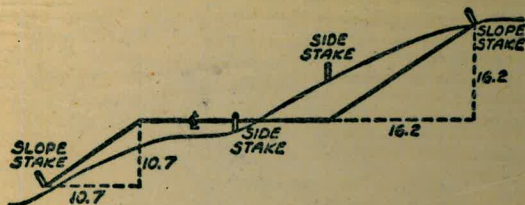


W911

WESTBURY





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

750  
75  
730



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.95	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

Remove Dr. Country C/Dr 60 Belton 1-30 ✓  
 La Jolla View Res. Alice  
 "C" St. 39th to 35th 31-34 ✓  
 Boston St. 39th to 40th 34-38 ✓  
 Alley Bk 58 E of 32nd & N. of Monroe Alice  
 Malden St. Collingwood to Lamont 39-41 ✓  
 42-49 ✓  
 Alice  
 SPRINGFIELD ST. SWAN TO ORICK ST. (Belton) 50-53 ✓  
 VILAND ST., WEAVER ST. TO 260' WEST ( " ) 54-57 ✓  
 SEA BREEZE DR, POTOMAC TO 250' N. of ANNECHANNY 58-61 ✓  
 CALLE TOWN, CALLE AGUA DULCE 210' ERY 62 ✓  
 Basement Survey Alice  
 Country Club Res to Encina Dr 65 ✓  
 for Topo Survey Alice  
 Lower OTAY Lake Transit Traverse 75 ✓  
 Alice  
 Check Levels Otoy Lake Topography 76-79 ✓  
 Alice



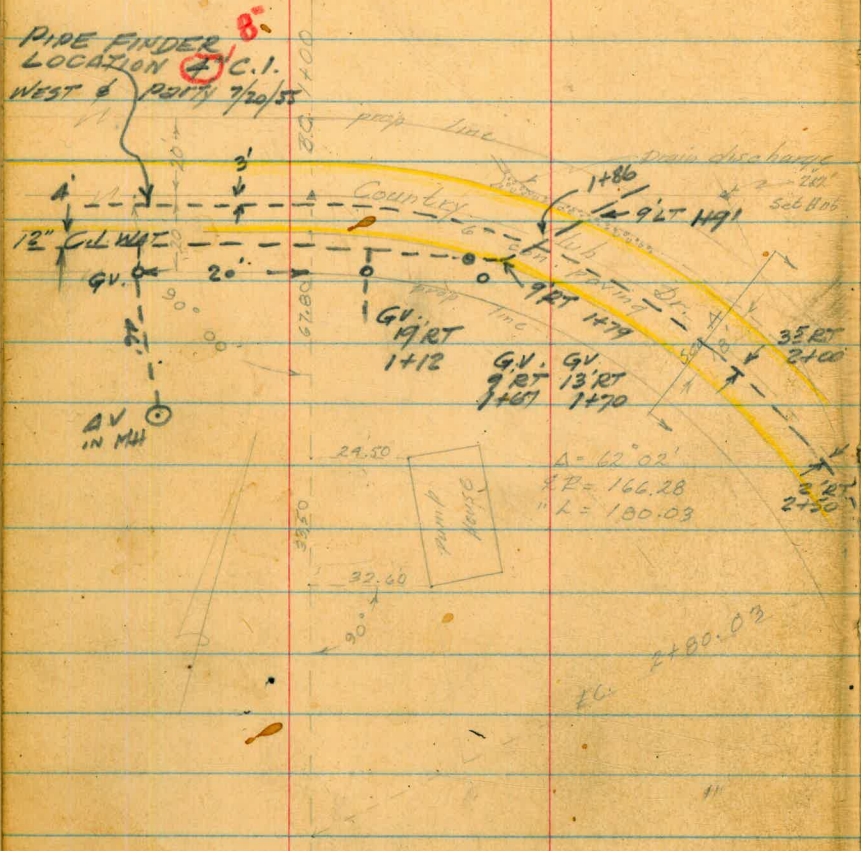
WERT  
KEMP  
ALEXANDER  
HOLAHAN

3-16-55

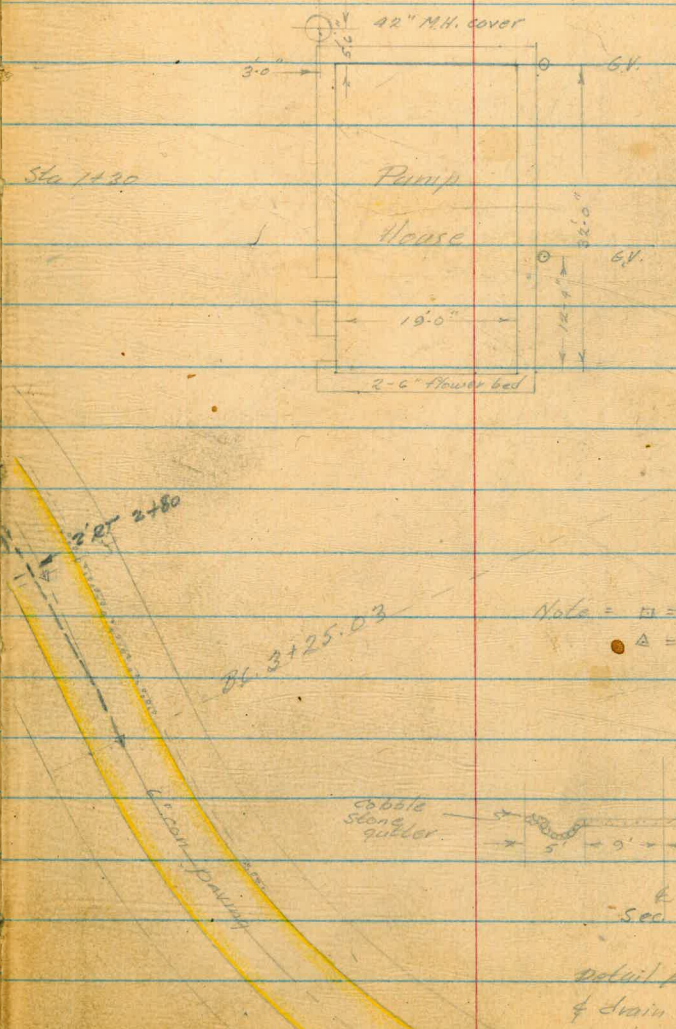
Profile of Proposed Water Line  
Romero Dr. Country Club Pump House  
to La Jolla View Reservoir

See Map 1975  
See Book 17

PIPE FINDER  
LOCATION  $\frac{7}{8}$  C.I.  
WEST of party 7/20/55



$\Delta = 62^{\circ}02'$   
 $R = 166.28$   
 $L = 180.03$

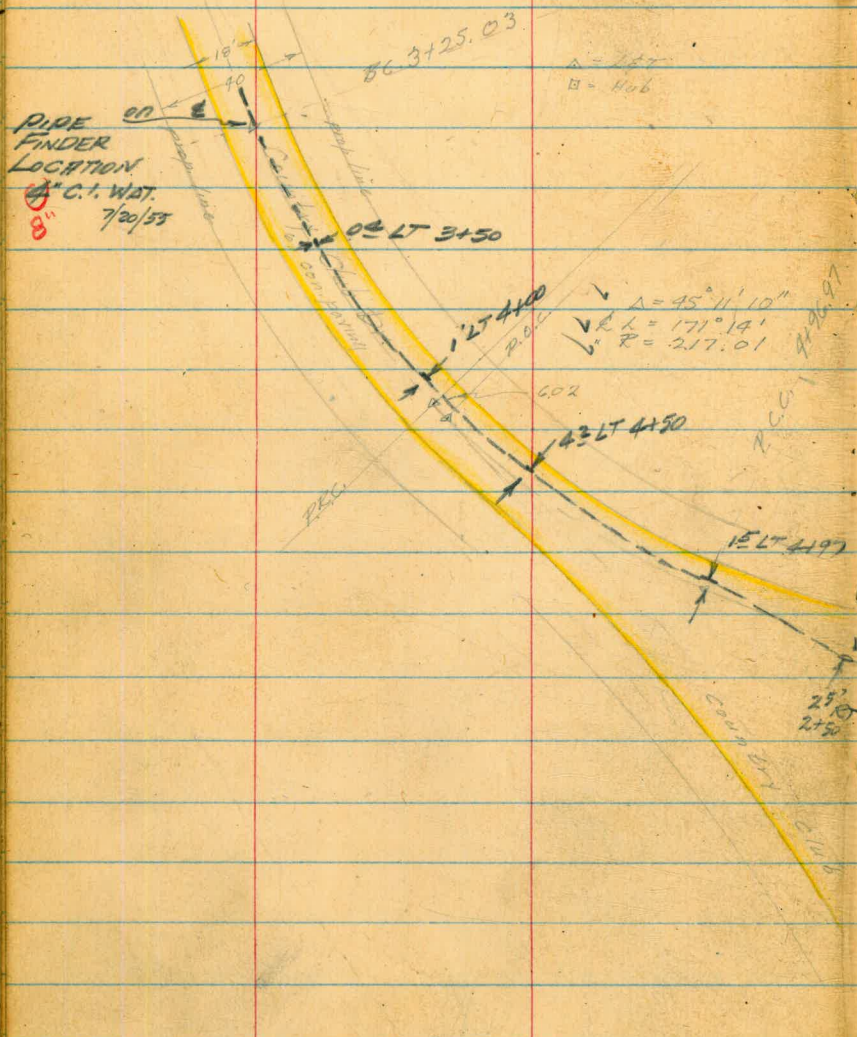


Note =  $\square$  = hub  
 $\Delta$  = L.S.T.

Note: All measurements on curves are radial  
" " " tangents are right angle

Detail paving  
& drain on left





56 3+25.03

$\Delta = 155^\circ$   
 $\square = 406$

PIPE FINDER LOCATION  
C.I. WAT.  
7/20/53  
8"

02 LT 3+50

12 LT 4+40

$\Delta = 95^\circ 11' 10''$   
 $\sqrt{RL} = 171.14'$   
 $\sqrt{R} = 217.01$

43 LT 4+50

15 LT 4+97

$\Delta = 17^\circ 03' 50''$   
 $\sqrt{RL} = 696.08$   
 $\sqrt{L} = 207.31$

2+75 ? Questionable

18 RT 6+00

65 RT 6+50

55 RT 7+00

6 RT 7+50

25 RT 2+50

25 RT 2+50

GV 2' RT 5+02

GV 2' RT 5+16

GV 2' RT 5+70

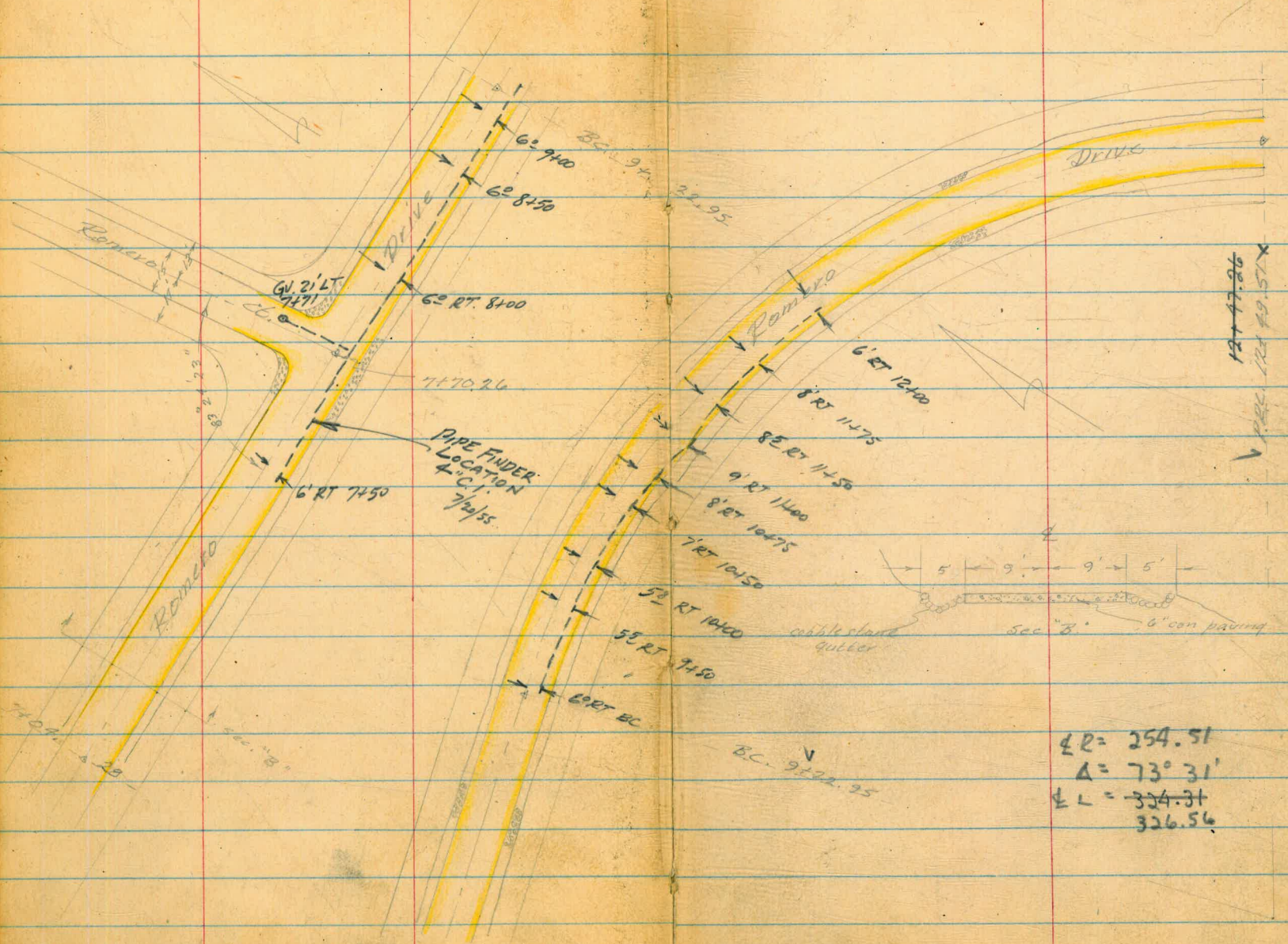
9 FH 13' RT  
GV 4' RT

limits of 6" con. paving shown

See Map 1975  
& Book 17

EC 7+09.28





$E R = 254.51$   
 $\Delta = 73^{\circ} 31'$   
 $E L = 324.31$   
 $326.56$

$12+77.26$   
 $12+49.57X$

$B.C. 9+22.95$



Romero

Drive

Drive

Romero

Romero

PIPE FINDER  
 LOCATION  
 4" CI.  
 7/2" SS.

white stone  
 gutter

Sec "B"  
 6" con paving

GN 21 LT  
 74791

7170.26

6' RT 7450

6' RT 8400

6' RT 8150

6' RT 9400

7' RT 10450

8' RT 11450

8' RT 12400

8' RT 13450

8' RT 14400

8' RT 15450

9' RT 16400

9' RT 17450

5' RT 18400

5' RT 19450

6' RT BC

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95

BC 9+22.95



PIPE FINDER  
Location & CI.  
7/20/55

8' RT 15+94

3' RT 15+50

on E 15+13

15 E. P.B.C.  
15+93.98  
15+91.78

14+90 3' LT

3' LT 14+50

0 FH 13'20" 14+90  
GV 6 RT 10+90

5' 22" 26' W  
Romero developed

$\Delta = 73^{\circ} 01' 20"$   
 $\angle B = 195^{\circ} 23'$   
on E 12+25  
 $EL = 248.82$

12' RT 12+50

5' 22" 26' W

B.C. 13+45.15  
 $\Delta = 118^{\circ} 29' 10"$   
 $\angle B = 45'$   
 $EL = 93.06$

$\Delta = 11^{\circ} 29' 40"$   
 $R = 25.63$   
 $L = 5.14$

12+47.86  
12+49.51  
9' RT 12+50

10' RT 13+25  
13+42.57  
in cobble stone gutter

13+44.30

See page 26



Romero Drive Cont.

		435.33
		436.10
	435.47	
0.14	436.24	
		425.96
	9.51	426.73
	426.44	
0.48	427.21	
		413.42
	13.02	414.19
	414.27	
0.85	415.04	
		400.95
	13.32	401.72
	401.27	
0.32	402.04	
		387.94
	13.33	388.71
	389.47	
1.53	390.24	
		380.46
	9.01	381.23
	380.75	
0.29	381.52	
0+00		
		11.7
0+39		

Where from?

L.E.T., common BC, Country Club Dr. & Carrizo

Note B.M. marked 436.10 was found to be 0.77  
in error. Corrections in red.

7  
500 p.p.  
25

Note: All x sec. & distance  
measured radial on  
curves & 90° on tangents

T.B.M. L.E.T. Sta. 1400 B.C.

16

22

$\frac{11.9}{9}$

$\frac{11.7}{9}$

$\frac{12.0}{9}$

20' G.V.



380.75  
381.52

0+50 6.0

0+51

1+00 B.C. 0.30

380.4

T.P. 0.52

380.23

381.00

393.15

12.92 393.92

1+09

1+25 9.9

1+39 8.2

1+39 7.0

1+40 7.0

1+50 7.0

1+66 5.05

Reduced by J. Gray 4-11-55

LE E RL

$\frac{6.1}{9}$   $\frac{6.0}{9}$   $\frac{6.7}{9}$

67. Water M.H. Air V.

$\frac{0.4}{9}$   $\frac{0.3}{9}$   $\frac{0.4}{9}$

20 R. Water G.V.

$\frac{10.0}{9}$   $\frac{9.9}{9}$   $\frac{10.0}{9}$

Flute cross  $\frac{8.5}{9}$   $\frac{8.2}{9}$   $\frac{8.2}{9}$  radial

Flute M.H. 35' 4", cut 2.5 top 2" cable

$\frac{7.1}{9}$   $\frac{7.0}{9}$   $\frac{7.1}{9}$

Water M.H. 7' RL, GV 10' RL



Romero Dr. Cont.

393.15  
393.92

1+75 4.1

1+82 3.2

1+89

2+00 1.2

393.09

7.71 0.06 393.86

405.84

12.75 406.61

2+25 11.0

2+50 8.1

2+80.03 E.C. 4.6 5.4 = 400.44

3+00 2.4 2.8 = 403.04

405.60

0.24 406.37

418.06

12.46 418.83

11

4

.26

$\frac{4.2}{9}$

$\frac{4.1}{0}$

$\frac{4.3}{9}$

16" water cross @ 9.25

$\frac{3.7}{0}$

16" water cross @ 4

$\frac{2.5}{9}$

16" water cross @ 9

$\frac{1.3}{9}$

$\frac{1.2}{0}$

$\frac{1.3}{9}$

$\frac{11.1}{9}$

$\frac{11.0}{0}$

$\frac{11.1}{9}$

$\frac{9.0}{9}$

$\frac{8.1}{0}$

$\frac{9.0}{9}$

$\frac{6.2}{9}$

$\frac{4.6}{0}$

$\frac{6.0}{9}$

$\frac{3.2}{9}$

$\frac{2.4}{0}$

$\frac{3.5}{9}$



Pomero Dr. Cont

418.06  
418.83

3+25.83 BC 11.7

3+50 8.9

3+75 6.0

3+98

4+00 3.2

4+05

4+15

4+25 0.4

4+25

T.P.

13.17 431.09  
431.86

417.92  
0.14 418.69

16 4 PL

$\frac{11.9}{9}$   $\frac{11.7}{9}$   $\frac{11.2}{9}$

$\frac{9.0}{9}$   $\frac{8.9}{9}$   $\frac{9.0}{9}$

$\frac{6.2}{9}$   $\frac{6.0}{9}$   $\frac{6.0}{9}$

cable cross @ 9' PL

$\frac{3.2}{9}$   $\frac{3.2}{9}$   $\frac{3.5}{9}$

cable cross @ 4'

cable cross. 9' 16, begin standard curb, left hand 14'

$\frac{0.5}{9}$   $\frac{0.4}{9}$   $\frac{0.9}{9}$

Steel cross @ 9' PL



Romero Dr. Cont

931.09  
131.86

4150 11.1

4150

4175 8.7

4177 8.03

4195

4196.97 PCC. 6.5

4197. 6.5

4199

5100

5125 3.6

5150 1.0

16  $\frac{\text{¢}}{\text{ft}}$

$\frac{11.3}{9}$   $\frac{11.1}{8}$   $\frac{12.0}{76}$  So. gutter

Heel crossing @  $\frac{\text{¢}}{\text{ft}}$

$\frac{9.0}{9}$   $\frac{8.7}{8}$   $\frac{8.8}{4}$  Heel cross.  $\frac{9.2}{13}$   $\frac{\text{¢}}{\text{ft}}$  County Club Dr.

Gas MH. 12' 16"

Heel MH. 9' 76"

$\frac{6.7}{9}$   $\frac{6.5}{8}$   $\frac{7.5}{23}$  2 County Club Dr.

Gas cross @  $\frac{\text{¢}}{\text{ft}}$

Tele. cross @  $\frac{\text{¢}}{\text{ft}}$

Tele. MH. 11' 76"

$\frac{3.6}{9}$   $\frac{3.6}{8}$   $\frac{5.7}{23}$   $\frac{6.1}{39}$  2 County Club Dr.

$\frac{1.0}{9}$   $\frac{1.0}{8}$   $\frac{1.4}{9}$   $\frac{2.2}{18}$



Remero Dr. Cont.

431.09  
431.86

0.71 430.38  
431.15

13.08 443.46  
444.23

5+62

5+70.5

5+70.5

5+75

10.3

5+86

5+91

5+96

6+00

7.3

6+07

6+25

4.4

6+50

1.4

16

4

RE

Water CV. 2' RE

Water CV. 28' RE

Sewer line 38' RE

$\frac{10.6}{9}$   $\frac{10.3}{8}$   $\frac{10.9}{9}$   $\frac{12.4}{31}$  curb line

Sewer line @ 4'

Sewer line @ 9' RE

Water CV. 5' RE

$\frac{7.7}{9}$   $\frac{7.3}{8}$   $\frac{7.8}{9}$   $\frac{8.0}{13}$  curb face

Water CV. 9' RE, FH. 13' RE

$\frac{4.6}{9}$   $\frac{4.4}{8}$   $\frac{4.8}{12}$  curb line

$\frac{1.7}{9}$   $\frac{1.4}{8}$   $\frac{1.8}{12}$



Romero Dr Cont.

443.46  
444.23

0.49 442.97  
443.74

456.17  
1370 456.94

6+72.5

6+75

11.3

7+04.20 F.C.

8.0

7+50

2.4

7+60

1.07

7+65

0.62

7+71

T.P.

456.16  
0.01 456.93

469.27  
1371 470.04

LL

R

RL

End Sh. curd on Lt. Begin rubble gutter, Rt. & LL

11.6  
9

11.3  
8

11.4  
9

8.1  
9

8.0  
8

8.2  
9

2.5  
9

2.4  
8

2.6  
9

Tel. MH. 1' LL

Gas MH. 3' LL

Water CV. 71' LL



Pomero Dr. Cont

469.27  
470.04

8+00 9.6

8+50 3.8

T.P. 0.16 469.11  
469.8813.24 482.35  
483.12

9+00 10.9

9+22.95 8.2

9+52.95 4.1

T.P. 0.21 482.14  
482.9112.28 494.92  
495.19

9+82.95 11.9

10+12.95 7.6

10+12.95 7.6

10+12.95 7.58

10+19 6.73

16 4 26

 $\frac{9.7}{9}$   $\frac{9.6}{9}$   $\frac{10.0}{9}$  $\frac{3.8}{9}$   $\frac{3.8}{9}$   $\frac{4.1}{9}$  $\frac{11.1}{9}$   $\frac{10.9}{9}$   $\frac{10.1}{9}$  $\frac{8.3}{9}$   $\frac{8.2}{9}$   $\frac{8.9}{9}$  $\frac{4.2}{9}$   $\frac{4.1}{9}$   $\frac{4.2}{9}$  $\frac{12.2}{9}$   $\frac{11.9}{9}$   $\frac{12.0}{9}$  $\frac{7.8}{9}$   $\frac{7.6}{9}$   $\frac{7.8}{9}$   $\frac{7.5}{12}$   $\frac{8.2}{17}$ back  
curb

Gas &amp; Elect. MH. 4' Lt

Tele. MH. 2' Lt



Pomero Dr. Cont.

494.92  
495.19

10+42.95

3.4

 $\frac{3.6}{9}$  $\frac{3.4}{0}$  $\frac{3.6}{9}$  $\frac{3.3}{12}$  $\frac{3.4}{17}$ 

T.P.

0.31

494.11

494.88

back  
curb

12.84

506.95  
507.72

10+72.95

11.7

 $\frac{12.1}{9}$  $\frac{11.7}{0}$  $\frac{11.8}{9}$  $\frac{11.7}{12}$  $\frac{11.8}{17}$ back  
curb

11+02.95

7.7

 $\frac{7.8}{9}$  $\frac{7.7}{0}$  $\frac{7.7}{9}$  $\frac{7.7}{12}$  $\frac{7.8}{17}$ back  
curb

11+32.95

3.4

 $\frac{3.5}{9}$  $\frac{3.4}{0}$  $\frac{3.7}{9}$ 

T.P.

0.08

506.87

507.64

13.01

519.88  
520.65

11+62.95

12.7

 $\frac{12.3}{9}$  $\frac{12.2}{1}$  $\frac{12.5}{9}$ 

11+92.95

7.8

 $\frac{7.9}{9}$  $\frac{7.8}{0}$  $\frac{8.1}{9}$ 

12+22.95

3.6

 $\frac{3.7}{9}$  $\frac{3.6}{1}$  $\frac{3.8}{9}$ 

12+49.51 P.R.C.

0.4

 $\frac{0.8}{12}$  $\frac{0.0}{12}$  $\frac{0.6}{9}$  $\frac{0.4}{0}$  $\frac{0.5}{9}$



Romero Dr. Cont

519.88  
520.65

519.44

0.44 520.21

T.P.

532.60

13.16 533.37

12+64

12.08

Tele. MH. 2' PL

12+67

11.36

Gas &amp; Elect MH. 2' H

12+75

10.7

$\frac{8.3}{25}$	$\frac{10.2}{21}$	$\frac{10.6}{19}$	$\frac{11.2}{9}$	$\frac{10.7}{0}$	$\frac{10.9}{9}$
		back curb			

13+00

9.0

$\frac{6.4}{26}$	$\frac{8.8}{21}$	$\frac{9.0}{12}$	$\frac{9.5}{9}$	$\frac{9.0}{0}$	$\frac{8.7}{9}$
		back curb			

13+25

7.2

$\frac{4.9}{27}$	$\frac{7.2}{22}$	$\frac{7.4}{12}$	$\frac{7.8}{9}$	$\frac{7.2}{0}$	$\frac{6.9}{9}$
		back curb			

13+42.57 EC

5.8

$\frac{6.1}{9}$	$\frac{5.8}{0}$	$\frac{5.6}{9}$
-----------------	-----------------	-----------------

13+45.15 BC

5.6

$\frac{3.0}{22}$	$\frac{5.1}{19}$	$\frac{5.2}{12}$	$\frac{5.8}{9}$	$\frac{5.6}{0}$	$\frac{5.6}{9}$
------------------	------------------	------------------	-----------------	-----------------	-----------------

13+75

1.9

$\frac{2.3}{9}$	$\frac{1.9}{0}$	$\frac{1.7}{18}$	gutter
-----------------	-----------------	------------------	--------



## Remera Dr. Cont

532.60  
533.37

532.59

0.01 533.36

T.P.

545.43

12.84 546.20

14+00

112

 $\frac{11.9}{9}$  $\frac{11.2}{0}$  $\frac{10.7}{30}$ 

gutter

14+07

9.80

14+12

9.04

Gas &amp; Heat M.H. 19' PL

Tel. M.H. 24' PL

14+25

7.6

 $\frac{7.9}{9}$  $\frac{7.6}{0}$ 

cable cross

 $\frac{7.2}{75}$  $\frac{6.4}{46.5'}$ 

4.5

5.7

Sewer M.H.

14+50

4.2

541.23

 $\frac{4.7}{9}$  $\frac{4.2}{0}$ 

cable cross.

 $\frac{2.6}{32}$ 

sewer cross.

2.4

4.7

47 57

14+75

0.9

cable cross.

 $\frac{1.1}{9}$  $\frac{0.9}{0}$ 

0.7 gutter

 $\frac{0.7}{75}$ 

14+90

545.36

Water G.V. 6' PL &amp; F.H. 13' PL

T.P.

0.07 546.13

558.70

13.34 559.47

15+00

10.7

 $\frac{11.0}{9}$  $\frac{10.7}{0}$  $\frac{10.7}{9}$



## Pomero Dr. Cont

558.70  
559.47

15+25

7.2

 $\frac{7.9}{9}$      $\frac{7.2}{0}$      $\frac{7.2}{9}$ 

15+50

3.7

 $\frac{3.9}{9}$      $\frac{3.7}{0}$      $\frac{3.7}{9}$ 

T.P.

9.17

558.53  
559.30

571.35  
12.82 572.12

15+75

12.5

 $\frac{12.6}{9}$      $\frac{12.5}{0}$      $\frac{12.6}{9}$ 

15+93.98 P.P.C.

9.6

 $\frac{9.7}{9}$      $\frac{9.6}{0}$      $\frac{9.6}{9}$ 

16+00

8.7

 $\frac{9.0}{9}$      $\frac{8.7}{0}$      $\frac{8.9}{9}$ 

16+25

5.0

 $\frac{5.3}{9}$      $\frac{5.0}{0}$      $\frac{5.2}{9}$ 

16+50

1.2

 $\frac{1.6}{9}$      $\frac{1.2}{0}$      $\frac{1.3}{9}$ 

571.14  
0.21 571.91

583.92  
12.78 584.69

16+75

10.1

 $\frac{10.4}{9}$      $\frac{10.1}{0}$      $\frac{10.2}{9}$ 

16+85

7.02

Sewer. MH. 15' RL



## Pomero Dr. Cont

583.92  
584.69

17+00

6.3

L6.

±

R6

 $\frac{6.5}{9}$  $\frac{6.3}{9}$  $\frac{6.5}{9}$ 

17+30

2.0

Storm Dr.  
Grate 2.85  
9 $\frac{2.0}{9}$ 2.17 Storm Dr.  
9 Grate

17+30.91 FC.

2.0

 $\frac{2.8}{9}$  $\frac{2.0}{9}$  $\frac{2.2}{9}$ 

17+41.5

0.14

Tela M.H. 4' L6

583.85

T.P.

0.07

584.62

596.76  
12.91 597.53

17+47

12.16

Gas &amp; Elec. M.H. 6' L6.

17+50

11.7

 $\frac{11.9}{9}$  $\frac{11.7}{9}$  $\frac{11.7}{9}$ 

18+00

4.5

 $\frac{4.7}{9}$  $\frac{4.5}{9}$  $\frac{4.5}{9}$ 

T.P.

0.02

597.51

609.45  
12.71 610.22

18+50

9.9

 $\frac{10.2}{9}$  $\frac{9.9}{9}$  $\frac{9.9}{9}$ 

19+00

2.7

 $\frac{3.0}{9}$  $\frac{2.7}{9}$  $\frac{2.6}{9}$



## Pomero Dr. Cont

609.45  
610.22

609.37

008 610.14

622.34

12.97 623.11

19+50

8.2

 $\frac{8.6}{9}$  $\frac{8.2}{0}$  $\frac{8.3}{9}$ 

20+00

1.0

 $\frac{1.4}{9}$  $\frac{1.0}{0}$  $\frac{1.0}{9}$ 

20+01.5

0.86

Gas &amp; Elect. MN. 4' 16

T.P.

0.05

622.29

623.06

13.15

635.44  
636.21

20+50

7.0

 $\frac{7.3}{9}$  $\frac{7.0}{0}$  $\frac{7.0}{9}$ 

T.P.

0.13

635.31

636.08

13.03

648.34  
649.11

21+00

12.6

 $\frac{12.9}{9}$  $\frac{12.6}{0}$  $\frac{12.5}{9}$ 

21+15.04 BC

10.4

 $\frac{10.6}{9}$  $\frac{10.4}{0}$  $\frac{10.5}{9}$ 

21+25

8.9

 $\frac{9.0}{9}$  $\frac{8.9}{0}$  $\frac{9.2}{9}$ 

21+42

Water 6V. 1' 16



## Pomero Dr. Cont

648.37  
649.11

21+50

5.2

Lt.

4

Rt

 $\frac{5.1}{9}$  $\frac{5.2}{9}$  $\frac{5.4}{9}$  $\frac{4.9}{12}$  $\frac{4.4}{18}$ 

21+75

2.5

 $\frac{1.9}{9}$  $\frac{2.5}{9}$  $\frac{3.1}{9}$  $\frac{2.5}{12}$  $\frac{2.0}{18}$ 

21+86

Gas cross  $\frac{1.5}{9}$ 

21+95

0.9

Gas  
0.9 cross  
0

21+97.5

0.5

Gas &amp; Elect MH. 9'

22+00

0.4

 $\frac{0.4}{9}$  $\frac{0.4}{9}$  $\frac{0.5}{9}$  $\frac{0.7}{9}$  $\frac{0.1}{12}$  $\frac{10.6}{18}$ 

22+04

0.08

Tele. MH. 2' Lt.

T.P.

0.24

648.10

648.87

12.83

660.93

661.70

22+04

11.25

Sewer MH. 21' Lt.

cul. 5.0 Lt.

22+25

10.7

 $\frac{10.7}{9}$  $\frac{10.7}{9}$  $\frac{10.7}{9}$  $\frac{10.4}{12}$  $\frac{10.0}{18}$  $\frac{7.1}{18}$ 

22+50

8.7

 $\frac{8.2}{9}$  $\frac{8.2}{9}$  $\frac{8.1}{9}$



## Romero Dr. Cont

660.93  
666.70

22+55.23 F.C.

7.6

Lt.

E

Rt

 $\frac{7.6}{9}$  $\frac{7.6}{9}$  $\frac{7.6}{9}$ 

22+75

5.1

 $\frac{5.1}{9}$  $\frac{5.1}{9}$  $\frac{5.1}{9}$ 

23+00

1.9

 $\frac{2.0}{9}$  $\frac{1.9}{9}$  $\frac{2.1}{9}$ 

T.P.

0.06

660.87  
661.64

13.24

674.11  
674.88

23+25

11.9

 $\frac{12.0}{9}$  $\frac{11.9}{9}$  $\frac{12.2}{9}$ 

23+33.45

10.9

 $\frac{10.9}{9}$  $\frac{10.9}{9}$  $\frac{11.1}{9}$ 

23+50

8.9

 $\frac{8.9}{9}$  $\frac{8.9}{9}$  $\frac{9.1}{9}$ 

24+00

2.5

 $\frac{2.5}{9}$  $\frac{2.5}{9}$  $\frac{2.7}{9}$ 

T.P.

0.12

673.99  
674.76

8.08

682.07  
682.84

24+50

5.9

 $\frac{5.9}{9}$  $\frac{5.9}{9}$  $\frac{6.0}{9}$



Pomero Dr. Cont

682.07  
682.84

LE.

4

RE.

25+00

42

$\frac{4.2}{9}$

$\frac{4.2}{9}$

$\frac{4.3}{9}$

25+01

430 677.76

Tele. MH. 9' RE

25+07

411 677.96

G.E. MH. 8' RE

25+50

3.4

$\frac{3.6}{9}$

$\frac{3.4}{9}$

$\frac{3.7}{9}$

25+57

3.41 678.66

Sewer MH. 16' RE

25+59.12 P.P.C.

3.3

$\frac{2.3}{9}$

$\frac{2.7}{9}$

$\frac{3.4}{9}$

$\frac{3.3}{9}$

$\frac{3.6}{9}$

25+65

cut 18' totl.  $\frac{3.5}{9}$  Sewer cross

25+75

3.0

$\frac{3.1}{9}$

$\frac{3.0}{9}$

$\frac{3.3}{9}$

Sewer cross

25+87

$\frac{2.9}{9}$  Sewer cross

26+00

2.6

$\frac{1.0}{9}$

$\frac{2.0}{9}$

$\frac{2.7}{9}$

$\frac{2.6}{9}$

$\frac{2.9}{9}$

26+25

2.2

$\frac{2.4}{9}$

$\frac{2.2}{9}$

$\frac{2.4}{9}$



## Pomero Dr. Cont.

682.07  
682.04

680.45

681.22

T.P.

162

686.24

5.79

687.01

46+50

5.9

26+75

5.5

P.R.C.

26+04.78

5.3

26+07

27+00

5.0

27+07

27+25

4.7

27+50

4.4

L6

E

Rt

4.7	5.1	6.0	5.9	6.1
$\frac{70}{9}$	$\frac{72}{9}$	$\frac{9}{9}$	$\frac{59}{8}$	$\frac{9}{9}$

end con.  
wall

5.6	5.5	5.7
$\frac{9}{9}$	$\frac{8}{8}$	$\frac{9}{9}$

5.7	5.3	5.5
$\frac{9}{9}$	$\frac{8}{8}$	$\frac{9}{9}$

5.4  
Sewer Ch. 9

5.1	5.1	5.0	5.3
$\frac{9}{9}$	$\frac{8}{8}$	$\frac{8}{8}$	$\frac{9}{9}$

Sewer  
cross

6" MH 14' Rt

4.7	4.7	4.7	4.9
$\frac{9}{9}$	$\frac{6}{6}$	$\frac{8}{8}$	$\frac{9}{9}$

Sewer  
cross

4.4	4.4	4.4	4.6
$\frac{9}{9}$	$\frac{5}{5}$	$\frac{8}{8}$	$\frac{9}{9}$

Sewer  
cross



## Romero Drive Cont

			Ll.	¢	Rt.
	686.24 687.01		$\frac{4.3}{9}$	$\frac{4.3}{8}$ sewer cross	$\frac{4.5}{9}$ $\frac{4.6}{10}$ water c.v.
9355 27+64.30 Pl. 2925		45			
27+66					water c.v. online
27+79		12	edge pave. $\frac{4.1}{7}$	$\frac{4.2}{8}$ sewer cross.	$\frac{4.5}{6}$ , $\frac{5.1}{24.5}$ edge con. pave. c.v.
27+93.55		29	con. wall $\frac{1.8}{8}$	$\frac{2.8}{7}$ rock wall flower bed	$\frac{2.9}{10}$ $\frac{3.4}{8}$
28+00		22	$\frac{1.2}{8}$ con wall	$\frac{2.2}{7.5}$ rock wall	$\frac{2.2}{9}$ $\frac{2.7}{7}$ edge con. pave.
	663.86 2.38 684.63				
1310	696.96 697.73				
28+06					sewer M.H. 15' Rt., 70 to 6 ft.
28+08					F.H. 23' Rt.
28+33		10.1		$\frac{9.3}{7}$ rock wall cross	$\frac{10.1}{8}$



## Pomero Drive Cont

696.96  
697.73

28+50	7.7		6.3 8	7.7 0	7.6 1	8.3 7	8.8 8	8.6 15
-------	-----	--	----------	----------	----------	----------	----------	-----------

con wall

Top  
rock wallBottom  
rock wall

4 AG.

edge of  
P.C.

29+00	2.5		1.6 8	2.5 0	2.6 7	3.0 7	3.7 10	3.8 10
-------	-----	--	----------	----------	----------	----------	-----------	-----------

con wall

Top rock  
wallBottom  
rock wall

4 AG.

edge of  
P.C.

29+07	1.9							
-------	-----	--	--	--	--	--	--	--

East end rock wall &amp; Plower body, 1.9

Top  
wallBottom  
wall

T.P. 0.90 698.17

710.96  
1306 711.23

29+37.06 APL (45%)	13.5			13.2 10	13.5 0	14.1 7	13.9 7	
--------------------	------	--	--	------------	-----------	-----------	-----------	--

Back line

29+37+06 APL (45%)	13.5			13.8 13	13.5 0	13.4 7.5	13.0 26	face rock wall
--------------------	------	--	--	------------	-----------	-------------	------------	-------------------

Line ahead

29+67.06 APL	11.5			12.0 10	11.5 0	10.0 1	10.2 10	
--------------	------	--	--	------------	-----------	-----------	------------	--

Line ahead

face of  
rock wallPlower  
bed

29+78

G&amp;E MH. 3.5 LL.



## Romero Drive Cont

710.46

711.23

30+00

9.4

 $\frac{9.3}{10}$  $\frac{9.4}{0}$  $\frac{9.3}{6}$  $\frac{8.0}{7}$  $\frac{8.0}{10}$ Acc  
rock wall

30+50

4.8

 $\frac{4.6}{10}$  $\frac{4.8}{0}$  $\frac{4.8}{7}$  $\frac{3.7}{1.5}$  $\frac{3.7}{10}$ Rock  
wall

30+75

1.4

 $\frac{1.8}{10}$  $\frac{1.9}{7.5}$  $\frac{1.0}{7}$  $\frac{1.4}{0}$  $\frac{1.1}{10}$ Rock  
wall

T.P.

1.30

709.16

709.93

10.45

719.61

720.38

31+01.32

A PL

6.6

back line

 $\frac{6.3}{10}$  $\frac{6.6}{0}$  $\frac{7.0}{10}$ 

30+92

2.1

Ground line next to pump house

713.87

T.P.

5.74

714.64

10.79

724.66

725.43

721.10

3.56

721.87

USGGS A Sta. 721.10

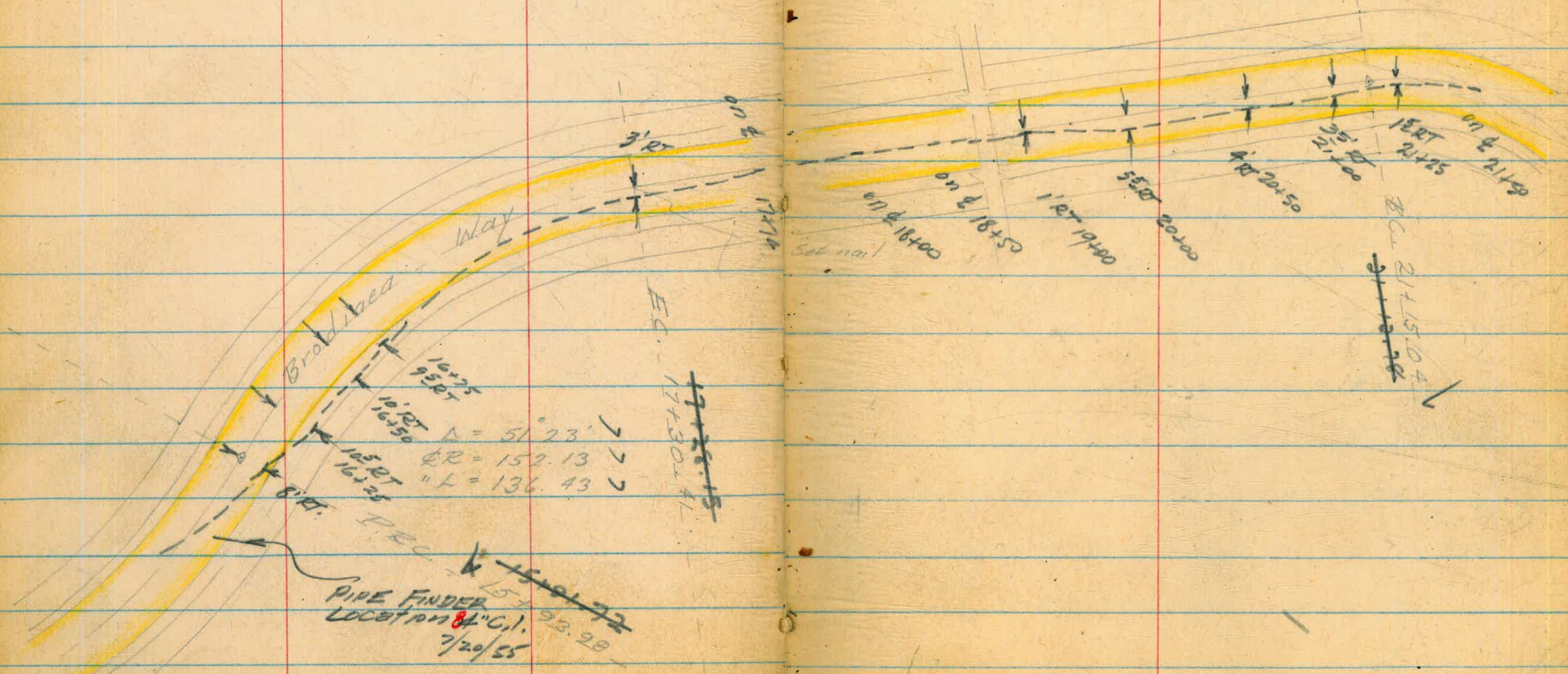
Note: This level circuit  
closed within 001

?



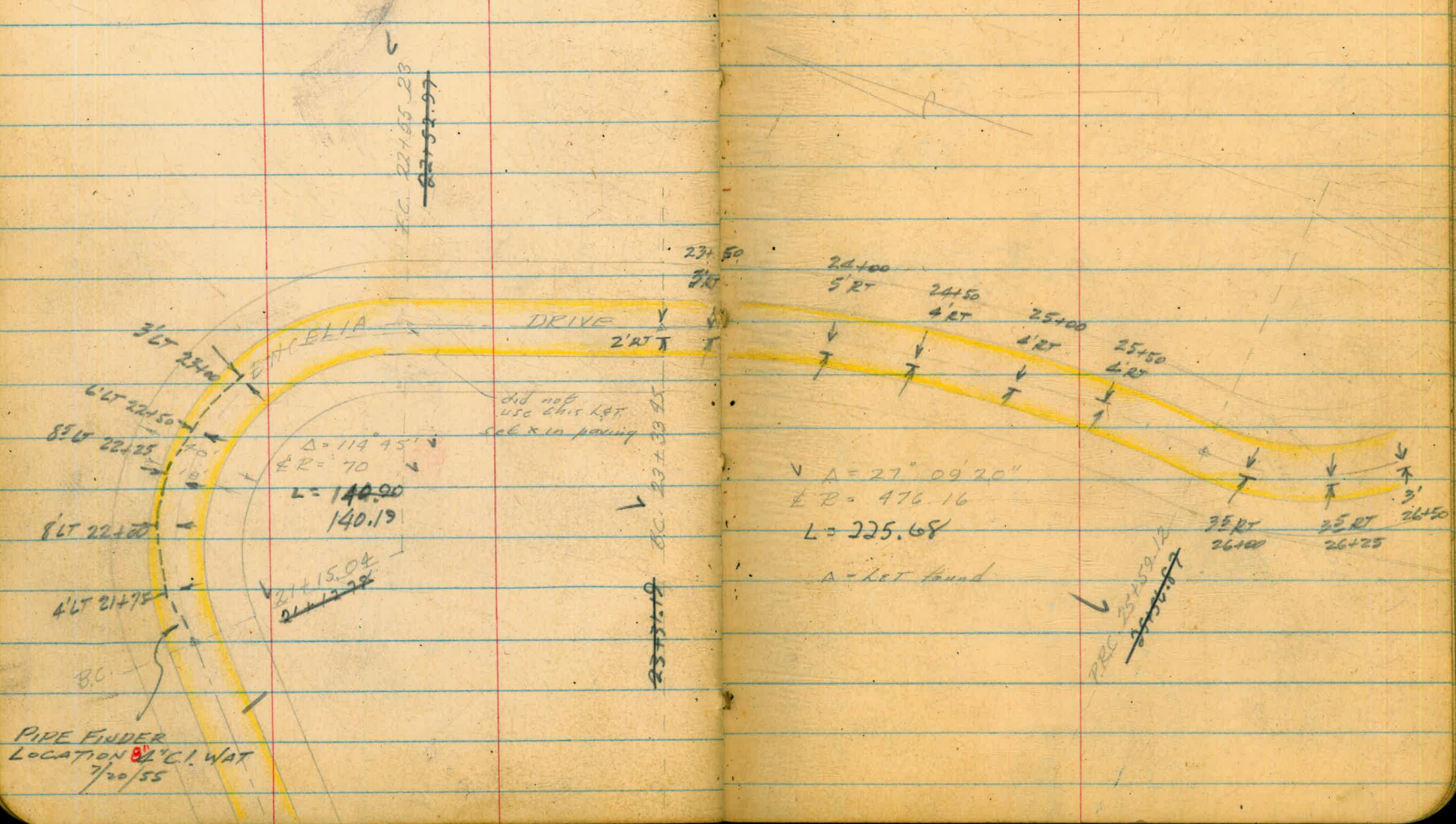
# Romero Drive Cont

Δ = L&T found





Pomero Drive Cont.





# Romero Drive Cont.

103.0  
N-16° 37' W

set nail

fd. 1/2 pipe

See page 29 for details

See Map 2977-B for Reservoir cement

concrete wall  
N-15° 12' 52" E

5' RT 27+37

6' RT 27+00

2' AC PAVT

25' RT 28+00

Set nail

6" rubble core  
15' RT 28+00  
See profile for details

X in pave.  
Set by intersect.

9' ground  
27+66

1.7 RT

$\Delta = 62^{\circ} 07'$   
 $R = 190.41$

P.C. 28+84.29

P.C. 27+84.53  
 $\Delta = 30^{\circ} 01'$

$\Delta = 30^{\circ} 01'$   
 $R = 190.41$   
 $L = 99.75$

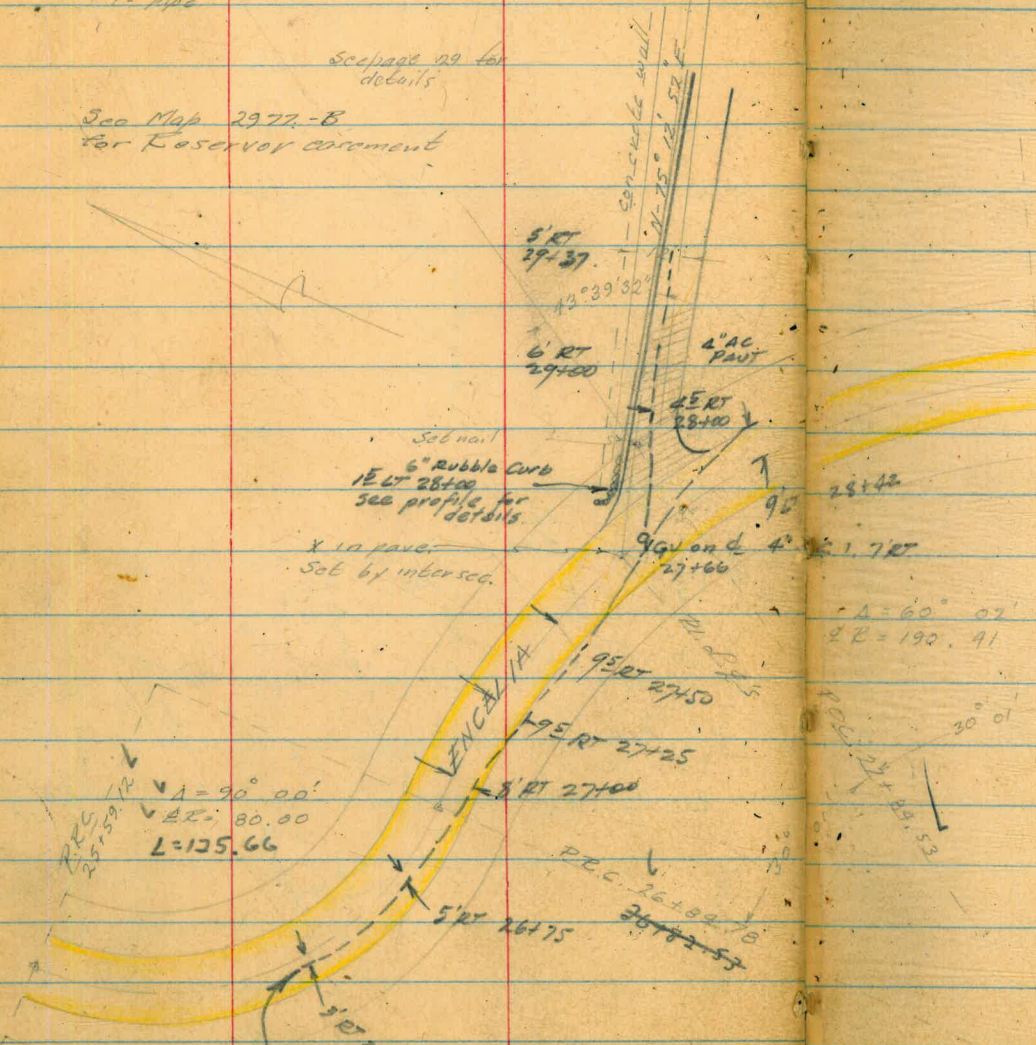
$\Delta = 90^{\circ} 00'$   
 $R = 80.00$   
 $L = 125.66$

5' RT 27+45  
5' RT 27+25  
5' RT 27+00

5' RT 26+75

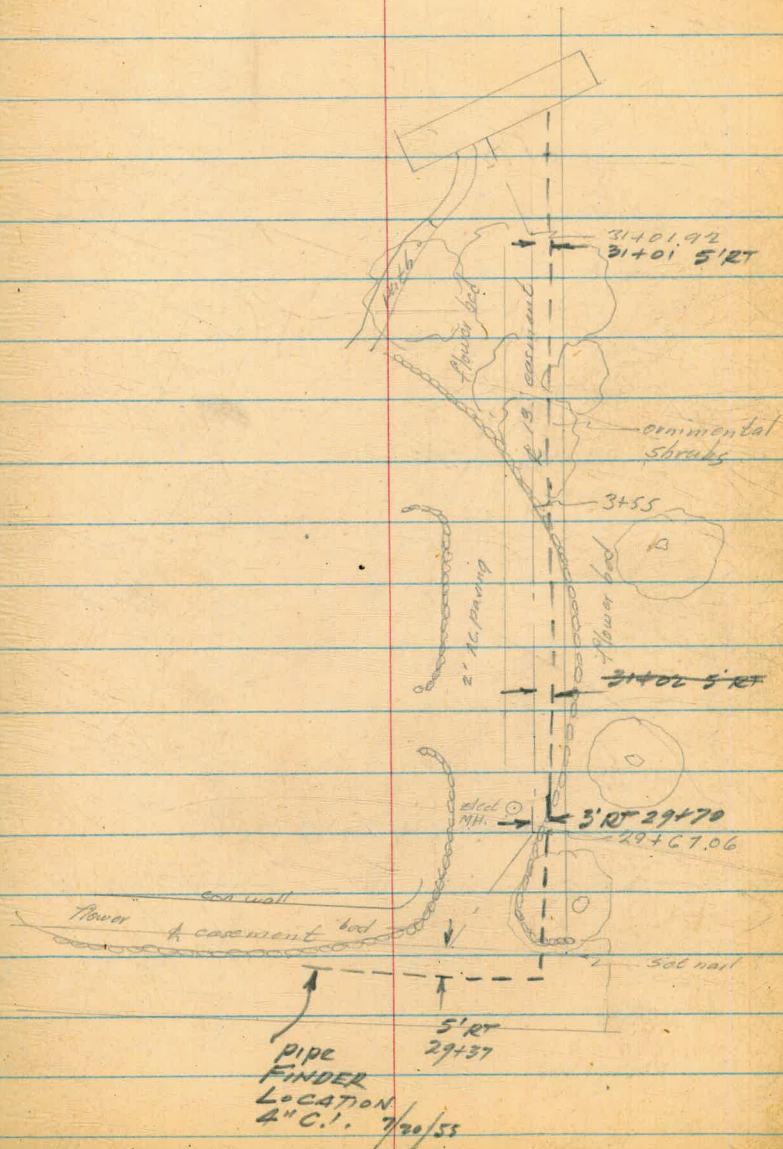
P.C. 26+82.78  
26+82.53

PIPE FINDER LOCATION  
7/20/55





Romero Drive Cont









Profile & Proposed Water Line  
 "C" St. 34th to 35th

0+00 W/L of 34th

0+60 E/W of 34th

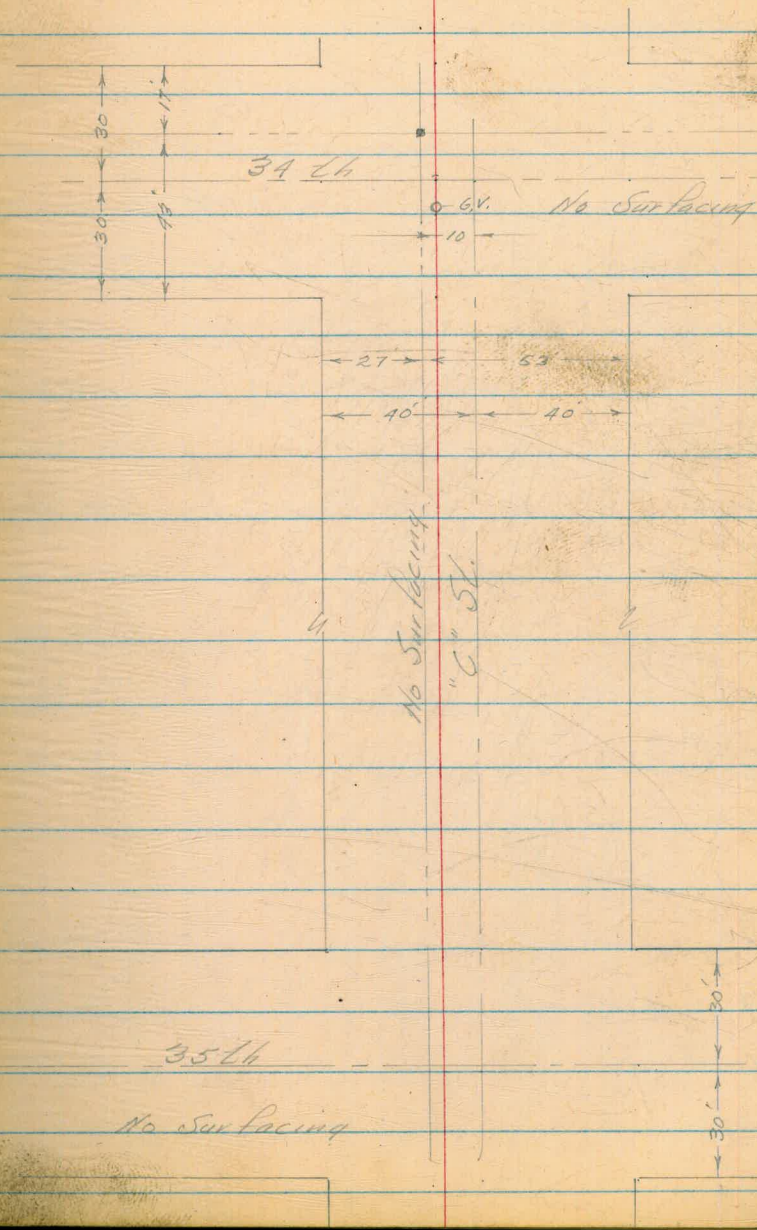
6+59.95 W/L of 35th

7+19.95 E/W of 35th St

Robert  
 Kemp  
 Holahan  
 Alexander

31

4-6-55





WERT  
LEWIS  
HALLOWAN &  
ALEXANDER T

32

137.88

MEMOR. PATH & C

0.68 138.56

0 + 00 12.9 125.66

+18 11.3 127.86

+37 20 129.56

+50 8.7 130.16

+62 6.9 131.66

+85 7.6 130.96

T.P. 12.82 125.79

0.13 125.87

1 + 50 2.5 123.37

+89 10.1 115.77

2 + 00 10.1 115.77

+12 2.2 115.97

WATER GATE

E.H. 36.18

Reduced by J Gray 5-6-55



	125.87		
2+50		2.2	123.67
T.P.		0.87	125.00
	3.85		128.85
2+69		1.9	126.95
+86		0.6	128.25
3+00		1.3	127.55
+35		4.9	123.95
+50		8.0	120.85
T.P.		12.86	115.99
	0.35		116.34
4+00		7.0	109.34
T.P.		12.69	103.65
	0.79		104.44
4+47		7.2	97.24
+55			TOP SLOPE
+71			10" GUM TREE
+76			" " " GUM TREE
			" " "



109.44

4 + 81

6" GUM TREE

+ 86

" " "

+ 91

" " "

+ 96

2" " "

T.P.

12.75 71.69

0.53 72.22

T.P.

12.09 79.12

0.27 79.40

4 + 93

5.7

73.70

5 + 03.37

9.7

69.70

BOTTOM SLOPE

+ 41

14.5

64.90

+ 46

12.5

66.90

+ 50

12.6

66.80

+ 68

12.4

67.0

+ 77

10.3

69.1

+ 78

9.79

68.61

TOP DIRT BERM W. SIDE A.C. ACCESS RD.

7.37 72.03

BM on Guard rail &amp; produced



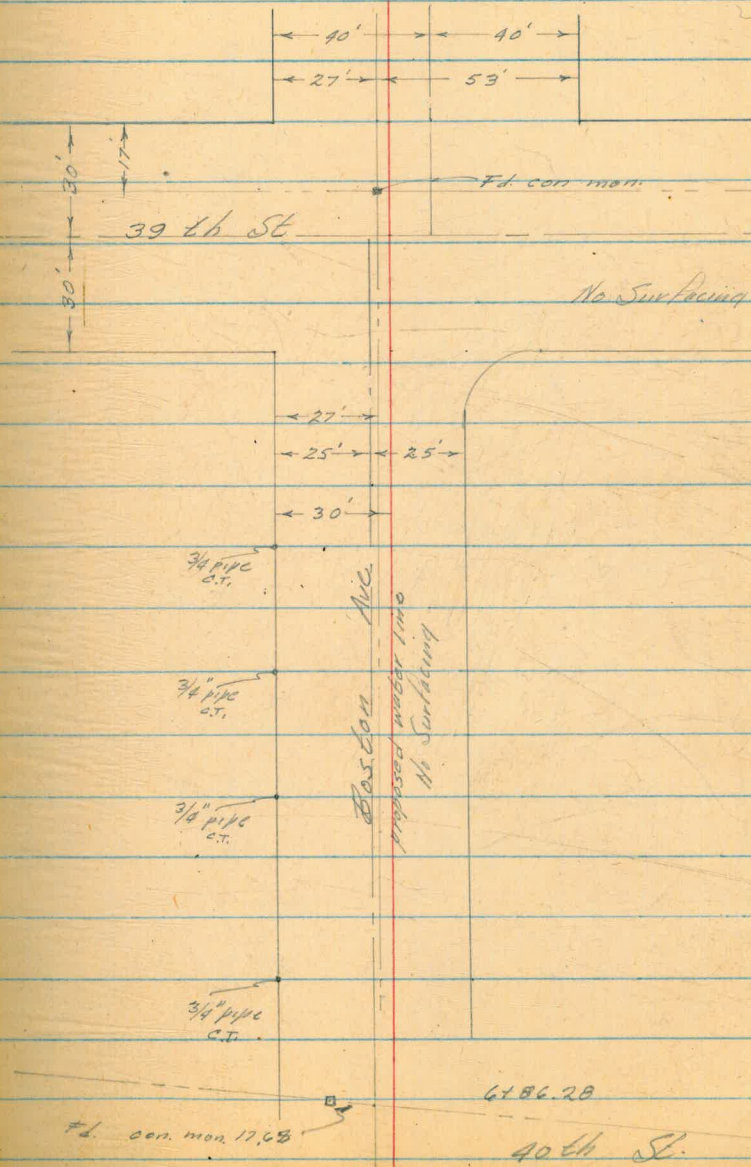
Wert  
Kemp  
Holohan  
Alexander

35

4-29-55

Profile & Proposed Water Line

Boston St, 39th to 40th





PROFILE & PROPOSED WATER LINE

BOSTON ST., 39<sup>TH</sup> TO 40<sup>TH</sup>

	20.31	
11.12	31.43	
T.P.	0.23	31.20
10.41	91.61	
0+00	5.9	35.7
T.P.	1.64	39.97
8.94	48.21	
0+41	1.9	47.0
0+50	1.3	47.6
0+60	2.6	46.3
T.P.	12.59	36.32
1.46	37.78	
1+00	5.8	32.0
1+18	11.9	26.9
T.P.	12.65	25.13
0.92	26.05	

15' RIGHT WATER  
SPR. IN POLE

WEST LINE 39<sup>TH</sup> 8.5 5.2  
T.B.M.  
CON. MON.

5.9 43.0 1.9

5.9 43.5 1.3

6.2 42.7 2.6

8.2 29.58 5.8

13.8 24.0 11.9



26.05

1+28	2.8	23.2
1+50	4.7	21.3
2+00	6.6	19.4
2+50	7.6	18.4
3+00	7.9	18.1
T.P.	7.91	18.14

5.62 23.76

3+50	5.6	18.2
4+00	5.5	18.3
4+50	5.1	5
5+00	5.0	
5+50	5.3	
6+00	4.5	
6+50	4.3	
7+00	4.0	
7+24.55	3.8	
T.P.	3.72	20.07

394 23.98

15' RIGHT WATER

4.2	21.8	2.8
5.8	20.2	4.7
7.1	18.9	6.6
8.0	18.0	7.6
7.8	18.2	7.9

5.4	18.36	5.6
5.1	18.66	5.5
4.8	19.0	5.1
4.7	19.1	5.0
4.9	18.9	5.3
4.4	19.4	4.5
4.5	19.3	4.3
4.5	19.3	4.0
3.9	19.9	3.8

SPK IN POLE 10' 50' CON. MON.



23.98

T.P.

5.98 18.50

3.03 21.53

T.P.

1.26 20.27 = 20.31

SPK. IN POLE



5-16-55

Profile of Proposed Water Line  
Alley B/W 58, No. of Monroe E. of 32nd

Station	Offset	Elevation	Description	Left	Right
		382.39	SERA, Monroe & 32nd		
	2.95	385.34			
0+00	5.0	380.34	S/W of Monroe		
0+12	5.2	380.14	S. curb		
0+32	4.6	380.74	E. of Monroe		
0+38	5.0	380.34	No curb line		
0+50	5.0	380.34		10.6	Right
0+60	4.8	380.54	N/W of Monroe	1.3 381.0 10.5 380.0	4.4 380.9 4.5 382.9
0+80	2.6	382.74		2.3 382.7 10.5 382.7	2.4 382.9 4.5 383.3
1+00	2.2	383.14		1.6 382.7 10.5 382.7	2.0 383.3 4.5 383.7
1+50	1.8	383.54		1.6 382.7 10.5 382.7	1.6 383.7 4.5 383.9
2+00	1.4	383.94		1.4 382.9 10.5 382.9	1.4 383.9 4.5 383.9
T.P.	1.86	383.48			
	4.97	388.45			
2+50	4.0	384.45		4.5 384.0 10.5 383.7	4.7 383.8 4.5 383.5
3+00	5.4	383.05		4.8 383.7 10.5 383.5	5.0 383.5 4.5 383.8
3+50	5.1	383.35		4.9 383.5 10.5 383.5	4.7 383.8 4.5 383.8



	388.95		
4+00	4.9	383.55	
4+50	4.8	383.65	
5+00	5.0	383.45	
5+50	5.0	383.45	
6+00	5.1	383.35	
6+50	5.1	383.35	
TP	4.55	383.90	

3.11 387.01

7+00.36	4.8	382.21	
7+12.36	5.2	381.71	
7+32.36	4.6	382.41	
7+48.36	4.9	382.11	
7+60.36	4.6	382.41	
	5.89	381.12	

Left

384.1

4.4

10.5

4.8

10.5

4.8

10.5

4.9

10.5

5.3

10.5

4.9

10.5

Right

383.6

4.9

4.8

4.8

5.0

4.5

5.0

4.5

5.0

4.5

5.0

4.5

S/W of Madison

So curb

↓

No. curb

1/2 Pa Madison

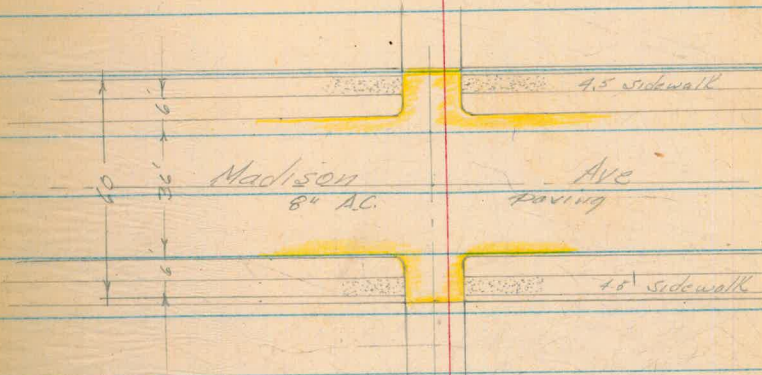
SEBP Bancroft &amp; Madison 381.01



Alley B/L 58 Cont.

7160.36

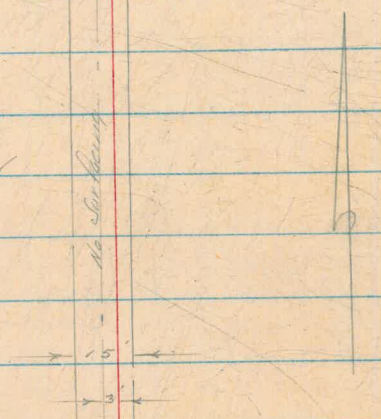
N/4 of Madison



7400.36

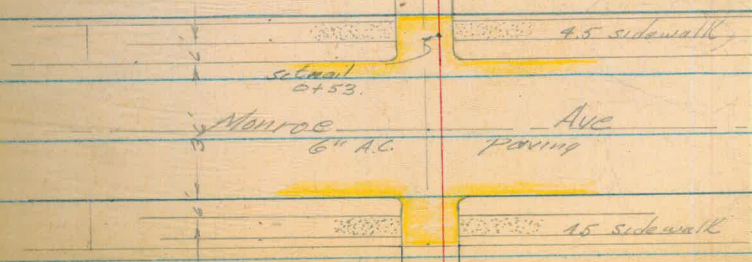
S/4 of Madison

Note LET'S on 32nd & Bancroft.



0+60

N/4 of Monroe



0+00

S/4 of Monroe



Profile & Proposed Water Line  
 Malden St, Collingwood to Lament

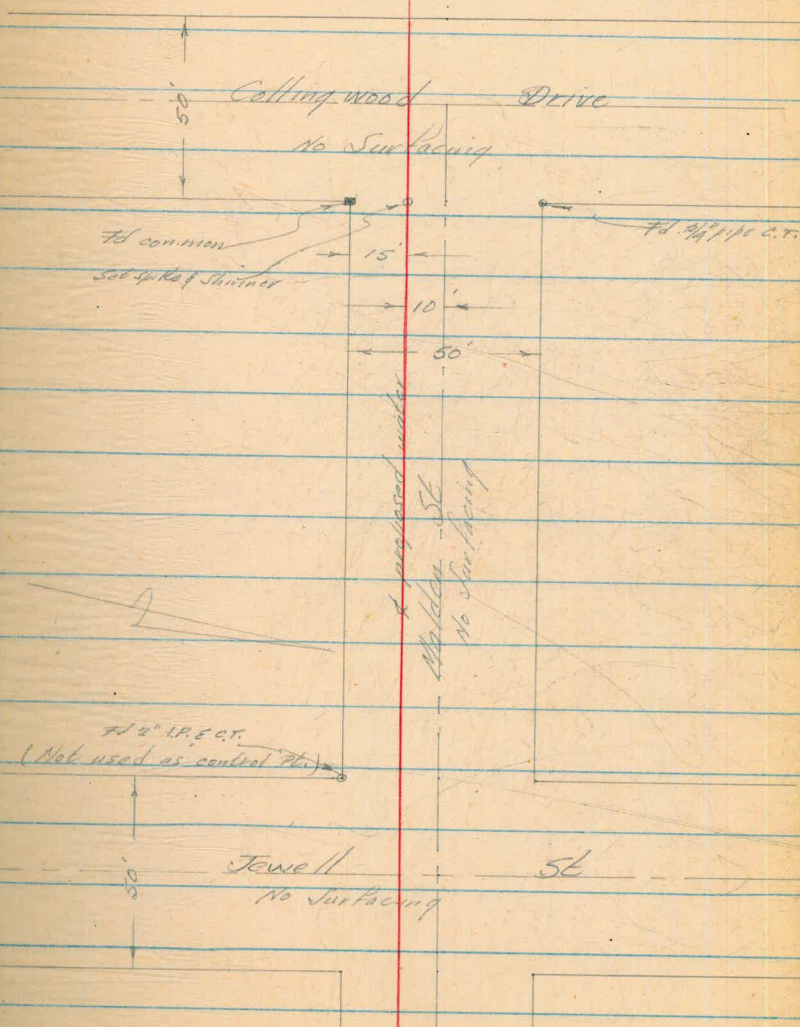
0400

W/ll. of Collingwood

Went  
 Kemp  
 Holahan  
 Alexander

42

6-6-55





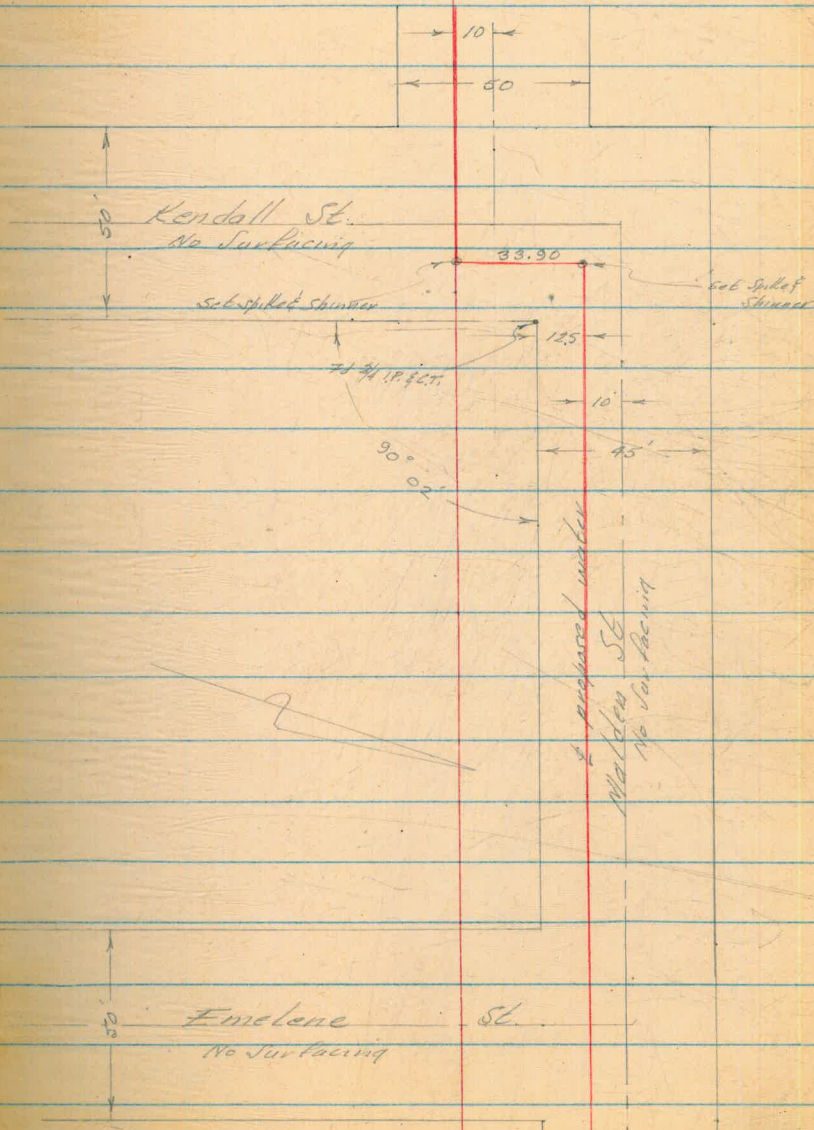
Malden St. Cont.

9+11.19

Angle point  $89^{\circ} 58'$  Del. L6.

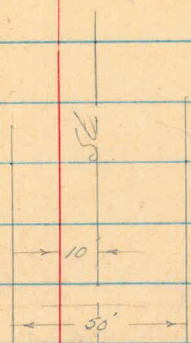
9+45.09

Angle point  $89^{\circ} 58'$  Del. R6.





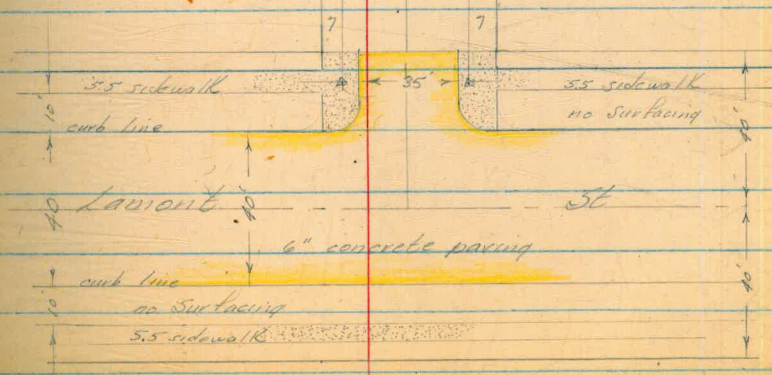
Malden St. Cont



Proposed water  
Malden  
No Surfacing

D = L.S.T.

14+90.40 W/L of Lamont



15+70.40 #11 of Lamont



## Malden St. Cont

		209.80	
	12.83	222.63	
P		0.10	222.53
	12.43	234.96	
P		0.17	234.79
	13.20	247.99	
P		9.36	238.63
	9.64	248.27	
0+00		10.0	238.3
0+18		9.3	239.0
0+20		9.8	238.5
0+43		9.7	238.6
0+50		8.6	239.7
1+00		5.2	243.1
1+50		3.5	244.8
1+75		3.0	245.3
2+00		3.8	244.5

N.W. 2" pipe Jewell &amp; Collingwood

Set TBM. SF. con. mon. Collingwood &amp; Malden



Malden Cont

248.27

2+50 6.9 241.4

3+00 10.4 237.9

3+39

7 13.09 235.18

0.02 235.20

3+50 0.5 234.7

3+59

3+77

4+00 3.0 232.2

4+11

4+29

4+50 4.0 231.2

4+51

4+58 4.2 231.0

5+00 4.8 230.4

5+50 7.2 228.0

6+00 9.4 225.8

12" pepper tree 6' PL

12" pepper tree 7' PL

12" " " 7' PL

24" " " 7' PL

12" " " 6' PL

12" " " 5' PL

Power pole (P-1699) 7' PL



Malden Cont

235.20

6+50 10.8 224.4

P 11.59 223.61

3.95 227.56

7+00 9.3 218.3

7+50 8.4 219.2

8+00 8.4 219.2

8+50 9.0 218.6

9+00 10.9 216.7

9+11.19 11.1 216.5

9+23

9+45.09 6.6 221.0

9+50 6.6 221.0

P 5.96 221.60

0.18 221.78

10+00 2.7 219.1

10+50 7.3 214.5

11+00 11.4 210.4

Angle point in line

Water Ck. 3' RL & 74.6' RL

Angle point in line



## Malden Cont

221.78

13.33 208.45

0.36 208.81

11+50	1.9	206.9
12+00	6.0	202.8
12+50	8.9	199.9
13+00	8.9	199.9
13+50	8.2	200.6
14+00	7.1	201.7
14+50	6.5	202.3
14+90.4	6.24	202.1
15+00	6.7	202.1
15+10.4	7.1	201.7
15+20.	6.8	202.0
15+30.4	6.7	202.1
15+50	6.0	202.8
15+66	6.4	202.4
15+70.4	5.6	203.2

Begin 6" con. pave. &amp; w/l. of lament

W curb line produced

Gas X ing

&amp; lament

F gutter &amp; 6" curb

E/l. of lament



Malden Cont

208.81

636 207.45

SW. LET Malden & Lamont



PROFILE of PROPOSED WATER LINE

SPRINGFIELD ST., SWAN TO ORIOLE ST.

0+00 E/L SWAN ST

1+60.54 X  
1 33  
1+60.20  
1+61.88

5+67.02 w/l ORIOLE ST.

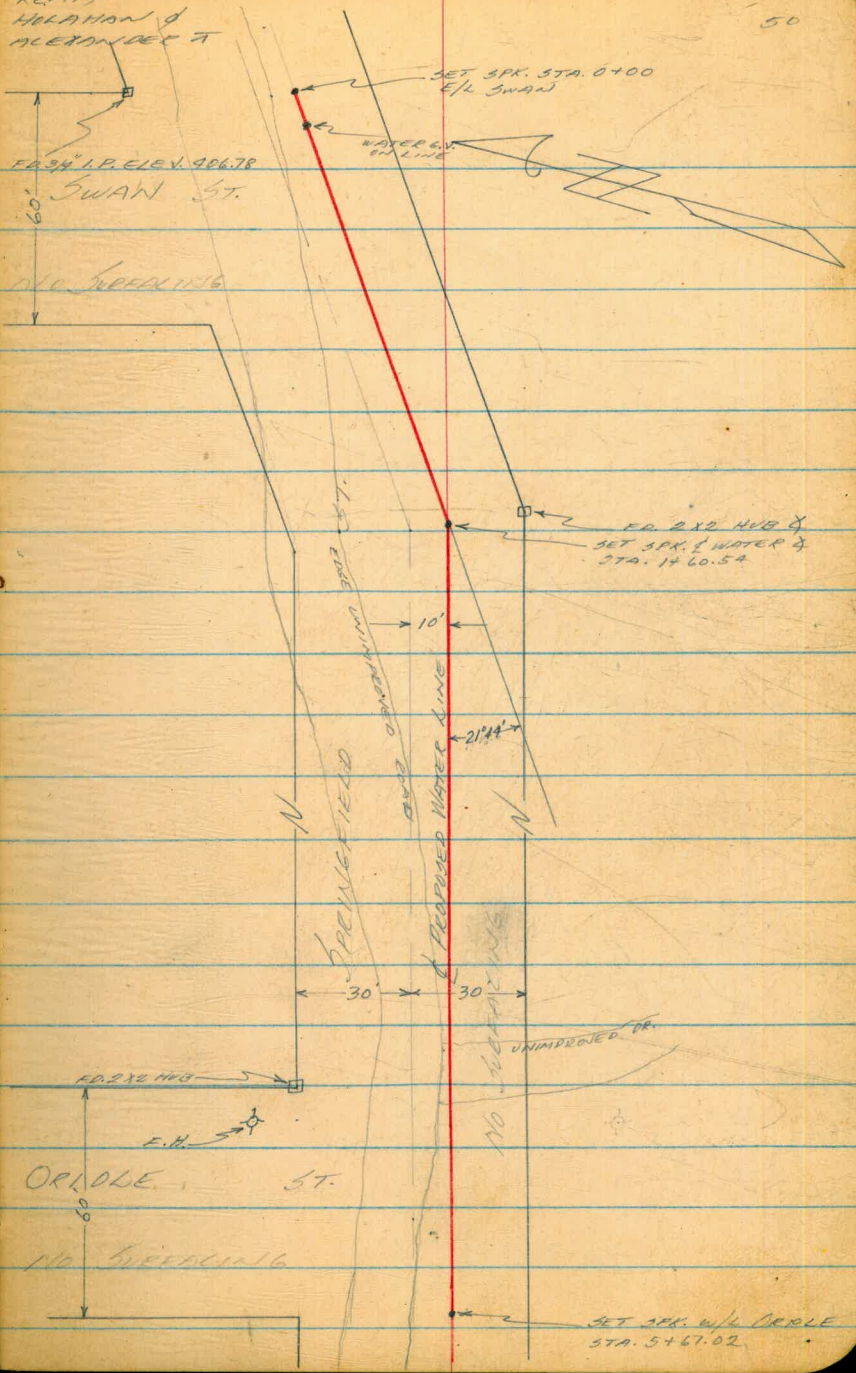
KEMP HOLDMAN & ALGERMAN DET 7

FA 34° L.P. ELEV. 986.78  
SWAN ST.

NO SIDEWALKING

ORIOLE ST.

NO SIDEWALKING



FA 21° HUB X  
SET SPK. & WATER X  
STA. 1+60.54

UNIMPROVED DR.

NO SIDEWALKING

SET SPK. W/L ORIOLE  
STA. 5+67.02



SPRINGFIELD ST. CONT.

406.78

(SEE DRAWING 6)  
NE 3/4" I.P. SWAN & SPRINGFIELD F.R. 896 P. 20

031 907.09

0+00 3.9

W/ SWAN ST

0+17

WATER G.V. ON LINE

0+30 4.6

0+50 6.5 400.6

T.P. 12.79 394.30

0.56 394.86

1+00 9.2 390.7

1+25 10.0

T.P. 12.89 381.97

0.51 382.48

1+50 2.0

1+60.54 3.6

7

2+00 9.3 373.2

T.P. 13.08 362.40

1.00 370.40

2+50 5.3



SPRINGFIELD ST. CONT.

370.40

2+75

2.4

3+00

12.2

T.P.

13.22 357.18

0.30 357.48

3+50

8.4

T.P.

12.64 344.84

1.09 345.93

4+00

7.7

4+25

13.3

T.P.

12.87 333.06

2.05 335.11

4+50

2.1

4+76

11.2

4+87

10.6

4+93

8.8

BEGIN UNIMPROVED DRIVEWAY

5+00

8.7

5+13

8.0

END

"

"

5+17

F.H. 52' BT



SPRINGFIELD ST. CONT.

335.11

5+50

4.1

5+67.02

20

0.68 334.43 = 334.14

53

W/2 ORIOLE ST, END PROFILE

± 2x2 HUB ORIOLE ± N/4 SPRINGFIELD

ADJUSTED ELEV. TO 334.43



KEMP  
HOLAHAN &  
ALEXANDER T

6-22-55

54

PROFILE OF PROPOSED WATER  
URLAND ST., WEAVER TO 360' WEST

WEAVER ST.

ST.

NO SURFACING

0+60

SET SPK. FOR CONTROL



ST.

10'

URLAND

Proposed water line  
No Surfacing

30' 30'

4+50

END PROFILE

SET NAIL STA. 4+50



UPLAND ST. CONT.

366.17

B.M.

CON. MON. E.C. WEAVER 40' S. OF TOOLEY. F.B. 8521 P. 7

235 368.52

T.B.M.

T.P.

10.79 357.73

TOP 9x9 MARKER O.T.A. LINE STA. 730+00

0.07 357.80

0+00

5.4 352.4

0+15

8.1 349.7

T.P.

12.47 345.33

0.59 345.92

0+22

1.4 344.5

E. EDGE UNIMPROVED ROAD - WEAVER

0+46

3.8 342.1

W " " " "

0+50

4.3 341.6

0+60

7.9 338.0

T.P.

13.17 332.75

0.06 332.81

1+00

2.1 330.7

1+50

2.5 323.3

T.P.

13.07 319.74

0.04 319.78



UPLAND ST. CONT.

312.78

2+00

3.1 316.7

2+25

7.0 312.8

2+50

10.3 309.5

T.P.

12.47 307.31

0.59 307.90

3+00

8.1 299.8

T.P.

12.42 295.48

4.37 299.88

3+50

8.8 291.1

4+00

14.4 285.5

4+50

17.0 282.9

T.P.

0.46 297.39

13.04 312.43

T.P.

0.14 312.29

12.64 324.93

T.P.

0.29 324.64

12.80 337.50



UPLAND ST. CONT.

337.52

T.P.

0.77 336.75

11.93 348.68

T.P.

0.02 348.66

10.17 358.83

T.P.

1.09 357.74

10.57 368.31

2.13 366.18 = 366.17

END

STARTING B.M.



SEA BREEZE DR - POTAMAC ST TO  
250' N'LY ALLEGHANY  
PLAN & PROFILE & PROPOSED WATER

3+56.66 FD 3/4" PIPE IN 3" PIPE & ALLEGHANY + SEA BREEZE

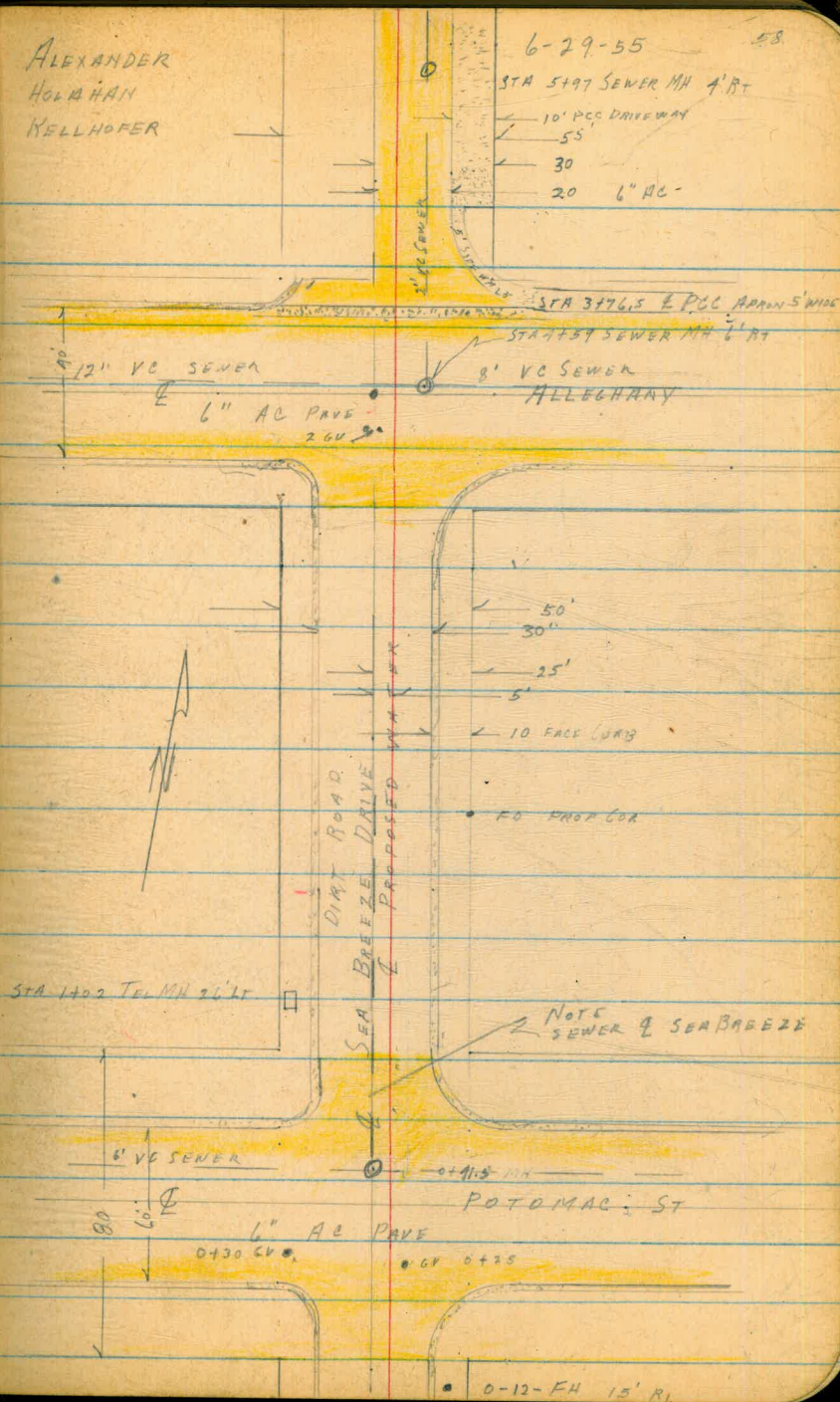
3+37 SLY CURB LINE

0+60 N'LY CURB LINE

0+20 SLY CURB LINE

0+00 SLY PROP LINE OF POTAMAC

ALEXANDER  
HOLMANN  
KELLHOFER





## SEA BREEZE DR

CONT

274.49

BM SWBP ALLECHANY + SEA BREEZE

2.45 276.94

TP

8.96 267.98

8.77 276.75

0-12

FH 15' RT

0+00

8.24

268.51

BEG 6" A.C PAVE

0+20

7.96

268.99

S'ly CURB LINE POTOMAC

0+25

GV 5' RT

0+30

GV 30' L

0+41.5

7.70

269.05

SEWER CROSSING

0+41.5

7.88

268.87

ELY RIM SEWER MH 5' LT 5.9' FLOW

0+50

7.69

269.06

0+60

7.76

268.99

N'ly CURB LINE POTOMAC

0+81

7.85

268.90

END 6" A.C PAVE

1+00

7.9

269.35

1+02

TEL MH 26' LT

1+50

6.1

270.65

2+00

5.0

271.75

2+50

3.8

272.95

Reduced by J Gray 7-5-56



## SEA BREEZE DR

CON

276.75

3+00 2.7 274.05

3+25 1.86 274.89

3+35 FH 46' RT

3+37 1.55 275.20

3+46 26' V 9.5' + 5.5' LET

3+50 1.30 275.45

3+56.66 1.30 275.45

3+59 1.30 275.45

3+59 1.12 275.63

3+67 GAS CROSSING &amp; GAS MH 20' RT

3+74 1.55 275.80

3+76.5 1.60 275.15

3+79 1.52 275.23

TP 0.95 275.80

5.96 281.76

4+00 9.64 277.12

4+50 1.83

BEG 6" AC PAVE

FH 46' RT

S'LY CURB LINE ALLEGHANY

26' V 9.5' + 5.5' LET

E ALLEGHANY

12" SEWER CROSSING 20' TO FLOW

WLY RIM SEWER MH 6' RT DROP FROM EAST 6.2' TO FLOW

GAS CROSSING &amp; GAS MH 20' RT

BEG PCC GUTTER AXON

E " " "

END " " "



SEA BREEZE DR (CONT)

281.76

5+00 1.53

5+50 1.37

5+97.5 1.25

6+00 1.14

6+10 1.14

7.25 274.51 = 274.49

SEWER MH. 4' RT 25' FLOW

SWBP ALLEGANY + SEABREEZE

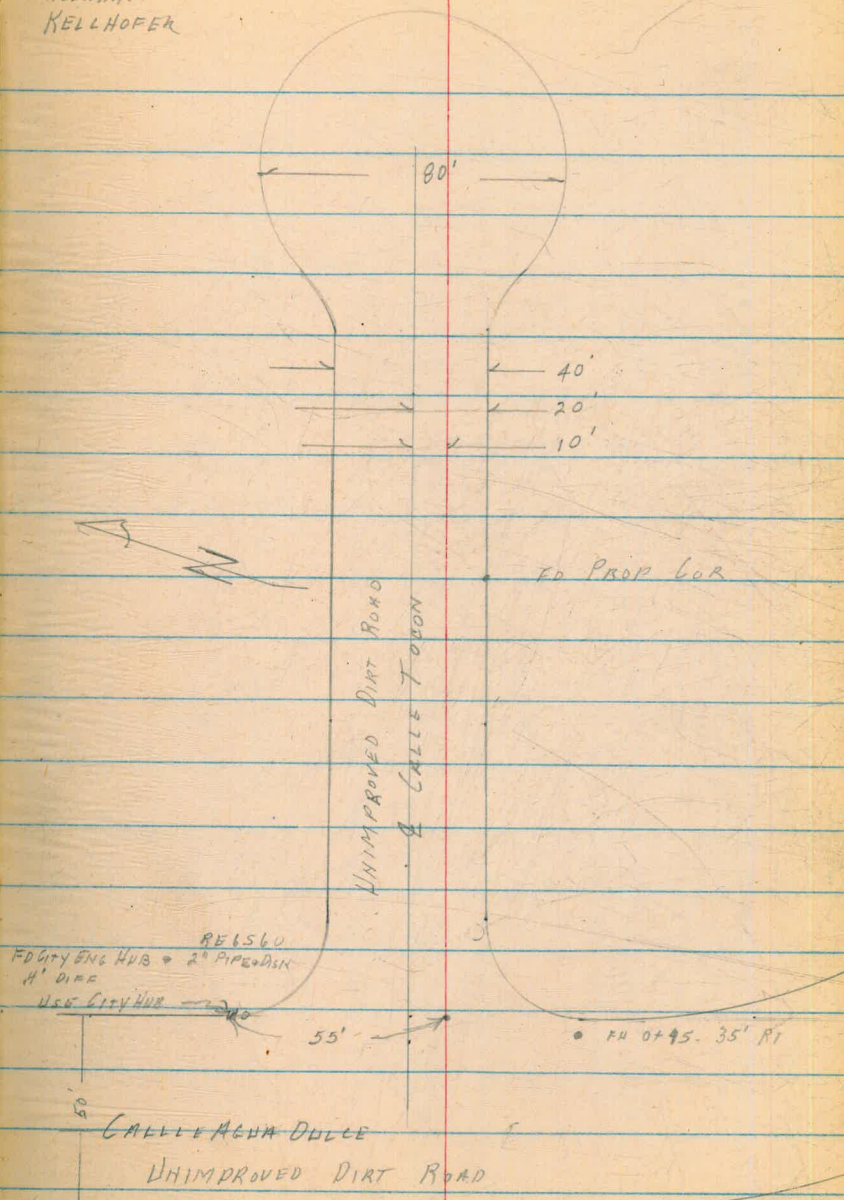
CALLE TOCON  
FROM CALLE AGUA DULCE 210 ELY  
PLAN + PROFILE & PROPOSED WATER

0+00 WLY PROP LINE OF AGUA DULCE

ALEXANDER  
HOLAHAN  
KELLHOFER

6-29-55

62





CALLE TOCON

CONT

BM

278.15

NW BP. IN Roll CURB CUMBERLAND &amp; CALLE SERENA

11.72 289.87

TP

0.73 289.14

12.64 301.78

TP

0.46 301.32

13.01 314.33

TP

3.58 310.75

3/4 TP RE 6560 STA 0.475 30' LEFT

8.50 319.25

0+00

10.1

309.15

0+08

POWER POLE 5' LEFT

0+50

7.9

311.35

LEFT

 $\frac{9.6}{10}$ 

4

RIGHT

 $\frac{3.0}{10}$ 

1+00

5.1

314.15

 $\frac{10}{10}$  $\frac{2}{2}$  $\frac{1}{10}$ 

1+12

4.6

314.65

 $\frac{7.1}{10}$  $\frac{6.9}{7}$  $\frac{3.7}{10}$ 

1+50

4.1

315.15

 $\frac{6.4}{10}$  $\frac{6.4}{6}$  $\frac{3.2}{10}$ 

2+00

4.3

314.95

 $\frac{5.7}{10}$  $\frac{5.6}{3}$  $\frac{4.2}{3}$  $\frac{3.3}{10}$ 

2+50

1.8

314.45

 $\frac{6.4}{10}$  $\frac{6.0}{1}$  $\frac{4.2}{1.2}$ 

Reduced by J. Gray 6-30-55

## CALLE TOCAN (CONT)

319.25

TP

13.07 306.18

0.65 306.83

TP

12.70 294.13

0.39 294.52

TP

9.92 284.60

2.55 287.15

CK BM

9.06 278.09 = 278.15

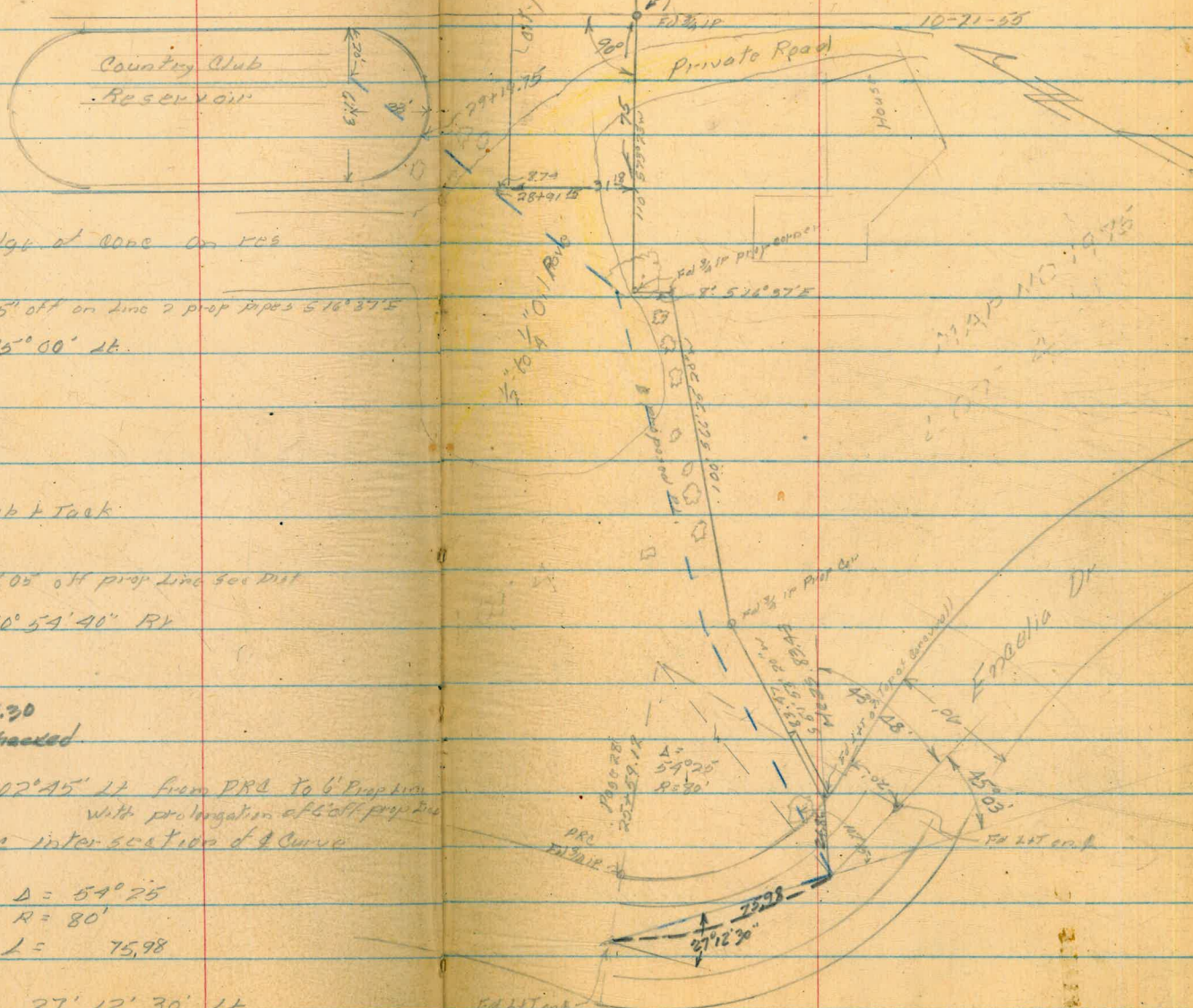
NWBP CUMBERLAND + CALLE SERENA



Country Club Res  
to Encelia Dr

West  
Williams  
Kellhofer

65



29+19.75 Top edge of cone on res

5' off on line 2 prop pipes S 16° 37' E

28+41 1/2 35° 00' Lt.

22+76.78 POT Hub & Tack

6.05' off prop line see dist

27+39.46 AH 10° 54' 40" Rt

27+43.40 BK

108.30  
Rechecked

26+35.10 102° 45' Lt from PRC to 6' Prop line  
with prolongation of 6' off prop line

26+35.10 POC intersection of 4 Curve

$\Delta = 54^{\circ} 25'$   
 $R = 80'$   
 $L = 75.98$

25+59.12 PRC 27° 12' 30" Lt



Country Club Res  
Cont

	6.13	684.78		678.66
26+35 <sup>12</sup>			4.74	680.04
26+46 <sup>50</sup>			4.76	680.02
+48 <sup>6</sup>			4.72	680.06
+48 <sup>2</sup>			4.13	680.65
+50			4.0	680.78
26+60			3.9	681.48
26+59			3.5	681.28
JP	1298	696.86	0.80	683.98
26+67				
+71				
+75			11.1	685.76
+78				
+83				
27+00			5.5	691.36
	11.15	707.85	0.16	696.70
27+39 AL & AH			5.9	702.0
27+43 <sup>40</sup> BK				
+50			4.0	703.9
+56				

25+50 See page 21  
TBM East River Sewer MH 16' RT 678.66  
6.13  
694.78  
7.03  
677.75 gutter  
edge of. Cone paving Begin Rock Cement  
butt of gutter  
Top Rock cement curb 8" wide  
4" Flowering Acacia Tree on ♀  
6' RT begin 4' High Cone Ret wall  
end of cone retaining wall 6' RT  
8' RT 3 3/4" Acacia Tree  
11.8  
6' RT  
10.3  
6' RT  
8' RT 5" Dia Flowering Acacia Tree  
4' RT 1/2" Dia Olive Tree  
6.4  
6' RT  
4.6  
6' RT  
5.6  
6' RT  
5.4  
6' RT  
4.1  
6' RT  
3.8  
6' RT  
4' RT 6" Dia Acacia Tree



	707.85		
11.60	716.43	3.02	704.89
27+76		6.7	709.73
+78			
+85			
+90			
+94			
28+00		4.7	711.73
+03			
+13			
+16		4.55	711.88
+ 41.12 $\Delta$		4.52	711.91
+41.12			
+44			
+50		4.30	712.13
+95		2.11	714.32
+96		1.42	715.01
+98			
29 +00		0.8	715.63
8.90	725.20	0.03	716.40

$\frac{6.8}{6.21}$        $\frac{6.9}{6.81}$       Rock Wall  
 6' RT Small Ornamental scrub  
 4' RT 1" Dia Acacia Tree  
 6' LT 1/2" Dia Oleander Bush  
 25' RT 2" Dia Acacia    5' RT 5" Dia Acacia  
 $\frac{1.27}{8' RT edge AC pave}$        $\frac{4.7}{6' RT}$   
 5' LT Ornamental Bush      4' RT 1" Dia Acacia  
 2' RT 1" Dia peach tree      9' RT 12" long Bush Ornamental  
 begin AC pave      6" Rock wall border  
 5' RT to Rock wall border  
 6' RT to clump ornamental bush  
 7' RT to 12" Dia Overhanging Tree evergreen  
 end of AC paving face of 6" Rock border  
 Top of Rock border  
 2' RT to Native Calif bush  $\frac{3}{4}$  Dia  
 $\frac{0.6}{6.11}$        $\frac{1.3}{6.81}$

5.6  
13.3  
18.9

725.20

29+03

6' x 7" Dia Acacia Tree

+16

5.3

719.90

7' High Cyclone Fence

+19.25

5.0

720.2

edge Concrete wall edge Res

+19.8

3.9

721.3

Top wooden Roof of Res

18.9 ±

Bottom of Res

4.13 721.07 = 721.07

0.845 Mon see page 25



COUNTRY CLUB RES FEEDER  
MAIN.

STKS FOR 12" A.C.

T.B.M.	11.83	690.49	178.66
26+50			10.2 680.3 676.1
+62			7.8 682.7 677.4
+75			3.9 686.6 681.7
T.P.	12.04	702.11	0.42 690.07
27+00			10.2 691.9 687.8
T.P.	11.74	713.37	0.48 701.63
27+43.40 BK			
27+38.46 AH			11.2 702.2 698.1
27+50			9.2 704.2 699.9
28+00			1.8 711.6 707.2
+12			1.5 711.9 707.8
28+41 <sup>12</sup>			1.4 712.0 708.0
28+50			1.3 712.1 708.1
T.P.	5.86	718.93	0.30 713.07
28+88			5.2 713.7 709.8
29+00			3.1 715.8 711.6
29+09			1.0 717.9 714.0
CHECK			6.76 712.17 = 712.13

WEST  
WILLIAMS  
VARONFAKIS X  
KELLHOFER †

69.

11/22/55 SUNNY

EAST RIM SEWER M.H 16' RT. (SEE PAGE 21)

C4 <sup>2</sup>

C5 <sup>3</sup>

C4 <sup>9</sup>

C4 <sup>1</sup>

C4 <sup>1</sup>

C4 <sup>3</sup>

C4 <sup>4</sup>

C4 <sup>1</sup>

C4 <sup>0</sup>

C4 <sup>0</sup>

C4 <sup>0</sup>

C3 <sup>9</sup>

C4 <sup>2</sup>

C3 <sup>9</sup>

END WORK

STA 28+50

PAGE 67

Country Club Di-  
12" AC Feeder Main

70

26+30

4' 11" to CI Pipe

26+20

4' " " " "

26+10

4' " " " "

26+00

4' 11" " " "

25+90

4' 11" " " "

25+80

4' 11" " " "

25+70

5' 11" " " "

25+59 1/2

5' 11" " " "

25+50

5' 11" " " "

25+25

3' 11" " " "

25+00

1' 11" " " "

24+75

2' 01" " " "

24+50

2' 11" " " "

24+25

2' 11" " " "

24+00

2' 11" " " "

23+75

3' 11" " " "

23+50

3' 11" " " "

23+00

3' 11" " " "



22+55<sup>23</sup>

22+50

22+40

22+30

22+20

22+10

22+00

21+90

21+80

21+70

21+60

21+50

21+40

21+30

21+20

21+15<sup>00</sup> 504<sup>0</sup> Lt to 2 pipe4<sup>5</sup> Lt " " "4<sup>6</sup> Lt " " "4<sup>7</sup> Lt " " "4<sup>8</sup> Lt " " "4<sup>9</sup> Lt " " "4<sup>3</sup> Lt " " "4<sup>5</sup> Lt " " "4<sup>6</sup> Lt " " "4<sup>8</sup> Lt " " "5<sup>0</sup> Lt " " "5<sup>0</sup> Lt " " "5<sup>0</sup> Lt " " "5<sup>5</sup> Lt " " "5<sup>5</sup> Lt " " "5<sup>1</sup> Lt " " "

COUNTRY CLUB DR.  
12" A.C. FEEDER MAIN

T.B.M.	11.09	391.55	380.46
T.P.	7.43	397.40	1.58 389.97
0+00		9.90	387.50
0+00 (D)		2.5	393.9 386.8
0+22 <sup>2</sup> 45' Bend		5.6	391.8 385.2
0+30		6.7	390.7 385.0
0+40 (L)		8.9	388.5 384.6
0+48 45' Bend		10.0	387.9 384.3
0+58 <sup>5</sup> 45' Bend		9.3	388.1 384.5
14+75		8.3	389.1
	2.93	388.56	11.77 385.63
			8.10 380.46 = 380.46

WEST  
WILLIAMS X  
VARONFAKIS  
KELLHOFER †

72

12/7/55 Windy + Cold

14T STA 1700 B.C. (PAGE 5)

Top of 8" Tee

C7	<sup>1</sup>	H. 397.40	
C6	<sup>6</sup>		6.7 = 390.7
C5	<sup>7</sup>		7.7 391.7
C3	<sup>9</sup>		9.4 388.0
C3	<sup>1</sup>		10.6 386.8
C3	<sup>6</sup>		9.4 389.0

ST

WATER METERS

4+22	RT.	7354
7+58	RT.	7330
9+25	RT.	
10+03	LT.	
10+71	RT.	7308
13+29	RT.	7260
14+75	RT.	7258 } Not Highlined
14+60	RT.	7252 }
15+00	LT.	
15+63	RT.	
16+91	LT.	7330
16+95	RT.	
17+68	LT.	
18+16	RT.	
18+55	RT.	



## WATERS METERS (CONT.)

19+05	RT.
19+95	RT. & LT.
21+05	RT.
22+00	RT.
22+55	RT.
23+04	LT.
24+20	LT.
25+15	LT.
25+97	LT.
26+74	LT.

ASH ST.  
31<sup>ST</sup> TO FERN ST.

74

BM	218	237.25	235.07	NWBP ASH 31 <sup>th</sup>
0+35	G.V. BY CITY		231.2	
0+50			231.2	
0+75			231.2	
1+00			230.8	
1+50			229.9	
2+00			227.4	
3+50			226.2	
2+75			225.5	
3+00			224.7	
3+10	8" x 6" CROSS BY CITY		224.4	NOT MK'D
3+10	5' 50" G.V. BY CITY			
3+20			224.0	
3+50			226.0	
4+10			226.9	
4+50			227.7	
5+00			228.8	4985.50 5412.50.
5+50			229.8	
5+53	F.H.TEE (3)		229.8	
5+85	G.V. BY CITY		229.6	
5+90	16" x 6" REDUCER END W/EE		229.5	NOT MK'D
			233.01	



Lower OTAY Lake  
Transit Traverse for Topo Survey

WEST  
WILLIAMS  
VARONFAKIS  
KELLHOFER

75

15+60  
11 30  
A 24

12/29/55

4  
1 + 61.25 =  
42 + 75      109° 34' 50 RT To 2 + 39.85 X

25 + 95 X      108° 53' 20 RT. R.H. NAIL      Set Hub + Tack      30' S.E. FROM S.E. CORNER HOUSE # 1548

22 + 00 X      55° 35' 15 RT R.H. NAIL      Set Hub + Tack      STATION ON TREE 16.5 OFF  
9/19/62 CAW      35' S.E. FROM S.E. CORNER HOUSE # 1538

18 + 30<sup>02</sup>      Set PK in @ AC Road      Set Hub + Tack  
45 41 50 LT R.H. NAIL

15 + 60 X      67° 00' 45 RT - R.H. NAIL      Set Hub + Tack      32.7 No. OF LIGHT POST  
LT SIDE OIL TOP RD.      17+29  
15+60  
7:29

11 + 36 X      57° 27' 20 RT R.H. NAIL      Set Hub + Tack      13.5 LT P.P. 181501  
DAM DEC 28, 60 (57° 28' 05")

5 + 46.85 X      62° 21' 10 LT R.H. NAIL      Set Hub + Tack      RC Set 2" x 2" Redwood 12,2360, CAW  
N SIDE DIRT RD @ TREE STUMP 2' DIA.

2 + 39.85 X      69° 30' 40 RT      Lt To      & DAM 6' OUT FROM OTAY DAM NAME PLATE

1 + 61.25 X      11° 49' 10 LT      Lt T      & DAM B.C. of CURVE

0 + 00      East End Cone Wall West Side      Spillway      Lt to Top of Wall



LEVELS AT LOWER OTAY  
(FOR TOPOGRAPHY)

1-19-56  
SHOREY  
KEMP  
SMITH

76

BM	4.80	502.82		498.02
TP	12.24	510.53	4.53	498.29
TP	8.83	518.43	6.93	509.60
TP	2.32	517.19	3.62	514.81
TP	6.42	516.01	7.60	509.59
TP	10.27	525.82	0.46	515.55
TP	11.66	536.74	0.74	525.08
CK BM	4.93	537.14	4.53	532.21
TP	0.03	524.25	12.92	524.22
TP	3.33	516.67	10.91	513.34
TP	0.03	504.90	11.80	504.87
TP	0.34	492.01	13.23	491.67
TP	0.21	479.80	12.42	479.59
TP	0.02	466.70	13.12	466.68
TP	0.02	453.65	13.07	453.63
TP	0.08	440.45	13.28	440.37
TP	0.20	427.72	13.93	427.52
TP	0.24	414.67	13.29	414.43
TP	0.25	401.73	13.19	401.48
TP	2.74	395.56	3.11	392.62

CHISEL MK. ON 6" I. BEAM AT LEVEL GAUGE ON DAM

BRASS TABLET  
U.S.C. & G.S. SURVEY BM H-891 - 1955 IN 1" DIA. CONG. MK.



LEVELS  
(CONT'D)

1-20-56  
SHOREY  
KEMP  
SMITH

77

NOTE: See Also pg 79  
For check Levels

395.56

CK. BM	7.13	388.43	= 397.253	U.S.G. & G.S. BM. { 27'S.W. ROAD - 30'S. GATE & FENCE COR. & APPROX. 800' S.E. FILTRATION PLANT H-50 - 388
BM	5.27	502.11	496.84	✓ CHISEL MK. ON 6" T. BEAM GAUGE ON DAM (ADJ. ELEV.) 1.18
TBM	12.02	508.53	5.60 496.51	HUB STA. 5+46 <sup>25</sup> Δ PT.
TP	13.15	521.14	0.54 507.99	
TP	13.17	534.19	0.12 521.02	
TP	6.76	540.92	0.03 534.16	
TBM	0.36	540.76	0.52 540.40	HUB STA. 11+26 Δ PT.
TP	3.36	537.23	6.89 533.87	
TBM	0.67	529.73	8.19 529.04	HUB STA. 15+60 Δ PT.
TBM	4.72	527.12	7.33 522.40	HUB STA. 17+29 Δ PT.
TP	13.03	540.04	0.11 527.01	
TP	8.04	547.48	0.60 539.44	
TBM	6.18	549.67	3.97 543.51	HUB STA. 22+00 Δ PT.
TBM	3.48	542.06	11.11 538.58	HUB STA. 25+25 Δ PT.
CK. BM	11.01	531.05	= 531.03	U.S.G. & G.S. SURVEY BM - 4891-1255 { ADJUSTED ELEV. CORR. 1.18 SEE PG. 76 70' N. HOUSE NE 1072 1/2 CROWELL RD. & 30' W. OILED RD.



TIES TO TRAVERSE AT  
OTAY DAM LOCATION

NAIL IN  
3'x3'  
RW POST

37+05<sup>10</sup>

N.G.  
BEATTY

OTAY RANCH  
FENCE  
LINE

CONC.

MAINTAIN WITH 4'x4' POST INTERSECTION OTAY RANCH FENCE  
LINE

34+45 APT. 00° 12' RT.

FD. 2'x2' HUB

260.10'  
36° 02' 15"  
39' 10 1/2"

6° 54'

72.94'  
300'

31+45 APT. 16° 48' RT.

FD. T. PIN

14° 23' 30"

5.50'

△ SOUTH  
DAM

NAIL IN  
3'x3"  
RW POST

NE Cor. Otay Ranch.

April 26 1956  
BEATTY  
SMITH.

See also pg 11  
FB 432

25+95 APT. 7° 40' LT.

SEE PAGE 75 FOR TRAVERSE

POST IN  
CONC MON SW Cor. SANJAL RANCH

2° 59' 30"

33° 02' 20"

23+00 APT.

34+45  
A PT.  
0° 12' RT

TO So. DAM



CHECK LEVELS  
OTAY RES  
USGS BM to DAM

Beatty  
WEST  
4/23/57

BM	11.16	398.41		387.253
ID	11.17	409.38	0.20	398.21
SET TBM	1.14	408.44	2.08	407.30
CK TBM	7.72	408.44	7.72	400.72 = 400.58
TBM	13.14	420.44	1.14	407.30
ID	12.74	432.89	0.29	420.15
ID	13.07	445.91	0.05	432.84
ID	12.39	457.97	0.33	445.58
ID	13.29	471.17	0.09	457.88
ID	13.02	483.93	0.26	470.91
ID	13.05	496.77	0.21	483.72
TBM	12.89	508.50	1.16	495.61
ID	12.97	521.28	0.19	508.31
ID	12.66	533.13	0.81	520.47
ID	11.10	541.18	3.05	530.08
ID	0.48	541.46	0.20	540.98
ID	0.12	528.68	12.90	528.56
ID	0.01	515.62	13.05	515.63
ID	5.80	508.48	12.96	502.68
CK BM on Dam.			11.72	496.76 = 498.02

496.81 FB 281-69  
496.84 P9.77

USGS BM 480 - 388 - 1938

P.P. 81011 Junct. of roads Spike in Pole  
CHIS # NE COR CHLOR. LOADING PLATFORM FB 281-74

NW Cor Conc Stone platform

= 531.35 (Mike)  
= 542.26 (Mike)

498.02  
496.76  
diff 1.26

496.36  
5.61  
75



3°10'15"  
6°20'30"

710424  
65 94  
7+70.26

36°02'15"  
~~43°58'~~  
72°04'30"

14

*[Handwritten signature]*

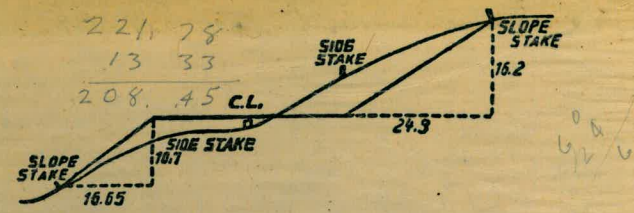
721.87  
720.38  
7 1.49

584.69  
5 77.67  
4.02

2640  
25 59.12  
80.88

285  
217  
302  
25

N  
75 12 52  
16 37  
91 49 52



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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