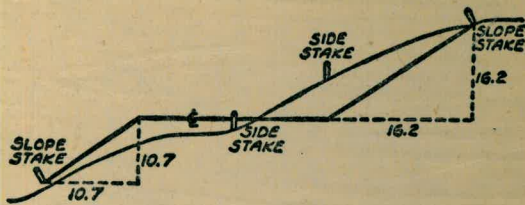


W 913



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.053	.058	.063
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

about depth of Main U.C.I.
 33rd St Webster to Steel St 1 ✓
 Group 24 Prelim
 Mallard Alameda to Bluebird 2-4 ✓
 STKS FOR METERS
 Hornblend. Marrell to Noyes 5 ✓
 STKS FOR METERS
 Balboa St Marrell to Noyes 6 ✓
 Group 25 Prelim
 Silvergate Pl Silvergate to Nly Term 7-9 ✓
 Group 2.5 PRELIM.
 LINWOOD ST. SAN DIEGO ST. TO ARISTA 10-12 ✓
 Group 25 Prelim
 Arista St Arista Dr. to Nly Term 13-15 ✓
 Group 25 Prelim
 Talbot St Akron to La Roy 16-18 ✓
 Group 25 Prelim
 Carleton Evergreen to Willow 19-20 ✓
 Group 25 Prelim
 Perry St San Bernardino to San Fernando St 21-23 ✓
 Group 25 Prelim
 Donahue St Quince to Yuma St 24-26 ✓
 Alice
 (Group 25 - Prelim)
 Alta Vista St - ALTA VISTA RD. TO ALTA VISTA WAY 27-28 ✓
 Alice
 Group 24
 Mallard St Blue Bird to Paradise 29-31 ✓
 Group 24
 Paradise 7550 Paradise to Mallard 32-34 ✓
 Group 26 Prelim
 Row Terrace Nutmeg to Sly Term 35-36 ✓
 Prelim Group 26
 Martin Ave 3rd to 15th West 37-38 ✓
 Prelim Group 26
 Martin Ave 3rd to Nly East of 32nd 39 ✓
 Alice
 CEDAR ST., FELTON TO GREGORY - PRELIMINARY 40-43
 Alice
 GREGORY ST., DATE ST. TO 141st SO. CEDAR ST. - PRELIM. 44-47
 OVER
 Alice

INDEX (Cont'd)

OLIPHANT ST, WILLOW to EVERGREEN, Prelim 50-52 ✓
Alice

GREGORY ST, DATE to CEDAR. 8 STEPS 6" A.G. MAIN 53 ✓

CEDAR ST, FELTON to GREGORY 8 STEPS 6" A.G. MAIN 54 ✓

Sperry St. Long Branch to Brighton, prelim 55-57 ✓

Martin Ave, Steps & Grd 6" AC. 58 ✓

BANCROFT ST. " " " " 59 ✓
Alice

33rd St
 Steel St to Webster
 check depth of existing main

149	24.15	22.66
1+29 Nly	6.64	17.51
0+79 Nly	7.00	17.15
0+58 Sly	7.39	16.76
1+09 Sly	6.97	17.18
1+59 Sly	7.07	17.08
2+11 Sly	7.31	16.84
2+62 Sly	7.60	16.55
3+86 Sly	8.19	15.96
5+02 Sly	8.73	15.42
6+19 Sly	9.58	14.57
6+49 Sly	9.93	14.22
6+78	12.1	11.8
149	22.66	= 22.66

West
 Williams X
 Varonakis
 Kullhoter

5/18/55 Fair + Warm

0+00 Nly prop line Durant St
 Top FH 33rd + Steel St 2659D

Top pipe opp FH edge pave Steel St

" "

" "

" "

" "

" "

" "

" "

" "

" "

" "

Top existing Transit pipe

Mollard St
Alcedo to Bluebird
Pelvin

7+40^E P.O.T.
7+40^L 90° to Old Hub 9.56' RT

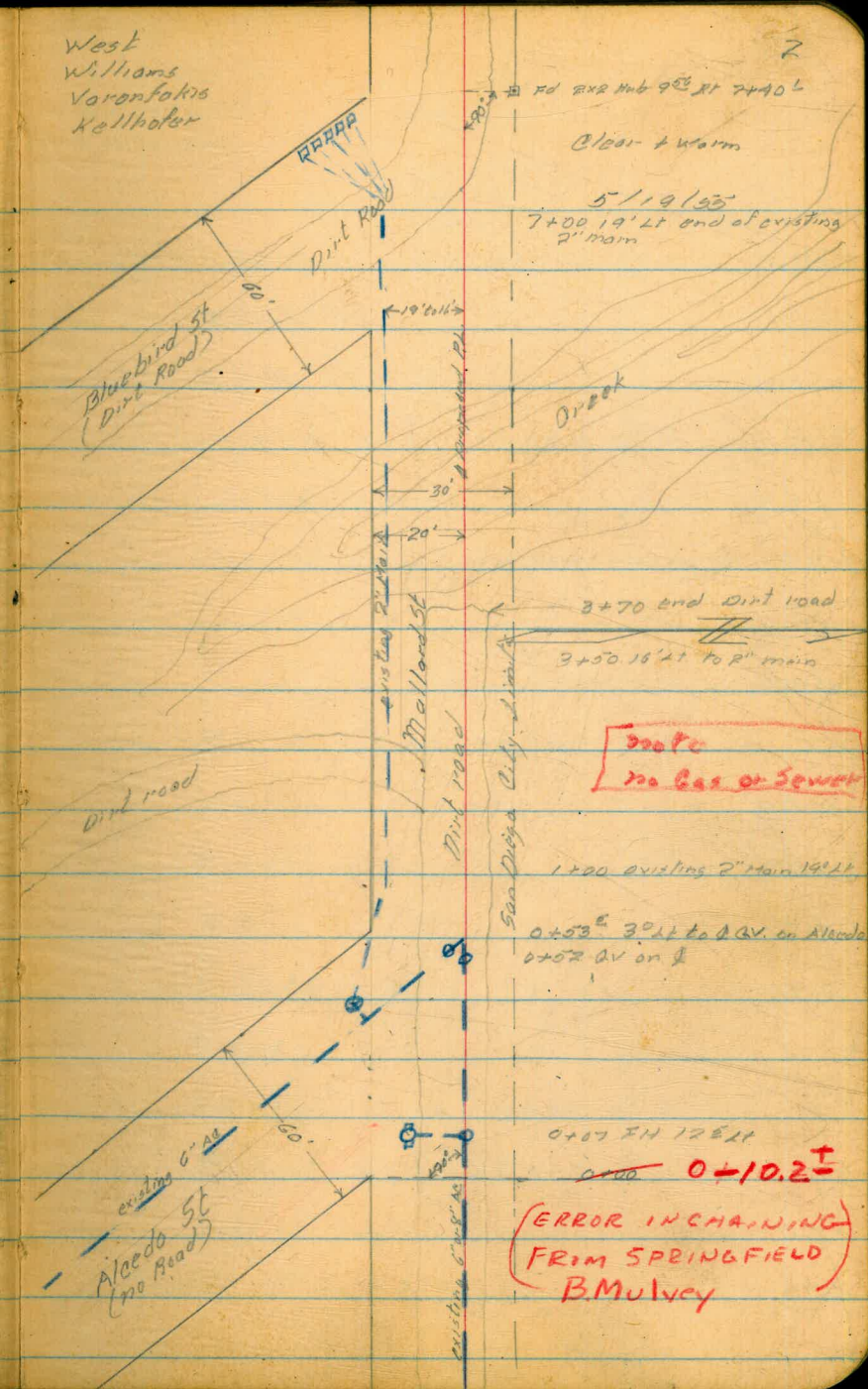
3+90 P.O.T Spike

0+00 90° to Fly Strip Line Alcedo

0-01⁵⁰ P.O.T Spike RR³ LT to PP 211166

Line produced from Springfield st
P.O.T Spike 16 North of PP 170582 Top of Hill

West
Williams
Vorontakis
Kellhofer



5/19/55
7+00 19' LT end of existing
2" main

3+70 end dirt road
3+50 16' LT top P' main

1+00 existing 2" main 19' LT

0+53^E 30' LT to 8" AV on Alcedo
0+52 AV on it

0+07 IN 12" LT

~~0+00~~ 0+10.2[±]

(ERROR IN CHAINING)
FRIM SPRINGFIELD
B. Mulvey

note
no Gas or Sewer

Mallard St
Q Profile

T.B.M.	0.92	402.76		401.84
0+07			6.49	396.27
0+00			7.9	394.9
T.P.	0.34	390.10	13.00	389.76
+50			4.4	385.7
T.P.				
1+00	0.48	377.52	13.06	377.04
+50			6.9	371.6
2+00			11.5	366.6
T.P.	0.71	365.40	12.83	364.69
+50			2.0	363.4
3+00			3.9	361.5
+50			6.1	359.3
+90			9.7	355.7
4+00			11.7	353.7
T.P.	0.65	353.20	12.85	352.55
T.P.	0.91	341.37	12.74	340.46
+50			1.6	339.8
+90			15.8	325.6

WEST
WILLIAMS X
VARONFAKIS +
KELLHOFER

3

5/19/55

27166 500 X 8 818 Page 25

TBM Nail in power pole 28' 91 0-01

Top F.H.

LT. E RT

	11.0	9.0
Top Bank	9.7	10' RT
	13.1	9.7
	10'	10'

	3.4	0.6
	10'	10'
Bottom Bank	15.3	13.6
	10.8	10'

Mallard St. Cont

341.37

5+00	16.2	325.2
+10	16.0	325.4
+50	5.8	335.6

12.57 352.75 119 340.18

6+00 6.6 346.2

9.70 361.86 0.59 352.16

+50 10.8 351.1

7+00 6.1 355.8

7+40⁺ 1.1 357.8

0.95 354.57 8.24 353.62

12.08 366.20 0.45 354.12

12.89 378.94 0.15 366.05

12.82 391.20 0.56 378.38

12.73 403.16 0.77 390.43

1.30 401.86 = 401.84

Crack Bott $\frac{15.9}{10.21}$ $\frac{16.7}{10.81}$

Bott of Bank $\frac{14.3}{10.21}$ $\frac{12.0}{10.81}$

$\frac{4.2}{10.21}$ $\frac{7.5}{10.81}$

$\frac{5.5}{10.21}$ $\frac{8.5}{10.81}$

$\frac{8.7}{10.21}$ $\frac{13.1}{10.81}$

$\frac{4.6}{10.21}$ $\frac{9.4}{10.81}$

$\frac{1.3}{10.21}$ $\frac{1.5}{6.21}$ $\frac{7.9}{10.81}$

Turn on 2x2 Hub 10'RT 7+40⁺

HORNBLEND S.T. MORRELL To NOYES

STKS. FOR METERS

Backs of meters set 23' from 2

25560

B.M.	1.90	56.05	54.15
0+21 M.S			4.1 52.0 51.6
+70 M.N.			3.8 52.3 52.4
0+99 M.S			7.3 48.8 49.7
1+05 M.N.			5.1 51.0 51.3
+50 M.S			8.6 47.5 48.5
+89 M.N			8.4 47.7 48.7
2+16 M.N.			9.0 47.1 48.4
+50 M.S			9.4 46.7 46.8
+76 M.S.			9.9 46.2 47.0
+83 M.N			8.9 47.2 48.0
3+26 M.N			9.3 46.8 47.7
+35 M.S.			9.6 46.5 46.7
+76 M.N			8.7 47.4 47.6
CHECK B.M.	1.90	56.05	= 56.05

WEST

WILLIAMS

VARONFAKIS X

KELLHOFER 9

5.

5/20/55 SUNNY + WARM

N.W.L + T. HORNBLEND + MORRELL ST
 4 0+00 Ely Prop Lion Morrell

Co	2005
Fo ¹	2004
Fo ²	2015
Fo ³	2022
Fo ⁰	
Fo ⁰	2030
Fo ³	2036
Fo ¹	
Fo ⁸	
Fo ⁸	2044
Fo ⁹	2050
Fo ²	
Fo ²	2060

Balboa St
57ks for Morrell to Noyes
for wet mets

meters set 45° from 2558 A D

0.37 54.52 54.15

(5) FH 7.3 47.2 45.8

1.57 49.73 49.36 45.14

0+90 N 54 5.4 44.3 43.4

3+67 N 1.5 45.2 45.0

4+80 N 3.9 45.8 45.3

5.21 50.49 4.45 45.28

5+30 N 14 4.6 45.9 45.4

8.03 56.37 2.15 48.34

2.22 54.15 = 54.15

West
Williams +
Varonfakis
Kellhofer +

6

5/23/55 Cloudy

Hornblend + Morrell

Wet (P) 2.5 T

0+00 Noyes St + Nly line Balboa

C1^A Alley N of Balboa Morrell by should be
Morrell 2.5 T

C0⁹ 2075 - 2067 Apt

C0² 2034

C0⁵ 2017

C0⁵ 2004 2002

SILVERGATE PLACE

± PROFILE

B.M.	1.72	384.88	383.16
T.P.	0.53	373.59	11.82 373.06
T.P.	0.62	366.07	8.14 365.45
T.P.	0.55	356.52	10.10 355.97
T.P.	6.14	350.50	12.16 344.36
T.P.	2.15	344.91	7.74 342.76
T.B.M.	1.82	342.76	3.97 340.94
0+00			5.3 337.46
+15			5.61 337.15
+40			4.98 337.78
+50			4.3 338.46
1+00			4.7 338.06
+50			5.7 337.06
2+00			7.4 335.36
+50			9.1 333.66
3+00			11.3 331.46
T.P.	1.15	331.57	12.34 330.42
+			
3+40.03			2.07 329.50
+49.71			2.56 329.01

WEST
WILLIAMS
VARONAKIS †
KELLHOFER X

8.

5/23/55 PARTLY CLOUDY

TOP CORNER MON @ Catalina + Military Gate

SILVERGATE
TOP F.H. SILVERGATE ST + PLACE

EDGE PAVE. WEST

EDGE PAVE. EAST

OIL 7.52T

6.38

OIL 9'LT

8.10

OIL 9'LT

10.21

OIL 7.52T

11.90

OIL 5'LT

SILVERGATE CONT.

9.

331.57

B.	4+00		5.41	326.16	
T.	+50		8.01	323.56	
T.	5+00		10.16	321.41	
T.	+50		12.00	319.57	
T.	+79.4		12.26	319.31	
T.	T.P.	11.59	342.86	0.30	331.27
T.	T.P.	6.22	347.16	1.92	340.94
O.	T.P.	7.28	352.39	2.05	345.11
-	T.P.	9.20	353.07	8.52	343.87
-	T.R.	12.08	364.95	0.20	352.87
-	T.P.	4.87	369.70	0.12	364.83
1-	T.P.	9.27	378.49	0.48	369.22
-	T.P.	9.54	386.77	1.26	377.23
2-	CHECK B.M.		3.61	383.16	= 383.16

SILVERGATE
TOP F.H. SILVERGATE ST PLACE

LINWOOD ST
SAN DIEGO ST TO ARISTA

2+02 ±

Ely prop line Arista

2+30 ± PT

26° 24' 30" RT

1+95 ±

P.O.T

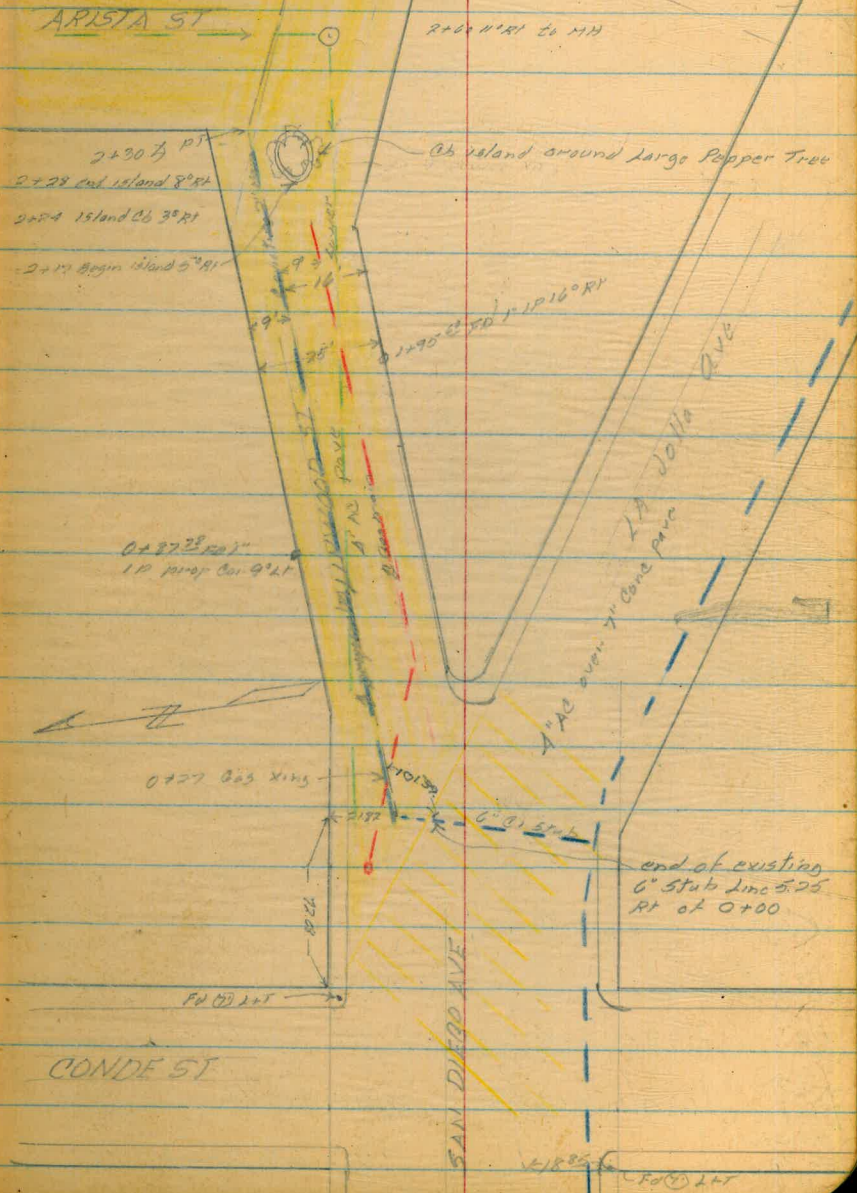
0+87 ±

P.O.T

1+99
21.92

0+00

7268 from Ely prop line Conde
21.82 South of the Nly prop line San Diego



Profile Linwood

B.M.	8.18	36.98	28.80	
	8.99	41.00	4.97	32.01
0+00			8.25	
+50			8.44	
1+00			8.13	
+29			8.02	
+50			8.84	
2+00			8.77	
+50			1.54	
3+00			0.16	
	2.53	47.58	0.95	40.05
3+29 ⁵⁶			5.09	
+50			4.83	
+78			4.22	
4+00			4.50	
+09 ⁵⁶			4.50	+5.4 To Flow Line
T.P.	2.90	37.61	12.87	34.71
T.P.	6.02	36.73	6.90	30.71
CHECK B.M.			7.93	28.80 = 28.80

Void shifted
16' North
Alignment

WEST
WILLIAMS T
VARONFAKIS T
KELLHOFER

71

5/24/55 LIGHT RAIN + COOL

SW @ 2+T Twigg + San Diego Ave

Turn on @ copper disk SW Cor Conde + San Diego

Wly prop line Conde st

Outer line San Diego

Turn on 1" IP Prop Cor. 7² RI 2+70⁵

Top fly rim sewer MH 8' LT

end of work

Lipwood St & Profile

	9.11	41.12	32.01	
0+00		10.33	30.79	
0+00		7.72	33.40	
+50		4.55	36.57	
1+00		1.80	39.32	
+50		0.20	39.92	
	9.04	49.09	1.09	40.03
2+00		6.33	42.76	
+30 ±		5.24	43.85	
+50		5.38	43.71	
			+54 to Flow Line	
+60		5.75	43.34	
+92 ±		6.05	44.04	
	1.96	38.53	12.52	36.57
		6.55	31.98	= 32.01

West
Williams
Varonakis
Alexander

12

5/25/55

See page 11

Copper Disk @ Tag SW Cor. Conde + San Diego

5.25 FT Top 6" of Stub Pipe

North rim lower 12 1/2 FT

ARISTA CT
Arista Dr. to Nly Term

Pel'm Groupe #25

West
Williams
Varonforks

13

5/26/55

[see Note]

2+31 intersection of prop line on skew

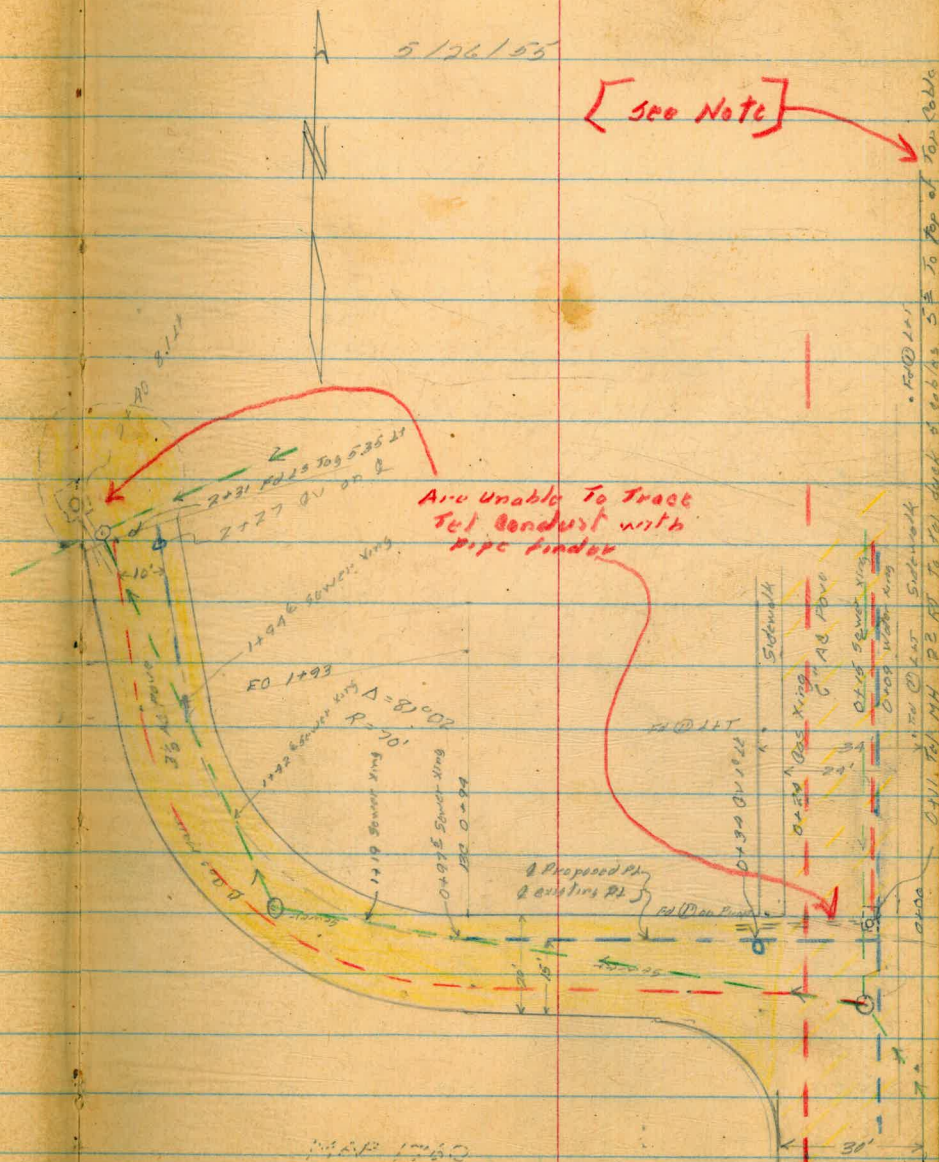
1+93 EL

$\Delta = 81^{\circ} 02'$
 $\frac{1}{2}\Delta = 40^{\circ} 31'$
 $R = 70'$
 Def per foot = 24.553'
 Def for 10' chord = 4' 05" 33"

0+94 BC BC

0+33 POT

0+00 Fly Prop Line Arista Dr



MAP 1260

Anista Ct

Q Profile

14

8.83	258.86	250.02	
0.49	259.19	0.14	258.71
1.41	248.38	12.27	246.97
0+05		6.89	41.49
			+6.8 To Flow line
0+14 ³		7.53	240.85
0+33		7.48	241.90
+50		8.63	239.75
2.52	240.59	10.31	238.07
+94.50		3.80	236.79
1+00		4.07	236.52
1+0		4.17	236.12
+20		4.82	235.77
+30		5.08	235.51
			+4.2 To Flow Line
+39		5.15	235.44
			231.31
+40		5.22	235.37
+50		5.40	235.17
+60		5.90	235.19
+70		5.44	235.15
+90		5.50	235.09

Reduced by datum 113.31

BM NE BP Hickory + Ampudia

Center Line Fly Side Anista Dr

Top Nly Rim Sewer MH 17° Lt

Top Fly Rim Sewer MH 6° Lt

240.59

1+90 5.46 235.13

+93 EC 5.51 235.08

2+00 5.53 235.06

+31 6.23 234.36

+32 5.99 234.65

0.78 240.74 0.63 239.96

1287 246.75 4.86 233.88

6.84 252.81 0.78 245.97

2.79 250.02 = 250.02

Reduced by polemic 10/10/55

+5.6 to Flow Jan 238.76

Top Ely from sewer MH 10⁶ J1

Top FH Hickory + Arista

Talbot St
Akron to Le Roy
& Profile

+74	216.83		216.09
0.52	209.44	12.91	202.92
0.26	191.99	12.71	191.73
0.76	179.86	12.89	179.10
0.78	168.44	12.20	167.66
0.67	156.64	12.97	155.97
0.59	144.61	12.68	144.02
0.19	132.24	12.51	132.10
0.53	120.23	12.09	119.70
0.47	109.69	11.01	109.22
0+00		4.27	105.4
0+01 ²		5.49	104.2
0+30		7.45	102.2
1+00		10.37	99.3
0.29	97.08	12.90	96.79
+50		0.78	96.3
2+00		3.61	93.5
+50		6.50	90.6
+55		6.48	90.6

Reduced by A.E. Matison 11-29-55

N.W. CP Talbot & Concord

Top FH Talbot & Bogt Dr.

Top FH 0-07

Top Corp dock end existing main

5' ft edge AS part

6' 8" " " " "

7' 3" ft edge AS part

Top South rim sewer 19' ft

97.08

3+00 9.21 87.9 8° RT edge AC pave

+50 12.00 85.1

0.64 86.23 12.49 84.59

4+20 2.90 82.3 9° RT edge AC pave

+50 5.86 79.3

5+00 9.05 76.1 76.18 12° RT edge AC pave

+50 12.40 72.8

0.92 73.95 12.20 73.03

+83.72 3.30 ~~71.74~~ 70.65 ^{After}

Ely prop line LaRoy St

0.79 63.44 11.30 42.65

11.25 52.19 = 51.77

NW AC Talbot & Evergreen

BARLETON ST

Evergreen to Willow
Palms #25

3+70²⁵

Wly prop line Willow

3+10²⁵

POT

0+00 = 0+70 on Dwng

0+00 POT

Wetty prop line evergreen

West

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

W

19

12/14/55
Bull's Eye

12/14/55

0-30 Wot
Met 21
31-46

Dine Pawa

0-30 Wot Met
31-45

0-25 FH
9' RT
8' RT

0+00

70'

Evergreen

0+00 is shown
on Wly Line
of Evergreen
in Book

0+00 = 0+70
on Dwng

Barleton St
Proposed Pk

0+00 6.78

0-50 7.40

0-50 0.62 lower

Than 0+00

Barleton St

CARLETON ST

Evergreen to Willow
POT #25

3+70²⁵

Wly prop line Willow

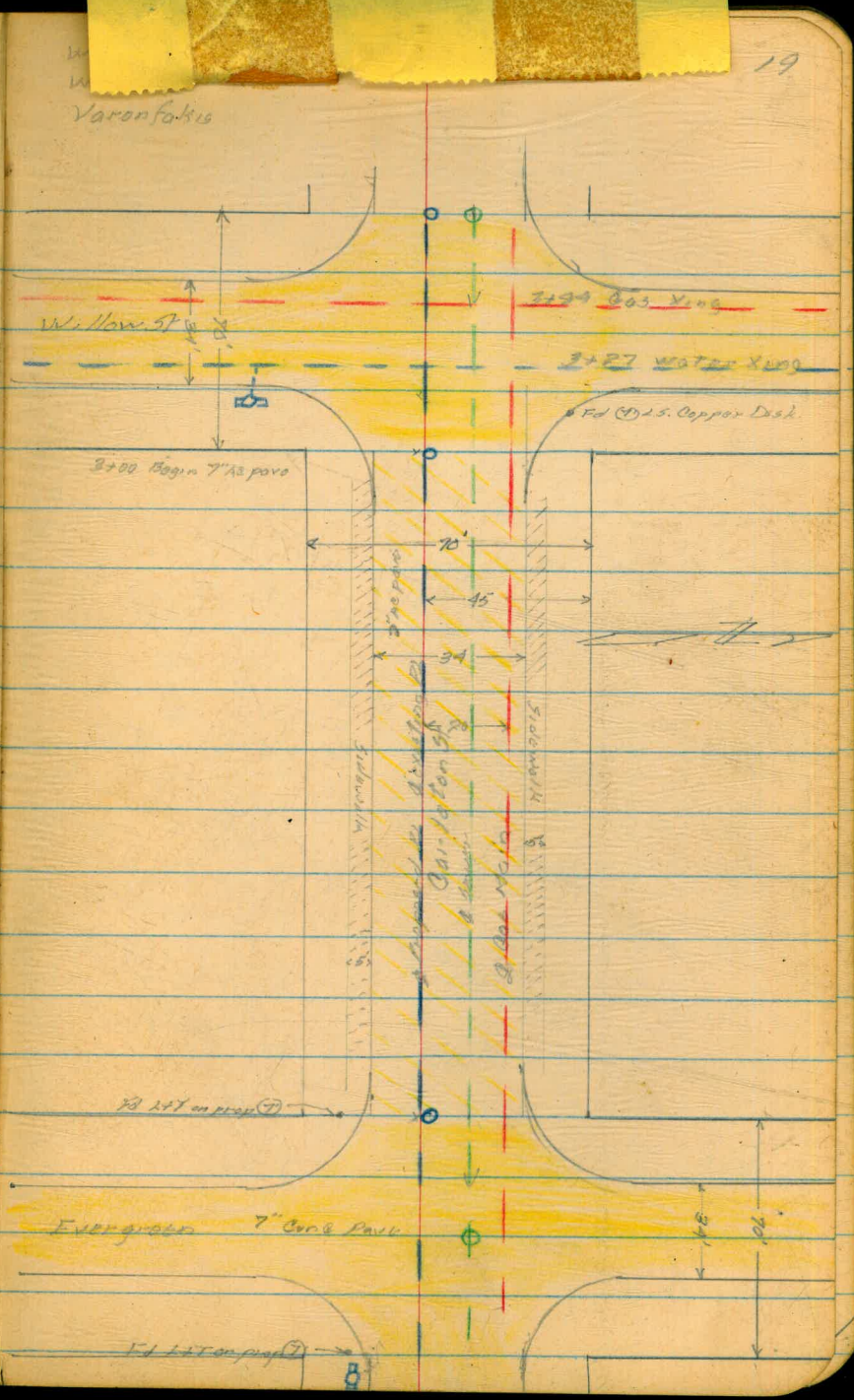
3+10²⁵

POT

0+00 = 0+70 on Dwng

0+00 POT

Woolly prop line evergreen



Cartleton

Profile

	0.65	25.76		25.11
	9.94	30.61	5.09	20.67
0-35			5.65	
0+00			4.56	26.05
	13.75	43.26	0.10	30.51
0+50			8.29	34.99
	12.96	55.46	0.76	42.50
1+00			10.74	44.72
+50	12.81	67.49	0.78	54.68
2+00			2.83	64.66
	12.69	79.89	0.29	67.20
+50			5.29	74.60
	9.79	89.57	0.11	79.78
3+00			5.95	83.62
+50			4.28	85.29
+69			3.76	
+70 ^{25'}			3.66	85.91
			3.20	86.37 = 86.40

West
Williams
Varonfakis

20

5/31/55

sw @ top Dick Fenelon + Evergreen

Top west rim sewer MH 10' RL

West prop line Evergreen

AV 05' RL

Top south rim sewer MH 10' RL

AV on E Willy prop line Willow

BM BP SW Cor Cartleton + Willow

Perry St & Profile

West
Williams
Vorontakis

22

BM

Top FH Ovaltrough + San Elijo

0.23 160.25 160.02

11.63 165.89 5.99 154.26

12.17 174.46 3.60 162.29

12.48 186.77 0.17 174.29

12.54 199.18 0.13 186.64

10.57 209.56 0.19 198.99

0+05 3.25 206.31

+06 4.0 205.56

+12⁵ 3.71 205.85

+30² 3.72 205.84

+50 4.49 205.07

+91 8.27 201.29

0.64 208.17 2.03 207.53

1+00 6.7 201.47

+25¹³ 6.5 201.67

+32 7.9 200.27

1.07 197.27 11.97 196.20

+50 1.8 195.47

+57 2.4 194.87

Redwood on Palomares 10-18-55

Top ch whj side San Geronimo

Bottom " "

Top slj Rim Service MH 10⁵ 14

edge core pave begin AC pave

end AC pave

Top FH San Geronimo + Perry St

7.70 5.1 5.6
8'4" edge AC pave 0" RT 10' RT

10² 7.5 6.9
9'4" edge AC 4' RT 10' RT

2.4 1.5
12'4" edge AC pave 10' RT

197.27

1+72 10.1 187.17

2+00 11.2 186.07

0.42 185.02 12.67 184.60

2+50 6.7 178.32

+68 10.1 174.92

+91 ^{Top of cut} 8.4 176.62

0.42 173.19 12.25 172.77

2+95 5.7 167.49

3+00 7.1 166.09

+50 10.7 162.49

+56 12.55 160.64

+68 11.83 161.36

2 90⁷⁸ 12.0 161.19

7.99 168.53 12.15 161.04

1.56 158.08 12.01 156.52

8.82 161.44 5.46 152.62

1.42 160.02 = 160.02

Reduced by performance

10-12-55

Begin ornamental barbs

4.4
12.2L

8.2
12L

12.0
10.5RT

(edge AC pave)
9.2L

7.1
6.2L

15.4
7.5RT

20.6
12.5RT

4.0
10.2L

9.9
8.5RT

11.7
10.5RT

7.5
10.4L

11.8
10.5RT

9.4
10.2L

9.0
8.5RT

13.5
13.5RT

0.0
11.2L

5.5
4.2L

6.5
8.5RT

5.6
10.5RT

Top North rim sewer MH 18² RT

end AC pave

Allen #2 913

Turn on pipe pipe 15² RT 3+80²

Donahue St

Gaines To Yuma St

Proposed Pl. & Profile
Group #25

0.34	87.96		87.62
0.53	75.79	12.70	75.26
0.36	63.26	12.89	62.90
0.41	51.39	12.48	60.78
0.43	39.03	12.79	38.60
0+00		10.4	28.06
+10		4.8	
+16		4.87	34.16
+25		4.87	
+33		5.14	
+40		4.7	
+53		12.3	
0.74	27.36	12.41	24.62
1+00		6.4	
1.50		8.6	
2+00		10.1	
0.52	16.48	11.40	15.96
+50		0.5	

See page 26 for cont

West
Williams
Varonakis

24

6/21/65
See FB 819 page "

IRM Top 3/4 IP prep Cor NE Cor Fureka Bldg

Nil prep line bases

Top road fill

edge AC pave

Roofing Nail

edge AC pave

Top road fill

11.5
10.1

12.3
10.1

3+75²⁵ POT

Rd Const Mon
 On prop line
 SW Cor
 Furuta + Yuma

Row of Large Eye Trees

3+77 24" Eye Trees
 00 R

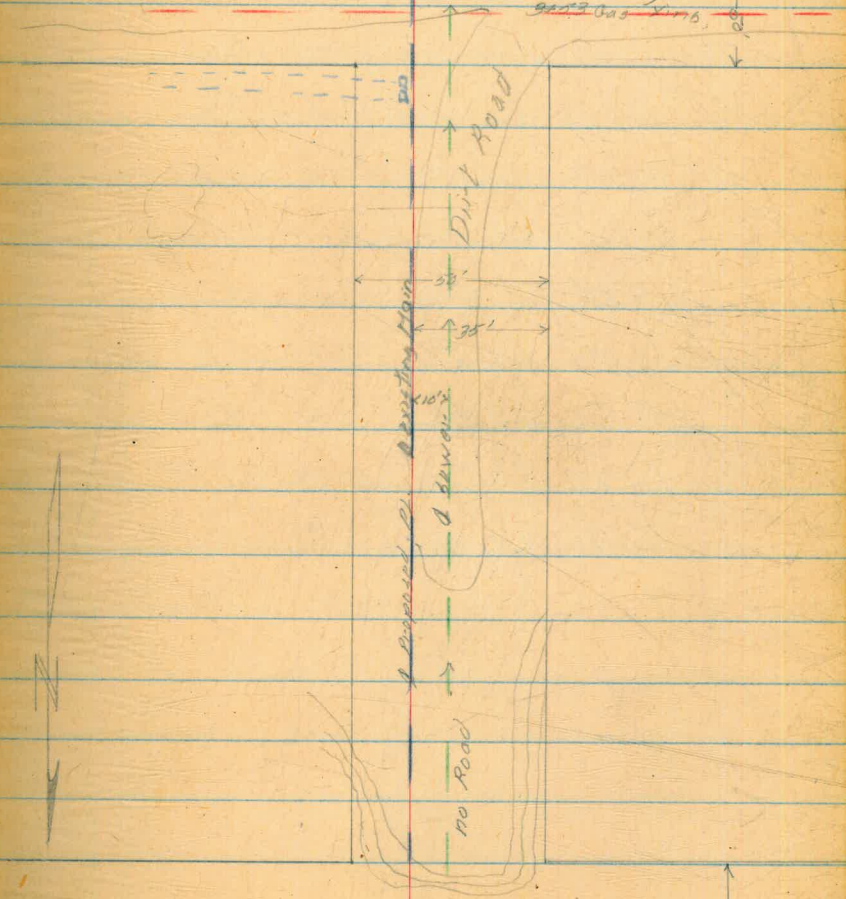
3+88 Water Main

Rd Const Mon on prop line

3+69 Sewer MHT 15"

Yuma St

9000 Gas Line



0+25 POT Nail

0+00

Nly prop line Goines

One pave
 0 1/2 in nail
 in 2 Goines
 Furuta

Goines St

No Road

Dorahue St Cont.
From page 2A

16.48

3+00

2.6

+50

5.5

+69

6.42 10.06

4+00[±] ±

6.8

11.89 27.93 0.44 16.04

12.47 39.79 0.61 27.32

8.28 47.44 0.63 39.16

11.95 58.67 0.72 46.72

9.82 67.98 0.51 58.16

12.74 80.39 0.33 67.65

10.98 90.77 0.60 79.79

3.12 87.65 = 97.62

16.48
6.42
10.06

6/2/55

Top Fly line Sewer MH 10' RL
Fly prop line yuma

ALTA VISTA ST.

ALTA VISTA RD. TO ALTA VISTA WAY
& PROFILE PROPOSED 6" MAIN

6+20⁰⁰ = NORTHLINE ALTA VISTA WAY SET SPIKE

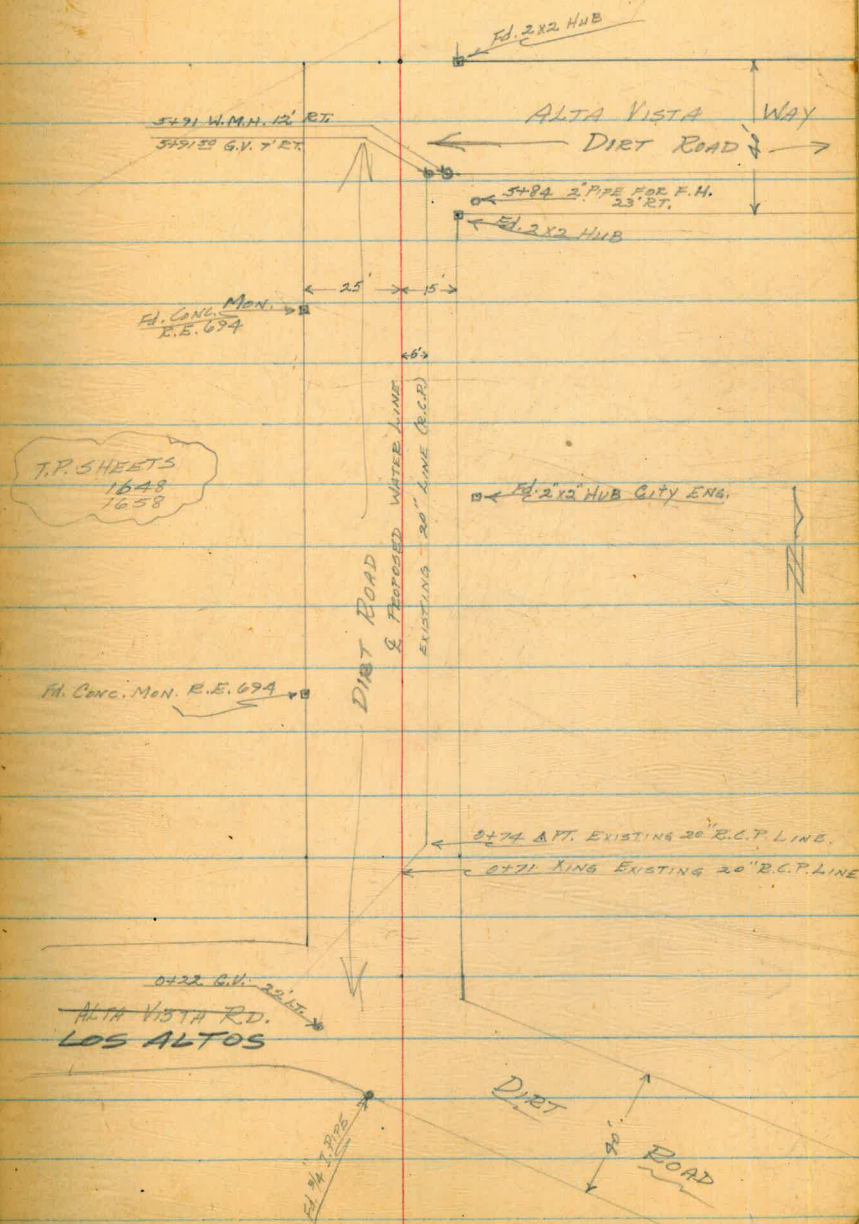
5+80⁰⁰ = So. LINE ALTA VISTA WAY

3+60⁰⁰ = Hd. 2x2 HUB City Eng. 20' RT

2+30⁰⁰ P.O.T. SET SPIKE

0+00 = So. LINE ALTA VISTA RD.

7/5/55
SHOREY
ALEXANDER
KELLHOFER
HOLAHAN



T.P. SHEETS
1648
1658

Hd. Conc. Man. R.E. 674

0+22 G.V. 22' 55" RT
ALTA VISTA RD.
LOS ALTOS

DIET ROAD
20'

ALTA VISTA ST.
(CONT'D)

7/5/55
SHOREY
ALEXANDER
KELLHOFFER
HOLAHAN

TBM	9.51	303.23 103.23	293.72	
0+00			8.5 294.7	
0+10			11.1 292.1	
0+32			10.4 292.8	
0+50			10.7 292.5	
0+71			2.8 293.4	
1+00			8.8 294.4	
1+50			6.6 296.6	
2+00			4.0 299.2	
2+50		301.7	1.5 301.7	
TP	13.22	316.27 146.27	0.18 303.05	
3+00			11.5 304.8 104.8	
3+50			6.2 308.1 108.1	
4+00			311.7 4.6 411.7	
4+50		315.2	1.1 415.2	
TP	6.66	322.77 122.77	0.16 44.71 316.11	
5+00			5.5 317.3 117.3	
5+50			5.4 317.4 117.4	
5+90			5.77 317.0 117.0	
6+00			6.0 316.8 116.8	
6+30			6.1 316.7 116.7	
7BM	3.50	121.09 321.09	5.58 44.75 317.19	
	0.36	44.96 308.96	12.49 44.80 308.60	
	2.21	298.79	12.38 44.58 296.58	
CK TBM			5.10 293.69 = 293.72	

Reduced by A. Morrison 9-23-55

CURT REM 9-23-55

3/4" IRON PIPE S/LINE ALTA VISTA RD. & ALTA VISTA ST.

Edge dirt road

NOTE: Corrected elevation of 3/4" I.P.
S/LINE ALTA VISTA RD (LOS ALTOS RD)
AND ALTA VISTA ST. 293.72'
REM 9-23-55

E. Edge W.M.H.

TEMPYR. HUB. S.E. COR. ALTA VISTA ST. & ALTA VISTA WAY

Mallard St Profile

12.50	366.12		353.62
7+50		3.0	358.12
8+00		4.0	362.12
+50		1.9	364.22
9+00	0.49	366.28	0.33 365.79
+50		1.8	364.48
10+00		4.4	361.88
+50		8.2	358.08
11+00		11.3	355.0
	0.16	353.39	13.05 353.23
+50		1.1	352.3
12+00		4.3	349.1

Turn on 2x2 Hub See Page 4

$\frac{5.1}{10.21}$ $\frac{10.9}{10.81}$

$\frac{4.3}{10.21}$ $\frac{8.9}{10.81}$

$\frac{1.9}{10.21}$ $\frac{1.9}{3.81}$ $\frac{5.9}{10.81}$

$\frac{0.4}{10.21}$ $\frac{0.4}{2.81}$ $\frac{5.0}{10.81}$

$\frac{1.7}{10.21}$ $\frac{2.1}{2.81}$ $\frac{4.1}{6.81}$ $\frac{4.5}{10.81}$

$\frac{4.3}{10.21}$ $\frac{4.4}{5.81}$ $\frac{6.3}{10.81}$

$\frac{8.0}{10.21}$ $\frac{8.0}{4.81}$ $\frac{8.2}{10.81}$

mollard St Cont

353.39

12+50	6.8	346.6
13+00	8.5	341.9
+50	10.3	343.1
14+00	11.8	341.6
+35 ¹²	13.0	340.4

9.13 349.68 12.84 240.55

10.66 339.02 =

338.37 Mon Feb 1859 Page 60

0.65 high

PARADISE

7+50 to MALLARD

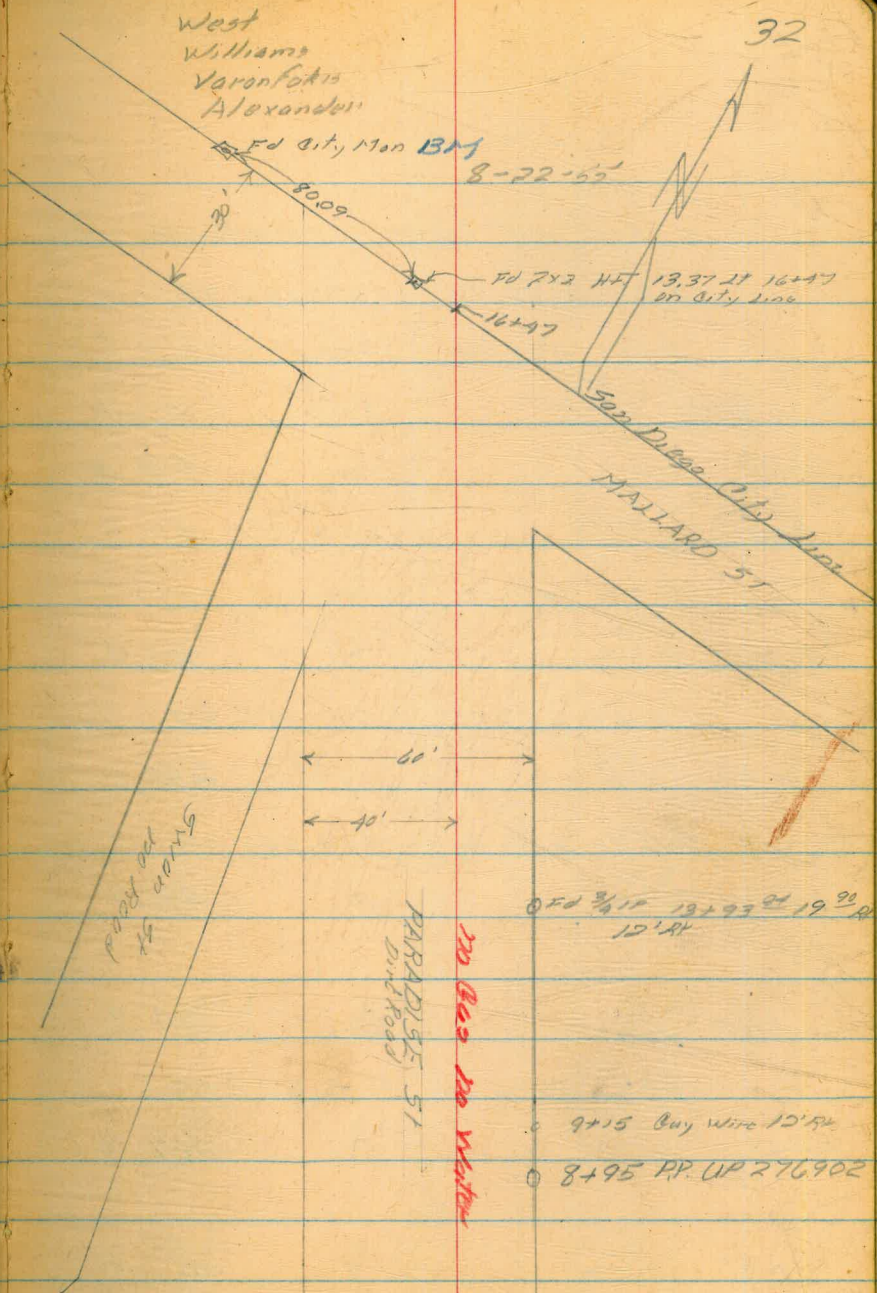
Group 24 Palms

16+99

San Diego City Line

10+50 POT

7+50 POT cont from FB 905 P68



Paradise Q Profile

33

0.62	448.26		447.64
1.32	436.71	12.87	435.39
0.39	424.30	12.79	423.92
9+00		4.0	420.3
+13		5.5	418.8
+50		13.0	411.3
0.05	411.40	12.95	411.35
10+00		9.4	402.0
0.48	399.32	12.56	398.84
+50		11.3	388.0
0.07	386.30	13.09	386.23
11+00		5.1	381.2
+50		12.6	373.7
0.08	373.12	13.26	373.04
12+00		5.6	367.5
+50		11.3	361.8
0.40	360.47	13.05	360.07

3/4 IP RT 913 40' LT

52 12 305 Page 72

1100

Q

$\frac{5.9}{10' LT}$	$\frac{3.9}{3' RT}$	$\frac{1.7}{10' RT}$
$\frac{15.0}{10' LT}$	$\frac{12.6}{3' RT}$	$\frac{12.4}{10' RT}$
$\frac{14.6}{10' LT}$	$\frac{6.8}{10' RT}$	
$\frac{14.0}{10' LT}$	$\frac{8.4}{10' RT}$	
$\frac{8.1}{10' LT}$	$\frac{5.5}{3' LT}$	$\frac{4.3}{10' RT}$
$\frac{14.9}{10' LT}$	$\frac{10.6}{6' LT}$	$\frac{12.2}{10' RT}$
$\frac{7.8}{10' LT}$	$\frac{6.1}{6' LT}$	$\frac{5.5}{10' RT}$
$\frac{12.8}{10' LT}$	$\frac{11.1}{6.5' LT}$	$\frac{11.2}{10' RT}$

Paradise Cont.

360.47

8-23-55

13+00

4.2

356.3

$\frac{5.7}{10}$

$\frac{4.7}{9.0}$

$\frac{4.1}{10.0}$

13+50

9.0

351.5

$\frac{10.1}{10}$

$\frac{9.3}{9.2}$

$\frac{9.0}{10.0}$

14+00

12.9

347.6

$\frac{14.0}{10.2}$

$\frac{13.3}{8.2}$

$\frac{12.6}{10.0}$

0.51 347.64 13.34 ~~347.13~~

+50

2.9

344.7

$\frac{3.3}{10.2}$

$\frac{2.8}{10.0}$

15+00

4.9

342.7

$\frac{5.5}{10.2}$

$\frac{4.5}{10.0}$

+50

5.5

342.1

$\frac{5.6}{10.2}$

$\frac{5.4}{10.0}$

16+00

5.5

342.1

+49

5.5

342.1

Nly Line Mallard St City Body

9.05 338.59 =

338.37

Mon FB 1859 Page 60

KEW TERRACE
NUTMEG TO SOUTH TERM
Pelin Group 27

West
Williams
Varonakis
Alexander

35

9-23-55

2+12

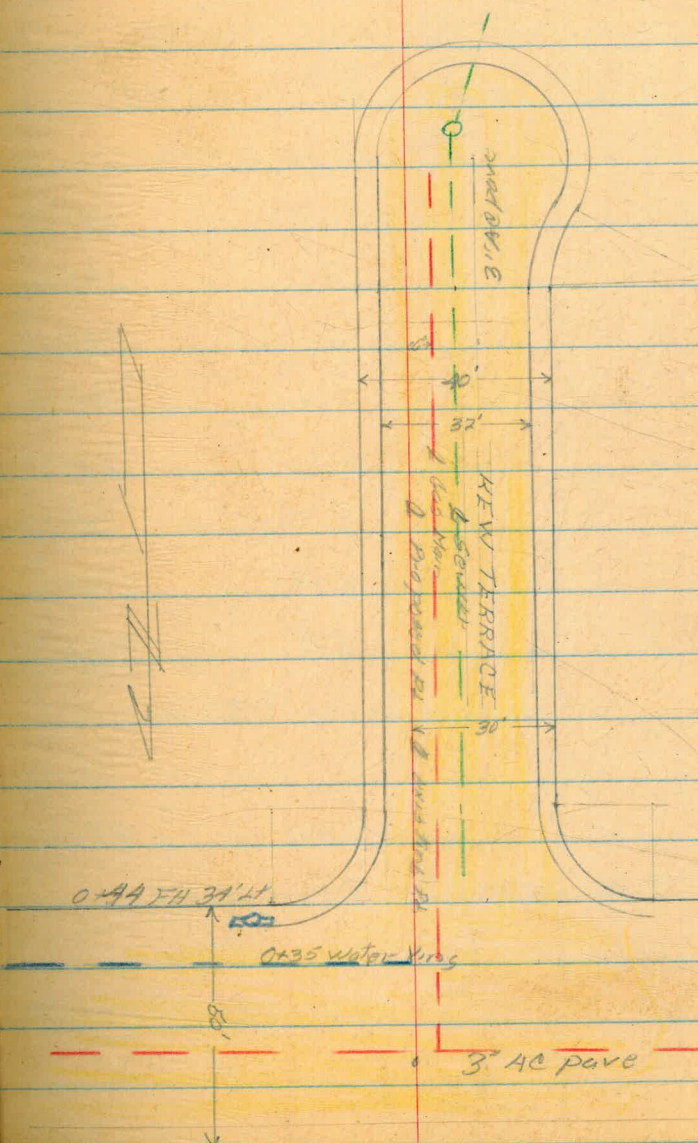
edge of cb

0+25

POT

0+00

N/y prop line Nutmeg



Kew Terrace
Q profile

Red'd
by Rocky

36

7.16 302.78 295.12

SE BP Maple + Boundary

0.31 296.40 619 296.09

5.95 291.35 11.00 285.40

0+00 1.8 289.6

Nly prop Line Nutmeg

+09 2.4 289.0

+11 4.0 287.4

+14 5.3 286.1

+25 5.3 286.1

+50 5.70 285.7

+100 6.99 284.4

+50 8.35 283.0

+89 9.41 281.9
+6.0 To Flow Line

Top Ely Kim Sewer MH

2+00 10.07 281.3

+12 10.69 280.7

edge ab to banjo

9.31 291.25 9.41 281.94

Turn on Ely Kim Sewer MH

11.67 302.83 0.09 291.16

7.78 295.05 = 295.12

MARTIN AVE 32nd St to 130' West
Pelin Group 26

West
Williams
Varonakis
Alexander

37

8-24-55



2+00±

End of Work

1+86 end of 2'
Main 15' LT

Existing Man
& proposed PL

Martin Ave
21+6 St

00'

20'

45'

FLIGHT

40'

FLIGHT

0+40 Gas Vintg

7" AC pipe

0+20 Water Xing

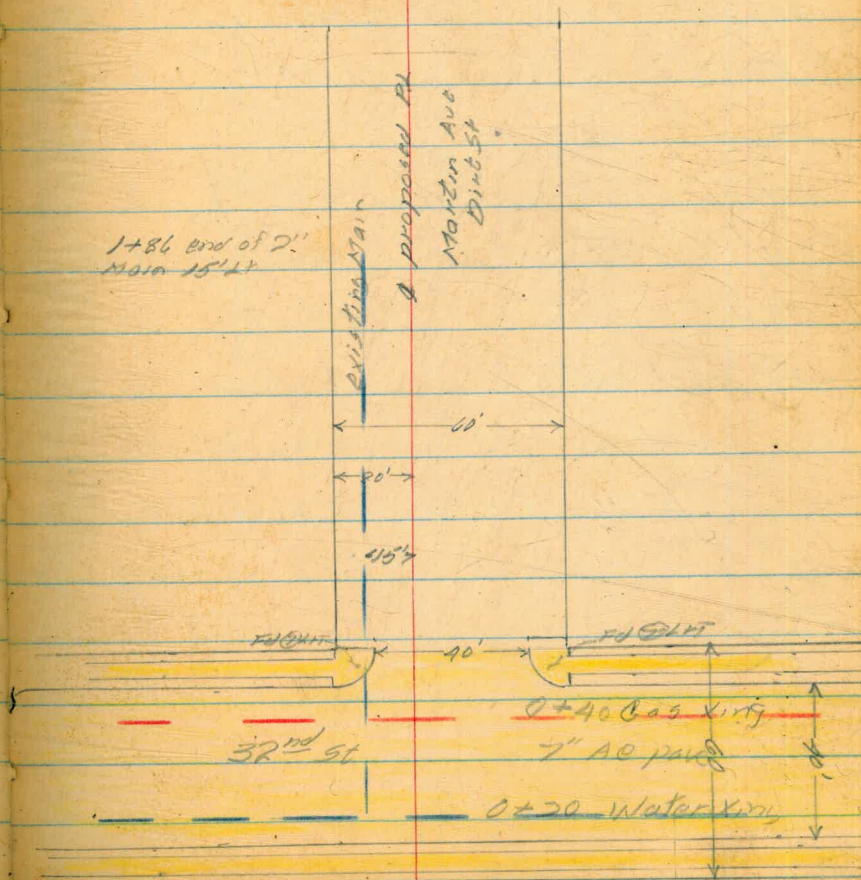
0+53

DOT

32nd St

0+00

Fly prop line 32nd St



Martin St
32nd St West
Q Profile

0.62	61.02		60.40
0.90	48.79	12.63	48.39
5.62	46.65	7.76	41.03
0+10		9.10	37.55
+10		9.59	37.06
0+30		9.15	37.5
+50		9.15	37.5
+60		7.6	39.1
1+00		5.2	41.5
+50		5.2	41.5
2+00		6.7	40.0
12.66	58.87	0.44	46.21
5.01	41.72	2.16	56.71
		1.32	60.40 = 60.40

Reduced by J. Gray
82 255.55

SW Top FH Oceanview +32

Turn Top FH SW Cor Martin +32nd

Top of Fly Side 32nd St

bottom of Eb

Q St

$\frac{6.9}{10' RT}$

$\frac{8.3}{5' RT}$ $\frac{8.2}{10' RT}$

$\frac{5.5}{10' RT}$

$\frac{4.8}{10' RT}$

$\frac{5.9}{10' RT}$

$\frac{4.5}{10' RT}$

$\frac{7.2}{10' RT}$

$\frac{6.7}{10' RT}$

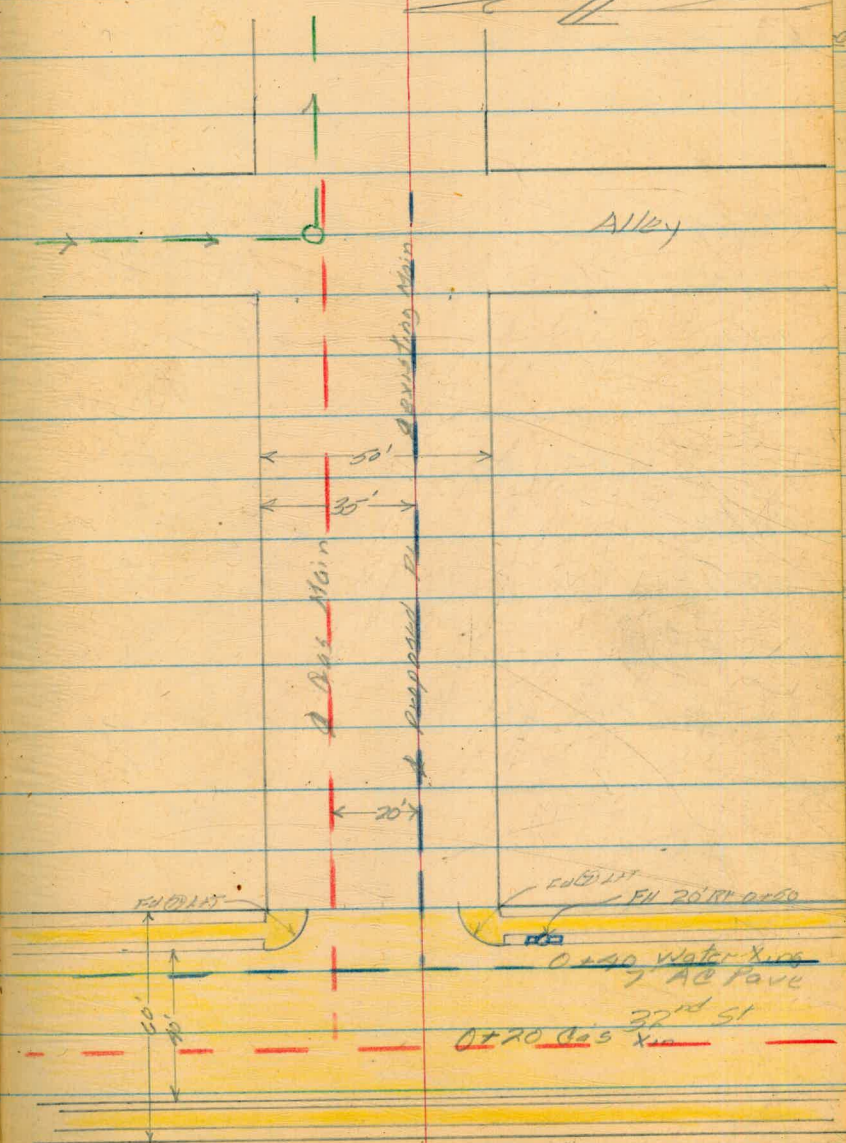
MARTIN ST 32nd ST
to Alley East of 32nd

Palin Group 26

West
Williams
Varonfakis
Alexander

39

9-24-55



0+59 POT

0+00 Wly prop line 32nd St

	0.71	41.79		41.03
0+10			1.78	39.96
0+10			2.29	39.45
0+30			2.26	39.18
0+50			3.28	39.16
1+00			7.2	39.54
+50			12.4	29.34
	6.84	35.78	12.80	29.94
2+00			11.6	24.18
+10			12.58	
2+21 ⁺			13.3	22.18
	6.64	41.41	1.01	34.77
			0.37	41.04 = 41.03

Reduced by J. Gray
8-25-53

TRM Top FH SE Cor-Martin + 32nd

Top Ob W/Ly Line 32nd

Bottom Ob

Q SK 100'

end of AC pave

19' 1" Q Sewer MII Top South

CEDAR ST.
 FELTON TO GREGORY
 (PRELIMINARY)

0+00 = W/L FELTON ST.

H50 45° LT
 to 20' S/N DL
 then 45° RT
 to proposed
 w.l. on Gregory

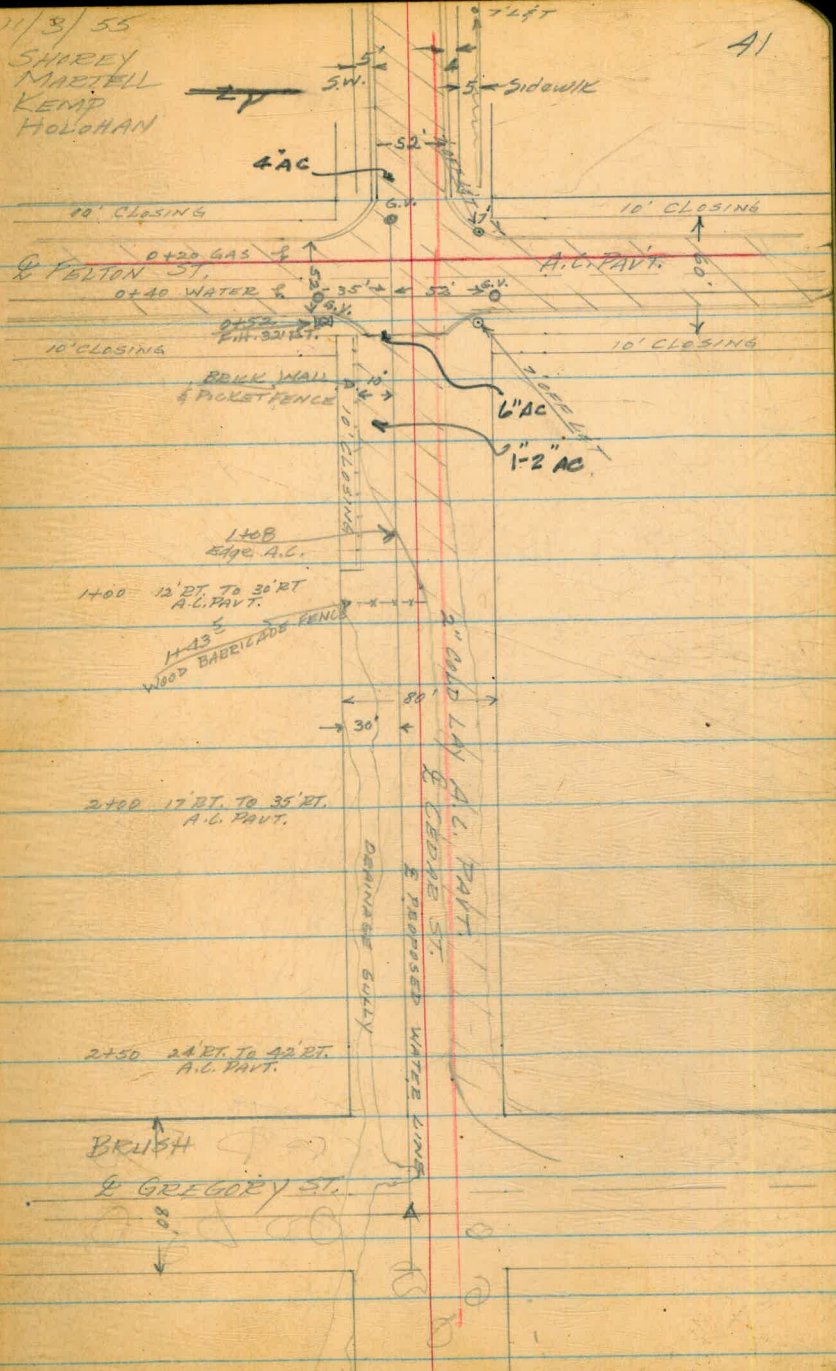
NOTE: SEE PAGES 48 & 49
 FOR REVISED LOCATION & PROFILE

2+69⁷⁰ W/L GREGORY ST.

3+19⁷⁰ P.I. PROPOSED WATER LINE ON GREGORY ST.
 3+19⁷⁰ = 4+30⁷⁰ GREGORY ST.

11/8/55
 SHIRLEY
 MARTELL
 KEMP
 HOLLOHAN

A1



CEDAR ST.
FELTON TO GREGORY
(PRELIMINARY)

BM	11.03	242.50	231.47
TP	0.74	236.26	7.18 235.32
TP	0.51	224.03	12.74 223.52
SET TBM	1.42	222.47	2.98 221.05
0+00	TOP G.H. CAP	3.1	219.37
0+20		3.3	219.17
0+30 ^E	SEW. KING	3.4	219.07
	SEW. M.H. S&P.M	2.93	219.54
0+40		3.6	219.87
0+50		3.7	219.77
0+60		4.0	218.47
1+00		5.7	216.77
1+08	Edge A.C. PANT	5.9	216.57
1+50		8.8	213.67
1+51		9.8	212.67
1+78		12.1	210.37
TP	0.10	210.31	12.26 210.21
1+88		8.80	209.51
2+00		8.4	201.91

Produced By Preliminary 12-5-55

11/3/55
SHOREY
MARTELL
KEMP
HOLLOMAN

NEBR. CEDAR & 32nd ST.

LT RT

7' OFF LET N.W. COR. FELTON & CEDAR

0+30^E SEW. M.H.

10.1 9.9
12 Edge A.C. * 8.2

13.5 13.0
15 Edge A.C. * 11.0

5.0 4.6
11 Edge A.C. * 11.1

CEDAR ST.
(CONT'D)

	216.31			
TP	0.49	198.04	12.76	197.55
2+50			7.1	190.94
TP	0.14	186.21	11.97	186.07
2+96			2.4	183.81
2+96 ⁵			2.8	176.41
3+05			11.3	174.91
3+06			3.7	182.51
3+19 ⁷⁰ = 4+30 ⁹² GREGORY ST.			2.4	183.81
3+41			4.3	181.91
3+47 ⁷⁰ = EL GREGORY			8.6	177.61
SET TBM	12.78	196.58	2.41	183.80
TP	12.18	208.70	6.06	196.52
TP	12.63	221.06	0.27	208.43
CK. TBM			0.01	221.05 = 221.05

Reduced by Potomina 12-5-55

LT

RT

+2.2
24
EDGEM.
+2.0
20
2.0
10

11.0
10

+0.5
10

5.9
10

7.7
10

12.0
3 8.2
10

P.L. HUB. 3+19⁷⁰ = 4+30⁹² GREGORY ST

1' OFF L&T N.W. COR. FELTON & CEDAR

GREGORY ST.
DATE ST. TO 100' SO. CEDAR ST.
PRELIMINARY

11-14-55
SHOREY
MARTEL
KEMP

49

0+00 = N/L DATE ST.

DATE ST.
4" 2" X 2" CITY ENG.
0+53 23' ET.

BRUSH
NO ROAD

0+66 3' HIGH BARRICADE
0+75 BEGIN A.C. PAVT

Z
↑

2+25 3' LT. CONC. BLOCK
RETAINING WALL

MAIL BOX 2+84. 05 ET.

3+87 WOOD FENCE 05 EX TO 16 ET.

4+30²² P.I. PROPOSED WATER LINE CEDAR ST.
4+30²² = 3+19⁷⁰ CEDAR ST.

4+60²² S/L CEDAR ST.

9" CEDAR ST.
9" PROPOSED WATER
DRAINAGE GULLY
SEW. M.H.
4+68 10' ET.

EMPTY 16" PIPE
USED TO PROTECT SEWER LINE
FROM EROSION! SEWER LINE
LAYS BARE UNDER THE PIPE

8" CASING
5+62 2" WHEEL VALVE

6" CASING 62' RISE TO

GAS

GREGORY ST.
DATE TO 100' SO. OF CEDAR ST.
(CONT'D)

TBM	12.20	196.00	183.80
TP	12.13	207.00	113 194.87
TP	12.90	219.37	0.53 206.47
TP	5.20	224.46	0.11 219.26
SET TBM	5.24	221.04	8.66 215.20
0+00			2.7 199.3
0+25			2.1 211.9
0+50			5.3 215.7
0+66			1.2 219.8
TP	3.14	224.16	0.02 221.02
0+75	Edge of Cold Lay PAVT.		3.0 221.16
1+00			1.3 222.8
1+30			0.3 223.8
1+50			1.3 222.8
2+00			7.6 216.5
TP	0.46	212.25	12.37 211.29
2+50	Edge PAVT		2.4 209.8
2+75			5.1 207.1
2+88			5.7 206.5
3+00			7.4 204.8

Reduced by Palomina 11-12-55

45

LT

RT

P.L. HUB 4+30²² = 3+19²² CEDAR ST PG. 43

2" X 2" HUB 0+59 23' RT.

2.1
10

22.4
10

5.7
10

5.1
10

3' HIGH WOOD BARRICADE

1.8
1.6
Edge PAVT

1.8
1.8
Edge PAVT.

1.4
8.5
Edge PAVT.

1.6
10
1.6
Edge PAVT

7.8
7.7
Edge PAVT

7.8
17
Edge PAVT

3.3
10

2.5
21
Edge PAVT

11.2
10 7.7
4

7.5
7
Edge PAVT 8.0
27
Edge PAVT

GREGORY ST.
(CONT'D)

212.25

3+09			22	203.0
TP	1.46	201.42	12.29	199.96
3+50			9.0	192.4
3+56			10.9	190.5
4+00			12.0	189.4
4+19			14.4	187.0
TP	0.25	188.46	13.21	188.21
4+30 ²² = 3+19 ⁷⁰		CEDAR ST.	4.6	183.8
4+50			11.3	177.1
TP	0.28	175.74	13.00	175.46
		SEW. M.H. F. RIM	6.24	169.50
			13.65	162.09
4+64			5.2	170.5
4+76			7.1	166.6
4+80			13.2	162.5
4+83			13.2	162.5
4+86			8.9	166.8
4+94			5.4	170.3
5+00			3.0	172.7

Reduced by Palomares 1416.65

LT

RT

46

15.0
10

10.8
5

8.6
Edge PAWT

9.3
29 Edge PAWT

14.3
10

2.3
10

0.7
12

6.5
17

1.2
19.5

1.8
37.2

1.8
37.2

15.8
10

7.4
10

11.8
10

12.6
10

SEW. M.H. 4+68 10' RT

H " " "

4.5
10

0.9
8

2.2
10

GREGORY ST.
(CONT'D)

		175.74		
TP	12.34	187.84	0.24	175.50
5425			2.2	178.6
TP	7.29	195.00	0.13	187.71
5445			2.3	185.7
5450				
5461	GRD. @ 2" RISER PIPE	(6" CASING)	3.1	191.9
5462	GRD. 2" WHEEL VALVE	(8" CASING)	3.1	191.9
OK. TBM			1117	183.83 = 183.80

Reduced by Polymine 11/16.85

LT

RT

10.9
10

6.5
9

7.0
10

8.3
10

4.2
10

P.I. HUB 4+30²³

CEDAR ST.
 FELTON ST. TO GREGORY
 REVISED LOCATION OF PRELIMINARY
 (SEE PAGES 41-43)

0+00 = W/L FELTON ST.

0+60 = E/W FELTON ST.

(SEE PAGES 41-43)

1+50 Δ 45° LT.

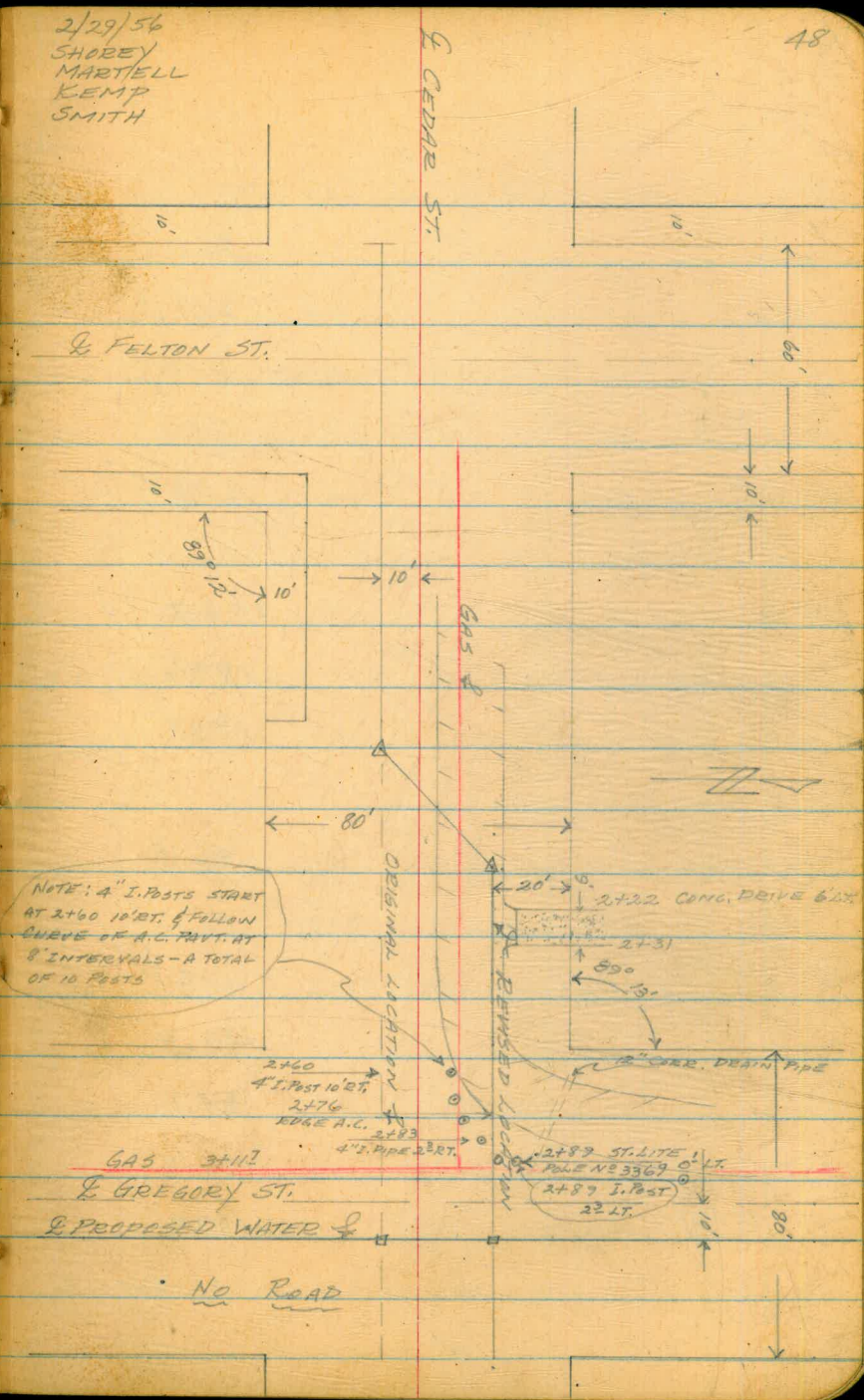
1+92⁴³ Δ 45° RT.

3+31⁷² P.I. OF PROPOSED WATER ON GREGORY ST.

3+61⁷² = E/W GREGORY ST.

2/29/56
 SHOREY
 MARTELL
 KEMP
 SMITH

48



CEDAR ST.
(CONT'D)

TP	4.48	214.69		210.21
1+50	APT		1.6	213.0
1+66			3.4	211.2
1+71	EDGE A.C. PART ON E		4.4	210.2
1+92 ⁴³	APT. 45° RT.		7.1	207.5
2+00			8.2	206.4
TP	0.01	202.00	12.70	201.99
2+50			1.3	200.7
2+76	EDGE A.C. PART ON E		2.4	199.6
2+83			2.1	199.9
3+00			5.5	196.5
TP	1.70	190.83	12.87	189.13
3+31 ⁷²	P.L. WATER LINE ON GREGORY		1.7	189.1
3+40			6.3	184.5
3+45			6.7	184.1
3+55			11.8	179.0
3+61 ⁷²	E/L GREGORY ST.		12.9	177.9
CK JBM			7.02	183.81 = 183.80

Reduced by Volume's 3-7-52

LT

RT

SEE PAGE 42

EDGE A.C. PART ON E

5.0	7.1		6.8
10	10		10 ON A.C. PART
		EDGE A.C.	
6.1	7.8	8.2	7.8
10	4	10	10 ON A.C. PART
		EDGE A.C.	

+3.3	1.7	1.8	
17	8.5	10	
		EDGE A.C.	

EDGE A.C. PART ON E

2.7	2.4		3.3	2.8	5.8
10	4		6	10	15
		EDGE A.C.			

1.8	5.9	4.1		8.2	11.9
19	9.5	7		14	2.1
		FLOW LINE			
		12" CORR. STORM DRAIN			

1.5			2.2	3.5
10			10	20

14.7			12.6
10			10

ORIG. P.L. HUB - SEE PAGE 43

OLIPHANT ST
WILLOW to EVERGREEN
Prelim. for 6" A.C.
(City Force)

4+30⁶ Sely # Evergreen

3+80⁶ Nwly # Evergreen

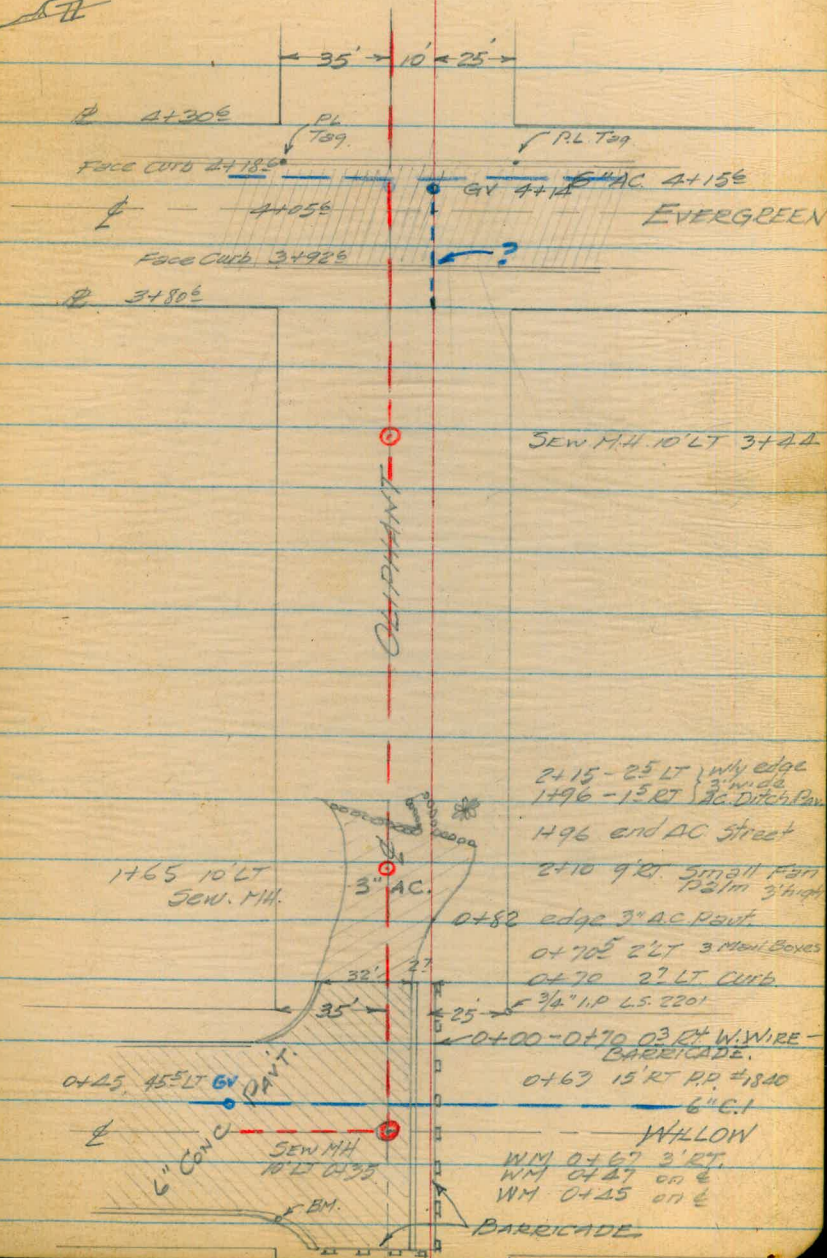
0+70 Sely # Willow

0+00 Nwly # Willow

12/12/56
BEATTY
PAULSON

50

ST



OLIPHANT ST
& Profile
Proposed 6" A.C

12/12/56

51.

BM	1.71	154.52	152.81	151.22	
0+00			3.3	154.1	
0+35			3.0	151.52	
0+70			3.3	151.22	
0+82	Edge 2" A.C		5.00	149.52	
1+00	on A.C		7.35	147.17	
1+50	on A.C		13.25	141.27	
IP	0.16	141.39 ^{141.29 asm}	13.39	141.13	
1+96			3.00	138.29	
2+00			3.3	137.99	
2+10			4.8	136.49	
2+22			10.8	130.49	
IP	0.13	128.44 ^{128.34 asm}	13.08	128.31 ^{128.21 asm}	
2+50			6.6	121.74	
IP	0.00	115.54 ^{115.44 asm}	12.90	115.34 ^{115.44 asm}	
3+00			7.8	107.64	
IP	0.01	102.36 ^{102.26 asm}	13.19	102.35 ^{102.25 asm}	
Rim Sew 14" H			6.10	96.16	
Inv.					

NW BR. Oliphant & Willow

0.85 1.70 3.60 2.88
3.27 3.28 2.8 2.7
Top curb Gutter Gutter Top curb

Edge A.C. 5' RT 12' LT

Palm tree 9' RT

c Sew 14" H. 3" A4 10' LT

OLIPHANT ST
(Cont'd)

12/12/56

52

		102.26 ^{ain}		
		102.26		
3+50			9.1	93.16
TP	0.26	89.26 ^{ain}	13.26	89.00 ^{ain}
		89.26		89.10
3+75			2.2	87.06
3+92 ⁶	Top curb		8.75	80.51
3+92 ⁷	conc		9.17	80.09
4+00	"		8.80	80.46
4+05 ⁶	" & 5'		8.73	80.53
4+18 ⁵	"		9.10	80.16
4+18 ⁶	Top curb		8.65	80.61
4+30 ⁶	Sely of Evergreen		9.6	79.66
Set TOM			4.84	
		84.42 ^{ain}		
		81.52		

W. GV. 4+12

Prop line tag on curb Sely Cor Willow & Evergreen
L3 22.01

GREGORY ST.

DATE TO CEDAR

③ STR'S 4' GRD 6" A.C. MAIN

TBM 12.81 228.61 215.80

2/8/57

SHOREY
KEMP
SMITH

2X2 HUB 23' RT. 0+53 PG. 45

BEGIN WORK
0+93 F.H. TEE

6.4 222.2 215.8

C6⁴

⑤

6.2 222.4

C2⁵ TO FLANGE C6⁶ TO BOTTOM

1+00

6.0 222.6 215.5

C7¹

1+50

5.8 222.8 214.2

C8⁶

1+60

6.7 221.9 214.0

C7²

2+00

12.2 216.4 210.4

C6⁰

TP 0.09

216.27 12.43 216.18

2+35

4.6 211.7 207.4

C4³

2+50

7.1 207.2 205.0

C4²

3+00

⑤ RT.

13.1 203.2 196.4

C6⁸

TP 1.15

⑤ LT.

204.32 11.4 204.9

C8⁵

3+50

⑤ RT.

13.10 203.17

C7⁴

⑤ RT.

5.1 195.2

C10⁵

⑤ RT.

6.0 198.3

3+55

186.8

3+95²²

6" TEE

⑩ RT.

13.3 191.0 185.0

C6²

⑤ RT.

11.9 192.4

C7⁴

TP

4.12

195.20 13.24 191.08

CK. TBM

11.39 183.81 = 183.80

PG. 43

WATER METERS

0+78 W

228.61

8.2 220.4

218.6

C18

0+98 E.

6.5 222.1

218.8

C32

"1643"

1+34 W.

2.6 226.0

217.9

C8¹

"1636"

1+41 E.

5.3 223.3

217.7

C56

"1635"

1+80 E.

9.0 219.6

215.5

C41

"1630"

2+16 W.

216.27

11.6 217.0

212.3

C42

"1621"

2+42 E.

5.7 210.6

207.5

C14

"1620"

2+67 W.

5.6 210.7

206.1

C46

"1614"

3+22 W.

204.32

2.4 201.9

199.6

C2³

CEDAR ST,
FELTON TO GREGORY
⑤ STK'S & GARD. 6" A.C. MAIN

3/11/57
SHOREY
KEMM
SMITH

54

TBM 1.03 222.08 221.05

⑦ L&T N.W. COR. FELTON & CEDAR ST. PG. 42

0+40	BEGIN WORK	3.4	318.7	215.0	C3 ⁴	CUT TO EXIST. MAIN
0+50		3.6	318.5	215.0	C3 ⁵	
1+00		4.9	317.2	210.5	C6 ²	
1+50	45° BEND LT.	9.0	313.1	206.0	C7 ¹	
	TP 0.11	209.26	12.93	209.15		
1+99 ⁵⁰	45° BEND RT.	2.7	206.6	202.3	C4 ³	
2+00	OMIT			201.5		
2+50		9.5	200.8	197.1	C3 ²	
3+00	TP 0.40	197.49	12.17	197.09	C4 ²	
3+33 ²²	END.	8.0	189.5	185.0	C4 ⁵	

CK. TBM 13.69 183.80 = 183.80

P.I. HUB. 3+19⁷⁰ (PG. 43)

WATER METER

2+49 N.	209.26	8.3	201.0	200.2	C0 ⁸	"3350"
---------	--------	-----	-------	-------	-----------------	--------

Spray St.
(Cont'd.)
& profile

2/13/57

26

BM	3.86	09.84	05.98		NW 7' CT Longbranch & Bacon
BM	5.25	08.59	6.50	03.34 = ?	OP NE Cor Longbranch & Abbott
Set BM	2.67	05.38	5.88	02.71	End of curb SE Cor Spray & Longbranch
0+00			3.37	2.01	on conc part
0+50			2.90	2.48	on conc part
0+09			2.30	3.08	on oil berm
0+51			2.30	3.08	" " "
0+52			2.8	2.58	
0+60			3.3	2.08	
0+68			4.1	1.28	
0+76			4.2	1.18	
0+95			4.1	1.28	
1+00			4.1	1.28	
1+02			4.2	1.18	
1+07			5.6	-0.22	on beach sand
1+50			5.1	+0.28	
2+00			4.9	+0.48	
2+50			4.8	+0.58	
3+00			4.2	1.18	

SPRAY ST.
Cont'd

2/3/57

57

	05.38		
3406 P1		2.1	1.28
3450		3.1	2.28
4400		2.6	2.78
44319		2.6	2.78
4438 @ barricade		2.3	3.08
set TOM	1.55 05.40 ✓	1.89 03.55 ✓	
CK TOM	5.55 08.56 ✓	2.69 02.71 ✓	
BM	6.32 09.66 ✓	5.22 03.30 ✓	
CK BM		3.66 06.00 = 05.98	

End of curb so. side Brighton St.

" " " SE Cor. Spray & Longbranch

T CT NW Cor Longbranch & Bacon

MARTIN AVE
3270 to BANCROFT
STR. 5 & GRDS for 6" A.C. MAIN

FEB. 20 1957
BEATTY
SMITH
O'BRIEN

58

TBM.				Sec. Level CHECK 11.59		
	9.84	22.16 22.40	12.32 12.56		1" I.P. SE Cor Bancroft	
3+73	6" TEE		11.2 11.4	07.0	C44 C42	
3+50			12.2 12.4	08.2	C42 C40	
3+00			15.1 15.3	12.3	C39 C28	
^D 2+50	12.49	32.64 32.88	20.15 20.39	16.4	C42 C38	
2+12			23.1 23.4	19.5	C39 C36	
2+00			24.1 24.4	20.7	C37 C34	
1+50		39.88 40.12	30 29.9	25.9	C42 C37	
^D 1+00	7.33		0.09 32.77	32.55	C39 C36	
0+60	GV. (CITY)		5.3 32.8 32.6	31.0		
0+50			1.40	34.72		
^D 0+00	0.29	28.43	11.98	28.14		
^D CK TBM	0.06	18.62	9.87	18.56		
WAT. SER			6.07	12.55-12.56		
1+29 sly		39.88 40.12	5.8	34.1 34.3	31.2	C37 C28
2+04 sly		32.64 32.88	6.9	25.7 26.0	23.7	C37 C20

BANCROFT ST
MARTIN AVE, NW
Stks & Grd.s for 6" AC Main

FEB. 20 1957
Same Party

59.

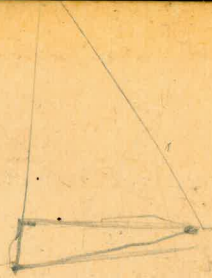
TE TBM	9.32	21.64 21.88	12.32 12.56		1" I.P. SE Cor Bancroft & Martin
3 0+00	6" TEE	10.3	11.3 11.6	07.0	C49 C43
3 0+37		9.5	12.1 12.2	06.5 06.0	C64 C56
3 0+50		8.2	13.4 13.7	08.0	C57 C54
4 0+91	Connect to Existing Main.	0.9	20.7 21.0	16.3	—
CK BM		9.32	12.32 12.56		NW B.P. 31st & Ocean View 48.61

CHECK LEVELS

2/2/57

CK BM	11.94	60.55	48.61		NW B.P. 31st & Oceanview
CK BM	0.58	60.99	0.04	60.51 = 60.20	Top F.H. 32nd & " see pg. 38
I.P.	0.08	50.79	10.28	50.71	
CK TBM	0.75	41.77	9.77	41.02 = 41.03	Top F.H. SE Cor. Martin & 32nd see pg. 38
I.P. 1450	0.10	29.68	12.19	29.58	
I.P.	0.19	17.08	12.79	16.89	
CK TBM	13.27	25.59	4.76	12.32 = 12.56	Inv. 6" Sew 1" I.P. SE Cor Bancroft & Martin p. 6-894 p. 75-894
I.P.	8.93	34.35	0.17	25.42	
I.P.	6.99	37.67	3.67	30.68	
CK BM		1.57	36.10 = 36.23		Top F.H. SW. Cor Bancroft & Oceanview see 894 - pg. 6

331.72
 172.43
 139.29
 5
 134.29
 179.50
 3433.79



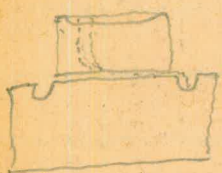
102 | 30.400
 204
 1000
 918
 820

112.50
 82.10
 30.40



52.19
 7.09
 59.27
 5.57
 53.40
 1.22
 54.62
 1.65
 50.07
 12.95
 63.06
 1.20
 61.86

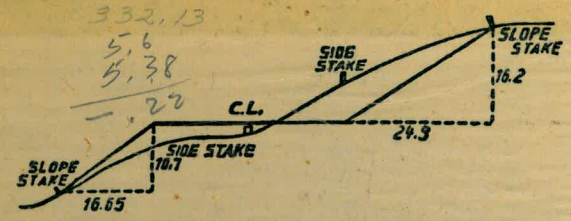
1298
 85
 1490
 2384
 25330
 82.10
 107.93
 25.33
 83.10
 708.93



110 | 30.400
 220
 840
 770
 700

2489 1 Post 2³ RT
 2489 1 LT STREET LITE
 Post N2 3369
 2489 1 Post 2³ LT
 34115 GAS MAIN XING 30.6

1276
 85
 1380
 2208
 23460
 82.10
 105.56



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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