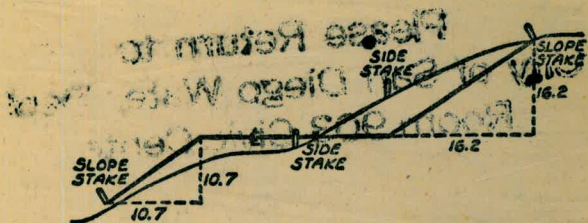


W 915



Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

MICROFILMED

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

50' E  
 GERTA  
 39 W  
 119 W



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.42	1.54
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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ALICE







LEVELS AT PROPOSED  
STORAGE RESERVOIR  
P.L. 1264

6/15/55

Kemp  
Alexander  
Hollahan

3.

TBM	11.16	719.65		708.49
IP	9.38	720.77	8.26	711.39
IP	3.54	714.56	9.75	711.02
			9.56	705.00
			9.56	705.00
IP	13.15	727.61	0.10	714.46
IP	12.90	740.33	0.18	727.43
IP	12.51	752.64	0.20	740.13
IP	2.28	754.80	0.12	752.52
IP	0.15	744.21	10.74	744.06
IP	0.35	732.01	12.55	731.66
IP	0.22	722.49	9.74	722.27
CK BM	9.22	722.84	8.87	713.62 = 712.25
IP	11.16	733.45	0.53	722.29
IP	12.54	744.21	1.78	731.67
IP	11.18	755.26	0.13	744.08
IP	0.08	752.62	2.72	752.54
IP	0.23	740.39	12.46	740.16

2x2 Hub (orig. Align) B.C. 119+06.13 (City Engr. F.B. 1291-58)

Set Hub Location #1

" " " #2

Chris X So. Porch Civil Defence Bldg FB 756 pg. 42

Don't  
CHECK!



6-15-55

4.

① 0.00 740.39 12.94 727.45

② 2.57 718.44 11.58 715.87

③ 7.62 719.04 7.02 711.42

CK BM 10.53 708.51 = 708.49 2x2 BC see pg. 3



REVISED LOCATION  
 PROPOSED STORAGE RESERVIOR  
 & Proposed Pipeline into Same.

AUG. 4 1955  
 WEST  
 WILLIAMS  
 VARDEN FAKIS  
 KELLHOFER

See page 2

7+14.46 Proposed Tank

4+75 POT Nail

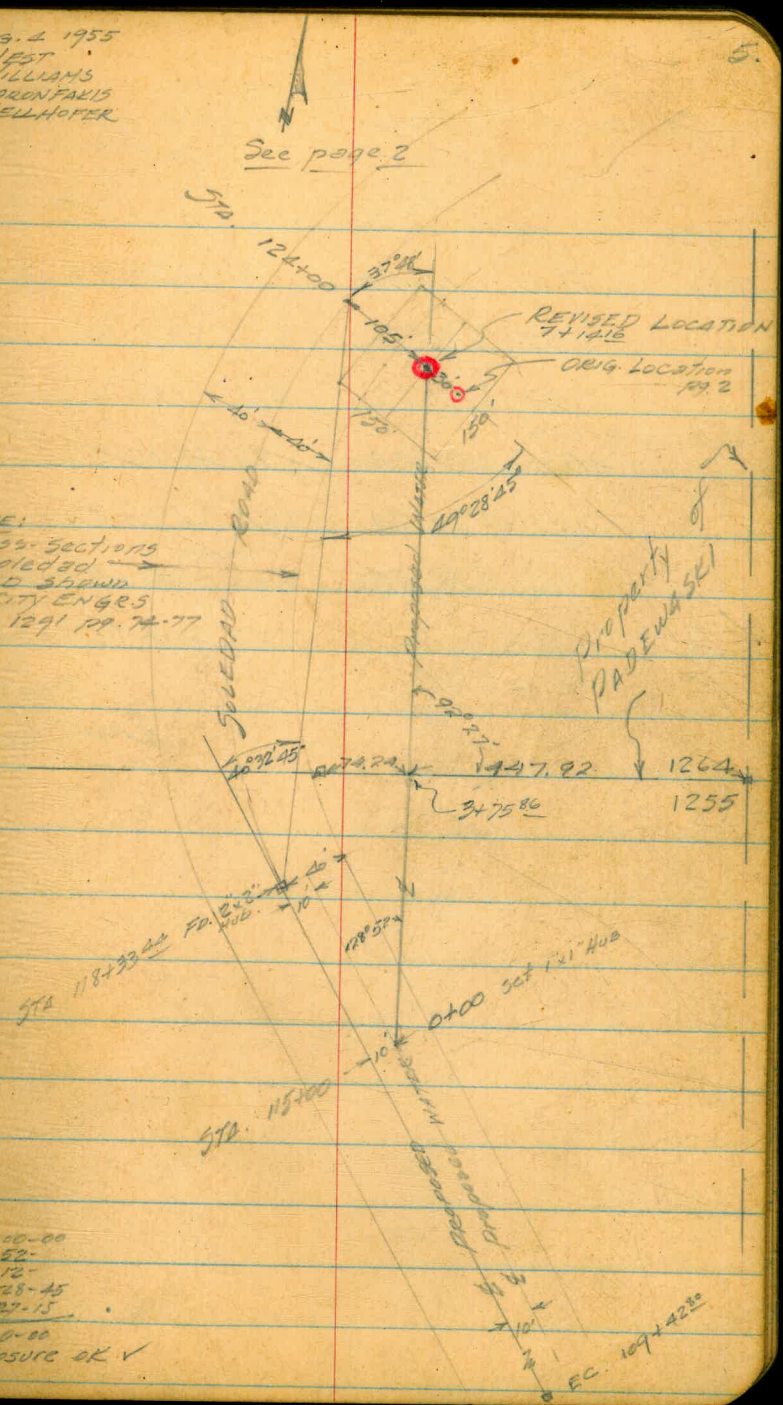
3+75.86 Intersection Public Lot Line

2+97.27 POT nail

= 0+00 Tank line Sta  
 115+00 Hwy Sta  $\angle 28^{\circ} 52' 00''$  RT

NOTE:  
 Cross sections  
 of folded  
 Road shown  
 in CITY ENGRS  
 FB 1291 19. 7-77

115-00-00  
 118-52-  
 122-12-  
 129-28-45  
 139-27-15  
 530-00-00  
 Closure OK V



Property  
 PADEWASEL

REVISED LOCATION  
 7+14.46  
 Orig. Location  
 139.2

Sta 118+33.44  
 Sta 115+00  
 0+00 set 1.51" Hub

EC. 109+42.20



CHECK LEVELS  
Profile Proposed  
Reset V. Oil and Pipe Line  
PL 1264

~~Tom~~

5.03	711.52		708.49
0.37	698.72	13.17	698.35
0.53	686.24	13.01	685.71
1.83	686.48	1.59	684.65
0.91	677.94	9.45	677.03
2.95	671.59	9.30	668.64
		6.69	664.90 = 663.56

FB 1291

page 51  
= 663.79 FB 1291

DONT CHECK!

8/2/55

West  
Williams  
Varonakis  
Alexander  
Kellhofer

(pg 3.)

Turn on 1" x 1" Hub & Jack 0+00 Tank Line Sta  
155+00 Hwy Sta

109+42<sup>80</sup> Turn on EC 2x2" Hub

page 71

Bone Man Pt. of Hwy Curve



PROPOSED PIPELINE INTO  
 PROPOSED STORAGE RESERVOIR  
 & PROFILE & CROSS-SECTIONS

8/3/55

7.

118+33.44

TBM	0.46	703.80	703.34
	1.09	691.65	13.24 690.56
		8.37	683.28

Bladed out!  
 8/30/56  
 party

309 FB 1291 Page 75  
 118+33.44 TBM 2"x2" Hub & B.C.

1x1 Hub 0+00

683.88  
 C-11-72  
 SHT 19

0+00		8.37	683.28
------	--	------	--------

0+50		6.4	681.3
------	--	-----	-------

1+00		4.8	686.9
------	--	-----	-------

+50		4.1	687.6
-----	--	-----	-------

1222	698.66	5.21	686.44
------	--------	------	--------

2+00		8.0	690.7
------	--	-----	-------

+50		4.8	693.9
-----	--	-----	-------

1206	708.09	2.63	696.03
------	--------	------	--------

NOTE:  
 SECTIONS taken  
 to left side are  
 out to Ely edge  
 of 80' Road.  
 See sketch

686.35	5.3	50' LT	681.15	12.00	50' RT
681.15	1.5	50' LT	681.5	10.5	50' RT
672.25	10.6	50' LT	682.15	9.5	50' RT
672.85	+1.2	64.4	682.75	+1.1	9.9
		50' LT			50' RT
694.86	2.2	80' LT	686.46	3.8	12.5
688.36	0.3	67	695.86	2.8	8.2
695.86	2.8	42	695.66	3.0	50' RT
		120			23.4







Proposed Res Cont

8/5

9.

Bottom of SE Bulley 718.71  
 5+11 26.4 692.31  
 5+16 23.8 694.91

End of Bulley 695.71  
 17.6 701.11  
 21.1 14.4

691.11  
 27.6  
 20.8

5+50 24.3 694.4

713.51 711.41 707.11 701.11  
 5.2 7.3 11.6 13.4  
 13.1 100 33 31.1  
 2.4 716.31 2.7 716.01  
 173.11 160.11

688.51 685.51 682.51  
 30.2 33.2 35.2  
 20.8 26.8 32.8  
 680.31 677.71  
 38.4 41.0  
 40 50.8

6+00 19.4 699.31

712.71 708.51 704.01  
 6.0 10.2 14.7  
 100 32.1 12.1  
 1.6 717.11 716.51 715.41  
 168 762 150.11

686.11 677.61  
 23.2 11.1  
 7.8 50

6+50 15.6 703.1

714.21 711.61 706.71  
 4.5 7.1 12.8  
 2.2 2.8 9  
 719.21 718.71 715.71  
 14.5 145.11 30 111.11

687.91 692.01  
 30.8 26.7  
 29.8 50.8

6+56 15.3 703.4

6+70 15.4 703.3

6+85 15.6 703.1

6+90 15.7 703.0

7+00 15.3 703.4

7+05 15.0 703.7

7+14<sup>16</sup> c of proposed tank 13.4 705.3

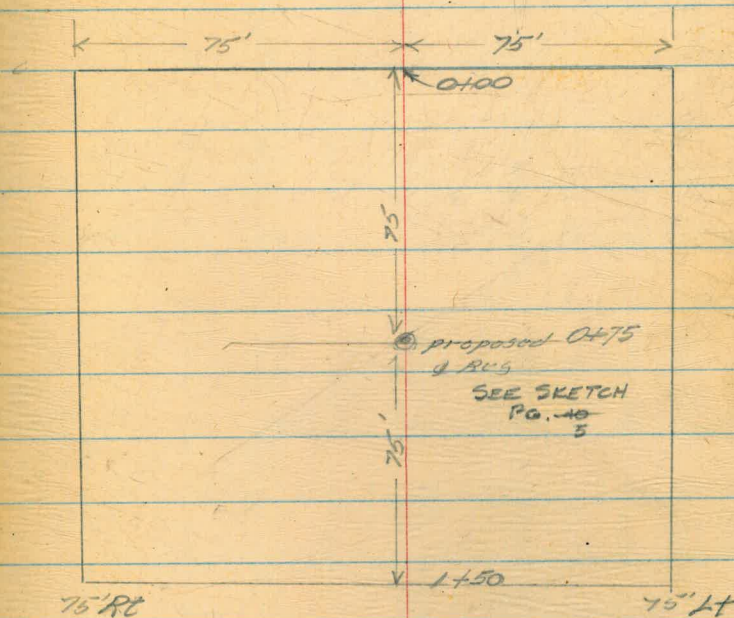
PD 1303 730.11 1.63 717.08



Proposed Res  
Plat showing Grid System  
Used

West  
Williams  
Varonfakis  
Alexander  
Kullhofer

Radial Line from Hwy Sta  
1294+00



Mag. Br. N. 55° W.



Proposed Res - (Brid) - sections

730.11 (from pp. 9)

(See sketch pp. 10)

0+00

5.6 724.51

735.1 737.9  
+5.0 +3.8  
730.1 731.1

0+10

7.9 722.21

0+20

9.8 720.31

0+30

12.2 717.91

6.58 728.22 8.47 721.64

0+40

13.8

714.4  
716.42

TBM Set 2.57 720.67 10.12 718.10

1.27 715.99 5.95 714.78

12.68 703.31 =

LT

8-5-55

RY

730.5	728.7	727.9	726.1	724.9	723.8	722.1	720.7	718.8	716.5	714.3	712.4	710.1
+0.9	1.4	2.8	4.0	5.2	6.3	7.7	8.7	9.5	10.3	10.8	11.2	11.5
60	53	40	32	20	10.1	10.4	20.4	30	40	50	60	75

732.31	728.11	726.11	725.01	724.11	723.51	722.71	722.61	722.61	723.61	723.51	723.71	722.91	722.61
+2.2	2.0	4.0	5.1	6.0	6.6	7.4	7.5	7.5	6.5	6.6	6.9	7.2	7.5
75	60	50	40	30	20	10	10.4	20	30	40	50	60	75

729.81	726.31	724.61	723.11	722.01	720.71	720.21	719.91	720.61	722.01	722.31	722.41	722.31	721.51
0.3	3.8	5.1	7.0	8.1	9.4	9.9	10.2	9.5	8.1	7.8	7.7	7.8	8.6
70	60	50	40	30	20	10.1	10.4	20	30	40	50	60	75

725.11	722.81	722.31	722.91	719.31	718.91	717.51	717.91	718.51	719.41	721.11	720.71	721.01	721.31
4.7	7.3	2.8	9.2	10.8	11.7	12.0	12.2	11.7	10.5	9.0	8.4	8.9	8.8
75	60	50	40	30	20	10	10.4	20	30	40	50	60	75

727.82	721.82	718.82	716.82	716.52	714.12	713.62	716.72	717.02	717.92	719.22	720.52	720.82	720.32
0.4	6.8	9.4	11.4	12.7	14.1	14.6	12.5	11.2	10.8	9.0	7.7	7.4	7.9
75	60	50	40	30	20	10	10.4	20	30	40	50	60	75

1x1 400 SET & RT 0+30

703.34 - where?



Proposed Res. Gald Sections

WILLIAMS  
ALEXANDER  
VANDYKE  
KELLROPER

8-8-55

12

718.10

IXI H. P. 11 E 0130

7.53 725.63

LT.

RT

0+50

15.9

709.73

729.6	726.9	721.9	719.4	715.8	711.1	710.6	710.0	705.5	705.3	705.7	711.7	719.1	717.5	719.4
+ 4.0	1.3	3.7	6.2	7.8	12.5	15.0	16.6	15.6	12.1	10.8	9.9	7.9	6.5	6.1
75	60	50	40	30	20	10	5	2.0	1.0	2.0	3.0	7.5	5.0	7.5

0+60

18.3

707.33

729.93	725.33	722.83	719.63	714.63	713.53	711.03	706.23	716.43	713.03	714.93	716.23	712.73	718.23	718.23
+ 7.1	0.3	2.8	6.0	9.0	12.1	14.6	19.9	14.2	12.0	10.9	9.1	7.9	7.4	3.4
75	60	50	40	30	20	10.17	1.17	7.0	2.0	3.0	4.0	5.0	6.0	7.5

0+70

19.1

706.53

729.93	724.93	722.43	720.73	717.23	713.43	709.53	705.63	708.53	711.03	710.93	713.63	715.63	716.93	717.13	716.63
+ 3.8	0.7	3.2	5.2	8.4	12.2	16.1	20.0	17.1	14.6	13.7	12.0	10.0	8.7	8.5	9.0
75	60	50	40	30	20	10.17	3.17	7.0	1.0	1.5	2.0	3.0	4.0	6.0	7.5

0+75 (center proposed tank) 20.33 705.31 ✓

729.73	725.23	723.03	720.63	717.53	713.33	708.83	705.13	707.53	710.5	711.7	713.4	715.2	716.1	716.9	716.0	
+ 7.1	0.4	2.6	5.0	8.1	12.3	16.8	20.5	18.1	15.1	13.9	12.4	10.4	9.5	9.3	9.6	
75	60	50	40	30	20	10.17	5.17	7.0	1.0	1.6	2.0	3.0	4.0	5.0	6.0	7.5

0+80

21.1

704.53

730.03	726.53	723.63	721.63	718.43	714.53	709.13	704.63	706.33	709.83	710.73	712.73	714.73	715.83	716.03	715.23
+ 4.4	0.9	2.0	4.0	7.2	11.1	16.5	21.0	19.2	15.8	14.9	12.9	10.9	9.8	9.6	10.4
75	60	50	40	30	20	10	7	10	17	20	30	40	50	60	75

0+90

21.3

704.33

729.93	729.13	729.33	721.93	718.73	716.53	714.13	711.93	709.13	701.83	707.13	702.83	705.33	708.33	711.23	713.13	714.63
+ 4.3	1.5	1.3	2.9	6.9	9.1	11.5	13.7	16.5	23.8	23.5	22.8	20.3	17.3	14.4	12.5	11.0
75	60	50	40	30	23	20	16	10	5	9	10	14	20	30	40	50

714.93  
714.83  
11.2 10.8  
75 60



PROPOSED RESERVOIR  
Grid - Sections

8/8/55

13

1+00	725.63	22.8	702.8
1+10		23.8	<u>721.8</u> X
1+20	5.50 723.60	25.3	718.10
1+30		22.7	700.90
1+40		24.1	699.5
1+50		27.9	696.2
1+50		30.2	693.4
		5.99	718.11 = 718.10

701.8 F.S.J.  
8/15/55

LT.											RT				
726.1	725.9	726.9	721.6	718.7	714.8	708.2	700.5	699.6	699.5	706.5	702.2	706.7	710.8	712.5	712.9
+2.5	+0.3	1.3	3.8	6.7	10.8	17.4	25.1	26.2	26.1	21.3	17.4	16.9	14.8	13.1	12.3
75	60	50	20	30	20	10	5	10	12	20	27	30	40	30	60
728.33	726.23	724.23	721.23	718.33	712.83	707.13	699.83	697.73	699.23	699.03	705.73	708.33	705.03	711.53	714.63
+3.7	+0.6	0.9	4.4	7.3	12.8	18.5	27.8	27.9	26.4	22.6	19.9	17.3	16.6	14.1	14.0
75	60	50	40	30	20	10	8	10	16	20	30	40	50	60	75
717.40	714.2	722.2	720.3	716.9	712.5	710.2	709.8	695.9	694.8	701.6	705.2	706.0	707.5	709.6	710.5
+3.8	+0.6	1.4	3.3	6.7	11.1	13.4	18.8	27.9	26.8	22.0	16.4	17.8	16.1	14.0	13.1
75	60	50	40	30	20	19	10	10	20	30	37	40	50	60	75
725.8	723.4	721.0	717.8	714.4	708.0	703.5	694.6	691.4	688.2	696.0	702.6	705.1	707.8	709.4	
+2.2	0.2	2.6	5.8	9.2	14.8	20.1	29.0	30.2	30.4	25.6	21.0	18.5	15.8	14.2	
75	60	50	40	30	20	10	10	15	20	30	40	50	60	75	
725.5	722.5	719.6	715.0	711.8	706.3	701.0	692.4	687.7	680.5	685.0	689.0	702.4	705.5	707.6	
+1.9	1.1	4.0	8.6	11.8	17.3	22.6	31.2	35.9	33.1	28.6	24.6	21.2	18.3	16.0	
75	60	50	40	30	20	10	10	17	20	30	40	50	60	75	
725.1	721.9	718.4	714.5	710.2	703.9	701.9	697.7	688.9	686.1	688.1	692.2	695.8	699.0	702.1	705.3
+1.5	1.7	5.2	9.1	13.4	19.7	21.7	25.9	34.7	37.5	35.5	31.4	27.8	24.6	21.5	18.3
75	60	50	40	30	20	19	10	10	17	20	30	40	50	60	75



8/9/55

14

ELEVATION ON  $\pm$  PROPOSED ROAD W/ OF PROPOSED TBM

TBM 12.64 730.74 718.10

6.59 737.02 0.21 730.43

124+50 (E Soledad Road) 1.9 735.1 = 734.9

124+00 (" " ") 4.8 732.2 = 732.2

123+50 (" " ") 9.6 727.4 = 727.6

0.36 728.48 8.90 728.12

10.43 718.05 = 718.10

(CONT'D - PAGE 2A)

181 HUB  $\pm$  40430 OF GRID} check orig. elev. S of Soledad Rd FB 1291  
pg. 76



38th St Redwood  
to 200' S of Quince  
51ks for 6" AC Main + Mets

West of  
Williams  
Kellhofen X

15.

Books of Maps Set 5<sup>th</sup> N + 35<sup>th</sup> E

10/17/55

0.00 297.02 297.01

100 FB 901 P17 E of 38th

TBM Top F.H. Alley Set Redwood

303 286.84 1921 283.81

1+83		9.2	277.6	273.9
2+00		7.6	279.2	273.7
+50		4.8	282.0	273.4
+66 m.w.		6.5	280.3	277.0
3+00		5.0	281.8	273.1
+15 m.w.		7.9	278.9	276.8
+50		6.0	280.8	272.7
+79 m.w.		8.5	278.3	276.4
4+00		6.8	280.0	272.3
+50		7.8	279.0	272.0
5+00		8.6	278.2	271.6
+37 <sup>5</sup> T.P.		10.5	276.3	270.2
+50	0.73	276.25	11.32	275.52 269.4
+85 M.W.		3.2	273.1	270.9
+87.5		3.3	273.0	267.1
6+00		4.3	272.0	265.8
+50		7.2	269.1	260.9

7 MARKED CUT TO EXISTING  
C3 Begin work

C5 <sup>5</sup>

C8 <sup>6</sup>

C3 <sup>3</sup>

C8 <sup>7</sup>

C2 <sup>1</sup>

C8 <sup>1</sup>

C1 <sup>9</sup>

C7 <sup>7</sup>

C7 <sup>0</sup>

C6 <sup>6</sup>

C6 <sup>1</sup>

C6 <sup>1</sup>

C2 <sup>2</sup>

C5 <sup>9</sup>

C6 <sup>2</sup>

C8 <sup>2</sup>

3064

3059

3052

Turn on Binney



38<sup>TH</sup> ST. CONT.

276.25

6+75	8.9	267.4	258.6
7+00	10.0	266.3	257.2
+12.5	10.7	265.6	256.5
+30	11.2	265.1	256.0
T.P. +50	11.3	265.26	12.12 264.13 255.8
7+75	22	263.1	255.3
+88 mE	3.1	262.2	258.4
8+00 mW	2.7	262.6	259.0
+00	4.6	260.7	254.0
+12.5	6.0	259.3	253.3
+48 mW	5.2	260.1	256.8
+50	9.6	255.7	250.0
+56 mE	10.5	254.8	253.3
0.11	252.25	13.12	252.14
8+87.5	2.6	249.7	246.0
9+20	4.6	247.7	244.3
+37.5	9.0	243.3	239.0
+50	9.3	243.0	237.7
+76 mE <sup>West</sup>	11.8	240.5	241.5

WEST  
WILLIAMS X  
KELLHOFER †

16.

10/18/55

C8	8
C9	1
C9	1
C9	1
C8	3
C7	8
C3	8
C3	6
C6	7
C6	0
C3	3
C5	7
C1	5
C3	7
C3	4
C4	3
C5	3
F1	0

2997

2948

2959



252.25

10/18/55

3.28 242.58 12.95 239.30

10+05

7.9 234.7 232.7

C2

 $\frac{0}{0}$ 

End of Work 2" 90

Quince St 38th St to Alley E of 38th

1.05 241.53 = 241.52

F.B. 901-20

4.59 268.72 264.13

Turn on Binney 7+50 PAGE 16

0+50

3.7 265.0 256.0

C9

 $\frac{0}{6}$ 

Begin Work

+90

5.5 263.2 256.6

C6

 $\frac{7}{6}$ 

+225

8.0 260.7 257.0

C3

 $\frac{1}{7}$ 

+50

9.8 258.9 255.8

C3

 $\frac{1}{8}$ 

+75

10.2 258.5 254.7

C3

 $\frac{2}{8}$ 

2+00

7.5 261.2 255.0

C6

 $\frac{7}{2}$ 

+35

5.3 263.4 258.7

C4

 $\frac{7}{7}$ 

no net marks

4.59 264.13 = 264.13



FAIRMOUNT AVE.  
 REDWOOD TO MAPLE  
 STKS. FOR 5" MAIN

BM	0.26	306.33	306.07
0+40			2.75 303.58
+50			3.0 303.3 300.5
+75			3.6 302.7 299.2
1+00			4.0 302.3 298.7
+50			5.2 301.1 297.4
2+00			6.4 299.9 296.4
+50			7.7 298.6 295.0
3+00			9.1 297.2 293.8
+50			9.4 296.9 293.6
4+00			8.8 297.5 293.6
+50			8.9 297.4 293.6
5+00			9.0 297.3 293.6
+50			9.2 297.1 293.5
TP	4.45	301.98	8.80 297.53
4			
5+70 <sup>15</sup>			4.85 297.13 293.4
7			
6+11 <sup>50</sup>			5.2 296.8 293.3
+50			5.2 296.8 293.2
7+00			5.2 296.8 293.1

WEST X  
 WILLIAMS +  
 KELLHAFER

18.

10/19/55 PARTLY CLOUDY

SEFH. FAIRMOUNT & REDWOOD

BEG. WORK CUT TO EXISTING

C2 <sup>8</sup>

C3 <sup>5</sup>

C3 <sup>6</sup>

C3 <sup>7</sup>

C3 <sup>5</sup>

C3 <sup>6</sup>

C3 <sup>4</sup>

C3 <sup>3</sup>

C3 <sup>9</sup>

C3 <sup>8</sup>

C3 <sup>7</sup>

C3 <sup>6</sup>

C3 <sup>7</sup>

C3 <sup>5</sup>

C3 <sup>6</sup>

C3 <sup>7</sup>



## FAIRMOUNT CONT.

19.

301.98

10/19/55

7+50		5.5	296.5	293.0	C3	<u>5</u>
8+00		5.6	296.4	292.6	C3	<u>8</u>
+50		5.8	296.2	292.5	C3	<u>7</u>
9+00		5.9	296.1	292.4	C3	<u>7</u>
+50		6.1	295.9	292.2	C3	<u>7</u>
10+00		6.4	295.6	291.8	C3	<u>8</u>
+50		6.5	295.5	291.6	C3	<u>9</u>
11+00		6.7	295.3	291.4	C3	<u>9</u>
+50		7.0	295.0	291.2	C3	<u>8</u>
TP	0.28	295.48	6.78	295.20		
12+00		0.8	294.7	291.0	C3	<u>7</u>
+50		1.2	294.3	290.3	C4	<u>0</u>
13+00		2.4	293.1	289.4	C3	<u>7</u>
+50		3.6	291.9	288.2	C3	<u>7</u>
14+00		5.0	290.5	287.0	C3	<u>5</u>
+50		6.2	289.3	285.8	C3	<u>5</u>
15+00		7.5	288.0	284.6	C3	<u>4</u>
+50		8.6	286.9	283.4	C3	<u>5</u>
16+00		9.7	285.8	282.2	C3	<u>6</u>



FAIRMOUNT CONT.

295.48

10/19/55

7 16+50

10.9 284.6 281.0

C3  $\frac{6}{6}$

8 17+00

12.1 283.4 279.8

C3  $\frac{6}{6}$

TP  
+50

2.34 284.61

13.21 282.27 278.7

C3  $\frac{6}{4}$

9 18+00

3.5 281.1 277.7

C3  $\frac{6}{6}$

+50

4.6 280.0 276.4

C3  $\frac{6}{6}$

10 19+03

5.5 279.1 275.5

END WORK CUT TO EXISTING

CHK. B.M.

4.47 280.14 = 280.<sup>17</sup><sub>57</sub>

NW.B.P. MAPLE & FAIRMOUNT

11

+

12

+

13

+

14

+

15

+

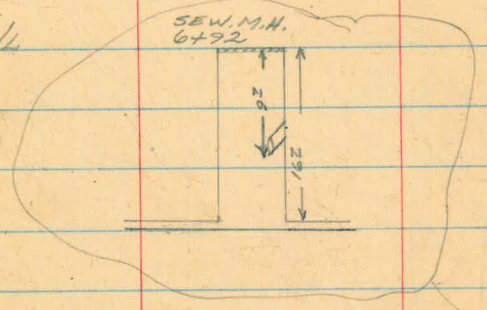
16



ALLEY BLK 7  
 E. of 46<sup>th</sup>, So. of WIGHTMAN

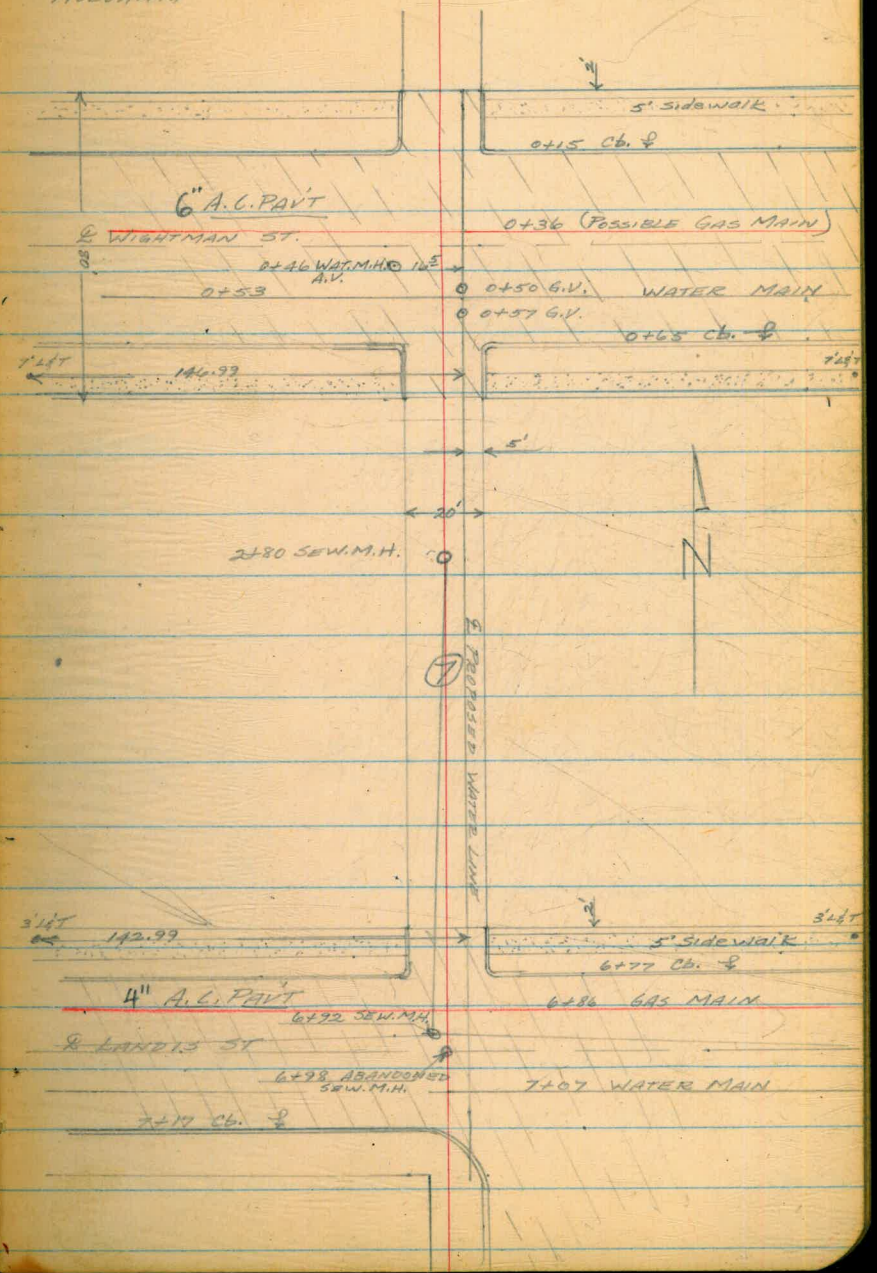
0+00 = N/L WIGHTMAN ST.

0+80 = S/L



7+29<sup>75</sup> S/L LANDIS

10/27/55  
 SHORBY  
 MARTELL  
 KEMP  
 HOLAHAN





ALLEY BLK. 7  
E. of 46<sup>th</sup>, So. of WIGHTMAN

10/27/55  
SHOREY  
MAITELL  
KEMP  
HOLOHAN

22

BM.	2.04	349.97		347.93	
0+00			7.2	342.77	
0+14			7.6	342.37	
0+46			7.4	342.57	
TP	5.68	348.24	7.41	342.56	6
0+50			5.8	342.4	
0+66			6.4	341.8	
1+00			5.7	342.5	
1+50			5.3	342.9	
2+00			4.9	343.3	
2+50			4.4	343.8	
	SEW. M.H.			344.23	
		3.97		336.23	
3+00			4.1	344.1	
3+50			4.8	343.4	
4+00			5.9	342.3	
4+50			7.1	341.1	
5+00			7.3	340.9	
TP	8.86	350.07	7.03	341.21	✓
5+50			8.1	342.0	
6+00			6.0	344.1	

N.W.B.P. WIGHTMAN & CHAMOUNE

GUTTER LINE

WATER LINE XING

WAT. M.H. 16<sup>5</sup> RT.

GUTTER LINE

2+80 SEW. M.H. 5 RT.

±

Reduced by A.E. MATHISON



ALLEY BLK. 7  
(CONT'D)

350.07

6+50 4.0 346.1

6+77 6.0 344.1

6+92 3.5 344.6

SEW. M.H.

{ 5.30  
12.22 337.9  
22.0 328.1  
5.2

344.8

SEW. M.H. 6+92 9' RT.

7+00 344.9

H  
E

7+17 5.6 344.5

GUTTER LINE - LANDIS ST.

7+24 5.5 344.6

GUTTER

7+24 4.9 345.2

TOP CB.

7+29<sup>35</sup> 4.9 345.7

SO. LINE LANDIS ST.

TP 3+16 347.00 6.23 343.84

CK. B.M. 5.99 341.01 = 341.00

N.W. B.P. CHAMOUNE & LANDIS ST.

10/27/55  
SHOREY  
MARTEL  
KEMP  
HOLAHAN



PROPOSED RES.  
GRID-SECTIONS  
(CONT'D FROM PAGES 10-14)  
& PROFILE

TBM	0.00	705.31	705.31
TP	0.64	673.47	12.48 672.83
1+60			2.4 671.1
1+70			3.1 670.4
1+80			5.2 688.3
1+90			6.8 686.7
2+00			8.5 685.0
2+10			10.2 683.3
2+20			12.0 681.5
TP	0.89	681.54	12.82 680.65
2+30			2.7 678.8
2+40			6.9 674.6
2+50			11.6 669.9
TP	3.91	673.22	12.23 669.31
2+60			5.2 668.0
2+70			9.3 663.9
2+80			12.8 660.4
2+90			14.9 658.3
3+00			19.2 654.0
TD	12.96	684.17	2.01 471.21

10/31/55  
SHREY  
MARTEL  
KEMP  
HOLEHAN

24

0+75' XI HUB & PROPOSED TANK (SEE PG. 12)  
684.17  
2 TP 12.86 696.58 0.45 683.72  
TP 10.03 705.49 1.12 695.46  
CK TBM 0.17  $\frac{705.32}{705.31}$



West  
Williams  
Varonakis  
Kellhofer

4.95 696.05 691.10

1+60

695.7 -0.2 10	702.5 +6.3 20	708.1 +12.0 30	710.0 +13.9 34.9	711.4 +15.9 35	686.2 2.3 10	694.3 11.8 18	684.9 11.2 20	688.1 7.0 30	692.5 3.6 40	686.7 +0.6 52	697.5 +1.4
712.9 +14.8 30	714.5 +20.4 50	720.6 +28.5 60	723.6 +27.5 70		698.4 +2.3 60	701.3 +5.2 70	702.3 +7.3 80	705.0 +8.9 90	705.7 +9.6 100		

1+70 150 694.90 690.4

706.0 +22.9 80	708.2 +32.1 90	720.7 +31.6 105			707.4 +11.1 110	707.6 +11.5 120	709.4 +11.7 130				
695.2 +0.9 10	699.1 +4.2 20	705.0 +10.1 30	709.4 +14.5 40		695.5 -2.4 10	683.2 -11.7 20	685.8 -9.1 30	689.1 -5.8 40	691.8 -3.1 50	696.1 +0.3 60	
713.5 +18.6 50	717.7 +22.8 60	722.5 +27.6 70			697.9 +3.0 70	699.9 +5.0 80	702.3 +7.9 90	702.4 +8.5 100			
722.7 +22.8 80	722.6 +32.7 90	720.2 +35.3 105			705.7 +10.8 110	706.4 +11.5 120	706.5 +11.6 130				

1+80 47 693.0 688.3

692.5 -0.5 10	697.2 +4.2 20	702.7 +8.9 30	709.1 +14.1 40		687.8 -9.2 10	681.4 -11.6 20	681.5 -11.5 30	685.2 -7.8 40			
711.8 +18.8 50	716.7 +22.7 60	721.4 +28.4 70	723.4 +30.5 80		688.8 -9.2 50	691.8 -1.2 60	694.9 +1.9 70	696.5 +3.5 80			
726.6 +33.6 90	727.8 +36.8 105				697.2 +6.2 90	701.2 +8.2 100	707.8 +10.0 110	704.8 +11.0 120	709.5 +11.5 130		



Proposed Res Grid Sections  
Cont

1+90 1.7 691.7 686.7

11  
690.7 696.0 701.3 705.9  
-0.7 +1.6 +9.9 +14.5  
10 20 30 40  
711.7 716.4 720.0 723.6  
+20.3 +25.0 +29.6 +31.2  
50 60 70 80  
725.6 729.1  
+32.2 +37.7  
90 100

11-2-55  
682.1 682.4 691.0 699.1 698.1 699.2  
-8.5 -9.0 -10.4 -12.3 -12.7 -12.2  
10 12 13 20 25 30  
661.5 664.4 668.8 691.9 694.6 696.4  
-9.9 -7.0 -2.6 +0.1 +3.2 +5.0  
40 50 60 70 80 90  
695.3 699.9 700.9 703.1  
+6.9 +8.5 +9.5 +11.7  
100 110 120 135

2+00 1.8 689.8 685.0

689.7 694.3 700.5 705.1 709.6  
-0.1 +5.5 +10.7 +15.3 +18.0  
10 20 30 40 42  
710.1 713.8 714.1 717.3  
+20.9 +24.0 +24.3 +28.5  
50 60 63 70  
720.1 722.7 725.7  
+30.3 +32.9 +38.9  
80 90 105

680.4 686.9 695.2 696.4  
-9.4 -12.9 -14.6 -13.4  
10 20 25 30  
695.1 691.1 685.8 688.7 691.9  
-11.1 -8.7 -7.8 -1.1 +2.1  
10 50 60 70 80  
694.1 696.2 697.5 698.4 701.7  
+4.9 +5.8 +7.7 +8.6 +11.9  
90 100 110 120 135

2+10 1.9 688.2 683.3

686.6 693.5 699.8 704.0  
+0.7 +5.3 +11.6 +15.8  
10 20 30 40  
706.2 708.3 710.4 715.8  
+18.0 +20.1 +22.2 +25.6  
41 50 60 70  
716.0 718.2 719.3 724.9  
+22.8 +30.0 +31.1 +36.7  
80 81 90 105

698.7 694.1 691.0 693.4 695.3  
-9.5 -12.1 -12.2 -12.8 -12.9  
10 20 20 30 40  
697.5 682.2 686.1 691.6 691.9  
-10.7 -6.0 -1.9 +1.4 +3.7  
50 60 70 80 90  
693.7 694.5 696.7 701.8  
+5.5 +6.9 +8.5 +13.6  
100 110 120 135



2+20 4.9 686.4 681.5

$\frac{686.5}{10}$   $\frac{691.5}{20}$   $\frac{696.0}{30}$   $\frac{700.8}{40}$   
 $+10.1$   $+11.9$   $+19.6$   $+14.4$

$\frac{677.5}{10}$   $\frac{682.7}{20}$   $\frac{689.6}{25}$   $\frac{690.5}{30}$   $\frac{692.8}{40}$   $\frac{695.3}{50}$   
 $-8.9$   $-13.5$   $-16.6$   $-15.9$   $-13.6$   $-11.1$

$\frac{703.1}{45}$   $\frac{705.3}{46}$   $\frac{705.7}{50}$   $\frac{708.0}{60}$   
 $+16.7$   $+18.9$   $+19.3$   $+21.6$

$\frac{694.5}{60}$   $\frac{697.9}{70}$   $\frac{686.5}{80}$   $\frac{688.7}{90}$   $\frac{690.3}{100}$   
 $-6.9$   $-1.5$   $+0.1$   $+1.9$   $+3.9$

$\frac{707.8}{70}$   $\frac{715.1}{74}$   $\frac{715.9}{80}$   $\frac{716.8}{90}$   $\frac{720.7}{105}$   
 $+23.1$   $+28.7$   $+28.5$   $+30.1$   $+34.3$

$\frac{692.7}{110}$   $\frac{695.4}{120}$   $\frac{699.9}{135}$   
 $+6.3$   $+9.0$   $+13.5$

2+30 1.8 683.6 678.8

$\frac{687.1}{10}$   $\frac{688.1}{20}$   $\frac{692.5}{30}$   $\frac{696.8}{40}$   $\frac{698.8}{42.2}$   
 $+10.5$   $+1.5$   $+9.2$   $+13.2$   $+13.2$

$\frac{674.9}{10}$   $\frac{670.4}{20}$   $\frac{663.6}{27}$   $\frac{663.2}{30}$   $\frac{670.6}{40}$   $\frac{672.5}{50}$   
 $-8.7$   $-13.2$   $-15.0$   $-13.4$   $-13.0$   $-10.1$

$\frac{703.1}{53.2}$   $\frac{705.0}{60}$   $\frac{705.4}{62.1}$   $\frac{711.2}{69}$   $\frac{712.2}{71.6}$   
 $+19.5$   $+21.9$   $+21.8$   $+36.6$   $+21.6$

$\frac{676.7}{60}$   $\frac{680.6}{70}$   $\frac{683.1}{80}$   $\frac{686.1}{90}$   $\frac{689.9}{100}$   
 $-6.9$   $-3.0$   $-0.5$   $+2.5$   $+5.3$

$\frac{719.5}{80}$   $\frac{716.4}{90}$   $\frac{717.0}{105}$   
 $+29.9$   $+31.8$   $+33.4$

$\frac{691.8}{110}$   $\frac{691.5}{120}$   $\frac{696.9}{135}$   
 $+8.2$   $+16.9$   $+13.3$

2+40 9.0 683.4 674.6

$\frac{680.0}{10}$   $\frac{684.9}{20}$   $\frac{688.6}{30}$   $\frac{691.5}{40}$   $\frac{696.4}{50}$   
 $-3.6$   $+1.3$   $+5.1$   $+8.2$   $+12.8$

$\frac{671.2}{10}$   $\frac{667.9}{20}$   $\frac{666.7}{27}$   $\frac{666.9}{30}$   $\frac{669.6}{40}$   $\frac{672.1}{50}$   
 $-12.9$   $-15.8$   $-16.9$   $-16.7$   $-14.0$   $-11.5$

$\frac{712.4}{58.8}$   $\frac{712.8}{67.7}$   $\frac{712.8}{66}$   $\frac{713.0}{70.6}$   
 $+18.8$   $+19.2$   $+21.2$   $+24.4$

$\frac{675.9}{60}$   $\frac{679.4}{70}$   $\frac{681.8}{80}$   $\frac{686.0}{90}$   $\frac{689.8}{100}$   
 $-7.7$   $-4.2$   $-1.8$   $+2.4$   $+5.4$

$\frac{711.9}{80}$   $\frac{712.4}{90}$   $\frac{717.1}{105}$   
 $+27.3$   $+28.8$   $+33.5$

$\frac{691.6}{110}$   $\frac{693.8}{120}$   $\frac{697.1}{135}$   
 $+8.0$   $+10.2$   $+13.5$



Proposed Saludad Res  
Grid Sections

2+50      4.6      674.5      669.9

2+60           674.5      668.0

2+70      4.8      668.7      663.9

West  
Williams  
Varanfokis  
Kellhofer      11-3-55

$\begin{array}{r} 676.0 \\ +1.5 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 670.7 \\ +5.8 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 684.3 \\ +9.8 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 686.9 \\ +18.1 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 691.2 \\ +16.7 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 666.2 \\ -8.3 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 663.4 \\ -14.1 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 660.7 \\ -13.8 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 664.6 \\ -9.9 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 668.9 \\ -6.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 701.2 \\ +26.7 \\ \hline 60 \end{array}$ 
 $\begin{array}{r} 707.1 \\ +32.6 \\ \hline 70 \end{array}$ 
 $\begin{array}{r} 708.1 \\ +33.6 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 710.7 \\ +36.2 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 672.7 \\ -1.8 \\ \hline 60 \end{array}$ 
 $\begin{array}{r} 673.6 \\ +1.9 \\ \hline 70 \end{array}$ 
 $\begin{array}{r} 682.3 \\ +7.8 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 686.5 \\ +4.0 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 686.6 \\ +14.1 \\ \hline 100 \end{array}$

$\begin{array}{r} 714.2 \\ +37.7 \\ \hline 105 \end{array}$ 
 $\begin{array}{r} 691.0 \\ +16.5 \\ \hline 110 \end{array}$ 
 $\begin{array}{r} 692.6 \\ +18.1 \\ \hline 120 \end{array}$ 
 $\begin{array}{r} 696.6 \\ +22.1 \\ \hline 130 \end{array}$

$\begin{array}{r} 691.7 \\ -2.8 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 694.7 \\ +0.8 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 698.5 \\ +3.8 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 663.0 \\ -11.5 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 657.4 \\ -15.1 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 662.9 \\ -10.6 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 666.5 \\ -8.0 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 671.4 \\ -3.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 685.3 \\ +10.8 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 691.4 \\ +16.9 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 702.5 \\ +28.8 \\ \hline 70 \end{array}$ 
 $\begin{array}{r} 675.5 \\ +1.0 \\ \hline 60 \end{array}$ 
 $\begin{array}{r} 677.1 \\ +9.6 \\ \hline 70 \end{array}$ 
 $\begin{array}{r} 683.1 \\ +8.6 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 685.8 \\ +11.3 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 689.0 \\ +12.5 \\ \hline 100 \end{array}$

$\begin{array}{r} 705.7 \\ +31.8 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 707.5 \\ +32.8 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 708.0 \\ +33.5 \\ \hline 105 \end{array}$ 
 $\begin{array}{r} 690.8 \\ +16.3 \\ \hline 110 \end{array}$ 
 $\begin{array}{r} 697.6 \\ +19.1 \\ \hline 120 \end{array}$ 
 $\begin{array}{r} 696.1 \\ +21.6 \\ \hline 130 \end{array}$

$\begin{array}{r} 666.9 \\ -1.8 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 670.7 \\ +2.0 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 676.7 \\ +8.0 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 680.8 \\ +12.1 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 660.7 \\ -8.0 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 656.9 \\ -12.0 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 664.7 \\ -4.0 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 668.4 \\ -0.3 \\ \hline 40 \end{array}$ 
 $\begin{array}{r} 671.8 \\ +3.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 684.2 \\ +15.5 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 688.9 \\ +20.2 \\ \hline 60 \end{array}$ 
 $\begin{array}{r} 700.3 \\ +31.6 \\ \hline 71.5 \end{array}$ 
 $\begin{array}{r} 702.5 \\ +33.8 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 675.7 \\ +7.0 \\ \hline 60 \end{array}$ 
 $\begin{array}{r} 677.1 \\ +10.4 \\ \hline 70 \end{array}$ 
 $\begin{array}{r} 683.7 \\ +14.6 \\ \hline 80 \end{array}$ 
 $\begin{array}{r} 685.4 \\ +16.7 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 685.3 \\ +19.6 \\ \hline 100 \end{array}$

$\begin{array}{r} 704.1 \\ +35.4 \\ \hline 90 \end{array}$ 
 $\begin{array}{r} 705.2 \\ +36.5 \\ \hline 105 \end{array}$ 
 $\begin{array}{r} 691.1 \\ +22.4 \\ \hline 110 \end{array}$ 
 $\begin{array}{r} 697.4 \\ +25.1 \\ \hline 120 \end{array}$ 
 $\begin{array}{r} 697.5 \\ +29.8 \\ \hline 135 \end{array}$



2+80 5.1 665.5 660.4

<sup>662.8</sup> -2.7 10	<sup>667.4</sup> +2.0 20	<sup>672.8</sup> +2.3 30	<sup>676.7</sup> +1.2 40	<sup>680.9</sup> +1.4 50	<sup>657.0</sup> -3.5 10	<sup>655.0</sup> -1.5 15	<sup>PK</sup> <sup>658.2</sup> -2.3 20	<sup>663.3</sup> -2.2 30	<sup>667.5</sup> +2.0 40
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<sup>685.1</sup> +1.6 60	<sup>693.7</sup> +3.2 79	<sup>700.8</sup> +3.3 90	<sup>701.2</sup> +3.7 105	<sup>671.7</sup> +6.2 50	<sup>675.7</sup> +10.2 60	<sup>679.0</sup> +3.5 70	<sup>683.1</sup> +17.6 80	<sup>685.5</sup> +20.0 90
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<sup>688.5</sup> +23.0 100	<sup>691.2</sup> +25.7 110	<sup>694.0</sup> +28.5 120	<sup>697.2</sup> +31.7 135
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2+90 7.2 665.5 658.3

<sup>665.9</sup> +3.1 30	<sup>672.5</sup> +1.2 40	<sup>676.7</sup> +1.2 50	<sup>677.8</sup> +1.3 54	<sup>652.6</sup> -12.9 10	<sup>658.6</sup> -6.9 20	<sup>662.9</sup> -2.6 30	<sup>667.7</sup> +2.2 40	<sup>671.7</sup> +6.2 50
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<sup>696.4</sup> +20.2 81.5	<sup>697.7</sup> +32.2 90	<sup>695.2</sup> +29.7 105	<sup>675.5</sup> +10.0 60	<sup>679.3</sup> +13.8 70	<sup>682.4</sup> +16.9 80	<sup>685.3</sup> +19.8 90	<sup>688.3</sup> +22.8 100
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<sup>690.5</sup> +23.0 110	<sup>693.8</sup> +28.3 120	<sup>697.1</sup> +31.6 135
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3+00 1.6 658.6 654.0

<sup>675.5</sup> -3.1 10	<sup>679.5</sup> +0.9 20	<sup>682</sup> +1.6 30	<sup>662</sup> +2.6 40	<sup>670.5</sup> +1.9 50	<sup>650.0</sup> -8.6 9	<sup>657.1</sup> -1.5 20	<sup>661.8</sup> +3.2 30	<sup>667.1</sup> +8.5 40	<sup>671.9</sup> +13.9 50
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<sup>675.6</sup> +1.0 60	<sup>679.8</sup> +2.2 70	<sup>683.6</sup> +2.0 80	<sup>686.4</sup> +2.8 85.5	<sup>675.1</sup> +16.5 60	<sup>678.8</sup> +20.2 70	<sup>682</sup> +23.6 80	<sup>687.2</sup> +26.6 90
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<sup>674.5</sup> +35.9 91	<sup>691.9</sup> +33.3 105	<sup>671.6</sup> +29.0 100	<sup>690.0</sup> +31.4 110	<sup>692.7</sup> +34.1 120	<sup>695.9</sup> +37.3 135
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Extended Grid Sections

0+00 to 1+50 75' N to 105' L+

12.68 730.78 718.10

13.03 743.49 0.32 730.46

0+00

0+10

0+20

0+30

0+40

0+50

0+60

0+70

West  
Williams  
Varonfakis †  
Kellhofer X

30

11-4-55

"X" Hub on E of Grid sections page 11

737.0  
6.5  
10  
739.3  
1.2  
20  
741.7  
1.8  
30

735.7  
7.8  
10  
738.8  
5.3  
20  
740.0  
3.5  
30

732.8  
10.7  
10  
736.4  
7.1  
20  
738.8  
4.7  
30

727.6  
15.9  
1  
730.8  
12.7  
10  
735.4  
8.1  
20  
738.9  
4.6  
30

731.8  
11.7  
10  
735.3  
8.2  
20  
737.9  
5.6  
30

732.9  
10.6  
10  
735.6  
7.9  
20  
737.7  
5.8  
30

732.7  
10.8  
10  
735.5  
8.0  
20  
737.5  
6.0  
30

732.6  
10.9  
10  
735.5  
8.9  
20  
736.7  
6.8  
30



743.49

0+80

0+90

1+00

1+10

1+20

1+30

1+40

1+50

0.19 731.14 12.5A 730.95

13.01 718.13 = 718.10

<sup>732.3</sup> 11.2 10	<sup>734.6</sup> 8.9 20	<sup>736.3</sup> 7.2 30
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<sup>731.9</sup> 11.6 10	<sup>733.7</sup> 10.2 20	<sup>735.1</sup> 8.4 30
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<sup>730.4</sup> 13.1 10	<sup>731.9</sup> 11.6 20	<sup>733.8</sup> 9.7 30
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<sup>729.1</sup> 13.8 10	<sup>731.1</sup> 12.4 20	<sup>733.4</sup> 10.1 30
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<sup>728.9</sup> 14.6 10	<sup>730.9</sup> 12.1 20	<sup>733.3</sup> 10.2 30
--------------------------------	--------------------------------	--------------------------------

<sup>728.2</sup> 15.3 10	<sup>730.9</sup> 12.6 20	<sup>732.7</sup> 10.8 30
--------------------------------	--------------------------------	--------------------------------

<sup>727.8</sup> 15.7 10	<sup>730.0</sup> 13.5 20	<sup>731.8</sup> 11.7 30
--------------------------------	--------------------------------	--------------------------------

<sup>729.2</sup> 16.3 10	<sup>729.2</sup> 14.3 20	<sup>731.2</sup> 12.9 30
--------------------------------	--------------------------------	--------------------------------



Topo survey in Pueblo lot 1290  
For Standpipe site

B.M.	0.79	372.27		371.48
T.P.	0.48	361.19	11.56	360.71
T.P.	0.91	351.92	10.18	351.01
T.P.	7.01	352.92	6.01	345.91
T.P.	2.21	349.22	5.91	347.01
T.P.	2.84	347.65	4.41	344.81
T.P.	1.64	343.94	5.35	342.30
T.P.	6.50	341.81	8.63	335.31
T.P.	5.42	343.89	3.34	338.47
T.P.	4.02	339.78	8.13	335.76
T.P.	4.36	337.83	6.31	333.47
T.P.	7.13	337.76	7.20	330.63
			7.35	
B.M.			7.16	330.60 = 330.81
			6.01	
T.P.	6.20	343.78	0.18	337.58
T.P.	6.20	346.72	3.26	340.52
T.P.	6.50	349.77	3.45	343.27
T.P.	2.72	348.79	3.70	346.07

WEST  
WILLIAMS T  
VARONFAKIS T  
KELLHOFER

32

PARTLY CLOUDY + WINDY  
2/21/56

#91134 (SECOND CLAIRMONT AREA)  
SPIKE IN P.P. N.W. COR. TANK AREA

RETURN ON CLAIRMONT MESA  
S.E. COR COR DISC CLAIRMONT MESA + MOREGA  
RETURN ON MOREGA  
S.E. COR COR DISC CLAIRMONT MESA + MOREGA  
RETURN ON MOREGA  
S.W. COR COR DISC CLAIRMONT MESA + MOREGA  
RETURN ON CLAIRMONT MESA  
S.W. COR COR DISC CLAIRMONT MESA + MOREGA



2/21/56

	348.79		
T.P.	5.14	345.44	8.49 340.30
T.P.	4.78	343.85	6.37 339.07
T.P.	7.17	349.40	1.62 342.23
T.B.M.	0.20	347.99	1.61 347.79
T.P.	4.77	343.95	8.81 339.18
T.P.	4.04	346.04	1.95 342.00
T.P.	7.59	349.13	4.50 341.54
T.P.	2.52	350.71	0.94 348.19
T.P.	5.10	348.99	6.82 343.89
T.P.	5.34	345.59	8.74 340.25
T.P.	2.77	342.94	5.42 340.17
T.P.	3.66	336.45	10.15 332.79
CHECK			
B.M			5.85 330.60 = 330.81

REF 8107 S.E. COR. ENO  
2" PIPE PUEBLO LOT LINE 1240 GALLATIN WAY

RETURN ON MORAGA PAGE 32  
S.W. COR. COR. DISC. CLAIRMONT MESA + MORAGA

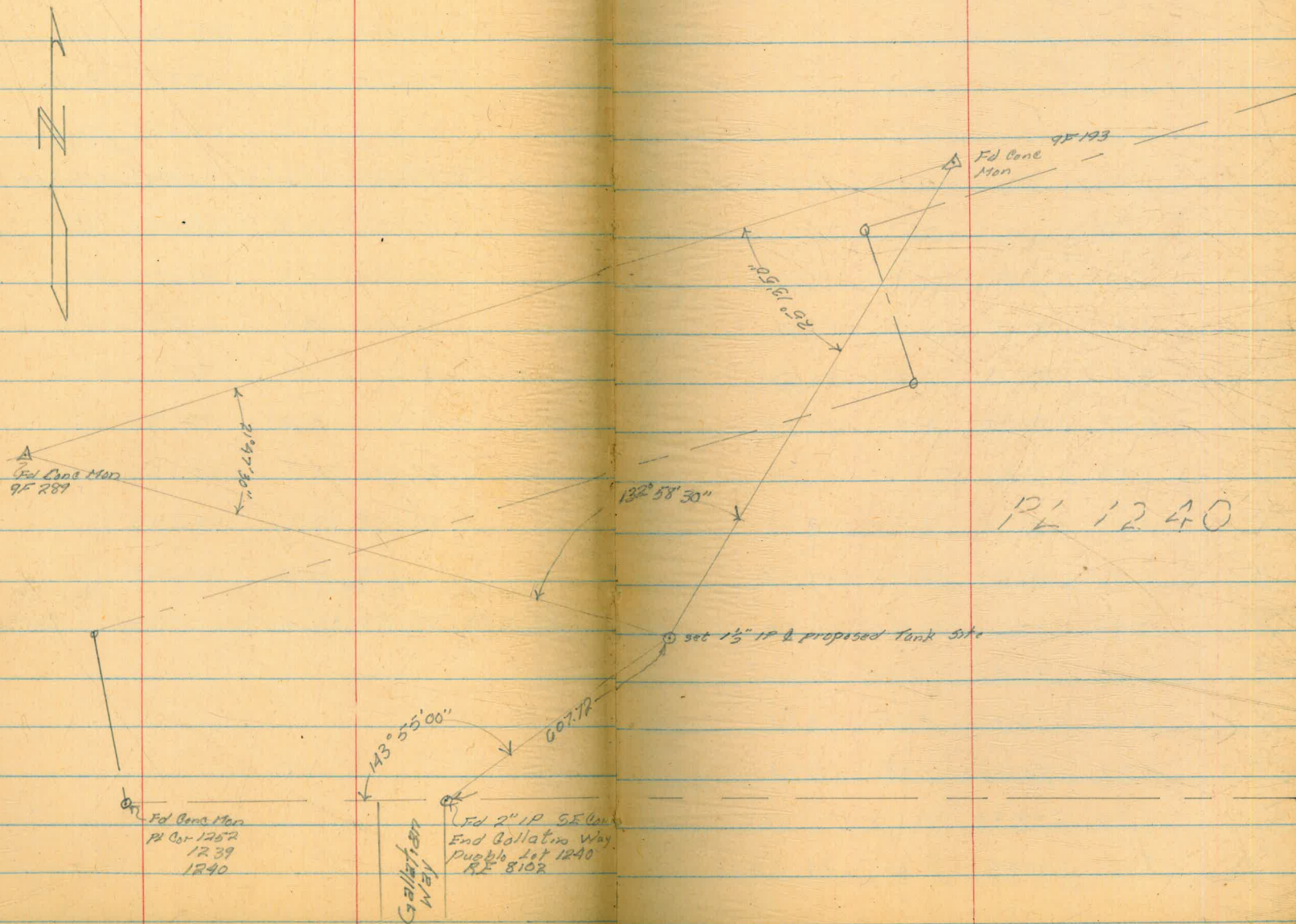


Topo Survey Standpipe Site  
Ties to PL 1240

West  
Williams  
Varonakis  
Kellhofer

34

2/22/56





GK. LEVELS  
 COUNTRY CLUB RESERVOIR TO  
 PROPOSED SOLEDAD STANDPIPE

Aug 30 1956  
 Williams  
 Kalkofer  
 Paulson

35

See NOTE Pg. 50

BM	131	722.41	721.10	←
		3.16	719.25	✓ -
		2.23	720.18	-
		2.18	720.23	-
		0.95	721.46 = 721.45	*

Top 4" PIPE USC&GS Δ "TANK" 1933 on  
 Ely side of Res. outside cyclone fence  
 On conc. lip of spillway NELY cor. of RES.  
 on conc. curb of Res. Nly end.  
 on conc. curb of Res Sly end.  
 Top 4" pipe USC&GS Δ → RR TANK #1 on  
 Wly side of Res. outside fence

T.P.	0.15	710.00	12.56	709.85
T.P.	0.45	697.55	12.90	697.10
T.P.	3.66	688.15	13.06	684.49
T.P.	2.02	684.80	5.37	682.78
T.P.	0.08	671.86	13.02	671.78
T.P.	0.07	658.72	13.21	658.65
T.P.	0.21	645.69	13.24	645.48
T.P.	5.54	638.26	12.97	632.72
T.P.	13.00	651.22	0.04	638.22
T.P.	13.10	663.90	0.42	650.80
T.P.	11.67	675.49	0.08	663.82
T.P.	12.92	688.38	0.03	675.46
T.P.	13.17	701.45	0.10	688.28



CK. LEVELS CONT.

SAME PARTY

35.

8/30/56

		701.45			
T.P.	11.67	712.49	0.63	700.82	
T.P.	8.69	716.88	4.30	708.19	
CHECK B.M.			4.60	712.28 = <del>712.64</del> 712.25	
BM.	5.65	717.93		712.29	
IP rock	10.47	728.33	0.07	717.86	
IP rock	13.23	740.76	0.80	727.53	
IP rock	7.29	747.76	0.29	740.47	
Set TBM	11.65	756.45	2.96	744.80	
IP rock	6.95	754.03	9.37	747.08	
Set TBM	3.99	755.93	2.09	751.94	
Set TBM	2.08	749.35	8.66	747.27 (747.9) see below	
IP rock	1.00	737.73	12.62	736.73	
IP rock	0.98	726.04	12.62	725.06	
IP rock	4.98	719.30	11.72	714.32	
CK TBM.	10.27	717.40	12.17	707.13 = 708.49	
IP	2.02	716.90	2.52	714.88	
			13.24	703.66	
CK Elev. & proposed tank			11.52	705.38 = 705.31 705.95	
IP	13.03	718.41		705.38	

CIVIL DEFENSE BLDG. F.B. 756 -42  
CHISEL + CON PLATFORM So. SIDE BLDG. 12' W OF BLOWER

9/7/56 Betty Paulson

Nail in P.P. # 61704 SW intersection of Soledad Rd Hillside Dr. & Road to Easter Cross

E of road E.C. Hub (127+8100)

Nail in Tele pole # 511258 H. (100' Nly & proposed tank)

BC 119+06.3 (see pg. 2) 2x2 Hub

= gnr location #1 pg. 2

= gnr & proposed tank (pg. 12)

(C-11-12 pg. 19)

See Note pg. 50



718.41

TP 12.83 731.01 0.23 718.18 = 718.10 ginc (see pg. 11)

TP 12.29 741.65 1.65 729.36

TP 9.65 750.47 0.83 740.82

OK TBM

3.21 747.26 = 747.27

747.91

Not in Tele pole # 51258 H. pg. 35















Abermarle ST  
Morningside Dr To Flintridge

STKS for 6" AC Main

	4.12	186.49	182.37
	12.95	199.20	02186.75
	3.87	202.74	033198.87
0+15		0.7	202.01
+20		0.7	202.0 199.0
+50	Actual	1.7	201.0 197.7
1+00		3.8	198.9 195.4
+50		6.6	196.1 193.0
2+00		10.5	192.2 189.1
TD	0.29	190.41	1262 190.12
+50		2.1	188.3 185.5
3+00		5.6	184.8 181.7
+34.6		7.7	182.7

Flintridge St Abermarle To  
190.41

0+20	(A)	7.4	183.0
+25	(B)	7.3	183.1 179.1
+50	Actually 0+45	7.4	183.0 179.7
1+00	0+95	6.1	184.3 181.4

Field  
CHK  
Best  
7-2-57

West  
Williams X  
Kellhofer P

40

HOT  
9/4/56

SW BR Abermarle & Hopkins

C TO EXISTING	202.7	0
Begin Work	0.5	202.2
C3 $\frac{0}{\pm}$	0.5	202.2
C3 $\frac{3}{-}$	1.9	201.3
C3 $\frac{5}{-}$	3.5	199.2
C3 $\frac{1}{-}$	6.4	196.3
C3 $\frac{1}{-}$	10.2	192.5
		190.41
C2 $\frac{8}{-}$	1.9	188.5
C3 $\frac{1}{-}$	5.6	184.8
C TO EXISTING		
End of work Tee	7.6	182.8

Palomero

C TO EXISTING	190.4	
Begin Work	7.5	182.9
C4 $\frac{0}{-}$	7.5	182.9
C3 $\frac{3}{-}$	7.5	182.9
C2 $\frac{9}{-}$	6.1	184.3



Elmridge Dr. Abermarle St To Potomac

West  
Williams  
Kellhofer

41

190.41

9/4/56

~~7+50~~ ③ 1+45 4.2 186.2 183.0

C3 <sup>2</sup>

4.2 186.2

5.64 192.70 3.35 187.06

~~7+00~~ 1+95 4.0 188.7 185.2

C3 <sup>5</sup>

192.70

4.0 188.7

~~750~~ 2+45 1.6 191.1 187.4

C3 <sup>7</sup>

1.6 191.1

~~775~~ 2+70 1.5 191.2 187.4

C3 <sup>8</sup>

1.5 191.2

~~7700~~ 2+95 2.0 190.7 186.6

C4 <sup>1</sup>

2.0 190.7

~~750~~ 3+45 3.7 189.0 184.8

C4 <sup>2</sup>

3.7 189.0

~~765~~ 3+59.5 4.3 188.4 184.1

C4 <sup>3</sup>

4.4 188.3

~~7700~~ 3+95 6.1 186.6 182.4

C4 <sup>2</sup>

6.2 186.5

~~750~~ 4+45 8.7 184.0 180.2

C3 <sup>8</sup>

8.7 184.0

~~5700~~ 4+95 11.1 181.6 177.9

C3 <sup>7</sup>

10.6 181.7

0.65 180.81 12.54 180.16

~~750~~ 5+45 1.5 179.3 175.6

C3 <sup>7</sup>

180.8

1.4 179.4

~~6700~~ 5+95 3.7 177.1 173.3

C3 <sup>8</sup>

3.7 177.1

~~750~~ 6+45 5.9 174.9 171.0

C3 <sup>9</sup>

5.7 175.1

~~7965~~ 6.8 174.0

To EXISTING  
Tee End at work

6.9 173.9

TP TAM 11.98 185.99 6.80 174.01

SW BP Potomac + Elmridge St

7.37 192.84 0.50 185.49

0.95 183.52 10.29 182.57

1.16 182.36 = 182.57



GARDENA AVE GARDENA PL.  
5TKs for Lowering (12" AC)  
and Stub Line and moving  
Fire Hyd

West  
Williams &  
Kellhofer &

SUNNY

33H-D 9/6/56  
TBM nail in PP No Number 6 West  
Proposed

C 7 1/2 @ 12" AC 6' NW of Q of 15 Storm Drain  
C 7 1/2 " " " 6' SE " " " " " "

To Vent riser  
C 1 1/2 16' SE of Q Storm Drain  
To Vent riser  
D 1 1/2 5' NW " " " "

	4.50	30.59	26.09
0+00		5.7	24.9 17.5
0+12		5.7	24.9 17.5
for Air valve meter Box		5.4	25.2 24.1
Air Valve meter Box for		5.6	25.0 24.0

			Bottom of Pipe
Top of Pipe	10.27	20.9	-1.0 = 19.4
Q Fire Hyd	6.0	24.6	24.8

STUB Line

on 12" AC pipe			(A) To South
0+00	6.0	24.6	19.5
0+00	6.0	24.6	19.5
+15	5.7	24.9	20.0
+30	5.2	25.4	20.5
+43±	4.8	25.8	21.0
4.88	28.55	6.92	23.67
		4.94	23.61 = 23.60

Top of 12" AC pipe 62' NW of Q Storm Drain  
E 0 2 To Flange C 5 2 To E11

Q of Storm Drain 22 1/2 Bend out of Tee  
C 5 1/2 12" x 6" Tee for Stub 20' West of  
C 5 1/2  
C 4 2  
C 4 2  
C 4 2 End of Stub of prop line

PP # 4637



GARDENA AVE

STUB for future SB

West  
Williams X  
Kellhofer &

42

WARM

3310D

9/6/56

T.B.M. 4.39 30.18

26.09

TBM see p 41

0+00

2.1 28.4 24.3

04'

on E of 12" AC main

0+35

1.0 29.5 24.8

04 1/2

end of stub on prop line

Ck.

T.B.M.

4.39 26.09 = 26.09

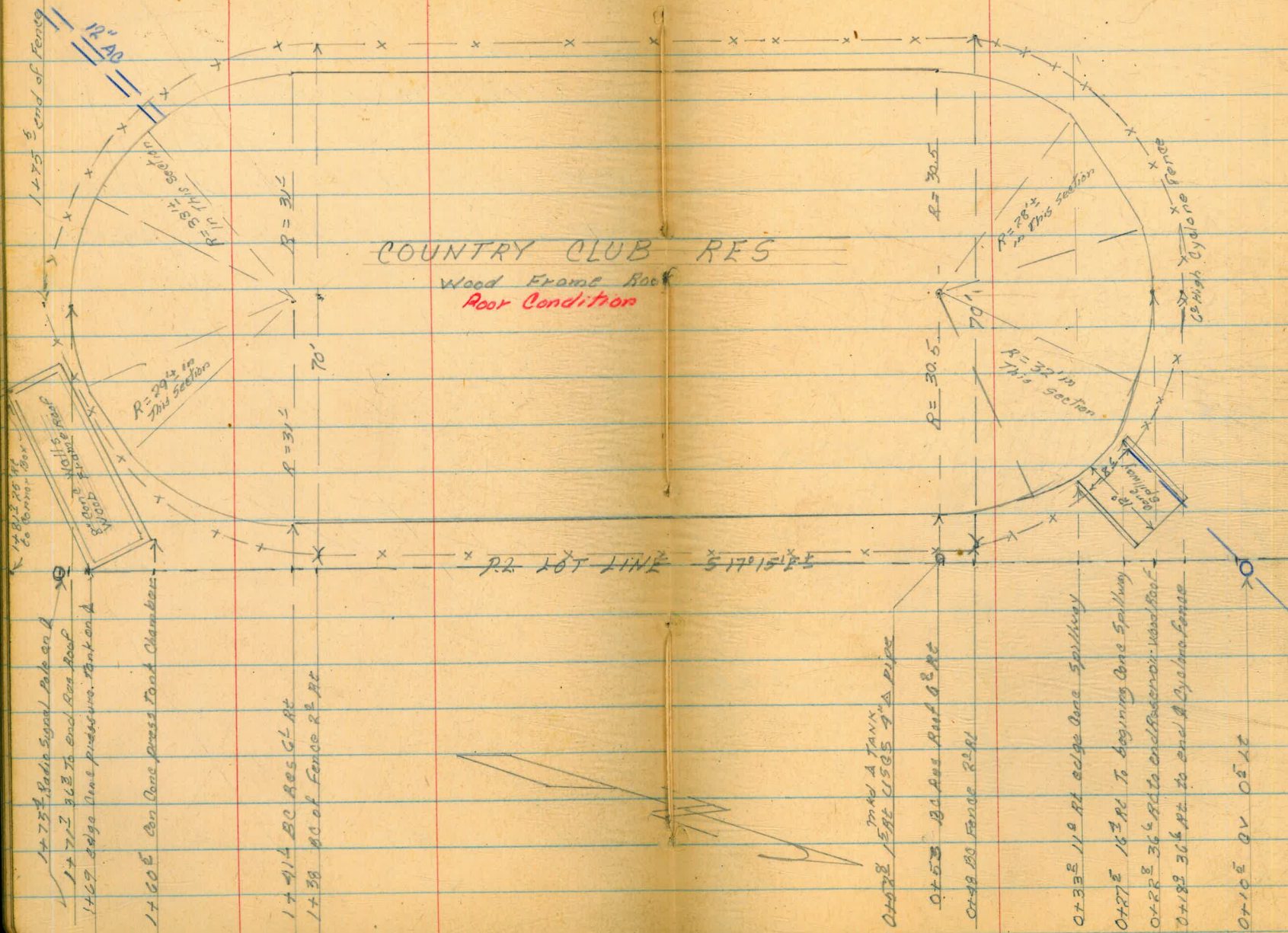


COUNTRY CLUB RESERVOIR

West  
Williams  
Kellhofer

Warren  
9/6/56

43



1+75 Radi Signal Pole on R  
1+77 30' to End Res Roof  
1+69 Selgo One Pressure Tank on A

1+60 Con One Press Tank Chamber

1+41 BC Res G1 Rt  
1+39 BC of Fence R2 Rt

0+53 24 Res Roof G2 Rt  
0+48 BC Fence R2 Rt

0+33 11' Rt edge One Spillway

0+27 16' Rt to beginning One Spillway

0+22 36' Rt to end Reservoir Wood Roof

0+18 36' ft to end of Cyclone fence

0+10 QV O5 Rt

500 Feb 24 1956  
O+100 Feb 24 1956

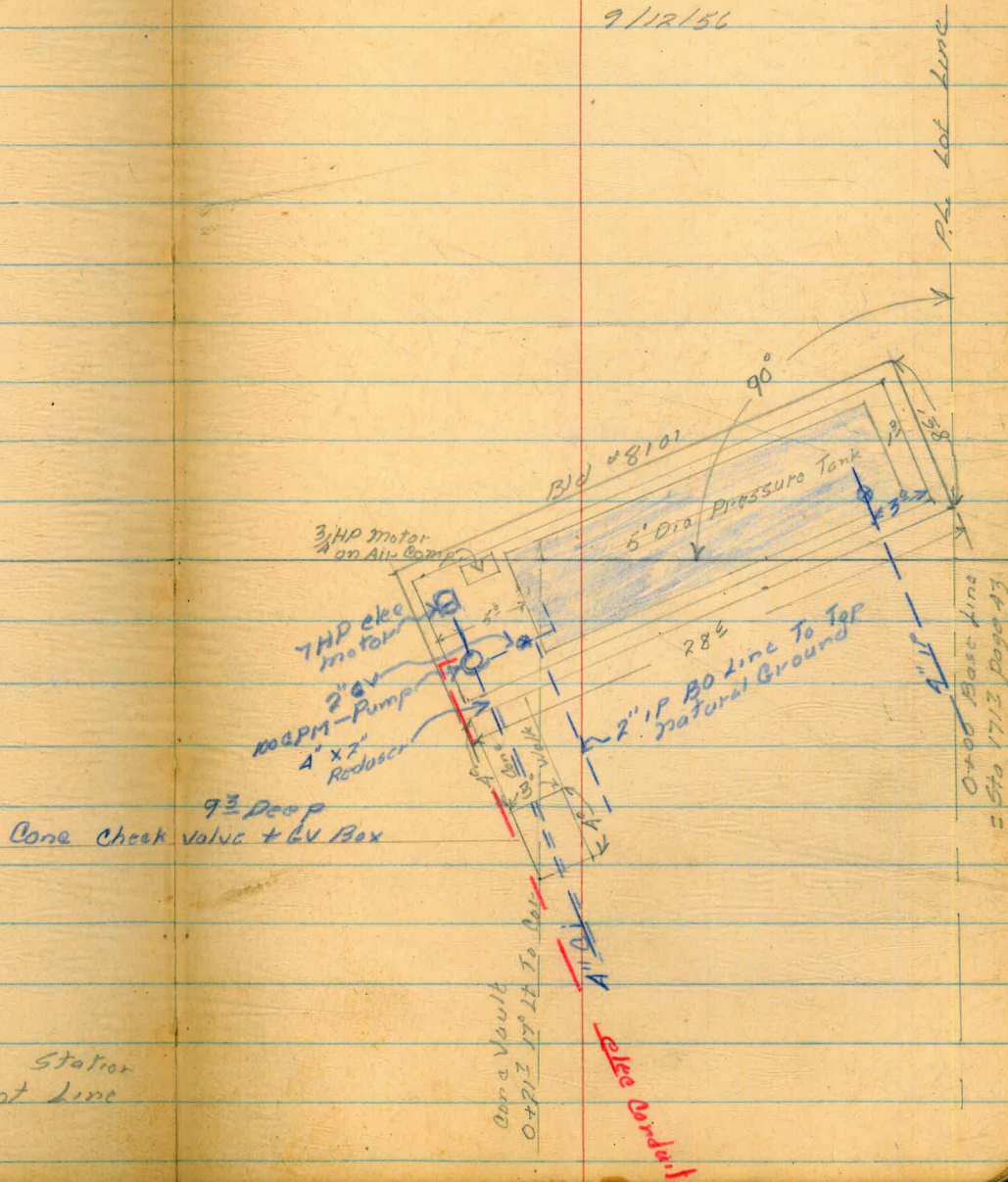


Country Club Reservoir  
 Topo South side

West  
 Williams  
 Kellhofer

44

9/12/56



Station  
 0+00 Base Line = Sta 1712 P.L. Lot Line



Country Club Res  
Cross Sections South Side

	3.91	725.01	721.10	←
0-20			11.6	
0-10			9.7	
0+00			7.4	
0+00 <sup>3</sup>				
0+03 <sup>2</sup>				
0+04 <sup>3</sup>				
0+10			1.79	

West  
Williams  
Kellhofer

45

See NOTE pg. 50

9/12/56

Top 4" U60+05 Δ TANK on Ely side of Res  
 $\frac{12.8}{20' Lt}$        $\frac{10.5}{20' Rt}$

$\frac{11.9}{20' Lt}$

$\frac{8.7}{20' Rt}$

$\frac{10.5}{20' Lt}$

Radio Signal Pole  
15' Lt

$\frac{7.0}{32' Rt}$

$\frac{5.2}{16' Rt}$

$\frac{4.8}{20' Rt}$

$\frac{7.0}{32' Lt}$

edge cone pressure tank around lin

$\frac{5.41}{30' Lt}$

Top " "

$\frac{4.85}{30' Lt}$

" "

Wood Roof " "

$\frac{5.40}{28' Rt}$

+03' To Top 4" pipe from pressure Tank  
Top of cone wall pressure tank chamber

$\frac{5.1}{112' Rt}$

around line at NE Cor pressure Tank Box

$\frac{4.36}{112' Rt}$

Top of Wood Roof

$\frac{4.87}{12' Lt}$

edge Roof

$\frac{6.9}{12' Lt}$

Ground line

$\frac{4.36}{82' Rt}$

edge of Roof

$\frac{4.7}{82' Rt}$

Ground



725.01

0+10

 $\frac{9.5}{20' Lt}$ 

A 02 721.85 718 717.83

 $\frac{11.1}{30' Lt}$ 

0+13

9' Lt to 5" ornamental Tree

19' Lt to 12" Acacia tree

0+20

1.38

on Top of Roof of pressure box

 $\frac{1.65}{7' Lt}$ 

edge of " " " "

 $\frac{4.5}{7' Lt}$ 

Around

 $\frac{6.7}{12' Lt}$ 

Top of Rock wall

 $\frac{2.95}{14' Lt}$ 

Top of Cone Check Valve + Gate box

 $\frac{8.6}{30' Lt}$  $\frac{1.21}{3' Lt}$ 

At edge Top of Roof

 $\frac{1.8}{3' Lt}$ fence line  
Ground line + cyclone

0+26

1.22

Top end of Roof on Q

0+26<sup>1</sup>

1.8

Around Line + cyclone fence King

720.21

 $\frac{1.62}{2' Lt}$ 

At Top Cone Reservoir

 $\frac{0.62}{2' Lt}$ 

Top Wood Roof of Reservoir

 $\frac{2.1}{12' Lt}$ 

To cyclone fence

 $\frac{8.3}{27' Lt}$ 

butt at slope

0+30

2.0



721.85

0+36

14' Lt to 8" Acacia Tree

0+40

0.59

Top Reservoir Roof on A

1.7  
0 Lt Ground1.9  
42 Lt To Cyclone Fence Line9.79  
33' Lt To Edge AC driveway

0+42

4' Lt begin 10' wide Gate in Cyclone fence

1.43 721.58 1.76 720.09

0+50

1.3

1.3  
12 Rt Ground Line at Reservoir0.28  
12 Rt Top of Wood. Roof at Reservoir2.1  
6 Lt Top of Slope

23' Lt 3' High Ornamental Bush

8.40  
26' Lt edge AC driveway

Cyclone Fence Xing

12" AC pipe Xing

0+56<sup>5</sup>0+59<sup>5</sup>



Country Club Res Cont

West  
Williams  
Kellhofer

48

721.52

9/12/56

0+60

2.0

$\frac{1.6}{2.0}$  To Cyclone fence

6" RE To Reservoir Roof

$\frac{7.96}{22.14}$  edge AC Driveway

0+68<sup>5</sup>

QV

11<sup>5</sup> LT

0+70

4.0

$\frac{1.6}{19.84}$  To Cyclone Fence

$\frac{7.25}{16.3}$  LT To edge AC pave

0+72

4<sup>0</sup> LT

To 6" Dia Casahia Tree

0.47 721.05 = 721.10 BM



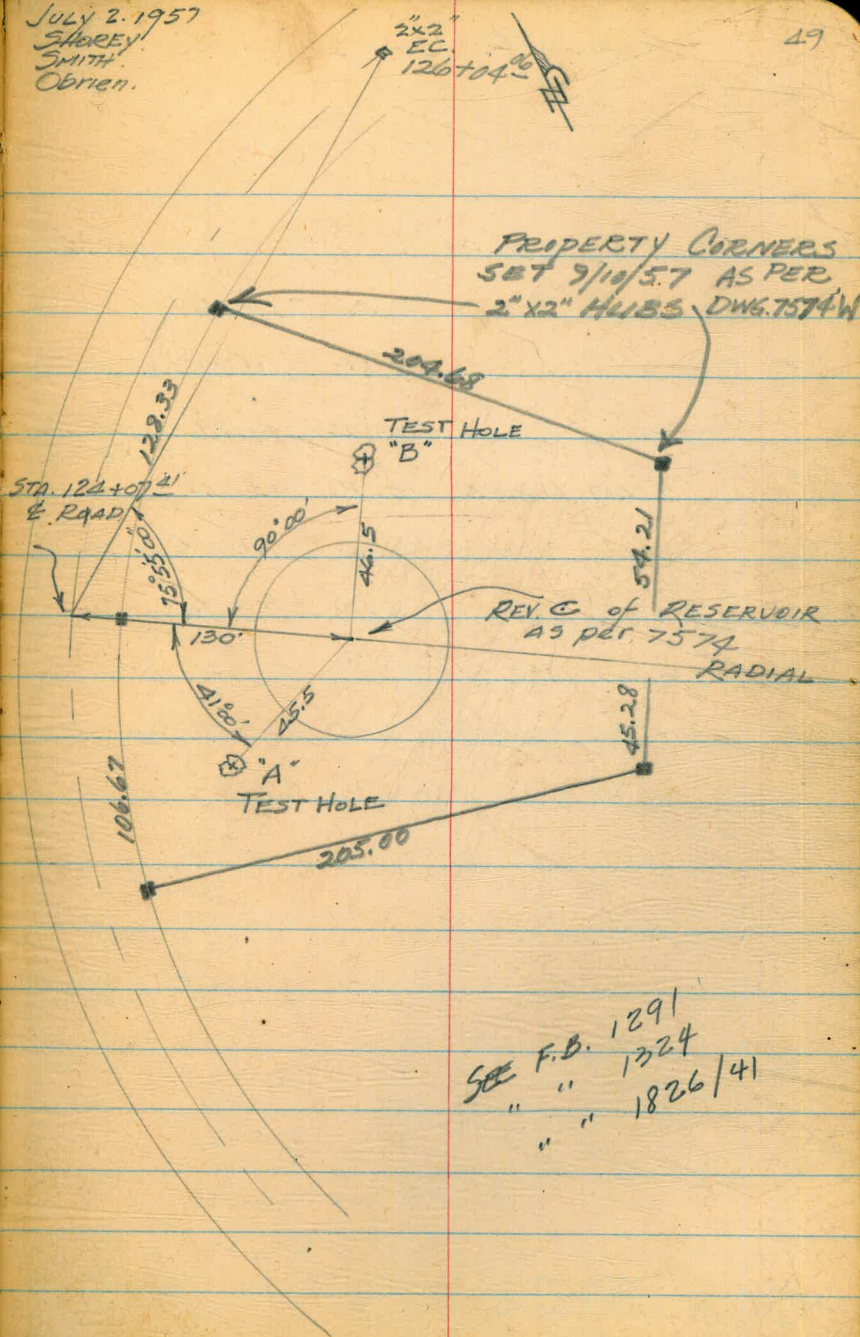
SOLEDAD RESERVOIR  
LOCATION & ELEVATION  
TEST HOLES

See Note  
pg. 50

TP	12.18	717.49	705.31	(09.24)
GROUND @ TEST HOLE "A" 3.83 713.66				
REV. C OF RES. (HUB) 12.30 705.19				
TP	12.85	727.92	2.42	715.07
GROUND @ TEST HOLE "B" 2.86 725.06				
TP	1.29	717.04	12.17	715.75
CK. TP		11.74	705.30 = 705.31	

JULY 2, 1957  
SHOREY  
SMITH  
O'Brien.

49





# COUNTRY CLUB RESERVOIR

JULY 9 1957  
BEATTY  
SMITH

50

BM	3.80	724.90	721.10	(pg. 35)
		3.40	721.46	
		5.69	719.21	
		5.64	719.26 = 719.25	pg. 35
IP	2.40	716.54	10.76	714.14
			2.50	714.04
IP	0.46	704.22	12.78	703.76
IP	0.80	692.13	12.89	691.33
TBM	10.70	695.41	7.42	684.71 =
IP	11.99	707.11	0.29	695.12
IP	10.79	716.84	1.06	706.05
IP	6.06	722.19	0.71	716.13
CK BM			1.10	721.09 = 721.10

Top 4" pipe USC & GS & TANK 1933 E. side  
Top 4" pipe USC & GS RP #1 TANK 1933 W. side  
Brass plate " " RP #2 TANK 1933. <sup>Curb of</sup> overflow  
On conc Lip - overflow of Reservoir  
& shaft centrifugal pump in pump house

Top of FH SE Cor. Romero & Encelia

Top 4" pipe USC & GS & TANK

NOTE: These elevations are in same relative datum as Country Club - Romero DR. pipe, FB 911-68. Subsequent Levels & checks indicate this BM & TANK to be in error. Should be 721.76.

Prelim Levels for Country Club - Romero DR pipeline FB 911-5-25 Corrected 0.77 but for reasons unknown.

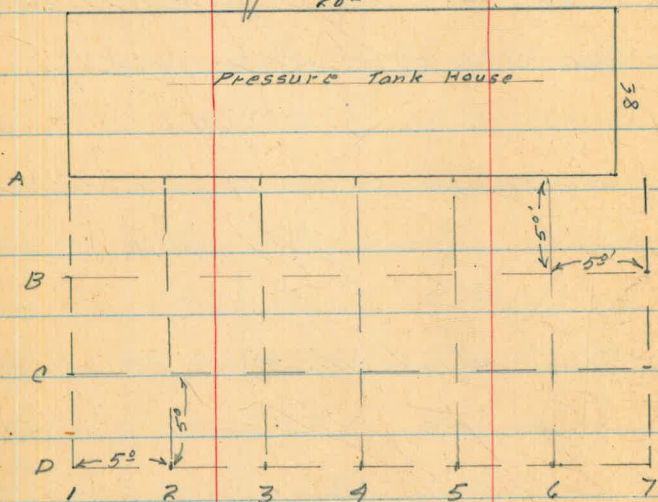
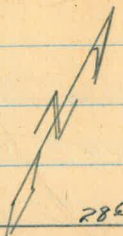
LEVELS in FB 730-1, 67, 68 has error of 0.66 which would make BM & TANK = 721.78  
LEVELS on pg 34-35 from BM & TANK to center proposed SOLEDAD RESERVOIR, checked City Engrs Levels. BUT LEVELS brought up from PAYVERWEE'S show error of 0.64 SH. 19 C-11-12



COUNTRY CLUB RESERVOIR

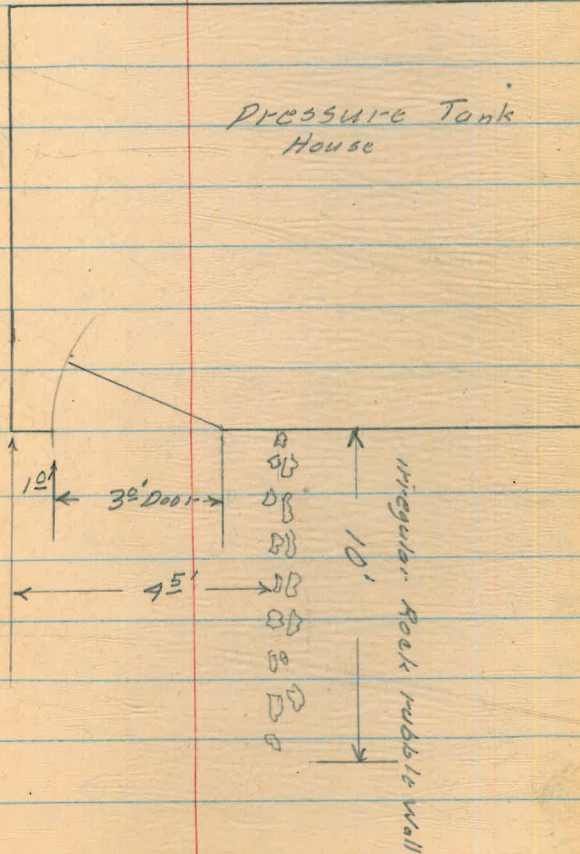
• TOPO

Grid Location and Numbering system



West  
Williams  
O'Brien  
Courtney

11-10-57





COUNTRY CLUB RES  
 TOPO. PRESSURE TANK

OCT. 12 1957  
 WEST  
 WILLIAMS  
 O'BRIEN  
 COURTNEY

52

	HI		
	1.95	723.05	721.10
A 1		6.7	
A-1		9.08	713.97
A 1 45' Towards A2		9.07	
A 2		6.1	
A 3		5.6	
A 4		5.1	
A 5		5.0	
A 6		5.0	
A 7		5.0	
B-1		9.33	
B-2		7.6	
B-3		5.8	
B-4		5.4	
B-5		5.2	
B-6		5.3	
B-7		5.8	
	2.67	718.94	6.78 716.27

Top 4" USG+AS ATANK on ENJ side of Res

Top of Bank SW Cor pressure Tank Chamber

on cone sidewalk to " " "

" " " " " " "

Top of Dirt Slope and Rubble wall

On cone Sidewalk



COUNTRY CLUB RES  
(Cont'd.)

10/4/57

53

718.94

C-1	5.2
C-2	4.2
C-3	2.7
C-4	2.1
C-5	1.8
C-6	2.2

Top of Ground

C-7	2.7
-----	-----

D-1	5.0
-----	-----

D-2	4.4
-----	-----

D-3	4.3
-----	-----

D-4	3.1
-----	-----

D-5	3.2
-----	-----

D-6	3.4
-----	-----

D-7	4.3
-----	-----

7.17	724.13	1.98	716.96
	3.00		721.13 = 721.13

Turn on Ginney

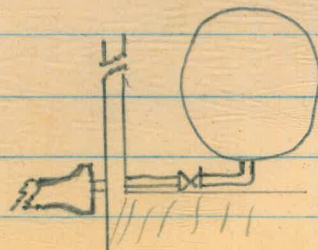
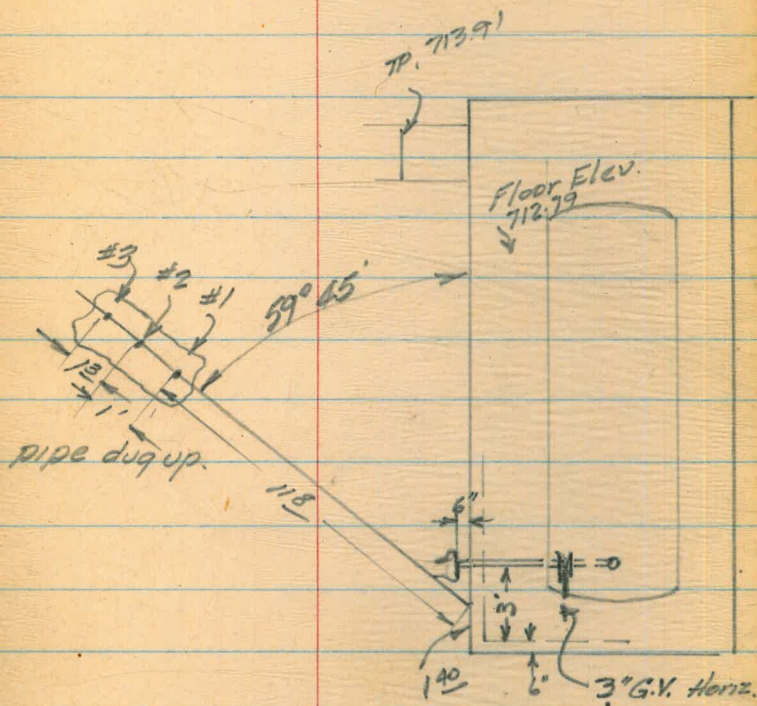


COUNTRY CLUB RES.  
(Cont'd)

OCT. 14 1957  
BEATTY  
COURTNEY

54

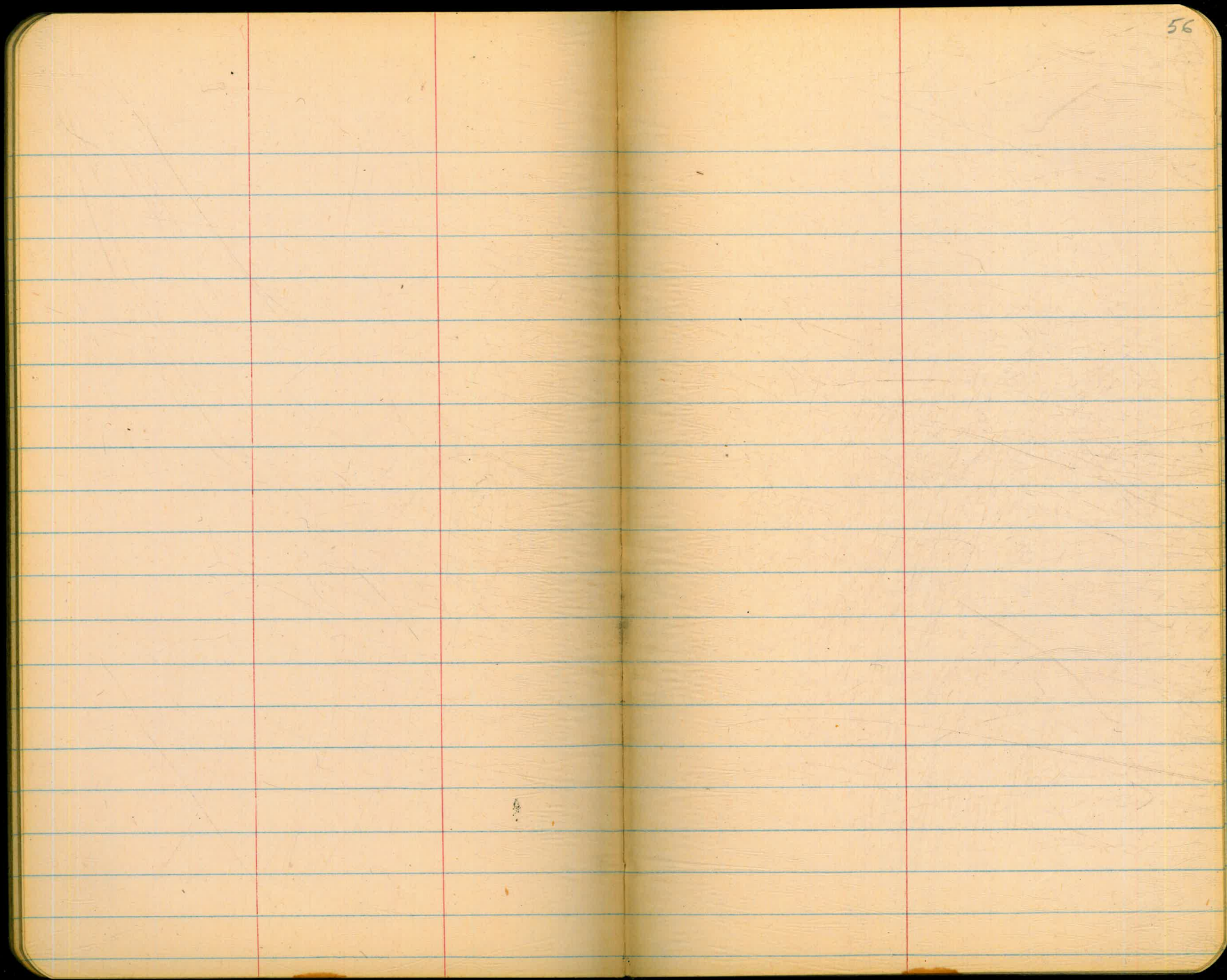
BM	1.23	722.33	721.10	
GRD Line		5.5	716.8	
#1 Top 6" C.I. Pipe	10.26	712.07		
#2 " " " "	10.36	711.97		
#3 " " " "	10.50	711.83		
TP	4.56	718.47	8.42	713.91
				COR Sidewalk
Floor Elev		5.68	712.79	
P	7.58	721.09	4.56	713.91
CK BM		0.39	721.10	











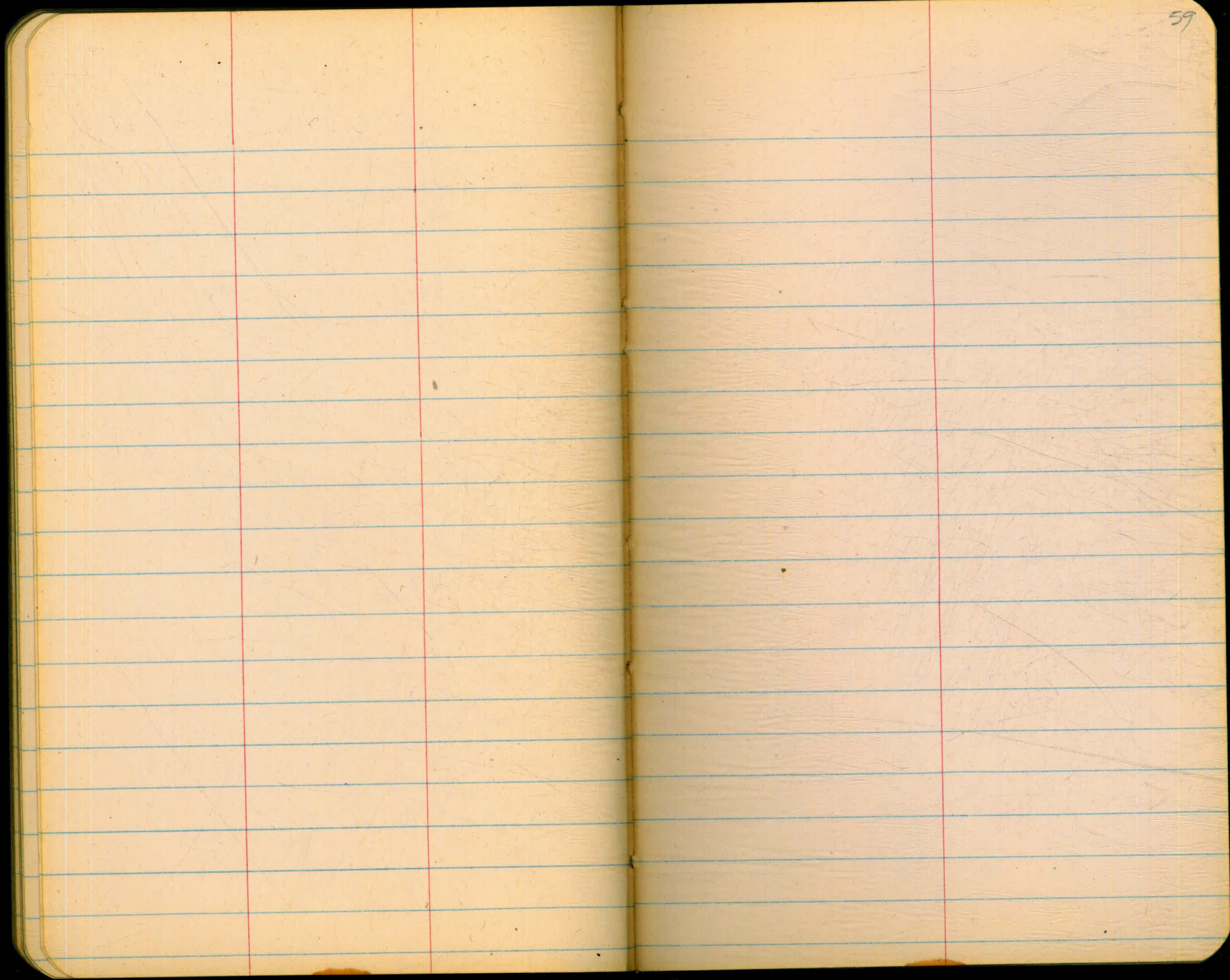




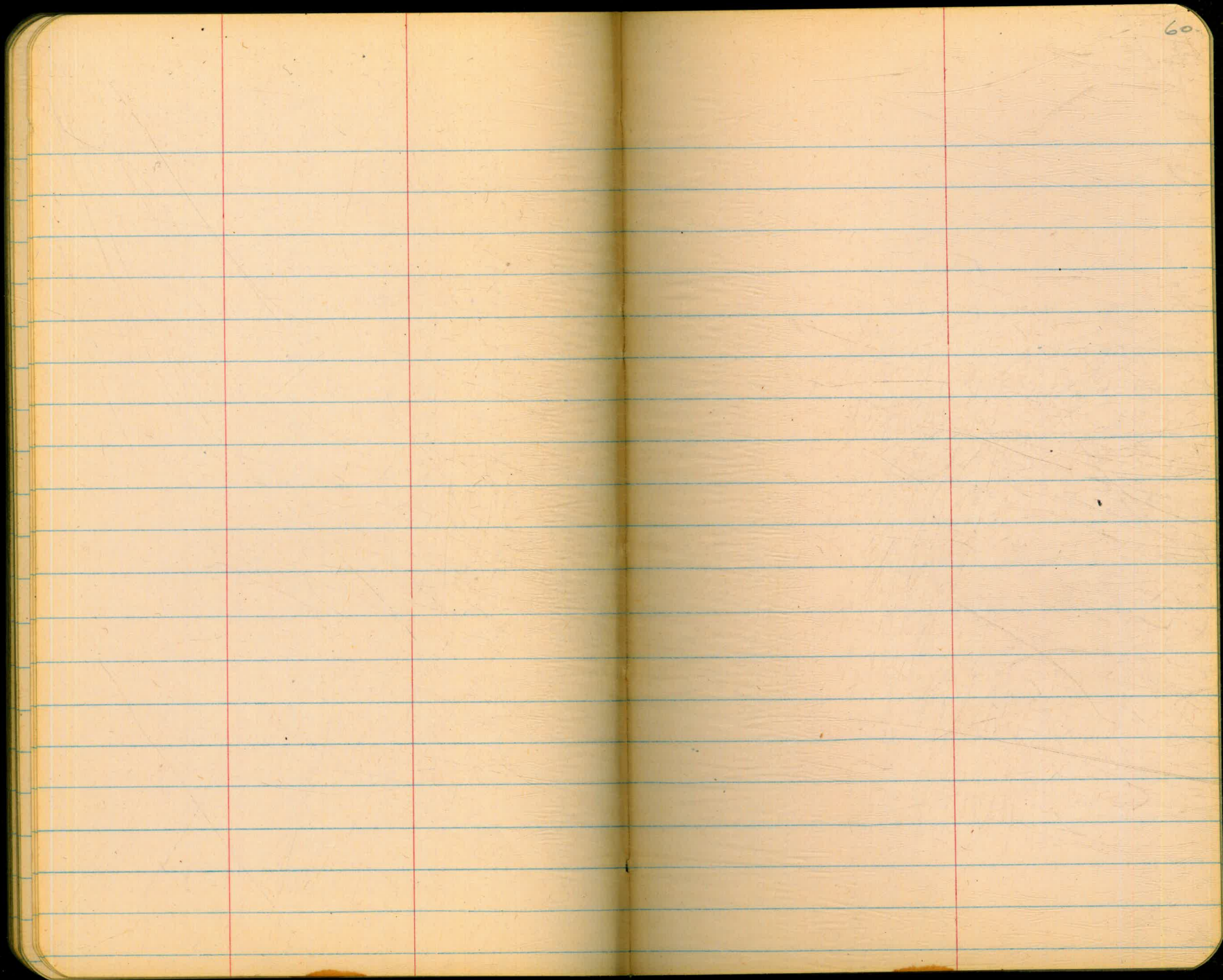




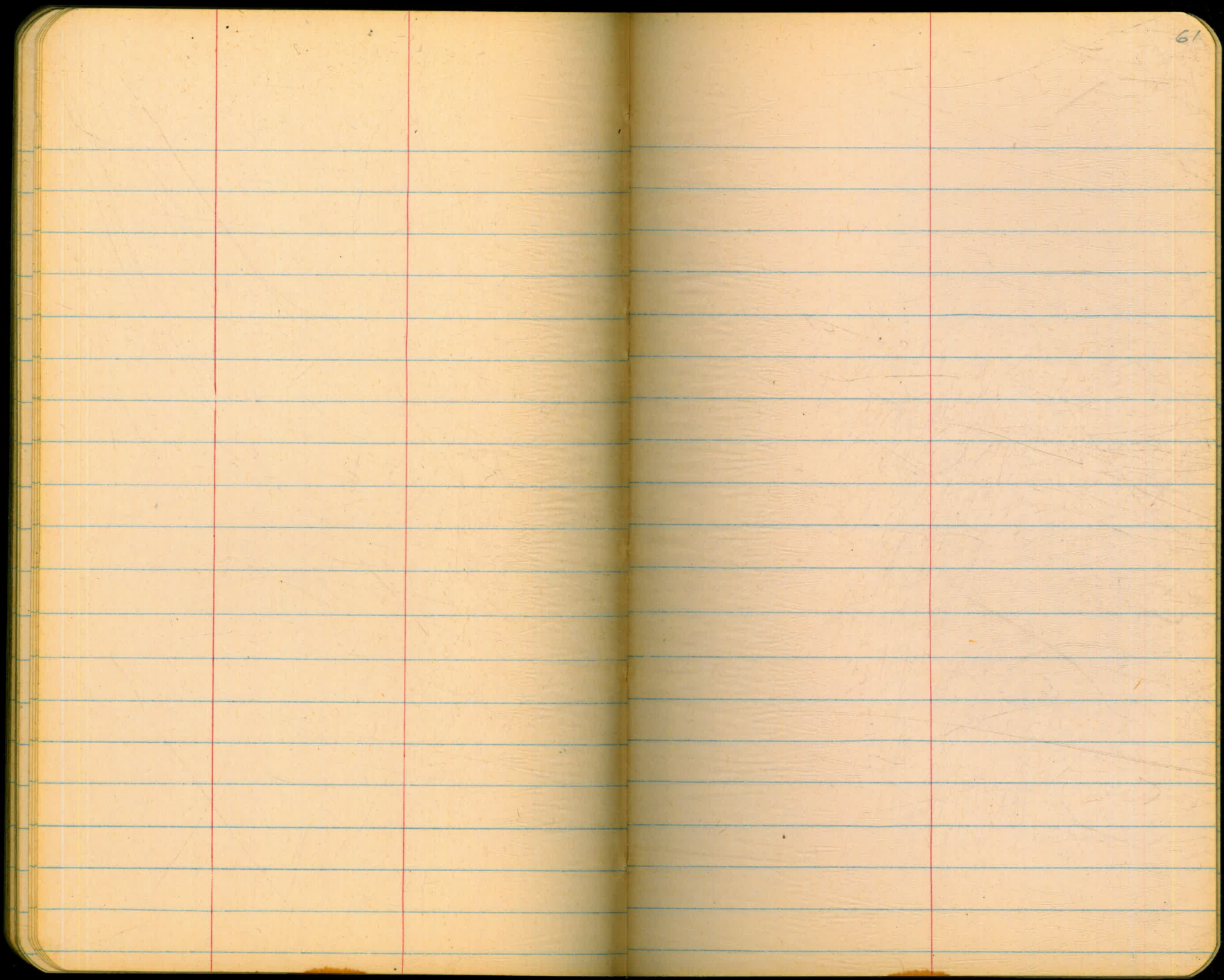








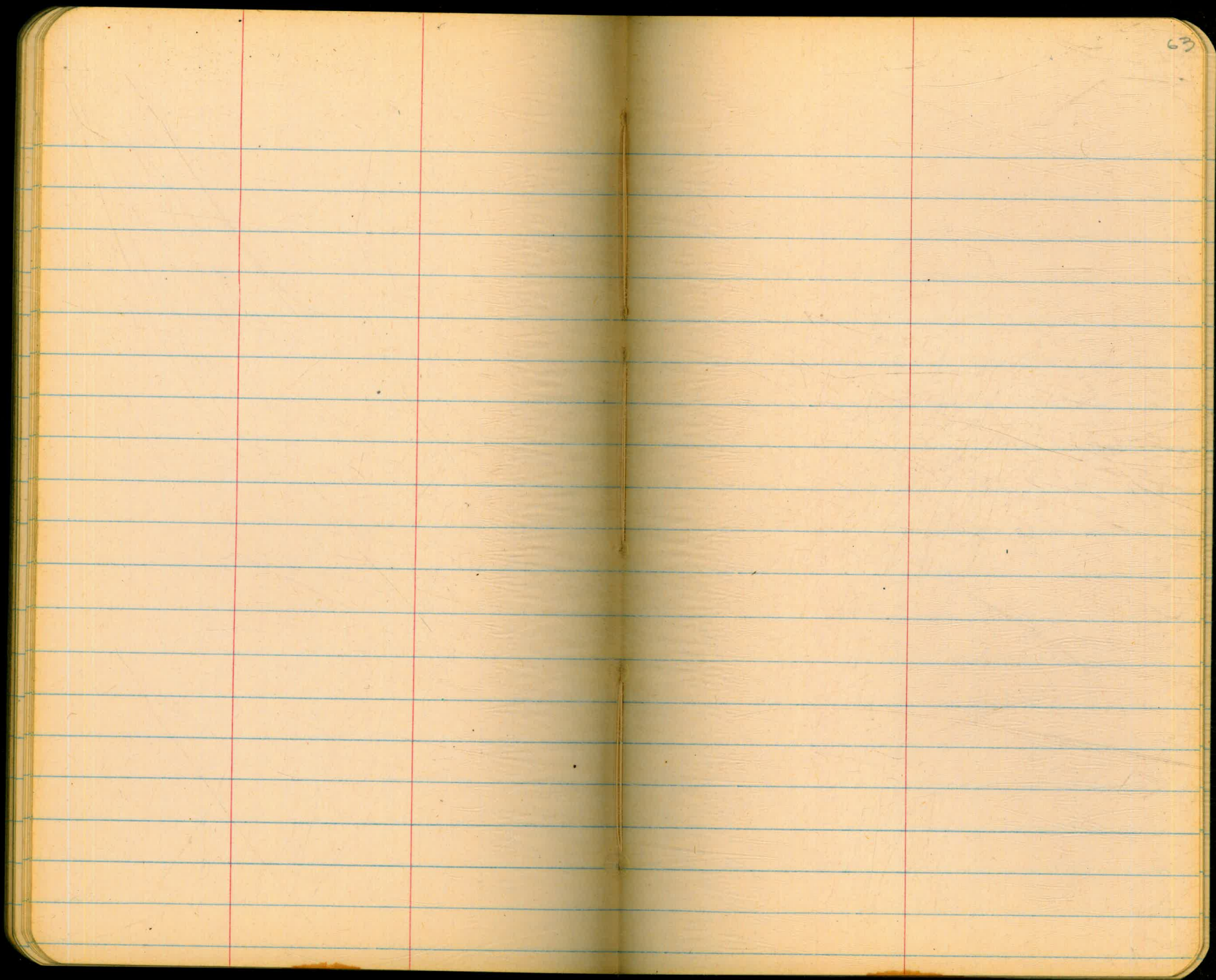




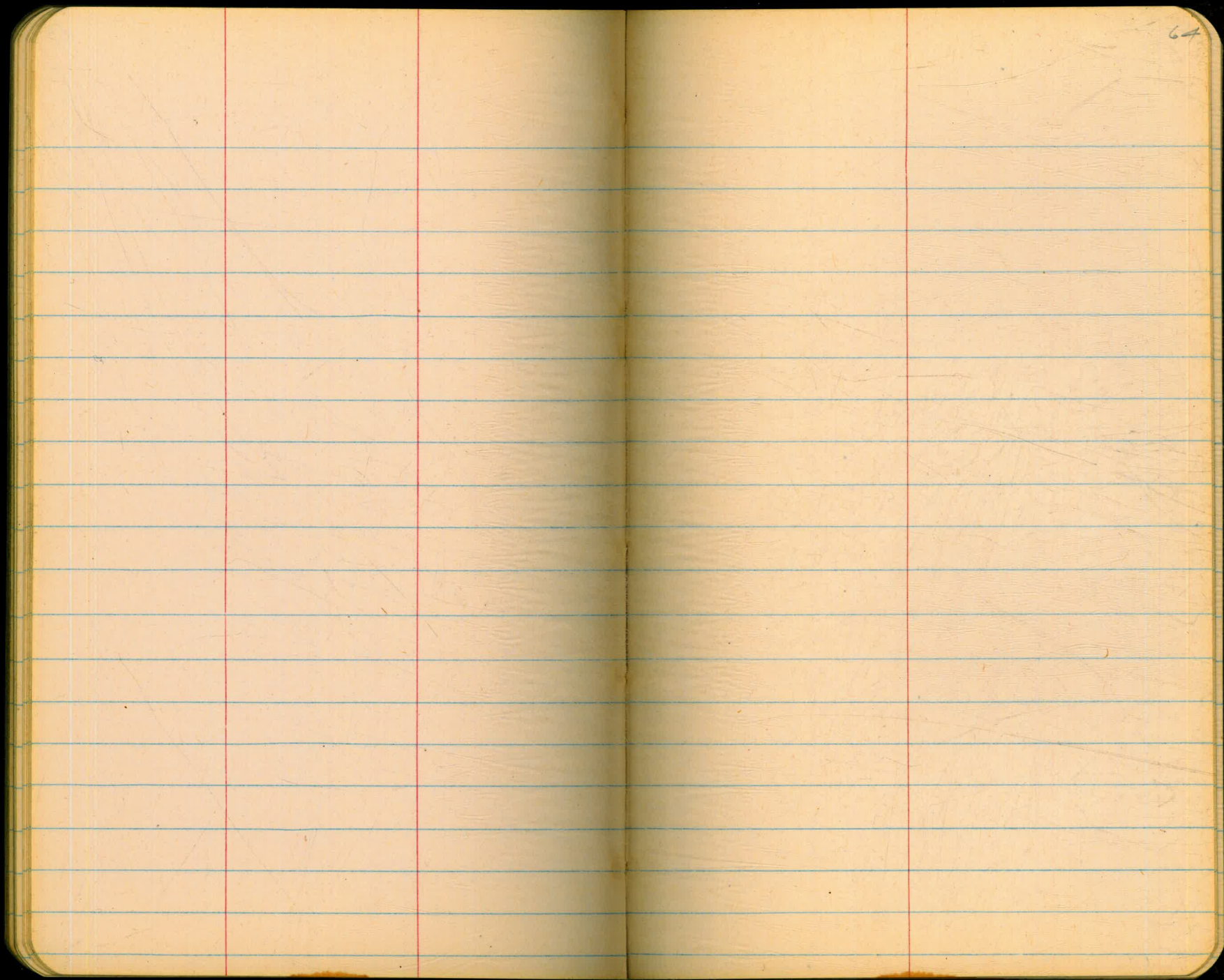




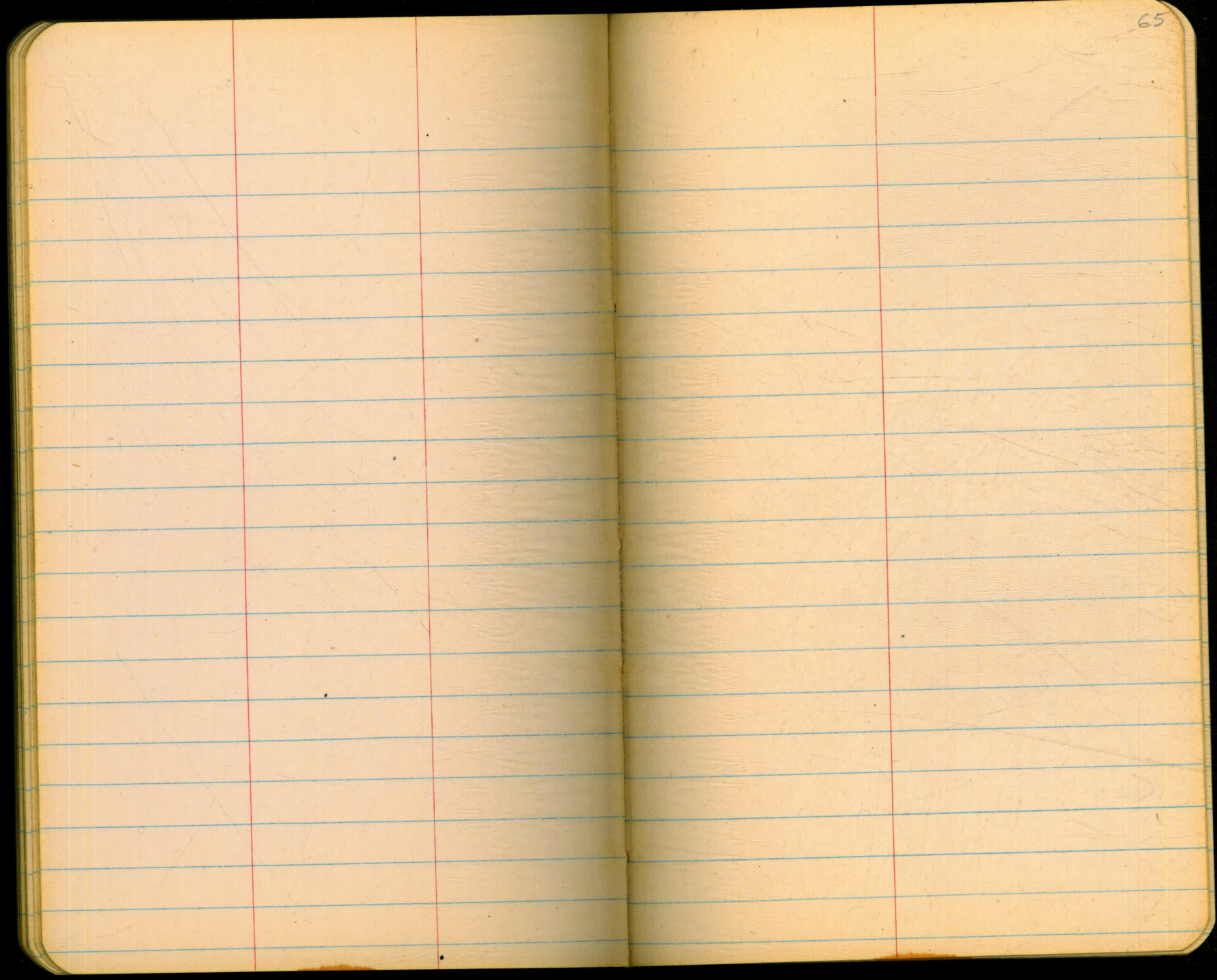




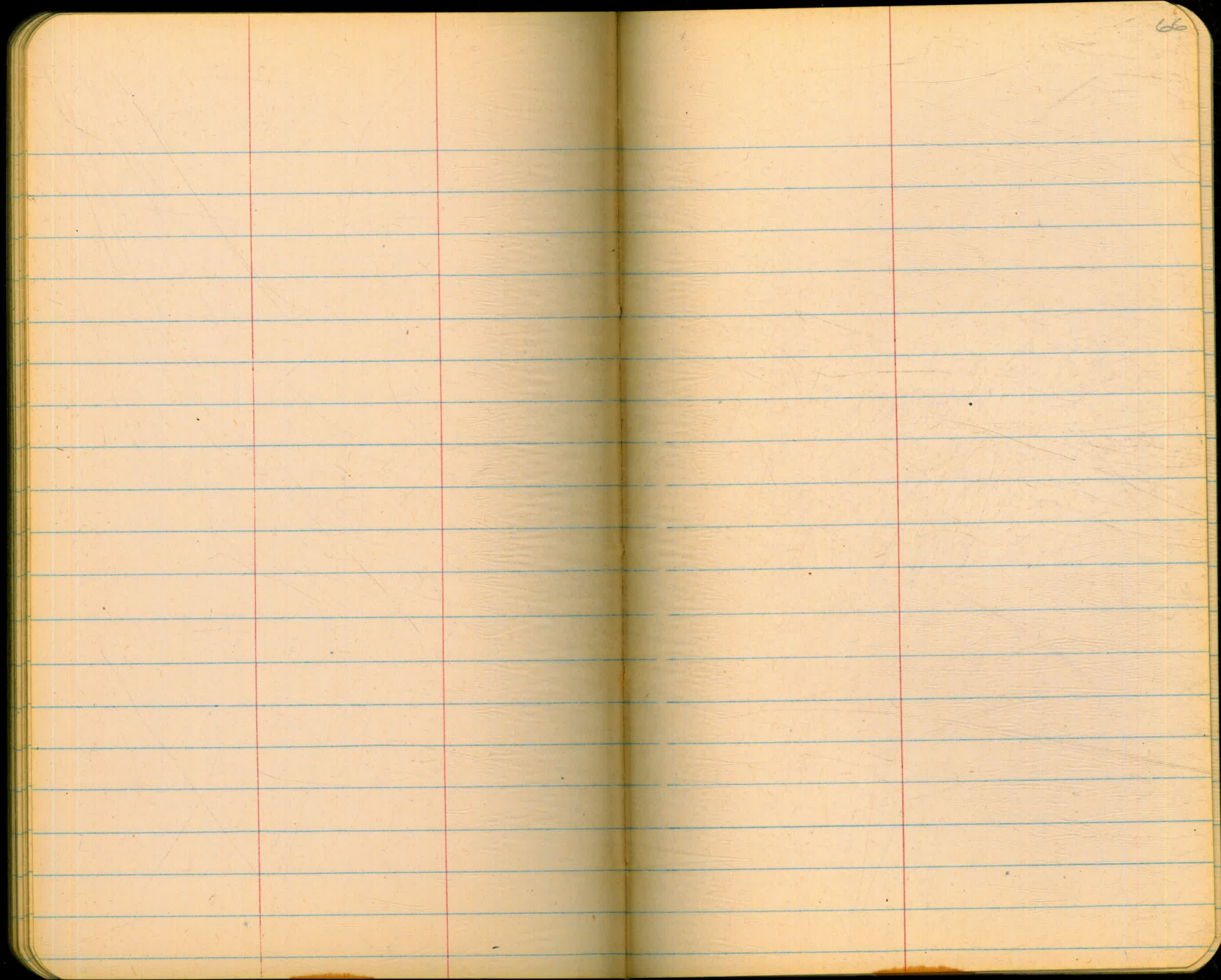




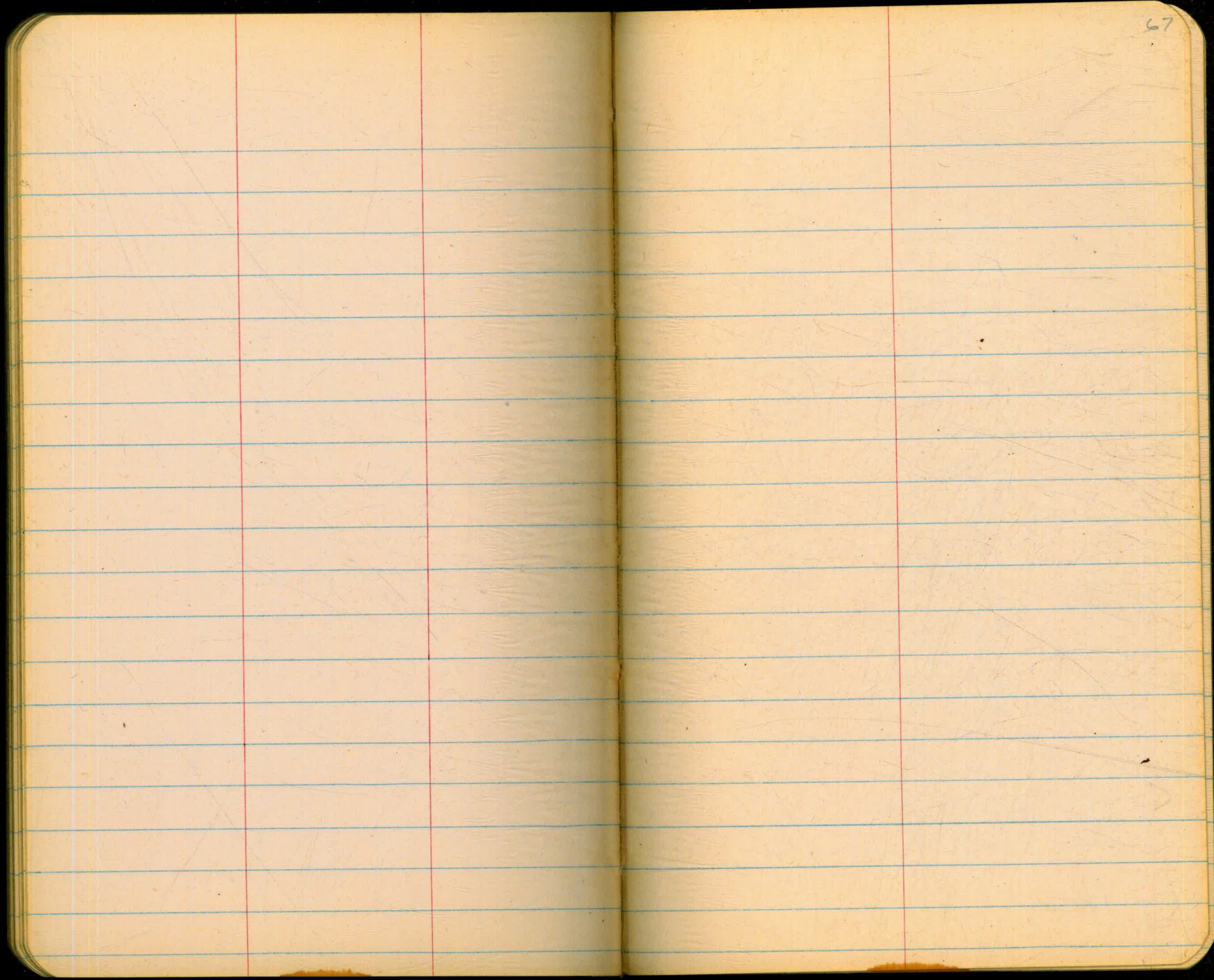




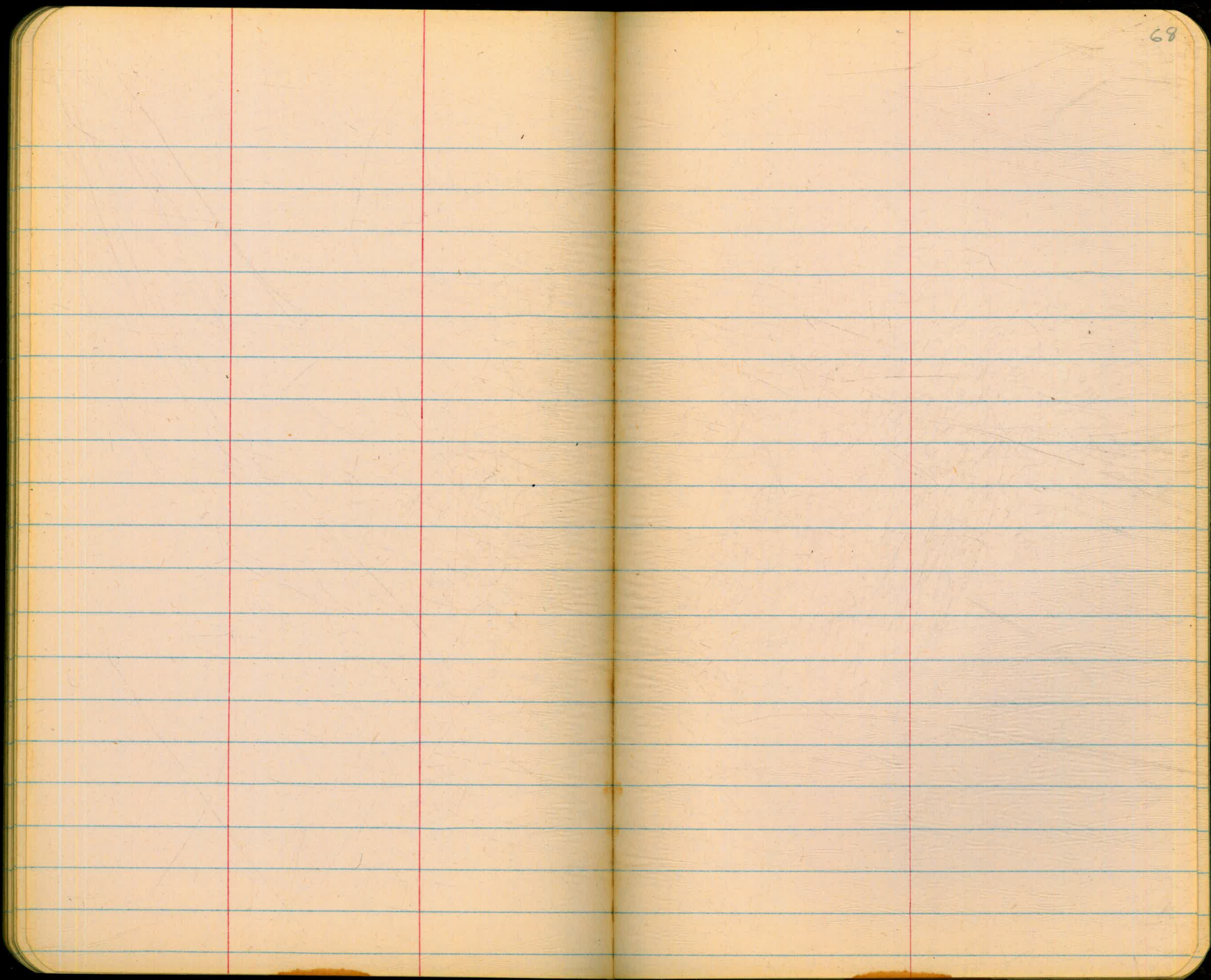






















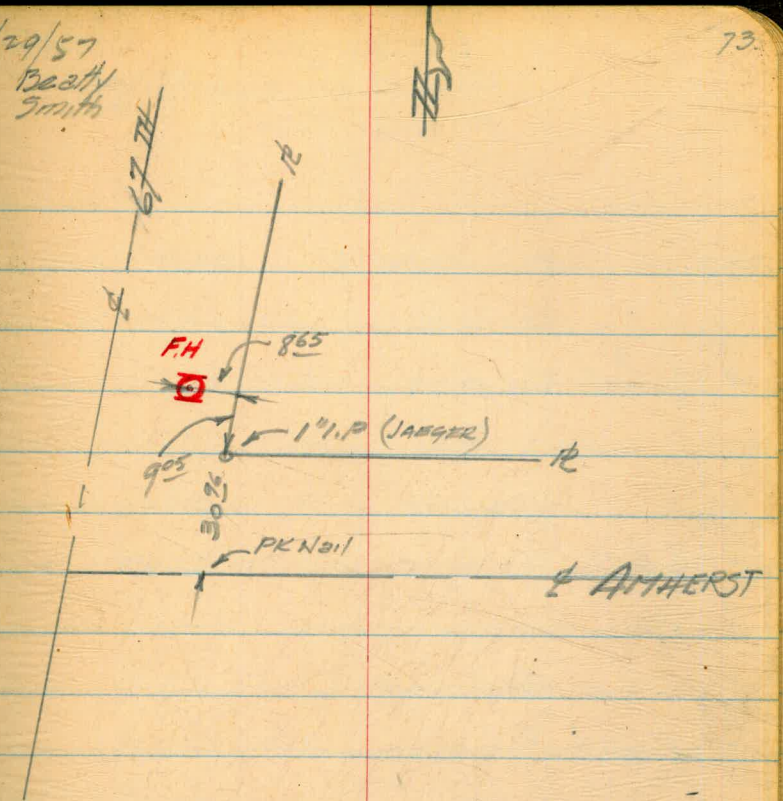






67<sup>TH</sup> & AMHERST  
Location of Existing F.H

3/29/57  
Beatty  
Smith



VIOLA ST  
 Check on depth of  
 8" AC MAIN

3/28/57  
 Betty  
 Smith

74

BM.	1.10	10.90	39.80		
	GRD LINE	6.2	34.70		
1483 ♀	50' Ely Gart	Top pipe	9.06	31.84	
Ⓟ	1.00	30.21	11.69	29.21	
	GRD LINE	2.80	27.41		
0+96	39' Wly Gart	Top pipe	5.28	24.93	
	GRD LINE	7.5	22.7		
0+16	119' Wly Gart	Top pipe	10.37	19.84	
	CK 0+29	7.06	23.15	22.4	20 <sup>6</sup> C08
	= 0+16				
	CK 0+26	5.52	24.69	23.3	23 C14
	= 0+46				
	CK 0+50	4.06	26.15	24.6	25 C16
	= 0+70				
	CK 0+74	2.22	28.00	26.2	27 C18
	= 0+94				
	CK FH 0+18	6.73	23.48	23.2	F03
	= 0+05				
Ⓟ	11.54	41.71	0.00	30.17	
CK. BM.		187	39.84		



36<sup>TH</sup> ST.  
 NATIONAL to Newton  
 16" C.I.  
 Eleu. Top of Main

3/20/57

75

BM 11.55 48.53 36.98

0+00 = sly of Newton 0.2 48.3

0+75 3.1 45.4

2+20 5.7 42.8

3+35 9.62 38.9

TBM 3.77 52.09 0.21 48.32

94' sly of 0+00 3.10 49.0

" " " " 8.06 44.03

150' sly of 0+00 3.50 48.6

8.07 44.0

Groundline & pipe

Top of pipe (48±) (Not Fd! Too hard)

Grd line & pipe

Top of pipe (35±) Not Fd!

Grd line & pipe (48 to Top pipe) Not Fd

Grd line & pipe (42 to Top pipe) Not Fd

Nail in pole SE Cor 36<sup>TH</sup> & Newton

Ground line & pipe

Top 16" C.I.

Ground line & pipe

Top 16" C.I.

} Fd pipe  
 new series  
 being  
 put in.

ELEV. Top of pipe  
Amherst St

3/15/57  
Beatty  
Smith

76

BM	1.96	455.99	451.03	Nail in P.P. 5th Cor 68th Amherst
70' wly W. Line 68th	Grd line	5.04	450.95	
	Top 6" C.I.	9.15	446.84	
270 wly	Grd line	5.61	450.38	
	Top 6" C.I.	9.91	446.08	
CK TBM		5.85	450.14 = 450.10	Nail in P.P.



Ck Levels Bayview Res

2/28/57

77.

BM	13.05	375.92		362.87	
BM	13.02	388.41	0.53	375.39	= 375.25
TD	12.95	400.93	0.43	387.98	
TD	12.79	413.29	0.43	400.50	
TD	13.14	426.23	0.20	413.09	
TD	13.32	439.12	0.43	425.80	
TD	6.01	444.20	0.93	438.19	
			3.08	441.12	= 441.08

Nail TELE POLE 477416 H **CITY Eng's 3941-0**

Guy Pole Elev. mark'd on pole at nail

NOTE SEE SH. 20  
C-11-12

NE COR VAL CHAMBER



Top 12" #6" Main  
Amherst. & 69TH

3/1/57  
Beatty  
Smith

TBM	5.16	459.81	454.65	RP 5th Cor 69TH
	Top 12"	9.20	450.61	
ELY at R 69TH	Grd line	5.40	454.41	
	Top Val Stem FH. GV.	7.83	451.98	
Amherst	Top 6"	9.10	450.71	
	Grd line.	5.0	454.81	
CK TBM		5.16		

Top 4" Main, PECK PLACE  
at Catch Basin

3/1/57 Beatty  
Smith

BM	4.85	470.97	466.12	
P	1.52	466.76	5.23	465.24
	Ground line	9.85	456.91	
	Top 4" AC	12.35	454.41	
	Curb inlet	10.78	455.98	
TBM in pole	9.54	466.80	9.50	457.26
P		1.57	465.23	

NW Cor 59TH El Cajon

175  
400

ING.

.9	
1.35	0
2.85	1
4.35	2
5.85	3
7.35	4
8.85	5
10.35	6
11.85	7
13.35	8
14.85	9
16.35	10
17.85	11
19.35	12
20.85	13
22.35	14
23.85	15
25.35	16
26.85	17
28.35	18
29.85	19
31.35	20
32.85	21
34.35	22
35.85	23
37.35	24
38.85	25
40.35	26
41.85	27
43.35	28
44.85	29
46.35	30
47.85	31
49.35	32
50.85	33
52.35	34
53.85	35
55.35	36
56.85	37
58.35	38
59.85	39
61.35	40
62.85	41
64.35	42
65.85	43
67.35	44
68.85	45
70.35	46
71.85	47
73.35	48
74.85	49
76.35	50

Y  
S  
O

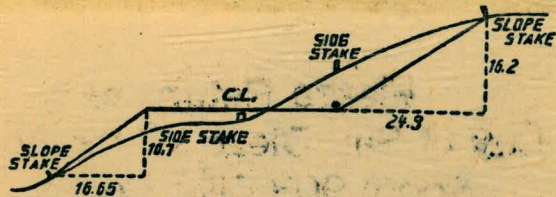
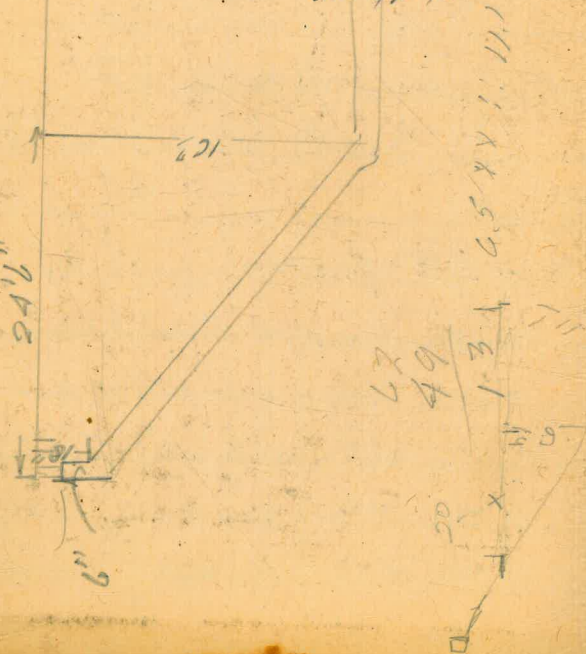


1652-58.69  
56.11

1986'-59.02  
56.15

Please Return to  
City of San Diego Water Dept.  
Room 903 Civic Center

76°16'00  
17-12-15  
S 59-03-65 W  
28-29-05  
S 87-33-30 W  
69-52-40  
157-26-10  
22-33-50  
91-51-30  
88-08-30  
59-03-05  
147-12-15  
32-47-65



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.  
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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