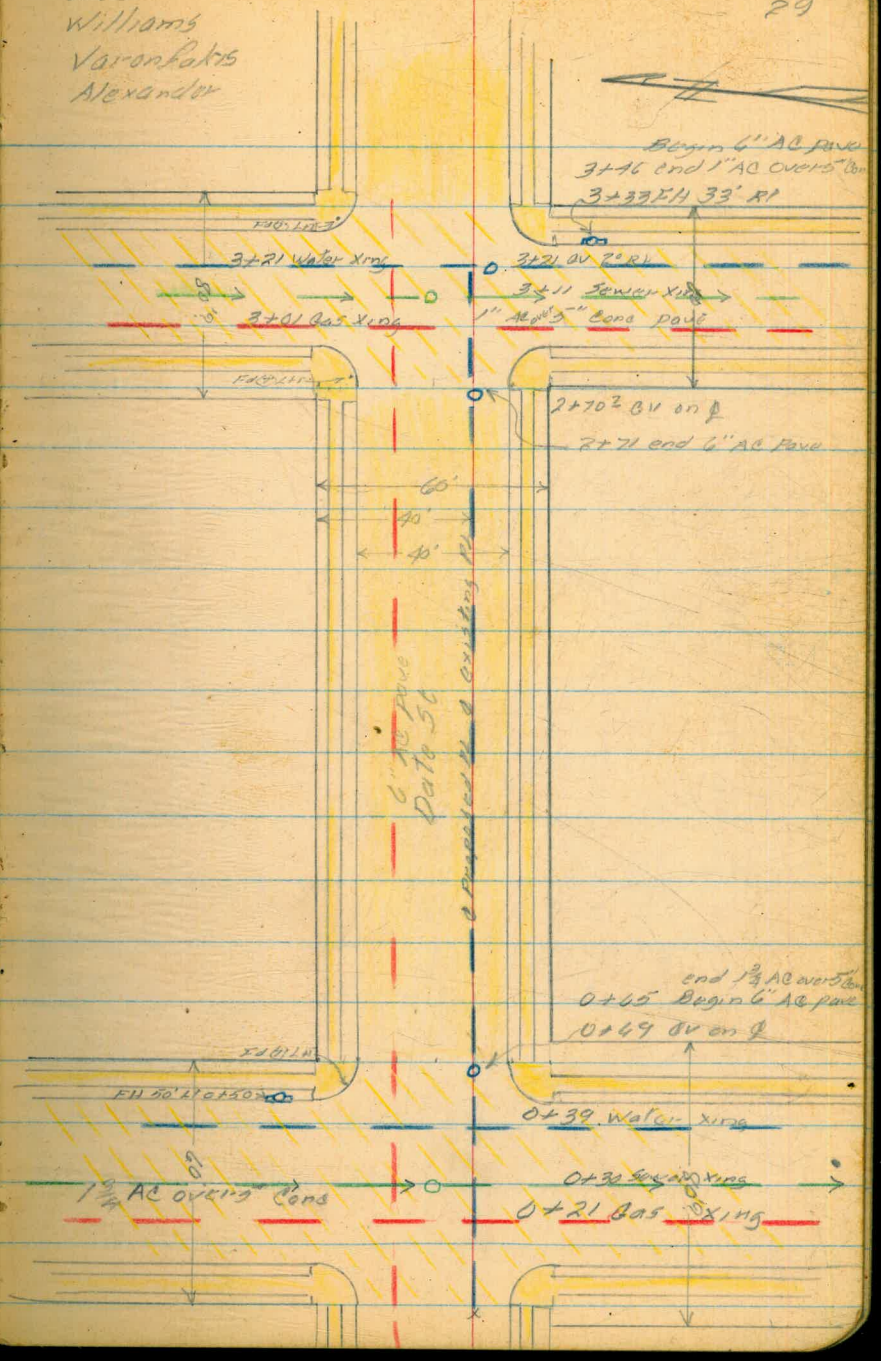
29th to 75' E of Dale St

Proposed P2

Group 26

4+05.77	75' E of Ely Prop Line Dale St
3+77.77	POT
0+53	POT
0+00	Wly prop Line 29th St

West
Williams
Varonkakis
Alexander



Date St
℄ profile

	0.57	237.61		237.04	BM NE BP Dale + Date St
	1.98	226.47	13.12	224.49	
0+00			6.25	220.2 +6.0 To Flow	Wly prop Line 29th St
+30			5.42	221.1	Top Sly rim Sewer MH 10'Lt
+50			5.42	221.1	
+67			5.16	221.3	
1+00			3.43	223.1	
+50	12.24	238.58	0.13	226.34	
2+00			9.07	229.5	
+50			5.78	232.8	
+70 ?			4.51	234.1	
3+00			3.82	234.8 +7.0' To Flow	Top Sly rim Sewer MH 9' Lt
+11			3.27	235.3	
+50			4.05	234.5	
4+00			3.32	235.3	
+05 TT			3.27	235.3	75' East of Ely prop Line Dale
			1.56	237.02 = 237.04	

Reduced by AE MATHISON 10-10-35 [illegible]

53
14
67

QUINCE ST
HALLER TO NILE

STKS for meters

West
Williams
Varonfakis
Alexander

0+00 FH, prop line Vancouver

meters set 28' from ℄ and 22½ in Sly Side Quince between Vancouver & Nile — 12041 L — 8-24-55

10.55 290.24 279.69 — BM NE BP Nile & Quince

Vancouver to Nile

3+61 MN	9.7	280.5	279.9	℄ O 6	
3+56 MS	11.6	278.6	278.8	F O 3	35
2+54 MS	7.9	282.3	281.9	℄ O 4	3561
1+23 MS	1.3	288.9	288.3	℄ O 5	3591
	8.86	298.98	912	290.12	
Top CV Cap 0+05	6.87	292.11	291.7	℄ O 4	
0+05 ⓒ CV	6.6	292.4	291.7	℄ O 7	
0+05	6.9	292.1	292.2	E O 1	Flange of existing FH 21² from ℄ St
0+05 ⓒ FH	6.6	292.4	292.2	℄ O 3	
0+45 MN	1.4	294.6	293.4	℄ 1 2	3005 Vancouver
1+86 MS	5.9	293.1	291.4	℄ 1 7	2958
2+71 MS	9.2	289.8	285.4	℄ 4 1	2966
2+90 MN	9.2	289.8	284.0	℄ 5 8	3644
Top existing CV 3+20 Vancr	13.3	285.7	280.3	℄ 5 1	
3+20 ⓒ CV	13.0	286.0	280.3	℄ 5 1	
	11.78	287.20 =		287.23	TBM Power pole

CORDOVA Dr. Hill St to 275' North

Preliminary Survey

2+75 end of Work

0+60 POT North line Hill St

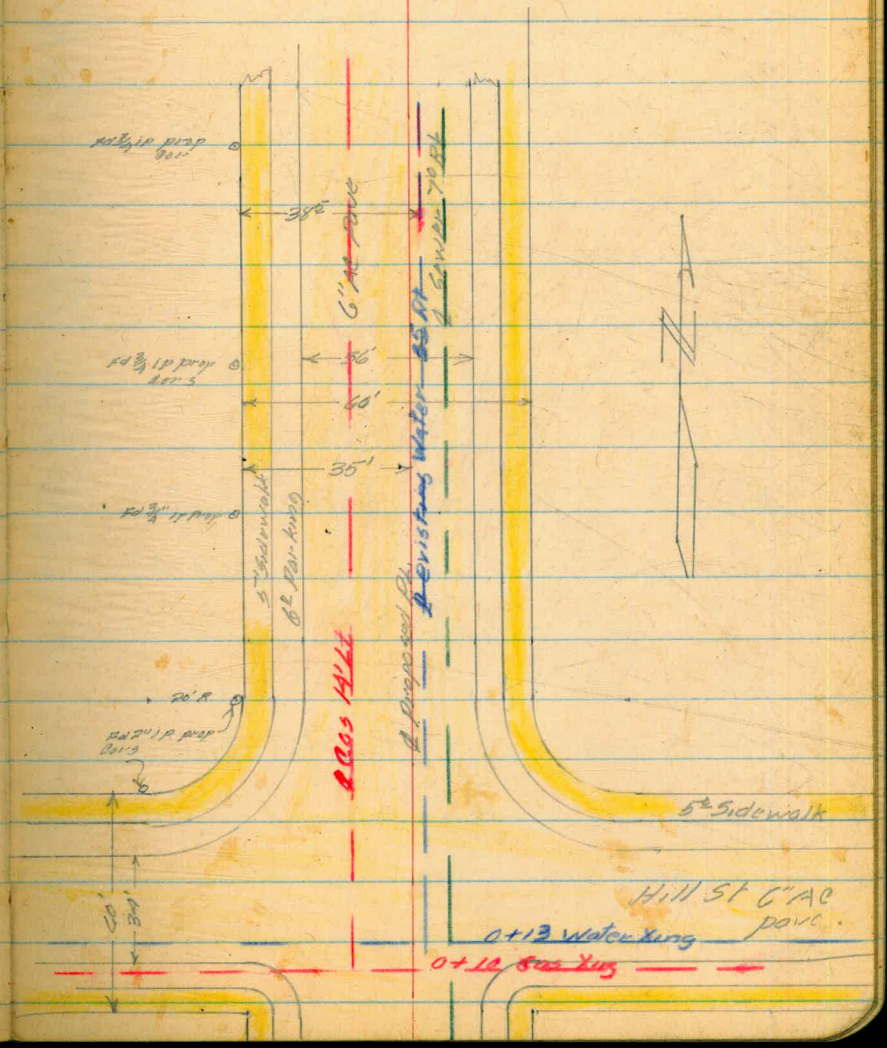
0+00 South prop line Hill St

West
Williams
Varanfakis
Kellhofer

2679-L

32

4/26/56

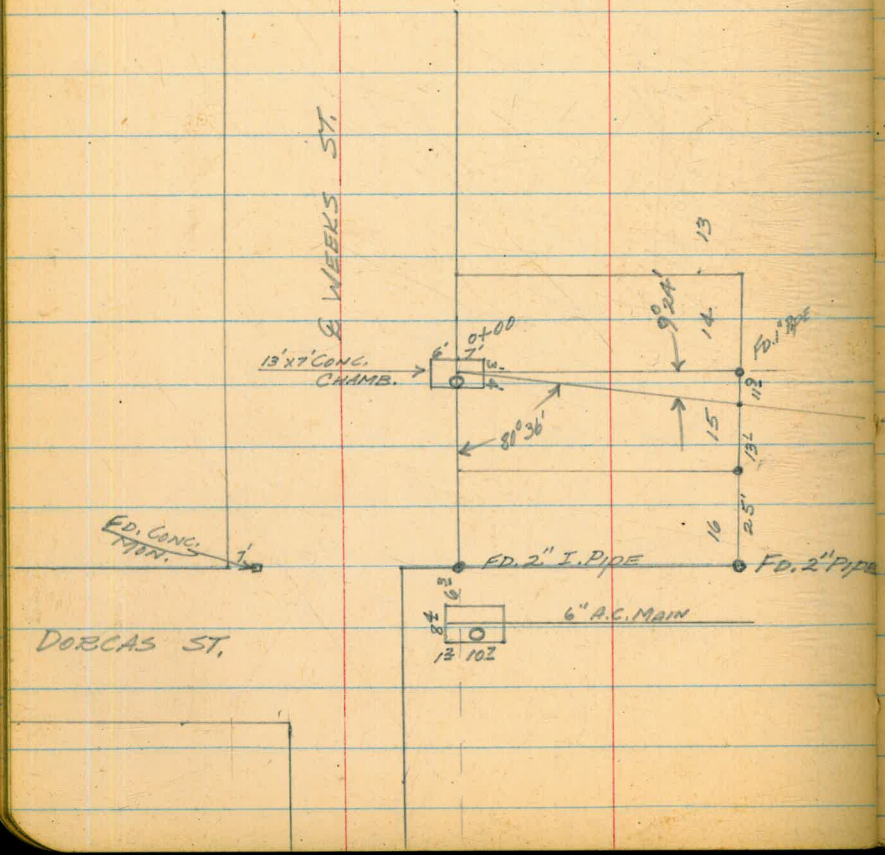


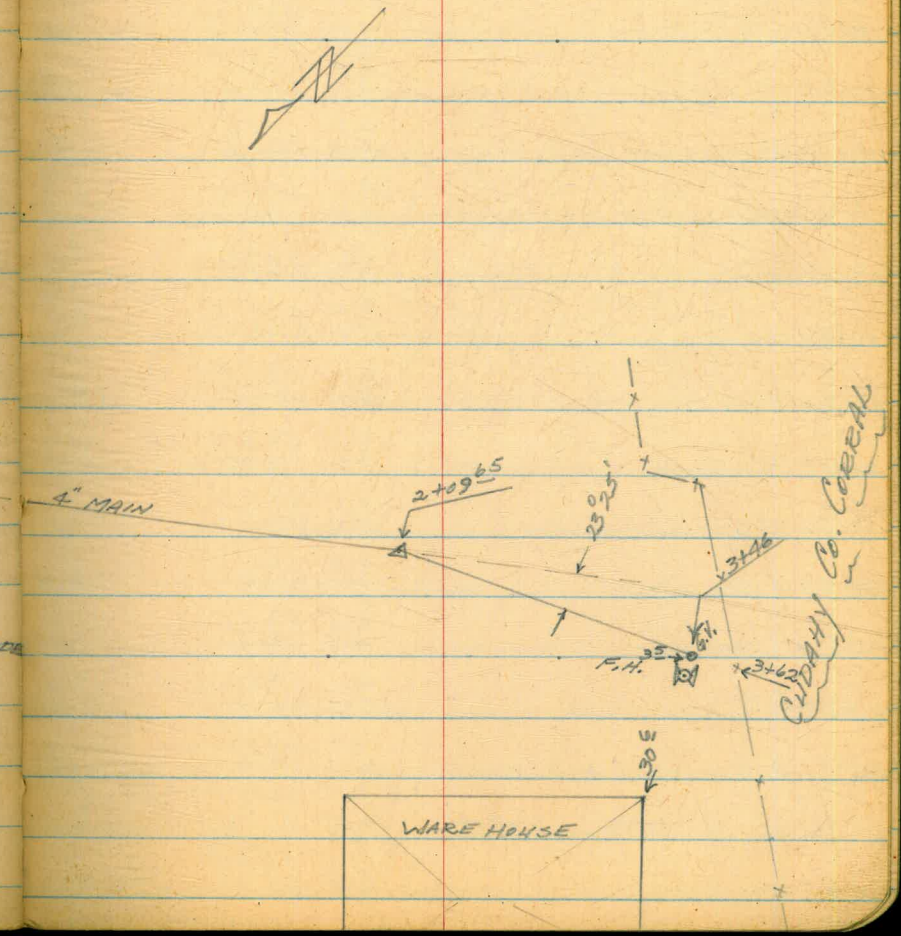
℄ Profile

	12.57	53.97		41.40	BM SE BP Hill St & Sunset Cl. Stg Blvd
	13.22	66.52	0.67	53.30	
0+00			6.14	60.38	South prop Line Hill St
+08	Tapp. Sleeve & G.V.			60.2	56.5 C3.7
+13			6.11	60.11	56.6 C3.5
+30			5.8	60.7	56.7 C4.0 Cutter Line
+46			6.14	60.38	Cutter Line
+50			6.13	60.39	56.8 C3.6
1+00			4.43	62.09	58.5 C3.6
+12			4.1	62.4	59.0 C3.4
+58			3.48	63.04	57.4 C3.6
2+00			3.12	63.40	Reduced by Levels 60.0 C3.4
+50			2.66	63.86	60.5 C3.4
+75			2.30	64.22	60.7 C3.5
3+00		2" B.O. Assy.	2.1	64.4	61.0 C3.4
	1.35	65.77	2.10	64.42	
	1.09	54.42	12.44	53.33	
	1.61	44.96	11.07	43.35	
			8.00	36.96 =	37.02 SE BP Froude & Sunset Cliffs Blvd

4" WATER MAIN LOCATION
BETWEEN LOTS 14 & 15 - WEEKS ST. & DORCAS ST.

6/28/56
SHOREY
KEMP
VARONFAKIS





WATER METERS
ALLEY, BLK. 17; NORMAL HGHTS
E. of 34th ST, COLLIER TO COPLEY

0+00 = S/L COLLIER

	5.99	398.17			
BM	~~5.78~~	~~397.96~~		392.18	
	4.54	399.39	3.32	394.85	
TP	~~4.81~~	~~399.48~~	~~3.32~~	~~394.64~~	
			5.5	393.9	
0+73 E.			~~5.6~~	~~393.9~~	391.6
			5.0	394.0	
1+08 W.			~~5.1~~	~~394.4~~	393.0
			4.9	394.5	
1+24 W.			~~5.0~~	~~394.5~~	393.3
1+30 E.			~~4.4~~	~~394.8~~ 394.8	393.1
1+82 W.			~~4.6~~	~~394.9~~	393.5
			4.5	394.9	
1+82 E.			4.8 ~~4.9~~	394.6 ~~394.6~~	393.3
			4.8	394.6	
2+33 E.			~~4.9~~	~~394.6~~	393.4
			4.6	394.8	
2+42 W.			~~4.6~~	~~394.9~~	393.7
			4.6	394.8	
2+96 W.			~~4.7~~	~~394.8~~	393.8
			5.0	394.4	
2+97 E.			~~5.1~~	~~394.4~~	393.7
			4.9	394.5	
3+29 E.			~~5.0~~	~~394.5~~	393.7
			4.5	394.9	
3+41 W.			~~4.6~~	~~394.9~~	394.0
			5.0	394.4	
3+86 E.			~~5.1~~	~~394.4~~	393.7
			4.9	394.5	
4+05 W.			~~5.0~~	~~394.5~~	393.7
			4.8	394.6	
4+29 W.			~~4.7~~	~~394.6~~	393.6
			4.8	394.6	
4+46 E.			~~4.9~~	~~394.6~~	393.5
			4.8	394.6	
4+48 E.			~~4.9~~	~~394.6~~	393.5
4+71 W.			4.5 ~~4.5~~	~~395.0~~ 394.9	393.5
4+89 E. TP	~~2.74~~	~~397.89~~	~~4.62~~	~~394.86~~	393.3
			4.5	394.9	
			4.6	394.8	
5+28 E.			~~3.0~~	~~394.8~~	393.2

7/12/56
SHOREY
KEMP
VARONFAKIS
SMITH

S.E.B.P. 34th ST. & COPLEY

℄ VERT. RISER SET
5 82 FROM ℄ ALLEY

RE-STAKED 7/25/56

~~℄ 3~~ 2 3	
~~℄ 4~~ 1 4	
~~℄ 2~~ 1 2	
~~℄ 2~~ 1 2	
~~℄ 5~~ 1 5	
~~℄ 3~~ 1 3	
~~℄ 2~~ 1 2	
~~℄ 3~~ 1 1	
~~℄ 0~~ 0 7	
~~℄ 0~~ 0 8	
~~℄ 0~~ 0 9	
~~℄ 0~~ 0 7	
~~℄ 0~~ 0 8	
~~℄ 0~~ 1 0	
~~℄ 1~~ 1 1	
~~℄ 1~~ 1 1	
~~℄ 1~~ 1 4	
~~℄ 1~~ 1 6	
~~℄ 1~~ 1 6	

ALLEY BLK. 17
(CONT'D)

7/12/56
SHOREY
KEMP
VARONFAKIS
SMITH

		399.39 ~~397.80~~				
5+50 W.			4.5 ~~2.9~~	394.9 ~~394.9~~	393.4	~~CT~~ 5, 1 5
5+78 E.			4.7 ~~3.1~~	394.7 ~~394.7~~	393.1	~~C 6~~ 1 6
5+89 W.			4.5 ~~2.9~~	394.9 ~~394.9~~	393.3	~~C 6~~ 1 6
6+39 W.			4.7	394.7	392.9	C 1 8
~~CK. BM.~~			~~5.62~~	~~392.18~~ =	~~392.18~~	
TP	3.11	397.79	4.71	~~394.68~~		
CK. BM.			5.59	392.20 =	392.18	

SEE PG. 35

WATER METERS
S.E. COR. MYRTLE & WILSON

BM	10.63	313.57		302.94	
			5.6	308.0	303.9
			5.6	308.0	303.9
CK. BM.	12.90	315.84	10.63	302.94	=302.94
TP	12.96	328.32	0.48	315.36	
CK. BM.			0.78	327.54	=327.55

7/13/56
SHOREY
KEMP
VARONFAKIS
SMITH

B.P. N.W. COR. 36th & MYRTLE

C4 1 2 WATER METERS

C4 1 & VERT. RISER 9° FROM PROP.

NWB.P. 36th & DWIGHT

NOTE: CK. GRD. PROFILE 12870-L

WATER METERS
BOND ST.; BALBOA TO GRAND AVE.
0+00 = S/L BALBOA

B.M.	8.23	12.25	4.02	
⑤ F.H. 0+11		0.8	11.5	12.2
1+32 W.		3.5 ~~3.9~~	8.8 ~~8.4~~	7.6
1+98 W.		4.4	7.9	6.5
4+21 E.		6.5	5.8	5.1
4+91 E. TP	3.18	8.62 6.81	5.44	4.6
5+69.5 ⑤ F.H.		3.4	5.2	5.4
5+85 W.		3.8	4.8	4.0
6+39 E.		4.3	4.3	4.1
7+21 W.		4.7	3.9	3.6
7+48 E.		5.0	3.6	3.6
7+52 W.		5.0	3.6	3.5
7+99 W.		5.4	3.2	3.4
8+79.5 ⑤ F.H.		5.6	3.0	4.2
8+79 W.		5.8	2.8	3.1
9+52 W.		5.7	2.9	3.4
10+71 W.		6.2	2.4	3.9
CK. BM		4.61	4.01 = 4.02	

7/13/56
SHORRY
KEMP
VARONFAKIS

7" CONC. MON. S.W. COR. BOND & MAGNOLIA

FO^1 TO FLANGE	
C_1^2	"4562"
~~CO^8~~	
$C1^4$	"4548"
CO^7	"4511"
CO^9	"4503"
FO^2 TO FLANGE	
CO^8	"4484"
CO^2	"4475"
CO^3	"4458"
CO^6	"4457"
CO^1	
FO^2	"4450"
$F1^2$	
FO^3	"2687" HORNBLEND
FO^5	"4434"
$F1^5$	"4414"

WATER METERS

HORNBLEND ST.; PICO TO FIGEROA

0400= E/L PICO ST.

7/16/56
SHOREY
VARONFAKIS
SMITH

BM	3.71	7.73		4.02	
P	5.53	9.49	3.77	3.96	
0+76 N.			4.4	5.1	5.1
1+30 N.			4.6	4.9	5.1
1+30 S.			4.4	5.1	4.6
1+81 N.			4.5	5.0	5.0
2+28 N.			4.5	5.0	4.8
2+64 N.			4.5	5.0	4.7
3+07 N.			4.5	5.0	4.6
3+49 S. F.H. Ⓔ			4.2	5.3	5.2
4+29 S.			5.3	4.2	3.8
4+44 S.			5.4	4.1	3.7
4+93 N.			5.7	3.8	4.0
5+00 S. TP	5.09	8.79	5.79	3.70	3.5
5+32 N.			4.8	4.0	3.9
6+85 N.			5.3	3.5	3.7
7+29 N.			5.0	3.8	4.1
7+72 N.			4.9	3.9	4.2
8+30 N.			4.5	4.3	4.4
8+36 S.			4.2	4.6	3.9
8+68 S.			3.9	4.9	4.1

7" Conc. Mon. S.W. Cor. Bond & Magnolia

"2612"

Co^{9} SET & VERT. RISER 29' FROM TURNAROUND RADIUS PT.

Fo^{2} "2620"

Co^{5} SET & VERT. RISER 19' & ST.

Co^{0} "2630"

Co^{2} "2636"

Co^{3} "2644"

Co^{4} "2652"

Co^{1} TO FLANGE

Co^{4} "2667"

Co^{4} "2661"

Fo^{2} "2676"

Co^{2} "2681"

Co^{1}

Fo^{3} "2704"

Fo^{3} "2710"

Fo^{3} "2718"

Fo^{1} "2724"

Co^{7} "2725"

Co^{8} "2735"

WATER METERS
HORNBLEND ST.
(CONT'D)

8.79

8+85 N.		3.7	5.1	4.6
9+49 N.		3.1	5.7	4.9
9+81 S.		3.1	5.7	4.5
9+86 N.		2.8	6.0	5.1
10+24 N.		2.6	6.2	5.2
TP	5.81	8.54	6.06	2.73
CK. BM			4.54	4.00 = 4.02

7/16/56
SHOREY
VARONFAKIS
SMITH

$Co_{\bar{5}}$	"2736"
$Co_{\bar{8}}$	"2744"
$C_{1\bar{2}}$	"2751"
$Co_{\bar{2}}$	"2752"
$C_{1\bar{0}}$	"2758"

ALLEY BLK. 155
N. of EMERALD, E. of OCEAN BLVD
④ STK's & GRD. 6" A.C. MAIN

7/16/56
SHOREY
VARONTAKIS
SMITH

S.W.B.P. DIAMOND & MISSION BLVD

B.M.	3.68	34.60		30.92	
TP	3.66	31.08 (By City)	7.18	27.42	
0+68.5 E.H. TEE					
⑤			5.5	25.6	25.5 $C0^{\frac{1}{2}}$ TO FLANGE
0+80. BEGIN WORK			5.6	25.5	21.4 $C4^{\frac{1}{2}}\pm$
1+00			5.2	25.9	21.7 $C4^{\frac{2}{2}}$
1+50			4.4	26.7	22.6 $C4^{\frac{1}{2}}$
2+00			3.7	27.4	23.5 $C3^{\frac{9}{2}}$
2+50			2.9	28.2	24.4 $C3^{\frac{8}{2}}$
3+00			2.1	29.0	25.3 $C3^{\frac{7}{2}}$
3+25			1.7	29.4	25.7 $C3^{\frac{7}{2}}$
3+50 END WORK		{ CITY TO CONN. EXIST. 6" C.I.	1.3	29.8	26.2 $C3^{\frac{6}{2}}\pm$ NOT MK'D
TP	6.75	36.48	1.35	29.73	
CK. B.M.			5.52	30.96 = 30.92	

WATER METERS
31.08

0+80 E.					
0+80 W.	1" METER		5.7	25.4	24.5 $C0^{\frac{8}{2}}$
1+75 W	1" METER		4.2	26.9	25.7 $C1^{\frac{2}{2}}$
1+46 E.	2" METER		4.6	26.5	25.2 $C1^{\frac{3}{2}}$
2+15 W.			3.6	27.5	26.5 $C1^{\frac{0}{2}}$
2+70 W.			2.7	28.4	27.6 $C0^{\frac{8}{2}}$
2+80 E.			2.5	28.6	27.8 $C0^{\frac{8}{2}}$
3+17 W.			1.8	29.3	28.5 $C0^{\frac{8}{2}}$

26.4
1.25
25.15

RILEY ST.
AZUZA TO COLUSA ST.
(5) STK'S & GRD

TBM	11.65	39.70	28.05	
0+35 BEGIN WORK			11.7	28.0	23.4
0+40 G.V. BY CITY			11.7	28.0	23.5
0+50			11.6	28.1	23.6
0+55 F.H. TEE			11.6	28.1	23.8
(3)			10.5	29.2	
1+00			10.9	28.8	25.0
1+50			9.8	29.9	26.3
2+00			8.7	31.0	28.0
2+50			6.9	32.8	29.7
3+00			5.1	34.6	31.4
3+50			3.7	36.0	33.2
4+00			1.6	38.1	34.7
TP	11.56	50.33	0.93	38.77	
4+50			10.6	39.7	36.2
5+00			8.9	41.4	37.7
5+15 F.H.G.V.			8.5	41.8	38.2
5+20 F.H. TEE			8.3	42.0	38.4
(3)			7.7	42.6	
5+50			7.6	42.7	39.2
6+00			5.9	44.4	40.8

1/17/56
SHOREY
VARONFAKIS
SMITH

B.R.: SPIKE & AZUZA & RILEY

OUT TO EXIST.

$C4^{5}$

$C4^{5}$

$C4^{3}$

$C5^{4}$. CO^{5} TO FLANGE

$C3^{8}$

$C3^{6}$

$C3^{0}$

$C3^{1}$

$C3^{2}$

$C2^{8}$

$C3^{4}$

$C3^{5}$

$C3^{7}$

$C3^{6}$

$C3^{6}$

$C4^{2}$ CO^{0} TO FLANGE

$C3^{5}$

$C3^{6}$

RILEY ST. (CONT'D)

7/17/56.
SHOREY
VARONFALOS
SMITH

		58.33				
6+50			4.6	45.7	42.3	$C_3\frac{4}{-}$
7+09			3.3	47.0	43.8	$C_3\frac{3}{-}$
TP	7.13	56.97	0.49	49.84		
7+50			8.3	48.7	45.3	$C_3\frac{4}{-}$
8+00			6.5	50.5	46.7	$C_3\frac{8}{-}$
8+50			5.4	51.6	48.3	$C_3\frac{3}{-}$
9+00			3.5	53.5	49.8	$C_3\frac{7}{-}$
9+25			3.2	53.8	50.6	$C_3\frac{2}{-}$
9+50			2.2	54.8	51.5	$C_3\frac{3}{-}$
9+58 G.V.			1.8	55.2	51.8	$C_3\frac{4}{-}$
9+63 END WORK			1.6	55.4	52.0	CUT TO EXIST.
TP	0.30	46.99	10.28	46.69		
TP	0.15	37.24	9.90	37.09		
C.K. TBM			9.22	28.02 = 28.05		

WATER METERS

		39.70				
1+60 N.			7.1	32.6	31.0	$C_1\frac{6}{-}$
~~1+48 N.~~			~~7.9~~	~~31.8~~	~~30.6~~	~~$C_1\frac{2}{-}$~~
						"5520"
2+15 N.			5.8	33.9	32.7	$C_1\frac{2}{-}$ "5530"
2+80 N.			2.9	36.8	34.7	$C_2\frac{1}{-}$ "5538"
3+06 N.			2.0	37.7	35.5	$C_2\frac{2}{-}$ "5546"
3+48 N.			1.3	38.4	36.8	$C_1\frac{6}{-}$ "5548"
3+94 N.		50.33	10.3	40.0	38.3	$C_1\frac{7}{-}$ "5556"
4+48 N.			7.9	42.4	40.1	$C_2\frac{3}{-}$ "5562"
5+32 N.			4.4	45.9	42.1	$C_3\frac{8}{-}$ "5602"
5+31 S.			7.5	42.8	41.6	$C_1\frac{2}{-}$ "5605"
6+21 S.			4.9	45.4	44.5	$C_0\frac{9}{-}$ "5615"
6+50 N.			3.0	47.3	45.9	$C_1\frac{4}{-}$ "5628"

RILEY ST.
(CONT'D)
WATER METERS

50.33

6+69 S.	3.7	46.6	46.0	C_0^6
7+20 S.	2.6	47.7	47.6	C_0^1
56.97				
7+47 N.	7.2	49.8	49.0	C_0^8
7+76 S.	7.0	50.0	49.5	C_0^5
8+00 N.	4.8	52.2	50.1	C_2^1
8+46 S.	3.9	53.1	51.7	C_1^4

7/17/56
SHOREY
VARONAKIS
SMITH

C_0^6	"562.5"
C_0^1	"5637"
C_0^8	"5648"
C_0^5	"5645"
C_2^1	"5650"
C_1^4	"5653"

FRIARS RD.

LAKE TO U.S. HWY. 395

(5) STK'S 6" A.C. MAIN

BM		9.89	35.74	25.85	
B.C. 1+00	BEGIN WORK 2" B.O. Assy.		9.4	26.3	21.9
1+25			9.2	26.5	22.0
1+50			9.2	26.5	22.1
1+75			8.7	27.0	23.0
2+00			8.2	27.5	23.8
2+25			7.5	28.2	24.7
2+50			6.0	29.7	25.6
2+75			5.5	30.2	26.5
E.C. 01 2+90			4.9	30.8	27.0
3+00			4.5	31.2	27.3
3+50			2.7	33.0	29.2
TP 4+00		8.45	43.85	0.34 35.40	30.9
4+50			6.6	37.3	32.7
4+92	F.H. TEE		5.2	38.7	34.2
(5)			5.2	38.7	
5+00			4.9	39.0	34.4
5+50			4.1	39.8	35.2
5+61	6" G.V. By City		3.8	40.1	35.0
5+66	6" x 4" TEE By City Δ PT. 2°15' RT.		3.5	40.4	35.0

7/18/56

SHOREY

VARONFAKIS

SMITH

L & T 1400 13.75 LT.

C4.4

C4.5

C4.4

C4.0

C3.7

C3.5

C4.1

C3.7

C3.8

C3.9

C3.8

C4.5

C4.6

C4.5

C4.5 TO FLANGE

C4.6

C4.6

C5.1

CUT TO EXIST. 4" C.I. (38.51)

FRIARS RD.
(CONT'D)

7/18/56
SHOREY
VARONFAKIS
SMITH

43.85

6+00			3.7	40.2	34.7
6+24 END WORK	8"XL" RED. CONN. BY CITY		4.5	39.4	34.5
CK. TBM				=	38.51
TP	1.05	35.39	9.51	34.34	
CK. B.M.			9.52	25.87	= 25.83

WATER METERS
35.74

1+10 E.			9.1	26.6	25.5
1+20 W. (3 METERS)	1" MET.		11.7	24.0	25.0
			9.7	26.0	25.0
1+75 NWLY					
3+76 S.			1.6	34.1	33.0
		43.85			
5+95 S.	1" METER		5.2	38.7	37.7

C 5 5

CUT TO EXIST. 8" C.I.

R/W MON (DESTROYED)

C 1 1

F 1 0

C 1 0

SET 6' VERT. RISER
15' RT. & 55' LT.

C 1 1

C 1 0

WATER METERS
OPAL ST.; GRESHAM TO FANNIEL
0+00 = E/L GRESHAM

BM	1.10	162.38		161.28	
TP	13.06	164.57	10.87	151.51	
5+64 N.			12.8	151.8	150.8
5+04 N.			11.24	153.33	152.4
4+61 N.			10.17	154.40	153.6
4+19 N.			8.45	156.12	154.7
3+66 N.			6.66	157.91	156.3
3+28 N.			5.08	159.49	157.2
2+79 N.			3.74	160.83	158.2
2+28 N.			3.27	161.30	159.0
1+77 N.			2.77	161.80	159.6
1+18 N.			2.33	162.24	160.0
0+96 N.			2.27	162.30	160.2
0+80 @ G.L.			3.57	161.0	160.6
CK. ELEV.			3.85	160.72	=160.70
TBM	3.64	164.34			160.70
1+30 S.			4.5	159.8	158.3
2+00 S.			4.9	159.4	158.9
2+23 S.			5.1	159.2	158.6
2+57 S.			5.3	159.0	158.1
2+96 S.			5.5	158.8	157.4
3+48 S.			6.6	157.7	156.1
3+98 S.			8.2	156.1	154.7
4+48 S.			9.8	154.5	153.1
5+00 S.			11.3	153.0	151.5
5+48 S.			12.6	151.7	149.9

9/23/56
BEATTY
SHOREY
SMITH

TOP S.E. F.H. TOURMALINE & FANNIEL

C_1^0	"1304"	OPAL	
C_1^1	"1312"		SET & VERT. RISER 21' LT. & RT
C_0^8	"1318"		
C_1^4	"1324"		
C_1^6	"1334"		
C_2^3	"1340"		
C_2^6	"1348"		
C_2^3	"1356"		
C_2^2	"1364"		
C_2^2	"1372"		
C_2^1	"3060"	GRESHAM	
C_0^4			

Top of EXIST. PAVT @ 0+00 & ST.

Top of EXIST PAVT @ 0+00 & ST.

8/10/56 SHOREY
~~KEMP~~
PAULSON

C_1^5	
C_0^5	
C_0^6	
C_0^9	
C_1^4	
C_1^6	
C_1^4	
C_1^4	
C_1^5	
C_1^8	

WATER METERS
LORING ST.; LAMONT TO 500' ELY.

7/24/56
SHOREY
SMITH

BM	12.78	219.63	206.85	
0+10 F.H. (5)		10.2	209.4	209.4
0+10 F.H. G.V. (4)		10.3	209.3	209.0
1+02 W.M.S.		6.2	213.4	212.0
TP	7.95	227.11	0.47 219.16	
1+87 S		7.3	219.8	218.5
2+23 S.		6.2	220.9	220.3
2+69 S.		5.2	221.9	221.0
3+41 S.		4.2	222.9	221.4
4+00 S.		4.3	222.8	221.7
4+86 3 G.V. & B.O. (4)		3.8	223.3	223.1
4+97 W.M.		3.8	223.3	222.1
TP	0.94	220.90	7.15 219.96	
TP	10.12	219.19	11.83 209.07	
CK. BM.			12.33 206.86	= 206.85

3' L & T S.E. COR. LAMONT & LORING

GO^{0}	
$CO^{3}_{=}$	
$C1^{4}_{=}$	"1921"
$C1^{3}_{=}$	"1927"
$CO^{6}_{=}$	"1937"
$CO^{8}_{=}$	"1945"
$C1^{5}_{=}$	"1953"
$C1^{1}_{=}$	
$CO^{2}_{=}$	
$C1^{2}_{=}$	

WATER METERS
MAGNOLIA ST.; PICO TO FIGUEROA

0+00 = E/L PICO

7/24/56
SHOREY
SMITH
BEATTY

BM	7.07	11.09	4.02	
0+56 N.		4.4	6.7	5.8
0+85 S.		4.59	6.50	5.7
0+89 N.		4.59	6.50	5.7
1+42 N.		4.4	6.7	5.6
1+42 S.		4.4	6.7	5.6
1+47 F.H. (5)		4.4	6.7	6.6
1+47 G.V. (A)		4.8	6.3	6.0
1+93 S.		4.6	6.5	5.4
1+97 N.		4.4	6.7	5.4
2+37 S.		4.6	6.5	5.3
2+50 N.		4.5	6.6	5.2
2+61 S.		4.6	6.5	5.2
2+99 N.		4.39	6.70	5.0
3+25 S.		4.69	6.40	5.0
3+37 N.		4.5	6.6	5.0
3+68 S.		4.8	6.3	4.9
3+80 N.		5.0	6.1	5.0
4+12 S.		4.89	6.20	4.7
4+15 N.		5.39	5.70	4.7
4+72 N.		5.20	5.9	4.6
5+38 N.		5.20	5.9	4.4
CK. BM.		7.07	4.02 = 4.02	

S.W. CONC. MON. MAGNOLIA & BOND

$C0^{9}$	"2604" SET & VERT. RISER 19^{3} & ST.
$C0^{8}$	"2615" " " " " 19' & ST.
$C0^{8}$	"2612" " " " "
$C1^{1}$	"2624"
$C1^{1}$	"2619"
$C0^{3}$	
$C1^{3}$	"2627"
$C1^{3}$	"2634"
$C1^{2}$	"2635"
$C1^{4}$	"2642"
$C1^{3}$	
$C1^{7}$	"2648"
$C1^{4}$	"2653"
$C1^{6}$	"2652"
$C1^{4}$	"2661"
$C1^{1}$	"2660"
$C1^{5}$	"2669"
$C1^{0}$	"2664"
$C1^{3}$	"2670"
$C1^{5}$	"2686"

WATER METERS
MAGNOLIA ST.; PICO TO FIGUEROA
(CONT'D)

B.M.	7.07	11.09		4.02	
TBM	7.38	12.28	6.19	4.90	
6+75 S.			7.0	5.3	5.0
7+36 S.			6.5	5.8	5.3
7+40 N.			5.7	6.6	5.4
7+76 S.			5.6	6.7	6.0
8+09 N.			5.3	7.0	6.1
8+42 S.			4.8	7.5	6.6
8+68 N.			4.2	8.1	6.8
8+92 S.			3.9	8.4	7.2
8+97 N.			3.5	8.8	7.2
9+28 S.			3.1	9.2	7.7
CK. BM.			1.64	10.64 = 10.67	

7/26/56
SHOREY
SMITH

S.W. Conc. Mon. Bond & Magnolia

Set TBM End S.W. Cb. Return

C_0^3	"2707"
C_0^5	"2711"
C_1^2	"2716"
C_0^7	"2717"
C_0^2	"2724"
C_0^9	"2727"
C_1^3	"2730"
C_1^2	"2731"
C_1^6	"2736"
C_1^5	"2739"

N.E. Cor. Conc. Mon. Magnolia & Figueroa

WATER METERS
FIGUEROA BLVD.; PICO TO BOND ST.
0+00 = E/L PICO

7/26/56
SHOREY
SMITH

TBM	6.28	11.18		4.90		TOP S.W. CB. MAGNOLIA & BOND – (SEE PG. 50)
0+56 S.			3.3	7.9	6.6	C_1^3 "2603" SET & VERT. RISER 31' FROM CUL de SAC P.T.
1+36 N.			3.7	7.5	6.6	C_0^2 SET & VERT. RISER 19' E ST.
1+52 S.			4.3	6.9	6.0	C_0^2 "2625"
2+07 S.			4.3	6.9	5.9	C_1^0 "2635"
2+19 N.			4.1	7.1	6.4	C_0^7 "2634"
2+61 S.			4.4	6.8	5.8	C_1^0 "2645"
2+67 N.			4.0	7.2	6.2	C_1^0 "2644"
2+84.5 (S) E.H. SO.			4.3	6.9	6.8	C_0^1 TO FLANGE
2+97 S.			4.2	7.0	5.6	C_1^4 "2649"
3+2 A N.			3.8	7.4	6.1	C_1^3 "2652"
3+37 S.			4.4	6.8	5.6	C_1^2 "2655"
3+71 N.			4.1	7.1	5.9	C_1^2 "2660"
4+00 S.			4.6	6.6	5.4	C_1^3 "2665"
4+07 N.			4.2	7.0	5.8	C_1^3
4+34 S.			4.7	6.5	5.3	C_1^3 "2669"
4+66 S.			5.0	6.2	5.1	C_1^1 "2671"
4+98 N.			4.8	6.4	5.6	C_0^8 "2680"
5+08 S.			5.1	6.1	5.1	C_1^0 "2671"
5+89 N.			4.8	6.4	5.4	C_1^0 "2686"
CK. TBM			6.28	4.90 =	4.90	

ELEV. & GRADES FOR LOWERING 12" C.I. MAIN LA JOLLA MESA DR. AT COLIMA ST. & EXTENDING WITH 6" A.C. MAIN (AS PER 3027-D)

0+00 = S/L ALLEY BLK 29

(A) GRDS

7/27/56
SHOREY
SMITH

TBM	3.16	170.90	167.74	
0+00		16.3	154.6	149.9 ~~150.4~~
0+25		15.0	155.9	151.2 ~~151.7~~
0+50		13.2	157.7	152.3 ~~152.8~~
0+75		11.8	159.1	153.4 ~~153.9~~
1+00		10.3	160.6	154.6 ~~155.1~~
1+25		8.8	162.1	155.8 ~~156.3~~
1+52.6	WATER DEPT. M.H. B.O. ON 12" C.I. MAIN	7.3	163.6	157.0 ~~157.5~~
1+52.6	12" C.I. = 0+00 ON 6" A.C. MAIN EXTENSION			
0+00		7.3	163.6	157.0 ~~157.5~~
0+50		5.0	165.9	160.3
1+00		3.0	167.9	163.1
1+50		0.3	171.0	166.4
TP	9.30	167.00	13.20	157.70
CK. EXIST. CB. ELEV. ON COLIMA		9.83	157.17 =	157.22

ELEV. OF EXIST. CURB INLET APPROX. 1+05 A.C. MAIN.

~~C4.2~~ C4.7

~~C4.2~~ C4.7

C4.8 C5.1

~~C5.2~~ C5.7

~~C5.5~~ C6.0

~~C5.8~~ C6.3

C6.1 C6.6

RE-STAKED 14' PARALLEL TO EXIST. CB. 8/1/56

C6.1 6.6

C5.6

C4.8

C4.2 C4.6

WATER METERS
LA JOLLA MESA DR.
TURQUOISE TO COLIMA
0+00 = N P/L TURQUOISE

BM	10.00	113.56		103.56	
0+29 19 FH ⑤			7.4	106.2	106.64
1+85 E.			3.6	110.0	109.0
2+24 W.			3.9	109.7	109.5
2+36 E.			2.3	111.3	110.4
TP	6.82	118.81	1.57	111.99	
4+36 E.			3.0	115.8	116.1
TP	12.13	130.48	0.46	118.35	
TP	12.98	143.10	0.36	130.12	
TP	13.14	155.58	0.66	142.44	
10+68 E.			10.9	144.7	144.0
11+19 E.			8.1	147.5	146.5
11+94 E.			3.9	151.7	150.3
TP	12.41	166.97	1.02	154.56	
12+22 E.			14.0	153.0	151.8
12+74 E.			10.8	156.2	154.6
13+24 E			8.6	158.4	157.1
13+77 E.			5.3	161.7	159.6
14+33 E			2.5	164.5	163.9 ~~160.2~~
14+93 E.			0.2	166.8	166.1
CK. END Cb. ELEV.			4.42	162.55	= 162.58
CK END Cb. ELEV.			9.80	157.17	= 157.22

8/1/56
SHOREY
KEMP
SMITH

N.W.B.P. TURQUOISE & LA JOLLA MESA DR.

$Fo\frac{1}{-}$ TO FLANGE		SET & VERT. RISER 25' RT. & LT.
$C1\frac{0}{-}$	"5233" & 38" OF & ST.	
$Co\frac{2}{-}$	~~"5240"~~	
$Co\frac{2}{-}$	"5248" & 45"	
$Fo\frac{3}{-}$		
	"5355"	
$Co\frac{1}{-}$		
$C1\frac{0}{-}$	"5365"	
$C1\frac{4}{-}$	"5373"	
$C1\frac{2}{-}$	"5379"	
$C1\frac{6}{-}$	"5381"	SET & VERT. RISER 35' RT.
$C1\frac{3}{-}$	"5385"	
$C2\frac{1}{-}$	"5389"	147.52 N.E. 5 LOT TANT & COLIMA
~~$C3\frac{6}{-}$~~ $Co\frac{6}{-}$		
$Co\frac{7}{-}$	"5397"	

SEE PG. 52

FERN GLEN

VISTA DEL MAR TO MONTE VISTA ST.

Ⓑ STK'S & GRD. 6" A.C. MAIN

TBM	11.28	52.37	41.09	
~~BM~~			~~59.52~~	
	CITY TO CONN. TO			
0+57	EXIST. F.H. TEE	13.5	38.9	35.2
Ⓒ F.H.		13.0	39.4	39.2
1+00		11.3	41.1	36.9
1+50		9.1	43.3	39.0
2+00		6.7	45.7	41.0
2+50		5.5	46.9	43.1
2+87		4.1	48.3	44.2
3+00		3.6	48.8	44.3
3+25		3.6	48.8	44.6
3+50		4.0	48.4	44.3
4+00		4.9	47.5	43.4
4+25		5.3	47.1	42.8
4+50		5.5	46.9	42.7
4+75		5.4	47.0	42.6
4+95		6.0	46.4	41.4
5+12		5.4	47.0	41.4
5+45 G.V.		4.3	48.1	44.0
5+50. END WORK		4.1	48.3	44.4
TP	3.35	51.53	4.19	48.18
CK. BM			5.48	46.05 = 46.04

8/6/56

SHOREY
KEMPO
SMITH

TOP F.H. S.E. COR. FERN GLEN & VISTA DEL MAR

~~S.W.B.P. MONTE VISTA & BELVEDERE~~

$C_3 \frac{7}{+}$ NOT MK'D

$C_0 \frac{2}{-}$ TO FLANGE

$C_4 \frac{2}{-}$

$C_4 \frac{3}{-}$

$C_4 \frac{2}{-}$

$C_3 \frac{8}{-}$

$C_4 \frac{1}{-}$

$C_4 \frac{5}{-}$

$C_4 \frac{2}{-}$

$C_4 \frac{1}{-}$

$C_4 \frac{1}{-}$

$C_4 \frac{3}{-}$

$C_4 \frac{2}{-}$

$C_4 \frac{4}{-}$

$C_5 \frac{0}{-}$

$C_5 \frac{6}{-}$

$C_4 \frac{1}{-}$

$C_3 \frac{2}{-}$

N.W. B.P. ARENAS & MONTE VISTA

FERN GLEN
CONT'D

WATER METERS
52.37

0+58 S.	13.4	39.0	38.2
0+60 S.	12.9	39.5	38.2
1+95 S.	6.6	45.8	43.7
2+07 N.	6.9	45.5	44.2
2+42 S.	4.9	47.5	45.9
3+00 N.	4.1	48.3	47.2
3+44 S.	3.6	48.8	47.1
3+90 N.	4.9	47.5	46.4
3+97 S.	4.2	48.2	46.1
4+40 N.	5.8	46.6	45.7
4+40 S.	5.2	47.2	45.7
4+64 S.	5.3	47.1	45.6
5+00 N.	6.0	46.4	45.6

8/6/56
SHOREY
KEMP
SMITH

55

C_0^8	"305" . SET	& VERT. RISER 6'ET. & 26'LT.
C_1^3	"307"	
C_2^1	"321"	
C_1^3	"324"	
C_1^6	"343"	
C_1^4	"336"	
C_1^7	"341"	
C_1^4	"346"	
C_2^1	"351"	
C_0^9	"350"	
C_1^5	"361"	
C_1^5	"369"	
C_0^8	"360"	

MONTE VISTA ST.

VISTA DE LA PLAYA TO FERN GLEN

⑧ STK'S & GRD. 6" A.C. MAIN

TBM	11.28	52.37		~~41.09~~	
~~BM~~				~~52.37~~	
TP	3.35	51.53	4.19	48.18	
1+69 4 EXIST. G.V.			5.1	46.4	
2+00			4.4	47.1	42.7
2+50			4.2	47.3	43.2
3+00			3.8	47.7	43.6
3+50			3.4	48.1	44.1
3+85 6" TEE			3.3	48.2	44.4
CK. BM			5.48	46.05 =	46.04

WATER METERS

2+19 W.	"7125" METERS BEHIND EXIST. Cb.
2+30 E.	"7125"
2+47 W.	
2+75 E.	"7117"
3+39 E.	
3+44 E.	
3+45 E.	

8/6/56

SHOREY

KEMP

SMITH

TOP F.H. S.E. COR. VISTA DEL MAR & FERN GLEN

~~S.W.B.P. MONTE VISTA & BELVEDERE~~

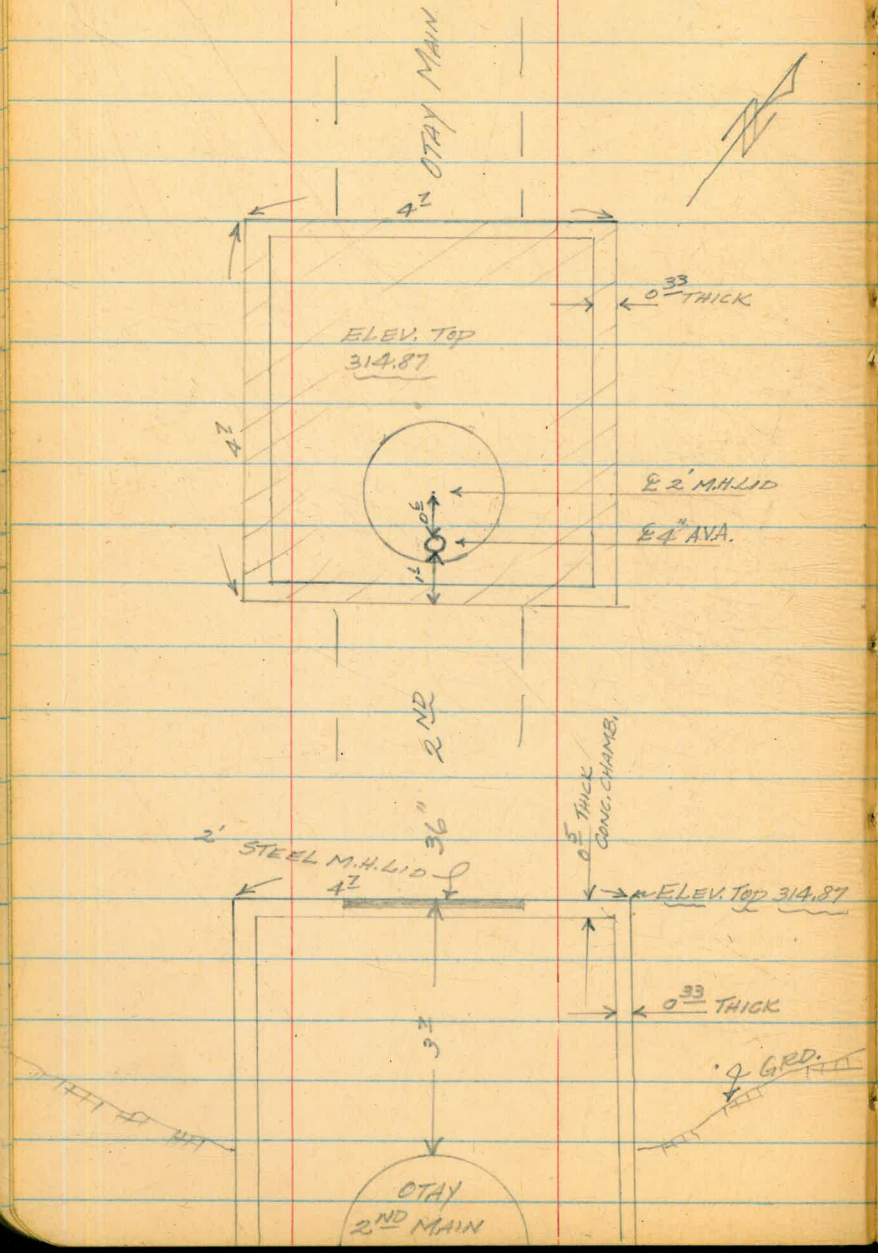
NOT MK'D

C_4^4	WATER METERS BEHIND EXIST. Cb.
C_4^1	
C_4^1	
C_4^0	
C_3^B	

N.W.B.P. ARENAS & MONTE VISTA

DETAIL OF CONC. A.V.A CHAMBER ON 2ND OTAY MAIN - APPROX. 700' N.W. OF ALTADENA ST.; AT NEW MARSHALL ELEM. SCHOOL

8/7/56
SHOREY
KEMP
SMITH



SEA LANE
DRAPER AVE. TO LA JOLLA BLVD
(5) STKS & GRD. 6" A.C. MAIN

8/7/56
SHOREY
KEMP
SMITH

TBM	3.86	110.25		106.39	
0+20	BEGIN WORK		7.47	102.78	99.4
0+50			8.06	102.19	98.3
0+75			8.4	101.9	98.0
1+00			9.5	100.8	96.8
1+50			11.8	98.5	94.4
TP	0.50	97.85	12.90	97.35	
2+00			1.7	96.2	92.0
2+50			3.8	94.1	89.7
3+00			6.1	91.8	87.3
3+20			7.0	90.9	86.4
3+50			8.4	89.5	85.2
4+00			10.6	87.3	83.0
4+50			12.8	85.1	80.7
TP	0.20	84.85	13.20	84.65	
5+00			2.1	82.8	78.5
5+50			4.5	80.4	76.3
5+75			6.0	78.9	75.0
6+00			6.7	78.2	74.0
6+50			8.9	76.0	71.8
7+00			11.2	73.7	69.6
TP	2.96	75.39	12.42	72.43	
7+50			3.9	71.5	67.2

S.W.B.P. DRAPER & GENTER ST.

C_3^{4} ± NOT MK'D

C_3^{9}

C_3^{2}

C_4^{0}

C_4^{1}

C_4^{2}

C_4^{4}

C_4^{5}

C_4^{5}

C_4^{3}

C_4^{3}

C_4^{4}

C_4^{3}

C_4^{1}

C_3^{2}

C_4^{2}

C_4^{2}

C_4^{1}

C_4^{3}

SEA LANE
CONT'D

8/7/56
SHOREY
KEMP
SMITH

75.39

7+73 5	CITY TO CONN. TO EXIST. G.V.	4.9	70.5	67.2	C_3 3± NOT MK'D
CK. BM		5.52	69.87 = 69.83		N.E. B.P. LA JOLLA BLVD. & CENTER

WATER METERS

METERS BEHIND EXIST. CURBS

1+42 N.	"632"
1+20 S.	"635"
1+87 S.	"625"
2+02 N.	"622 & 29"
2+09 S.	"611"
2+13 S.	"571"
3+55 S.	"563"
4+28 N.	"554"
4+22 S.	"561"
4+70 S.	"551"
4+35 N.	"550"
5+01 S.	
5+04 N.	
5+36 N.	
6+08 N.	
6+37 N.	
6+62 S.	"521"
6+99 S.	"511"

GERTRUDE ST.
LILLIAN ST. TO 105' NLY.
④ STK'S & GRD. 4" A.C. MAIN

8/8/56
SHOREY
KEMP
SMITH
PAULSON

TBM	8.06	64.66	56.60	
0+15	BEGIN WORK	5.2	59.6	54.8
0+20	4" G.V.	5.0	59.7	54.8
0+30	Δ PT.	4.9	59.8	54.6
0+50	Δ PT.	5.5	59.2	53.7
1+00		5.4	59.3	54.8
1+55	2" B.C. Assy.	3.9	60.8	55.8
CK. BM		8.06	56.60 =	56.60

CONC. MON. 1+75 13 35' LT. (F.B. 921-38).

C4 8± NOT MK'D
C4 8
C5 3
C5 3
C4 5
C5 0

WATER METERS
BYRON ST.; SCOTT TO ROSECRANS

8/8/56
SHOREY
KEMP
PAULSON

0+00 = NWLY LINE SCOTT

TBM	8.78	16.28	7.50	
0+16 S.W.		7.8	8.5	7.5
0+21 N.E.		8.0	8.3	7.3
0+28 S.W.		7.2	9.1	7.7
0+48 S.W.		6.1	10.2	8.4
0+85 S.W.		5.4	10.9	9.6
0+92 N.E.		5.1	11.2	9.7
1+21 N.E.		4.7	11.6	10.5
1+27 S.W.		3.8	12.5	10.7
1+71 N.E.		3.4	12.9	12.1
1+80 S.W.		2.5	13.8	12.7
TP	5.35	19.43	2.20	14.08
2+68 E.H.			3.0	16.4	16.6
2+71 S.W.			2.9	16.5	15.6
2+95 N.E.			2.8	16.6	15.8
CK.			1.14	18.29 = 18.30	

Top EXIST. Cb. E.C. NLy. COR. BYRON & SCOTT

C1 E	"2903"	SET & VERT. RISER 26' FROM E ST.
C1 E	"2904"	
C1 4		
C1 8	"2907"	
C1 3	"2911"	
C1 5	"2912"	
C1 1	"2920"	
C1 6	"2919"	
CO 8		
C1 —	"2929"	
FO 2	TO FLANGE	
CO E		
CO 8		

Top EXIST. Cb. E.C. SLy. COR. BYRON & ROSECRANS

33 RD ST
120' N. of "A" ST. TO "A" ST.
④ STK'S 6" A. C. MAIN

TBM			165.05	
~~BM~~	3.98	169.03	~~165.10~~	
0+00		1.1	167.9	164.2
0+50		4.7	164.3	160.5
1+00		7.8	161.2	157.3
1+01 F.H. TEE ⑤			161.1	
1+16 END - 2" B.C. ASSY		8.3	160.7	156.8
CK. TBM		3.98	165.05	= 165.05

8/9/56
SHOREY
KEMP
SMITH
PAULSON

25' R.P. TO Cb. RADIUS ASH ℄ 33 RD
~~7' L ℄ T S.W. COR. ASH ℄ 33 RD~~

C TO EXIST. - PIPE FINDER LOCATION END OF MAIN

C_3^8

C_3^9
C_3^8 C06 TO FLANGE $C4^8$ TO BOTT
C_3^9

ALLEY BLK. 128
THORN TO LEXINGTON WEST OF VAN DYKE
0+00 = S/L THORN

BM	1.94	305.01		303.07	
0+25 W.			1.7	303.3	301.4
1+25 E.			6.9	298.1	297.7
1+83 E.			11.5	293.5	291.9
TP	0.85	292.97	12.89	292.12	
2+03 W.			1.8	291.2	289.4
2+62 E.			7.4	285.6	283.0
2+76 W.			10.7	282.3	281.1
TP	0.24	280.27	12.94	280.03	
3+61 E.			2.7	277.6	273.3
4+24 W.			12.4	267.9	268.2
4+33 E.			8.6	271.7	267.9
CK.			8.09	272.16 = 272.17	

BM	2.76	304.58		301.82	
TP	2.48	305.45	1.61	302.97	End W. curb at arch & Thorn
			4.20	301.25 = 301.4	
			8.00	297.45 = 297.7	
			3.30	302.15	301.52
			4.26	301.19	301.22
TP	0.77	293.18	13.04	292.41	
			8.75	284.43	= 283.0
TP	0.13	280 44	12.87	280.31	
CK TP			8.26	272.18 = 272.17	

8/9/56
SHOREY
KEMP
PAULSON

(1) HUB & ALLEY @ THORN } ELEV. AS PER MATCH - City ENG.

C1 9
C0 4
C1 6
C1 8
C2 6
C1 2
C4 3
F0 3
C3 8

SET & VERT. RISER
7.57 FROM & ALLEY

2"x2" HUB MK'D 4+35 (3) PAVT

3/11/57 Beatty

301.82 NW BP Marlborough & THORN

& wat. ser curb stop as exists 0+25 W
" " " " " " " 1+25 E

City Engr.'s 3'ok pavt 0+80 C0 58 Ely = C0 63
" " " " 0+80 F0 06 Wly = F0 3

= & wat ser curb stop as exist 2+62 E
addition curb stop 1E lower.

CK (1) 3'OK 4+35

POE ST.

EVERGREEN TO WILLOW LANE

@ STK'S & GRD. 6" A.C. MAIN

TBM	0.13	149.87		149.74	
TP	0.06	136.83	13.10	136.77	
TP	0.25	123.88	13.20	123.63	
TP	0.27	110.88	13.27	110.61	
TP	1.43	98.96	13.35	97.53	
SET TBM	12.62	105.72	5.86	93.10	
0+51 CONN. TO EXIST. 6" MAIN 22½° BEND			11.3	94.4	90.2
0+63			8.5	97.2	~~94.4~~ 93.6
TP	12.83	118.45	0.10	105.62	103.5
1+00			11.2	107.3	~~105.1~~
TP	12.25	130.48	0.22	118.23	118.0
1+50			8.7	121.8	~~121.2~~
					121.5
1+63			5.0	125.5	~~122.8~~
1+75 TP	12.66	142.85	0.29	130.19	126.0 ~~120.1~~
TP	9.19	151.60	0.44	142.41	~~149.4~~
2+00			7.7	143.9	~~145.8~~
2+08 22½° BEND	10.97	160.69	4.0	147.6	145.6
2+16 6" TEE			1.88	149.72	146.5
			9.0	151.7	
CK. TBM			10.97	149.72 = 149.74	

1+20 WM. N +0.8 −9.7 = 8.9

8/10/56
SHOREY
KEMP
SMITH
PAULSON

→ 2"x2" HUB & WILLOW LANE & SLY LINE POE (SEE PAGE 65.)

R.E. DISK SLY. POE & 12' OFF E. LINE EVERGREEN

C4 2 ± CUT TO EXIST.

~~C2 8~~ 3 6 8.1

~~C2 2~~ C3 8 11.0

~~C0 6~~ C3 8 8.7

~~C2 7~~ 4 0 5.0

~~C2 1~~ C4 2 0.3

C3 5 7.2

C2 0 3.3

C5 2 8.9

C0 0 1½"x1½" HUB MK'D 0+50 C7 9

WILLOW LANE

QUIMBY TO POE

④ STK'S & GRD. 6" A.C. MAIN

BM	2.32	180.11		177.79	
TP	0.02	166.78	13.35	166.76	
	6.45	162.43	10.80	155.98	
0+70 BEGIN WORK			6.5	155.9	152.6
0+88			6.0	156.4	152.5
1+00			5.7	156.7	152.6
1+50			5.2	157.2	153.0
2+00			5.3	157.1	153.4
2+50			6.4	156.0	151.6 ~~152.4~~
3+00			5.9	156.5	148.0 ~~151.5~~
3+15 END WORK		CONN. TO TEE	12.4	150.0	146.5 ~~150.0~~
SET TBM	10.37	160.71	12.69	149.74	
TP	12.18	172.10	0.79	159.92	
TP	9.47	181.17	0.40	171.70	
DK. BM.			3.37	177.80	= 177.79
		162.43			
1+22.E.			5.5	156.9	155.7
2+71 E.			6.5	155.9	157.8

6/10/56
SHOREY
KEMP
SMITH
PAULSON

S.W.B.P. WILLOW & POE

C_3^3 + CUT TO EXIST.

C_3^9

C_4^1

C_4^2

C_3^7

~~C_5^6~~ C_4^4 6.4

~~C_5^0~~ C_8^5 5.3 X

C_3^5 10.6 X 151.8

2"x2" HUB @ WILLOW LANE & SLY LINE POE ST.

C_1^2 SET @ VERT. RISER. $14\frac{3}{4}$ FROM PROP.

F_1^9

SOLEDAD RD. & SOLEDAD WAY

(4) STK'S & GRD 8" & 6" A.C. MAIN

8/10/56
SHOREY
KEMP
PAULSON

BM	11.93	366.56		~~344.88~~ 354.63		NAIL IN P.P. ~~#47111 H 250 So. SOLEDAD WAY~~ GUY POLE 0+03 ℄
0+00			15.2	351.4	346.0	C TO EXIST. MAIN
0+12			14.8	351.8	348.0	$C3^8$
0+50			12.0	354.6	350.7	$C3^2$
1+00			8.9	357.7	354.3	$C3^4$
1+25⁴ 8"x6" TEE			6.5	360.1	356.0	$C4^1$
1+31 6" G.V. & 11¼° BEND			6.4	360.2	356.4	$C3^8$
1+50			5.5	361.1	357.4	$C3^7$
1+74 CONN. TO EXIST. 6" MAIN			4.3	362.3	358.9	C TO EXIST. MAIN
CK. BM			11.93	354.63 = 354.63		

MAGNOLIA ST.
WATER METERS
FIGUEROA TO PACIFIC HWY
0+00 = N.E. COR. MAGNOLIA & FIGUEROA

BM.	4.82	15.49	10.67	
0+81 S.		4.0	11.5	10.1
1+41 S.		3.0	12.5	11.2
1+43 S.		3.1	12.4	11.2
1+66 N.		3.3	12.2	11.8
1+67 N.		3.3	12.2	11.8
2+87 S. F.H.		1.9	13.6	14.2
CK. BM.		4.82	10.67	= 10.67

8/10/56
SHOREY
KEMP
PAULSON

CONC. MON. N.E. COR. MAGNOLIA & FIGUEROA

C 1 4
C 1 3
C 1 3

C 0 4

C 0 4

F 0 6 TO FLANGE

CUVIER ST.

MARINE ST. TO SEA LANE

(5) STK'S & GRD 6" A.C. MAIN

BM	6.97	88.03		81.06	
TP	5.71	93.15	0.59	87.44	
0+60 BEGIN WORK		56" G.V. By City	6.7	86.5	83.0
0+80			5.9	87.3	83.2
1+00			5.7	87.5	83.3
1+50			5.2	88.0	83.8
2+00			4.7	88.5	84.4
2+50			4.1	89.1	84.9
3+00			3.5	89.7	85.4
3+50			2.7	90.5	86.0
3+67 E.H. TEE			2.4	90.8	86.2
(3)			2.3	90.9	
3+97.± 11¼° BEND & 6" TEE			2.8	90.4	86.4
CK.			2.31	90.84 =	90.88

WATER METERS

(BEHIND EXIST. CURB)

0+94 W.
1+30 E.
1+50 W.
2+05 E.
2+34 W.
2+78 E.
3+20 W.
3+28 E.

8/21/56
SHOREY
KEMP
SMITH

S.E.B.P. CUVIER & PEARL

C_3^5 ± CUT TO EXIST.

C_4'

C_4^2

C_4^2

C_4'

C_4^2

C_4^3

C_4^5

C_4^6

C_4^7 F0' TO FLANGE

C_4^0

(5) 3+20 SEALANE (PG. 58)

SPINDRIFT DRIVE

PRINCESS ST. TO PASEO DORADO
(5) STK'S & GRD. 6" A.C. MAIN

8/27/56
SHOREY
KEMP
SMITH

S.E.B.P. SPINDRIFT & ST. LOUIS TERRACE

BM	13.11	50.51		37.40	
TP	13.01	63.34	0.18	50.33	
TP	9.91	73.14	0.11	63.23	
0+00	BEGIN WORK		3.6	69.5	66.0
0+25			3.8	69.3	65.8
0+50			3.9	69.2	65.6
0+75			4.1	69.0	65.5
1+02[10]	P.C.C.		4.4	68.7	65.3
1+25			4.6	68.5	65.2
1+50			4.7	68.4	65.0
1+75			4.9	68.2	64.8
1+99[17]	P.C.C.		5.0	68.1	64.7
2+50			5.4	67.7	64.4
3+00			6.3	66.8	63.6
3+50			8.0	65.1	61.7
3+75	F.H. TEE		10.5	62.6	58.9
	(5)		8.8	64.3	
4+00			10.9	62.2	58.6
TP	0.06	60.71	12.49	60.65	
4+50			2.0	58.7	55.4
5+00			5.5	55.2	52.3

C_3^{5+} CUT TO EXIST. MAIN
C_3^5
C_3^6
C_3^5
C_3^4
C_3^3
C_3^4
C_3^4
C_C^4
C_3^3
C_3^2
C_3^4
C_3^1

C_5^4 C_1^0

C_3^6
C_3^3
C_2^2

8/27/56
SHOREY
KEMP
SMITH

SPINDRIFT DRIVE

CONT'D

		60.71			
5+50			8.3	52.4	49.1	$C_3\frac{3}{}$
6+00			11.4	49.3	46.0	$C_3\frac{3}{}$
TP	0.55	47.97	13.29	47.42		
6+50			1.7	46.3	42.9	$C_3\frac{4}{}$
7+00			4.8	43.2	39.8	$C_3\frac{4}{}$
7+50			7.3	40.7	36.8	$C_3\frac{2}{}$
8+00		OMIT			33.7	
8+02 $\frac{68}{}$ E.C.				10.6	37.4	33.6	$C_3\frac{8}{}$
8+34 $\pm$		6"x6" TEE By City		11.4	36.6		
		6" G.V. So. of TEE				→	
		10' 6" A.C. PIPE & 6" TEE				33.0	$C_3\frac{6}{} \pm$ CUT TO EXIST. MAIN
		6"x4" REDUCER					
8+50			12.0	36.0	32.6	$C_3\frac{1}{}$
TP	0.10	34.96	13.11	34.86		
8+80			0.7	34.3	30.4	$C_3\frac{9}{}$
8+91 $\frac{85}{}$ B.C.				1.3	33.7	29.7	$C_4\frac{0}{}$
9+00			1.9	33.1	28.9	$C_4\frac{2}{}$
9+25			3.9	31.1	27.0	$C_4\frac{1}{}$
9+50			5.8	29.2	25.1	$C_4\frac{1}{}$
9+75			7.9	27.1	22.6	$C_4\frac{5}{}$
9+85 $\frac{67}{}$ E.C.			9.2	25.8	21.4	$C_4\frac{4}{}$
10+00			10.7	24.3	20.0	$C_4\frac{3}{}$
TP	0.44	22.36	13.04	21.92		
10+50			3.4	19.0	14.8	$C_4\frac{2}{}$
10+90 $\frac{5}{}$		6" TEE By City		8.2	14.2	10.8	$C_3\frac{4}{} \pm$ CUT TO EXIST. MAIN
11+00				9.1	13.3	9.7	$C_3\frac{6}{}$

SPINDRIFT DRIVE
(CONT'D)

8/27/56
SHOREY
KEMP.
SMITH

22.36

11+50 TP	1.59	11.00	11.7 12.95	10.7 9.41	6.8	C_3^2
12+00			3.0	8.0	3.9	C_4^1
12+50			5.9	5.1	1.0	C_4^1
12+63 ± 45° BEND			6.5	4.5	0.3	C_4^2
12+75 OMIT					-0.4	
12+97.80 22½° BEND END WORK			7.8	3.2	-0.7	C_3^2
CK. TBM			5.31	5.69 = 5.70		E. RIM SEW. M.H. APPROX. 12+45 16' LT

PASEO DORADO

AVENDA ALAMAR TO SPINDRIFT
(5) STIC'S & 6RD 6"A.C. MAIN

9/7/56
SHOREY
SMITH
PAULSON

TBM	1.91	7.61		5.70	
TP	5.72	6.94	6.39	1.22	
0+15 BEGIN WORK			4.4	2.5	-1.0
0+20 G.V. By City					-1.1
0+25 B.C.			4.5	2.4	-1.1
0+50			4.7	2.2	-1.2
1+00			5.1	1.8	-1.5
1+50			5.1	1.8	-1.8
2+00			5.5	1.4	-2.0
2+22.62 E.C.			5.3	1.6	-2.2
2+25			5.3	1.6	-2.2
2+50			5.7	1.2	-2.2
3+00			5.3	1.6	-2.2
3+50			5.3	1.6	-2.2
4+00			5.2	1.7	-2.2
4+50			5.1	1.8	-1.9
5+00			4.9	2.0	-1.6
5+20 F.H. TEE			4.9	2.0	-1.5
(5)			4.4	2.5	
5+50			4.8	2.1	-1.4
6+00			4.5	2.4	-1.1

E. RIM SEW. M.H. (SEE PG. 71)

C_3^{5+} CUT TO EXIST. TEE

C_3^5

C_3^4

C_3^3

C_3^6

C_3^4

C_3^8

C_3^8

C_3^4

C_3^8

C_3^8

C_3^8

C_3^7

C_3^6

C_3^5

C_4^0 C_0^3 2.0

C_3^5

C_3^5

PASEO DORADO
⑤ STK'S
(CONT'D).

9/7/56
SHOREY
SMITH
PAULSON

6.94

6+50			4.4	2.5	-0.8 C3 3
6+83 65 END WORK =			3.7	3.2	-0.7 C3 2
12+97 8 SPINDRIFT					
TP	5.63	7.67	4.90	2.04	
CK. TBM			1.97	5.70	=5.70

9/14/56
SHOREY
SMITH
PAULSON

ELEV. TOP 6" A.C. MAIN
COLUMBINE ST.; FAIRMOUNT TO PEPPER DR.
0+00 = W/L FAIRMOUNT

N.W. 1' x 4.5' L & T FAIRMOUNT & COLUMBINE

BM	2.27	291.04		288.77
1+85 B.C. TOP 6" A.C. MAIN			9.16	281.88
1+85 B.C. GROUND			5.6	285.4
2+40.03 E.C. TOP 6" A.C. MAIN			9.27	281.77
2+40.03 E.C. GROUND			5.8	285.2
TP	4.10	289.29	5.85	285.19
3+91	TOP 6" MAIN		7.5	281.8

ELEV. TOP 10" C.I. JUNIPER ST.
SUMAC TO MODESTO
0+00 = P/L B.C. N.W. COR. MODESTO & JUNIPER

CONC. MON. @ JUNIPER & W/L SUMAC.

BM	11.38	264.22		252.84
0+85.5 TOP 10" C.I. MAIN			6.3	257.9
1+81 " " " "			5.5	258.7
CK. BM			11.38	252.84 = 252.84

2" A.V. AT THORN & VAN DYKE
④ STK & GRD

BM	7.57	309.39	301.82	N.W.B.P. MARLBOROUGH & THORN
④ HUB 2" A.V.		2.24	307.15	308.10 FI 05 TO FINISHED ST. GRD.

WATER METERS
ALLEY 66 – E. of 38th, N. of LANDIS

BM	BM	8.70	340.00	331.30		
	TP	5.00	339.38	5.62	334.38	
	0+17E			7.0	332.4	329.8 C2 6
	0+19E			7.0	332.4	329.9 C2 5
	0+27E			6.7	332.7	330.7 C2 0
	0+42W.			6.6	332.8	331.6 C1 2
	0+71W.			5.8	333.6	333.0 C0 6
	0+79E.			4.8	334.6	333.4 C0 2
	0+80W.			5.6	333.8	333.4 333.2 C0 6
	1+15W.			4.8	334.6	333.4 C1 2
	1+17E			4.4	335.0	333.8 C1 2
	1+76E.			4.1	335.3	334.1 C1 2
	2+21E.			4.3	335.1	334.2 C0 9
	2+45W.			4.6	334.8	333.8 C1 0
	2+76E.			4.8	334.6	333.8 C0 8
	2+80W.			4.7	334.7	333.4 C1 3
	3+01E.	TP	2.32	336.53	4.9 334.5	333.3 C1 2
	3+27W.				5.1 334.21	332.7 C0 9
	3+32W.				2.7 333.6	332.5 C1 1
	3+41E.				2.9 333.6	332.7 C1 1
	3+78W.				2.7 333.8	332.7 C0 6
	4+05E.				4.1 332.4	331.8 C0 9
	4+44W.				4.1 332.4	331.5 C0 9
	4+49E.				5.8 330.7	329.4 C1 3
	4+51E.				5.6 330.9	329.4 C1 5
	4+62W.				6.1 330.4	329.4 C1 0
	5+29E.				6.6 329.9	328.4 C1 5
					11.4 325.1	323.1 C2 0
	CK. BM.		5.23	331.30		=331.30

P.K. NAIL IN P.P. PA 3725 STA. 4+50 10' RT Ⓛ
SET Ⓛ VERT. RISER
8.07 FROM Ⓛ ALLEY

6.90
5.13
1.77

.00300
590 / 1.77000

220
.003
.660

5.79
2

4.9

1.2

.9

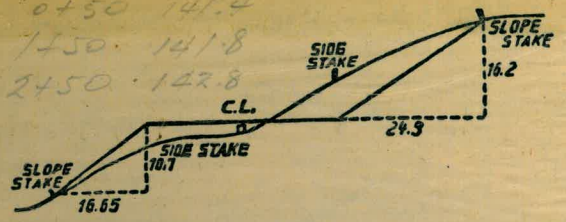
5.1

310.03
80.91
390.94

80.91

0+50 141.4
1+50 141.8
2+50 142.8

4.9



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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