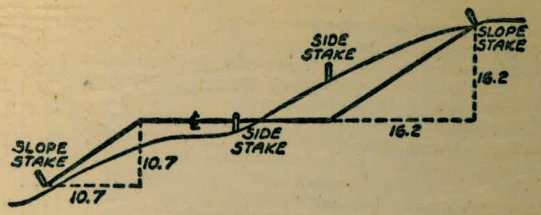


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

to 850' South prelim Cr-23 PRELIM alice 29

Altadena Ave 120' South of Sterling Ct 28

1st St Logan to T St Prelim Cr-73 31 alice

Alley Blk 119-120 N/O Kennebeck E/O Strandway PRELIM GRP 25 34-35 39

Alley Blk 123-124 N/O Kingston E/O Strandway PRELIM GRP 25 36-38

Alley Blk 127-128 N/O San Luis Obispo E/O Strandway PRELIM GRP 25 alice 40-42

Alley Blk 139-140 N/O Manhattan E/O Strandway PRELIM GRP 25 43-45

Alley Blk 143-144 N/O El Carmel E/O Strandway 46-48

Altadena St., To So. Terminus 120 So. of Sterling Ct. 6" A.C. Main ③ Stk's 49-50 alice

Alley Blk. 253, Nor. Upas, E. of Georgia St. ⑤ Stk's 4" A.C. Main 51

Alley Blk 3, N. Polk, E of 33rd ⑤ Stks 6" AC. 52-53

Alley Blk "G", N. of Monroe, E of Cherokee, 6" A.C. Main 54

Alley Blk "B", Nor of Meade, E of Wilson, 6" A.C. Main 55-56

Hilger St., Gibson to Madera ⑤ Stks. 6" A.C. 57

Zeller St., Gibson to Klauber ⑤ Stks. 6" A.C. 58-60

Gibson St., Hilger to 69th ⑤ Stks. 6" A.C. 61-64

Elevations Top Existing 6" A.C.

Noyes + Beryl 77-78

Alley Blk. 21 - So. Park Pl. & E. of Kensington ⑤ Stk's 4" A.C. Main 65 alice

Myrtle St
Florida to Georgia
5 Stks for 6" AC Main

	11.87	209.88		198.01
0+60		10.6	199.3	195.0
1+00		6.7	203.2	199.4
+17 MN		3.6	206.3	214.4
+25		3.6	206.3	202.0
	13.06	221.78	1.16	208.72
+38.5		10.0	211.8	205.6
+50		4.1	217.7	210.6
	12.79	233.87	0.70	221.08
+75		9.3	224.6	221.4
2+00		3.5	230.4	228.0
	12.75	246.32	0.30	233.57
+10	6"x6" Cross		11.2	235.1
+12.5		10.05	235.27	231.6
+37.5		4.6	241.7	234.0
+50		1.2	245.1	240.0
	12.50	258.23	0.59	245.73
2+75		6.9	251.3	249.0

West
Williams ⊼
Varonfakis ϕ

4/25/55

BM @ SW Cor Florida & Myrtle

Begin Work

C4 3

C3 8

F8 1

C4 3

C6 1

C7 1

C3 2

C2 4

C3 7

C7 7

C5 1

C2 3

Myrtle St Cont

4/25/55

	258.R3			
	12.12 269.77	0.58	257.65	
3+00		10.8	259.0 255.0	C4 0
+16 ms		10.1	259.7	C 0 0
+20 ms		4.5	265.3	C 0 0
+25		3.9	265.9 261.2	C4 1
+31 ms		3.9	265.9	C 0 0
	11.72 280.75	0.74	269.03	
+50		8.7	272.1 267.3	C4 8
+70		5.2	275.6 272.9	C2 1
		2.6	278.1 =	278.0 end of Work

See FD 822 Page 13

FRANKLIN AVE. EVANS ST.
TO 28 TH. ST

STKS FOR 6" A.C. MAIN

WEST, P
WILLIAMS
VARONFAKIS T

4/25/55 CLOUDY + WINDY

T.B.M.	5.04	80.12	75.08		F.H. S.E. COR FRANKLIN + EVANS F.B. 868-41
0+40			9.0	71.1	67.8 C 3 3
+63			8.7	71.4	68.0 C 3 4 F.H TEE
1+00			7.7	72.4	68.8 C 3 6
+50			6.4	73.7	69.8 C 3 9
2+00			5.3	74.8	71.0 C 3 8
+50			4.2	75.9	72.0 C 3 9
3+00			3.2	76.9	73.0 C 3 9
+50			2.1	78.0	74.2 C 3 8
4+00			1.1	79.0	75.2 C 3 8
+50	6.68	86.59	0.21	79.91	75.9 C 4 0
5+00			5.9	80.7	76.6 C 4 1
+50			5.3	81.3	77.2 C 4 1
6+00			4.6	82.0	77.8 C 4 2
+50			4.4	82.2	78.4 C 3 8
7+00			4.2	82.4	78.6 C 3 8
+25			4.2	82.4	78.8 C 3 6
+50			3.9	82.7	78.8 C 3 9
8+00			3.6	83.0	79.0 C 4 0

FRANKLIN CONT.

4/25/55

	86.59				
8+50		3.5	83.1	79.2	C 3 9
9+00		3.4	83.2	79.4	C 3 8
+50		3.4	83.2	79.5	C 3 7
+75		3.0	83.6	79.6	C 4 0
+93		3.0	83.6	80.2	C 3 4
T.P.	5.24	89.23	2.60	83.99	
CHECK					
T.B.M.			0.65	88.58 = 88.59	

F.B. 868-43

Agate St

Dawes to Easterly Line Forued

Profile Los Altos Housing

	12.75	147.60		134.85
	10.92	158.50	0.02	147.58
	4.89	159.93	3.46	155.04
0+00			9.5	150.4
+50			8.7	151.2
1+00			7.6	152.3
+50			6.45	153.4
2+00			5.25	154.7
+50			3.7	156.2
3+00			1.9	158.0
+50	12.61	172.39	0.15	159.78
4+00			10.8	161.6
+50			8.5	163.9
5+00			6.0	166.4
+50			3.5	168.9
6+00	13.10	184.81	0.68	171.71
+50			10.3	174.5
7+00			7.75	177.0
+50			5.5	179.3

Reduced by A.E. MATHISON 6-24-55

West
Williams
Varonfakis

5.

4/26/55

BM SE BP Oaks + Turquoise

Easterly Property Line Dawes St

Agate St Cont

		184.81			
8+00			3.7	181.1	
+50			2.1	182.7	
9+00	1053	194.74	0.60	184.21	
+50			9.2	185.5	
10+00			7.8	186.9	
+50			6.25	188.4	
11+00			5.4	189.3	
719			5.4	189.3	
	0.97	182.84	12.87	181.87	
	1.00	171.50	12.34	170.50	
	2.31	166.48	7.33	169.17	
			5.23	161.25 =	161.28

Red. by AEM 6-24-55

Curb radius Fonuel

Toe of Dirt Slope eastardy

SE Top EH Tourmaline & Fonuel

Sapphire St
@ Dawes to @ Everts
Unimproved St

@ existing Pipe Profile
Los Altos Housing

	0.56	135.41	134.85	✓
	5.03	138.36	2.08 133.33	✓
0+00			10.6 127.8	
+50			9.6 128.8	
1+00			9.0 129.4	
	12.32	142.36	8.32 130.04	✓
+50			12.3 130.1	
2+00			11.3 131.1	
+50			10.4 132.0	
3+00			9.4 133.0	
+50			8.1 134.3	
4+00			6.5 135.9	
+50			4.9 137.5	
5+00			1.3 141.1	
+50			0.7 141.7	
+90 ±			0.2 142.2	
	13.00	149.70	5.66 136.70	
			6.29 143.41	
	12.90	162.33	0.27 149.43	
			1.05 161.28	=

5+80± ?

Reduced by AE Mathison 6-27-55

West
Williams
Varonfakis

7

1/26/55

Brt SE Bp @ Dawes & Turquoise

@ Dawes St

@ Everts in school playground

Top Fit SE Cor Tourmaline & Everts

161.28 SE Top Fire Hyd Fanuel & Tourmaline

Tourmaline St Dawes + Everts

Profile over Existing Pipe Line

Los Altos Housing

	129	144.70	143.41 ✓
	1.43	133.37	12.46 132.24 ✓
0+00		14.9	118.5
+50		13.5	119.9
1+00		12.2	121.2
+50		10.5	122.9
2+00		8.7	124.7
+50		7.0	126.4
3+00		5.2	128.2
+50		3.5	129.9
4+00		1.8	131.6
+50	10.98	44.25	0.10 133.27 ✓
5+00		9.3	135.0
+50		7.6	136.7
6+00		5.7	138.6
+50		4.0	140.3
+57		3.66	140.6
		0.89	143.42 ✓

Reduced by A.E. Mathison 6-28-55

West
Williams
Varonfakis

8

4/26/55

Top FH Tourmaline + Everts

Westerly Property Line Dawes St

Gate Valve end of Pipe?

= 143.41

Tourmaline St
Fanuel to Gresham

Profile over existing Pipe Line
Los Altos Housing

1250	173.78	161.28 ✓
0+00	13.9	159.9
+50	11.2	162.6
1+00	9.0	164.8
+50	7.4	~~166.4~~ 166.8
2+00	5.8	168.0
+50	4.4	169.4
3+00	3.7	170.1
+50	3.2	170.6
+98	2.75	171.0
4+50	2.4	171.4
5+00	2.15	171.6
+50	1.7	172.1
+771	1.2	172.6
1250	161.28 -	161.28

Redrawn by A.E. Mathison 6-29-55

West
Williams
Varon Fokos

9

4/26/55

SE Top FH Tourmaline + Fanuel
end of Cone pave
Easterly Property Line Fanuel

Beginning of Cone pave
easterly prop Line Gresham

Opal St
Everts to Fanuel
Profile of existing main
Los Altos Housing

	1.81	145.22	143.41 ✓
0+00		12.1	133.1
+50		11.6	133.6
1+00		9.3	135.9
	1285	148.59	9.48 135.741
+50		11.5	137.1
2+00		10.1	138.5
+50		8.6	140.0
3+00		7.1	141.5
+50		5.5	143.1
4+00		4.4	144.2
+50		2.9	145.7
5+00		1.3	147.3
	1234	159.92	1.01 147.581
+50		11.1	148.8
+79		11.6	148.3

Reduced by A E MATHISON 6-27-55

West
Williams
Varonfakis

10

4/27/55

TBM Top FH Tourmaline & Everts
Westerly Prop Line Everts

Westerly property Line Fanuel

Opal St
Fanuel to Crossbar
Profile of existing main
Los Altos Housing

	159.92			
0+00		10.1	149.8	
+50		7.3	152.6	
1+00		5.8	154.1	
+50		4.3	155.6	
2+00		2.6	157.3	
+50		1.1	158.8	
3+00		0.2	159.7	
	8.15 167.01	1.06	158.86	
+50		6.9	160.1	
4+00		6.4	160.6	
+50		6.0	161.0	
5+00		5.7	161.3	
+50		5.6	161.4	
+79		6.5	160.5	
	1.42 159.07	9.36	157.65	
	10.41 162.68	6.80	152.27	
		1.38	161.30	=161.28

Reduced by A.E. MATHISON 6-30-55

West
Williams
Varonfakis

11

4/27/55

Hi from page #10

Easterly prop line Fanuel

End of Pipe Begining Conc pave

55
TBM A Top Fire Hyd Tourmaline Fanuel

Chalcedony
Academy to Noyes
Stks for 6" AC Main

	1.34	163.36		162.02
	1.17	152.43	12.10	151.26
	0.31	142.25	10.49	141.94
	2.04	131.46	12.83	129.42
	1.55	126.68	6.33	125.13
0+34	(5')		10.0	116.7	109.4
	(10') 12.42	128.95	10.15	116.53	109.4
+50	(5')		5.7	123.3	116.2
	(10')		5.1	123.9	116.2
	12.78	141.56	0.17	128.78	
+75	(5')		7.2	134.4	127.4
	(10')		6.7	134.9	127.4
	9.32	150.63	0.25	141.31	
1+00	(5')		6.2	144.4	135.7
	(10')		6.5	144.1	135.7
+12.5			4.2	146.4	138.6
+23 mb			4.0	146.6	145.6
+25			3.2	147.4	140.4
+50			1.67	148.96	142.0

West
Williams X
Varontakis ¢

5/5/55

BM NW. 7' Lt T Lamont + Beryl

C7	3	Begin Work
C7	1	Turn on Pinney
C7	1	
C7	7	
C7	0	
C7	5	
C8	7	
C8	4	
C7	8	
C1	0	
C7	0	
C7	0	Turn on Pinney

Chalcedony Cont

5/5/55.

9.26	158.22		148.96		
1+75	ms	9.0	149.2	147.6	C1 6
2+00		7.3	150.9	145.4	C5 5
+27	ms	8.2	150.0	148.2	C1 8
+34	mN	1.9	156.3	151.4	C4 9
+45	mN	1.2	157.0	151.6	C5 4
+50	"	6.5	151.7	147.0	C4 7
+75		6.5	151.7	147.0	C4 7
3+00		6.7	151.5	146.4	C5 1
+40		7.3	150.9	145.3	C5 6

end of Work

Noyes St
Chalcedony to Beryl

		158.22			
0+33			5.5	152.7	145.3
	11.93	167.14	3.01	155.21	
+75 (5')			9.2	157.9	147.2
+ (10)			9.3	157.8	147.2
+98^4 ℄			6.7	160.4	149.9
(10')			6.6	160.5	149.9
1+12^5			5.3	161.8	152.4
(10')			5.0	162.1	152.4
+25			6.7	160.4	156.0
+38 BC			5.1	162.0	158.4
+50			3.9	163.2	159.9
+75			1.4	165.7	163.0
	12.76	179.54	0.36	166.78	
2+00			11.2	168.3	165.5
+25			8.6	170.9	168.0
+25 MW			7.1	172.4	172.6
+50			6.3	173.2	170.5
+75			4.3	175.2	172.1

West
Williams ⊼
Varonfakis ℄

5/5/55

Hi from Page 13

C7 4	152.3 / 5.9	5' Lt 8.3 Begin Work
C10 7	157.8 / 9.3	5 Lt / 11.7
C10 6		
C10 5 / 19° 46' 40 Lt	160.1 / 7.0	5 Lt / 9.8
C10 6		
C9 4	158.9 / 8.2	
C9 7		
C4 4		
C3 6		
C3 3		
C2 7		
C2 8		
C2 9		
F0 2		
C2 7		
C3 0		

	179.54						
3+00		2.1	177.4	174.1	C3	3	
9.85	189.03	0.36	179.18				
+25		9.0	180.0	175.4	C4	6	8'LT
+50		8.0	181.0	176.7	C4	3	8.6
+75		7.0	182.0	177.3	C4	7	
4+03 29 EO		6.2	182.8	178.0	C4	8	
+50		5.7	183.3	178.8	C4	5	
+77 09 BC		5.3	183.7	179.4	C4	3	
5+00		5.3	183.7	179.5	C4	2	
+50		5.3	183.7	179.8	C3	9	
6+00		6.5	182.5	178.3	C4	2	
+50		8.2	180.8	175.9	C4	9	
+50 mW		4.4	184.6	179.7	C4	9	
7+00 1.34	179.24	11.13	177.90	173.1	C4	8	Turn on Quincy
+50		3.7	175.5	170.3	C5	2	
+85 Tee FH		5.8	173.4	168.4	C5	0	
(5) Q FH		6.4	172.8	171.8	C1	0	
+98 81 EO		6.2	173.0	167.6	C5	4	
8+50 ~~A~~ 18°14'		8.4	170.8	166.3	C4	5	
+82		9.3	169.9	165.9	C4	0	End of Work

Beryl St
Chalcedony to Academy

		179.24				
0+25			9.3	169.9	165.9	C4 0
+50	0.32	170.04	9.52	169.72	165.9	C3 8
1+00			1.6	168.4	165.0	C3 4
+50			4.5	165.5	162.5	C3 0
2+00			8.8	161.2	157.5	C3 7
	0.40	158.37	12.07	157.97		
+50			2.8	155.6	151.6	C4 0
3+00			9.2	149.2	144.6	C4 6
	0.77	146.23	12.91	145.46		
+25			1.3	144.9	140.8	C4 1
+50			4.6	141.6	137.2	C4 4
4+00			10.1	136.1	131.6	C4 5
+28			12.3	133.9	130.4	C3 5
	11.74	147.12	10.85	135.38		
	11.95	158.78	0.29	146.83		
	6.08	164.16	0.70	158.08		
			2.12	162.04	=	162.02

West
Williams ⊼
Varonfalsis ϕ.

HI from page 15 | 5/5/55

Begin Work

Turn on Curvey
℄
1.5
4.4
9.0

2.9
9.7

1.1
4.7
10.2

end of work

Turn on top FH - SWly Cor Academy + Beryl

68th St

Amherst to Tower St

Stks for 6" AC

West
Williams ⊼
Kellhofer ϕ

5/11/55

	0.83	458.23		457.40				SWBP 68th + El Cajon	
0+46			7.4	450.8	447.5	C3	3	Begin Work	
1+00			9.5	448.7	445.1	C3	6		
	6.94	455.55	9.62	448.61					
+03 mE			6.1	449.5	448.8	C0	7		6805 Amherst
+50			8.1	447.5	443.2	C4	3		
+81 mE			8.3	447.3	446.3	C1	0		4859 68th
2+00			9.7	445.9	441.4	C4	5		
+50			10.1	445.5	441.4	C4	1		
+90 mE			9.9	445.7	445.2	C0	5		4841
3+00			10.4	445.2	441.4	C3	8		
+50			10.0	445.6	441.4	C4	2		
3+81 mE			9.3	446.3	446.1			C0 2	
4+00			9.3	446.3	443.0	C3	3		
+30 mW			6.6	449.0	448.2	C0	8		48.32
+50			6.7	448.9	445.2	C3	7		
+80 M.W			5.3	450.3	450.2	C0	1		4826
5+00			4.6	451.1	447.4	C3	7		
+05 mE			3.9	451.7	451.2	C0	5		4873
+15 mW			3.1	452.5	451.6	C0	9		4818

68th St Cont

5/11/55

		455.55					
5+50			2.6	453.0	449.1	C3 9	
+75 ME			1.7	453.9	454.0	F0 1	4817 68th
5+85 FH			1.9	453.7	454.6	F0 9	
5+88 60 △			1.1	454.5	450.4	C4 1	
6+00			0.9	454.7	450.9	C3 8	
	9.66	464.37	0.84	454.71			
+50			8.9	455.5	451.5	C4 0	
+54 mw			9.1	455.3	455.4	F0 1	4804
7+00			8.3	456.1	452.3	C3 8	
+50			7.4	457.0	453.0	C4 0	
8+00			6.9	457.5	453.9	C3 6	
+50			6.0	458.4	454.6	C3 8	
9+00 mw			4.1	460.3	459.0	C1 3	4778
9+00			4.5	459.9	455.1	C4 8	
+50			4.1	460.3	455.1	C5 2	4762
+75 M.W.			3.6	460.8	459.0	C1 8	
10+00			4.1	460.3	455.1	C5 2	
+05 mw			4.2	460.2	458.8	C1 4	4756
+50			5.8	459.2	454.4	C4 8	
10+89 mw			5.6	458.8	457.6	C1 2	4752
11+00			6.5	457.9	453.6	C4 3	

	464.37				5/11/55
11+50		7.8	456.6 452.7	C3 9	
+90 mw		8.3	456.1 456.0	C0 1	4738
12+00		9.1	455.3 451.8	C3 5	
2.1	457.13	9.35	454.99		
+35 mw		1.7	455.4 455.3	C0 1	4736
+50 FH Jct		2.7	454.4 451.0	C3 4	
+50 ⑥ Q FH		1.7	455.4 455.1	C0 3	~~4735~~
13+00		3.3	453.8 450.2	C3 6	
+05 mw		2.7	454.4 454.3	C0 1	4730
+35 mw		2.9	454.2 453.7	C0 5	4722
+50		3.8	453.3 449.5	C3 8	
14+00		4.4	452.7 448.7	C4 0	
+19 M.W.		4.3	452.8 452.3	C0 5	4718
+50		5.1	452.0 447.9	C4 1	
+65 mw		4.7	452.4 451.7	C0 1	4714
+92 mw		4.7	452.4 451.1	C1 3	4710
15+00		5.9	451.2 447.2	C4 0	
+26 mw		5.2	451.9 450.6	C1 3	4702
+50		6.9	450.2 446.3	C3 9	
+80		7.05	450.1 445.9	C4 2	
		6.05	451.08 =	451.17	

Solita St (Tower St)
68th to 67

0+23± LT	4.40 455.48	5.6	451.08 449.9	445.9
0+23±		5.4	450.1	445.9
+50		5.4	450.1	446.1
1+00		5.4	450.1	446.0 ~~446.6~~
+44 mN		4.7	450.8	
+50		5.7	449.8	445.8 ~~446.1~~
2+00		6.3	449.2	445.6
+43 mN		6.1	449.4	
+50		6.9	448.6	445.0
+60 mN		6.5	449.0	
3+00		7.6	447.9	444.0
+08 mN		6.9	448.6	
+46 FH Tee		6.9	448.6	444.8 ~~445.1~~
+45 (5) of FH		6.7	448.8	
+50		6.8	448.7	444.9 ~~445.2~~
7.17	456.57	6.08	449.40	
4+00		7.0	449.6	445.4 ~~446.2~~
+43 mN		4.9	452.7	
+50 L		6.3	450.3	446.1 ~~446.7~~

West
Williams x
Kellhofer

5/12/55

C4 0 TBM Nail in power pole see page 19	
~~C4~~ 2 Begin Work	
C4 0	
~~C3~~ 5 C4 1	
C0 0	6780
~~C3~~ 7 C4 0	
C3 6	
C0 0	6772
C3 6	
C0 0	6756
C3 9	
C0 0	6758
~~C3~~ 5 C3 8	
C0 0	
~~C3~~ 5 C3 8	
0	
~~C3~~ 4 C4 2	
C0 0	6744
~~C3~~ 6 C4 2	

Solita Cont

	456.57			
4+71 mn		5.4	451.2	
5+00		5.7	450.9	~~447.3~~ 446.6
+07 mn		5.5	451.1	
+50		5.4	451.2	~~447.8~~ 447.2
6+00		4.6	452.0	~~448.5~~ 447.9
+50		3.6	453.0	449.1
7+00		3.1	453.5	449.0
+13		2.9	453.7	449.0
		0.29	456.28	=

C0 ⁰		6734
~~C3~~ 6	C4 3	
C0 ⁰		6728
~~C3~~ 4	C4 0	
~~C3~~ 5	C4 1	
C3 9		
C4 5		
C4 7	end of work	

456.38 SW Top FH 67th + Solita St

67th St Tower (Solita) to Alimo St

West
Williams ⊼
Kellhofer

Stks for 8" AC

5/13/55

TBM Top FH SW Cor

Begin Work

	2.08	458.36		456.28		
0+29.6	(5)		4.6	453.8	449.0	C4 8
+50	(5)		4.8	453.6	449.2	C4 4
+75 FH Tee	(23) cb		4.3	454.1	449.6	C4 5
1+00	cb (23)		4.3	454.1	450.0	C4 1
+50	cb		4.4	454.0	450.0	C4 0
2+00	cb		4.6	453.8	~~450.0~~ 449.6	~~C3 8~~ C4 2
+50	cb		4.7	453.7	449.7	C4 0
3+00	cb		4.8	453.6	449.6	C4 0
+50	cb		4.9	453.5	449.5	C4 0
4+00	cb		5.0	453.4	449.4	C4 0
+50	cb		5.0	453.4	449.2	C4 2
5+00	cb		5.1	453.3	449.0	C4 3
+50	cb		5.9	452.5	448.4	C4 1
6+00	cb		8.8	449.6	444.0	C5 6
+25	cb		11.9	446.5	441.0	C5 5
	0.50	445.79	13.07	445.29		
+50	cb		2.9	442.9	437.4	C5 5
+75	cb		6.6	438.2	~~434.8~~ 434.0	~~C3 4~~ C4 2

67th St Cont

			44579			
				432.0		
9+00		10.1	435.7	~~432.4~~	C3 3 C3	1
				431.3		
+27 8x6" Tee		10.8	435.0	~~431.6~~	C3 4 C3	1
+50		11.4	434.4	430.9	C3 5 C3	9
+	0.34 435.93	10.20	435.59		Turn on Top EW SW Dai	
7+79 EH Tee		3.6	432.3	428.9	C3 4	
+86 BC		4.1	431.8	428.3	C3 5	
				426.0		
8+00		5.3	430.6	~~427.4~~	C3 3 C4	6
+50		10.1	425.8	422.4	C3 4	
	0.67 423.87	12.79	423.20			
9+00		2.8	421.1	417.6	C3 5	
				416.2		
+18 EC		4.1	419.8	~~416.6~~	C3 2 C3	6
				414.3		
+50		5.5	418.4	~~414.9~~	C3 5 C4	1
				412.6		
10+00 End of WH		7.0	416.9	~~413.0~~	C3 9 C4	3
	12.57 435.77	0.67	423.20			
		0.18	435.59	= 435.59	Eq 882 Top EW SW Dai 67th + Vantage Dr	

ALLEY BLK 10
N of Copley E of 34th
Stks for Meters

119032

Meters set 19.25 from Q Alley

6.00	398.13		392.13	
0+45 meas E		2.9	395.2	393.9
0+96 MW		3.1	395.0	393.9
+86 MW		3.1	395.0	394.1
+88 ME		2.6	395.5	394.1
1+35 MW		3.3	394.8	394.2
+38 ME		3.2	394.9	394.2
+73 ME		3.6	394.5	394.4
+79 MW		3.2	394.9	394.4
2+30 MW		3.2	394.9	394.5
+34 ME		3.5	394.6	394.5
+71 MW		3.3	394.8	394.6
6.09	400.74	3.8	394.65	
2+87 ME		5.8	394.9	394.7
3+20 ME		5.6	395.1	394.8
+21 MW		5.7	395.0	394.8
+74 MW		5.3	395.4	395.0
+79 ME		5.2	395.5	395.0
4+20 MW		4.9	395.8	395.3

West
Williams &
Varontakis
0+00 Mtg Prop
Copley 6/6/55

BM SE BP Copley +34th

Cl	3
Cl	1
Co	9
Cl	4
Co	6
Co	7
Co	1
Co	5
Co	4
Co	1
Co	2
Co	2
Co	3
Co	1
Co	4
Co	5
Co	5

Alley Blk 10 Cont

	400.74			6/6/55
1+37 ME		5.0	395.7 394.4	C1 3
+72 ME		4.6	396.1 395.7	Co 4
5+02 MW	400.67	4.36 4.43	396.31 395.8	Co 5
+20 MW		4.2	396.5 396.0	Co 5
+24 ME		4.0	396.7 395.9	Co 8
+56 ME		4.0	396.7 395.6	C1 1
+78 MW		4.2	396.5 395.3	C1 2
4.50	399.10	6.07	394.60	
5.08	398.33	5.85	393.25	
		6.17	392.16	392.13

29th St
E St to Broadway
stks for Meters on Conors 11556L

	1.88	185.48		183.60
0+06 MW			2.2	183.3 182.3
	0.68	176.22	9.94	176.54
2+98 MW			2.2	174.0 171.3
2+98 ME			4.0	172.2 171.3
	12.22	188.01	0.43	175.79
	3.66	190.58	1.09	186.92
			2.88	187.70 =

West
Williams. x
Varonfakis +

Backs of Meters set 25' from ℄ St

SE Top Fire Hyd 29th + Broadway

C1 0

C2 1

C0 9

187.63 NW BP 30th + E St

California St
2" Copper Across AT + SF R×1

	4.35	22.38		18.03	
	5.50	27.52	0.36	22.02	
0+00			2.2	25.3	21.5
+50			1.5	26.0	21.5
+75			1.8	25.7	19.7
1+01.2 Begin			5.2	22.3	
~~1+96~~ encase			4.7	22.8	18.3
1+40 end			6.8	20.7	
~~1+35~~ encase			6.3	21.2	16.6
+55 Δ			10.6	16.9	13.5
2+00			9.7	17.8	14.0
+50			9.0	18.5	14.4
3+00			9.1	18.4	14.9
+25 End of work			9.1	18.4	15.2
	4.52	21.42	10.58	16.94	
			3.44	18.02 =	18.03

West
Williams ⊼
Varonfakis P

Clear + warm

57

6/6/55
See FB 910 Page 18
TBM 2" pipe So Line lot 178 + 17

C3 8
C4 5
C6 0
~~C4 5~~ C4 0
C4 6 C4 1
C3 4
C3 8
C4 1
C3 5
C3 2

18.03

Altadena St
120' South of Sterling Ct
to 850' South
Palm Ct 23

			Bol 30670	
	9.18	326.41		317.23
	3.64	329.39	0.66	325.75
0+00			4.0	325.39
0-00[5]			9.99	
0+45 ~~-48~~			2.2	327.19
+50			2.2	327.19
1+00			2.6	326.79
+50			3.7	325.69
2+00			5.6	323.79
+50			8.3	321.09
3+00			10.3	319.09
+50			12.3	317.1
	1.80	318.21	12.98	316.41
4+00			3.4	314.8
+25			4.32	313.89
+50			5.0	313.21
5+00			6.3	311.91
+50			7.4	310.81
6+00			7.5	310.71

Revised by J. Gray 6-15-55

West
Williams
Varontakis

28

6-9-55

BM Nail in pole SW cor. Altadena St & Sterling Ct

AV 120'± South of Sterling Ct

Top 2" AV end of existing Main

end ½" O.I pave

Altadena Cont

	318.21		
6+22 30 BC		7.2	311.01
+50		6.6	311.61
7+00		5.8	312.41
+25 65 EC		5.4	312.81
+50		5.0	313.21
8+00		4.3	313.91
+50		4.1	314.11
+53 73		4.2	314.01
		3.56	314.65
	4.78 321.19		316.41
3+64		6.44	314.75
3+86		9.72	311.47
		6.35	314.84 =

End of Work

= 314.60 BM 1/2 IP 21' Lt 8+53 73

Turn on Rock

Top 36" Pipe 6° Rt

Top 36" Steel Pipe 6° Rt

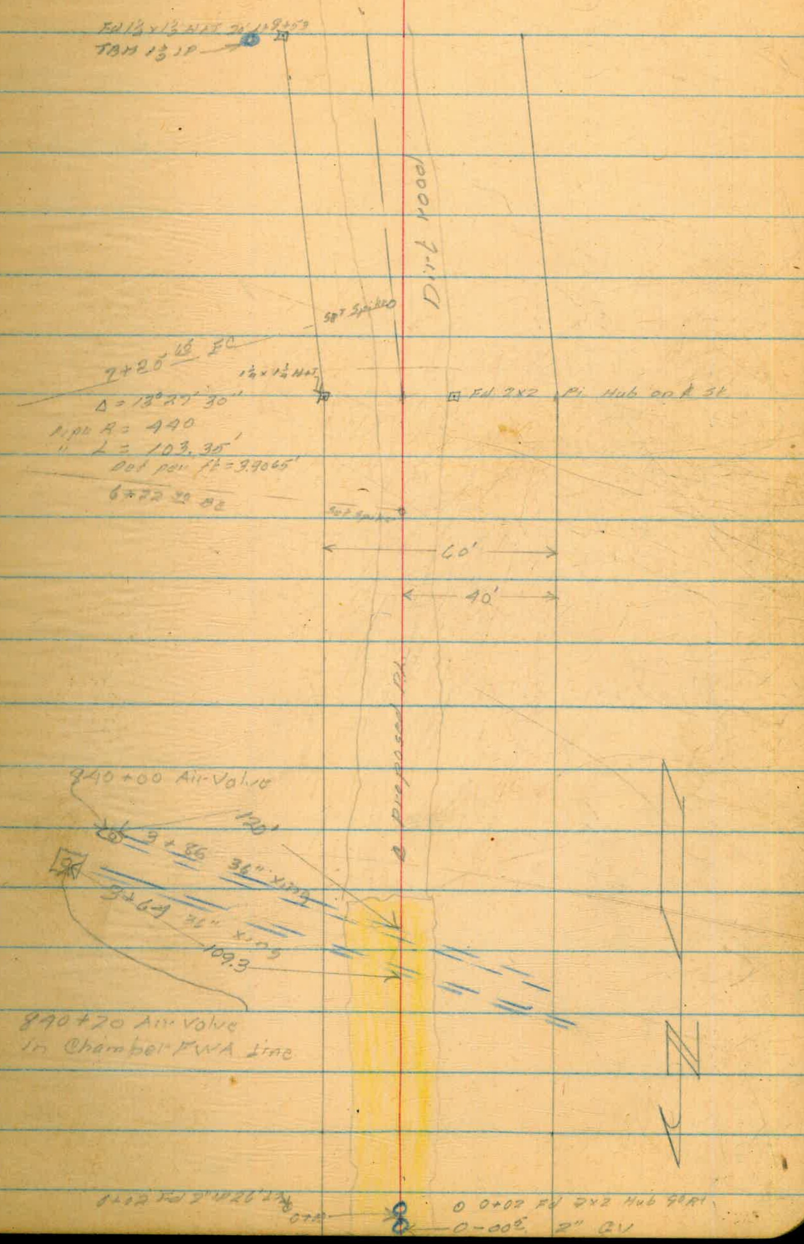
314.8 4+00

ALTADENA St

Group 23

8+53.73	End of Work	
7+25.65 EC		
	Δ = 13°27'30" Lt	Sec 30620
	R = 440	
	L = 103.35'	
6+22.30 BC		
0+46.47 ∠	0° 50' 30" Rt	
0+00	120'± South of Sterling Ct	

West
Williams
Varonfokis



41st St

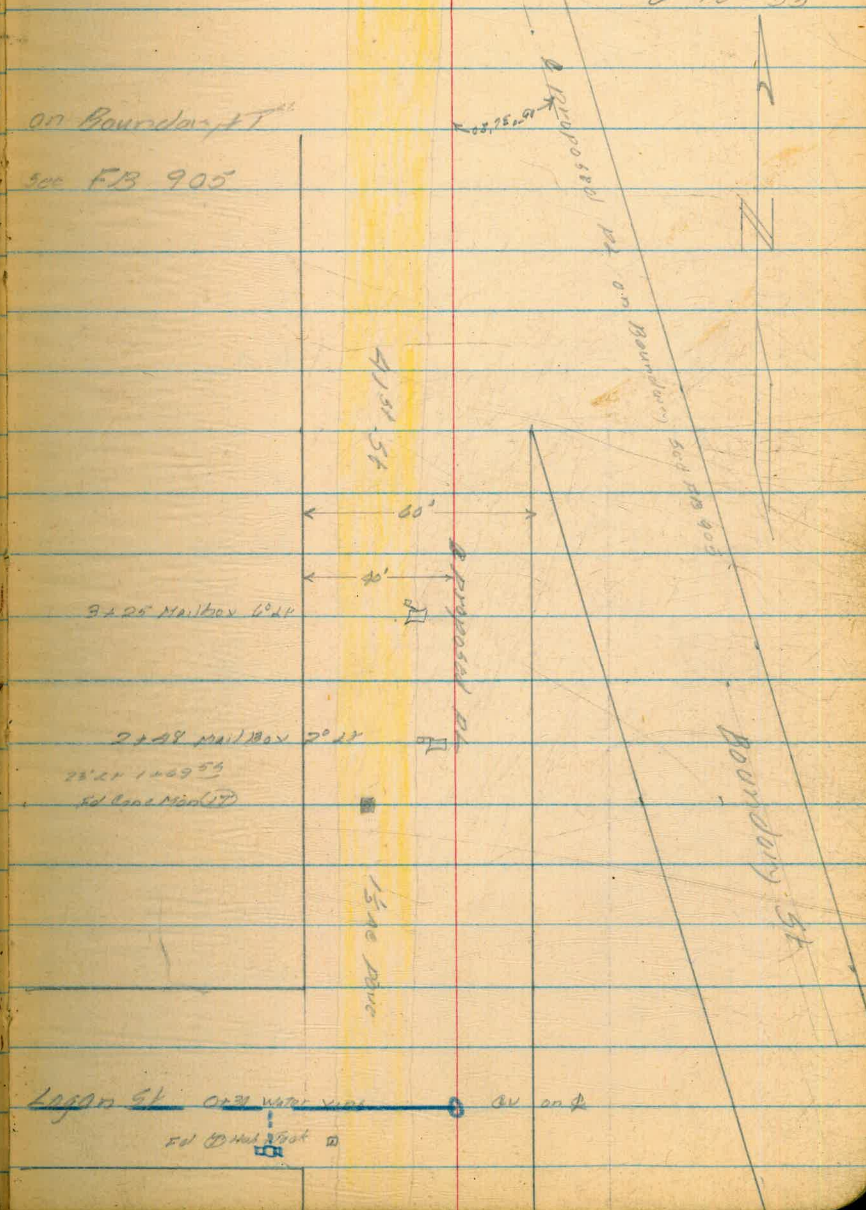
Logan to "T" St

Prelim Group #23

	15° 36' 20" Lt to 0+00	
5+55.10	41st St = 1+32.16 Boundary St	
1+69.54	℄	0° 28' 00" Rt
0+07	POT	
0+00	Sly prop Line Logan St	

West
Williams
Yaronfakis

6-10-55



41st St

℄ Profile

	9.96	45.21	35.25
0+00		5.2	40.0
+14		4.4	40.8
+17		1.3	43.9
+30		2.5	42.7
+41		1.9	43.3
	12.08	56.35 0.94	44.27
0+50		11.1	45.3
+79		10.1	46.3
+86		8.2	48.2
1+00		7.0	49.4
+50		1.7	54.7
	7.03	62.10 1.28	55.07
1+69 56 ℄		7.5	54.6
2+00		7.8	54.3
+50		5.9	56.2
3+00		3.3	58.7
+50		3.1	59.0

West
Williams
Varonfolios

PM NW SP 41st & National

5½ prop line Logan

Bottom at end of 3' High Conc retaining wall

℄

Top of ℄

Edge AC	7.8 / 7'Lt	9.0 / 1'Rt	+0.6 / 8'Rt
Edge AC	12.9 / 10'Lt	10.9 / 5'Lt	11.1 / 10'Rt
" "	11.0 / 8'		9.2 / 10'Rt
" "	10.6 / 9'	10.1 / 5'Lt	7.1 / 10'Rt
25' edge AC →	9.9 / 9'Lt	7.9 / 5'Lt	5.2 / 10'Rt
edge AC	6.7 / 8'Lt	5.7 / 4'Lt	2.3 / 2'Lt	+1.3 / 10'Rt
edge AC 10' / 25'Lt	10.6 / 10'Lt	10.1 / 7'Lt	8.7 / 5'Lt	4.9 / 10'Rt
edge AC	9.3 / 10'Lt	8.7 / 4'R	6.5 / 3'Lt	1.0 / 10'Rt
edge AC	8.9 / 9'Lt	6.6 / 6'Lt	3.7 / 3'Lt	1.2 / 10'Rt
25'Lt edge AC	7.6 / 10'Lt	7.1 / 9'Lt	4.6 / 6'Lt	1.1 / 10'Rt

4th Const

	62.10		
8.18	62.73	7.49	54.61
1+00		6.5	56.2
+50		7.6	55.1
5+00		6.7	56.0
+50		3.2	59.5
+55.10		2.6	60.1
1.24	53.99	9.98	52.75
0.45	41.74	12.70	41.29
		6.50	35.24 = 35.25

Ø

edge AC $\frac{8.0}{9'Rt}$ $\frac{7.6}{7'Rt}$ $\frac{6.4}{5'Rt}$ $\frac{6.3}{3'Rt}$ $\frac{5.0}{10'Rt}$

$\frac{6.6}{20'Rt}$ ← edge AC → $\frac{6.6}{3'Rt}$

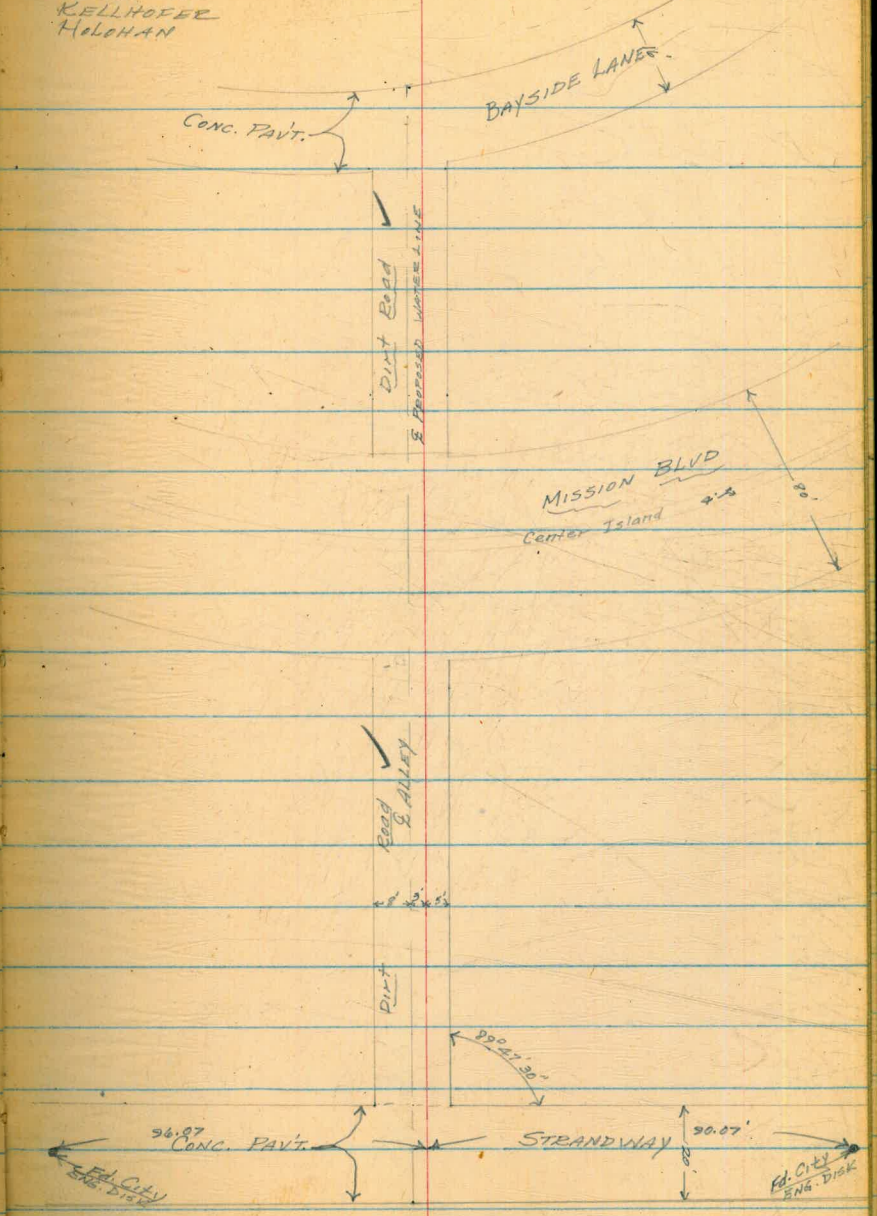
Ø of pipe on east edge AC pave

ALLEY BLKS 119, 120;
N. of Kennebeck Ct., E. of Strandway
Preliminary

7/6/55
SHOREY
ALEXANDER
KELLHOFER
HOLOHAN

4+47 E/L BAYSIDE LANE

0+00 = W/L STRANDWAY



Alley BM 119 +20 Cont.

		+7.03
2.63	+9.66	
	2.72	+6.94
2.84	+9.78	
	4.77	+5.01
1.30	+6.31	
0+00	1.1	5.2
0+05	1.3	5.0
0+10	1.4	4.9
0+10	1.30	5.0
0+20	1.4	4.9
0+50	3.6	2.7
1+00	5.2	1.1
1+50	6.6	-0.3
1+73	7.0	-0.7
1+83	7.7	-1.4

B.M. Mission Sidewalk & Santa Barbara

T.B.M. N. rim Sewer M.H. & Strandway & Alley

W/L Strandway & edge of 6" con paving

Water G.V. 10' Lt.

Sewer crossing

Sewer M.H. 3' Lt. 3.5 to flow

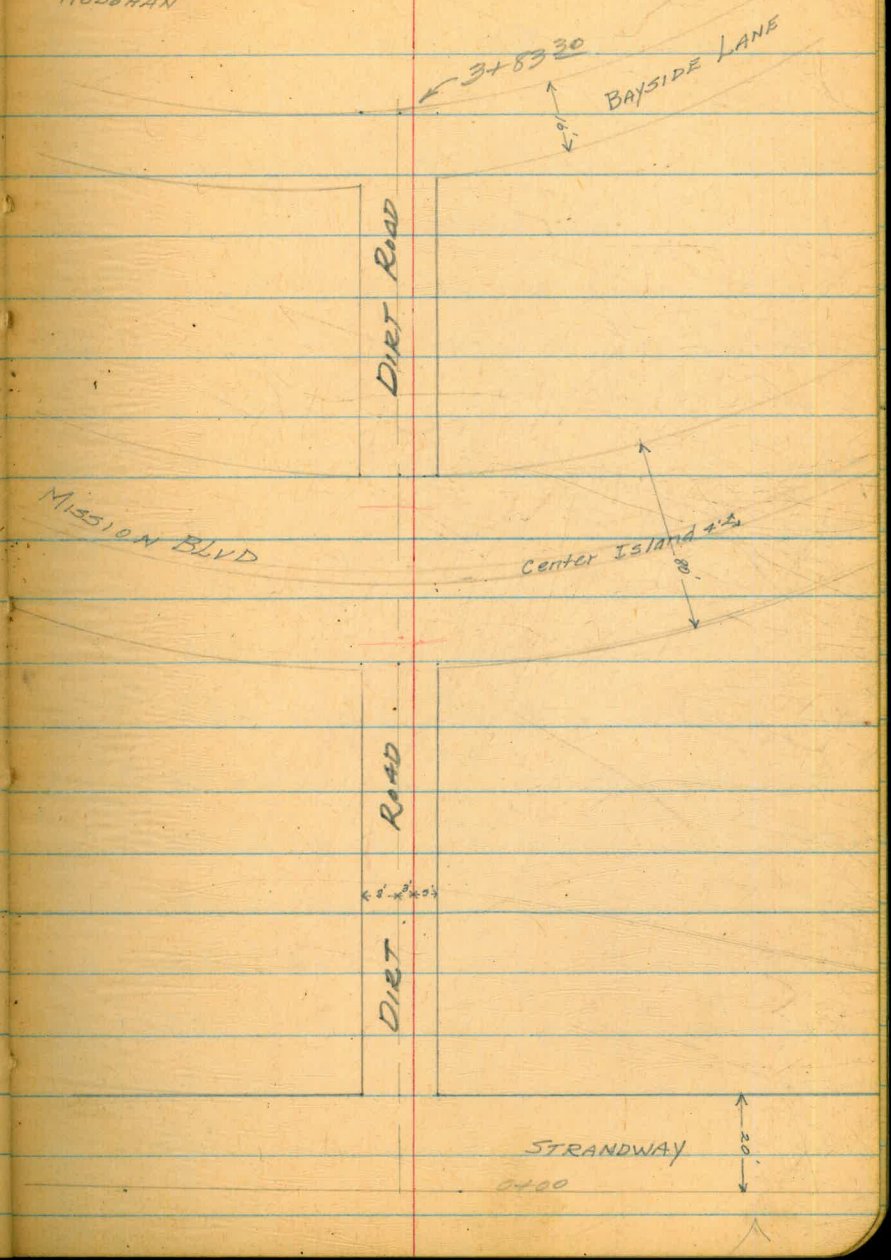
E/L of Strandway & edge of 6" con paving

W/L of Mission & begin 6" Con. paving

W curb line & W edge of 2'x2' S.D. grate 1' Lt, begin A.C. crown surfacing

ALLEY BLK'S. 123, 124;
N. of Kingston Ct., E. of Strandway
Preliminary

7/7/55
SHOREY
ALEXANDER
KELLHOFER
HOLOHAN



Alley Blk 123 - 124 Cont'd

		-0.94	TBM. 1" pipe St. Cor. Alley Blk 119-120 & Mission Blvd
	5.86	+4.92	
3+83.30		7.0 - 2.08	E/L of Bayside Lane & edge of 6" con. paving
3+75		7.6 - 2.68	8" Sewer crossing & center Storm Dr. grate, 2' to flow
3+75		7.5 - 2.58	Sewer MH. 3' Lt. 4.6 to flow line
3+66		7.5 - 2.58	W/L at Bayside Lane edge 6" con. pave.
3+50		6.9 - 1.98	
3+00		6.7 - 1.78	
2+50		6.6 - 1.68	
2+11		6.8 - 1.88	E/L at Mission, edge 6" con. paving
2+01		6.7 - 1.78	℄ curb line, begin A.C. crown surfacing, Sta. on grade 5'.16.
1+83		6.0 - 1.08	Water Gt. on line
1+80		6.0 - 1.08	Water Gt. on line
1+73		5.8 - .88	face curb @ center island
1+73		5.2 - .28	top curb
1+69		5.0 - .08	top curb
1+69		5.6 - .68	face curb

Reduced by planimeter 8-24-55

Alley Blk 123 - 129 Cont'd

	+1.92		
1+50		5.9	- .98
1+41		6.3	- 1.38
1+31		5.7	- .78
1+00		4.4	.52
		22.6	+2.66
	7.76 +10.42		
0+50		6.9	3.52
0+20		5.1	5.32
0+10		5.3	5.12
0+10		5.30	5.12
0+00		4.9	5.52
		5.05	5.37
	4.85 10.22		
		3.26	6.96 = C98

W curb line & Storm Dr. grate 5' Lt.; edge AC. crown

W/L at Mission & edge of 6" Con. pave.

E/L Strandway edge of 6" con paving

Sewer crossing

Sewer MH. 3' Lt 4.4 to flow

W/L at Strandway, edge 6" con. pave.

T.B.M. NE. cor L.S. tag Strandway & Alley 123 - 124

Luis

SW. BP. Mission Seawall & San Luis Obispo

Alley Blk 119 - 120 Cont

+6.31

2+00		7.1	-0.8	
2+12		7.0	-0.7	curb face center island Mission Blvd.
2+12		6.3	0.0	top curb
2+16		6.5	-0.2	top curb
2+16		7.2	-0.9	
2+25		7.3	-1.0	Water GV. 2' Lt
2+27		7.3	-1.0	Water GV. 0.5 Rt
2+45		7.9	-1.6	℄ curb line & edge of AC crown surfacing
2+55		7.4	-1.1	E/L of Mission & end 8" con. paving
3+00		7.8	-1.5	
3+50		7.8	-1.5	
4+00		8.1	-1.8	
4+31		8.4	-2.1	W/L Bayside Lane & edge of 6" con. pave.
4+39		8.5	-2.2	Sewer crossing 12"
4+39		8.50	-2.2	Sewer MH. 3' Lt. 5.3 to flow line
4+47.41		8.2	1.9	E/L of Bayside Lane
		7.25	-0.94	T.B.M. Alley Blk 119-120 1" pap pipe Sta 14+55 7' Rt.
	5.86	+4.92		

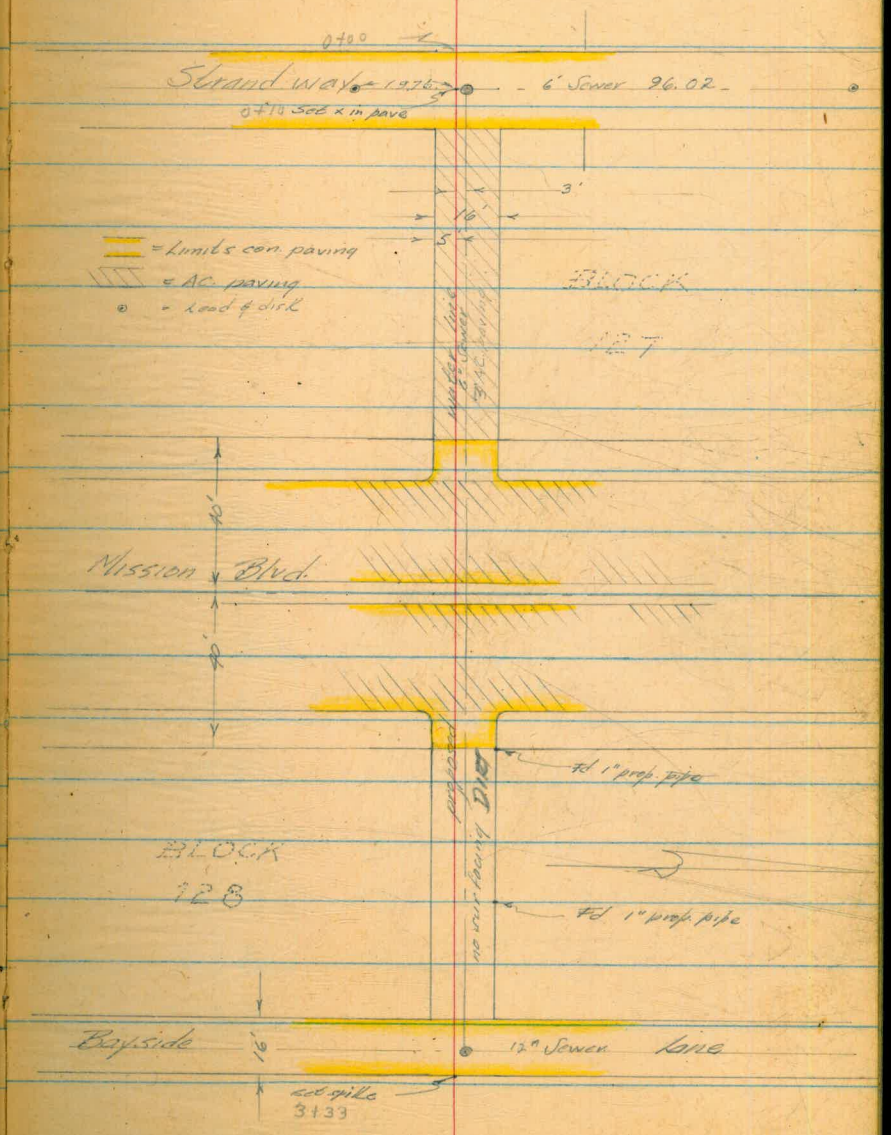
Profile & Proposed Water Line
Alley Blk 127-128, No. of San Luis Obispo
Strand way to Bayside Lane.

West Alexander

7-12-55

0+00 W'ly Line Strand Way

3+33 E'ly Line Bay Side Lane



Alley Blks 127-128 Cont

		+ 6.98	BM SW Cor Mission Sea wall & San Luis Obispo
	3.04	10.05	
		5.19 4.86	T.B.M. SE. prop. cor., 1" pipe, Alley No. San Luis Obispo & Strandway
	0.37	5.23	
0+00		0.1 5.13	W/L of Strandway (6" con. paving)
0+01			P.P. 3' Lt.
0+08		0.5 4.73	Water G.V. 12' Lt.
0+10		0.6 4.63	℄ Strandway & Sewer crossing
0+10		5.58 -.35	Sewer M.H. 3' Lt. 3.8 To Flow
0+20		0.5 4.73	E/L of Strandway edge con. pave. begin 3" A.C.
0+50		2.3 2.93	
0+95.5		5.3 -.07	W/L of Mission, end 3" A.C. pave. begin 6" con. G.V. on this
1+00		5.5 -.27	
1+05		5.7 -.47	W curb line, Storm grate 6' Lt, begin 2" A.C. crown pave
1+33.2		5.2 .03	Face center island curb
1+33.2		4.5 .73	Top curb P.P. 4' Rt.
1+35.4			Top curb
1+37.2		4.7 .53	Face center island curb
1+37.2		5.3 -.07	

Reduced by Planimeter 8-15-55

Alley Blks 127-128 Cont

5.23

1+44	5.4	- .17	Water GV 2' Lt
1+48	5.4	- .17	Water GV on line
1+65.6	6.0	- .77	E curb line, end 2" AC crown
1+75.6	5.7	- .47	E/L of Mission, end 6" conc (prop pipe 11' Lt)
2+00	6.3	- 1.07	
2+55	7.1	- 1.87	
3+00	7.3	- 2.07	
3+19	7.5	- 2.27	W/L of Bayside Lane, begin 6" conc pave
3+21.7	7.4	-2.17	Sewer crossing
3+21.7	7.46	- 2.23	Sewer MH 127 Lt 4.5' TO FLOW
3+28.7			PL 3' Lt
3+33	7.2	- 1.97	E/L of Bayside Lane
	4.60	+ 0.63	End NE curb return, Mission & Alley No at Lido Ct

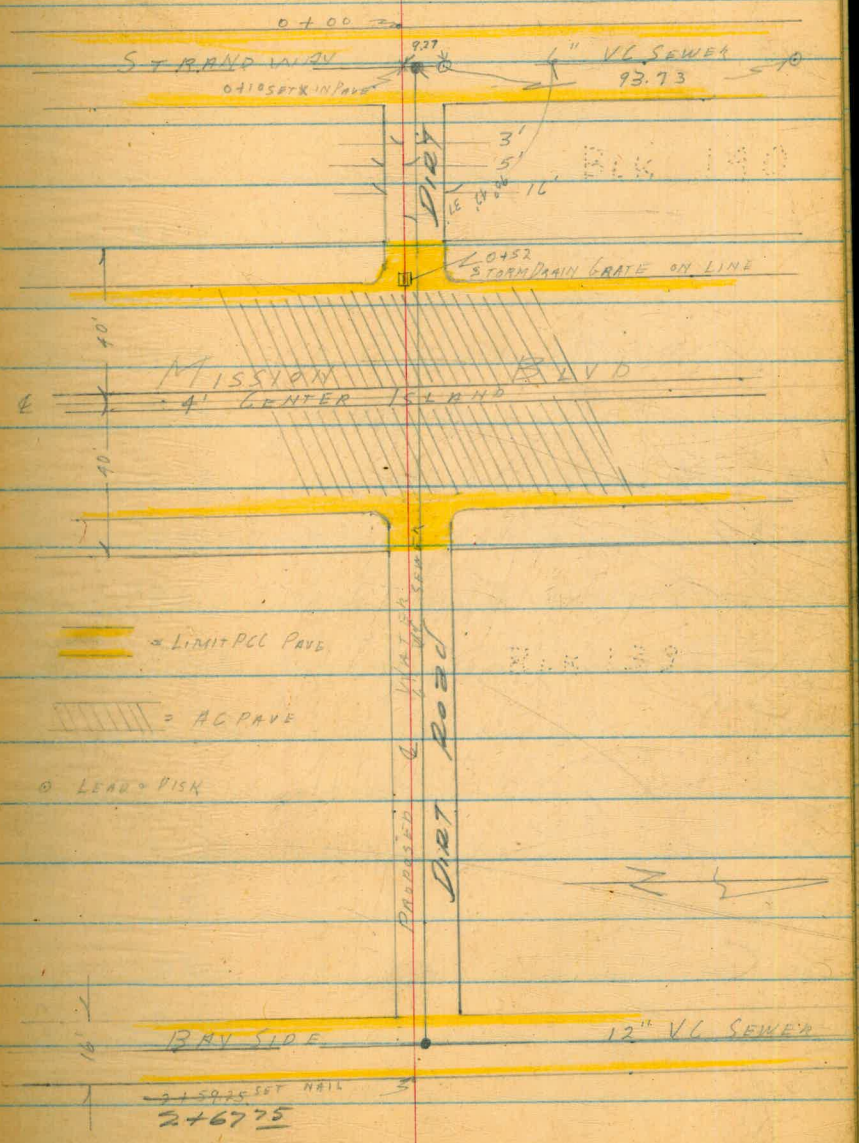
7-13-55

WEST ALEXANDER

PROFILE & PROPOSED WATER LINE

ALLEY BLKS 139 - 140, STRAND WAY TO BAY SIDE LANE

0+00 W'LY LINE STRAND WAY



~~2+59.25~~ 2+67 75 ELY LINE BAY SIDE LANE

ALLEY BAR 139-140 CONT.

BM		3.77	SW Cor El Camelo & Mission Top FH Book 916 Pg 22
	3.42 7.19		
0+00	2.6	4.59	W'ly Line Stairway Begin 6" PCC
0+10	3.0	4.19	Sewer Crossing
0+16	3.09	4.10	S'ly Rim Sewer MH 3' Left 3.6' to Flow
0+20	3.1	4.09	E'ly Line Stairway End 6" PCC
0+56	5.1	2.09	
0+51.80 ✓	5.2	1.99	Begin 6" PCC W'ly Line Mission Blvd
0+52	5.7	1.49	W'ly Curb Line Mission Blvd Begin 2" AC Crown Cont Storm Gate and Line
0+89?	5.1	2.09	Bott Curb Center Island
0+89?	1.4	2.79	Top " " "
0+91.9			Power Pole 9.25' Rt
0+93.6	1.6	2.59	Top Curb Center Island
0+93.6	5.3	1.89	Bott " " "
1+00	5.4	1.79	
1+00.5	5.4	1.79	6 V On Line ✓
1+02.5	5.4	1.79	6 V 5' Left ✓

Reduced by Palomino 8-10-55

ALLEY BLK 139-140 (CONT)

7.19

1+13.50		6.2	.99
~~1+23.5~~	1+31 29	6.2	.99
~~1+50~~	1+58 30	6.7	.49
~~2+00~~	2+08 30	8.0	- .81
~~2+43.9~~	2+52 15	8.1	- 1.51
~~2+50~~	2+58 30	8.8	- 1.61
~~2+52~~	2+60 30	8.8	- 1.61
~~2+52~~	2+60 30	8.74	1.55
~~2+59.35~~	2+67 75	8.5	1.31
TP		2.89	4.35
	4.99 9.34		
		7.26	7.08 = 7.09

ELY CURB LINE MISSION BLVD END 2" AC CROWN CONT

END 6" PCC ELY LINE MISSION BLVD

WLY BAYSIDE LANE BEGIN 6" PCC

SEWER CROSSING

SLY RIM SEWER MH 3.5 LEFT 4.0' TO FLOW

ELY BAYSIDE LANE END 6" PCC

TBM LEAD & TACK N/E COR. STANDWAY ALLEY BLK 140

SEA WALL & EL CHANNEL BP

WEMT
ALEXANDER
HOLAHAN

7-14-55

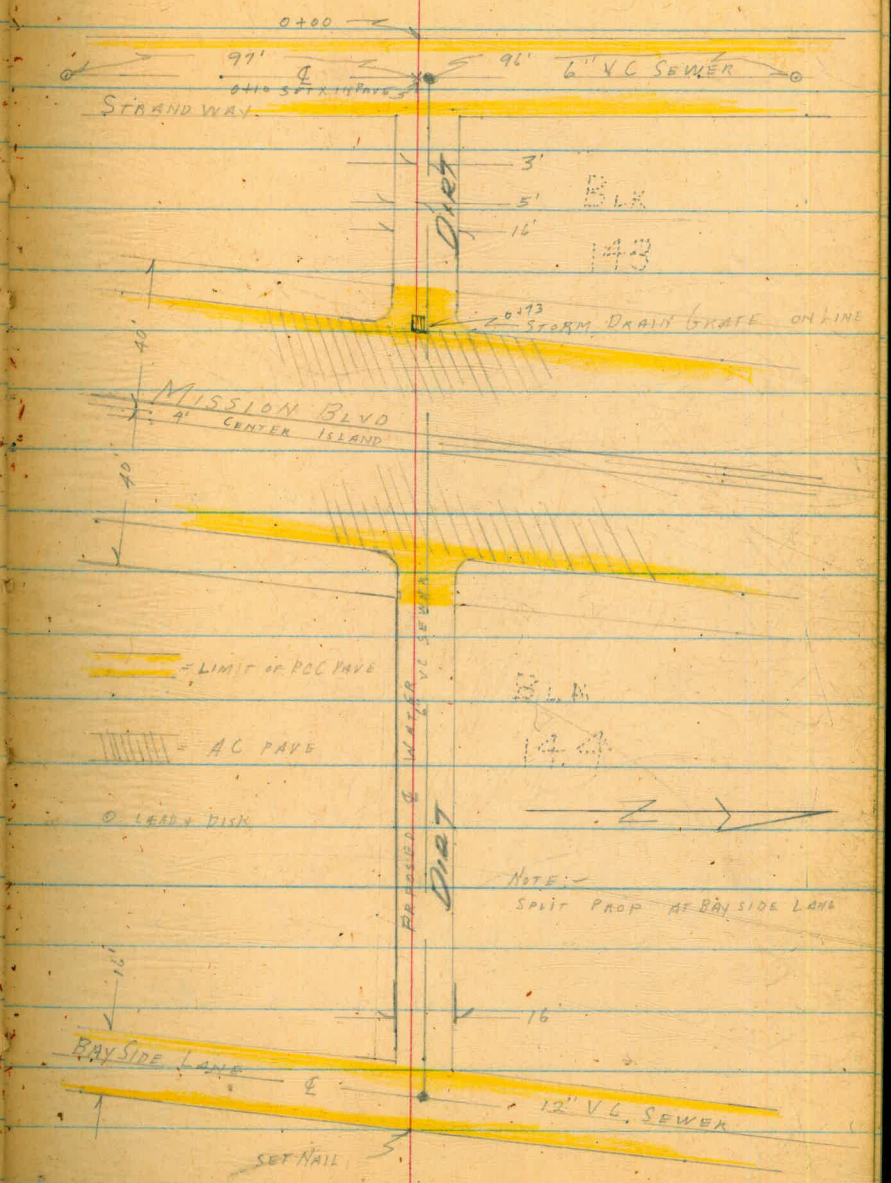
ALLEY BLKS 143-144

N/O EL CARMEL - STRANDWAY TO BAY SIDE LANE

PLAN & PROFILE & PROPOSED WATER LINE

0+00 W'LY LINE STRANDWAY

2+80.09 E'LY LINE BAY SIDE LANE



ALLEY BLK 143-144 (CONT)			
		7.09	BM BP IN SEA WALL S'LY EL CARMEL
	2.30	9.39	
		5.13 4.26	TBM S'LY RIM SEWER MH 2.5' LFT 0+10
	2.81	7.07	
0+00		2.5 4.57	BEGIN 6" PCC W'LY LINE STRANDWAY
0+08			6 V. 11' LEFT
0+10		2.8 4.27	SEWER CROSSING
0+10		2.81 4.26	S'LY RIM SEWER M.H. 2.5' LEFT 3.7 TO FLOW
0+20		2.6 4.47	END 6" PCC E'LY LINE STRANDWAY
0+50		4.6 2.47	
0+62			G.V. 0.5' RT
0+62.4		5.0 2.07	W'LY EDGE MISSION BLVD BEGIN 6" PCC
0+73		5.7 1.37	W'LY CURB LINE BEGIN 2" A.C. CROWN CONT STORM GRATE ON LINE
1+00.5		5.2 1.87	BOTT CURB CENTER-ISLAND
1+00.5		4.6 2.47	TOP " " "
1+04.4		4.8 2.27	TOP " " "
1+04.4		5.4 1.67	BOTT " " "

Reduced by Pantograph to 8-11-53

ALLEY BLK 143-144 (CONT)

7.07

1+11	5.5	1.57	GV 1' RT
1+13.5	5.5	1.57	GV 0.5' LFT
1+32	6.0	1.07	W'LY CURBLINE END 3" AC CROWN CONT
1+42.32	5.7	1.37	W'LY LINE MISSION BLVD END 6" PCC
1+50	6.1	.97	
2+00	7.7	-.63	
2+50	8.8	-1.73	
2+63.9	8.7	-1.63	W'LY LINE BAYSIDE LANE BEGIN 6" PCC
2+73.5	8.8	-1.73	SEWER CROSSING
2+73.5	8.85	-1.78	S'LY RIM SEWER MH 3' LFT 3.5' TO FLOW
2+76			GV 8' LEFT
2+80.09	8.6	-1.53	E'LY LINE BAYSIDE LANE END 6" PCC
	3.29	3.78 = 3.77 TBM	TOP FH S/E EL CARMEL & MISSION

ALTADENA ST.

120' So. of STERLING CT. To So. Termini

2/27/56
SHOREY
MARTELL
KEMP
SMITH

		⑤ STK's & GRD		6" A.C. MAIN		
BM	5.03	322.26		317.23		
TP	10.28	331.15	1.39	320.87		NAIL IN P.P. S.W. COR. STERLING CT. &
		CITY WILL MAKE CONN. TO EXIST. MAIN				
0+00			5.7	325.5	319.2	$C6\frac{3}{-}$ NOT MK'D
0+25			4.3	326.9	320.3	$C6\frac{6}{-}$
0+50			3.9	327.3	321.3	$C6\frac{2}{-}$
1+00			4.3	326.9	322.0	$C4\frac{9}{-}$
1+50			5.4	325.8	321.4	$C4\frac{4}{-}$
2+00			7.3	323.9	319.5	$C4\frac{4}{-}$
2+50			9.8	321.4	317.5	$C3\frac{9}{-}$
3+00	9.76	320.59	11.82	319.33	315.5	$C3\frac{8}{-}$
3+41			2.7	317.9	313.9	$C4\frac{0}{-}$
3+50			3.2	317.4	313.0	$C4\frac{4}{-}$
3+73			4.3	316.3	310.8	$C5\frac{5}{-}$
3+91			5.2	315.4	311.7	$C3\frac{7}{-}$
4+00			5.6	315.0	311.4	$C3\frac{6}{-}$
4+10 G.V. (OMIT)					311.0	
4+15 F.H. TEE ⑤			6.1	314.5	310.8	$C3\frac{7}{-}$
			5.5	315.1		$64\frac{3}{-}$ $F;\frac{3}{-}$
4+50			7.3	313.3	309.6	$C3\frac{7}{-}$
5+00			8.7	311.9	308.4	$C3\frac{5}{-}$
5+50			9.7	310.9	307.2	$C3\frac{7}{-}$
6+00	4.29	318.89	9.76	310.83	307.1	$C3\frac{7}{-}$
6+22 $\frac{30}{-}$ B.C.			7.9	311.0	307.4	$C2\frac{6}{-}$
6+50			7.4	311.5	307.9	$O3\frac{6}{-}$

ALTADENA ST.
(CONT'D)

	318.89			
7+00	6.6	312.3	308.8	C3 5
7+25 65 E.C.	6.1	312.8	308.6	C4 2
7+50	5.8	313.1	308.5	C4 6
8+00	5.1	313.8	308.2	C5 6
8+50 (OMIT)			308.0	
8+53 6"Cap-2"B.O.	4.9	314.0	308.0	C6 C.
	4.29	314.60 =	314.60	1½" I.P. 21' LT. STA. 8+53 73 (SEE PG. 29)

314.60

ALLEY BLK 253
NORTH of LYRAS, E. of GEORGIA ST.
⑤ MK'S & GED. 4" A.C. MAIN

2/27/56
SHOREY
MARTELL
KEMP
SMITH

BM	4.66	240.77		236.11	
0+92	{6"x4" REDUCER BY City BEGIN WORK.		6.7	234.1	231.2
0+96	6.V & 45° BEND BY City		7.2	233.6	231.3
0+67 21	45° BEND		4.2	236.6	232.0
0+75			4.3	236.5	232.2
1+00			4.5	236.3	232.3
1+25			4.7	236.1	232.4
1+50			4.7	236.1	232.3
2+00			4.8	236.0	231.7
2+50			5.1	235.7	231.3
3+00			5.5	235.3	230.7
3+50	11¼° VERT. BEND		10.0	236.8	230.0 ~~230.0~~
4+00	4"Cap - 2" S.O. Assy. ⑩ RT.		19.7 12.1	221.1 228.7	221.5 ~~221.5~~
CK. BM			4.66	236.11 = 236.11	

WATER METERS
240.77

1+19 E	5.4	235.4	236.8	
1+25 W.	2.4	238.4	236.5	
1+27 W.	2.4	238.4	236.5	
2+15 W.	3.7	237.1	235.6	
2+16 E.	6.0	234.8	236.1	
2+58 W.	6.6	234.2	235.2	

L & T & WILSHIRE TERRACE & 3' NOR. N/L MYRTLE

$C2^{2}_{+}$	NOT MK'D		
$C2^{3}_{-}$	" "		
$C4^{6}_{-}$			
$C4^{3}_{-}$			
$C4^{0}_{-}$			
$C3^{7}_{-}$			
$C3^{2}_{-}$			
$C4^{3}_{-}$			
$C4^{4}_{-}$			
$C4^{6}_{-}$			
~~$C7^{2}$~~ $C0^{8}_{-}$		6.8	
$F0^{4}_{-}$		15.4	
$C7^{2}_{-}$			
$F1^{4}_{-}$	"3446" FLORIDA		(SET METERS 15' RT. & 13' LT.
$C1^{9}_{-}$	"3446"		
$C1^{2}_{-}$	"3438"		
$C1^{5}_{-}$			
$F1^{2}_{-}$			
$F1^{0}_{-}$			

ALLEY BLK. 3

NOR. OF POLK - E. OF 33RD ST.

④ STK'S & GRD. 6" A.C. MAIN

2/28/56
SHOREY
MARTELL
KEMP
SMITH

BM	2.40	369.06		366.66	S.W. BP 33RD & ORANGE	
TP	2.37		BEGIN WORK	364.33	7.10	361.96
0+40			CITY CONN. TO EXIST. G.V.	9.3	355.0	352.0 C3.0± NOT MK'D
0+50				8.5	355.8	352.4 C3.4
0+75				6.6	357.7	353.3 C4.4
1+00				6.2	358.1	354.0 C4.1
1+25				5.6	358.7	354.6 C4.1
1+50				5.2	359.1	355.0 C4.1
2+00				4.5	359.8	355.7 C4.1
2+50				3.5	360.8	356.5 C4.3
3+00				2.6	361.7	357.2 C4.5
3+50				2.0	362.3	358.0 C4.3
4+00	TP	6.52	369.97	0.88	363.45	358.8 C4.2
4+50				6.4	363.6	359.7 C3.9
5+00				5.3	364.7	360.4 C4.3
5+50				4.0	366.0	361.3 C4.7
6+00				4.0	366.0	362.1 C3.9
6+25			G.V. BY CITY (OMIT)			362.4 ± NOT MK'D
6+38.5			END WORK 6"x6" TEE BY CITY	3.8	366.2	362.5 C3.7 ± " "
CK. BM				3.30	366.67 = 366.66	

MOVED LINE 4' LT. TO MEET EXIST. G.V.

MOVED LINE 3.30 LT.

MOVED LINE 1.67 LT.

LINE ON ℄

(CONT'D)

ALLEY BLK. 3
(CONT'D)

WATER METERS
364.33

0+58 E.		7.0	357.3	356.6	CO 2
0+83 W.		7.0	357.3	357.5	FO 2
0+94 E.		6.3	358.0	357.8	CO 2
1+02 E.		6.2	358.1	358.0	CO 1
1+18 W.		6.3	358.0	358.3	FO 3
1+44 E.		5.5	358.8	358.7	CO 1
1+47 W.		5.5	358.8	358.8	CO 0
1+92 E.		4.8	359.5	359.5	CO 0
1+98 W.		4.9	359.4	359.6	FO 2
2+37 E.		4.0	360.3	360.2	CO 1
2+47 W.		3.8	360.5	360.3	CO 2
2+84 E.		2.7	361.6	361.0	CO 6
3+04 W.		2.8	361.5	361.2	CO 3
3+26 E.		2.2	362.1	361.6	CO 5
3+38 W.		2.2	362.1	361.8	CO 3
3+75 W.		1.6	362.7	362.4	CO 3
3+90 E.		1.3	363.0	362.7	CO 3
4+35 E.	369.97	6.5	363.5	363.4	CO 1
4+39 W.		6.4	363.6	363.4	CO 2
4+90 E.		5.9	364.1	364.4	FO 3
5+07 W.		5.1	364.9	364.5	CO 4
5+13 E.		4.8	365.2	364.7	CO 5
5+18 W.		4.8	365.2	364.7	CO 5
5+30 W.		4.8	365.2	364.8	CO 4
5+42 E.		4.2	365.8	365.1	CO 7
5+65 W.		3.3	366.1	365.5	CO 6
5+69 E.		4.0	366.0	365.5	CO 5

(5+42 NO METER)

ALLEY BLK. "G"

TERALTA HGHTS UNIT 2
NORTH of MONROE, EAST of CHEROKEE
(4) STK'S & GRD. 6" A.C. MAIN

3/12/56
SHOREY
MARTELL
KEMP
SMITH

BM	2.94	389.62	386.68		TOP NEW CURB ~~S.E.B.P. MONROE & CHEROKEE~~ (OUT)
	CITY TO CONN. TO EXIST. 6" G.V.				
0+60	BEGIN WORK	5.1	384.5	380.7	$C3^{8}_{-}$ NOT MK'D
1+00		4.3	385.3	381.4	$C3^{9}_{-}$
1+50		4.7	384.9	381.1	$C3^{8}_{-}$
2+00		4.9	384.7	380.7	$C4^{0}_{-}$
2+50		5.5	384.1	380.4	$C3^{7}_{-}$
3+00		5.8	383.8	380.1	$C3^{7}_{-}$
3+50		5.8	383.8	379.8	$C4^{0}_{-}$
4+00		6.0	383.6	379.5	$C4^{1}_{-}$
4+50		6.5	383.1	379.1	$C4^{0}_{-}$
4+68±	END WORK - CITY TO CONN. TO EXIST. 6" G.V.	6.9	382.7	379.0	$C3^{7}_{+}$ NOT MK'D
CK. TBM		4.89	384.73	= 384.74	TBM SPIKE IN P.P. W&N END ALLEY F.B. 870-60

WATER METERS

389.62

0+93	W.	4.6	385.0	385.1	$F0^{1}_{-}$	3+59	W.	383.9	383.6	$C0^{3}_{-}$
1+02	E.	4.3	385.3	385.1	$C0^{2}_{-}$	3+83	W.	384.1	383.4	$C0^{7}_{-}$
1+12	W.	4.2	385.4	385.2	$C0^{2}_{-}$	4+25	W.	383.7	383.2	$C0^{5}_{-}$
1+35	E.	4.4	385.2	384.9	$C0^{3}_{-}$					
1+63	E.	4.7	384.9	384.7	$C0^{2}_{-}$					
1+65	W.	4.7	384.9	384.8	$C0^{1}_{-}$					
2+01	W.	5.0	384.6	384.6	$C0^{0}_{-}$					
2+25	E.	4.9	384.7	384.5	$C0^{2}_{-}$					
2+60	W.	5.2	384.4	384.2	$C0^{2}_{-}$					
2+83	W.	5.4	384.2	384.1	$C0^{1}_{-}$					
2+97	E.	5.7	383.9	383.8	$C0^{1}_{-}$					
3+14	W.	5.5	384.1	383.8	$C0^{3}_{-}$					
3+18	E.	5.7	383.7	383.7	$C0^{0}_{-}$					

ALLEY BLK "B"
TERALTA HGHTS
NORTH of MEADE, E. of WILSON

3/12/56
SHOBEY
MARTELL
KEMP
SMITH

BM	3.46	391.66		388.20
	BEGIN WORK			
0+80	CITY TO CONN. EXIST. 6"G.V.		4.1	387.6	383.3
1+00			3.1	388.6	383.6
1+50			2.7	389.0	384.5
1+75			2.5	389.2	385.0
2+00			2.6	389.1	385.1
2+50			2.6	389.1	385.4
3+00			2.1	389.6	385.6
	TP	5.99	395.53	2.12	389.54	
3+50				5.7	389.8	385.9
4+00				5.6	389.9	386.2
4+50				4.6	390.9	386.4
5+00				4.6	390.9	386.7
5+50				3.7	391.8	387.0
6+00				3.6	391.9	387.3
6+37 5				3.8	391.7	387.5
6+50				3.9	391.6	387.3
6+81 4	END WORK					
	CITY TO CONN. EXIST. 6"G.V.		5.0	390.5	387.0
CK. TP			3.99	391.54 = 391.56	

(CONT'D)

N.W.B.P. MEADE & WILSON

$C_4^{3\pm}$	NOT MK'D
C_5^{0}	
C_4^{5}	
C_4^{2}	
C_4^{0}	
C_3^{7}	
C_4^{0}	
C_3^{2}	
C_3^{7}	
C_4^{5}	
C_4^{2}	
C_4^{8}	
C_4^{6}	
C_4^{2}	
C_4^{3}	
$C_3^{5\pm}$	NOT MK'D

SEW. M.H. 6+63 (F.B. 867-51)

NOTE: ℄ of pipe staked 4.5' w'ly of E. prop. line of Alley

391.56 | 6+69

ALLEY BLK "B"
CONT'D

WATER METERS

	391.66						395.53		
1+20 W.	3.2	388.5	388.0	Co 5	5+47 E.	3.6	391.9	390.8	C1 1
1+26 E.	2.8	388.9	388.1	Co 8	5+52 W.	3.9	391.6	390.8	Co 8
1+54 W.	2.5	389.2	388.4	Co 8	5+58 W.	3.6	391.9	390.9	C1 0
1+57 W.	2.6	389.1	388.5	Co 6	5+77 E.	3.8	391.7	391.0	Co 7
1+79 E.	2.5	389.2	388.8	Co 4	6+02 W.	3.7	391.8	391.1	Co 7
2+07 E.	2.6	389.1	388.7	Co 2	6+07 W.	3.6	391.9	391.1	Co 8
2+11 W.	2.6	389.1	389.0	Co 1	6+22 E.	3.8	391.7	391.2	Co 5
2+38 W.	2.5	389.2	389.1	Co 1	6+42 E.	3.7	391.8	391.3	Co 5
2+61 E.	2.5	389.2	389.2	Co 0	6+52 W.	3.4	392.1	391.2	Co 9
2+72 W.	2.3	389.4	389.3	Co 1					
2+91 E.	2.2	388.5	389.4	Co 1					
3+41 W.	5.4	390.1	389.7	Co 1					
3+71 W.	4.8	390.7	389.8	Co 2					
4+03 W.	4.9	390.6	390.0	Co 6					
4+21 E.	5.4	390.1	390.1	Co 0					
4+48 E.	4.6	390.9	390.3	Co 6					
4+48 W.	4.9	390.6	390.3	Co 3					
4+89 E.	4.6	390.9	390.5	Co 4					
5+05 W.	4.2	391.3	390.6	Co 7					

HILGER ST.

GIBSON TO MADERA
(3) STK's & GRD. 6" A.C. MAIN

3/19/56
SHOREY
KEMP
MARTELL
SMITH

TBM	1.02	318.92		317.90		S.E. ¾" I. PIPE GIBSON & HILGER
BEGIN WORK						
0+41	CITY TO CONN. EXIST. TEE		3.5	315.4	309.7	C5 7 ± NOT MK'D — 9.0 309.9 TOP EXIST. TEE
0+50			4.1	314.8	309.4	C5 4 ±
1+00			7.1	311.8	306.9	C4 2 ±
1+50			10.0	308.9	304.5	C4 4 ±
2+00 TP		0.48	306.72	12.68	306.24	301.9 C4 3 ±
2+50			3.3	303.4	299.4	C4 0 ±
3+00			6.1	300.6	296.8	C3 8 ±
3+50			8.5	298.2	294.2	C4 0 ±
4+00			10.8	295.9	291.8	C4 1 ±
4+11	13 6"x6" TEE BY CONT.		11.2	295.5	291.2	C4 3 ±
4+50 TP		1.53	295.10	13.15	293.57	289.2 C4 4 ±
5+00			3.0	292.1	286.7	C5 4 ±
5+50			5.9	289.2	284.1	C5 1 ±
6+00			8.3	286.8	281.6	C5 2 ±
6+50			10.6	284.5	279.0	C5 5 ±
7+00 TP		2.04	283.90	13.24	281.86	276.4 C5 5 ±
7+25			3.6	280.3	275.0	C5 3 ± — TO MEET EXIST. G.V. — MOVED LINE 1L RT.
END WORK						MOVED LINE 1 2 RT
7+41	CITY TO CONN. EXIST. G.V.		6.1	277.8	274.6	C3 2 ± NOT MK'D — TOP F.H. 20' RT. 8+03
CK. TBM			3.86	280.04 =	280.07	"332"
1+83 S.		WATER METERS		12.0	306.9	306.4 C0 5 ±
2+56 S.				4.1	302.6	302.7 F0 1 ± "13.4"

ZELLER ST.

GIBSON TO KLAUBER AVE.
(5) STA'S & GRD. 6" A.C. MAIN

3/21/56
SHOBEY
KEMP
MARTELL
SMITH

BM	3.20	366.24		363.04	2X2 HUB N.W. COR. GIBSON & ZELLER
0+32.3 BEGIN WORK - G.V.			12.5	353.7	350.5 C_3^2
0+50			11.2	355.0	351.6 C_3^4
0+75			8.1	358.1	353.2 C_4^2
1+00			6.5	359.7	355.0 C_4^2
1+25			4.5	361.7	357.2 C_4^5
1+50			3.7	362.5	359.0 C_3^5
1+75			1.7	364.5	360.8 C_3^7
2+00			0.9	365.3	361.8 C_3^5
TP	11.00	376.38	0.86	365.38	
2+50			9.9	366.5	363.0 C_3^5
3+00			9.5	366.9	363.8 C_3^1
3+50			8.8	367.6	364.6 C_3^0
4+00			7.9	368.5	365.4 C_3^1
4+25			7.2	369.2	365.8 C_3^4
4+50			7.0	369.4	366.1 C_3^3
4+70 F.H.GV.			7.0	369.4	366.3 C_3^1
4+75 F.H. TEE			6.8	369.6	366.4 C_3^2
(5)			10.0	366.4	C_0^0 F_3^8 (370.2)
5+00			7.1	369.3	366.7 C_2^6
5+50			6.1	370.3	367.1 C_3^2
6+00			5.2	371.2	367.6 C_3^6

ZELLER ST. (CONT'D)

3/21/56
SHOREY
MARTELL
KEMP
SMITH

376.38

6+25			4.6	371.8	368.2
6+50			3.2	373.2	369.3
6+75			1.9	374.5	370.5
7+00			0.10	376.3	372.2
TP	13.28	389.66	0.00	376.38	
7+25			11.3	378.4	374.6
7+50			8.8	380.9	377.5
7+75			5.7	384.0	380.4
8+00			2.2	387.5	383.8
TP	13.26	402.72	0.20	389.46	
8+50			7.6	395.1	390.6
9+00			0.7	402.0	397.0
TP	12.94	415.47	0.19	402.53	
9+50			6.3	409.2	403.4
10+00			0.4	415.1	409.8
TP	13.21	428.32	0.36	415.11	
10+50			7.5	420.8	416.7
11+00			1.2	427.1	423.4
TP	12.67	440.21	0.78	427.54	
11+25			9.3	430.9	426.8
11+50			6.4	433.8	429.4
11+75			2.9	437.3	431.2
12+00			1.5	438.7	432.6
12+24.5	END WORK - CITY TO CONN. EXIST. G.V.		1.0	439.2	434.0
CK. TBM			3.14	437.07	= 436.87

C3 6
C3 8
C4 0
C4 1
C3 8
C3 4
C3 6
C3 7
C4 5
C5 0
C5 8
C5 3
C4 1
C3 7
C4 1
C4 4
C6 1
C6 1
C5 2± NOT MK'D

E. RIM M.H 12+53 10' LT.
F.B. 909-41

H.I.
440.21 − 3.00 = 437.21
437.17

CHISL + 12' N.W. SEWER M.H. ON KLAUBER AVE.
F.B. 909-41

ZELLER ST.
(CONT'D)

3/21/56
SHOREY
KEMP
MARTELL
SMITH

WATER METERS.

	376.38				
3+90 W.		2.6	373.8	368.3	C_5^5
5+62 W.		2.9	373.5	370.2	C_3^2
	389.66				
7+20 E.		12.4	377.3	377.1	C_0^2
	402.72				
8+22 E.		13.1	389.6	389.8	F_0^2

SET 4 VERT. RISER 29' LT. & 9' RT.

GIBSON ST.
HILGER TO 69th ST.
⑤ STRS & GRD. 6" A.C. MAIN.

3/21/56
SHOREY
MARTELL
KEMP
SMITH

BM	11.03	328.93		317.90	
0+21	BEGIN WORK		14.1	314.8	303.7
0+26	G.V. By City		13.5	315.4	309.7
0+50			11.9	317.0	311.8
0+75			8.0	320.9	314.6
1+00			4.4	324.5	318.5
TP	12.75	341.53	0.15	328.78	
1+50			11.0	330.5	326.1
2+00			4.1	337.4	333.7
2+25			0.9	340.6	337.0
TP	13.00	354.45	0.08	341.45	
2+75			7.3	347.2	342.2
3+25			2.9	351.6	345.4
3+75			1.0	353.5	346.8
4+00			1.1	353.4	347.0
4+50			1.8	352.7	347.2
5+00			2.5	352.0	347.5
5+25 TP	4.25	355.50	3.20	351.25	347.6
5+50			4.6	350.9	347.6
6+00			5.4	350.1	346.7
6+01 F.H. TEE			5.5	350.0	346.6
⑤			7.5	348.0	
6+50			7.2	348.3	345.1

$C5^{1}$ ± NOT MK'D.
$C5^{2}$ ± NOT MK'D
$C5^{2}$
$C6^{3}$
$C6^{0}$
$C4^{4}$
$C3^{7}$
$C3^{6}$
$C5^{0}$
$C6^{2}$
$C6^{7}$
$C6^{4}$
$C5^{5}$
$C4^{5}$
$C3^{7}$
$C3^{3}$
$C3^{4}$
$C3^{4}$
$C1^{4}$ $F3^{5}$ 351.5
$C3^{2}$

GIBSON ST. (CONT'D)

3/21/56
SHOREY
MARTELL
KEMP
SMITH

355.50

6+57 14 6"x6" TEE			7.7	347.8	344.8	C_3^0
6+75			8.6	346.9	343.8	C_3^1
7+25			10.1	345.4	342.0	C_3^4
7+75			9.4	346.1	342.8	C_3^3
8+12 5			7.2	348.3	344.7	C_3^6
8+50			4.6	350.9	347.4	C_3^5
9+00			0.7	354.8	351.0	C_3^8
TP	12.43	367.19	0.74	354.76		
9+50			8.7	358.5	354.6	C_3^8
9+75			6.7	360.5	356.4	C_4^1
10+25			2.8	364.4	360.6	C_3^8
TP	5.56	372.47	0.28	366.91		
10+75			5.0	367.5	363.7	C_3^8
11+25			3.6	368.9	365.3	C_3^6
11+75			3.7	368.8	365.4	C_3^4
11+82 F.H. TEE			3.9	368.6	365.2	C_3^4
(5)			3.7	368.6		C_3^4 F_3^6 (372.2)
12+25			5.0	367.5	364.3	C_3^2
12+50			6.0	366.5	363.4	C_3^1
13+00			8.5	364.0	361.4	C_2^6
13+50			11.6	360.9	357.5	C_3^4

GIBSON ST. (CONT'D)

3/22/56

		372.47				
CK. TBM	0.83	363.87	9.37	363.10 =	363.04	
14+00			6.8	357.1	353.7	C_3^4
14+35 17 G.V.			9.9	354.0	350.4	C_3^6
14+40 17 6"x6" WYE			10.2	353.7	350.0	C_3^7
14+50			11.1	352.8	349.8	C_3^6
TP	2.31	363.66	12.52	351.35		
15+00			5.8	347.9	345.1	C_2^8
15+25			8.2	345.5	342.8	C_2^7
15+50			9.3	344.4	341.3	C_3^1
15+62.5			9.9	343.8	340.6	C_3^2
16+00			10.0	343.7	340.6	C_3^1
16+50			8.6	345.1	341.3	C_3^8
16+75			7.9	345.8	342.3	C_3^5
17+00			6.6	347.1	344.0	C_3^4
17+25			4.0	349.7	345.8	C_3^9
17+50 TP	12.28	364.76	1.18	352.48	348.9	C_3^6
17+75			8.9	355.9	351.9	C_4^0
18+00			5.6	359.2	355.2	C_4^0
18+25			2.1	362.7	358.6	C_4^1
18+28 E.H. TEE			1.8	363.0	358.8	C_4^2
(5)			2.1	362.7		C_3^9 F_3^7 (36.4)
TP	10.15	374.57	0.64	364.12		
18+50			8.2	366.4	362.8	C_3^6

GIBSON ST. (CONT'D)

3/22/56

		374.57			
18+78 93 END –	2" B.O.	2.7	371.9	367.5	C_4^4
CK. TBM		11.52	363.05	363.04	
	WATER METERS				
1+80 W.	341.53	6.1	335.4	333.7	C_1^2
	354.45				
3+50 W.		+3.9	358.4	349.3	C_9^4
	354.45				
3+65 E.		1.7	353.8	349.3	C_3^5
4+72 W.		+5.2	359.7	350.3	C_9^4
4+93 E.		2.9	351.6	349.9	C_1^2
	355.50				
5+81 E.		5.6	349.9	350.1	F_0^2
7+99 E.		8.4	347.1	351.5	F_4^4
	372.47				
12+58 W.		+3.0	375.5	367.6	C_7^2
13+26 E		10.1	362.4	362.0	C_0^4
13+26 W.		3.1	369.4	362.1	C_1^3
13+29 E.		10.3	362.2	362.3	F_0^4
	353.66				
16+70 E.		8.4	345.3	346.0	F_2^2

SET G VERT. RISER 9' RT. & 29' LT.

ALLEY BLK. 21
So. of PARK PL., E. of KENSINGTON DR.
(5) STK's & GRD. 4" A.C. MAIN

3/23/56
SHOREY
MARTELL
KEMP
SMITH

TBM	8.58	372.19		363.61	LET 7' OFF N.E. END ALLEY 21	
0+20.	BEGIN WORK		9.1	363.1	359.4	C_3^7 ± NOT MK'D	MOVED LINE 2' LT. } TO MEET EXIST. TEE
0+25	10"x4" REDUCER & 4" G.V. BY City		9.0	363.2	359.4	C_3^8 ± NOT MK'D	" " 1' LT } TEE
0+50			8.8	363.4	359.4	C_4^0	
0+62.5			7.5	364.7	360.0	C_4^2	
1+00			5.1	367.1	362.7	C_4^4	
1+25			4.8	367.4	363.4	C_4^0	
1+50.			4.7	367.5	362.6	C_3^9	
2+00			4.5	367.7	364.0	C_3^7	
2+50			5.0	367.2	363.5	C_3^2	
2+75			5.5	366.7	363.2	C_3^5	
3+00			7.1	365.1	362.0	C_3^1	
3+25			9.8	362.4	358.7	C_3^5	
3+28	4" G.V. By City		9.9	362.3	358.9	C_3^4 ± NOT MK'D	
3+33	6"x4" TEE By City		8.7	362.5	358.9	C_3^6 ± NOT MK'D	
CK. TBM			8.58	363.61 = 363.61		
		WATER METERS				
1+00 N.		372.19	4.7	367.5	366.6	C_0^9	
1+32 N.			4.6	367.6	367.2	C_0^4	
1+40 N.			4.6	367.6	367.3	C_0^3	
2+02 N.			4.2	368.0	367.3	C_0^1	
2+30 N.			4.2	368.0	367.2	C_0^8	
2+50 S.			4.5	367.7	367.1	C_0^6	
2+82 N.			5.0	367.2	366.4	C_0^8	

TARBOX ST.
HILGER TO 69th ST.
⑤ STA'S & GRD.
6" A.C. MAIN

3/26/56
SHOREY
KEMP
MARTELL
SMITH

TBM	13.08	310.84		297.76	2x2 HUB N.E. COR. HILGER & TARBOX
0+26	11¼° BEND		15.3	295.5	291.2 C4 3
0+50			14.3	296.5	291.7 C4 8
0+67	F.H. TEE		11.9	298.9	292.6 C6 3
	⑤		11.5	299.3	C6 7 C3 0 296.3
0+72	F.H.G.V.		11.2	299.6	292.9 C6 7
1+00			9.3	301.5	294.4 C7 1
1+50			6.3	304.5	298.0 C6 5
2+00			4.2	306.6	300.8 C5 8
2+25			3.5	307.3	301.8 C5 5
2+50			2.9	307.9	302.4 C5 5
3+00			2.0	308.8	303.2 C5 6
3+50			1.3	309.5	303.9 C5 6
4+00	TP 6.99	317.03	0.80	310.04	304.6 C5 4
4+50			6.6	310.4	305.3 C5 1
5+00			6.2	310.8	306.1 C4 7
5+50			5.8	311.2	306.8 C4 4
6+00			5.3	311.7	307.5 C4 2
6+50			4.6	312.4	308.2 C4 2
7+00			3.9	313.1	308.9 C4 3

TARBOX ST. (CONT'D)

3/26/56

		317.03			
7+50 F.H. TEE		2.8	314.2	309.6	$C4^6$
(5)		3.4	313.6		$C4^0$ $C0^2$ 313.4
7+55 F.H.G.V.		2.6	314.4	309.7	$C4^7$
8+00		1.7	315.3	310.4	$C4^2$
8+50		1.1	315.9	311.1	$C4^8$
9+00 TP 7.50	323.58	0.95	316.08	311.8	$C4^3$
9+50		7.2	316.4	312.5	$C3^2$
10+00		6.6	317.0	313.3	$C3^7$
10+50		5.7	317.9	314.0	$C3^2$
11+00		4.7	318.9	314.8	$C4^1$
11+50		3.8	319.8	315.6	$C4^2$
12+00		2.5	321.1	316.3	$C4^8$
12+50		1.5	322.1	317.0	$C5^1$
13+00 TP 7.44	330.95	0.07	323.51	317.8	$C5^7$
13+50		5.6	325.4	318.5	$C6^2$
14+00		5.0	326.0	319.3	$C6^7$
14+50		5.1	325.9	320.0	$C5^2$
14+65 F.H. TEE		5.0	326.0	320.2	$C5^8$
(5)		6.6	324.4		$C4^2$ $C0^5$ 323.9

TARBOX ST. (CONT'D)

	330.95			
15+00.		4.4	326.6	320.7
15+20 2' B.O.		3.8	327.2	321.0
CK. TBM		1.82	329.13 =	329.14
	310.84			
1+16 E.		8.3	302.5	298.9
1+90 E.		5.4	305.4	303.5
3+66 E.		2.2	308.6	306.9
	317.03			
3+70 W.		5.7	311.3	307.3
4+53 W.		5.3	311.7	308.5
4+97 E.		6.8	310.2	308.7
7+14 E.		3.9	313.1	311.8
7+85 W.		0.6	316.4	313.4
8+00 E.		1.8	315.2	313.0
	323.58			
9+13 E.		7.9	315.7	314.7
10+53 W.		4.1	319.5	317.2
11+04 E.		5.2	318.4	317.5
11+70 W.		1.6	322.0	318.9
11+91 E.		3.5	320.1	318.9
12+73 E.		1.3	322.8	319.9

C5 2

C6 2

E MON. TARBOX & NELY LINE 69th

C3 6

C1 2

C1 7

C4 0

C3 2

C1 5

C1 3

C3 0

C2 2

C1 0

C2 3

C0 9

C3 1

C1 2

C2 4

330.95

12+88 W.	7.2	323.8	320.7	C3 1
13+83 W.	3.9	327.1	322.1	C5 0
14+14 W.	4.1	326.9	322.5	C4 4

PLOVER ST.
KLAUBER TO GIBSON ST.
(5) STK'S & GRD. 6" A.C. MAIN

4/11/56
SHOREY
MARTELL
KEMP
SMITH

TBM	5.17	448.94		443.77	S.E.F.H. KLAUBER & PLOVER
0+69	BEGIN WORK CITY TO CONN. G.V.		10.4	438.5	434.2
1+00			9.0	439.9	433.4
1+50			6.7	442.2	435.5
2+00			5.1	443.8	437.5
2+25			4.6	444.3	438.4
2+75			3.8	445.1	439.2
3+00			3.7	445.2	439.2
3+50			5.3	443.6	438.6
4+00			8.2	440.7	436.9
4+50			11.7	437.2	435.1
TP	7.13	443.88	12.19	436.75	
4+75			8.3	435.6	433.0
5+00			9.5	434.4	432.1
5+50			11.2	432.7	430.4
5+88.5			11.8	432.1	430.0
6+12.5			11.5	432.4	430.0
6+50			10.3	433.6	431.4
6+75			9.1	434.8	431.8
7+00			7.9	436.0	431.6
7+50	F.H. TEE		4.9	439.0	431.4

C4 3.1 NOT MK'D
C6 5
C6 7
C6 3
C5 9
C5 3
C6 0
C5 0
C3 8
C2 1
C2 6
C2 3
C2 3
C2 1
C2 4
C2 2
C3 0
C4 4
C7 6

PLOVER ST. (CONT'D)

		443.88			
~~7+45~~	~~F.H. TEE~~			~~431.3~~	
(5)		2.8	441.1		C_9^{7} C_5^{3} (435.8)
7+55	F.H.G.V.	4.7	439.2	431.4	C_7^{8}
8+00		4.4	439.5	431.2	C_8^{3}
8+50	TP 2.14 439.99	6.03	437.85	430.8	C_7^{1}
8+75		3.3	436.7	430.6	C_6^{1}
9+00		4.9	435.1	430.1	C_5^{0}
9+25		7.0	433.0	428.8	C_4^{2}
9+48 91 B.C.		9.4	430.6	426.8	C_3^{2}
	TP 0.36 427.02	13.33	426.66		
~~9+50~~	~~(OMIT)~~			~~426.7~~	
9+98 06 E.C.		3.7	423.3	419.2	C_4^{1}
~~10+00~~	~~(OMIT)~~			~~419.1~~	
10+25		8.6	418.4	415.2	C_3^{2}
10+50		12.9	414.1	410.6	C_3^{5}
	TP 0.21 414.33	12.90	414.12		
10+75		5.1	409.2	405.8	C_3^{4}
11+00		10.6	403.7	400.6	C_3^{1}
	TP 0.25 401.45	13.13	401.20		
~~11+50~~		8.4	393.1	~~389.4~~ ~~390.4~~	C_2^{7} $_3^{7}$
	TP 0.55 389.69	12.31	389.14		
11+75		2.2	387.5	~~384.3~~ ~~385.3~~	C_2^{2} C_3^{3}
~~12+00~~		6.7	383.0	379.2	C_3^{8}

PLOVER ST.
(CONT'D)

		389.69				
12+0.5			10.7	379.0	375.0	$C4^{0}$
	TP 0.36	377.59	12.46	377.23		
12+50			2.8	374.8	369.0	$C5^{8}$
12+56⁵			3.9	373.7	368.0	$C5^{7}$
12+75			6.4	371.2	367.0	$C4^{2}$
13+00			10.0	367.6	363.6	$C4^{0}$
	TP 0.04	364.31	13.32	364.27		
13+50			5.2	359.1	356.2	$C2^{9}$
14+00			11.8	352.5	348.4	$C4^{1}$
14+19 22½° BEND			14.8	349.5	346.0	$C3^{5}$
~~14+24 GV.~~					345.2	
	1.06	358.16	7.31 7.56	357.10 350.60	= 350.67 NAIL IN RR. SWITCH, GIBSON + PLOVER	
WATER METERS						
		448.94				
3+09E			2.9	446.0	442.3	$C3^{7}$
3+16E			3.5	445.4	441.9	$C3^{5}$
3+49E			3.6	445.3	441.8	$C3^{5}$
3+93W.			8.1	440.8	440.1	$C0^{7}$
4+19W.			12.2	436.7	437.8	$F1^{1}$
		443.88				
5+00W.			10.3	433.6	436.3	$F2^{7}$ $F3^{1}$
5+30E.			8.0	435.9	436.1	$F0^{2}$
6+07W.			10.3	433.6	434.6	$F1^{0}$
8+09E.			2.5	441.4	434.3	$C7^{1}$

(350.07)

	439.99				
8+69W.		2.2	437.8	433.4	$C4^{4}$
9+41W.		9.2	430.8	430.7	$C0^{1}$
9+83E.	427.02	11.7	428.3	426.5	$C1^{8}$
10+52E.		12.3	414.7	413.2 ~~416.5~~	~~F1.8~~ $C0^{8}$
10+85W.	414.33	4.6	409.7	407.1 ~~410.6~~	~~F0.9~~ $C2^{6}$
12+20W.	401.45 389.69	4.8	384.9	380.9 ~~384.5~~	4^{2} ~~C0~~

℄ VERT. RISER SET 9' LT. ℄ 29' RT.

JAMACHA ROAD
LISBON TO GLENCOE
(5) STK'S & GRD. 8" & 10" A.C. MAIN

4/17/56
SHOREY
MARTELL
KEMP
SMITH

BM		4.32	315.79		311.47		1" I. PIN 10' RT. FENCE COR. LOT 12	
TP		7.76	320.24	3.31	312.48			
0+79	BEGIN WORK BY CITY REMOVE 3" B.O. & CONN			2.0	318.2	314.0 ~~314.6~~	4.2 ~~C5.6+~~	NOT MK'D
1+00				2.8	317.4	313.0 ~~313.4~~	~~C4.0~~ 4.4	2.7
1+47	∆ PT. & B.C.			4.5	315.7	310.8 ~~311.0~~	~~C4.7~~ 4.9	4.7
1+88.5	8" G.V.			6.0	314.2	309.0	C5.2	5.9
1+95	8" PRESS. REDUCER			6.2	314.0	308.7	C5.3	6.2
2+01.5	8" G.V. & 10"/8" REDUCER			6.4	313.8	308.6	C5.2	6.4
2+50				7.1	313.1	308.2	C4.9	7.5
3+00				7.3	312.9	307.8	C5.1	7.9
3+40	E.C.			8.1	312.1	307.5	C4.6	8.1
3+50				8.0	312.2	307.4	C4.8	8.9
4+00				7.5	312.7	307.0	C5.7	9.2
4+50				7.4	312.8	307.0	C5.8	9.3
5+00	TP	5.87	317.31	8.80	311.44	307.0	C4.4	9.2
5+50				6.4	310.9	307.0	C3.9	6.4
6+00				6.3	311.0	307.1	C3.9	6.2
6+25				6.0	311.3	307.2	C4.1	5.9
6+50				5.7	311.6	307.3 ~~307.4~~	~~C4.2~~ 4.3	5.6
6+91.96	B.C.			5.5	311.8	307.7 ~~307.9~~	~~C3.9~~ 4.1	5.3
7+00				5.4	311.9	307.8 ~~308.0~~	~~C3.9~~ 4.1	5.2

JAMACHA RD. (CONT'D)

4/17/56
SHOREY
MARTELL
KEMP
SMITH

317.31

7+50		4.8	312.5	308.3 ~~308.7~~	C_3^8 4^2	4.7	
8+00		4.3	313.0	308.8 ~~309.5~~	C_3^5 4^2	4.1	
8+50		3.6	313.7	309.3 ~~309.9~~	C_3^8 4^4	3.6	
	CK. BM	5.84	311.47				
8+86 34 — E.C.		3.6	313.7	309.6 ~~310.1~~	C_3^6 4^1	3.5	
9+00		3.6	313.7	309.7 ~~310.2~~	C_3^5 4^0	3.5	
9+12 F.H. TEE		3.6	313.7	309.8 ~~310.3~~	C_3^4 3^8	3.6	SET 5' F.H. FROM PROP.
(5)		4.2	313.1		C_3^3 F_1^1		(314.2)
9+17 F.H. G.V.		3.6	313.7	309.8 ~~310.4~~	C_3^3 3^9	3.4	
9+50		3.1	314.2	310.1 ~~310.6~~	C_3^6 4^1	3.1	
10+00		3.0	314.3	310.6 ~~311.7~~	C_3^4 3^7	2.8	
10+50		2.3	315.0	311.1 ~~311.2~~	C_3^7 3^9	2.4	
11+00 TP	6.91	322.38	1.84	315.47	311.6	C_3^8	1.7
11+50			6.5	315.9	312.2	C_3^7	6.5
12+00			5.8	316.6	312.8	C_3^8	5.8
12+50			5.0	317.4	313.2	C_4^2	5.1
13+00			5.1	317.3	313.5	C_3^8	4.8
13+50			4.7	317.7	313.7	C_4^0	5.0
13+62 F.H. TEE			4.2	318.2	313.8	C_4^4	4.6 SET 5' F.H. FROM PROP.
(5)			5.6	316.8		C_3^0 F_1^2	(317.8)

JAMACHA RD. (CONT'D)

4/17/56
SHOREY
KEMP
MARTELL
SMITH

			322.38					
13+67	F.H.G.V.			4.2	318.2	313.8	c 4^{4}	4.5
13+75				4.2	318.2	313.9	c 4^{3}	4.4
14+00				4.2	318.2	314.0 ~~314.2~~	~~c 4^{0}~~ 4^{2}	4.3
14+50				3.9	318.5	314.6 ~~315.0~~	~~c 3^{5}~~ 3^{9}	3.9
14+75				3.1	319.3	314.8 ~~315.5~~	~~c 3^{8}~~ 4^{5}	3.4
15+00				2.7	319.7	315.0 ~~315.6~~	~~c 4^{1}~~ 4^{7}	2.9
15+50				2.3	320.1	315.5 ~~315.9~~	~~c 4^{2}~~ 4^{6}	2.7
16+00				1.9	320.5	316.0 ~~316.2~~	~~c 4^{3}~~ 4^{5}	2.1
	TP	6.81	327.27	1.92	320.46			
16+50				6.5	320.8	316.4 ~~316.6~~	~~c 4^{2}~~ 4^{4}	6.8
16+75				6.2	321.1	316.8	c 4^{3}	6.6
17+00				5.7	321.6	317.0	c 4^{6}	6.4
17+50				5.2	322.1	317.6	c 4^{5}	5.9
18+00				4.5	322.8	318.2	c 4^{6}	5.3
18+50				4.5	322.8	318.4 ~~318.6~~	~~c 4^{2}~~ 4^{4}	5.0 ℄ approx same as ⑤
19+00				4.4	322.9	318.5 ~~318.9~~	~~c 4^{0}~~ 4^{4}	4.7
19+50				4.5	322.8	318.7 ~~319.3~~	~~c 3^{5}~~ 4^{1}	4.7
19+75				4.5	322.8	318.9 ~~319.4~~	~~c 3^{4}~~ 3^{9}	4.1
19+91	B.C.			4.4	322.9	319.1 ~~319.7~~	~~c 3^{2}~~ 3^{8}	
20+00				4.3	323.0	319.0 ~~320.0~~	~~c 3^{0}~~ 4^{0}	3.7

JAMACHA ROAD (CONT'D)

4/17/56
SHOREY
KEMP
MARTELL
SMITH

327.27

20+00 F.H. TEE		4.3	323.0	~~319.0~~ ~~321.6~~	C_3^2 4^0
(5)		4.9	322.4		C_3^4 $F1^2$
20+05 F.H.G.V.		4.3	323.0	~~319.1~~ ~~320.1~~	C_2^2 3^2
20+25		3.8	323.5	~~319.4~~ ~~321.4~~	C_3^2 4^1
20+50		3.2	324.1	~~319.7~~ ~~321.0~~	C_3^1 4^4
20+63 E.C.		3.0	324.3	~~319.8~~ ~~321.20~~	C_3^1 4^5
21+00		2.8	324.5	~~320.3~~ ~~321.5~~	C_3^2 4^2
21+50		2.2	325.1	~~321.2~~ ~~322.0~~	C_3^1 3^2
22+00 PI 2.99	333.94	1.32	325.95	~~322.2~~ ~~323.0~~	C_3^2 3^2
22+50		6.8	327.1	~~323.2~~ ~~324.0~~	C_3^1 3^2
23+00		5.7	328.2	~~324.2~~ ~~325.0~~	C_3^2 4^0
23+50		4.7	329.2	~~325.3~~ ~~326.1~~	C_3^1 3^2
23+91 Δ PT. 11¼° BEND -LT.		3.7	330.2	~~326.4~~ ~~327.0~~	C_3^2 3^8
24+00		3.3	330.6	~~326.7~~ ~~327.6~~	C_3^6 3^2
24+27 Δ PT. 11¼° BEND-RT. REMOVE 3" B.O. INSTALL		2.7	331.2	~~327.5~~ ~~327.7~~	C_3^5 3^7
24+75 10"G.V. By City		1.6	332.3	328.6	C_3^7 + NOT MK'D
~~24+79 END WORK~~					
CK. TP		1.43	332.51	332.55	TP ON END Cb. 10' ET. 15 RS E.B. 909-73
WATER METERS 317.31					
6+14 S.E.		6.2	311.1	310.5	$C0^6$ "7551" SET 6 VERT RISER 4⅝ RT.

323.6

(OVER)

JAMACHA RD.
(CONT'D)

WATER METERS
317.38 (CONT'D)

8+71 W.	3.0	314.3	312.9	C1 4/5		SET ℄ VERT. RISER 32 5/5 LT.
8+71 E.	3.6	313.7	312.9	CO 8/5		SET ℄ VERT. RISER 11 FT. ℄ 39' LT.
9+40 E.	3.4	313.9	313.4	CO 5/5	"7615"	
9+92 E.	1.9	314.4	313.7	CO 7/5	"7629"	
10+51 E.	1.9	314.4	314.1	CO 3/5	"7633"	
10+68 E.	2.6	314.7	314.3	CO 4/5	"7641"	
322.38						
11+74 E.	6.8	315.6	315.4	CO 2/5	"7655"	
12+05 W.	3.6	318.8	315.8	C3 0/5	"7655"	
12+36 E.	5.9	316.5	316.2	CO 3/5	"7665"	
12+76 W.	4.0	318.4	316.5	C1 9/5	"815"	
12+90 E.	6.2	316.2	316.5	FO 3/5	"7671"	
13+10 E.	6.3	316.1	316.6	FO 5/5	{ TO BANNER ST	
13+11 E.	6.0	316.4	316.6	FO 2/5		
14+96 E.	4.2	318.2	318.7	FO 5/5	"7715"	
15+15 E.	3.4	319.0	318.8	CO 2/5	"7723 & 7727"	
15+47 W.	0.3	322.1	319.1	C3 0/5	"7730"	
20+15 E	+0.7	323.1	322.2	CO 2/5	"7793"	

ELEVATIONS TOP EXISTING 6" A.C.
NOYES ST + BERYL ST.

WEST
WILLIAMS ST
VARONFAKIS +
KELLHOFER

4/17/56 CLOUDY
SEE PAGE 16

	12.67	148.05		135.38			TOP FH SW COR. BERYL + ACADEMY
T.P.	13.11	160.41	0.75	147.30			
T.P.	13.06	173.33	0.14	160.27			
T.P.	10.58	180.37	3.54	169.79			
T.P.	6.87	187.22	0.02	180.35			
T.P.	1.15	176.06	12.31	174.91			
2+00			10.03	166.03			TOP A.C. PIPE
2+00			7.9	168.2			TOP GROUND
2+00			8.26	167.8	165.3	C2 5	GIN. (5')
1+75			13.13	162.93			TOP PIPE
1+75			11.7	164.4			TOP GROUND
T.P. 1+75	1.14	165.37	11.83	164.23	162.3	C1 9	GIN. (5')
1+50			5.36	160.01			TOP PIPE
1+50			5.0	160.4			TOP GROUND
1+50 B.C.			4.86	160.51	158.1	C2 1	GIN. (5')
1+38.0			6.75	158.62			TOP PIPE
1+38.0			5.9	159.5	156.2	C3 2	TOP GROUND
1+38.0			6.0	159.4	156.2	C3 2	GIN (5')
1+38.0			0.18	165.19	160.63	✓	(5') PROP STK. C5 2 OK

EL. CONT. NOYES + BERYL

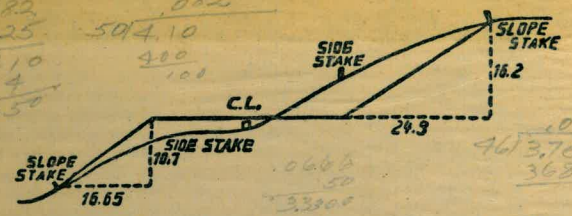
		165.37		
	1+00.		13.82	151.55
T.P.	1+00		9.1	156.3
T.P.	1+00		4.9	160.5 150.0
T.P.	1+15			154.7
T.P.	T.P. 0.90	153.72	12.55	152.82
T.P.	T.P. 0.84	141.30	13.26	140.46
2+00.	CHECK T.B.M.		12.64	128.66=
2+00				
2+00				
1+75				
1+75 T.P.				
1+75				
1+50				
1+50				
1+50 B.C.				
1+38.				
1+38.				
1+38.				
1+38.0				

760
602

Top pipe 1+00 8.2
Top Ground
Gin. (5') @ 10.5

160.5
J.A
162.9
8.2
154.7

128.72 P.P. # P. 4774 (200' ± So of Beryl On Noyes)



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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