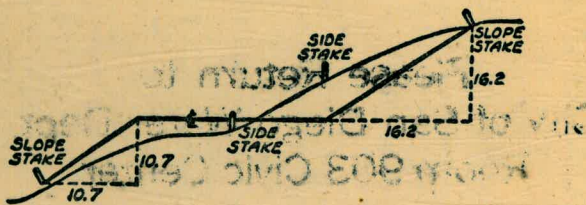


W 9/6



Please Return to
City of San Diego Water Dept.
Room 903 Civic Center

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should target. If it does not make the slight adjustment necessary.

Jim Friday

27854

14237 Springside

600

1995172

300

598551600

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.036	.041	.043	.047	.051	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.970	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

5ths for meters alic
 Pynchon Franklin to Oceanview 1 ✓
 East of 42 5ths for meters ✓
 Alley Blk 72 South of Whightman 2-3
 Prelim Group 25 ✓
 Missouri St Jewell to Ingraham alic ✓
 Prelim Group 25 4-5 ✓
 Olney St Balboa St to Thomas 6-8 ✓
 Prelim Group 25 ✓
 Olney St Road to Alley South of Road 9-10 ✓
 Prelim Group 25 ✓
 Alley N of Emerald St East Ocean Blvd 12-13 ✓
 Prelim Group 25 ✓
 Main Ave Abbott to W Pt Loma Blvd 14-16 alic ✓
 Prelim Grp 25 ✓
 Alley Blk 131-132 Strandway to Bayside 17-19 ✓
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 46th Olive to Maple St 23-25 ✓
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 Olive St 46th to Alley East of 46th 26-27 ✓
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 AMALFI ST TORREY PINES Rd to HILLSIDE 40 alic ✓
 TWAIN AVE Crawford to Mission ✓
 George Rd. Prelim 41 ✓
 Fairmount Ext Mission George Rd to 450' N 52 alic ✓
 Fairmount Ext Sta 7+45' to Twain Ave. 53+56 ✓
 Twain Ave. Fairmount Ext to Mission George Rd. 56 alic ✓

Mission Gorge Rd Twin St to 57

Lassen
(Rainier) Ave palm Glacier ✓

Vandever St. Riverdale St 64 ✓

to Mission Gorge Rd 64 ✓

Glacier Ave Riverdale to Mission ✓

Gorge Rd 65 - 67 ✓

Glacier Ave Mission Gorge Rd ✓

to Holabird St 68 - 69 ✓

* LASSEN AVE.
(Rainier St) Mission Gorge Rd

to Holabird St 70 - 71 ✓
alice

Relocation F.H. Hammond Dr @ Sandrock Road 72 ✓

LOCATION 8" C.I. Water - Hwy 395 Thru 73-76
Montgomery Field ✓
alice

REALIGNMENT PROFILE 77-78
46th ST OLIVE TO MAPLE ALSO 23 ✓
alice

* "Rainier St." name changed to "Lassen
Ave" - Existing St. Sign is in error ✓
alice

FILE 2000 9

$\Delta = RE = 4'$

$R = 15.5'$

$L = 44.3'$

$E = 118'$

$20 = 4 + 36'$

ST

Ryochon St
Franklin to Oceanview
425 for Water Meters

meters set 205 from 0.51 2818 D

1.14	117.63	116.49	
0.34	105.35	105.01	
0+24 MW	9.0	96.4	98.0
+54 ME	6.3	99.1	98.9
1+41 ME	8.4	97.0	97.5
+49 MW	11.1	94.3	96.8
2+50 ME	6.3	99.1	96.7
+68 MW	8.9	96.5	96.2
3+18 MW	8.1	97.3	96.5
4+25 ME	6.1	99.3	97.5
+28 MW	9.5	95.9	97.2
+78 ME	5.6	99.8	97.8
6+06	5.2	100.2	100.2
6+06	4.3	101.1	100.2
12.92	117.73	059	109.81
	1.23	116.50	= 116.49

West
Williams
Varonakis

7-5-55

0+02 south line Franklin

BM SW BP Oceanview +47^{ft}

F1⁶

C0²

F0⁵

F2⁵

C2⁷

C0³

C0⁸

C1⁸

F1⁹

C2⁰

C0⁰

C0⁹

Tap BV Cap

(8) To BV

Alley BIK 72
South of Wightman
N of Van Dyke

West
Williams
Varonfakis

2

Meters set 9.25 from 14752

7/5-55

7.05 350.13 343.08

at NW/8P Landis + Marlborough

10.23 357.22 314 346.99

2.38 355.60 400 353.22

0+40 MW	1.7	353.9	353.3	CO ⁶
+45 ME	1.9	353.7	353.2	CO ⁵
+98 ME	2.8	352.8	352.4	CO ⁴
1+18 MW	3.2	352.4	352.1	CO ³
+29 ME	3.3	352.3	352.0	CO ³
2 Meters +52 MW	4.2	351.4	351.3	CO ¹
+62 ME	4.0	351.6	351.3	CO ³
2+08 MW	4.6	351.0	350.6	CO ⁴
2 Meters +25 ME	4.6	351.0	350.2	CO ⁸
+46 MW	5.4	350.2	349.9	CO ³
+78 ME	5.8	349.8	349.4	CO ⁴
+95 MW ^M	6.0	349.6	349.1	CO ⁵
3+28 ME	6.3	349.3	348.3	CO ⁰
+44 MW	6.8	348.8	348.3	CO ⁵
+65 ME	7.0	348.6	348.3	CO ³
3 Meters +85 MW	7.6	348.0	347.6	CO ⁴

355.60

3+92 ME	7.8	347.8	347.4	CO 4
1+24 ME	8.2	347.4	346.8	CO 6
+25 MW	8.7	346.9	347.0	FO 1
+65 MW	9.1	346.5	346.3	CO 2

2.92 348.87 9.05 346.55

4+69 ME	2.0	346.9	346.1	CO 8
2 MW				
5+21 MW	3.2	345.7	345.3	CO 4
+21 ME	2.6	346.9	345.2	CI 1
2 MW				
+76 ME	3.9	345.0	344.3	CO 7

5.35 348.21 6.01 342.84

5.12 343.09 = 343.09

Missouri St Ingraham to Jewell
 Pelim Group 25

West
 Williams
 Varantakis

A

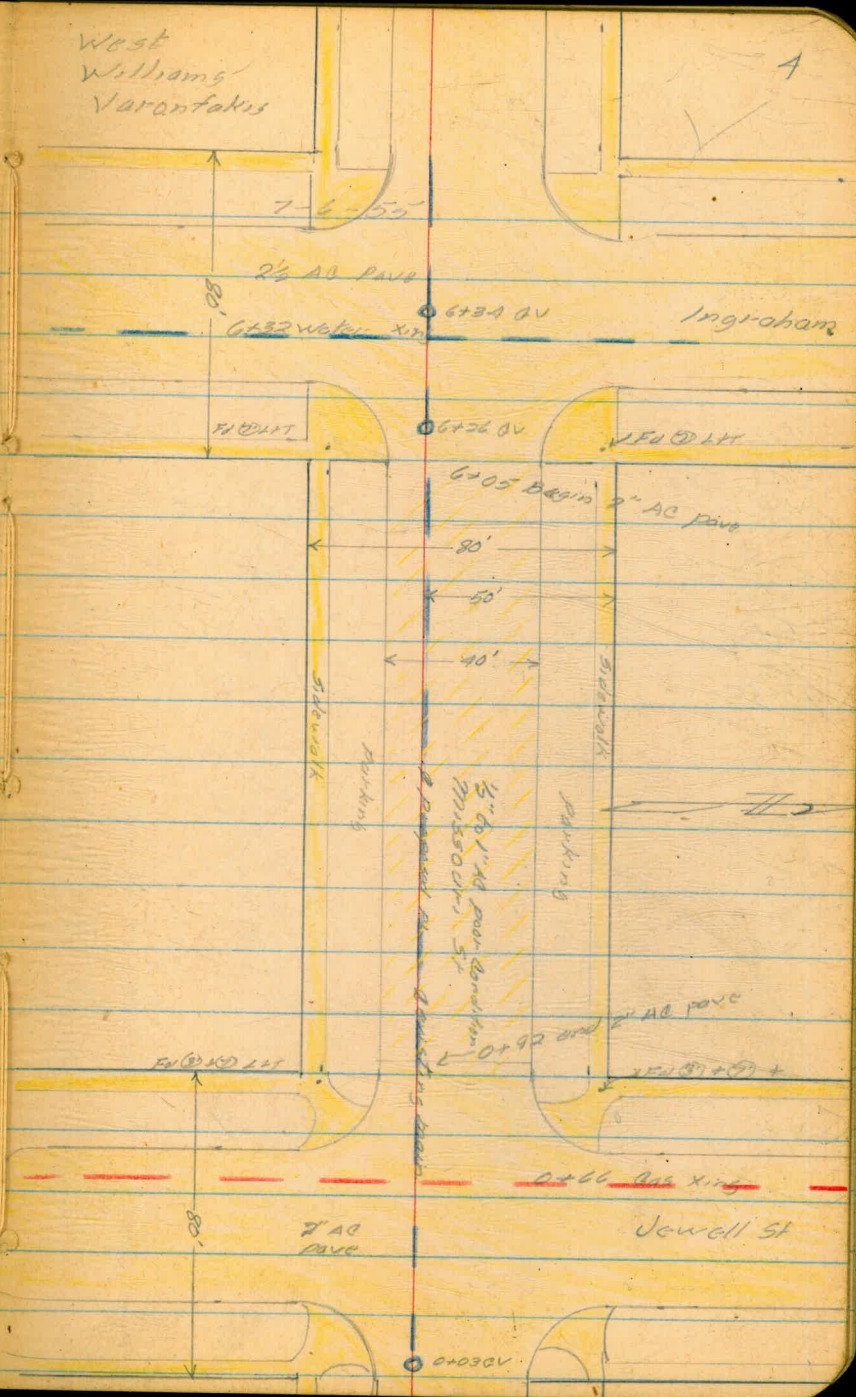
6+06 20

Why prop line Ingraham

6+06 20 POT

0+83 POT

0+00 Why prop line Jewell St



Missouri St

Q Profile

0.50	113.78		113.29
1.03	104.70	10.11	103.67

0+00		3.53	101.17
+50		3.75	100.95
+92		4.66	100.04
1+00		4.80	99.90
+50		5.72	98.98
2+00		6.58	98.12
+50		7.47	97.23
3+00		8.35	96.35
+50		9.37	95.39
4+00		10.40	94.30
+50		11.32	93.38
5+00		12.19	92.51

4.97	97.33	12.34	92.36
------	-------	-------	-------

+50		6.04	91.29
6+00		7.54	89.79
+50		8.69	88.64
+79.3		9.18	88.15

9.13	109.89	2.68	94.75
11.61	119.49	0.40	103.48
		1.19	113.30 - 113.28

7-6-55

NW BP
Chalcedony + Jewell

Top FH SE Cor Jewell + Missouri St

E prop Line Jewell St

End AC pave

Reduced by J Gray 7-19-55

Olney St Balboa Ave to Thomas Ave
Group 25 Pelim

West
Williams
Varanakis

6

8+81⁷⁰

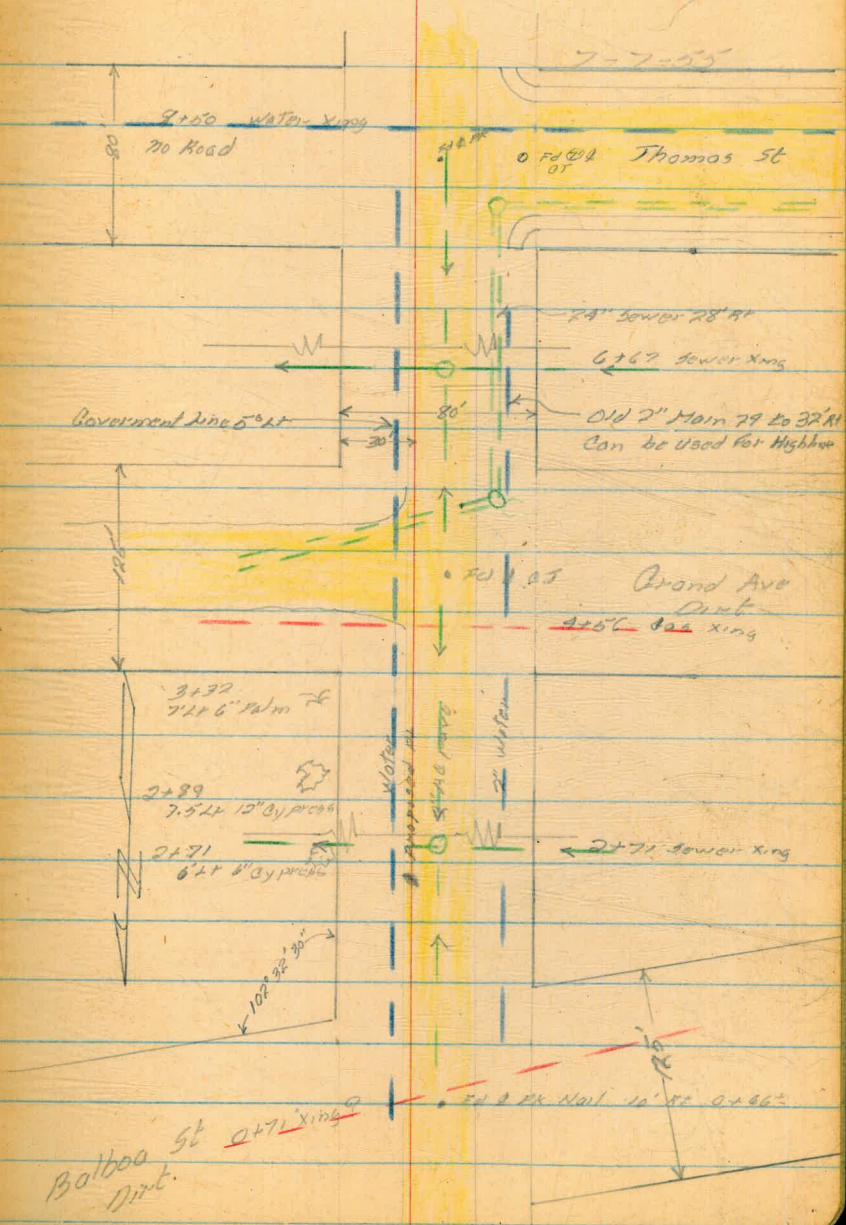
slly prop line Thomas

8+41⁷⁰ POT

0+64⁰² POT

0+00

slly prop line



7-7-55

Government line 5' at

24" sewer 28' 5"

6767 sewer xing

Old 2" Main 79 to 32' 41"
Can be used for Highway

Grand Ave
Dirt
4+56 Gas xing

3+77
7.2' 6" 14m

2+89
7.5' 4" 10' 3" by prop

2+91
6' 2" 8' 3" by prop

Water
Proposed
8' 4" 10' 3" by prop

2+71 sewer xing

1-108 32' 30"

Balboa St
Dirt
0+71 xing

5' 2" 24' 10' 40' 0+66

Olney St
Q Profile

	1.68	55.83		54.15
	7.87	55.82	2.88	47.95
	0.87	44.01	12.68	43.14
0+00			5.28	
+50			5.92	
1+00			6.41	
+50			7.60	
	2.69	40.14	6.50	37.51
2+00			4.39	
+50			5.09	
+71			6.00	+7.3 To Flow
3+00			6.22	
+55			7.55	
4+00			9.06	
+50			10.93	
5+00			12.62	
				+18.8 To Flow Line
5+01	0.94	29.10	11.98	28.16
+50			2.61	
6+00			3.92	

BM NW 1/4 Hornblend + Morrell 25520

6.06
2'4" edge AC
N 1/4 prop line Balboa

5.84
10' RT

6.52
2'4" edge AC

7.11
10' RT

Turn on Q PK Nail Q Balboa + Olney

4.2
5'4" edge AC

4.88
10' RT

Top West 12" Sewer MH 10' RT

8.87
2'4" edge AC

9.52
10' RT

12.06
2'4" edge AC

12.82
10' RT

Turn East Rim Sewer MH 28' RT

3.76
2'4" edge AC

4.34
10' RT

Olney St Cont

8

29.10

6+50 5.26 +6.2 to flow

+67 6.02

7+00 6.47

+50 7.70

8+00 8.85

10.5 flow line 24" sewer

+25 8.92

+50 9.94

+81.20 10.61

12.73 41.09 0.79 28.36

8.76 47.59 2.26 38.83

7.97 55.46 0.10 47.49

9.62 56.45 8.88 46.78

2.31 54.14 = 54.15

Top West rim Sewer MH 10' RT

6.90
2' at edge AC 10' RT

8.75
2' at edge AC 10' RT

Top West rim Sewer MH 28' RT

Turn on D.C.T. Grand + Olney

OLNEY ST

Reed St to Alley South
of Reed
Group 25 Polm

West
Williams
Yaronfakis
Kullhofer

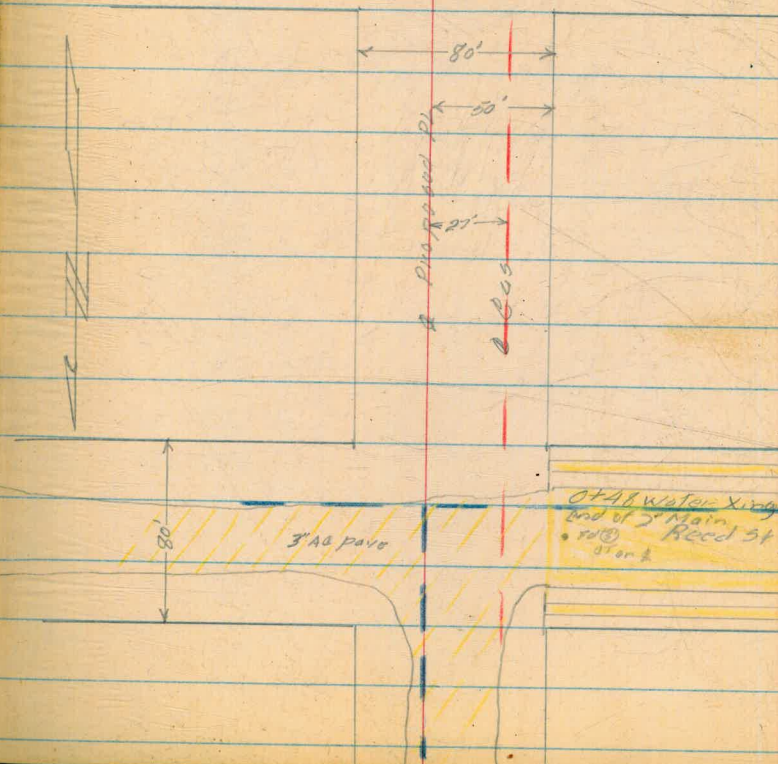
9

7-8-55

2+25±

Sly prop line Alley

Alley



0+40 P.O.T

0+00 Sly prop Line Reed St

Olney St
Profile

0.85 29.01 28.16

1.82 20.33 10.50 18.51

0+00 6.22

+50 7.14

+63 7.40

1+00 9.3

+50 11.2

2+00 12.7

+25 12.9

11.13 29.24 2.22 18.11

1.05 28.19 -28.16

10

See Page 7
Turn on east side of road MH 28' RT 6+01

Nly prop line road

end of 3" AC pave

9.0	9.7	8.4
10' RT	3' RT	10' RT

11.7	12.0
10' RT	9' RT

Ocean Blvd

Diamond to Felspar

Relin Group 25

7+91⁰⁹

South prop line Felspar

7+08⁰⁹

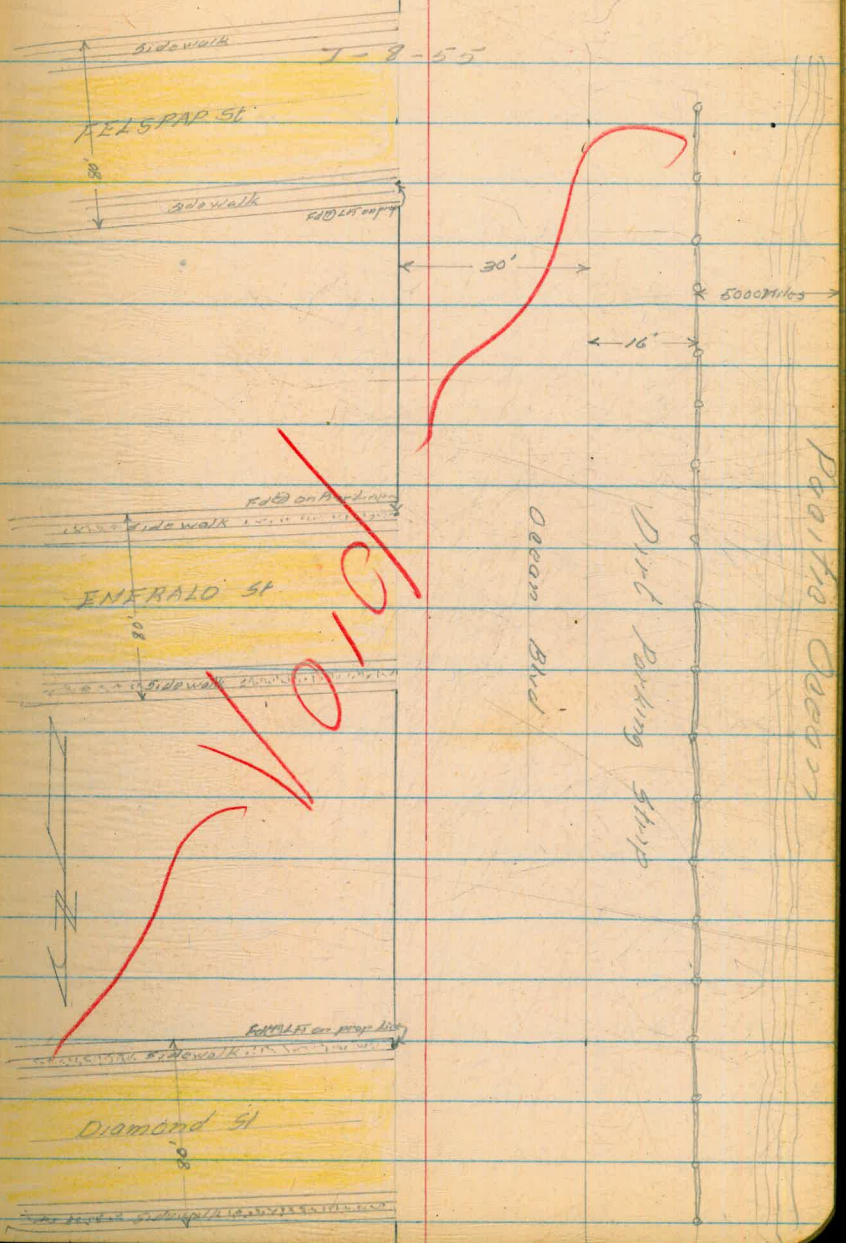
POT

0+73 POT

0+00 NY prop line Diamond St

West
Williams
Karonakis
Kullhofer

11



Alley

N of Emerald
E of Ocean Blvd

	2.63	33.55	30.92	
	5.47	32.97	6.15	27.40
0+00		9.66		23.21
			+6.6 To Flow	
+40		8.20		
+50		8.04		24.83
+80		7.57		25.30
1+00		7.22		25.65
+50		6.42		26.45
2+00		5.64		27.23
			+6.4 To Flow	
+15		5.47		27.40
+50		4.84		28.03
3+00		4.00		28.87
			+3.6 To Flow	
+47.2		3.46		
+49.2		3.19		29.68
4+00		2.63		30.24
+16		2.51		30.36
+16	5.49	36.48	1.88	30.99
			+9.6 To Flow	
4+22		4.95		
		5.61		30.87

West
Williams
Varonakis16
6A
A2

12

BM SW CP Diamond + Mission Blvd

5/4 prop line Emerald

Top East Rim Sewer MH 5' LT

Top east edge Sewer MH 5' LT

Top East edge Storm Drain MH 8' LT

BV

bit of cb Nly Side Diamond St

Top of cb " " "

Top East Rim Sewer MH 5' LT

Alley N of Emerald
E of Ocean Blvd

4+29²

slly prop line Diamond

3+49²

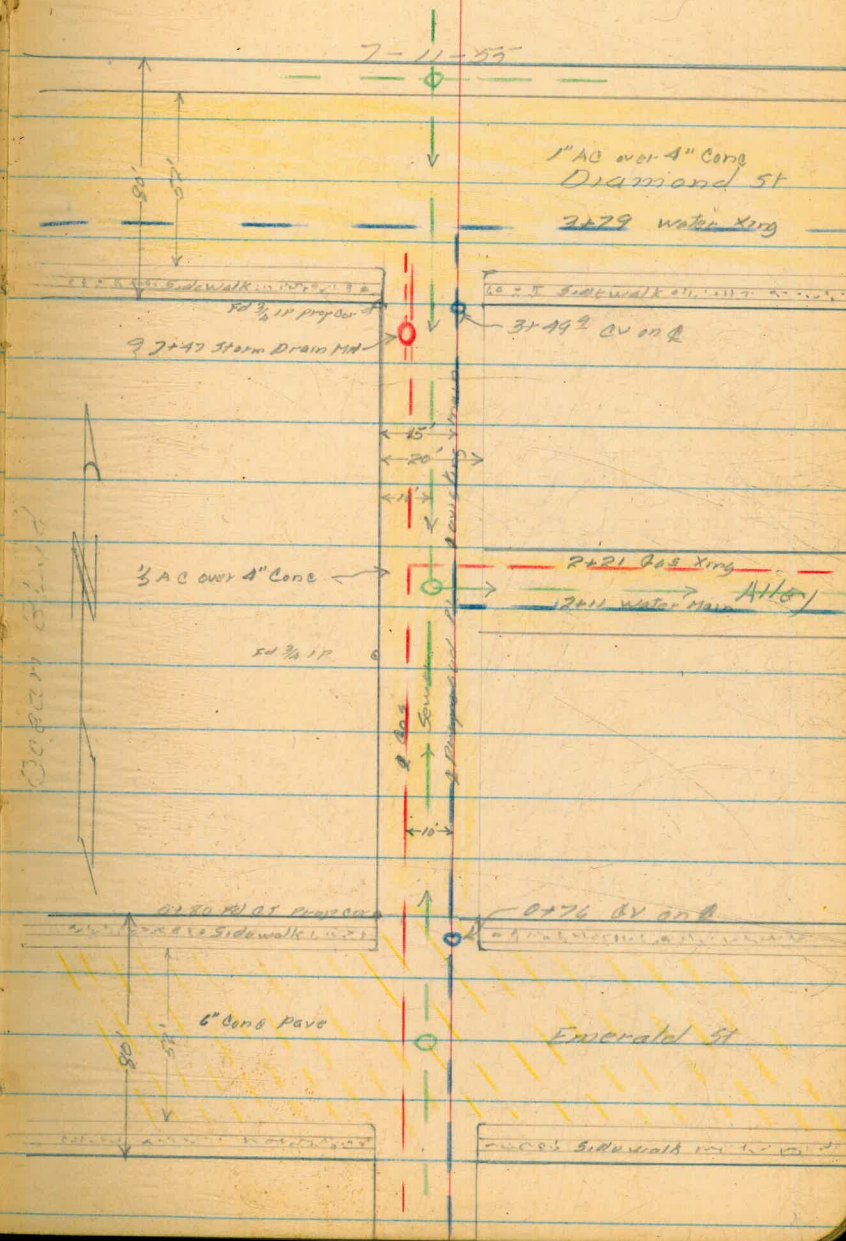
POT on CV slly prop line Diamond

0+80 POT

0+00 slly prop line Emerald

West
Williams
Varonakis

13

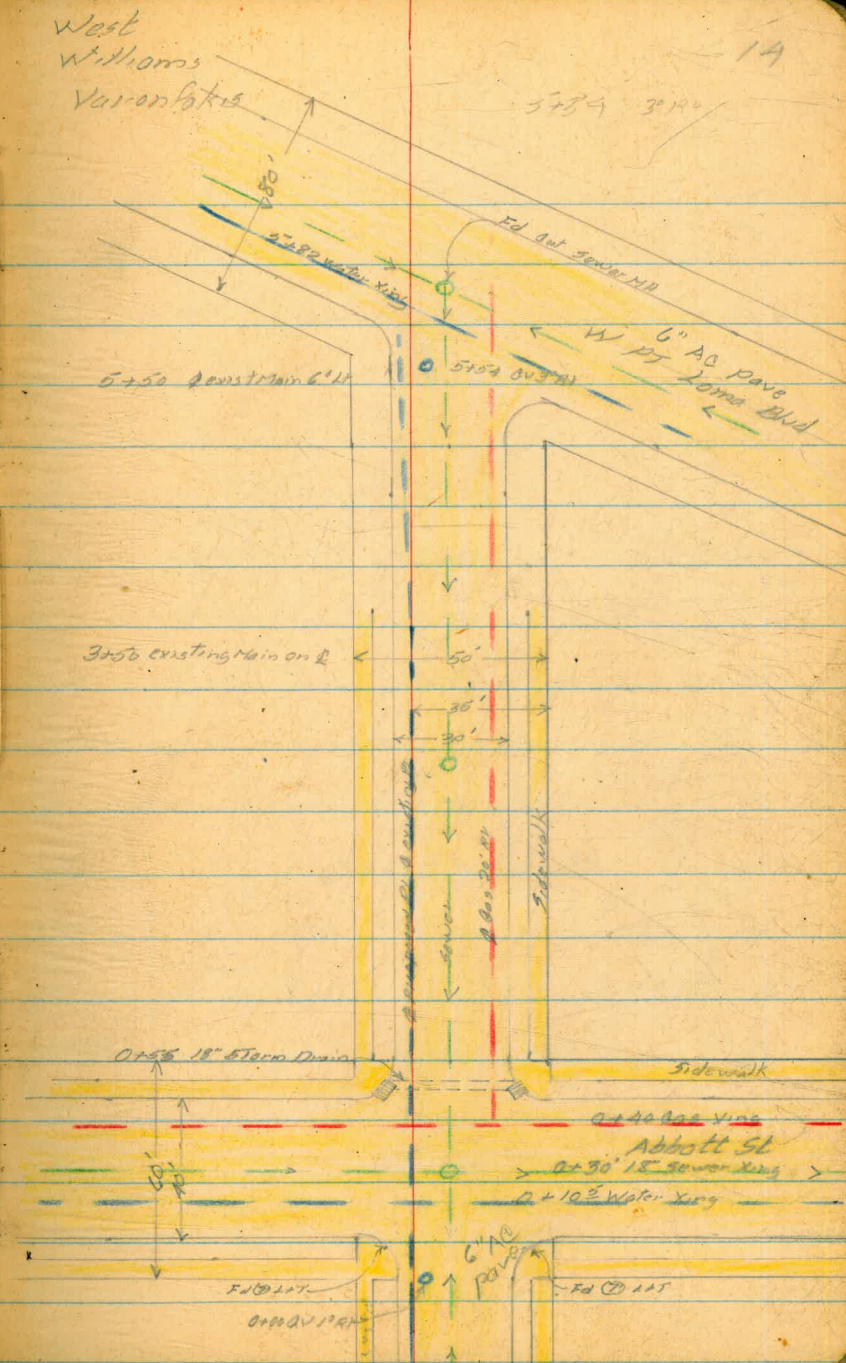


Muir Ave
Abbott to W Pt Loma
Pelino Group 25

6+25 Ch Line WPT Loma
5+87 ⁷²POT 90° 10' RT Out Sewer MH

0+07 POT

0+00 Fly prop Line Abbott



Muir Ave
Abbott St to W Pt Loma
Profile

	4.36	6.30	1.94	
0+00			4.27	2.03 + 8.2 To Flow
+30			4.25	
+50			4.23	2.07
+55			4.50	1.80 + 4.6 To Flow
+55			5.14	+ 4.8 To Flow
+55			5.22	
1+00			4.93	1.37
+50			5.08	1.22
2+00			5.23	1.07
+50	5.11	6.09	5.32	0.98
3+00			5.19	0.90 + 6.3 To Flow
+00			4.94	
+50			5.37	0.72
4+00			5.44	0.65
+00			5.20	0.89
5+00			5.39	0.76
+50			5.46	0.63 + 4.9 To Flow
187 ^B			5.05	

15

7-11-55

BM NW BP Muir + Abbott St

Ely prop line Abbott St

Top sly rim sewer MH 10' RT

Storm Drain King
18"

Top Storm Drain Grade 6° 11'

Top 18" storm " " 28' RT

Top sly rim sewer MH 10' RT

609

5+87	72	5.06	
6+00		5.08	1.01
+25 ²		5.38	0.71
+25 ²		4.93	1.16
4.45	6.16	4.38	1.71
		4.26	1.90 =

Top East Rim sewer M11 10' RY

Bottom of C6 NWly side W of dam

Top " " " " "

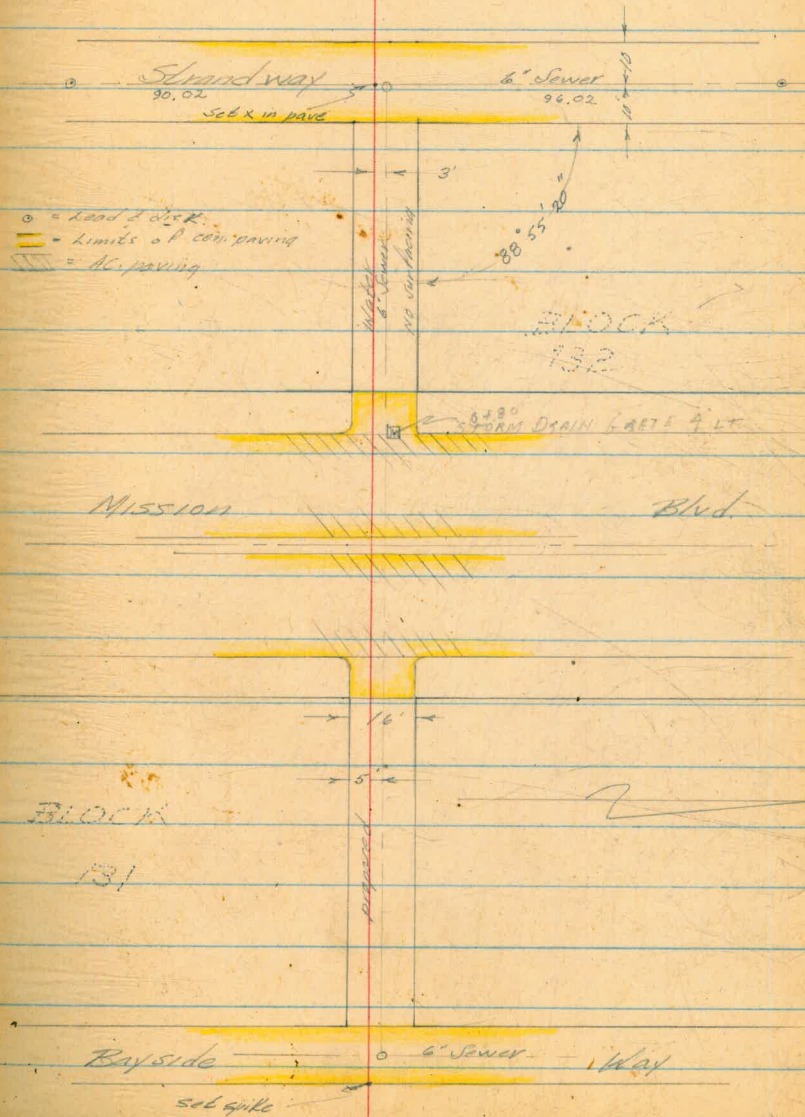
1.94

West
Alexander

17

7-12-55

Profile & Proposed Water Line
Alley B/K 131-132, Strandway
to Bayside Lane



Alley Bills 131-132 Cont

*0.63

5.56 6.19

0400	16	4.59
0410	20	4.19
0410	196 (to cur)	4.23
0420	20	4.19
0450	42	1.99
0470	51	1.09
0480	57	.49
1400	53	.89
1408	52	.99
1408	45	1.69
1410	46	1.59
1411.9	52	.99
1419	55	.69
1421	55	.69

Reduced by Palmetto 6-2-5-5-5

End NE, curb return, Alley No. 132 CT. & Mission

W/ft of Strandway 6" con pave.
 Sewer crossing
 Sewer MH. 3' H 3.6' To Flow
 E/ft of Strandway curd 6" con.
 W/ft of Mission, begin 6" con pave, 64. 11.6 ft
 W curb line, Storm gale 4' H, begin 3" Ag. crown pave
 face curb center island Mission Blvd.
 top curb 20. 4' H
 top curb
 face curb
 Water 6" on line
 Water 6" 5' H

Alley Bills 131-132 Cont

619

1440	61	.09
1450	57	.49
2100	73	-1.11
2150	80	-1.81
2178.5	80	-1.81
2181	80	-1.81
2186.5	80	-1.81
2186.5	802	-1.83
2194.43	77	-1.51
	196	4.23
5.09	9.32	
	2.40	6.92

19

E curb Mission, end 8" AC crown cont

E/H of Mission, end 6" con.

W/H of Bayside Lane begin 6" con.

S.D. G.P.E. MH 4' Ht

Sewer crossing

Sewer MH, 2' Ht 4.7 To Flow

E/H Bayside Lane & RP 2' Ht

SURP. St. Louis Office, Mission Sewerwall

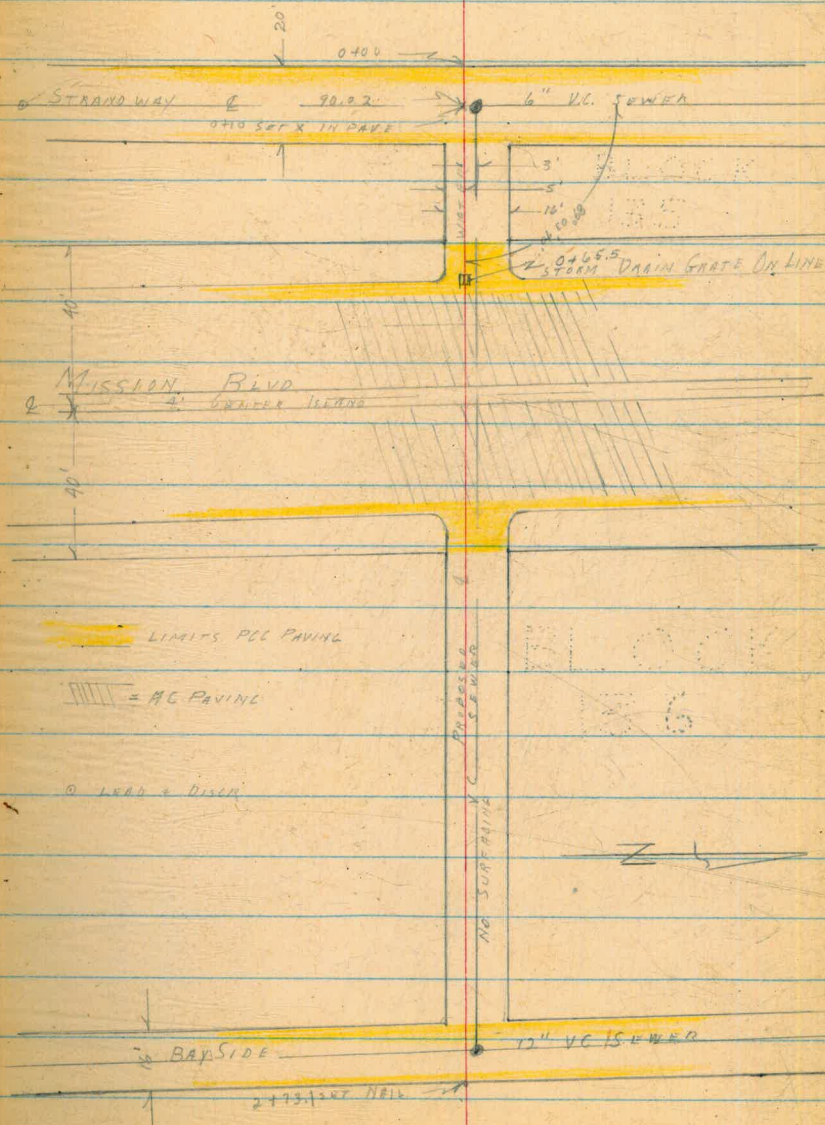
PROFILE & PROPOSED WATER LINE
 ALLEY BLS 135-136 ; STRANDWAY
 TO BAYSIDE LANE

0+00 WLY LINE STRANDWAY

WEAT
 ALEXANDER

7-13-55

20



ALLEY BLK 135-136

CONT

BM		6.98	BP	SAN LUIS OBISPO & SEA WALL
	1.97	8.95		
TP		1.19	7.81	
	1.93	9.79		
		5.09	4.65	TBM NEW RIM SEWER MH 3' LEFT 0410
	2.32	6.97		
0+00		1.9	5.07	WLY LINE STRANDWAY 6" P.C.C
0+08				GV 10' LEFT
0+10		2.3	4.67	SEWER CROSSING
0+10		2.32	4.65	NEW RIM SEWER MH 2' LEFT
0+20		2.3	4.67	END P.C.C PAVE
0+50		4.1	2.27	
0+55.3		4.9	2.07	BEGIN 6" P.C.C
0+65.5		5.5	1.47	WLY CURB LINE MISSION BLVD, BEGIN 2" AC. KNOWN CURB, STORM DR. GRATE ON LINE
0+93.3		5.2	1.77	BOTT CENTER ISLAND CURB
0+93.3		1.1	2.57	TOP " "
0+95.45				POWER POLE 3412 2' RT.

6.97

0+97	1.6	2.37	TOP CENTER ISLAND CURB
0+97	5.2	1.77	BOTT
1+00	5.3	1.67	
1+09	5.7	1.57	GV ON LINE
1+07	5.9	1.57	GV 1' LEFT
1+27.5	5.9	1.07	Ely CURB LINE MISSION BLVD END 2" AC CROWN COAT
1+34.86	6.0	0.97	END 6" PCC
1+50	6.4	0.57	
2+06	7.7	-0.73	
2+50	8.6	-1.63	
2+57.3	9.0	-2.03	BEGIN 6" PCC
2+66	9.1	-2.13	SEWER CROSSING
2+66	9.12	-2.15	Sly RIM SEWER MH 3.4' LT
2+69			GV 11" LEFT
2+73.1	8.9	-1.93	END NEAR Ely LINE BAYSIDE LANE END PCC
	3.20	3.77	TBM SW TOP FIRE HYDRANT FI CANNERY MISSION

46th St Olive to Maple St

Preliminary Survey Apr 28th

7+26.8 ±

Sly prop line Maple

7+13.80

POT FD (12) Conc Man 22.63 RT

5+15

SEWER XING

(NEW ALIGNMENT 4/26)

3+60.55 P.O.T. R.H. NAIL IN A.C.

3+54.5 BEGIN 1 1/2" A.C. (POOR GRADE)

NEW ALIGNMENT

0+43 POT CON. MAN 45' RT.

0+43 POT FD Conc Man 23' RT

0+00

Nly prop line Olive

West
Williams
Varanforks
Kellhofer

23

11/28/55

60

Maple St
No Road

FD (27) L (13) Man

Proposed R.

8

Sewer under

NOTE
REVISED ALIGNMENT
APRIL 26, 1957
PROFILE - P. 77

REVISED &
ROADWAY SET UP

3+80.5 Sewer Xing
Cut 15' in This Area

60

30

8

Olive St Dirt

60

FD (27) L (13) Man

0

0+25 Poor Xing

Profile 46th St

72
1 1/3
5 3/4
5

24

198	293.05	291.07
0+00	+1.4	294.4
+50	0.2	292.85
1+00	2.0	291.05
+50	3.3	289.75
2+00	4.8	288.25
+50	7.2	285.85
3+00	9.5	283.55
0.58	281.16	1247 280.58
3+50	3.1	278.06
4+00	7.7	273.46
+50	12.4	268.76
0.18	268.39	12.95 268.21
5+00	12.9	255.99
0.67	254.14	12.92 255.47
5+50	15.6	240.54
1.01	244.40	12.75 243.39
6+00	11.0	233.40

Reduced by P. ...

BM Olive + 46th 17' Mon 291.07

1/4 prop line Olive St

5.9	9.6
12.1	17.1 RT
7.7	13.1
15.2	17.1 RT
1.7	3.2
15.1	15.1 RT
2.4	11.9
16.1	19.1 RT
10.5	16.0
18.1	5.1 RT
7.23	19.9
24.1	10.1 RT
3.9	23.1
26.1	15.1 RT
0.5	19.6
24.1	15.1 RT

edge of road

edge of road

18' Lt edge of road

24' Lt edge of road

26' Lt edge of road

24' Lt edge of road

244.40

6+50

108 233.60

3.40 234.87 12.93 231.17

7+00

5.7 229.17

+26+

13.0 221.87

3.94 226.31 12.50 222.37

9.44 216.87 = 216.72

Revised by Robinson

2-28-56

75

Maple + 16 216.72

6.8
21.2 + edge AC

7.9
7.14

20.3
15.14

9.2
19.4 edge AC Road

3.2
10.14

10.4
15.14

9/4 Prop Line Maple

= SW (27) + (17) Non Maple + 16"

Olive St 46th to Alley
East of 46th
Preliminary Group 28

West
Williams
Varonakis
Kellhofer

26

11-28-55

0+435 ±

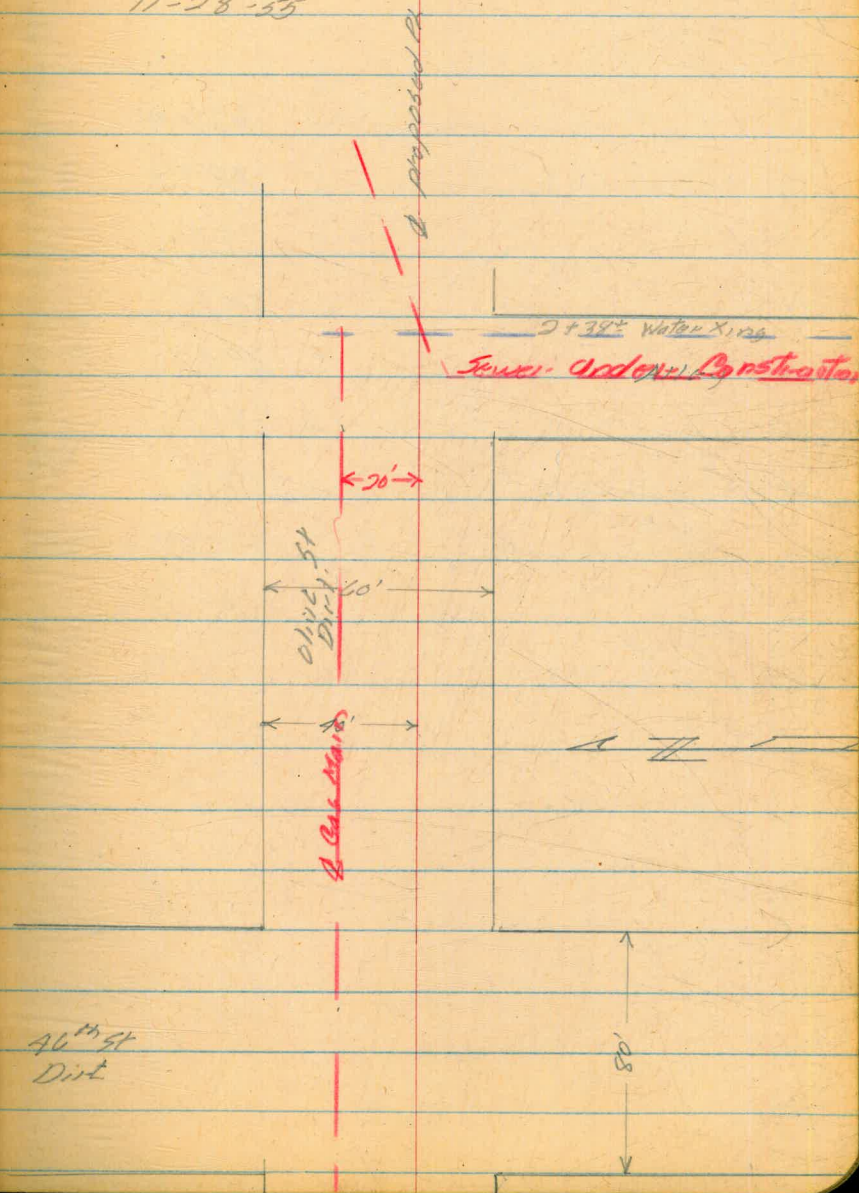
0+27

Ed. Conc. Man 3' R1

0+00

Wly prop Line 46th

46th St
Dirt



Olive St 46th to Alley East
of 46th & profile

	7.81	298.88	291.07
0+00		9.4	289.4
+50		5.5	293.3
1+00		2.2	296.6
+25		1.5	297.3
+50		2.7	296.1
2+00		7.3	291.5
+43 ⁵		10.6	288.2

8.03 290.85

7.81 291.07

Reduced by $3-1-50$ *Pabunna*

= 290.71
= 291.07

Wly prop line 46th

city prop line Alley

Nail in PP SW cor Alley & Olive ^{City Eng}

Springfield St
Paradise St to 600' North

West
Williams
Voronfakis
Kullhofer

28

11-29-55

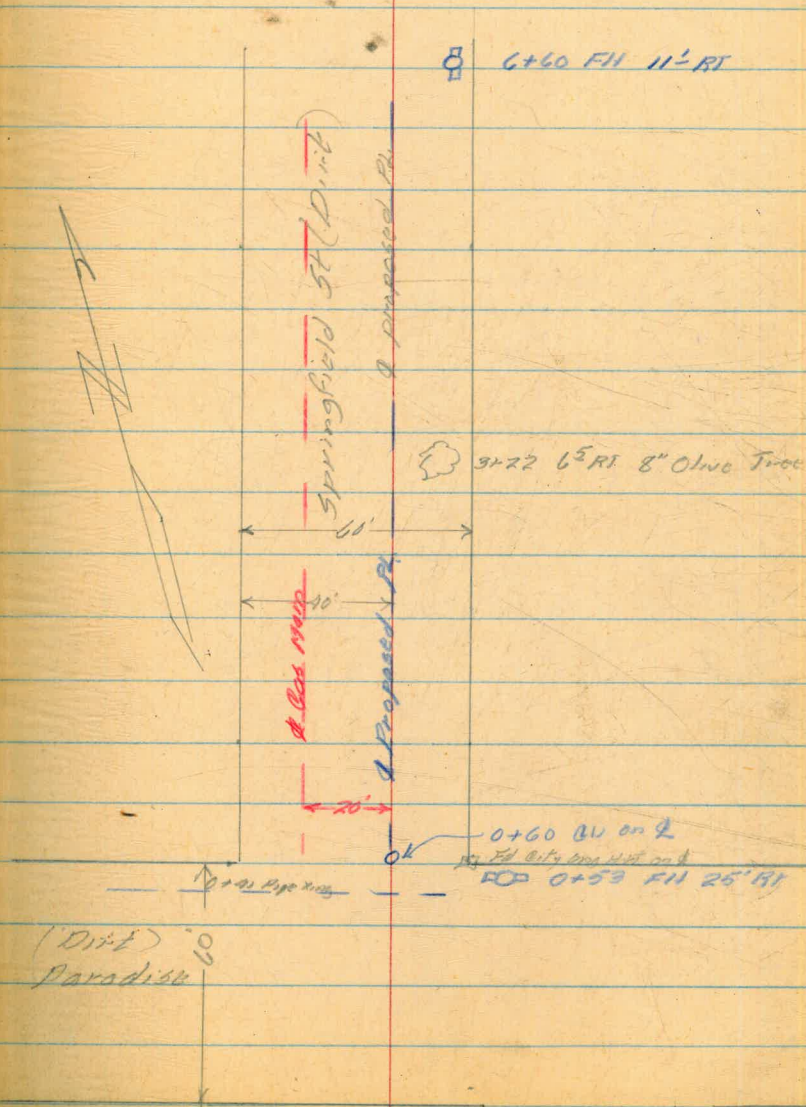
6+60 P.O.T

3+11.75 P.O.T

0+60 P.O.T

0+00

Sty prop line Paradise



Profile Springfield

TBM	6.23	440.40	434.17	FB 85% 89.4
0+00			28	437.6
+09			4.9	435.5
+16			5.8	434.6
+50			5.9	434.5
+56				
+66				
1+00			8.3	432.1
+50			10.0	430.4
2+00			13.0	427.4
TP	+0.76	427.83	-13.33	427.07
+50			5.9	421.9
3+00			11.3	416.5
+50			13.2	414.6
4+00			13.9	413.9
+50			13.3	414.5
5+00			11.0	416.8
+50			6.3	421.5
6+00			0.3	427.5

NE Cor
TBM Top Ell Springfield + Paradise
Sly prop line Paradise st

Begin 5 Mail Boxes 15' RI
end " " " "

8.0	7.5	7.8
5' 11"	2' RT	10' RT
9.7	9.7	9.2
5' 11"	3' RT	5' RT
12.8	12.3	
5' 11"	3' RT	
5.8	5.3	3.5
5' 11"	5.5' RT	8' RT
11.2	11.1	10.6
5' 11"	2' RT	6' RT
		9.2
		8' RT

		427.83		
TP	9.98	437.68	0.13	427.70
6+50			5.9	431.6
6+60			5.3	432.4
PD	+ 1.60	437.38	1.90	435.78
PD	5.17	440.37	2.18	435.20
CL TBM.			- 6.22	434.15 = 434.17

TP Top FH 11² Rt 6+60

Top FH - Springfield + Paradise

Water Meters

1+07	West	6500	✓
2+77	West	New House	✓
3+08	East	6593	✓
3+22			
4+13	East	6605	✓
4+35	West	6610	✓
4+81	East	6621	✓
6+10	East	6629	✓

SAN ONOFRE TERRACE
Olvera Ave to Santa Isabela

8+35 S Wly prop line Santa Isabela

7+70.01 EC

$\Delta = 28^{\circ}37'05''$
 $\frac{1}{2}\Delta = 14^{\circ}18'32''$
 $R = 295'$
 $L = 147.35$
 5.827' per ft
 $T = 75.24'$

6+22.66 PCC

$\Delta = 18^{\circ}13'00''$
 $\frac{1}{2}\Delta = 9^{\circ}06'30''$
 $R = 965'$
 $L = 306.81$
 1.781' per ft
 $T = 154.71$

3+15²⁵ BC

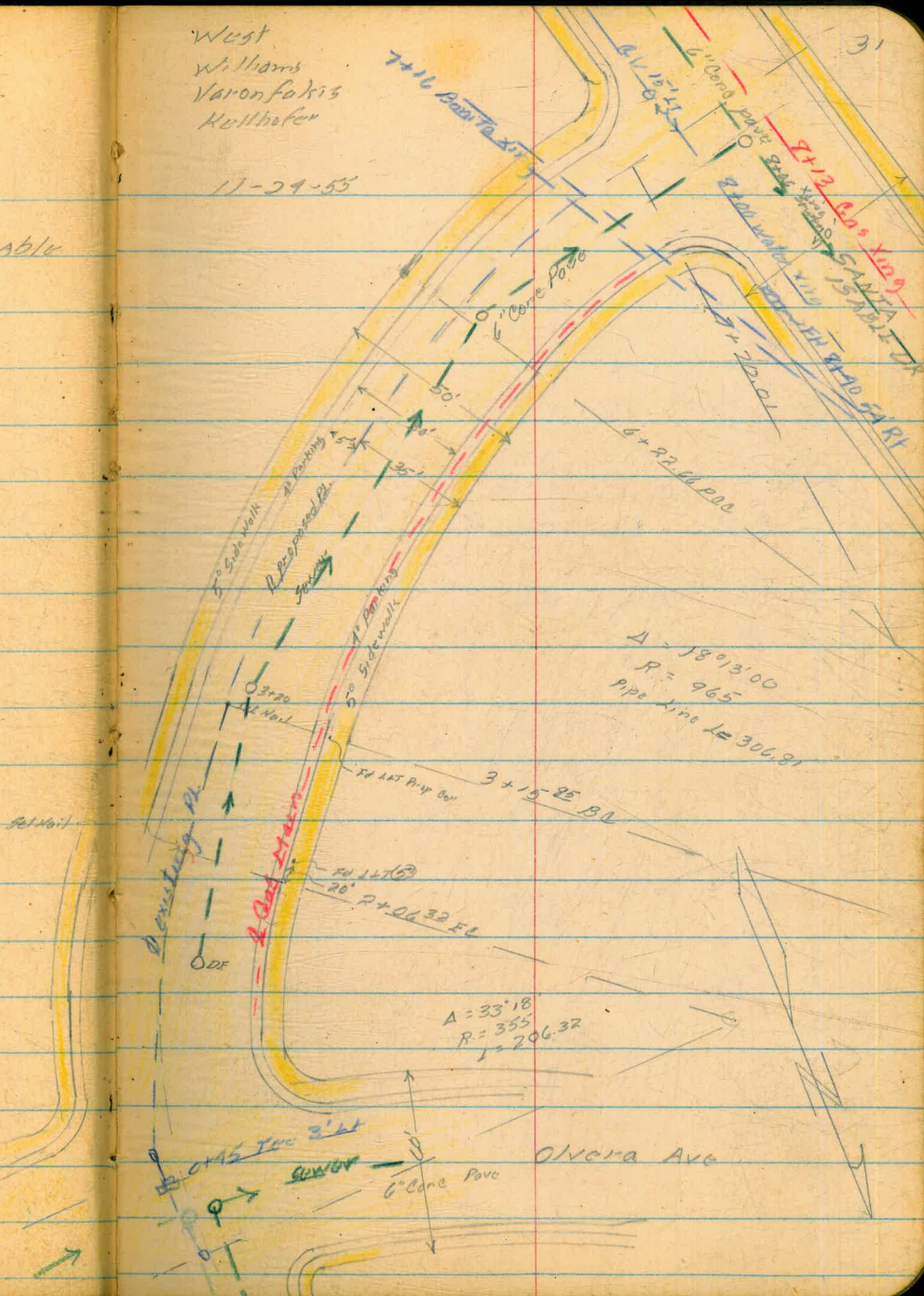
2+06³² EC

$\Delta = 33^{\circ}18'00''$
 $\frac{1}{2}\Delta = 16^{\circ}39'00''$
 $R = 355'$
 $L = 206.32$
 4.824' per ft

0+00 NEly prop line Olvera Ave \rightarrow

West
Williams
Varonakis
Kullhofer

11-29-55



San Onofre Terr
 & profile

10.85	162.62		151.77
12.87	175.01	0.48	162.14
13.09	197.79	0.30	194.71
0.44	175.07	13.16	194.63
12.39	186.07	2.39	172.68
11.12	193.21	2.95	182.12
10.96	203.28	0.92	192.32
1.81	205.04	0.05	203.23

Reduced by A.E. Mathison
 12-5-55

0+00		1.74	203.3
0+07			
0+39		2.37	202.6
0+50		2.53	202.5
0+69		3.52	201.5
1+00		5.57	199.5
1+15			
+50		7.63	197.4
2+00		8.52	196.5
+50		9.25	195.7
3+00		10.51	194.5

11-29-55

BM Santa Maria + Trinidad & Ch Ret BP

Top FH San Onofre Terr + Santa Fe RR

P170192

Spike in PP 58 bet ONofre St + San Onofre Terr

CV 1 1/2 RT

Top Ely Rim Sewer MH 9.R1

3' RT TO CV

12' RT SEWER DE

	205.0A		+7.8 To Flow Line
3+19		1106	193.9
3+50	TPM1	193.41	12.74 192.30
4+00		3.77	189.6
+50		6.19	187.2
5+00		7.71	185.7
+50		8.51	184.9
6+00		9.02	184.4
+26		9.30	+7.0 To Flow 184.1
+50		9.51	183.9
7+00	R 221	195.64	9.98 183.43
+50		2.54	183.1
8+00		2.87	182.7
+06.		3.14	+9.3 To Flow 182.5
+24		3.30	182.3
+24		2.82	182.8
0.59	182.70	3.53	182.11 = 182.12
0.48	172.58	10.60	172.10
9.70	179.31	2.97	169.61
13.35	179.76	12.90	166.41

Top Sly Rim Sewer-MH 7⁵ RT
Water Meters

0+96 South
2+12 South 5477
2+75 South 5469
3+86 South 5463
3+47 North 5460
3+49 South 5455
4+12 North 5450
4+54 South 5447
5+13 South 5439
5+35 North 5432
5+72 South 5433
6+11 North 5420
6+31 South 5421
7+48 South 5405

Top Sly Rim Sewer-MH 6' RT

11' RT Top South Rim Sewer MH

Butter Line Wly Line Santa Isablo

Top of Ch

Top Fire Hyd NE Cor. Santa Isablo^{OnoPia} San

San Onofre Point

59

179.74

12.73 192.01 0.48 179.28

8.16 199.85 0.92 191.01

0.85 196.57 3.53 195.72

2.68 196.12 2.93 193.74

6.76 189.66 = 189.45

Q LTT Church Ward + San Jacinto

AMALFI ST TORREY Pines Rd
to Hillside Dr Proposed PL

FO = 5+93.15 6° 11' 10" RT to Mass Sewer

$\Delta = 28^{\circ} 29' 41''$
 $R = 315.50$
 $L = 156.38$
 5.498093' per ft

BC 4+36.77 = 4+80.65 FB 2303

MH & Pumps

TORREY PINES RD

$\Delta = 28^{\circ} 29'$
 $R = 315.50$
 $L = 156.38$

BC 4+36.77

West
Williams
Varenfakis
Kelhofer

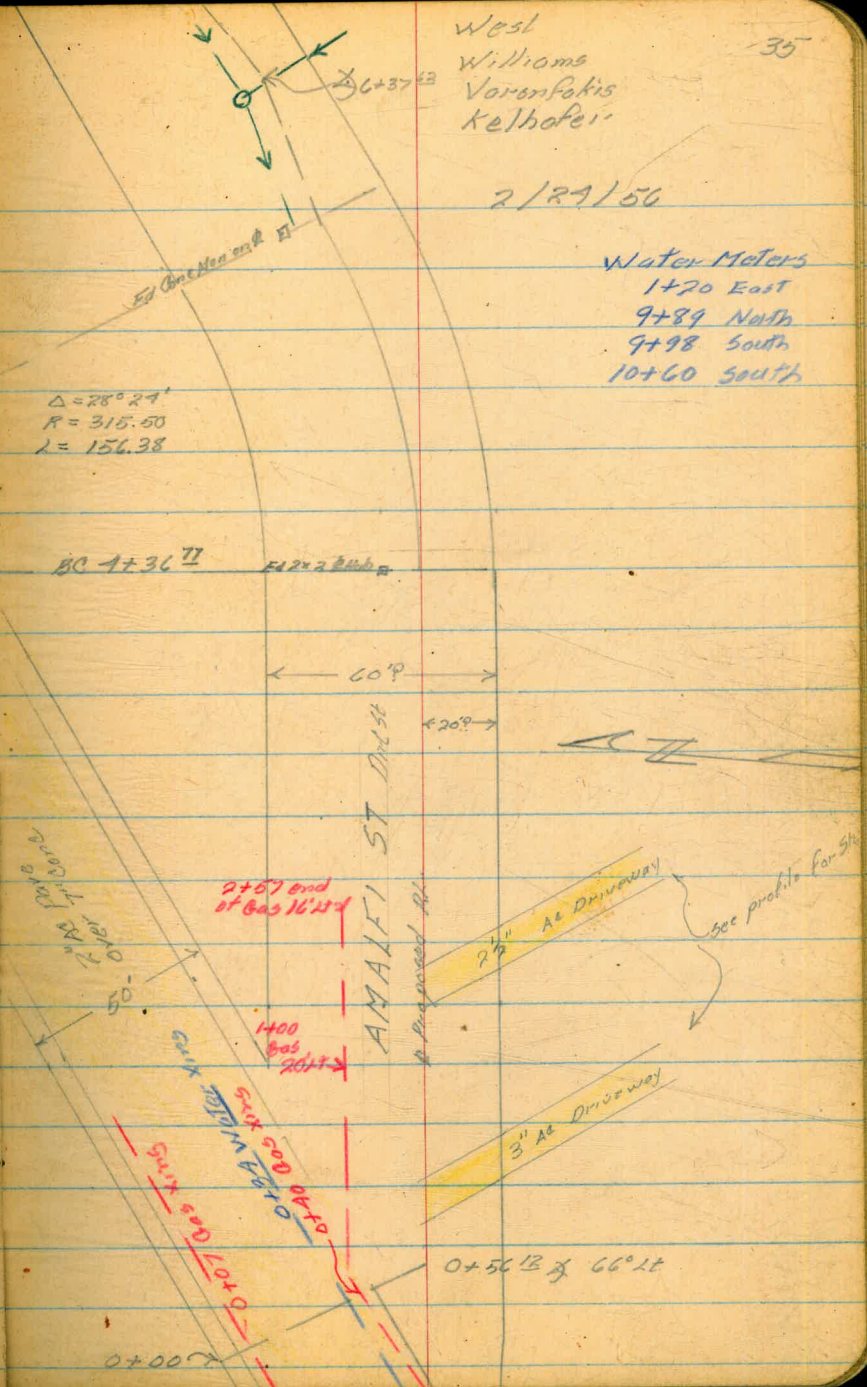
35

2/27/56

Water Meters
 1+20 East
 9+89 North
 9+98 South
 10+60 South

0+56.12 Δ 66° LT = 1+00 @ Sta FB 2303

0+00 ± Nly prop line Torrey Pines Ad



Page 18

AMALFI ST Cont

HILLSIDE Dr

10+73 Begin
2" AC on Main

NOTE: SEE F.B. 380
69
FOR NEW ALIGNMENT

9+52 ³² EC

$\Delta = 22^{\circ} 34' 27''$
 $R = 395.58$
 $L = 155.80$

7+96 ⁵² BC

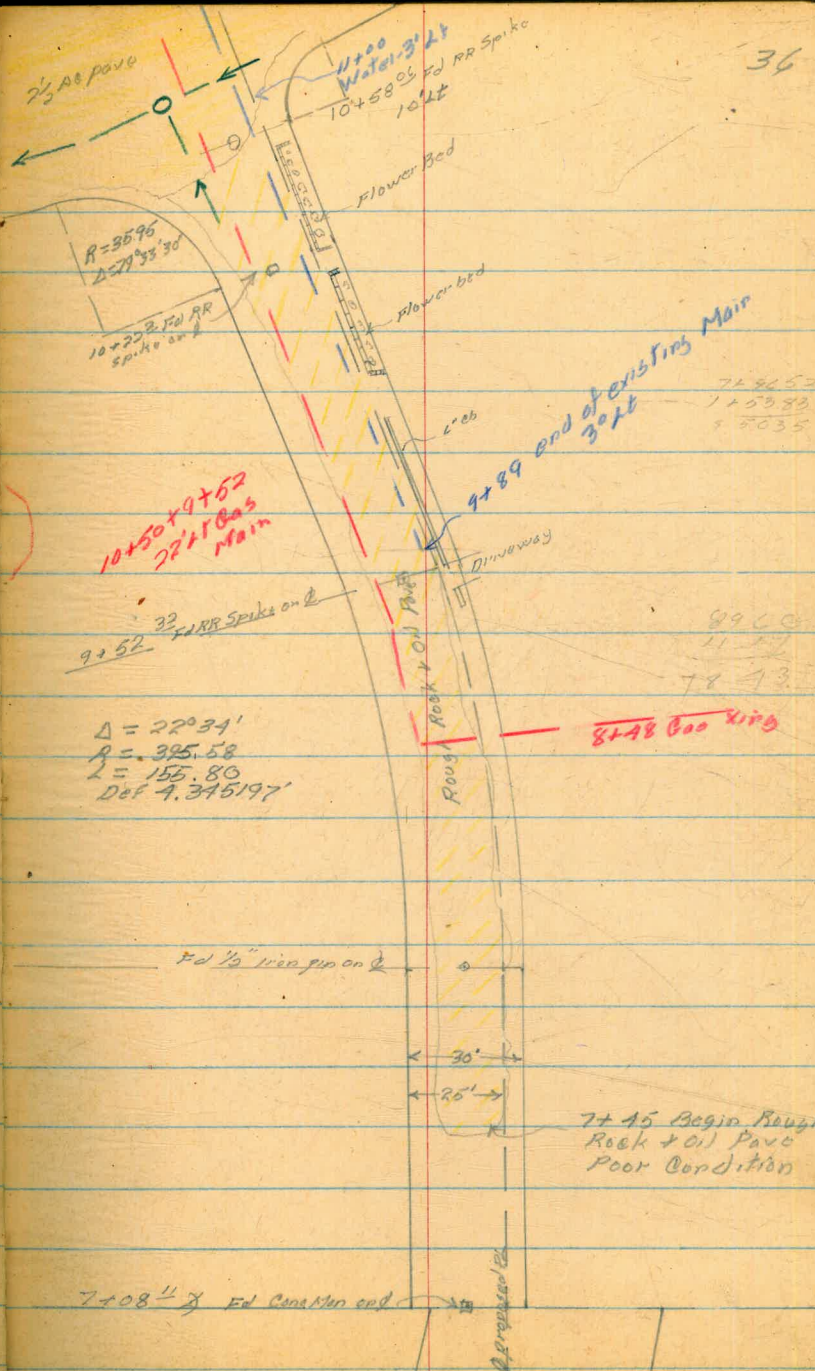
7+58 ¹¹

$3^{\circ} 55' 00''$ RL

6+37 ⁶²

$10^{\circ} 11' 50''$ LT

SOWER MH 5' LT



2 1/2" AC pave

11+00 Water 3" LT
10+58 0.5' Rd RR Spike
10' LT

Flower Bed

Flower bed

10+22 2" Rd RR Spike on 2

2" es

9+89 end of existing Main
30' LT

7+86 52
7+53 83
7+53 55

10+50 + 9+62
22' 1" Gas main

9+52 32" RR Spike on 2

Driveway

Rough Rock + Oil Pave

8+48 Gas King

89 60
11 52
78 43

$\Delta = 22^{\circ} 34'$
 $R = 395.58$
 $L = 155.80$
Def 4.345197'

Ed 1/2" iron pipe on 2

30'

25'

7+45 Begin Rough Rock + Oil Pave Poor Condition

7+08 ¹¹ Ed Connection end

Proposed 12"

AMALFI ST
Proposed RL

2.06	102.91	100.35
0+00		7.89
+05 ⁵		7.98
+05 ⁵		8.39
+20		7.91
+39		8.36
+50		6.7
+56 ¹³		3.4
+69		2.2
+100		5.3
		edge AE Driveway
+25		11.60
		NE edge AE Driveway
+42		10.22
+50		10.6
+78		12.6

Wed
Williams
Varonfatis
Kullhofer

37

2/27/06

From FB R303 P 20

75' West of 0+00

BM Nail in Power pole #1850 Nly Side of Torrey Pines Rd

Nly prop line Torrey Pines Rd

Top of Ck

Cutter Line

of Torrey Pines Rd

Cutter Line South Side

$\frac{8.7}{12.11}$

$\frac{6.0}{10.81}$

Section Taken 90' Back Top $\frac{9.8}{23.21}$

$\frac{1.5}{10.81}$

$\frac{11.3}{7.11}$

$\frac{5.6}{7.11}$

$\frac{3.0}{10.81}$

$\frac{12.6}{9.11}$

$\frac{7.2}{6.81}$

$\frac{6.4}{10.81}$

$\frac{13.5}{10.11}$

$\frac{8.6}{11.81}$

$\frac{14.0}{9.11}$

$\frac{8.7}{5.81}$

edge driveway

$\frac{15.6}{4.11}$

$\frac{8.6}{9.81}$

60
4.3
1.4

102.41

61

RT

202 91.33 13.10 89.31

W/ edge driveway

1+79 4.7

2+00 5.16

2+11 6.00

2+50 7.29

2+77 14.31

3+00 7.39

+50 6.23

4+00 2.57

12.76 103.81 0.28 91.05

+36⁷² BE 12.6

+50 10.2

5+00 0.6

12.64 115.57 0.88 102.93

+50 10.0

5.61

end driveway RT

3.74

15 RT

3.98

10 RT

8.91
14.21

20 RT Elbow line 24" Storm Drain

10.5
3 RT

10.4
8 RT

9.0
10 RT

11.3
3 RT

6.4
4 RT

4.2
13 RT

7.5
7 RT

3.4
5 RT

11.7
11 RT

10.10
4.20
2.8

14.3
4 RT

5.8
3 RT

	115.57		
5+93 ⁵		10.2	
6+00		9.8	
6+37 ⁶² 2		7.25	
6+37 ⁶		7.43	+8.3 To Flow
7+00		0.5	
	12.16	127.49	0.24 115.33
7+08 ² 2		11.1	
+50		7.6	
+91 ⁵² BC		6.5	
8+50		5.3	
8+95			
9+00		5.3	
+09			
+24			
9+52 ³² rc		6.3	
+74			
+74			
+91			
+94			

5' RT Top East Rim Sensor 114

Dead man 5' RT

4' RT P1891 Power pole

Begin 6" Cone Ob 2° RT

1' RT to Ob

end of Ob 1' RT

Begin Cone Driveway 1° RT

end " " "

Begin brick enclosed Flower Bed 1° RT

	127.49		
10+00	6.99		2' RT brick border
+03			begin Conc sidewalk 0 ² RT
+17			end " " 0 ² RT
+17			begin brick Flower-bed 1 ⁵ RT
10+50	7.50		end " " " 2 ⁰ RT
+57			2 ⁰ RT 48" Dia Palm Tree
+58			1 ⁰ RT power pole P7825
11+00	6.31		
		+6.2 To Flow	
10+74	8.40		Top Sly rim sewer MH 18' LT
			1 ¹ RT 9+09
	1.53	122.96	= 122.95 Nail in PP # P1891 FB 2123 PG

TWAIN AVE Crawford to Mission
Gorge Rd

Pelms

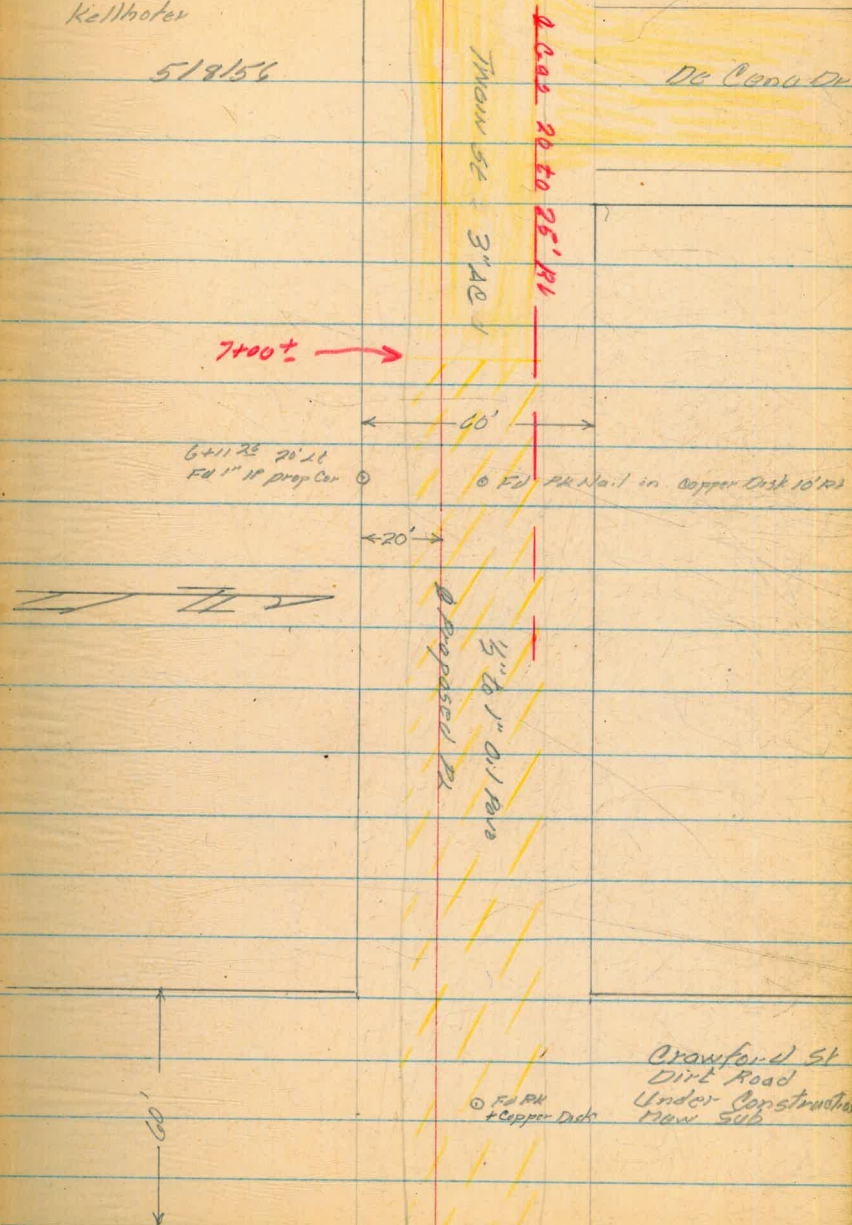
6+11²⁶ POT FD 1" IP Prop Cor- 20' Lt
Ed City Eng PK + Copper Disk 10' Rt

0+30 POT BE 1534 10' Rt
Crawford St FD PK + Copper Disk

0+00 Ely Prop Line Crawford St

West
Williams
Varon Lakes
Kellhofer

5/9/56



TWAIN AVE Cont

Turned $\Delta = 64^{\circ} 56' 00''$ [RCS $64^{\circ} 52' 45''$]
 $R = 925'$
 $L = 1048.20'$
Def = 1.858' per ft

12+86 ²⁸ BC

11+75 ⁴¹ X

89° 43' 20" Lt

10+70 ²⁹ POT

Ed PK Now 10' Rt

12+86 ²⁸ BC = 22+97 ⁰³ County "A"

13+78 ²⁹ BC

13+61 ²⁹ BC

10+93 ²⁹ Begin 36 10' Lt

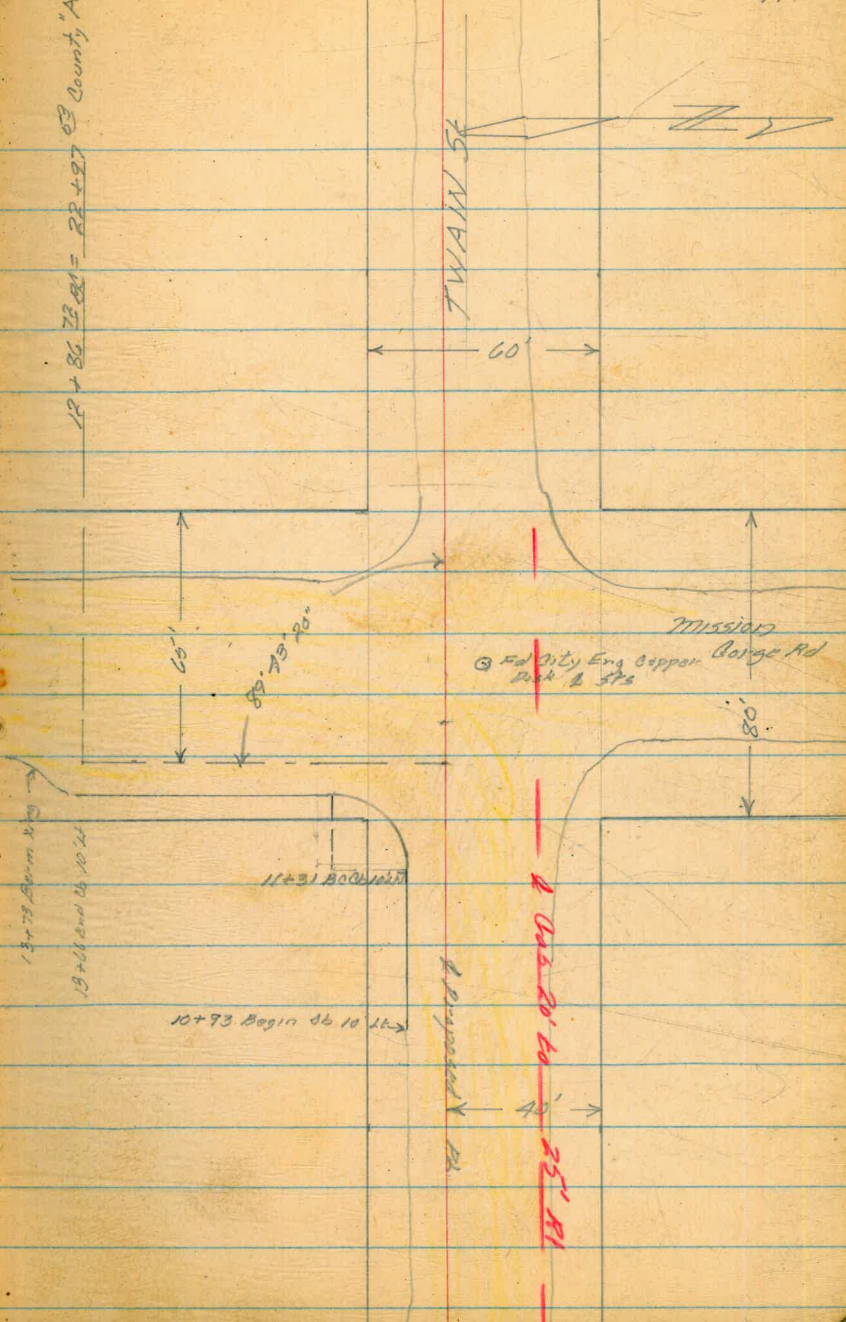
11+51 ²⁹ BC

Proposed

TWAIN ST

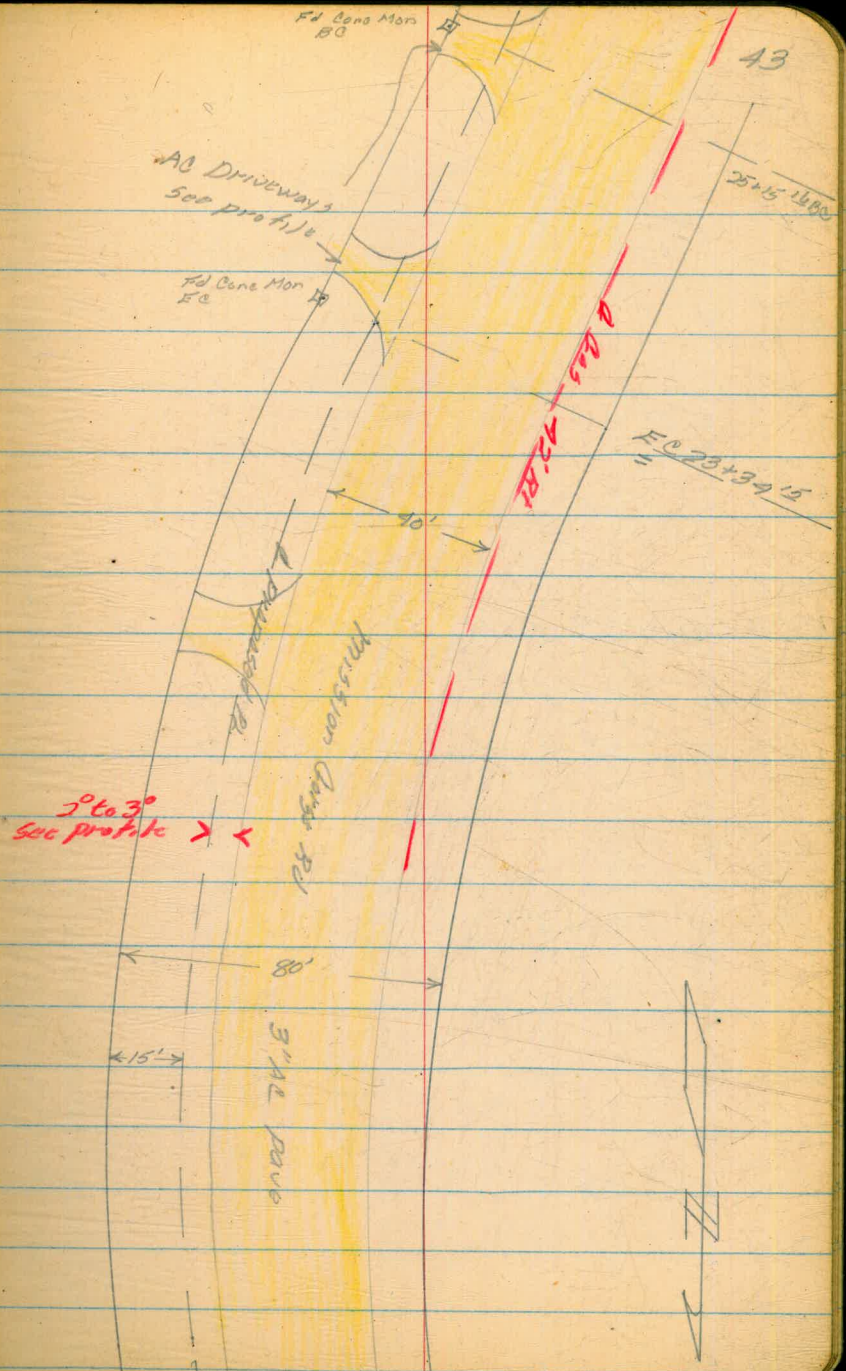
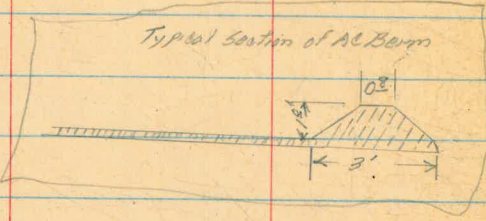
MISSION
City Eng Copper Barge Rd
Dist 2 572

42



MISSION GORGE Rd
 Twin Ave to Fairmount EXT

23+35 ⁰² EC



MISSION GORGE RD Cont
 Fairmount Ext Mission Gorge Rd to 450N

1+62⁶⁶ POT = 6+60"5" Line

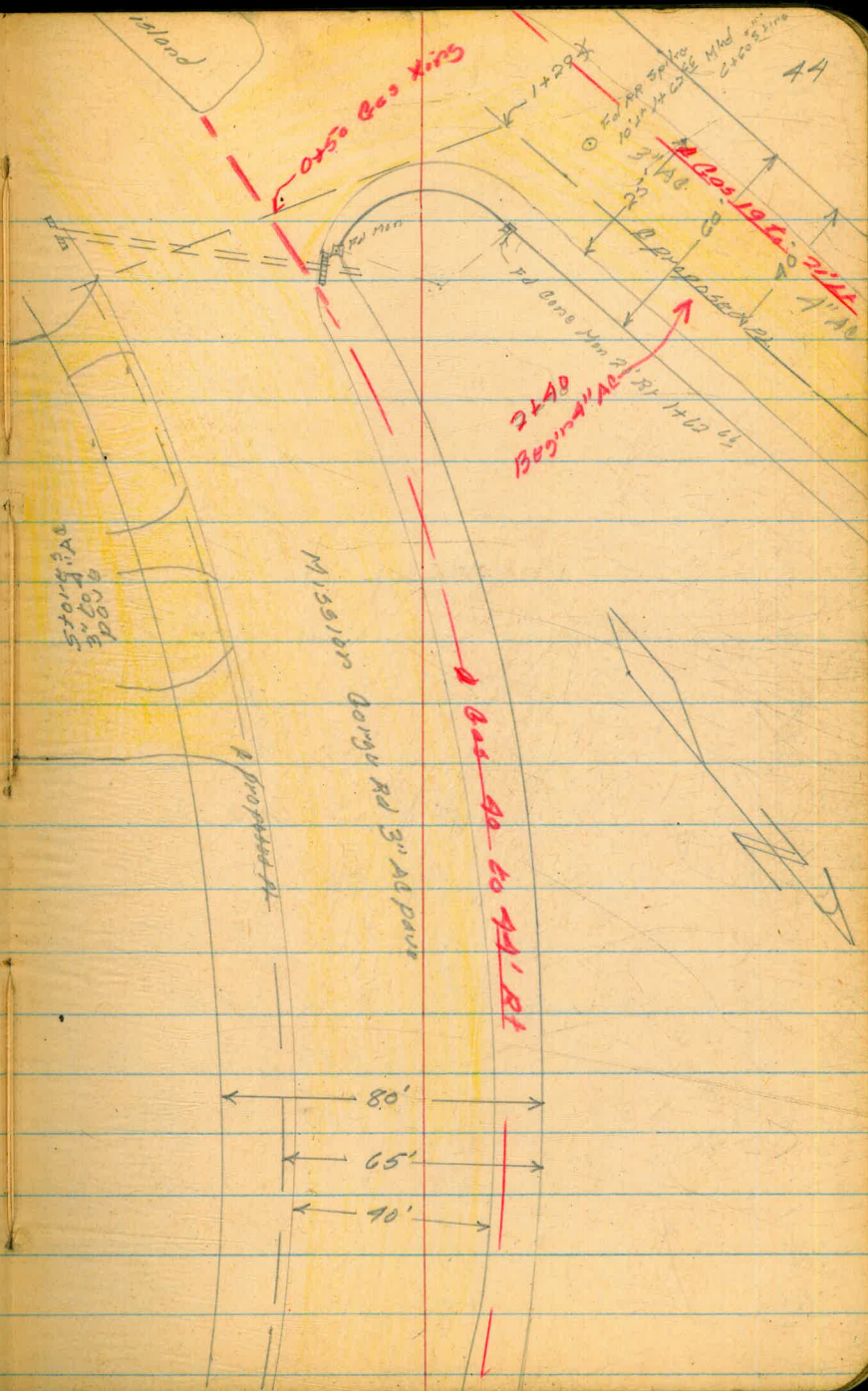
1+29 Δ 65° 15' 20" Rt

29+95 = 0+00
 29+95 EC + Δ 85° Rt off Tangent

29+00 P.O.C

$\Delta = 35^{\circ} 24' 38''$
 $\frac{1}{2}\Delta = 17^{\circ} 42' 19''$
 $R = 775'$
 $L = 479.40$

25+15⁶⁰ BC



Q Profile Twain Ave Mission Gorge
RD + Fairmount Est

			77.30
			-6.12
3.38	74.56		71.18
6.83	74.22	7.17	67.39
4.77	76.18	3.81	70.41
5.72	76.61	4.29	70.89
13.09	98.73	0.96	75.65
13.03	101.29	0.47	88.26
13.03	113.92	0.40	100.89
8.26	121.48	0.70	113.22
5.46	123.85	3.09	118.39
13.10	136.54	0.41	123.44
12.68	148.90	0.32	136.22
8.15	153.65	3.40	145.50
0+00		0.78	152.77
+50		7.12	146.53
0.66	141.78	12.53	141.12
1+00		1.65	140.13
+50		7.89	133.89

NOTES Reduced by A. Mathison
5-14-56

45

ADD +10' to Sta for new alignment FB 872 aem.
ON MISSION GORGE Rd - Twain to Sta 30+00

5/9/56

U.S.C.S.
BM Ohio \square NE Wg wall of Bridge

City Datum

Turn on City Peg PK Nail + Copper Disk 108+00

1.01
75.21 Begin Berm Fly prop Lime Chalkford

7.39
75.21 Begin Berm

1.83
58.11 Begin Berm

8.10
50 " "

141.78

0.58 129.63 1273 129.05 ✓

2+00 1.83 127.80

+50 6.36 123.27

3+00 8.75 120.88

+50 9.64 119.99

4+00 10.12 119.51

4.76 123.51 10.88 118.75 ✓

4+39 10.23 113.28

4+39 8.39 115.12

4+50 4.43 119.08

5+00 4.89 118.62

5+32 5' LT end AC Perm

+50 5.22 118.29

6+00 5.99 117.52

+50 7.58 115.93

7+00 10.37 113.14

0.85 113.50 10.86 112.65 ✓

+50 4.76 109.24

8+00 8.68 104.82

2.0
5' LT Basin AC Perm6.50
5' LT " " "8.50
5' LT " " "9.80
5' LT " " "10.36
5' LT " " "

21' LT Flow Line 24" Conc Drain

34' RT Flow Line 24" Conc Drain

4.64
5' LT Basin AC Perm5.08
5' LT " " "

5' LT end AC Perm

5.43
5' LT edge of pave6.57
5' LT " " "7.90
7' LT " " "10.66
8' LT " " "5.00
4' LT edge of pave8.92
7' LT " " "

	113.50		
9+50	0.92	101.21 ✓	13.21 100.29 ✓
9+00		3.57	97.64
+50		5.03	96.18
10+00		7.29	93.92
+50		11.80	89.41
	0.41	89.21 ✓	12.41 98.80 ✓
11+00		5.95	83.26
+50		11.93	77.28
	0.30	79.79 ✓	9.72 79.49 ✓
+75 11		1.20	75.59
12+00		4.64	75.15
+50		5.01	74.78
12+86 ^B BC		5.10	74.69
13+00		5.13	74.66
+50		5.54	74.25
13+72		5.47	74.32
+73		4.87	74.92

$\frac{13.7}{10.21}$ edge of pave

$\frac{3.91}{9.11}$ " " "

$\frac{7.69}{8.21}$ LT edge AC pave

$\frac{6.37}{10.11}$ Edge of Ob

Mission Bridge Rd
Turn on RR Med NE Cor Twain St

$\frac{4.38}{14.26}$ Face of Ob

$\frac{4.35}{15.11}$

$\frac{5.62}{9.24}$ Face of Ob

$\frac{4.89}{15.11}$

AC
Begin a Barm Xing

Top of Barm

	79.79		
13+75	5.59	74.20	
13+90			
14+00	5.8	74.0	
+50	5.9	73.9	
15+00	6.6	73.2	
+50	6.8	73.0	
16+00	352 76.33 [✓] 6.98	72.81 [✓]	
+50	7.0	72.3	
16+54			
17+00	4.0	72.3 73.2	
+50	4.1	72.2	
+50	8.57	67.76	
18+00	4.5	71.8	
+50	4.7	71.6	
+90			
19+00	4.8	71.5	
+50	4.8	71.5	

5/10/55

End AC Berm

Guy pole 3° Lt

5.7
15' Lt5.7
15' Lt5.6 edge Berm 5.65
2° Rt 15' Rt6.8
15' Lt6.6 edge Berm 6.55
3° Rt 15' Rt7.0
15' Lt7.1 edge Berm 7.24
2° Rt 15' Rt

Pedestrian Xing Sign 0° Lt

4.3
15' Lt4.2 edge Berm 4.35
2° Rt 15' Rt

55' Rt Flow Line 18" CMPA

4.7
15' Lt4.5 edge 4.60
2° Rt 15' Rt

End of Berm 3° Rt Begin Drive way

Begin AC Berm 3° Rt End "

4.3
15' Lt4.7 edge 4.84
3° Rt 15' Rt

76.33

20+00 4.6 71.7

$\frac{4.6}{15'LL}$

$\frac{5.0}{3'RT}$

$\frac{5.18}{15'RT}$

1 +50 4.63 75.62 ✓ 5.34 70.99 ✓

$\frac{9.2}{15'LL}$

End of Filled Area to Left

+76 5.0 70.6

21+00 5.0 70.6

$\frac{9.3}{15'LL}$

$\frac{9.1}{8'LL}$

$\frac{4.6}{3'RT}$ edge

$\frac{4.70}{10'RT}$ Berm

+50 4.8 70.8

+59

3" AC
2nd RL End AC Berm 3rd RT Begin AC Driveway

+70 5.21 70.41

$\frac{7.14}{15'LL}$

+85

2nd RL Begin Berm

End AC Driveway

22+00 5.1 70.5

$\frac{8.9}{15'LL}$

$\frac{9.0}{8'LL}$

$\frac{5.0}{3'RT}$ edge

$\frac{5.00}{15'RT}$ Berm

+50 5.3 70.3

23+00 6.0 69.6

$\frac{8.8}{15'LL}$

$\frac{8.9}{7'LL}$

$\frac{5.2}{2'RT}$ top

$\frac{5.3}{3'RT}$ edge

$\frac{5.12}{15'RT}$ Berm

+35⁰³ EB 5.5 70.1

+50 5.8 69.8

+50

BUS STOP SIGN 0th RT

+57

3 Mail Boxes 1st RT

+64

1" AC
End AC Berm 2nd RT Begin AC Driveway

24+00 3.87 73.15 ✓ 6.04 69.58 ✓

$\frac{7.3}{15'LL}$

$\frac{5.88}{15'RT}$

+06

Begin AC Berm 3rd RT

End AC Driveway

	73.45		
24+50		4.1	69.4
24+99			
25+00		4.6	68.9
+35			
+50		4.6	68.9
26+00		4.9	68.7
+50		5.0	68.5
26+69			
+98			
27+00		4.96	68.49
+50		5.20	68.3
27+75			
+77			
+86			
+93			
28+00		5.55	67.90
422	72.76 [✓]	1.91	68.54 [✓]
+44			
+50		5.19	67.63

2^o Rt end AC Berm Begin AC Driveway
 $\frac{6.3}{15' Lt}$ $\frac{4.16}{15' Rt}$

2^o Rt Begin AC Berm end AC Driveway

$\frac{7.2}{15' Lt}$ $\frac{7.0}{6' Lt}$ $\frac{4.8}{20' Rt}$ edge Berm $\frac{4.45}{15' Rt}$

4" AC Paved Area to 2^o
 2^o Rt end AC Berm Begin AC Driveway end

2^o Rt Begin AC Berm
 $\frac{4.97}{15' Lt}$ AC area $\frac{4.87}{20' Rt}$ edge Berm $\frac{4.77}{15' Rt}$

2^o Rt 3 Mail Boxes on wooden stand
 Deadman 18" Lt
 PP 18" Lt # 79916

2^o Rt end AC Berm Begin AC Driveway
 $\frac{5.36}{15' Lt}$ AC paved area $\frac{5.21}{15' Rt}$

3^o Rt Begin AC Berm

ON DRAWING
 NOTE: 0+00 Fairmount Exten.
 = 30+20 Mission George Rd.
 29+70 A. Mathison 5-25-56
 1-14-56 *am*

72.76

29+00	5.09	67.67
29+26		
+44		
+50	5.39	67.37
29+61		
= 0+00		
29+95	5.42	67.34
0-03	9.34	63.42
0+04	5.25	67.51
+25 +15	4.75	68.01
+50 +40	4.72	68.04
+55 +45	8.85	63.91
+81 +		
1+00	5.84	66.92
+29	5.74	67.52
+50	5.28	67.48
2+00	5.39	67.37
+50	5.80	66.96
3+00	5.98	66.78
+50 4.70	71.36	66.66

51

$\frac{5.06}{15' Lt}$	AC paved area	$\frac{5.03}{25' Berm}$ edge Berm	$\frac{4.74}{15' Rt}$
Deadman 0 ⁵ Lt		Bus Stop Sign 0 ³ Rt	
4 ⁰ Lt	pp. # D473226		
		3" AC	
		2 ⁵ Rt end AC Berm Begin AC Driveway	
		22' Lt Flow line 24" Core Drain	
		End AC Berm 0 ³ Lt	
		0 5t	
34' Rt	15' Rt edge AC Berm		
41' Rt	22' Rt Flow line 24" Core Drain		
20' Rt	0 ² Rt edge AC Berm		
21' Rt	$\frac{60'}{3' Rt}$ edge AC berm		

71.36

5/10/55

4+00	4.61	66.75
+50	4.62	66.74
5+00	4.57	66.79
+50	4.69	66.72
6+00	4.60	66.76
+50	4.44	66.92
7+00	4.21	67.15
+45 ⁵	4.07	67.29

7.37 74.10 4.63 66.73

176 74.53 1.33 72.77

3.39 71.14 = 71.18

74.6 City Elev

79.49 (79.47)

R 0.94 80.43

CK BM. 6.11 74.32 = 74.23

+ 6.12
80.44 = 81.38

BM. 5.39 76.57

77.30 USGS
- 6.12
71.18 City Datum

5.37 71.20 = ?

4.96 71.61 = 71.49

BM Chris II Wing Wall Bridge

Hwy dept Row Marker, Bl. Mon NE Cor Mission

{ 5715-D
Chris II Hdwall. NE Cor Twain & Mission Gorge Rd

2550-D (Mk'd 80.48 on Grd post)

Chris II on NE W.W of Bridge pg 45

{ A-896 1955
USCGS BM NW Cor Fairmount & Mission Valley

Mon w/L Fairmount N/L Mission Valley Fwy

FAIRMOUNT EXT

Sta 7+45 to Twain Ave.

	5.20	72.49		67.29 ✓
8+00		5.15		67.34
+50		5.13		67.36
9+00		5.01		67.48
+50		4.96		67.53
10+00		4.94		67.55
+50		4.74		67.75
11+00		4.50		67.99
+50		4.29		68.20
12+00		4.14		68.35
+50		3.86		68.63
13+00		3.71		68.78
+50		3.19		69.30
TP	2.28	73.40	1.37	71.12 ✓
14+00		2.20		71.20
14+13.22		2.00		71.40
= 0+40 Twain St				

Reduced by A. Mathison
 10-8-56

West
Williams
Kellhofer

7/27/56

7+45 Nail Fairmount Extension

5.58
80 ft edge AC pavo

5.39
70 ft " " "

5.39
80 ft " " "

4.86
80 ft " " "

4.71
80 ft " " "

4.21
60 ft " " "

TWAIN ST FAIRMOUNT EXT
TO MISSION BORSE RD

Q profile
73.40

Reduced by
H. Wada 8-10-56

0+50	2.15	71.25	
1+00	3.84	69.56	$\frac{5.02}{1084}$ edge A & pave
+50	4.29	69.11	
2+00	4.29	69.11	$\frac{4.85}{8084}$ " " "
+50	4.29	69.11	
3+00	4.17	69.23	$\frac{4.62}{7084}$ " " "
+50	4.11	69.29	
4+00	4.16	69.24	$\frac{4.70}{7084}$ " " "
+50	4.11	69.29	
5+00	4.12	69.28	$\frac{4.48}{7084}$ " " "
+50	4.16	69.24	
5.44	74.46	4.38	69.08
6+00	5.20	69.26	
+50	5.10	69.36	
7+00	5.16	69.30	$\frac{5.37}{3084}$ edge A & pave
+50	5.12	69.34	
8+00	5.09	69.37	$\frac{5.10}{0284}$ " " "
+50	4.72	69.74	
9+00	4.21	70.25	$\frac{4.34}{30}$ " " "

74.46

9+50 3.73 70.73

10+00 3.19 71.27

+50 2.19 72.27

11+00 0.69 73.77

TP 7.66 81.80 0.38 74.14

+50 6.58 75.22

+ 90²⁷ (Mission Garage Rd) 11+35²¹ 6.18 75.62

2.30 79.50 = 79.49

3.48
40 RT edge AE pave

15' East of D of Mission Garage Rd
see page 47
Emission Gas
TBM Conc Mon NE Cor Twain

West
Williams
Kellhofer

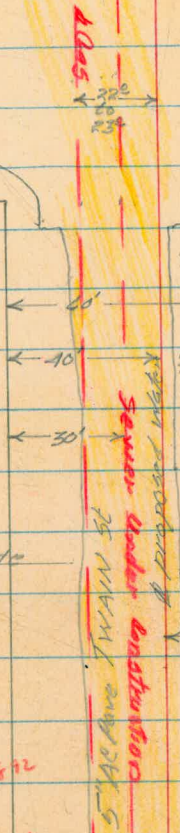
FAIRMOUNT EXT STA 7+45.2 To TWAIN ST 19° 56' 30" 56
TWAIN ST Fairmount Ext To Mission Gorge Rd

7/27/56

11+90²² Twain St
= 11+85⁴¹ Mission Gorge Rd
See page

Mission Gorge Rd

- 10+94 Begin Paving AC Shoulder 6' RL
- 10+76 72" 279857 9' RL
- 10+65 30" Cypress 9' RL
- 10+71 18" Poplar 10' RL
- 9+97 24" Cypress 9' RL
- 9+53 36" Cypress 10' RL
- 9+97 40" 1279557 6' RL
- 9+00 Dup Pole 6' RL
- 8+95 36" Cypress 10' RL



AC Pave 25' to 30' Wide

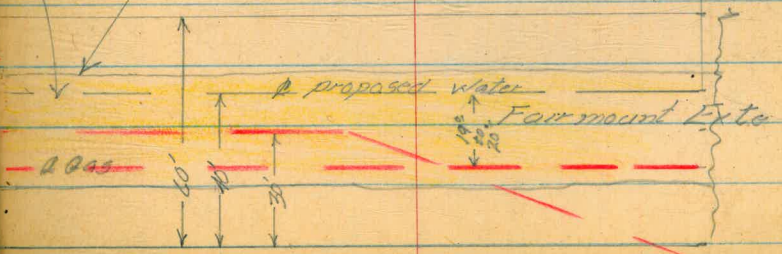


10-8-56
NOTE: Survey 14+13.92 = 14+18.92
SW Drwg. by Mathison
at 00 of Fairmount EXT
changed due to realignment
of Mission Gorge Rd pipeline.
REM

14+13.92 Fairmount Ext
= 0+40 Twain St

Sewer Under Construction
AC Pave 20' Wide

3" AC Pave



7+45.2 Cont Sta from Survey of 5/10/55

MISSION GORGE RD
TWIN ST TO RAINIER

Q Transil Line 15' East of Q St

	1.31	80.80	REDUCED BY	1.64 8-16-56
0+50		5.04		75.76
0+84		9.80		71.00
0+95		9.40		71.40
1+00		4.95		75.85
+50		4.57		76.23
2+00		4.38		76.42
+50		3.95		76.85
3+00		3.3		77.50
+50		3.0		77.80
4+00		2.5		78.30
+50		1.6		79.20
TD	6.76	85.86	1.70	79.10
5+00		6.8		79.06
+50		6.4		79.46
6+00		6.0		79.86
+50		4.8		81.06
7+00		1.5		81.36
+50		3.6		82.26

West
Williams
Kellhofer

57

7/30/56

29.99 TBM Core MOD NE Cor. Mission Gorge
1.97
50ft

47^{ft} Flow Line 24" ID Core Storm Drain

11^{ft} Flow Line 24" ID Core Storm Drain

4.78
50ft

4.36
50ft

4.15
50ft

3.93
50ft

3.30
50ft

3.39

50ft

20ft edge AC pave

2.87
50ft

2.25
50ft

2.98

1.78
50ft

15ft edge AC pave

6.52
50ft

6.71

50ft

20ft edge AC pave

6.21
50ft

5.64
50ft

5.92

50ft

05ft edge AC pave

4.81
50ft

4.48
50ft

4.48

50ft

2.5ft edge AC pave

3.67
50ft

MISSION GORGE RD CONT

Reduced by Lee
8-16-56

85.86

8+00		3.2	82.66
+50		2.6	83.26
9+00		2.0	83.86
+50		0.8	85.06

3.04	3.19
5° LT	2° LT edge AC pave

2.42
5°

1.80	1.92
5° LT	2° LT edge AC pave

0.61
5° LT

JP	6.15	90.21	2.10	83.76
----	------	-------	------	-------

9+95		9.52	80.69 Flow Line
------	--	------	--------------------

9+95		11.58	78.63 Flow Line
------	--	-------	--------------------

9+99 ⁰⁵	Δ	3.8	86.41
--------------------	---	-----	-------

6' RT 1' x 4' Box Culvert

37' LT " " " "

3.37	3.75
5° LT	1° LT edge AC pave

JP	10.70	97.62	3.29	86.92
----	-------	-------	------	-------

Turn on City Eng PK Nail 15" LT 9+99⁰⁵

10+50		8.4	89.22
-------	--	-----	-------

8.14
5° LT

11+00		6.0	91.62
-------	--	-----	-------

5.69
5° LT

6.03
3° RT edge AC

+50		3.97	93.65
-----	--	------	-------

3.62
5° LT

12+00		2.08	95.54
-------	--	------	-------

1.88
5° LT

1.97
3° RT edge AC

+50		1.11	96.51
-----	--	------	-------

0.77
5° LT

JP	6.06	102.70	0.98	96.64
----	------	--------	------	-------

5.14
5° LT

13+00		5.57	97.13
-------	--	------	-------

5.56
1° RT edge AC

+50		4.86	97.84
-----	--	------	-------

1.43
5° LT

JP	4.90	104.94	2.66	100.04
----	------	--------	------	--------

1935	MISSION GORGE RD
Turn on USCLAS # A322	5' Cor. @ 100'.

MISSION GORGE RD CONT

59

Reduced by Lee
8-16-56

10494

13+99⁹¹

4.24 98.70

 $\frac{5.93}{5.014}$ 6.46
5° RT edge AC

14+50

5.57 99.37

 $\frac{5.21}{5.016}$ 5.19
6° RT edge AC

15+00

5.01 99.93

 $\frac{4.69}{5.014}$

6° RT edge AC

+50

4.39 100.55

 $\frac{4.08}{5.014}$ 3.83
6° RT edge AC

16+00

3.85 101.09

 $\frac{3.62}{5.014}$

6° RT edge AC

+50

3.57 101.43

 $\frac{3.26}{5.014}$ 3.26
2° RT edge AC

17+00

3.14 101.86

 $\frac{2.93}{5.014}$

2° RT edge AC

+50

2.79 102.20

 $\frac{2.55}{5.014}$

3.93 107.44 1.43 103.51

 $\frac{1.94}{5.014}$ 17+79⁹¹

5.18 102.26

 $\frac{5.03}{5.016}$ 18+19⁹¹

5.02 102.42

Nly prop line Rainier St

JD

4.39 106.94 4.88 102.56

Turn on US C+BS map #2892 SW Cor. Rainier
Mission Gorge Rd

2.74 101.79 7.89 99.05

0.42 90.53 11.68 90.11

2.83 84.29 9.07 81.46

3.30 80.73 6.86 77.43

1.27 79.46 = 79.49

MISSION GORGE RD

TWAIN ST TO RAINIER AVE

Transit Line 15' East of Q St

9+97.05 Δ 0° 01' 20" RC

0+20 P.O.T Nail (15" R Mission Gorge Rd

0+00 Slightly prop line Twain St

West
Williams
Kollhofer

60

7/36/56

100'

9+97.05 Ed City Eng PK
Nail 15" LF

Gas 20'
9+91

Dirt St

Vandever Ave

9+95 4'x4' Box Culvert King

Transit Line

32'

32'

80'

55'



60'

0+30.75 Ed City Eng PK
Nail 15" LF

24" Storm Drain

0+40 Gas Xing

Twain St

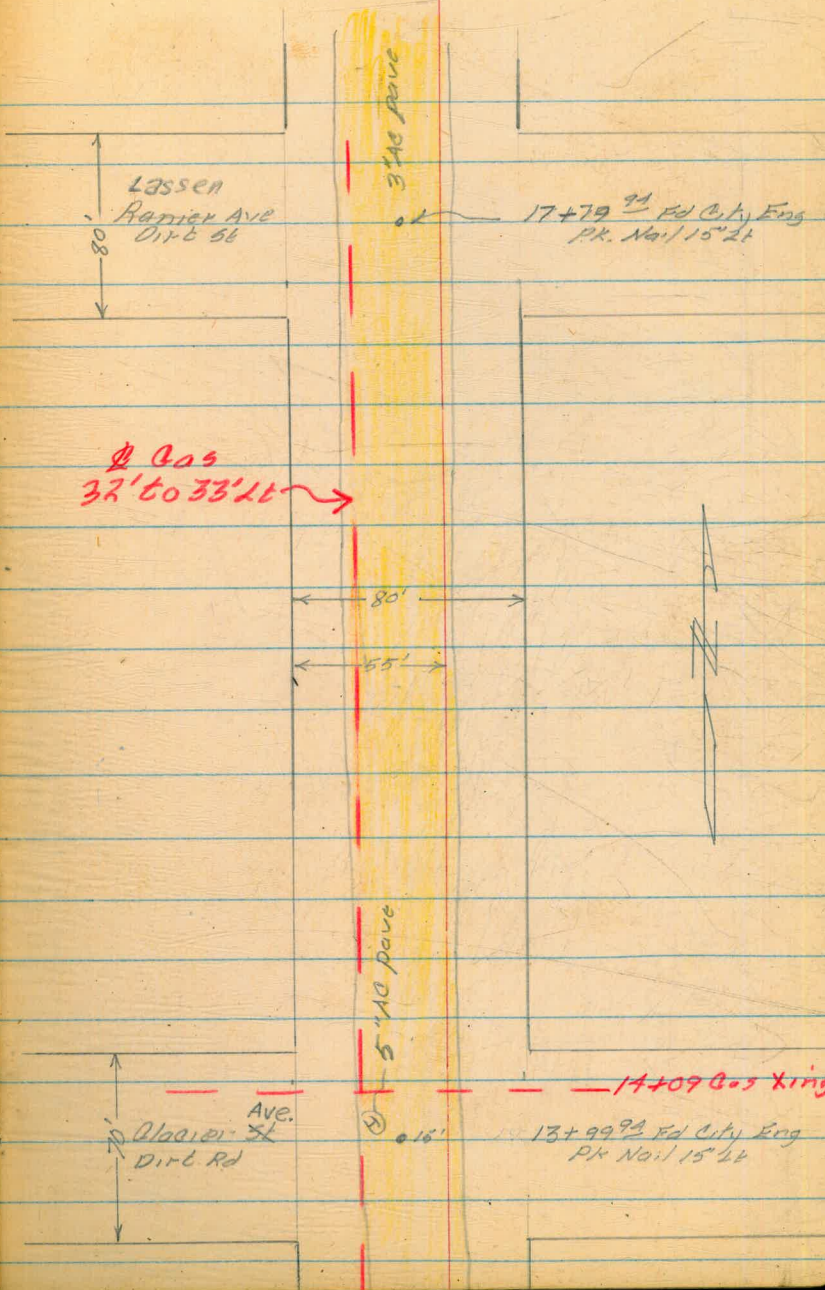
18+19⁹⁴

Nly prop

Line Lassen Ave.
Rainier St

17+79⁹⁴

POT



13+99⁹⁴

POT

Ave.
Rainier X
Dir 6 Rd

13+99⁹⁴ Rd City Eng
PK Nail 15 24

VANDEVER ST. RIVERDALE ST
TO MISSION GORGE RD

Prelim.

6+53⁴² Fly prop line Mission Gorge Rd

6+28⁴² Vandever = 10+00⁸² Mission Gorge Rd

6+13⁷ @ Mission Gorge Rd

5+73⁹² POT

3+73⁹⁵ POT

0+00 Fly prop line Riverdale Rd

West
Wilhams
Kellhofer

970 Road

61

7/21/56

7' All pave on S E
Mission Gorge Rd
6+28⁴² Gas Xing
6+13⁷ City Eng. No. 15344

6⁰ RC
5+91 4' x 4' Conc Box Culvert

5+73⁹² Ed 3/10 RE 1534-40' RI

3+73⁹⁵ Ed 3/10 RE 1534-40' RI

100'

60'

30'

Prange's Ditch

VANDEVER AVE (DUB)

1464
end of Gas

Dirt St

Riverdale (120 Road)

profile Vandever ST.

	1.09	88.01	86.92	
	0.86	75.19	1308	74.93
0+00		6.2	69.	
0+00				68.9 $\frac{6.3}{20}$
				+40 $\frac{5.8}{20}$
0+50		5.7	69.5	
1+00		5.1	70.09	$\frac{69.09}{20}$ $\frac{5.5}{20}$ $\frac{5.5}{20}$
1+50		5.4	69.8	
2+00		6.0	69.19	70.19 $\frac{5.5}{20}$
2+50		5.5	69.7	
3+00		3.5	71.7	71.89
3+50		1.9	73.3	

VANDEVER ST.

62

THE ± Rods ARE Diff. in Elev. Between Orig. Prelim. & New. Moved Lines 20' North

0+00	-0.1	
0+40	+0.4	
0+50	+0.5	
1+00	-0.4	
1+50	+0.0	
2+00	+1.0	
2+50	+1.5	
3+00	+0.2	
3+50	-0.5	
4+00	-0.2	
4+50	+0.0	
5+00	-0.6	
5+50	+1.0	
5+73 ⁵	+1.3	
5+91	+1.3	Edge A.C.
5+95	+1.3	GUTTER LINE
6+13 ⁸	+1.0	CROWN OF A.C. PAVT
6+28 ⁴⁷	+1.0	EDGE A.C.
6+53 ⁴⁷	+1.9	

$\frac{6+28}{5+91} = .57$

$\frac{4.8}{10' RT$

$\frac{3.4}{10' RT$

$\frac{2.4}{20}$

$\frac{1.4}{8' RT}$ 4 Ditch

Profile Vandever ST.

Handwritten notes on a yellow sticky note at the top right of the page, including numbers like 29.90, 68.80, 75.19, 61.94, 6.3, 6.9, 83.60, 29.98, 00 00, 1.63, and the number 62.

1.09 88.01 86.92

TBM on PK nail see page 58

0.86 75.19 1308 74.93

Why prop line Riverdale St

0+00 6.2 69.

0+00 68.9 $\frac{6.3}{20}$ $\frac{5.9}{16.4}$ $\frac{8.3}{10.21}$ $\frac{5.7}{3.4}$ $\frac{6.3}{10.84}$ ϕ Ditch

+46 $\frac{5.8}{20}$

0+50 5.7 69.5

$\frac{7.6}{80.16}$ ϕ Ditch $\frac{5.2}{20}$

1+00 5.1 70.09 $\frac{69.09}{5.5}$ $\frac{5.5}{16.24}$ $\frac{5.8}{10.16}$ $\frac{7.1}{60.14}$ ϕ Ditch $\frac{5.8}{10.84}$

+50 5.4 69.8

$\frac{5.4}{20}$ $\frac{6.8}{10.21}$

2+00 6.0 69.19 70.19

$\frac{5.0}{20}$ $\frac{5.2}{15.14}$ $\frac{4.2}{9.14}$ $\frac{6.1}{20.14}$ ϕ Ditch $\frac{4.1}{70.84}$ $\frac{4.8}{10.84}$

+50 5.5 69.7

$\frac{71.2}{4.0}$ $\frac{5.7}{10.84}$ ϕ Ditch

3+00 3.5 71.7 71.89

$\frac{3.3}{20}$ $\frac{3.7}{9.14}$ $\frac{2.5}{3.14}$ $\frac{5.4}{5.84}$ ϕ Ditch $\frac{3.4}{10.84}$

+50 1.9 73.3

$\frac{2.4}{20}$ $\frac{1.4}{8.84}$ ϕ Ditch

Profile Vandever St.

1.09 88.01 86.92

0.26 75.19 1308 74.93

0+00 6.2 69.

0+00 68.9 $\frac{6.3}{20}$ $\frac{5.9}{16.4}$ $\frac{8.3}{10.21}$ Ditch $\frac{5.7}{3.4}$ $\frac{6.3}{10.81}$

+40 $\frac{5.8}{20}$

0+50 5.7 69.5

$\frac{7.6}{80.16}$ Ditch $\frac{5.2}{20}$

TBM on PK rail see page 58

Why prop Line Riverdale St

Handwritten calculations and diagrams on a yellow sticky note. The calculations include:

- $5+91$
 - $\frac{5.60}{10+31}$
 - $\frac{6.137}{40}$
 - $\frac{68.16573.7}{61.54}$
 - $\frac{19.98}{8.86}$
 - $\frac{9.047}{4.06}$
- $10+73$
 - $\frac{5.60}{5.13}$
 - $\frac{63.69}{61.54}$
 - $\frac{76.19}{54}$
 - $\frac{10.58}{54}$
 - $\frac{90.47}{1.06}$
 - $\frac{73}{1.9}$
 - $\frac{73}{8.2}$
- 75.19
 - $\frac{75.19}{3.9}$
 - $\frac{63.69}{61.54}$
 - $\frac{76.19}{54}$
 - $\frac{10.58}{54}$
 - $\frac{90.47}{1.06}$
 - $\frac{73}{1.9}$
 - $\frac{73}{8.2}$
 - $\frac{26.6}{9.92}$
 - $\frac{73.62}{29.82}$
 - $\frac{68.89}{61.54}$
 - $\frac{75.19}{3.9}$

Diagrams show vertical profiles with points and slopes. One diagram shows a vertical line with a slope of 2.0 and a horizontal distance of 1.0. Another diagram shows a vertical line with a slope of 1.0 and a horizontal distance of 1.0.

75.19

10.68 83.62 2.25 72.94
4+00 9.7 73.9 73.7

73.7
9.9 / 20 10.1 / 10.22 10.4 / 3.22

9.2 / 3' RL 12.2 / 10' RL 9.7 / 20' RL

Ditch

+50 8.3 75.3 75.3

8.3 / 20 8.3 / 10.22

7.2 / 5' RL 11.2 / 10' RL 10.1 / 17' RL

Ditch

9.4 / 23' RL 8.4 / 20' RL 6.6 / 37' RL

5+00 5.3 98.3 77.72

5.9 / 20 5.6 / 10.22

5.2 / 2' RL 6.6 / 5' RL 6.8 / 7' RL

9.3 / 12' RL 8.4 / 14' RL 8.3 / 27' RL

5+33 3.15 80.4

4' RL Begin 18" Cone + Rock Retaining Wall 4' High

+50 2.0 81.62 82.62

1.0 / 20 1.2 / 10.22

1.7 / 3' RL cone net wall edge 6.8 / 42

7.00 90.47 0.15 83.47

+91 5.11 85.36 86.67

86.7
3.8 / 20

25' RL end Cone Ret Wall 11.8 / 7' RL

Bottom of Wall

+91 5.06 85.41

end of 8" Cone Heddwall to RL

90.47

6+00

4.23 86.24

6+13²

3.39 87.08 88.08

 $\frac{2.39}{20}$

Mission Gorge Rd

6+28²⁷

3.90 86.57 87.57

 $\frac{2.90}{20}$

end of AQ pave Mission Gorge Rd

6+35

4.6 85.87

0⁵ Lt To end of 10" concrete headwall

+35

4.62 85.85

11⁵ Rt " " " " " "

6+36

7.8 82.67

Bott of concrete ret wall

+53²⁷

7.3 83.17 85.07

 $\frac{5.4}{20}$

3.53 86.94 =

86.92

GLACIER AVE Riverdale
to Mission Gorge Rd

6+59¹⁰ Fly prop line Mission Gorge

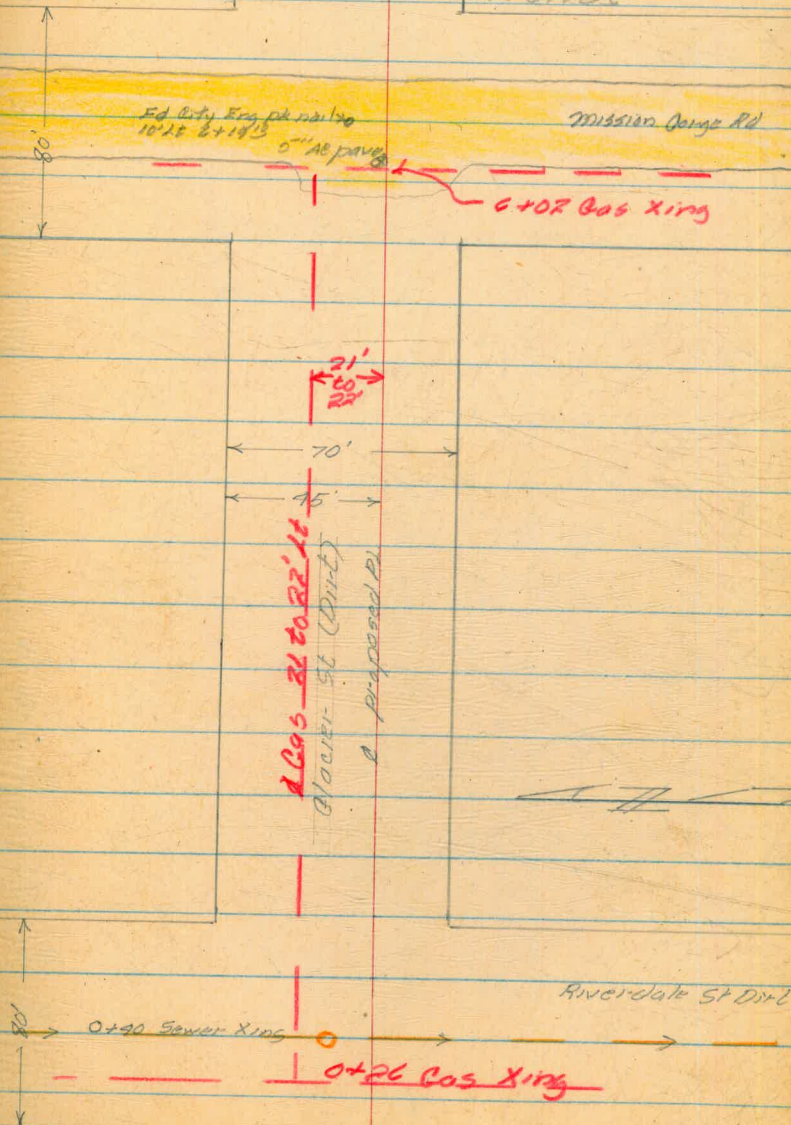
6+39¹⁰ Glacier = 13+89⁹⁴ Mission Gorge Rd

6+19¹⁰ Mission Gorge Rd

West
Williams
Kellhofer

65

7/31/52



0+00 Fly prop line Riverdale

GLACIER AVE RIVERDALE
TO Mission Gorge Rd

Q profile

Revised
by Rocky

see page 58

Mission Gorge

TBM on US 1 + 05 down Mon SF. Cor. Glacier

1.13 101.47 100.04

0.24 88.75 12.96 88.51

1.05 77.49 12.31 76.44

0+00 8.6 68.9

+7.7 To Flow

12" sewer

Wly prop line Riverdale

0+40 7.74 69.75

Top sewer MH 10' 21"

+60 7.2 70.3

1+00 5.1 72.4

+50 3.7 73.8

2+00 2.7 74.8

+50 12.25 88.69 1.05 76.44

3+00 9.7 79.0

+50 6.2 82.5

4+00 1.5 87.2

12.67 100.98 0.38 88.31

+50 9.4 91.6

5+00 6.9 94.1

+50 5.7 95.3

+92 3.20 97.8

Begin AP pave

6+00 2.78 98.2

Rede'd
by Rocky

100.98

6+19¹⁰

1.94

99.0

+39

2.57

98.4

+59¹⁰

1.6

99.4

0.95 100.03 =

100.01 TB11

67
Mission Gorge Rd
6+30 edge of AC.

EN prop line Mission Gorge Rd

1 Profile Glacier Ave
Mission Gorge Rd to Holabird St

For 0+00 to 0+80 see page 66

Redid
by Koccy
8/16/56

11.66	111.70	100.04	
0+80			
1+00		111	100.6
+50		8.4	103.3
2+00		5.9	105.8
+50		2.6	109.1
9.37	120.77	0.30	111.40
3+00		8.2	112.6
+50		6.3	114.5
4+00		7.3	113.5
+50		7.2	113.6
5+00		4.4	116.3
+50		2.0	118.8
6+00		+ 0.1	120.9
1.02	108.94	12.85	107.92
		8.90	100.04 = 100.04

West
Williams
Kellbaker

68

7/31/56

+ Glacier Ave

TBM Cone Mon SE Cor Mission Gorge Rd

Ely prop line Mission Gorge Rd

Glacier St Mission Gorge Rd
to Holabird

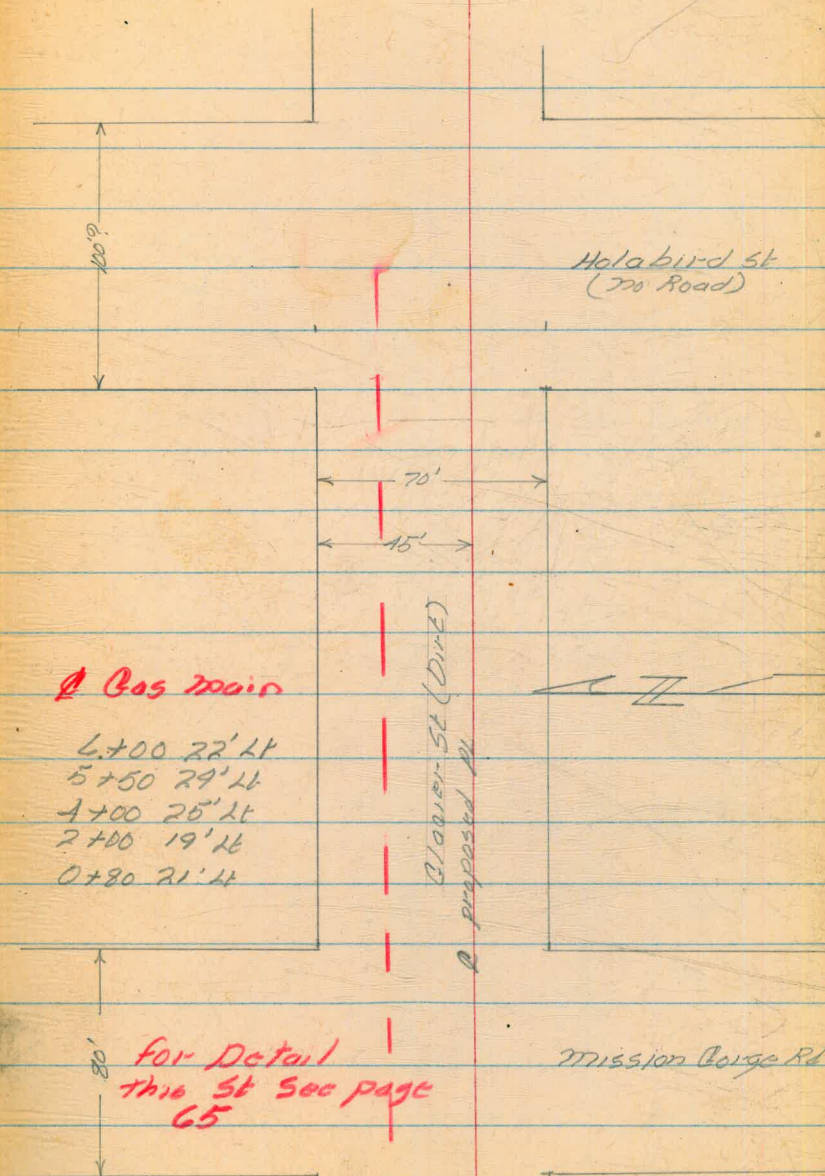
Preliminary

6+00±

end of work (no control)
(on Holabird St)

West
Williams
Kellhofer

69



0+00

Wly prop line Mission Gorge Rd

Lassen

(RAINIER) ST Mission Gorge Rd
to Holabird St

West
Williams
Kullhofer

70

5+10 end of work Why?
(Basty)

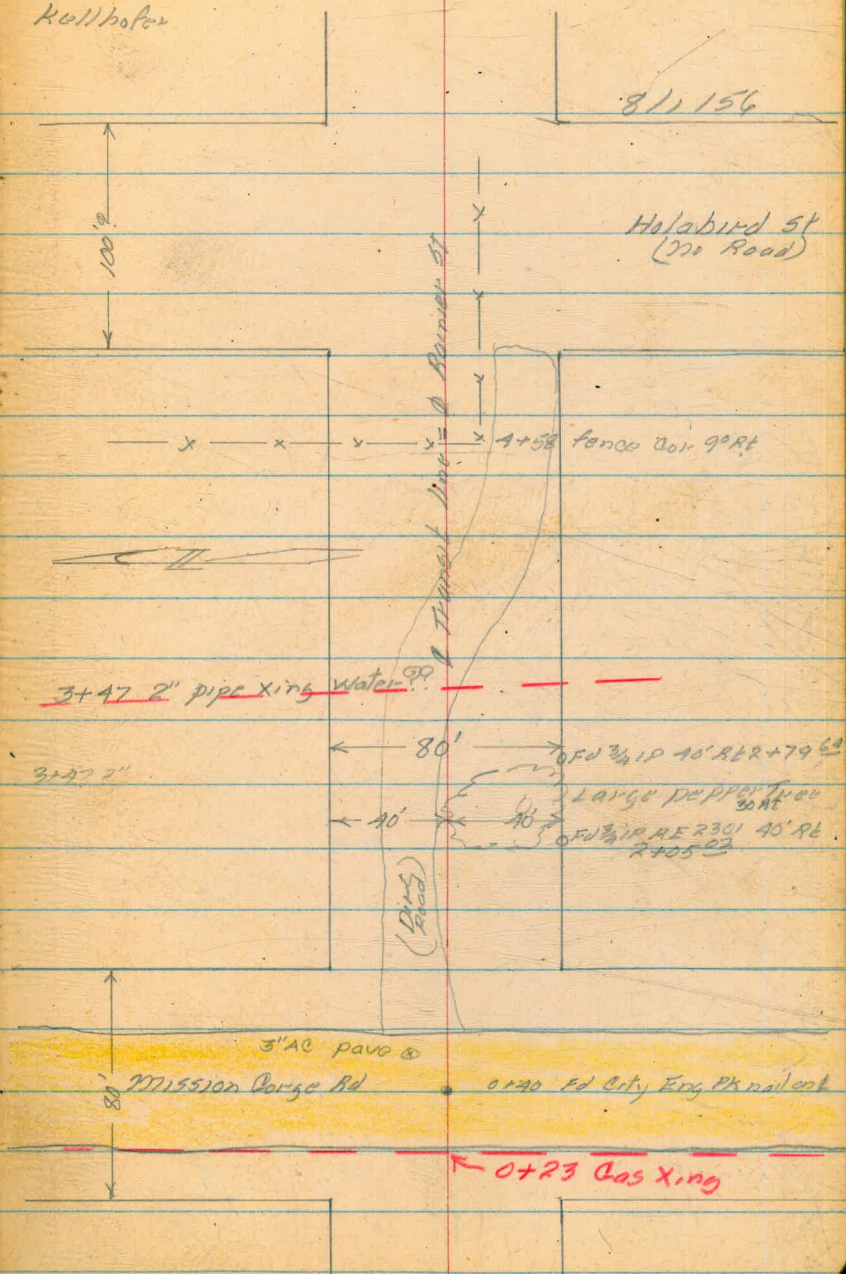
7+79^{CA} POT

2+05^{OR} POT

0+55 Transit Line Rainier St = 17+79^{CA} Gorge Rd
Mission

0+40 PIT PK nail City Eng on Mission Gorge Rd

0+00 Why prop line Mission Gorge Rd



Lessen
(RAINIER) 51

Q Profile

Note This profile 10' ^{on Q proposed R.L.} ~~at~~ of Transit Line

	7.16	109.72		102.56
0+00			2.0	101.72
0+27			2.18	102.54
+40			2.09	102.68
+55 ⁵			2.54	102.18
1+00			3.9	105.82
+50			2.1	107.62
P	12.12	121.10	0.74	108.98
2+00			10.5	110.6
+50			8.4	112.7
3+00			6.1	115.0
+50			3.0	118.1
4+00			2.0	119.1
+50			0.1	121.0
P	6.23	126.96	0.37	120.73
5+00			4.8	122.16
+50			3.8	123.16
6+00			2.1	124.86
TP	0.29	114.68	12.57	114.39
TP	1.46	107.93	8.21	106.47
ck TBM			5.38	102.55 = 102.56

71

TBM

See page 59

mission ^{to} Gorge

Turn on US 0+05 from SW Cor Rainier-L

Wly prop line mission Gorge

Begin AO pave

Q mission Gorge Rd

end AO pave

RELOCATION of F.H.
SE COR. HAMMOND DR
& SAND ROCK ROAD
(13001-L)

BM 3.17 407.77 404.60
3.08 404.69
⑥ 3.52 404.25 403.10
2.42 403.35 = 403.39
CK BM. 3.17 404.60 = 404.60

Nov. 9 1956
Beatty
PAULSON

72

SE PCR HILBURT & Murray Ridge rd.

C/15 C/16

Top existing curb proposed PCR Sandrock Rd
& Hammond St

LOCATION: 8" G.I (EXISTING)
 HWY 395, THRU MONTGOMERY
 FIELD

11/9/56
 BEATTY
 PAULSON

73

169.65 8°06' LT

113.42 2°35' LT

56.23 1°00' LT

0+825

W.M. 145 LT

0+805

5' RT C Sewer M.H.

0+765⁵⁰ B.C.

0+6970 Freeway Bdry Fence

76.50

568°30'E

0+00

F.H TEE

G.V 12 RT
 F.H 4 L RT

89°38' LT
 177' 16"

FD 2x2
 City Engr

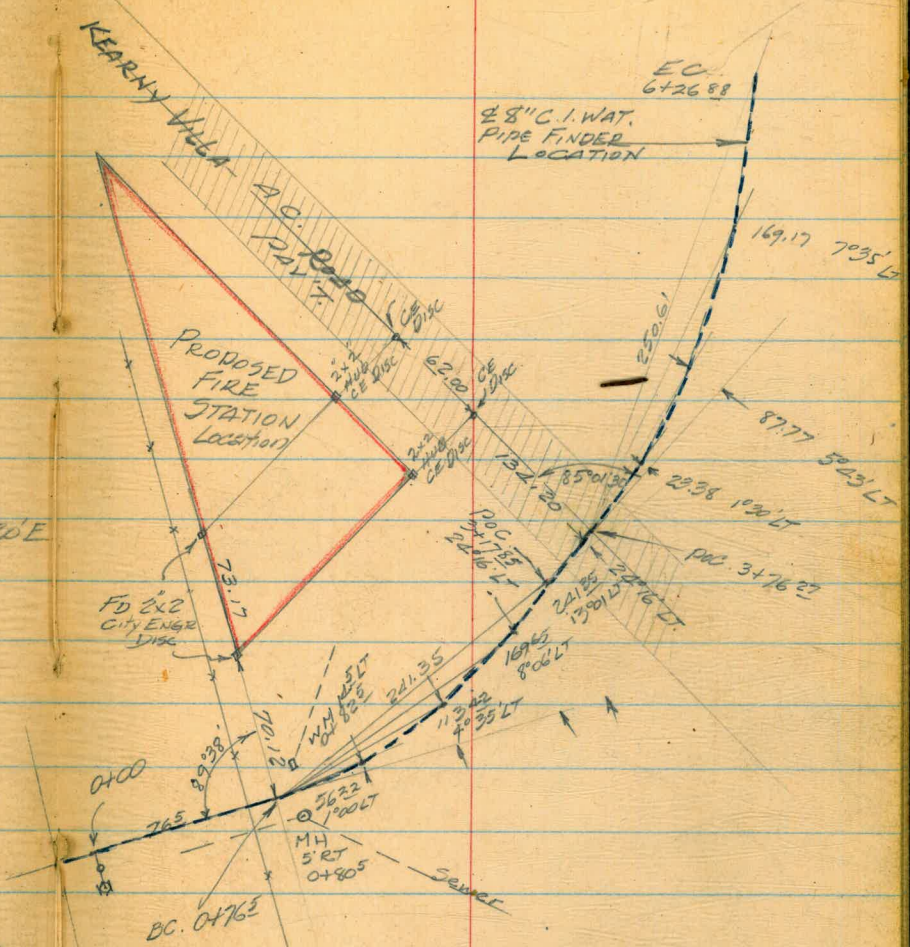
70.12

FD 2x2
 City Engr

73.12

395

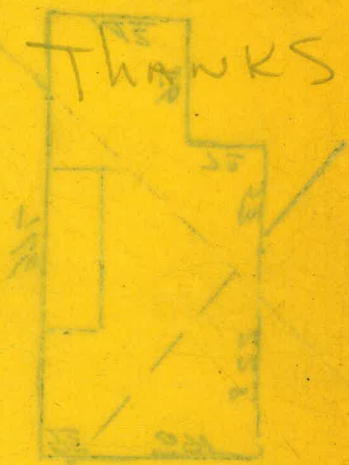
HWY



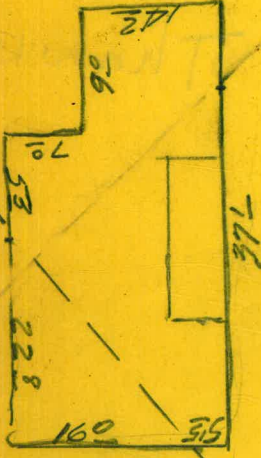
HOWARD:

FILL IN PAULSON'S
TIME FOR NOV. 9, 13, 14,
and 15.

W
A
S
S
E
E
D
C



CROWN AIR
OFFICE



LOCATION 8" C.I. WATER
Hwy 395, THRU MONTGOMERY
FIELD

11/14/56
BEATTY
PAULSON
O'BRIEN

26+84.87 X.P.T. 74.
26+59.28 G.V.

26+84.87 X.P.T. 2598' RT
1527.14 N 65°30' E
26+59.28 G.V.
1527.55 { 43 LT G.V.
83 LT F.H.
19+60.73 822.0
0°00' LT

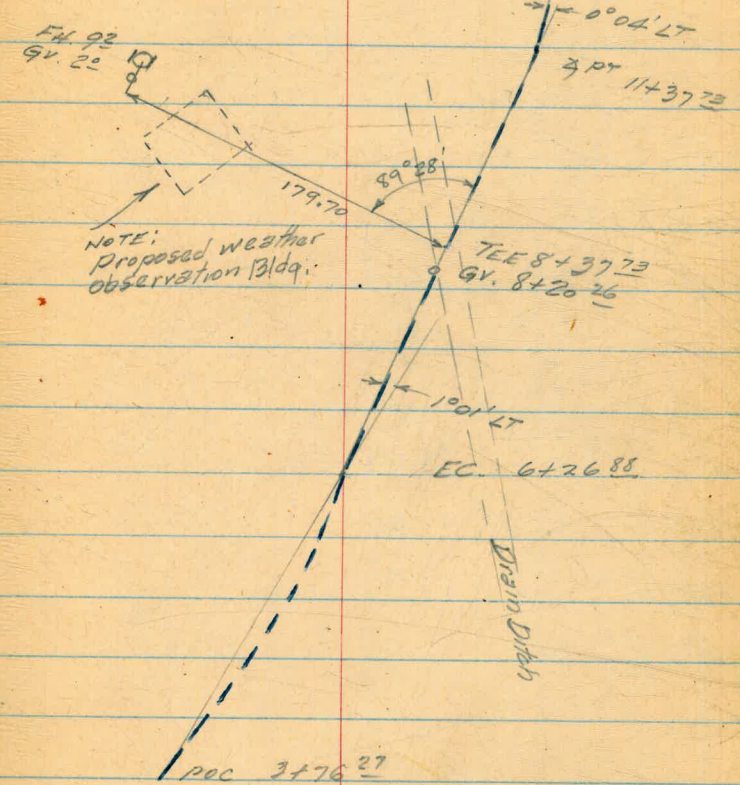
11+37.73 X.P.T. 300' N 65°30' E
P.O.T.

8+37.73 P.O.T. 8x6" TEE. (210.85) 89°28' LT
8+20.26 P.O.T. (193.38) to G.V. 179.70 F.H. TEE
20° RT G.V.
92 RT. F.H.

6+26.88 X.E.C. 1°01' LT
250.61 8°20' LT N 77° E
169.17 7°35' LT
87.77 5°43' LT
23.38 1°30' LT
196.20 { P.K. &
132.20 { City Eng
Disc

3+76.27 P.O.C. & Kearny Villa Rd
5822 24°16' LT
24°32'

3+17.85 P.O.C. 581°30' E
241.35 13°01' LT
26°02'



NOTE:
Proposed weather
observation Bldg.

Drain Ditch

LOCATION: 8" C.I. WAT.
 Hwy 395, Thru Montgomery
 FIELD

11/14/56

75

42+52²² x PT 24°58' RT
500.02

588°E

38+71²⁰ Wat Ser. W.H. 49³ RT

125.0

0°11' RT

37+46²⁰ x PT F.H. TEE

445.82

{ 33 RT GV.
 62 RT FH

37+31¹⁰ POT (90°03' RT, & RD, 180°47' to & AREG. Rd -

91°04'
 76.4
 to PK

35+25⁷

Wat. Ser. 2" WM LT. 72'-76'

35+20

Beacon Pole 3' LT

33+00²⁶

Begin AC parking area

32+92⁶⁶

F.H. TEE 3° RT to GV.
 6° RT to FH

173.60

31+21⁰⁶ x PT 90°23' LT

36.95 BL to Bldg

30+91⁰⁶ x PT 90° RT

29+91⁰⁶ x PT 90° RT

29+61⁰⁶ x PT 90° LT

182.17

AH.
 35²² to Bldg

27+78⁸⁸

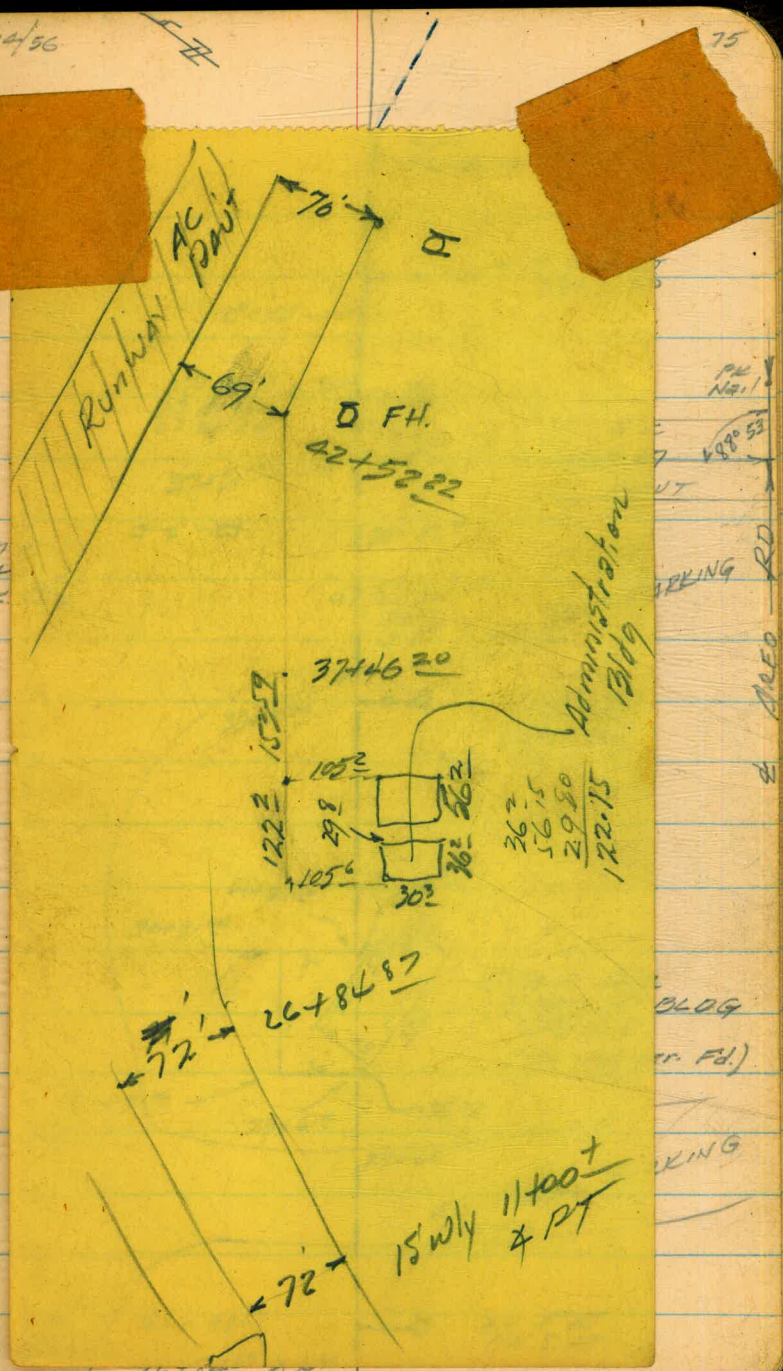
Begin A.C. parking apron

80.22

26+98⁶⁷

13.80

{ F.H. TEE
 5' RT GV.
 8' RT FH



PK No. 1
 488°53'
 UT
 PARKING
 & AREG. RD
 BLDG
 PARKING

LOCATION 8" C.I. WAT.
 Hwy 395, Thru Montgomery
 FIELD

42+ 52²² x PT 24° 58' RT
500.02

588° E

38+ 71²⁰ Wat Ser. W.M. 49³ RT
122.00

0° 11' RT

37+ 46²⁰ x PT F.H. TEE
445.84 { 33 RT. GV.
 67 RT. FH

37+ 31¹⁰ POT (90° 03' RT, & RD, 1807.47 to & AREF. Rd -
476.42 91° 07' LT
 to PK Nail

35+ 25.7 Wat Ser 2-W.M. LT. 74-76
 35+ 20 Beacon Pole 3' LT LT. 58'

33+ 00³⁶ Begin AC parking apron
5.79

32+ 91⁶⁶ F.H. TEE 30' RT to GV.
173.60 6' RT to FH

31+ 21⁰⁶ x PT 90° 23' LT 36.95 BX to
 Bldg

30+ 91⁰⁶ x PT 90° RT.

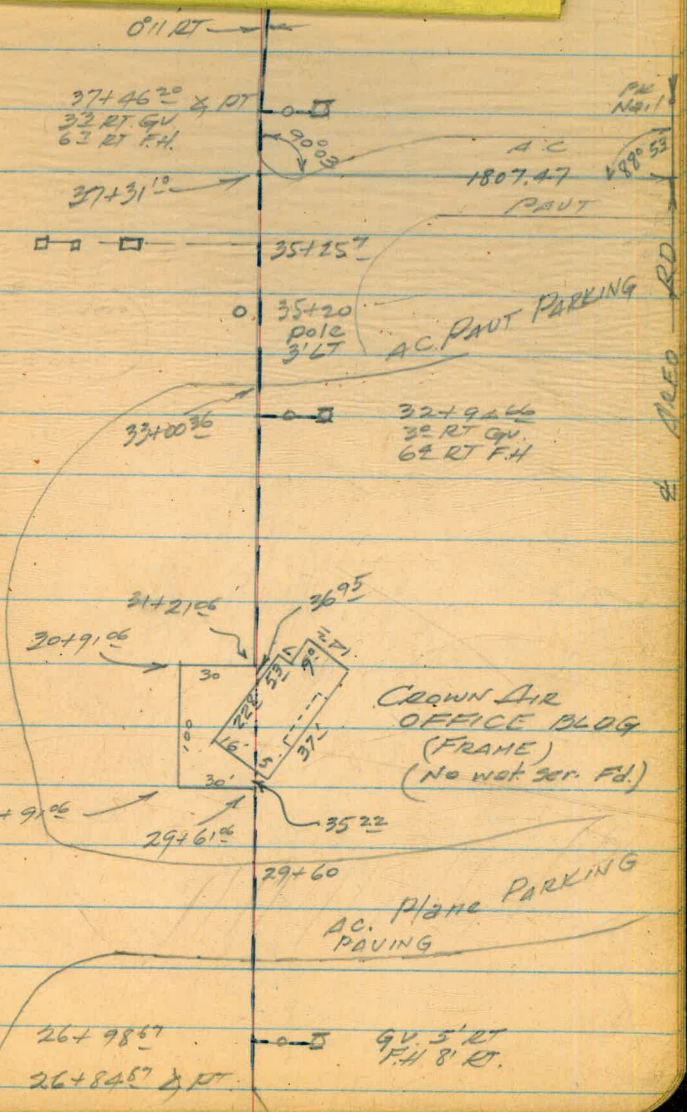
29+ 91⁰⁶ x PT 90° RT.

29+ 61⁰⁶ x PT 90° LT 35.22 To Bldg
182.17 AH.

27+ 78⁸⁹ Begin AC parking apron

80.22

26+ 98⁶⁷ 13.80 { F.H. TEE
 5' RT. GV.
 8' RT. FH



LOCATION 8" C.I. (EXISTING)
 HWY 395 THRU MONTGOMERY
 FIELD

11/15/56
 Beatty
 Paulson
 O'Brien

76.

61+50+ at Conc Mon. (City Engrs)
 350'±

49°20' RT.

58+49⁹⁹ at Conc Mon (City Engrs)
 1126.20

548°E

Δ = 15°30' RT

END 8" C.I.

48+07⁷⁹ X PT FH TEE
 555.57

GV. 37 RT
 FH 67 RT

563°E

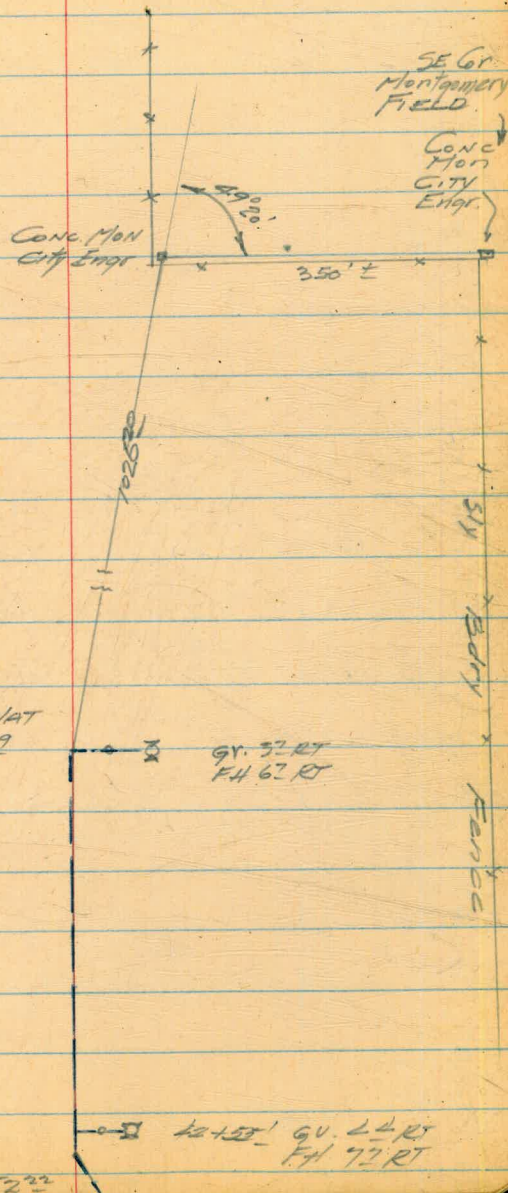
42+55⁻ FH TEE
 2.90

GV. 44 RT.
 FH 72 RT.

X PT
 42+52²³

12+52⁻ GV. 24 RT
 FH 72 RT

Montgomery
 AIR
 Field



REVISED ALIGNMENT PROFILE
46TH ST OLIVE TO MAPLE ST.
SEE PAGE 23

B.M.	5.79	^{46.9} 296.86	291.07 ✓ L.H. 4-3057
0+00		0.2	96.7
+50		2.5	94.4
1+00		4.3	92.6
+50		6.2	90.7
2+00		7.5	89.4
+50		9.2	87.7
3+00		^{83.9} 11.3	85.6 ✓
T.P.	0.04	283.86	13.04 283.82 ✓
+54.5	BEGIN A.C. 1 1/2"		0.42 83.5
4+00		4.95	79.0
T.P.		^{72.4} ✓	
+50	0.58	271.19	13.25 270.61 ✓
5+00		10.46	61.7
T.P.		^{59.1} ✓	
5+15	0.48	259.05	12.62 258.57 ✓
+50	SEWER XING 2"		0.6 58.5
		6.5	52.6
+65		8.94	50.2
T.P.		^{46.4} ✓	
	0.33	246.89	12.49 246.56 ✓
6+00		2.4	44.5
EDGE A.C.			
+50		9.1	37.8
T.P.	0.14	234.05	12.98 233.91 ✓

WEST,
WILLIAMS
KELLHOFER X
BULL †

77

4/29/57 CLOUDY

OLIVE + 46TH 17' MON.
NLY PROP LINE OLIVE ST

12' RT TO W. EDGE DIRT RD.

9' RT TO W. EDGE DIRT RD.

EDGE A.C.	0.0	0.9
	9.7 LT	7' RT EDGE A.C.
	4.7	5.3
EDGE A.C.	11.2 LT	6' RT EDGE A.C.
	12.7	13.7
EDGE A.C.	12' LT	4' RT EDGE A.C.
	10.5	10.3
EDGE A.C.	15.2 LT	1' RT EDGE A.C.

EDGE	7.0	7.3
A.C.	13.8 LT	2.0 LT

9' LT WEST RIM SEWER M.H. - 5.6 TO FLOW

EDGE	2.3	2.8
A.C.	13' LT	1' LT
EDGE	9.3	
A.C.	13' LT	

46TH ST CONT.

SAME PARTY

34.1 ✓
234.05 HI

B.M	EDGE A.C.		3.5	306
	7+00			
0+00	EDGE A.C.		7.5	266
	+26 I			
+50				
	T.P	3.07	224.87	12.25 221.80 ✓
1+00	CHECK		8.00	216.87 ✓
	B.M.			
+50				
2+00				
+50				
3+00				
	T.P.			
	+54.5			
4+00				
	T.P.			
	+50			
5+00				
	T.P.			
	5+15			
	+50			
+65				
	T.P.			
6+00				
	EDGE A.C.			
	+50			
	T.P.			

3.7
13.3 LT. EDGE A.C.

8.0
13.3 LT. EDGE A.C. SLY PROP. LINE MAPLE

216.72 S.W. (27) + (13) Mon. MAPLE + 46TH
SEE PAGE 25.

Please Return to
 City of San Diego Water Dept.
 Room 903 Civic Center

80.49
 + 6.11

 86.60
 - 0.94

 85.66
 + 84

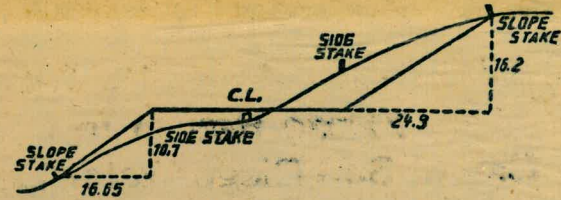
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 75.64

 79.54

11009886
 144.5

5049430
 4039544
 4039544
 1009886
 1009886

 115.58145270



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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