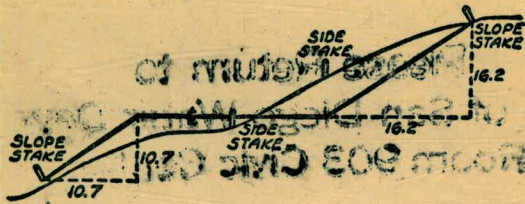


W 917



Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
 SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

000.29  
 73  
 35.6  
 37.9

000.29  
 35

80  
 50  
 28  
 14

L

300

30700 + 0433

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1 $\frac{1}{2}$  to 1  
If ground is nearly level, the cut or fill at side

IMPROVED TABLES  
AND  
INFORMATION

TABLE No. XVII

To find tangent and external for curve of  
any other degree divide by degree of curve and  
add correction found in column of corrections  
Degree of curve in a chain may be found  
by dividing tangent (or external) by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is only nearly the square of the tangent  
length divided by twice the radius.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.036	.041	.046	.051	.056	.061
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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alice

PROPOSED WATER MAIN  
KEARNY MESA  
NWLY HIGHWAY 395  
KEARNY MESA STANDPIPE SWLY.

4+45<sup>75</sup> A 45° LT.

3+73<sup>63</sup> A 45° RT. - INTERSECTION RANCHO MISSION

0+00

KEARNY MESA  
STANDPIPE →

7/7/55  
SHOREY  
ALEXANDER  
KELLHO  
HOLLAND

0+00 G.V. 21<sup>3</sup> LT.  
FENCE 24' LT  
EDGE PAVT SHOULDER 48' LT.  
" " 83' LT.  
" " 124' LT  
" " SHOULDER 157' LT  
FENCE 183' LT

0-19 FENCE

0+00 OIL ROAD 6' RIGHT  
21' LEFT

3+73<sup>63</sup> Δ OIL ROAD 3' RIGHT  
30' LEFT

FENCE 37<sup>3</sup> LEFT

SHOULDER  
EDGE PAVT. Δ 48' LEFT

" " 83' "

" " 124' "

" SHOULDER  
" Δ 157' "

2+76<sup>85</sup> OIL ROAD 49' ~~LT~~ 82'  
FENCE 83' ~~LT~~ LT  
EDGE PAVT SHOULDER 96' LT.  
" " 133'

115  
M.G.

0-19  
2' stand BW fence \*

PROPOSED WATER MAIN  
 KEARNY MESA  
 NWLY HIGHWAY 395  
 KEARNY MESA STANDPIPE SWLY

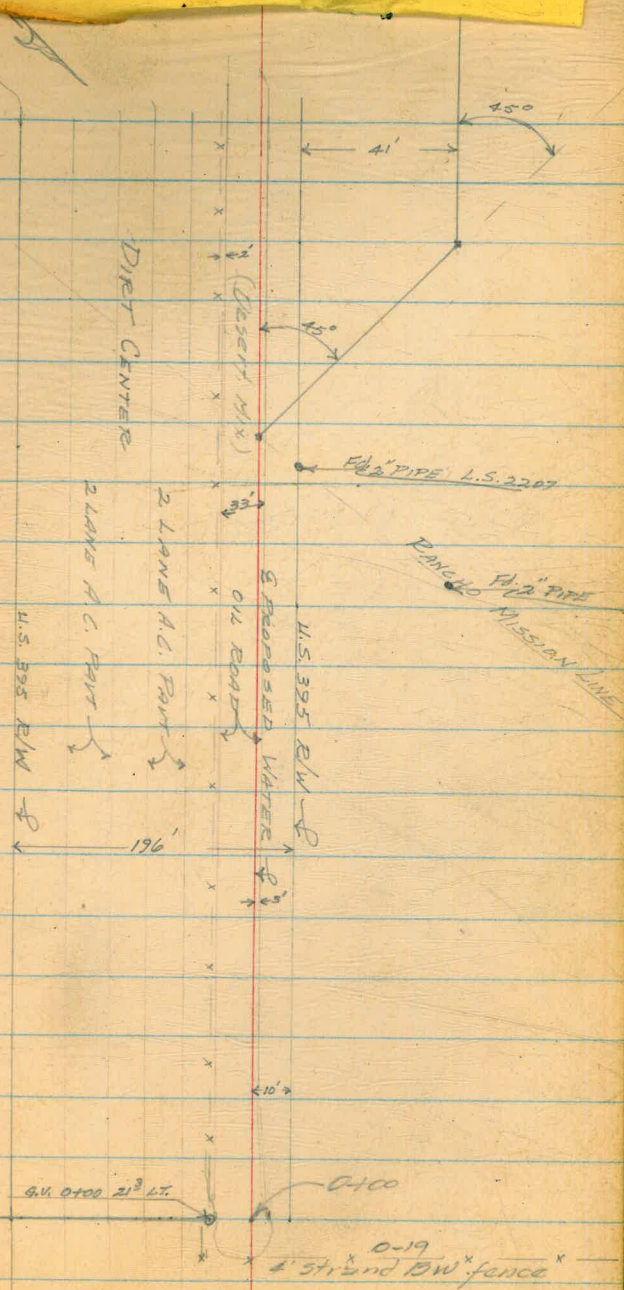
4+45<sup>75</sup> A 45° LT.

3+73<sup>63</sup> A 45° RT. - INTERSECTION RANCHO MISSION

0+00

KEARNY MESA  
 STANDPIPE →

7/7/55  
 SHOREY  
 ALEXANDER  
 KELLHOFFER  
 HOLLAND



1.5  
 M.G.

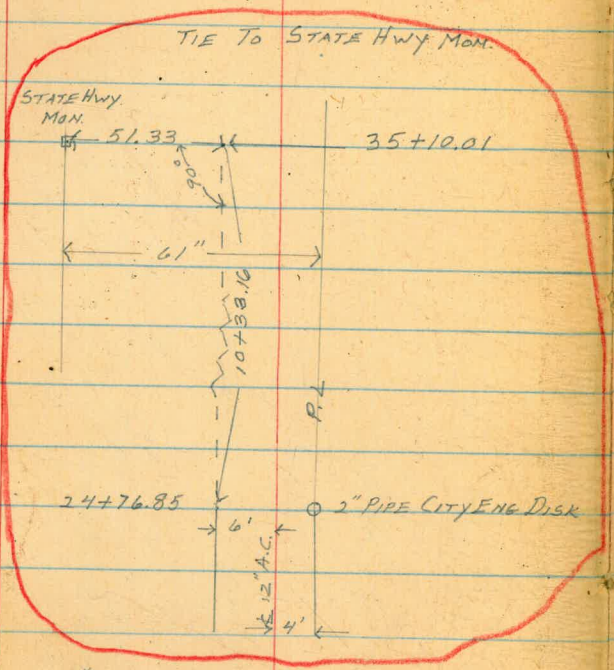
0+100  
 0+19  
 4" strand BW fence

# KEARNEY MESA (Cont'd)

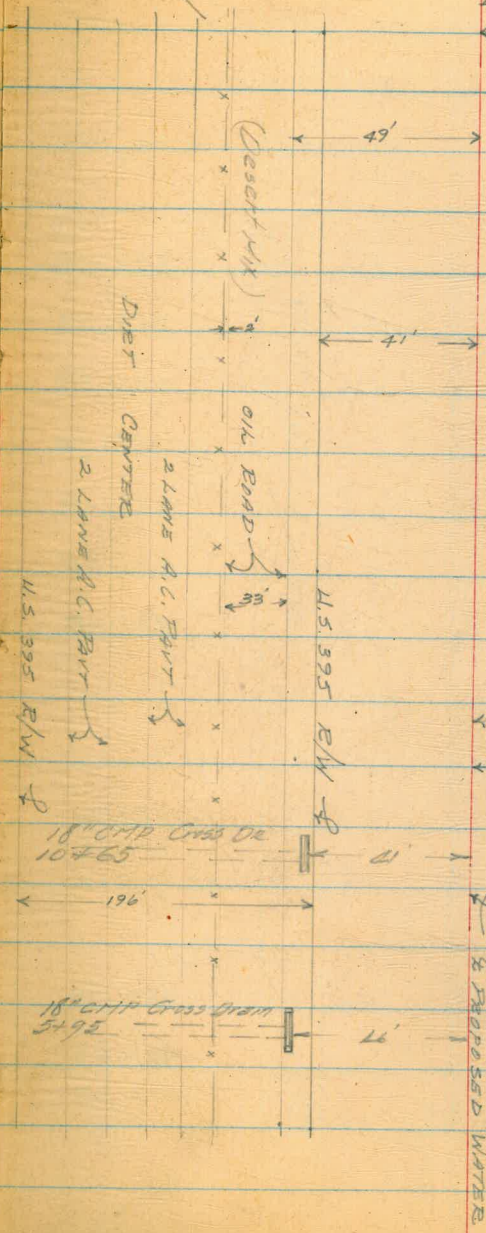
2-7-55

(2)

24+76.85 END OF LINE. 2" PIPE CITY ENG. 20' RT.



15+76.85 P.O.T. 2" PIPE CITY ENG. 20' RT.



20.7 ACRES  
CITY LAND





PROPOSED KEARNY MESA W.L.  
& PROFILE & X-SECTIONS

7/7/55  
SHOREY  
ALEXANDER  
KELLHOFFER  
HOBHMAN

(3)

B.M. 7.19 436.22 429.029

CHISL.D ON CULV. HEADWALL AT KEARNY MESA TANK  
F.B. 874.

TP 1.25 434.49 3.68 432.54

TBM 2.84 431.65

TOP OF G.V. APPROX. 22' LT. 0400 (6.6 down to  
top stem mt)

0.83 432.48

0+00 1.4 431.08

Left  
(35%) 425.05 431.0 431.0 Right  
(Top of G.V. 7.43) 1.5 1.5  
stem mt. 213 22 10  
27 G.V.

0+50 3.4 429.08

1+00 4.5 427.98

1+50 5.4 427.08

2+00 6.3 426.18

2+50 7.1 425.38

3+00 7.8 424.68

7.21 425.27

3.11 428.38

3+50 4.0 424.38

424.28

3+73.63 APL 4.1 45° ahead

4+00 7.4 420.98

4+25 6.1 422.28

4+45.75 APL 8.4 45° ahead

419.98

KEARNY MESA  
(Contd.)

7/7/55

④

422.38

LEFT

RIGHT

4+50	8.2	420.18
4+71	8.1	420.28
4+89	6.5	421.88
5+00	7.1	421.28
5+14	8.7	419.68
5+45	8.0	420.38
5+50	8.4	419.98
5+95	7.7	420.68
6+00	7.5	420.88
6+50	6.0	422.38
① 377 426.98	5.17	423.21
6+76	2.8	424.18
7+00	1.4	422.58
7+35	4.2	422.78
7+50	2.6	424.38
7+78	4.3	422.68
8+00	1.4	422.58
8+50	5.9	421.08

Edge of road  
5.1  
7.9  
7.6  
7.0  
7.1  
6.7  
7.0

419.2

Edge of road  
5.7  
4.9  
9.2  
1.26  
6.7  
2.3  
Flow line  
of concrete  
18" C.M.P.

Edge of road  
2.8  
2.9  
2.2  
1.10  
4.3  
1.0

Edge of road  
2.6  
2.9  
5.2  
1.10  
4.2  
1.0

KEARNY MESA  
(Cont'd.)

7-7-55

5

				Left		Right
	426.98					
9+00		6.5	420.48	Edge 6.0 Rd. 49	6.1 10	7.0 10
9+23		6.2	420.78			
9+50		8.3	418.68			
9+66		8.9	418.08			
10+00		7.8	419.18	Edge 7.0 Rd. 49	8.2 10	8.5 10
10+44		8.8	418.18			
10+50		8.0	418.98			
D	315	422.56	7.57 419.41	Nuc. end culvert ditto		
10+65		4.3	418.26	416.4 6.7 41 Flow line at Conc. ditto 18" C.P.		4.1 10
11+00		6.6	415.96	Edge 8.8 Rd. 49	5.8 10	6.0 10
11+10		5.0	417.56			
11+26		7.0	415.56			
11+50		7.5	415.06			
11+68		8.0	414.56			
11+84		5.6	416.96			
12+00		6.1	416.46	Edge 7.8 Rd. 49	5.7 10	6.7 10
12+25		7.2	415.36			
12+50		5.6	416.96			

KEARNY MESA  
(Cont'd.)

222.56

12+75	6.8	415.76
13+00	5.8	416.76
13+10	5.1	417.46
13+38	5.9	416.66
13+50	5.5	417.01
14+00	5.0	417.56
14+32	5.2	417.36
14+50	3.8	418.76
15+00	4.4	418.16
15+50	3.9	418.66
15+76.82 POT.	3.4	419.16
41) 7.15 425.69	4.02	418.50
16+00	6.4	419.29
16+50	6.6	419.09
17+00	5.8	419.89
17+50	5.7	419.99
17+91	4.3	421.39
18+00	4.8	420.89
18+50	5.1	420.59

7-8-55

①

Left

Right

Edge 3.3 5.4 6.2  
Rd. 4.9 10 10

Edge 3.4 4.9 5.2  
Rd. 5.0 10 10

Edge 3.5 4.8 5.2  
Rd. 4.9 10 10

28.10 76.82 15+76.82

Edge 5.8 6.2 6.6  
Rd. 4.9 10 10

Edge 5.0 5.8 5.6  
Rd. 4.9 10 10

Edge 4.9 4.3 5.4  
Rd. 4.9 10 10

KEARNY MESA  
(Cont'd)

	425.69		
18+82		6.4	419.29
19+00		6.0	419.69
19+24		5.5	420.19
19+50		6.0	419.69
19+79		5.8	419.89
20+00		6.4	419.29
20+50		6.7	418.99
TP	2.11	421.88	5.92 419.77
21+00		3.1	418.78
21+50		3.3	418.58
21+61		3.0	418.88
22+00		4.3	417.58
22+50		5.5	416.38
23+00		6.4	415.48
23+25		6.0	415.88
23+50		6.9	414.98
23+69		7.6	414.28
23+87		7.2	414.68
24+00		7.7	414.18

7-8-55

Left

Right

Edge 52  
Red 29

5.9  
10

6.4  
10

Edge 5.5  
Red 29

6.6  
10

6.3  
10

Edge 2.5  
Red 29

2.8  
10

3.2  
10

Edge 3.7  
Red 29

4.2  
10

4.5  
10

Edge 5.1  
Red 29

6.9  
10

6.6  
10

Edge 6.3  
Red 29

7.6  
10

7.9  
10

KEARNY MEJA  
(Cont'd.)

	221.88			
24+16		8.0	413.88	
24+50		8.5	413.38	
24+76.85	End of 100	10.0	411.88	
TBM	8.78	420.30	10.36	411.52
IP	6.35	421.81	4.84	415.46 ✓
OK BM.		3.09	418.72	= 418.71

CHECK ELEVATION

TBM	5.61	424.15		418.54
			5.74	418.41 = 424.565

7-8-55

(5)

Left

413.3

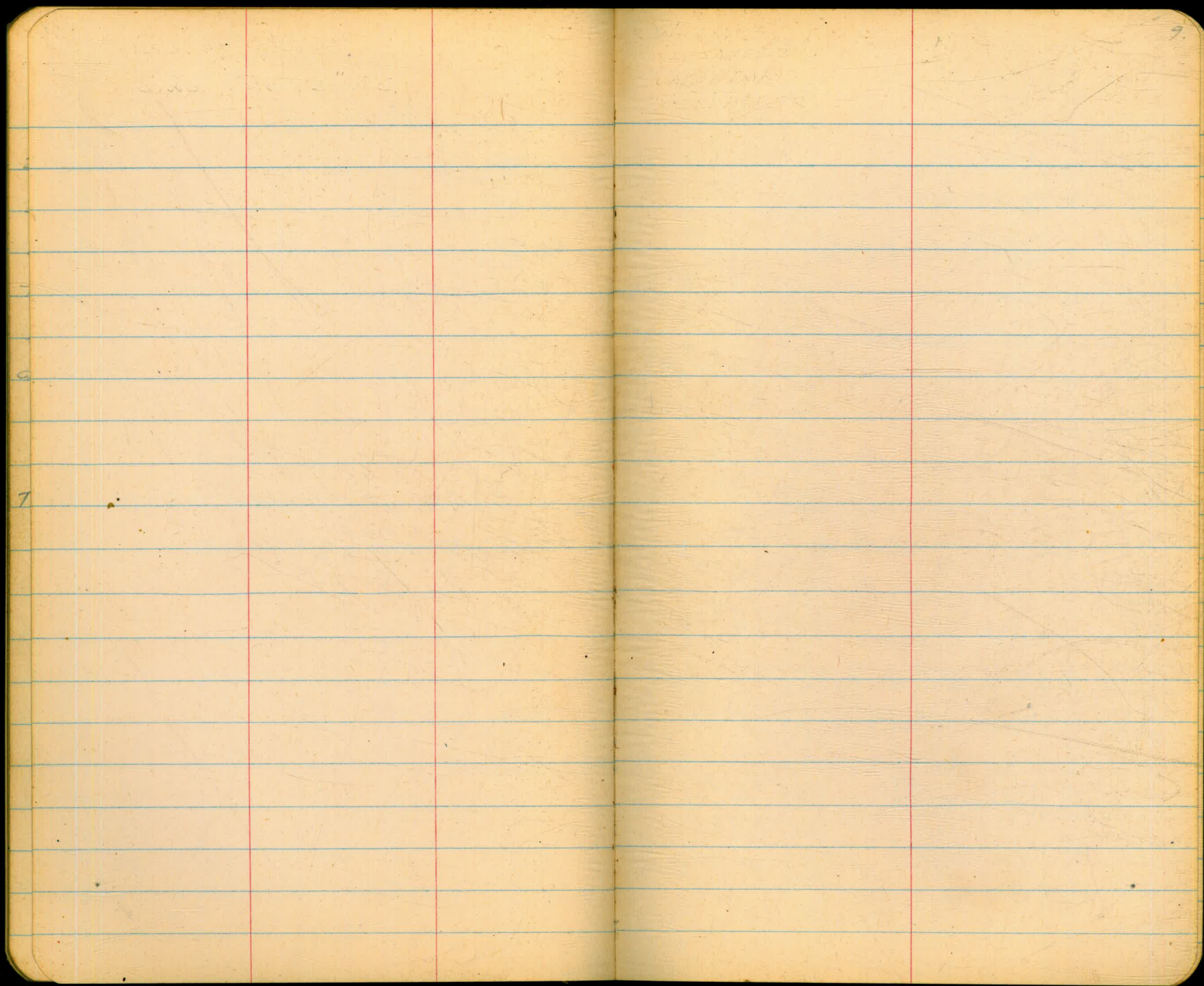
Right

Flow line 8.6  
3" Lane 49  
18" CHD  
Edge Rd 7/1 9.8 9.9  
48 10 10  
2" IP 20' RT 24+76.85

B.M. Telephone pole 537135 H. 200' S.W. on Elliott Rd

2" I. PIPE 20' RT. 15+76<sup>82</sup> (Pg. 6)

1/2" I. PIN 30" I.T. APPROX 14+00  
STATE HWY. B.M.



KEARNEY MESA INDUSTRIAL AREA  
 (C) STKS FOR 12" A.C. PIPELINE

WILLIAMS  
 ALEXANDER X  
 VARONFAKIS  
 KELLHOFER †

8/11/55

T.B.M.	0.25	431.90	431.65	
0+22	0.0	431.9	421.8	
0+00 F	0.6	431.3	423.5	
0+00 N	1.1	430.8	423.5	
+50 (2" A.V.A.)	3.0	428.9	424.7	
1+00	3.3	428.6	423.8	
+50	4.6	427.3	422.9	
2+00	5.7	426.2	421.9	
+50	6.5	425.4	421.0	
3+00	8.1	423.8	420.5	
+50	8.6	423.3	420.0	
SPLIT X				
3+73.63 (45° Bend)	7.9	424.0	418.5	
T.P.	4.23	426.65	9.48	422.42
4+00	4.9	421.8	416.8	
+25	5.5	421.2	416.3	
4+50	6.2	420.5	415.8	
4+68 <sup>38</sup> BK } (45° Bend) @ RT. 4+61 <sup>25</sup> AH } @ LT.	6.2	420.5	415.7	
5+125 (4" B.O.)	6.3	420.4	415.5	
5+50	4.9	421.8	415.8	
6+00	4.4	422.3	416.7	

C10	1	TOP G.V. 22' LT. 0+00 (SEE PAGE 3)
C7	2	Replaced by 16" x 4" B.O. 9/14/55 DEATY
C7	3	0-023 12" G.V. 0+023 12" G.V.
C4	2	INSTALLED 0+51
C4	8	
C4	4	
C4	3	
C4	4	
C4	3	
C3	3	
C3	3	
C5	5	

2" IRON PIPE 20' FROM SPLIT X (NELY)

C5	0	8/15/55
C	427	
C4	7	✓ OK
C4	8	
C4	9	
C6	0	✓ 0.2 low
C5	6	✓



KEARNY MESA 12" A.C.  
(Cont'd)

426.65

6+50		4.2	42 2.5	418.2	
7+00		3.9	42 2.8	418.1	
T.P.					
7+50	2.65	425.69	3.61	423.04	418.0
8+00		2.5	42 3.2	417.9	
8+25		4.0	42 1.7	417.4	
8+50		3.9	42 1.8	417.0	
9+00		5.7	42 0.0	416.1	
9+50		6.1	41 9.6	414.5	
10+00		7.5	41 8.2	414.3	
10+50		8.2	41 7.5	<del>414.0</del> 412.7	
OK P.	3.31	422.71	6.29	419.40 = 419.41	
11+00		6.1	41 6.6	411.8	
11+50		7.4	41 5.3	410.9	
11+625	4" B.O.	7.9	41 4.8	410.6	
12+00	12" G.V.	7.3	41 5.4	410.9	
12+50		6.7	41 6.0	410.4	
13+00		6.6	41 6.1	412.0	
13+50		6.0	41 6.7	412.4	
14+00		5.7	41 7.0	413.0	

8/15/55 WEST  
WILLIAMS  
VARONFAKIS &  
ALEXANDER X

C4  $\frac{3}{7}$   
C4  $\frac{0}{3}$   
C5  $\frac{3}{3}$   
C4  $\frac{3}{8}$   
C4  $\frac{9}{9}$   
C3  $\frac{1}{1}$   
C5  $\frac{9}{9}$   
C3  $\frac{5}{8}$   
C3  $\frac{5}{8}$  C4  $\frac{8}{8}$

Nly end Colv Hdwall pg 5

C4  $\frac{8}{5}$   
C4  $\frac{2}{5}$   
C4  $\frac{5}{6}$   
C4  $\frac{1}{3}$   
C4  $\frac{3}{0}$   
C4  $\frac{0}{0}$

✓ OK

✓ OK

KEARNY MESA 12" A.C.

(Cont'd.)

422.71

8/15/55.

12.

14450 4.9 417.8 413.5

C4  $\frac{3}{}$

15400 5.6 417.1 414.0

C3  $\frac{1}{}$

+50 3.9 418.8 414.4

C4  $\frac{4}{}$

CHECK  
T.B.M. 6.66 425.20 4.17 418.54 = 418.54

2" I.P. 20' RT STA 15+76.82 PAGE 6

16400 6.5 418.7 414.7

C4  $\frac{0}{}$

+50 6.3 418.9 415.0

C3  $\frac{9}{}$

17400 5.4 419.8 415.4

C4  $\frac{4}{}$

+50 5.6 419.6 415.9

C3  $\frac{7}{}$

18400 5.3 419.9 416.1

C3  $\frac{8}{}$

+50 5.2 420.0 416.4

C3  $\frac{6}{}$

A.V.A.

+87.5 6.1 419.1 415.2

C3  $\frac{9}{}$

19400 5.9 419.3 415.1

C4  $\frac{2}{}$

+50 5.7 419.5 415.1

C4  $\frac{4}{}$

20400 5.8 419.4 415.0

C4  $\frac{4}{}$

+50 6.2 419.0 414.8

C4  $\frac{2}{}$

21400 6.6 418.6 414.6

C4  $\frac{0}{}$

+50 7.0 418.2 414.4

C3  $\frac{8}{}$

22400 7.9 417.3 413.3

C4  $\frac{0}{}$

+50 9.2 416.0 412.3

C3  $\frac{7}{}$

KEARNY MESA 12" A.C.

CONT.

425.20

23+00		9.9	415.3	411.3
+50		9.4	415.8	410.5
24+00		11.2	414.0	410.0
T.P.				
+50	5.46	418.19	12.47	412.73 408.8
+84		5.8	412.4	407.0
+86		6.4	411.8	407.0
+93 FH (6)		6.3	411.9	407.0
CHECK				415.9
T.B.M.	6.66	411.53	= 411.52	

BM	2.71	421.48	418.77	pp. 8
P <sub>rock</sub>	4.06	420.46	5.08	416.40
P		8.45	412.01	
P		5.52	412.94	
P	6.60	418.61	412.01	
		4.89	413.72	= 414.25
		4.82	413.79	414.22
		5.38	413.27	414.22
CLP	8.81	420.82	6.60	412.01
P	5.11	422.06	3.87	416.95
CL BM			3.30	418.76 = 418.77

8/15/55

C4	$\frac{0}{3}$	
C5	$\frac{3}{0}$	23+41 12" x 8" TEE
C4	$\frac{0}{9}$	Beatty 9/2/55
C3	$\frac{9}{4}$	
C5	$\frac{4}{8}$	12x6 TEE
C4	$\frac{8}{9}$	90° BEND
C4	$\frac{9}{9}$	F.H. F3.5

PAGE 8  
2" I.P. 20' RT STA. 24+76.85

12/5/55 Beatty  
Kellhofer

spike pole 537135H  
24+84  
1 43 = 136  
23+41 145

on 2" I.P. prop Cor.  
Top F.H.

Contractors elev. for Elev. of AC entrance road wly  
(says about 0.56 off city datum) of Vault  
Top prop vault. @ prop line. Ely. F0 43  
" " " " " " Wly. F0 99 F10

2" prop Cor

KEARNY MESA  
(Cont'd.)

Reference of City Engr.'s  
Corners

Beatty  
Williams  
Alexander  
Varenfasco

8/15/55

14

2" I.P.  
CITY ENGR DISC

2" I.P.  
CITY ENGR  
DISC

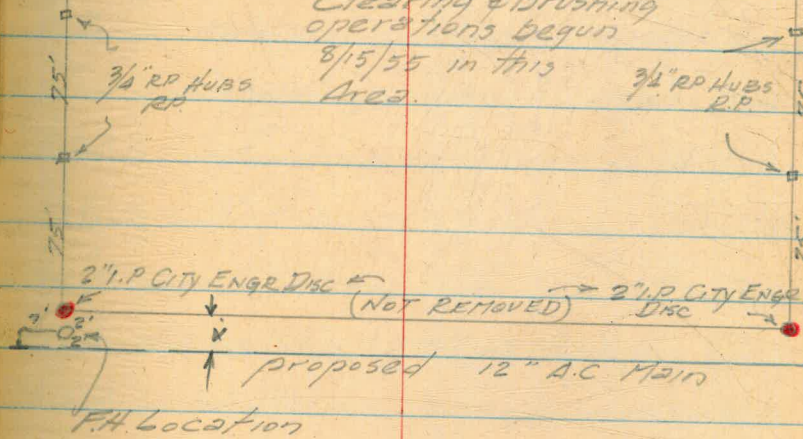
MAGNATRON  
INC.

LOT 78

NOTE:

Clearing & Brushing  
operations begun

8/15/55 in this  
Area.



Alley Blk 192 N of W. Highman  
E of Wabash  
325 for 6" AC Main

West T  
Williams  
Varonofakis  
Kellhofer P

10-19-53

Sub 901 Page 25

TBM rim sewer MH 5' L x 0' 40

Begin Work

	12.07	337.80	325.73	
0+30			12.6 325.2 321.0	C5 $\frac{2}{1}$
+50			11.6 326.2 321.0	C6 $\frac{1}{1}$
+75			10.7 327.1 321.0	C2 $\frac{3}{1}$
+87 ME			9.9 327.9 325.6	C2 $\frac{2}{1}$
+98 ME			8.9 328.9 326.2	C6 $\frac{4}{1}$
1+00			8.8 329.0 322.6	C0 $\frac{9}{1}$
+38 MW <small>metr in alley</small>			8.4 329.4 328.5	C5 $\frac{8}{1}$
+50			6.0 331.8 326.0	C1 $\frac{9}{1}$
+61 ME			5.6 332.2 330.3	C5 $\frac{1}{1}$
2+00			2.7 335.1 329.2	C1 $\frac{8}{1}$
+05 ME			3.4 334.4 333.3	C4 $\frac{5}{1}$
+50	13.09	350.34	0.55 337.25 332.5	C0 $\frac{3}{1}$
+56 ME			13.0 337.3 336.8	C0 $\frac{8}{1}$
+56 MW <small>2 metrs</small>			13.3 337.0 336.7	C3 $\frac{2}{1}$
3+00			10.3 340.0 336.2	F0 $\frac{4}{1}$
+30 M.E.			8.1 342.2 342.4	C0 $\frac{1}{1}$
+44 M.E.			6.6 343.7 343.3	C4 $\frac{2}{1}$
+50			6.2 344.1 339.9	

ALLEY 192 CONT.

350.34

10/13/55

4700		1.9	348.4	344.0	C4 <sup>4</sup>	
+03 M.W.		3.9	346.4	347.7	F1 <sup>3</sup>	
06 M.E.		1.6	348.7	348.1	C0 <sup>6</sup>	
+31	763 35795	0.02	349.32	350.0	F0 <sup>2</sup>	
+50 (4)		7.0	351.0	346.8	C4 <sup>2</sup>	
+56 ME		6.8	351.2	350.9	C0 <sup>3</sup>	
5700		5.7	352.3	348.4	C3 <sup>2</sup>	
+01 ME		5.6	352.4	352.6	F0 <sup>2</sup>	
+13 MW		5.6	352.4	352.8	F0 <sup>2</sup>	
+31 MW		4.1	353.9	353.5	C0 <sup>4</sup>	
+45 ME		3.8	354.2	354.1	C0 <sup>2</sup>	
+50 (5)		3.9	354.1	350.4	C3 <sup>7</sup>	
6700		2.6	355.4	357.0	C4 <sup>2</sup>	
+15 ME		2.5	355.5	354.9	C0 <sup>4</sup>	
+41 ME		3.0	355.0	354.7	C0 <sup>3</sup>	
+50		3.2	354.8	350.6	C4 <sup>2</sup>	
+56 MW		2.9	355.1	354.5	C0 <sup>6</sup>	
+90 FH To L		4.3	353.7	349.5	C4 <sup>2</sup>	
+90 (5) Q FH°		4.1	353.9	353.9	C0 <sup>0</sup> TO FLANGE	361.93
+95 CL		4.7	353.3	349.3	C4 <sup>0</sup> Do not mark	327
8.36	361.93	4.38	353.57			358.66

C4<sup>4</sup> To L

Alley 131K 196  
N of University E of 33

34Ks For 6" AC Group 22

7.18	329.33	322.15	
0+80	10.54 337.88	1.99 327.34	
1+00		10.2 327.7 323.9	
+15 ME		9.6 328.3 328.4	
+25 3		9.7 328.7 324.6	
+25 MWK		9.2 328.7 328.8	
+50 ④		8.3 329.6 325.5	
+52 ME		8.3 329.6 329.8	
+60 MW		7.4 330.5 329.8	
+94 MW		6.9 331.0 331.0	
2+00		5.8 332.1 327.9	
+29 MW		5.3 332.6 332.4	
+50		4.1 333.8 329.5	
+66 ME		3.6 334.3 334.0	
+75 MW		3.0 334.9 334.0	
3+00		2.0 335.9 331.8	
+08 MW		1.9 336.0 335.6	
	7.07 343.84	1.11 336.77	
+27 ME		6.1 337.7 337.0	
+50		5.1 338.7 334.1	
+63 MW		5.1 338.7 338.4	

WEST  
WILLIAMS T  
KELLHOFER †

17

10-18-53 PARTLY CLOUDY

BM SW BP N of University

C TO EXISTING Begin Work

8	
C3	
F0	1
F0	1 C4
C4	1
F0	2
C0	1
C0	0
C4	2
C0	2
C4	3
C0	3
C0	2
C4	1
C0	4
C0	7
C4	6
C0	3

10/18/55

	343.84		339.6	338.6
+75 3+77 MW		4.2	339.6	335.2
+99 MW		4.6	339.2	339.3
4+00		3.2	340.6	335.9
+11 MW		3.5	340.3	339.6
	4.32	345.31	2.85	340.99
+25		4.4	340.9	336.5
+50		3.9	341.4	336.8
+59 MW	6.16	346.67	4.80	340.51
+77 MW		5.7	341.0	341.2
		8.25	338.42	
		5.10	341.57	=

$C_4 \frac{4}{C_1 \frac{0}{ON METER}}$   
 $F_0 \frac{1}{}$   
 $C_4 \frac{7}{}$   
 $C_0 \frac{7}{}$   
 $C_4 \frac{4}{}$   
 $C_4 \frac{6}{}$   
 $F_0 \frac{3}{}$   
 $F_0 \frac{2}{}$

Top existing 6' 05" on Bell

SEE FB 867



Balboa St.  
 Noyes to Lamont  
 Grade For Lowmoss Pipe  
 0+00 @ Noyes + Balboa

	0.45	54.60	54.15	
	4.35	49.63	45.28	40.1
4 0+00			526	44.37 41.1
+50			541	44.22 41.2
1+00			545	44.18 41.2
+50			542	44.21 41.3
2+00			540	44.23 41.4
+50			529	44.34 41.5
3+00			517	44.46 41.6
+50			511	44.52 41.7
4+00			501	44.62 41.8
+50			482	44.81 41.9
5+00			459	45.04 42.0
+50			447	45.16 42.2
	6.08	51.00	47.1	44.92
6+00			638	44.62 41.8
+50			614	44.86 40.8
7+00			591	45.19 41.0
+50			550	45.50 41.0
8+00			528	45.72 41.3

West  
 Williams X  
 Kullbofer +

19

10-26-55

CLEAR

AMCO LIT New Hambleton + Marcell

<del>C3</del> <sup>3</sup>	<del>C4</del> <sup>3</sup>
<del>C3</del> <sup>0</sup>	<del>C4</del> <sup>0</sup>
<del>C3</del> <sup>2</sup>	<del>C4</del> <sup>0</sup>
<del>C2</del> <sup>9</sup>	<del>C3</del> <sup>9</sup>
<del>C2</del> <sup>8</sup>	<del>C3</del> <sup>8</sup>
<del>C2</del> <sup>8</sup>	<del>C3</del> <sup>8</sup>
<del>C2</del> <sup>9</sup>	<del>C3</del> <sup>9</sup>
<del>C2</del> <sup>8</sup>	<del>C3</del> <sup>8</sup>
<del>C2</del> <sup>8</sup>	<del>C3</del> <sup>8</sup>
<del>C2</del> <sup>9</sup>	<del>C3</del> <sup>9</sup>
<del>C3</del> <sup>0</sup>	<del>C4</del> <sup>0</sup>
<del>C3</del> <sup>0</sup>	<del>C4</del> <sup>0</sup>
<del>C2</del> <sup>8</sup>	<del>C3</del> <sup>8</sup>
<del>C4</del> <sup>1</sup>	
<del>C4</del> <sup>2</sup>	
<del>C4</del> <sup>5</sup>	
<del>C4</del> <sup>4</sup>	

## BALBOA ST. CONT.

20

57.00

9+50	5.03	45.97	41.5
9+00	1.65	46.35	42.7
+50	4.21	46.79	42.7
10+00	3.76	47.24	43.6
+50	3.32	47.68	44.0
11+00	2.77	48.23	44.1
11+50		48.7	44.8
9.44	54.49	59.5	45.05
	0.38	54.11	

Balboa St & Grand St  
Marrell to Lamont 5ths for meters  
0+00 Wly Line of Marrell St

B.M. 0.42 54.57 54.15

T.P. 6.38 50.19 10.76 43.81

3 METERS

0+00	10.0	40.2	40.2
+99	6.6	43.6	41.2
1+27	6.8	43.4	41.6
2+92	4.7	45.5	43.9
3+46	3.8	46.4	44.8
+86	3.5	46.7	45.6
4+15	3.0	47.2	46.1

10/26/55

C4 <sup>5</sup>  
C3 <sup>I</sup>  
C4 <sup>I</sup>  
C3 <sup>6</sup>  
C3 <sup>I</sup>  
C4 <sup>I</sup>  
C3 <sup>I</sup>

54.15

WEST KELLHOFER  
WILLIAMS VARONAKIS

10/31/55

BM (2) T. Marrell & Hornblend St

C0 <sup>0</sup>	#	1977	GRAND So. SIDE
C2 <sup>4</sup>		1965	
C1 <sup>8</sup>		1959	
C1 <sup>6</sup>		1937	
C1 <sup>6</sup>		1927	
C1 <sup>I</sup>		1917	
C1 <sup>I</sup>		1915	

BALBOA ST. STKS. FOR  
METERS

50.19

3+77 2.1 48.1 48.0

3+25 2.2 48.0 47.6

2+74 2.6 47.6 47.2

2+22 3.1 47.1 46.8

T.P. 5.63 55.79 0.03 50.16

CHECK  
B.M. 1.66 54.13 = 54.15

WEST  
WILLIAMS X  
VARONFAKIS  
KELLHOFER †

21

CLOUDY  
10/31/55

CO <sup>1</sup> #1924

CO <sup>4</sup> BALBOA ST No. SIDE

CO <sup>4</sup> #

CO <sup>4</sup> #

CO <sup>4</sup> #

CO <sup>3</sup> #

CO <sup>3</sup> # 1946-50

Grand Ave North Side  
 STKS for lowering 6" AC  
 at Storm Drain King 20+50-21+00

7.34	13.39	6.05	
20+25	2.4	11.0	7.0
+50	2.7	10.7	4.3
			4.4
+62 <sup>5</sup>	2.9	10.5	<del>3.0</del>
+75 <sup>5</sup>	6.4	7.0	2.5
+88 <sup>5</sup>	3.9	9.5	4.2
21+00	4.2	9.2	4.0
	9.7	3.7	
20+68	8.3	4.1	
20+80	8.5	3.9	

Grand Ave South Side 8" AC

5.57	11.62	6.05	
20+50	3.9	7.7	
+62 <sup>5</sup>	3.9	7.7	2.4
+75 <sup>5</sup>	6.5	5.1	1.0
+88 <sup>5</sup>	4.5	7.1	2.2
21+00	5.0	4.6	
20+75 <sup>5</sup>	8.46	3.17	2.3 to bottom
20+76 <sup>5</sup>	9.01	3.1	to butt 42" 11'
	5.57	6.05	

WEST  
 WILLIAMS  
 VARONAKIS  
 KELLHOFER

10/31/55 Cloudy

C4 <sup>0</sup>  
 C4 <sup>4</sup>  
 C6 <sup>5</sup> L  
 C4 <sup>5</sup> C6  
 C4 <sup>5</sup> = 22 1/2 BEND  
 C5 <sup>3</sup>  
 C5 <sup>2</sup>

13.39  
 1.03  
 9.31  
 3.9  
 4.41

Bottom of 16" OD Cone Storm Drain

Top of 6" AC pipe

Top of " " "

C5 <sup>3</sup>  
 C4 <sup>1</sup>  
 C4 <sup>2</sup>  
 11 1/4 BEND

11.62  
 4.66  
 7.0  
 7.0  
 11.6  
 -4.02  
 7.5  
 3.9  
 3.6

Top 8" AC Main

Top 36" ID Cone pipe Drain

11.62  
 4.00  
 7.6  
 4.0  
 3.6

Balboa St Noyes to Olney

STKs for Lowering 10" @

0+00 @ Noyes + Balboa

3.41 17.78 44.37

0+50 3.6 44.2 40.0

1+00 4.0 43.8 39.6

0+75 <sup>1.50</sup> (5) 4.1 43.7 43.0 C02 to flange C39 to EN

1+50 4.4 43.4 39.2

2+00 4.8 43.0 38.8

+50 5.4 42.4 38.0

3+00 6.0 41.8 36.8

+50 6.7 41.1 35.8

4+00 7.6 40.2 35.0

+50 8.3 39.5 34.4

5+00 9.1 38.7 33.5

+50 9.6 38.2 32.6

3.59 44.19 = 44.22 0+60 page 19

2.02 46.39 44.37

11.17 35.22

5.62 41.62 10.44 35.95

9.42 32.20

7.39 34.23

9.34 32.28

WEST  
WILLIAMS X  
VARONFAKIS  
KELLHOFER †

32.8

8

31.5

23

11/4/55 CLEAR + WARM

0+00 from page 19

C42

C42

C02 to flange C39 to EN

C42

C42

C42

C50

C52

C52

C51

C52

C56

41.62

- 5.29

36.33

+ 12.45

48.78 Hi

4.55

44.23 0+50 = 44.22

Noyes + Grand

Top 10" @ North Side Line

South Side Grand

Top 10" @ at 8" AC Main on  
10' East of 10" @ King

Top 6" AC Main North Side Grand @ Noyes

Top 8" " " South " " " "

Noyes St Grand Ave. to  
Hornblend Stks for lowering 10°01

Meters set 7<sup>2</sup> Rt 37<sup>2</sup> Lt 119641

3.84 48.21 44.37

0+00	13.3	34.9	30.6
+50	13.1	35.1	31.8
1+00	12.4	35.8	33.0
1+19 ME	9.0	39.2	38.4
1+50	8.9	39.3	34.6
1+93 ME	6.2	42.0	39.6
1+95 MW	5.0	43.2	40.4
2+00	5.3	42.9	36.4
+28 ME	4.7	43.5	41.3
+50	4.5	43.7	38.2
3+00	4.8	43.4	39.4
+50	3.7	44.5	40.2
A+00	1.0	47.2	41.2

7.42 55.11 55.2 47.69

+50	3.1	52.0	43.4
+76 ±	1.6	53.5	44.2

10.74 44.37 = 44.37

West  
Williams X  
Varenakis ↑  
Kellhofer

11/14/55 PARTLY CLOUDY

0+00 Nail see page 19

C4 <sup>3</sup> 0+00 South prop line Grand

C3 <sup>3</sup>

C2 <sup>8</sup>

C0 <sup>8</sup>

C4 <sup>7</sup>

C2 <sup>4</sup>

C2 <sup>8</sup>

C6 <sup>5</sup>

C2 <sup>2</sup>

C5 <sup>5</sup>

C4 <sup>0</sup>

C4 <sup>3</sup>

C6 <sup>0</sup>

C8 <sup>6</sup>

C9 <sup>3</sup>

Poe St Willow St to 300 NW

Stks for 6" AC Main

Group RR

6.39 184.18 172.29

0+70 6.3 177.9 175.0

1+00 2.6 181.6 174.4

+50 5.3 178.9 172.0

+70 MS 9.0 175.2 174.7

+70 MN 7.7 176.5 175.7

+75 9.6 174.6 169.2

2+00 0.64 172.72 12.10 172.08 165.0

+20 MN 3.1 169.6 167.0

+25 MS 4.0 168.7 165.6

+25 4.7 168.0 161.8

+50 8.6 169.1 156.5

+75 MN 11.6 161.1 158.0

+75 1.25 161.58 12.39 160.33 153.9

3+00 5.6 156.0 152.0

+10 2" BO 6.7 154.9 151.4

+30 MN 2.5 154.1 154.5

13.12 174.64 0.6 161.62

16.13 184.95 1.12 174.52

7.14 177.81 = 177.79

West  
Williams X  
Kathofer 4

10-21-55

0  
11  
16

16  
11  
11

25

RD SW Cor Poe St & Willow St

(2) <sup>9</sup> Begin Work (No Cut)

(7) <sup>2</sup>

c6 <sup>9</sup>

c0 <sup>5</sup>

c0 <sup>8</sup>

(5) <sup>4</sup>

c7 <sup>1</sup>

c2 <sup>6</sup>

c3 <sup>1</sup>

c6 <sup>2</sup>

c7 <sup>6</sup>

c3 <sup>1</sup>

c6 <sup>4</sup>

c4 <sup>0</sup>

c3 <sup>5</sup>

F0 <sup>4</sup>

3321

3318

3330

3329

3336

3374

POE ST WILLOW ST To 300' N.W.  
CONTINUED

WEST  
WILLIAMS X  
VARON FAKIS  
KELLHOFER †

26

11/22/55 SUNNY

B.M.	5.88	183.67	177.79
1+70 M.N.		8.3	175.5 175.8
1+70 M.S.		7.6	176.2 174.6
T.P.	0.71	171.59	12.69 170.98
2+20 M.N.		2.4	169.2 167.1
2+25 M.S.		2.5	169.1 165.5
2+75 M.N.		10.8	160.8 158.1
T.P.	2.81	161.87	12.53 159.06
3+30 M.N.		7.9	154.0 154.4
T.P.	12.51	174.23	0.15 161.72
T.P.	10.95	184.76	0.42 173.81
CHECK B.M.		7.07	177.69

S.W.B.P. POE ST + WILLOW ST	
F0 <sup>3</sup>	3318
C1 <sup>6</sup>	3321
C2 <sup>1</sup>	3330
C4 <sup>4</sup>	
C2 <sup>7</sup>	3336
F0 <sup>4</sup>	3344



Balboa St Noyes to Olney  
 STKS for Meters

0+00 Balboa + Noyes

283 47.20 44.37

1+39 MS	38	43.4	43.4
1+71 MS	4.3	42.9	43.2
2+23 MS	4.8	42.4	42.9
2+91 MS	5.5	41.7	42.0
3+28 MS	6.0	41.2	41.5
3+73 MS	6.7	40.5	40.8
3+95 MS	6.9	40.3	40.6
4+34 MS	7.3	39.9	40.0
5+17 MS	8.7	38.5	38.7
5+23 MN	7.5	39.7	39.3
4+76 MN	6.8	40.4	40.2
4+47 MN	6.7	40.5	40.5
4+05 MN	6.0	41.2	41.1
3+22 MN	5.1	42.1	42.2
2+79 MN	3.9	43.3	42.4
11.38	56.73	1.85	45.35
2+14 MN	9.1	47.6	42.9
1+83 MN	8.9	47.8	43.2
1+76 MN	6.2	50.5	43.5

West  
 Williams x  
 Varonakis +  
 Kullhofer 12/1/55

27

00015

JBM see page 19

Co <sup>0</sup>	2133
FO <sup>3</sup>	2135-37
FO <sup>5</sup>	2139-41
FO <sup>3</sup>	2143-45
FO <sup>3</sup>	2147-49
FO <sup>3</sup>	2151-53
FO <sup>3</sup>	2157-55
FO <sup>1</sup>	2159-61
FO <sup>2</sup>	1442 Olney
Co <sup>4</sup>	4460 Olney
Co <sup>2</sup>	2168
Co <sup>0</sup>	2160-59
Co <sup>1</sup>	2152
FO <sup>1</sup>	2144
Co <sup>2</sup>	2136 <sup>0</sup>
C4 <sup>1</sup>	2130
C4 <sup>6</sup>	2124-22
C7 <sup>0</sup>	2112

BALBOA ST. CONT.

56.73

0+73 MN

3.9 52.8 43.9

12.35 44.38 =

C<sup>2</sup><sub>8</sub>

44.37

12/1/55

2455 Noyce

177th St T<sup>st</sup> to Logan Ave  
 Preliminary Group 109

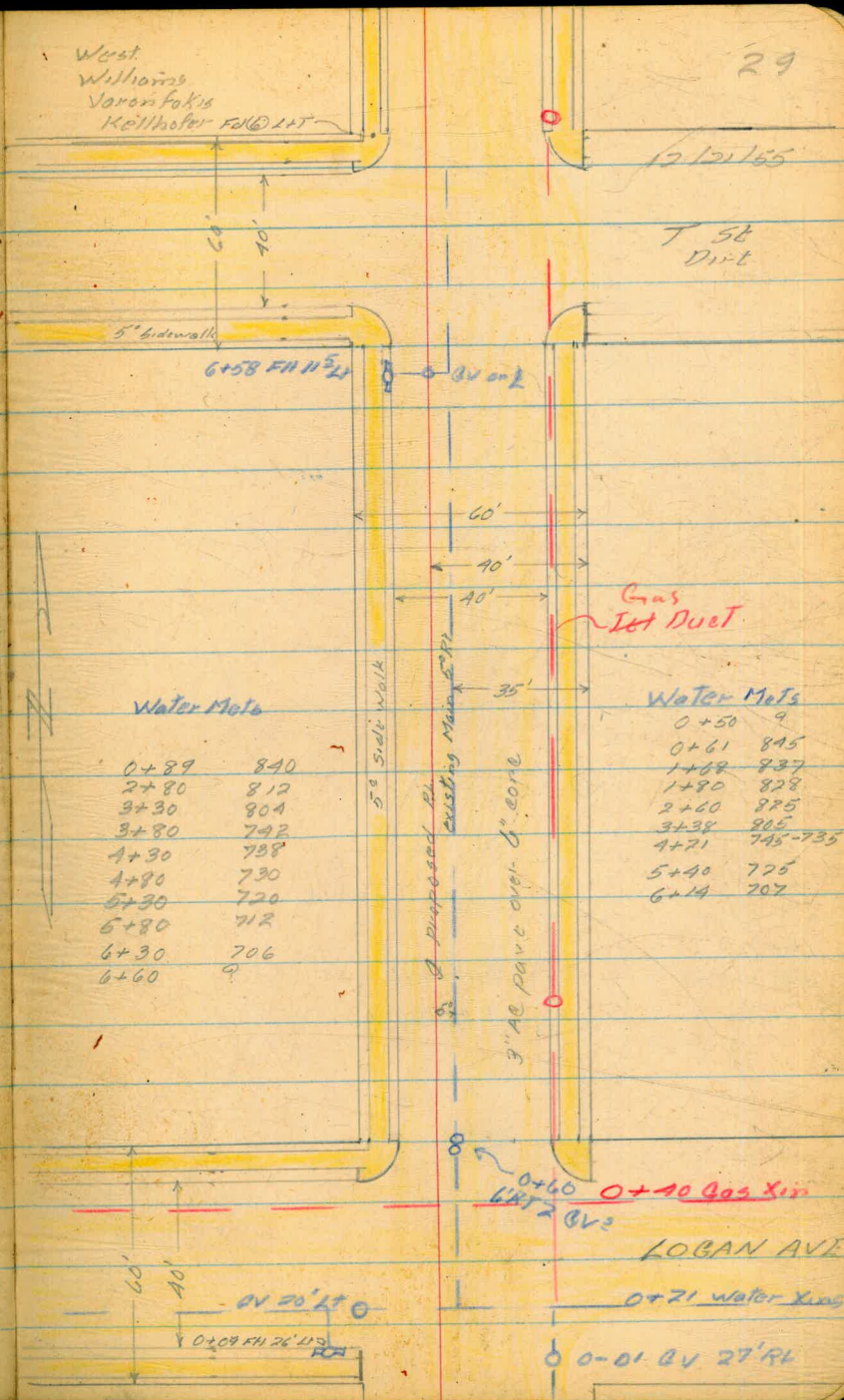
West  
 Williams  
 Varenakis  
 Kellhofer F&C LIT

29

12/21/65

7+20<sup>33</sup> P.O.T. Nly stop line T<sup>st</sup>

T<sup>st</sup> St  
 Dirt



Water Meters

0+89	840
2+80	812
3+30	804
3+80	792
4+30	788
4+80	780
5+30	720
5+80	712
6+30	706
6+60	9

Water Meters

0+50	9
0+61	845
1+68	837
1+90	828
2+60	825
3+38	805
4+21	745-735
5+40	725
6+14	707

0+30 P.O.T. FH @ 1" ID with @ T 10' R/L  
 0+00 sly prop line Logan

0+60 0+40 Gas Xing  
 0+71 Water Xing  
 0-01 BV 27' R/L

I Profile

	1.73	127.54	125.81
0+00		9.79	117.75
+50		8.86	118.68
1+00		8.29	119.25
+50		7.73	119.81
2+00		7.17	120.37
+50		6.61	120.93
3+00		6.06	121.48
+50		5.42	122.12
4+00		4.82	122.72
+50		4.25	123.29
5+00		3.59	123.95
+50		3.08	124.46
6+00		2.56	124.98
+50		2.01	125.53
7+00		1.76	125.78
+20		1.94	125.60

Reduced by J. Gray 1-17-56

1.98 127.19 1.73 125.81  
10.73 116.96 =

SWBP 47th + T St

9.64	
10.81	Sly prop Line Logan Ave
8.78	
10.81	Q 51
8.12	
10.81	"
7.59	
10.81	"
7.04	
10.81	"
6.47	
10.81	"
5.91	
10.81	"
5.30	
10.81	"
4.76	
10.81	"
4.10	
10.81	"
3.51	
10.81	"
2.95	
10.81	"
2.36	
10.81	"
1.84	
10.81	"
1.62	
10.81	"
1.74	
10.81	Q 51

Sly prop Line T St

116.49 SWBP 47th + Oceanview

10th St Division St to Marine View  
 Prelim Group 109

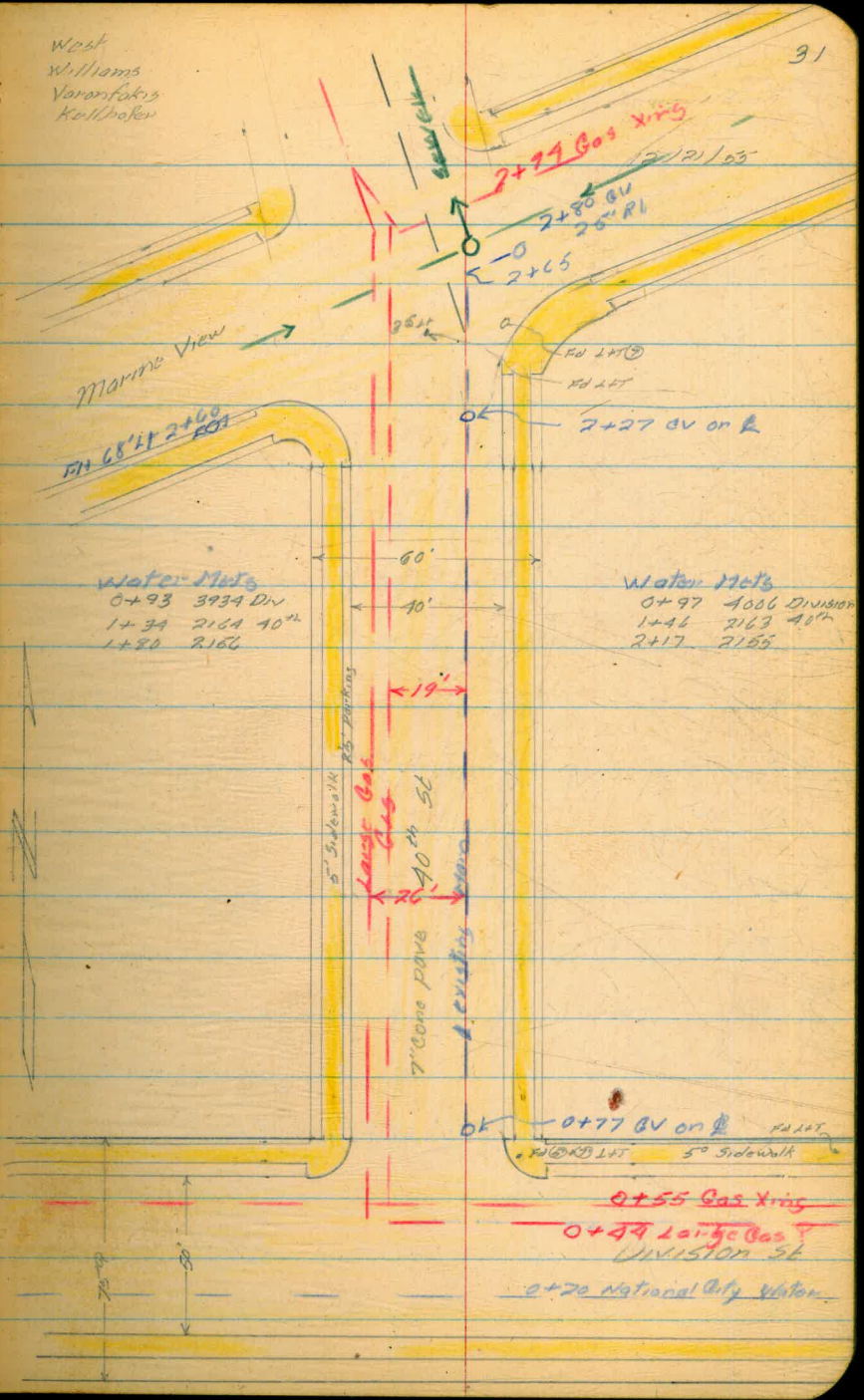
3+38 end of work

2+56 <sup>60</sup> 7° 23' 20" 1/4 CA 1+T 95%K

0+70 POT

0+00 Sky prop line Division 9

West  
 Williams  
 Varanfakis  
 Kallbaker



Profile

0+7	57.81	57.34	
223	48.50	11.54	46.27
0+00		2.4	46.1
0+13		2.60	45.90
0+13		3.21	45.29
+50		2.57	45.93
1+00		3.38	45.12
+50		4.25	44.25
2+00		5.25	43.25
+50		5.98	42.52
+56 <sup>60</sup>		6.05	42.15
+87		6.48	42.02
+87		6.72	42.02
3+00		6.69	41.82
+38		8.20	40.30
13.17	59.44	2.23	46.27
12.68	70.02	2.10	57.34 = 57.34
9.44	78.95	0.53	69.49
		5.14	73.79 = 73.75

Reduced by J. Gray 1-17-55

+53 to flow line

41<sup>st</sup> + Division NW BP

Turn on LTT NE Cor. 40<sup>th</sup> + Division

Sly prop line Division

Top Eb Division

Butter Line

Sewer Xray

Top East Rim Sewer MH 10' RT

West end Eb ret Marine View + Division

ETA ST

39th St to 270' East

Relco Group 104

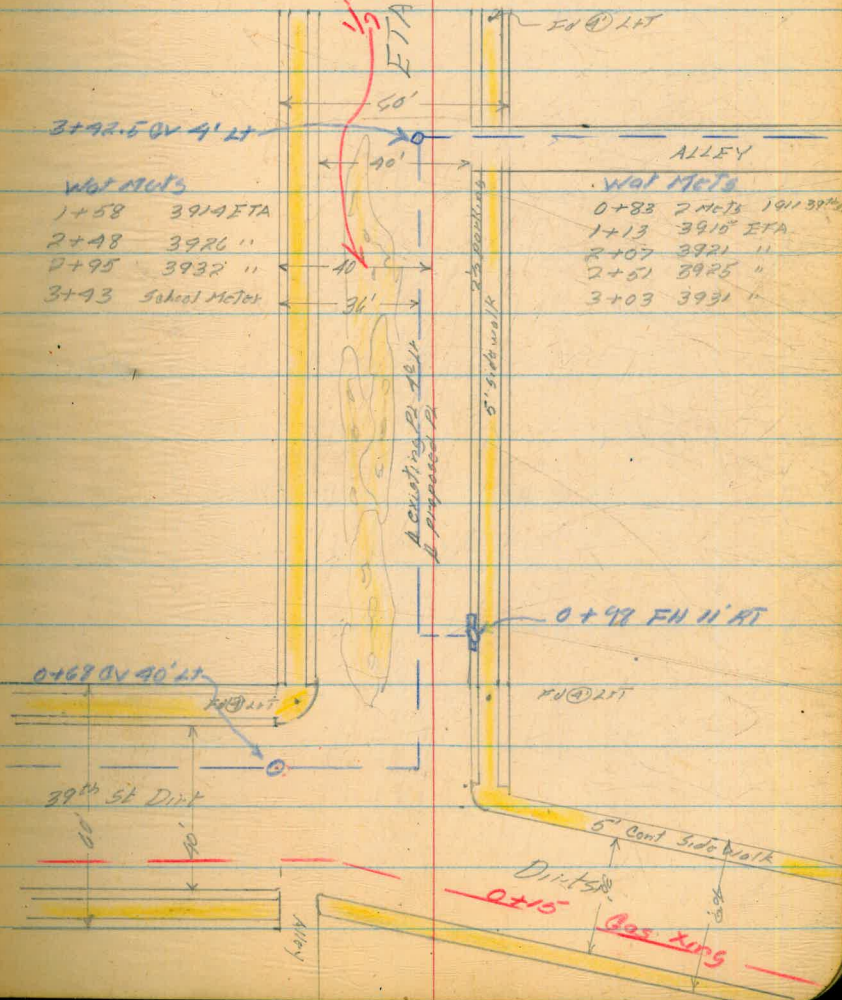
West  
Williams  
Varonfakis  
Kellhofer

39

12/22/53

3+50

End of Work



Oil pipe  
Broken Very Poor  
Condition

0+85 POT Ed Ltr. 10' R1 (P) Ed. prop line 39th

0+00 Why prop line 39th St

ETA ST.  
39<sup>th</sup> To 350' EAST  
PRISM GROUP 104

WEST  
WILLIAMS T  
VARDONAKIS P  
KELLHOFER

34

COLD & CLEAR 12/21/55

B.M.	0.56	42.62	42.06
0+00		7.06	35.56
+06 <sup>5</sup>		7.20	35.42
+50		6.3	36.32
1+00		5.2	37.42
+50		4.3	38.32
2+00		3.5	39.12
+50		2.7	39.92
3+00		2.1	40.52
+50		1.6	41.02
TP	9.18	51.11	0.69 41.93
TP	5.35	56.17	0.29 50.82
CHK. B.M.		3.11	53.06 = 53.06

S.W.B.P. 39<sup>th</sup> & EPSILON

CURB LINE

END OF WORK

N.W.B.P. 40<sup>th</sup> & EPSILON



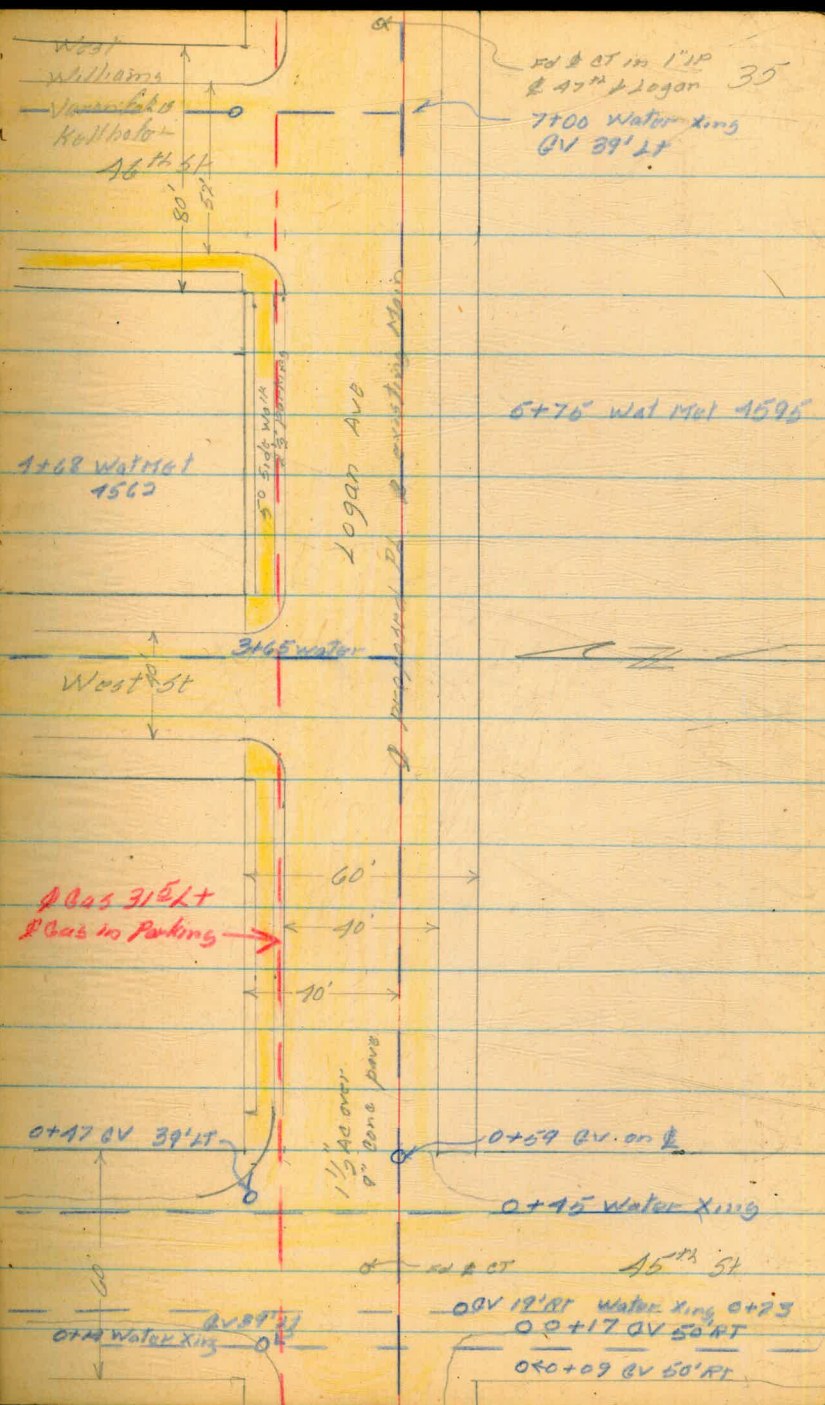
Logan St 45<sup>th</sup> to 46<sup>th</sup>

Palm Group 109

7+30  
62

7+30

Ely prop line 46<sup>th</sup> St



6+75 Wat Met 4596

1+62 Water 1562

Gas 315 LT  
Gas in Parking

0+30 POT Ed & CT 10' LT

0+00 Wly prop line 45<sup>th</sup>

Ed & CT 45<sup>th</sup> St

0+75 Water Xing 0+75  
0+17 GV 50' RT  
0+09 GV 50' RT

Profile Logan St  
45<sup>th</sup> St. To 46<sup>th</sup> St.

	1.77	119.52		117.75	
	0.07	107.33	12.26	107.26	
	0.73	95.08	12.98	94.35	
	9.73	194.66	10.15	84.93	=
0+00			9.78	84.88	
+50			9.70	84.96	
1+00			8.48	86.18	
+60			7.41	87.25	
2+00			6.40	88.26	
+50			5.30	89.36	
3+00			4.12	90.54	
+50			2.95	91.71	
4+00			1.36	93.30	
T.P.	10.54	104.89	0.31	94.35	
+50			9.63	95.26	
5+00			7.49	97.40	
+50			5.21	99.68	
6+00			2.96	101.93	
+50			0.94	103.95	

WEST  
WILLIAMS  
VARONEAKIS X  
KELLHOFER †

36

12/22/55 Partly Cloudy

117.75 0+00 Sta from page 30.

85.03 † at 45<sup>th</sup> + Logan

Why prop line 45<sup>th</sup>

Reduced by J Gray 1-18-56

LOGAN ST. CONT.

37.

104.89

12/22/55

T.P. 8.83 113.24 0.48 104.41

7+00 8.40 104.84

+30 7.99 105.25

T.P. 9.01 120.32 1.93 111.31

CHECK

T.B.M. 2.56 117.76 = 117.75

PAGE 36

ORANGE AVE Sharron Pl To Spartan Dr  
Relocation of 12" AC Main in Easement

PALM CITY FORCE

9+90<sup>86</sup>

End of Work

6+40<sup>86</sup>  $\Delta$

90° 09' 30" LT

5+52.66  $\Delta$

90° 00' 00" RT

2.3  
50.36

0+96  $\Delta$

90° 00' 00" RT

0+00

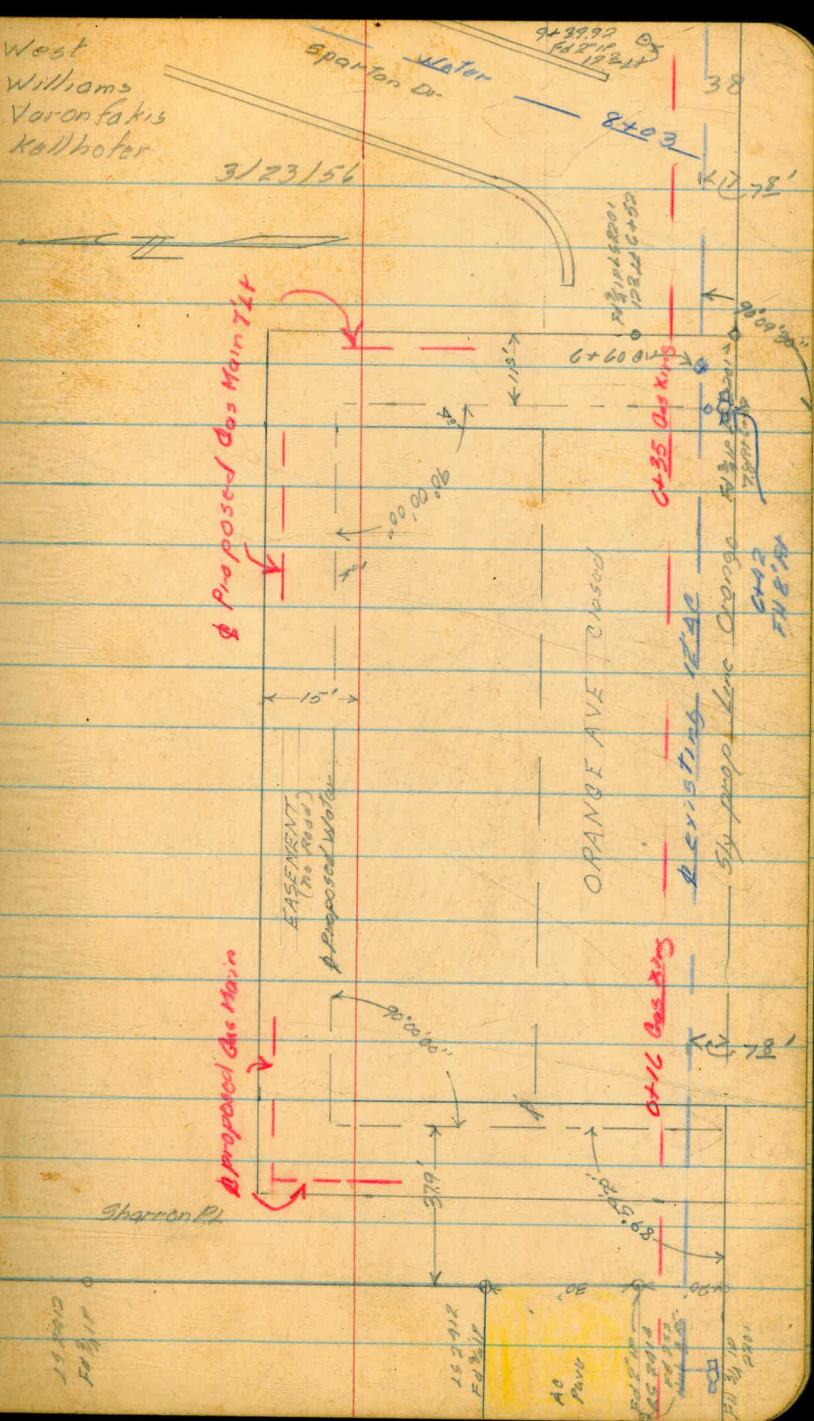
5ly prop line Orange Ave

West  
Williams  
Varonfakis  
Kallhofer

3/23/56

Proposed Gas Main 7ft

Proposed Gas Main



Q Profile  
Caseiment

39

	11.40	380.60		369.20
0+00			9.1	371.5
+50			9.6	371.0
0+96 $\Delta$			9.9	370.7
1+00			9.8	370.8
+50			5.2	375.4
	13.02	392.91	0.71	379.89
2+00			11.8	381.11
+50			6.7	386.21
3+00			1.9	391.01
	12.82	405.20	0.53	392.38
+50			8.9	396.3
4+00			1.8	403.4
	12.83	417.86	0.17	405.03
0+40			7.1	410.76
+50			6.7	411.16
+58			3.7	414.16
0+70			1.9	415.96
5+00			1.3	416.56

See FB 867

TBM Top FH 5E Cor 55<sup>th</sup> + Orange

51/4 prop line Orange St

	917.86		
5+52 <sup>66</sup> <del>7</del>	9.9	407.96	
+81	10.1	407.76	
6+00	12.4	405.46	
6+07			
0.57	406.44	11.99	405.87
6+21	2.9	403.54	
+29	1.8	404.64	
+36	3.2	403.24	
+40 <sup>86</sup> <del>7</del>	4.0	402.44	
+50	4.3	402.14	
7+00	9.7	396.74	
0.53	394.61	12.36	394.08
+50	2.8	391.81	
7+46			
8+00	8.9	385.71	
+09			
+10	10.07	384.54	
+15	8.8	385.81	
+16			

9' Lt to wood fence 12' Lt to 1' wire fence

10' Lt to wood fence (end south)  
6' Rt to Dead man 12' Lt to power pole

11547991

$\frac{13.4}{12' Lt. Burial}$  <sup>Road Cut</sup>  $\frac{8.1}{10' Lt. Top Bank}$

$\frac{6.10}{14' Lt. Edge of Pavement}$  <sup>splitter Dr.</sup>  $\frac{5.2}{12' Lt.}$   $\frac{2.0}{9' Lt. Top of Bank}$

Begin wood barricade on R

end wood barricade

9' Lt Flow Line 12" Steel Drain

12" Steel Drain Xing

5' Rt end storm drain (end is buried)

Profile

394.61

8+50	9.6	385.01
9+00	9.4	385.21
+50	9.6	385.01
+90 8L	11.4	383.21
	9.25	385.36 =

41

10.0	Bank	11.7
5' RT Top		15' RT
10.3	Bank	12.9
8' RT Top		20

end of work

FB 2099  
385.39 Top of East Ch A 13' Lt Sta 8+10  
Spartan Du

ROBINSON ST 10<sup>th</sup> Ave  
to PARK Blvd

Pelims

42+79<sup>85</sup>

12+47<sup>85</sup> POT

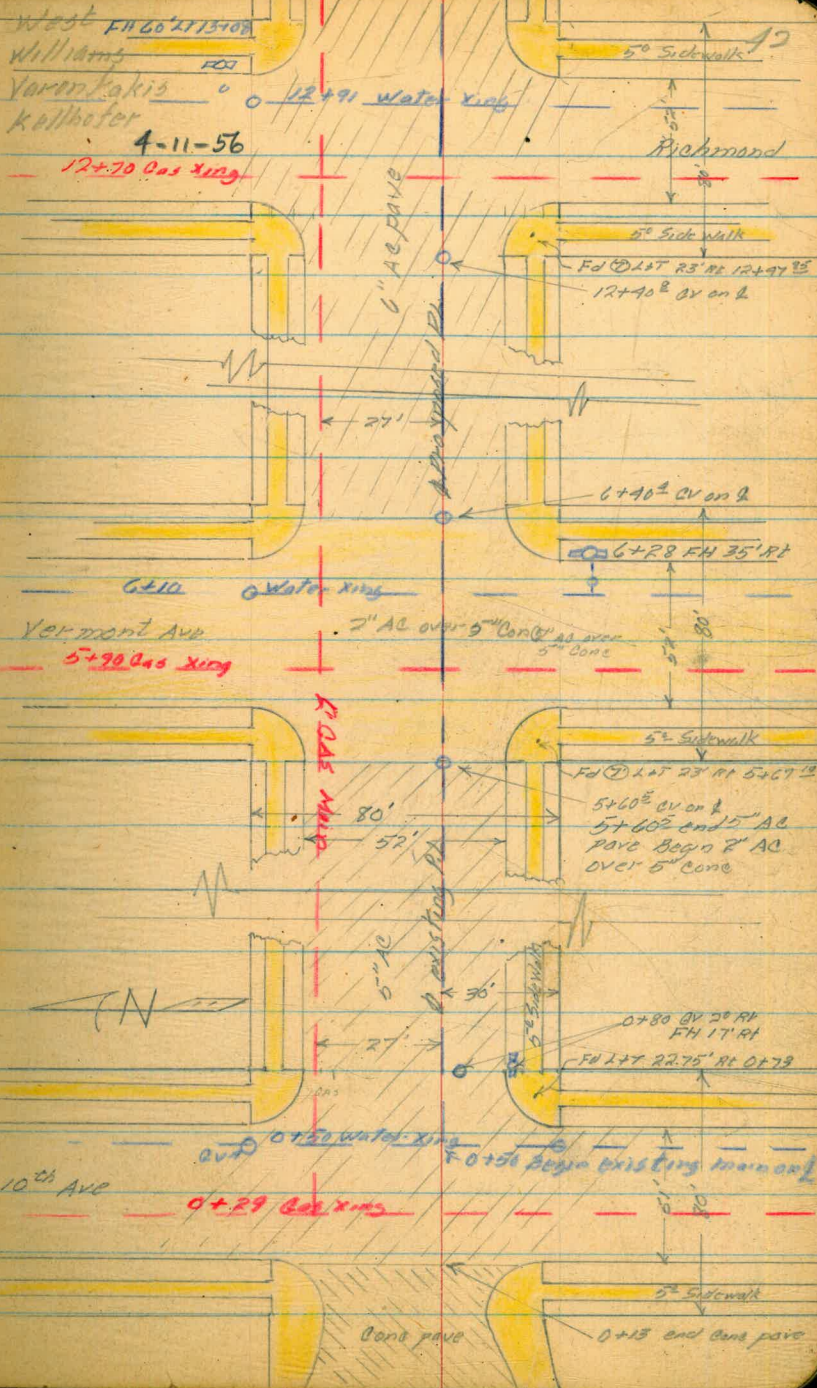
5+67<sup>13</sup> POT

(31+05 Plan S<sub>A</sub>)

0+73 POT

0+00

Why prep Line 10<sup>th</sup> Ave



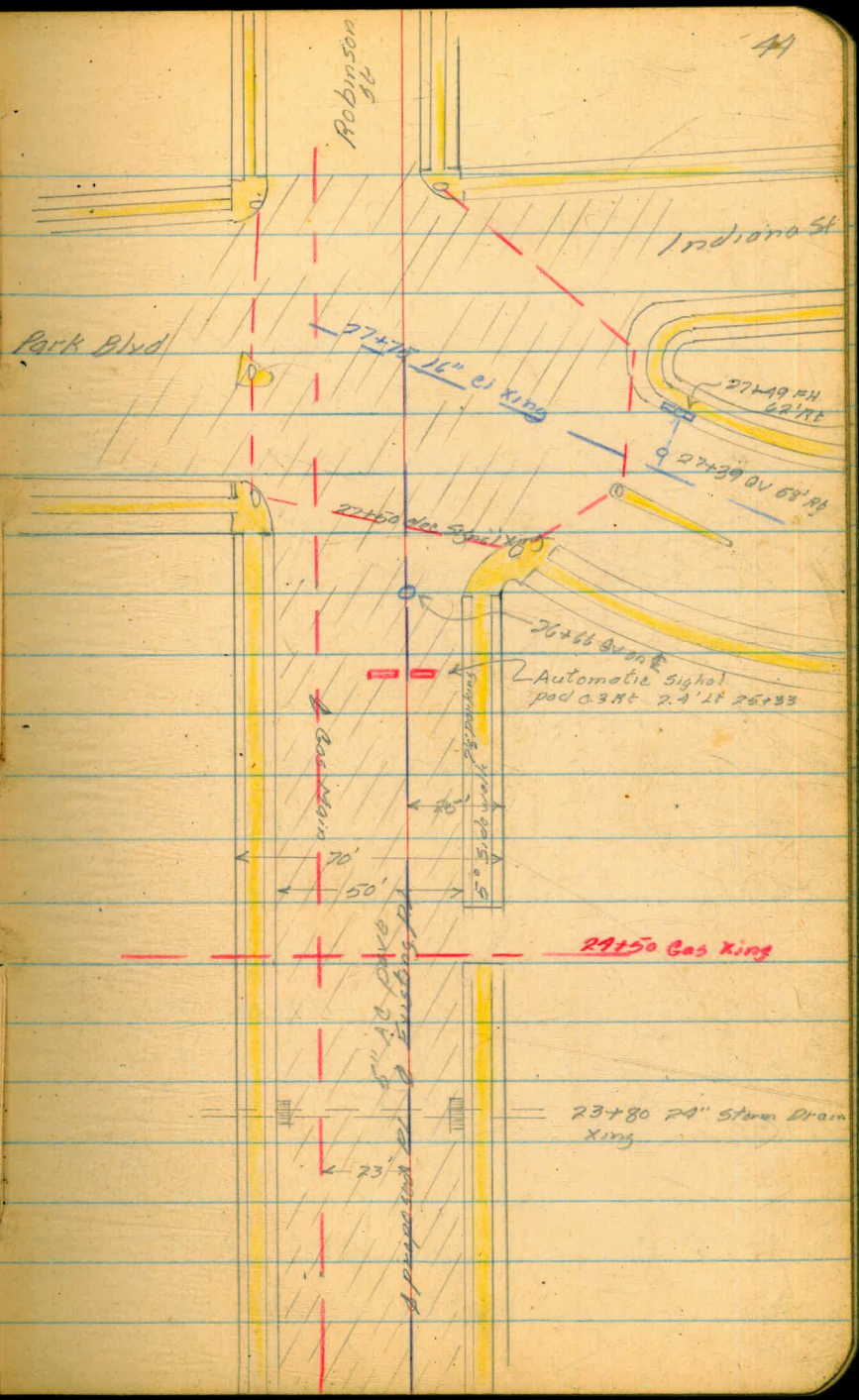






ROBINSON ST - Cont

28+46 Fly Cb Line Indiana  
27+75 16" Water Main Xing



## Robinson St. Q. Profile

	7.14	289.15 ✓	282.01
0+00		8.63	280.52 ✓
+13		8.25	280.90 ✓
+50		7.60	281.55 ✓
+50		9.12	280.03
+80		8.38	280.77 ✓
+80		7.34	281.81 ✓
1+00		7.04	282.11 ✓
+50		6.67	282.48 ✓
2+00		6.15	283.00 ✓
+50		5.74	283.41 ✓
3+00		5.28	283.87 ✓
+50		4.84	284.31 ✓
4+00		4.41	284.74 ✓
+50		3.98	285.17 ✓
5+00		3.43	285.72 ✓
+50		2.82	286.33 ✓
+60 <sup>±</sup> CV		3.96	285.19 ✓
+60 <sup>±</sup>		2.72	286.43 ✓
6+00		2.12	287.03 ✓

West  
Williams  
Voronofsky  
Kollhofer

45

4/11/56

BP SE Cor. 10<sup>th</sup> RobinsonWly prop line 10<sup>th</sup>

and some part begin AC

31' RT Top GV stem 7.67 on ground

Top stem GV on 2

Top AC pave

Top stem of GV on 2

Top AC pave

Robinson St Cont

289.15

6.69	293.78 ✓	286	287.09 ✓
6+10		7.59	<sup>286.19</sup> <del>286.2</del>
6+10		6.06	287.72 ✓
6+13		8.41	285.37 ✓
6+13		7.27	286.51 ✓
6+40		7.81	285.97
6+40		6.80	286.98 ✓
+50		6.57	287.21 ✓
7+00		5.95	287.83 ✓
+50		5.30	288.48
8+00		4.77	289.01 ✓
+50		4.26	289.52 ✓
9+00		3.72	290.06 ✓
+50		3.17	290.61 ✓
10+00		2.51	291.27 ✓
+50		2.04	291.74 ✓
11+00		1.54	292.24 ✓
+50		0.97	292.81 ✓
8.54	299.44 ✓	288	290.90 ✓

46

Top stem BV 35' RL

Top stem BV 50' LT

Top AC pave 50' LT

Top stem BV 35' RT } FH BV

Top AC pave 35' RT } 170 GV on Pipe Line

Top stem BV on 4

Top AC pave on 4

299.44

12+00	6.06	293.38 ✓
+40 <sup>2</sup>	6.58	292.86
+40 <sup>2</sup>	5.65	293.79 ✓
+50	5.52	293.92 ✓
+90	6.25	293.19
+90	5.00	294.44 ✓
13+00	5.00	294.44 ✓
	5.35	294.09 ✓
+50	5.71	293.73 ✓
+85	6.55	292.89 ✓
14+00	6.83	292.61 ✓
+50	2.97	291.47 ✓
15+00	9.13	290.31 ✓
+50	10.43	289.01 ✓
2.95	297.04 ✓	5.35 294.09 = 294.05
15+63	13.41	283.64 ✓
15+63	8.05	288.99 ✓
15+69	8.36	288.68 ✓

Top stem GV on  $\phi$   
 Top AC pave  
 Top stem GV 51' LT  
 Top AC pave 51' LT  
 SW BP Robinson + Richmond  
 Storm Drain  
 Top 54" dia A - M11 31' LT  
 SW BP Robinson + Richmond  
 Top 3'x4' Box Storm Drain 33' LT  
 Top storm Drain Grate 33' LT

Robinson St Cont

297.09

15+69	17.75	279.29 ✓
15+69	9.05	287.99 ✓
16+00	7.68	289.36 ✓
		+11.0 To Flow
16+11	7.32	289.72 ✓
+50	7.02	290.02 ✓
17+00	6.44	290.60 ✓
+50	6.11	290.93 ✓
+63	7.69	289.35
+63	6.19	290.85 ✓
6.68	300.73 ✓	2.99 294.05 ✓ = 294.05
18+91	8.00	292.73 ✓
18+91	7.16	293.57 ✓
19+00	8.02	292.71 ✓
19+10	8.91	291.82
+10	7.83	291.90 ✓
+50	7.43	293.30 ✓
20+00	6.74	294.2 293.99
+50	6.10	291.63 ✓
21+00	5.57	295.16 ✓

14' Rt Top 18" Storm Drain pipe

Top Storm Drain Grate

Flows South from N 24 W

Top sly rim sewer MH 10' ZL

Top Stem CV 30' Rt Robinson Pt

Top Ground 30' Rt

TP NE DP Robinson + Herbert

50' H Top Stem CV

Top AC pave 50' H

Top Stem CV on C

Top AC pave

300.73

21+50	4.93	295.80 ✓
+62 <sup>81</sup> <del>2</del>	4.98	295.75 ✓
22+00	5.53	295.20 ✓
22+00	7.18	293.55
22+00	5.73	295.00
22+18 <sup>92</sup> <del>2</del>	5.95	294.78 ✓
+50	7.98	292.75 ✓
23+00	12.40	288.33 ✓
23+50	9.63	297.17 ✓
23+80	11.51	285.66 ✓
+80	15.28	281.89 ✓
23+80	12.53	284.64 ✓
23+80	12.18	284.99 ✓
23+80	14.09	283.08 ✓
23+80	12.57	284.58 ✓
24+00	11.95	285.22 ✓
+50	10.72	286.45 ✓
25+00	7.59	289.58 ✓
+50	3.81	293.36 ✓
25+00	10.68	306.71 ✓
	1.19	296.03 ✓

Top stem by 44' Lt center of  
 Top AC pave 44' Lt.

Top 24" Storm Drain 13° Rt  
 Top Storm Drain Grate  
 12.53  
 2.25 13081  
 15.28

12.57  
 1.00  
 14.09  
 Top 24" Storm Drain 33' Lt  
 Top Storm Drain Grate 33' Lt



Robinson St Cont

306.71

26+00	9.66	297.05 ✓	
+50	6.83	299.88 ✓	
+66	7.05		299.66
+66	6.49	300.22 ✓	
27+00	5.55	301.16 ✓	
+50	4.48	302.23 ✓	
28+00	3.81	302.90 ✓	
+46	3.87		302.84

Top Stem QV on Q

Top AQ para

Q para blind t

end of Work by Bb line Indiana St

2.60 312.57 ✓ 1.74 304.97 ✓

3.17 309.40 = 309.78

SW (1) L&T Essex + Park Blvd

Robinson St 10<sup>th</sup> to Park Blvd  
List of Water Meters

51

Meters North		Meters South	
Sta	House Number	Sta	House Number
1+98	1020	1+59	1011
2+60	1030	2+16	1019
3+25	1036	2+23	1025
3+50	1042	2+86	1033
4+17	1058	3+47	1035 Randall Ct
4+52	1060	4+10	1039
4+92	1066	4+49	1057
7+20	1214	4+69	1063
7+61	1220	5+35	1075
8+03	1232	7+38	1215
8+68	1236	7+85	1225
9+15	1244	8+34	1231
9+89	1258	8+96	1239
10+37	1260	9+53	1247
10+57	1264	9+72	1253
11+14	1276	10+43	1263
11+83	1280	10+85	1269
14+37	1410	11+31	1277
14+52	1426	11+73	1281
15+81	1440	13+78	1405
16+10	1504	14+75	1417
16+90	1514	15+03	1441
17+27	1520	16+64	1505
18+30	1529	17+07	3749 Robinson Pl
20+17	1620	18+04	1521
20+83	1624	18+40	1601
23+38	1720	19+93	1607
24+58	1740	20+10	1611
25+26	1750	20+50	1619
25+68	1756	20+93	1625
26+21	1768	21+58	1631
27+03	3752 Park Blvd	22+08	1635
		22+59	1705
		22+97	1715
		23+59	1725
		24+19	1735
		25+91	3749 Park Blvd

ORANGE AVE 12" AC MAIN

55th ST To Spartan Dr

Main Relocation Thru Crawford High School

7.64 376.81 369.20

0+10 4.1 372.7 363.0

+50 4.8 372.0 363.1

0+92 45° Bend 7.3 369.5 363.3

0+97 45° Bend 7.3 369.5 363.4

1+12 7.0 369.8 363.4

+50 6.3 370.5 365.5

2+00 5.0 371.8 368.2

896

+50 TP 384.12 1.68 375.16 370.8

+75 7.8 376.3 372.2

3+00 7.3 376.8 372.6

+50 7.1 377.0 373.4

4+00 6.7 377.4 374.0

+50 5.6 378.5 374.6

5+00 2.4 381.7 375.3

+20 9.84 393.69 0.27 383.85 375.6

12.27 405.54 0.42 393.27

4.83 409.84 0.53 405.01

+46 45° Bend 6.1 403.7 393.6

+52 45° Bend 4.8 405.0 395.1

West  
Williams X  
Paulson †10/5/56 Partly Cloudy  
See page 39

TBM Top of 55th &amp; Orange

376.8

9<sup>2</sup> Begin Work 4.7 372.18<sup>2</sup> 5.3 371.5C6<sup>2</sup> 7.2 369.6C6<sup>1</sup> 7.1 369.7C6<sup>2</sup> 8.2 369.6C5<sup>2</sup> 6.0 370.8C3<sup>6</sup> 4.7 372.1C4<sup>4</sup> 1.5 375.3C4<sup>1</sup> 7.8 376.3C4<sup>2</sup> 7.3 376.8C3<sup>6</sup> 7.1 377.0C3<sup>2</sup> 6.7 377.4C3<sup>2</sup> 6.0 378.1C6<sup>4</sup> 4.3 379.8C8<sup>3</sup> 0.5 383.62C10<sup>1</sup> 5.8 404.0C9<sup>2</sup> 4.3 405.5

ORANGE AVE. 12" A.C. MAIN  
CONT.

409.84

409.8

10/5/56

6+00 5.7 404.1 397.6  
+15 8.8 401.0 397.5  
+34 9.4 400.4 389.8

C6 <sup>5</sup>  
C3 <sup>5</sup>  
C10 <sup>4</sup> +

4.9 404.9  
7.5 402.7  
8.2 401.6

0.23 397.13 12.94 396.90  
11.73 385.40 = 385.39

TBM end of 06 Ely Side Spartan Dr

10/29/56 SHOREY  
KEMP  
O'BRIEN

BOTTOM OF PIPE AS INSTALLED

TP 0.52 405.52 405.0  
5452. 45° BEND 9.8 395.7  
5488 10.0 395.5  
6+00 10.5 395.0  
OK TP 1.35 404.17 = 404.1

Ⓟ HUB 5452. 45° BEND (SEE Pg. 52)

6+00 Ⓟ HUB

NOTE: 6+00 TO 6+34 HAS BEEN BACKFILLED

BOLIVAR ST

Flintridge to Rauhac Ave

stks for 6" AC

West  
Williams +  
Paulson +

54

10/9/52 Sunny

	218.57	4505	Chisel n	Allegheny + Rec 100' North
	-6.12			
1.95	214.42	212.47		
0.44	202.01	1282	201.60	
3.80	197.16	8.68	193.36	

0+15'	8.89	188.27		Top of pipe 0+15' ±	Top of Tee
0+50	6.2	191.0	187.9	C3	1
+75	6.6	190.6	187.1	C3	5
1+00	7.0	190.2	186.5	C3	2
+50	8.7	188.5	184.9	C3	6
2+00	11.0	186.2	182.9	C3	3
	0.87	186.35	11.68	185.48	186.5
+50	2.3	184.1	180.5	C3	6
3+00	4.7	181.7	178.3	C3	4
+50	7.4	179.0	176.0	C3	0
+73' FH Tee	8.2	178.2	175.3	C2	9
4+00	8.6	177.8	174.7	C3	1
+50	9.7	176.7	173.5	C3	2
5+00	10.9	175.5	172.3	C3	2
+50	12.1	174.3	171.1	C3	2
6+00	13.3	173.1	169.8	C3	3

190.5  
6.7

186.5  
10.7

182.0  
4.4

178.1  
8.3

175.9  
10.5

173.5  
12.9

BOLIVAR ST. CONT

55

10/9/56

186.75  
 6+50 14.4 172.0 168.6

C3 <sup>4</sup>

+95 15.1 171.3 167.4

C3 <sup>9</sup>

end of work

11.63 197.27 0.71 185.64

11.55 204.93 3.89 193.38

10.15 214.85 0.23 204.70

2.40 212.45  
 + 6.12

218.57 = 218.59

SCHUYLER St.

West part St. to Rancho Dr.

Stks for 6" AC

		227.34	
		-6.12	
1.46	222.68	221.22	
4.90	220.78	8.80	213.98
1.25	221.63	0.40	220.38
11.06	222.71	9.98	211.65
0+00	FH Tee	1.6	221.1
0+00	Top of Ob	0.93	221.78
0+00	(3) R FH	0.6	222.1
+50		4.0	218.7 215.3
1+00		7.1	215.6 212.5
+50		9.6	213.1 209.8
2+00		10.3	212.4 209.0
+25		10.6	212.1 208.4
+50		10.2	212.5 209.1
3+00		9.0	213.7 210.4
+50		7.9	214.8 211.6
+62		7.6	215.1 212.0
3+95		2.4	215.3
	9.37	224.27	7.81 214.90
	3.07	218.50	8.89 215.43
	6.28	223.82	0.96 217.54
			2.61 221.21
			+ 6.12
			227.33 =

West  
Williams &  
Paulson's

56.

10/9/52 Sunny

Sta M 3+09

USGS Obis II Top Air Valve Bonita Line Res Dr

C. to exist Ely pi-op Line West part

00' to Flange

C3 4

C3 1

C3 3

C3 4

C3 1

C3 4

C3 3

C3 2

C3 1

C3

C. TO EXISTING end of work

215.7  
7.0  
212.4  
10.3

9.0

227.34

ALLEGHANY ST

Westport to Rancho Dr

Stks for 8" AC

		218.59	
		-6.12	
9.18	221.65	212.47	
8.90	230.09	0.46	221.19
3.05	228.40	4.74	225.35
0+53 FH Tee		1.8	226.6 223.0
+53		1.40	227.00
+53 @ R FH		1.5	226.9
1+00		4.6	223.8 220.5
+50		6.9	221.5 217.7
2+00		8.2	220.2 216.7
+50		9.3	219.1 215.7
3+00		10.3	218.1 214.7
+50		11.1	217.3 213.7
+62		11.2	217.2 213.4
+75		11.5	216.9 213.4
4+00		11.2	217.2 213.4
+50		10.1	218.3 214.9
5+00		8.5	219.9 216.4
+50		6.9	221.5 218.0

West  
Williams x  
Paulson †

57

10/9/56 WARM

200' NW of Res & Allegheny St

USGS Obs II on Air Valve Chamber Barite line

0+00 Fly prop line Westport

C TO EXISTING

Top of Ob

F0<sup>3</sup> TO FLANGE

C3 3

C3 8

C3 5

C3 4

C3 4

C3 6

C3 8

C3 5

C3 8

C3 4

C3 5

C3 5

C3 5



ALLEGHANY ST CONT.

10/9/56

	228.40				
6+00		5.4	223.0	219.6	C3 <sup>4</sup>
+394		4.8	223.6	219.8	C3 <sup>8</sup>
	3.66	228.88	3.18	225.72	
+394		8.26	220.62		
	1.16	216.81	13.23	215.65	
		4.33	212.48	=	212.47

Top of existing Tee

55<sup>th</sup> ST.  
 ORANGE ST. TO 715' SO.  
 (5) STR'S FOR 8" A.C. MAIN

BM 5.22 368.99 363.77

0+35 (55' RT. 12" X 6" F.H. TEE) 3.9 365.1

(5) 3.7 365.3

0+35 (12" X 8" TEE) 2.9 366.1 362.0

0+62 2.1 366.9 362.1

1+00 1.1 367.9 363.0

1+50 TP 11.29 380.00 0.28 368.71 364.3

2+00 10.5 369.5 365.6

2+50 9.3 370.7 366.8

3+00 7.5 372.5 368.1

3+14 (8" X 4" TEE) 6.7 373.3 368.5

3+50 4.8 375.2 369.4

3+87 3.2 376.8 370.4

4+00 2.8 377.2 370.4

4+50 1.8 378.2 370.4

5+00 1.8 378.2 370.5

5+25 TP 0.37 378.32 2.05 377.95 370.6

5+50 0.9 377.4 370.1

6+00 2.6 375.7 369.1

10/18/56  
 SHOREY  
 KEMP  
 O'BRIEN  
 L&T & SA<sup>th</sup> f ORANGE

59

CUT TO EXIST. MAIN

FD<sup>5</sup> TO FLANGE

CA<sup>1</sup> ± CUT TO EXIST. MAIN

CA<sup>8</sup>

CA<sup>2</sup>

CA<sup>4</sup>

CA<sup>3</sup>

CA<sup>3</sup>

CA<sup>4</sup>

CA<sup>8</sup>

CA<sup>8</sup>

CA<sup>4</sup>

CA<sup>8</sup>

CA<sup>8</sup>

CA<sup>7</sup>

CA<sup>4</sup>

CA<sup>3</sup>

CA<sup>6</sup>

55<sup>th</sup> ST.

(CONT'D)

378.32

6+25 3.7 374.6 368.6

6+50 5.0 373.3 367.6

7+00 7.9 370.4 365.0

7+50 10.5 367.8 363.5

7+73 F.H. TREE (END WORK) 11.1 367.2 362.7

③ 11.0 367.3 366.5

CK. TBM 9.04 369.28 = 369.29

10/18/56  
SHOREY  
KEMP  
O'BRIEN

60

C6<sup>0</sup>C5<sup>2</sup>C5<sup>4</sup>C4<sup>3</sup>C4<sup>5</sup>C4<sup>6</sup> C0<sup>8</sup>

Top F.H. 7+66 @ LT. (F.B. 867-73)

## WATER METERS

378.32

7+58 W. 9.7 368.6 366.1

C2<sup>5</sup>

## WATER CHAMBER AT CRAWFORD HIGH SCHOOL

BM 13.20 376.97 363.77

3+14 3.10 373.87 372.6

2.79 374.18 372.6

CK. BM 13.20 363.77 = 363.77

## 2" WATER SERVICE

TP 5.40 373.20 367.80

WM. 7+73 6.05 367.15 365.25

CK. TP 5.40 367.80 = 367.80

C1<sup>3</sup>C1<sup>6</sup>C1<sup>90</sup>

③ 7+50

MENTONE ST.

6" C.I. STUB.

0+00 = S/L CAMULOUS

TBM 1.62 23.62 22.00

2+18 HUB 5 BK. PROP.

2+16<sup>5</sup> EXIST. B.O. ON 6" C.I. MAIN 10.4 13.2 9.0 CA<sup>3</sup>

TP 2.93 16.20 10.35 13.27 CA<sup>3</sup>

2+50 6.4 9.8 5.6 CA<sup>3</sup>

2+89<sup>37</sup> END PART 9.1 7.1 2.2 CA<sup>2</sup>

TP 10.10 23.20 3.10 13.10

CK TBM 1.20 22.00 = 22.00

WATER METERS  
ALLEY BLK.'S 119 & 120  
MISSION BEACH

BM	3.00	9.98	6.98		
TP	0.86	5.87	4.97	5.01	
0+58N.			4.0	1.9	1.8
1+24N.			5.5	0.4	-1.0
1+71S.			6.4	-0.5	-1.5
2+57N.			7.0	-1.1	-2.2
2+83S.			6.8	-0.9	-2.2
3+12N.			7.0	-1.1	-2.4
3+36S.			7.4	-1.5	-2.5
3+38N.			6.9	-1.0	-2.7
3+40S.			7.5	-1.6	-2.6
3+99S.			7.6	-1.7	-2.7
4+02S.			7.6	-1.7	-2.8
SET TBM		0.86	5.01		

ALLEY BLK.'S 123 & 124

TBM	5.50	10.51	5.01		
TP	0.91	6.06	5.36	5.15	
0+44N.			2.2	3.9	3.1
0+53N.			2.8	3.3	2.6
0+96N.			4.8	1.3	0.1
1+08S.			5.8	0.3	-0.6
1+13S.			5.9	0.2	-0.8
2+34N.			7.3	-1.2	-2.6
2+41N.			7.3	-1.2	-2.5
2+67N.			7.3	-1.2	-2.6
3+02S. TBM	0.91	5.15	7.8	-1.7	-2.9

11/23/56

SHOREY  
KEMP  
SMITH  
O'BRIEN

9.8

9.5

62

B.P. SEAWALL & SAN LUIS OBISPO

C<sup>0</sup>

C<sup>1</sup>

C<sup>2</sup>

C<sup>1</sup>

C<sup>3</sup>

C<sup>3</sup>

C<sup>0</sup>

C<sup>2</sup>

C<sup>0</sup>

C<sup>0</sup>

C<sup>1</sup>

N.RIM SEW. M.H. 0+10

C<sup>0</sup>

C<sup>0</sup>

C<sup>2</sup>

C<sup>0</sup>

C<sup>1</sup>

C<sup>3</sup>

(over)

WATER METERS  
ALLEY BLK'S 127 & 128  
MISSION BEACH

10/23/56  
SHOREY  
KEMP  
SMITH  
O'BRIEN

63

TBM	4.81	9.96	5.15		
TP	0.90	5.59	5.27	4.69	
0+93 N (2 METERS)		5.1	0.5	-0.5	C1 <sup>0</sup>
1+76 N.		6.1	-0.5	-1.3	C0 <sup>8</sup>
1+97 N.		6.3	-0.7	-1.8	C1 <sup>L</sup>
2+38 N.		7.0	-1.4	-2.5	C1 <sup>L</sup>
2+72 N.		7.4	-1.8	-2.8	C1 <sup>0</sup>
3+01 S.		7.6	-2.0	-2.8	C0 <sup>8</sup>
SET TBM		0.90	4.69		

N. RIM SEW. M.H. 0410

ALLEY BLK'S 131 & 132

TBM	4.79	9.48	4.69		
TP	1.58	5.85	5.21	4.27	
0+50 N.		3.6	2.3	1.7	C0 <sup>6</sup>
0+66 S.		4.5	1.4	0.7	C0 <sup>7</sup>
1+51 N.		5.4	0.5	-0.3	C0 <sup>8</sup>
1+77 S.		6.3	-0.4	-1.4	C1 <sup>0</sup>
SET TBM		1.58	4.27		

N. RIM SEW. M.H. 0410

(OVER)

WATER METERS  
ALLEY BLK'S 135 & 136  
MISSION BEACH

TBM	5.23	9.50	4.27			
TP	2.27	6.93	4.84	4.66		
0+45 S.			4.0	2.9	2.0	CO <sup>2</sup>
1+53 N.			6.4	0.5	-0.3	CO <sup>8</sup>
1+55 S.			6.1	0.8	-0.2	CO <sup>2</sup>
SET TBM		2.27	4.66			

N. RIM SEW. M.H. 0+10

ALLEY BLK'S 139 & 140

TBM	4.94	9.60	4.66			
TP	2.73	6.88	5.45	4.15		
1+90 S.			7.1	-0.2	-0.8	CO <sup>6</sup>
1+96 N.			7.1	-0.2	-0.8	CO <sup>6</sup>
2+18 S.			7.5	-0.6	-1.1	CO <sup>5</sup>
SET TBM		2.73	4.15			

N. RIM SEW. M.H. 0+10

ALLEY BLK'S 143 & 144

TBM	5.02	9.17	4.15			
TP	2.62	6.89	4.90	4.27		
1+55 S.			5.9	1.0	0.0	CO <sup>2</sup>
1+77 N.			7.3	-0.4	-0.9	CO <sup>5</sup>
2+08 S.			7.5	-0.6	-1.6	CO <sup>2</sup>
SET TBM		2.62	4.27			

N. RIM SEW. M.H. 0+10

(OVER)

10/23/56  
SHOREY  
CAMP  
SMITH  
O'BRIEN

64

WATER METERS  
 ALLEY BLK. 148  
 MISSION BEACH

TBM	5.36	9.63	4.27		
TP	1.36	6.25	4.74	4.89	
0+41N.			2.8	3.5	2.6
0+60S.			4.2	2.1	1.3
TP	4.92	6.91	4.26	1.99	
TP	9.99		7.15	-0.24	
CK. BM		2.99	7.00	=6.98	

10/23/56  
 SHOREY  
 KEMP  
 SMITH  
 O'BRIEN

B.P. IN SEAWALL & SAN LUIS OBISPO (SEE PG. 62)



TROJAN AVE  
VALE WAY TO SHARRON PL.  
④ STK'S E' GRD. 8" A.C. MAIN

10/25/56

66

SHOREY  
KEMP  
SMITH  
O'BRIEN

BEGIN WORK - CONN. 0+90 TO EXIST. 8 C.I.	379.0	+ CUT TO EXIST. MAIN
1+00	378.5	
1+25	377.2	
1+50	376.6	
2+00	375.4	
2+45 8" X 6" TEE	374.2	
2+50	374.2	
3+00 B.C.	372.9	
3+23 8" X 6" F.H. TEE	372.3	
3+50	371.7	
3+62 <sup>63</sup> - P.R.C.	371.4	
3+75	371.1	
4+00	370.4	
4+25	369.5	
4+37 <sup>70</sup> E.C.	369.1	
4+50	368.7	
5+00	366.9	
5+50	365.0	

6+00

363.4

6+50

361.6

6+88

360.2

7+00

360.0

7+50

359.0

7+75

358.4

END WORK - CONN.

8+00 TO EXIST. 8" X 6" TEE

WATER METERS  
52<sup>ND</sup> ST.; POLK TO ORANGE

TP	12.84	330.97	318.13	
0+24 W.			9.8 321.2	319.2
0+86 W.			5.6 325.4	324.0
1+30 W.			1.8 329.2	327.4
TP	12.41	343.25	0.13 330.84	
1+80 W.			9.9 333.4	331.3
2+41 W.			5.3 338.0	336.1
2+70 W.			3.0 340.3	338.4
TP	12.67	355.84	0.08 343.17	
3+24 W.			10.6 345.2	342.7
3+65 W.			7.7 348.1	345.8
4+05 W.			5.4 350.4	348.9
TP	13.08	368.79	0.13 355.71	
4+65 W.			12.1 356.7	355.5
TP	12.41	380.35	0.85 367.94	
5+30 W.			10.6 369.8	367.7
CK. BM			2.80 377.55	377.51

10/25/56  
SHOREY  
KEMP  
O'BRIEN  
N.W. COR. CURB.

C2<sup>0</sup>

C1<sup>4</sup>

C1<sup>8</sup>

C2<sup>1</sup>

C1<sup>2</sup>

C1<sup>2</sup>

C2<sup>5</sup>

C2<sup>3</sup>

C1<sup>5</sup>

C1<sup>3</sup>

C2<sup>1</sup>

S.W. B.P. ORANGE & 52<sup>ND</sup>

HERBERT ST.  
 CYPRESS ST. TO HERBERT PLACE  
 & PROFILE PROPOSED WATER  
 MAIN

2+39<sup>80</sup> = N/L HERBERT PL.

2+22<sup>30</sup> = 0+40 HERBERT PL.

2+14<sup>80</sup> = S/L HERBERT PLACE

0+60 = N/L CYPRESS ST.

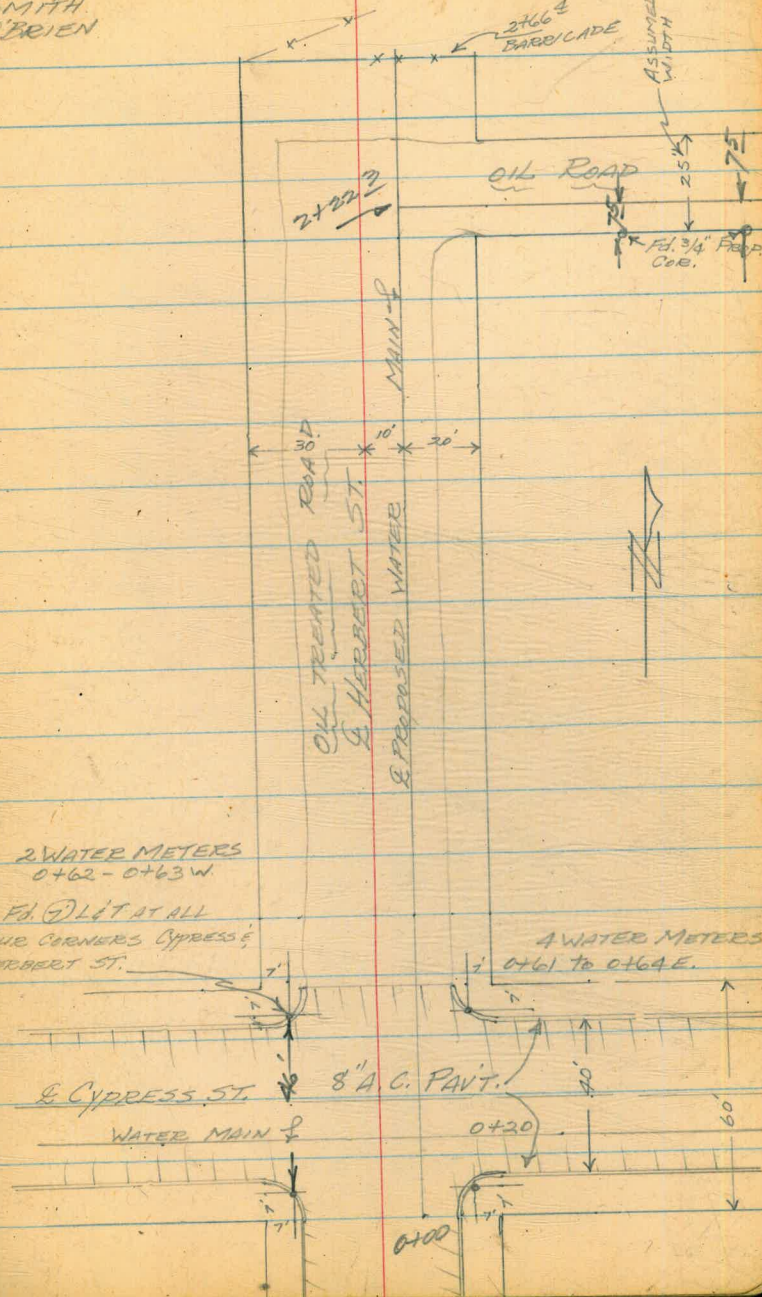
0+00 = S/L CYPRESS ST.

10/30/56  
 SHOREY  
 KEMP  
 SMITH  
 O'BRIEN

69

2 WATER METERS  
 0+62 - 0+63 W

FD @ LT AT ALL  
 FOUR CORNERS CYPRESS &  
 HERBERT ST.



4 WATER METERS

0+61 to 0+64 E.

& CYPRESS ST.

WATER MAIN

8" A.C. PAVT.

0+20

0+00

40'

60'

HERBERT ST.  
(CONT'D)

BM	6.72	297.21	290.49
0+00		7.4	289.81
+11		7.6	289.61
+31		7.2	290.0
+50		7.6	289.6
1+00		5.0	292.21
+50		4.2	293.0
2+00		4.3	292.9
2+22 <sup>30</sup>		4.7	292.5
+50		5.5	291.7
2+66 <sup>4</sup>		6.9	290.3
TP	4.92	297.40	4.73 292.48
CK. BM		6.91	290.49 = 290.49

10/30/50  
SHOREY  
KEMP  
SMITH  
O'BRIEN

S.E. B.P. CYPRESS & HERBERT ST.

S/L CYPRESS

S/L CURB LINE

& CYPRESS

N/L CURB LINE

INTERSECTION PRELIM. HERBERT ST & PL.

HERBERT PLACE  
HERBERT ST. TO 192' ELY  
& PROFILE PROPOSED  
WATER MAIN

3+39<sup>6</sup> Ely P.L. Alley

3+19<sup>6</sup> Wly P.L. Alley

2+45<sup>2</sup> Sew. MH. 1<sup>6</sup> LT

1+94<sup>5</sup> WOOD BARRICADE 0<sup>8</sup> LT  
1+92<sup>5</sup> WOOD BARRICADE 0<sup>11</sup> E

0+00 = W/L HERBERT ST.

10/30/56

3+39<sup>6</sup>

SHOREY  
KEMPI  
SMITH

CF

3+01 { 2' wide  
A.C. paved  
2+60 Drain 6' RT

3+00 E  
Begin AC PAVT.  
2 1/2" THICK

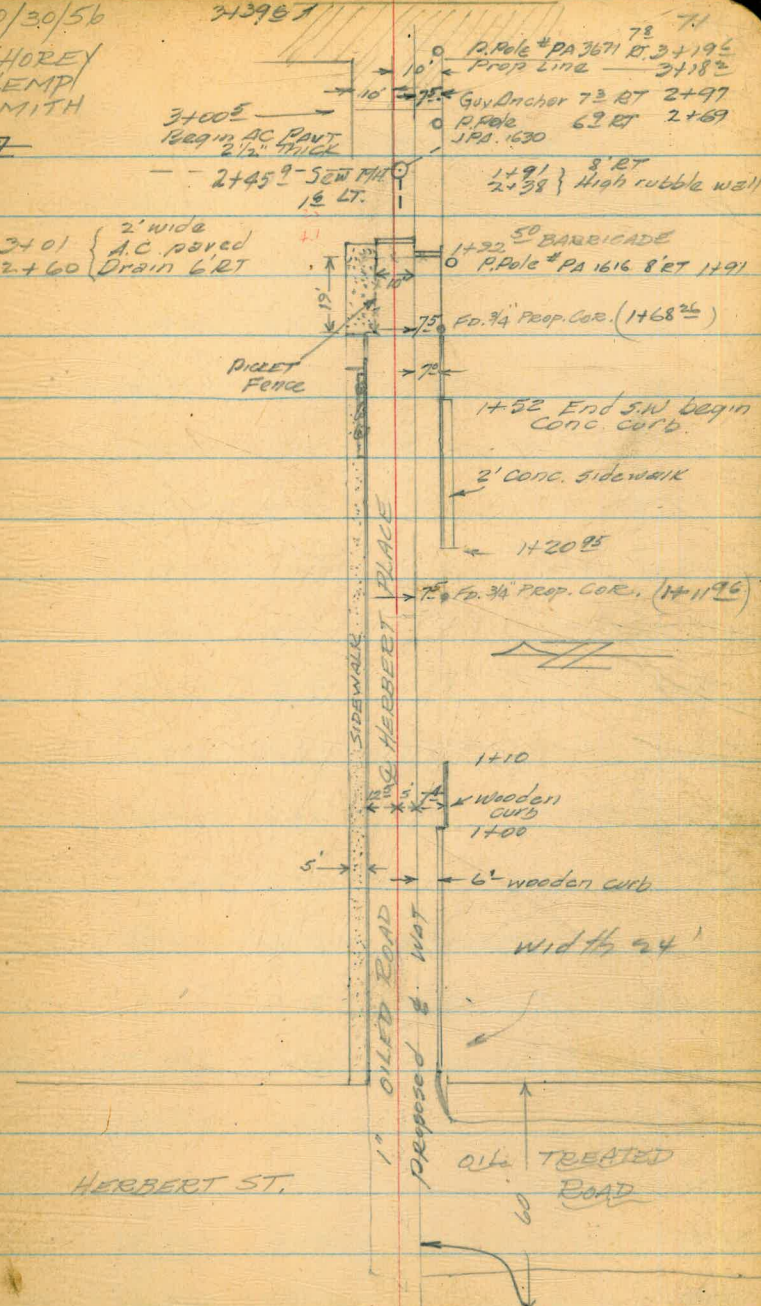
2+45<sup>2</sup> - Sew. MH.  
1<sup>6</sup> LT.

PICKET  
Fence

SIDEWALK  
W/L HERBERT PLACE

1" OILED ROAD  
proposed & wat

HERBERT ST.



NOTE -  
THIS LINE CAN BE  
SHIFTED 2E SLY CHANGE

HERBERT PLACE  
(CONT'D)

BM	6.72	297.21	290.49
TP	4.92	297.40 + 9.9	4.73 292.48
0+00			5.9 291.5
0+50			4.7 292.7
1+00			4.0 293.4
1+50			4.1 293.3
1+92 <sup>50</sup>	BARRICADE		5.8 291.6
CK BM			6.91 290.49 = 290.49
P	0.57	293.87	293.3 <span style="border: 1px solid black; border-radius: 50%; padding: 2px;">+ 1.50 above</span>
1+68			0.8 293.1
1+92			2.3 291.6
2+00			5.4 288.5
2+27			13.0 280.9
2+40			13.4 280.5
2+46	} Run MH	12.52	281.33
		11.20	
		23.94	270.0
	Ground	13.1	280.77
2+50			12.8 281.07
2+70			9.8 284.07
2+95			0.4 293.47
3+00			0.7 293.17
3+29.6	E Alley		0.3 293.57
3+39.6			+ 1.0 293.46
TP	4.92	298.40	2.41 293.67 = 293.67
TP			2.52

10/30/56  
SHOREY  
KEMP  
SMITH  
O'BRIEN  
S.E.B.R. CYPRESS ST. & HERBERT ST.

W/L Cypress

72

11.4

2+00 Alley 242 pg. 74

ALLEY BLK. 242  
 PENNSYLVANIA AVE TO HERBERT PLACE  
 & PROFILE PROPOSED WATER MAIN

10/30/56  
 SHOREY  
 KEMP  
 SMITH

73

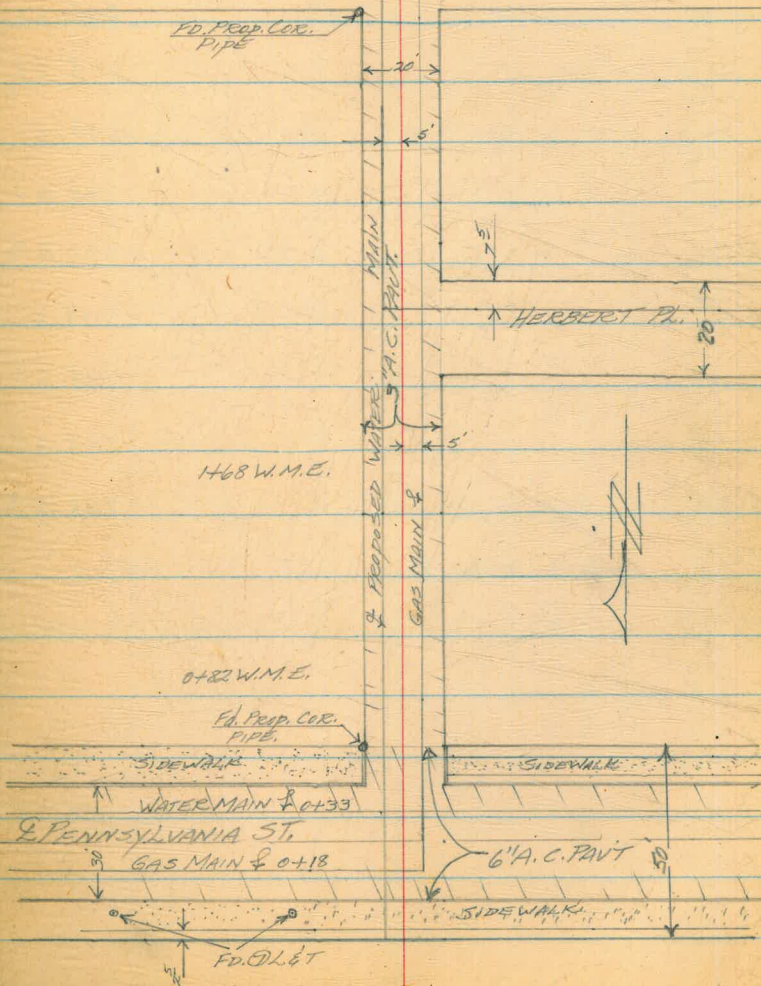
CYPRESS ST.

2+29<sup>75</sup> = S/L HERBERT PL

2+17<sup>25</sup> = P.I. PROPOSED MAIN HERBERT PL.

0+50 = S/L

0+00 = N/L PENNSYLVANIA AVE.





ALLEY BLK. 242  
 PENNSYLVANIA AVE. TO HERBERT PLACE  
 PROFILE PROPOSED WATER MAIN

10/30/56  
 SHOREY  
 KEMP  
 SMITH

74

BM	2.53	303.37	300.84
TP	3.51	298.67	8.21 295.16
0+00		2.8	295.87
0+10 TOP Cb		3.5	295.17
0+10 GUTTER		4.0	294.67
0+25 CROWN		3.6	295.07
0+40 GUTTERLINE		4.0	294.67
0+50		3.8	294.87
1+00		4.2	294.47
1+50		4.6	294.07
2+00		5.0	293.67
2+17 <sup>25</sup>		5.0	293.67
2+24 <sup>75</sup> S/L HERBERT PL.		5.1	293.57
TP	4.58	298.73	4.52 294.15
CK. BM.		9.30	290.43 - 290.49

Reduced by A. Mathison 11-19-56

S.E.F.H. PARK BLVD & CYPRESS ST.

S.E.B.P. CYPRESS & HERBERT ST.

ALLEY BLK'S 218 TO 221  
 NORTH of TOLSON, E. of STRANDWAY  
 @ STR'S & GRD. 6" A.C. MAIN

BM.	1.07	7.46	6.39 7.13
0+05 { BEGIN WORK 2" B.O. ASSY		2.0	5.5 1.6
0+50		1.7	5.8 1.8
1+00		3.0	4.5 0.4
1+50		6.4	1.1 -2.4
1+75 F.H. TEE		7.8	-0.3 -3.7
③		7.4	0.1 0.5
2+00		7.3	0.2 -4.0
2+11 6" Tapp. G.V.		7.6	-0.1 -4.1
2+16 10" x 6" Tapp. Cross		7.6	-0.1 -4.1
2+21 6" Tapp. G.V.		7.7	-0.2 -4.2
2+50		7.7	-0.2 -4.5
3+00		8.3	-0.8 -4.8
3+50		8.7	-1.2 -5.2
3+75		8.8	-1.3 -5.3
4+00		9.9	-2.4 -5.3
4+50		8.4	-0.9 -4.5
4+55 2" B.O. ASSY.		8.3	-0.8 -4.5
OK. BM		1.07	6.39 ± 6.39

11/2/56

SHOREY  
 WEND  
 SMITH  
 O'BRIEN

SPIKE IN P.P. 0+52 2' RT.

S.W. B.P. SEAWALK & SAN RAFAEL PL.

75

C3<sup>2</sup>

C4<sup>0</sup>

C4<sup>1</sup>

C3<sup>5</sup>

C3<sup>4</sup>

C3<sup>8</sup> F0<sup>4</sup>

C4<sup>2</sup>

C4<sup>0</sup> ± CUT TO EXIST. MAIN

C4<sup>0</sup> ± " " " "

C4<sup>0</sup> ± " " " "

C4<sup>3</sup>

C4<sup>0</sup>

C4<sup>0</sup>

C4<sup>0</sup>

C2<sup>2</sup>

C3<sup>6</sup>

C3<sup>2</sup>

ALLEY BLK'S 218 TO 221  
(CONT'D)

WATER METERS

	7.46		
0400 N.	2.0	5.5	4.5
0400 S.	2.2	5.3	4.5
0432 N.	1.4	6.1	4.4
0449 S.	1.5	6.0	4.4
0480 N.	2.1	5.4	3.5
0493 S.	2.8	4.7	3.1
1401 N.	3.3	4.2	2.8
1420 S.	4.2	3.3	1.8
1426 S.	5.1	2.4	1.5
1462 N.	6.9	0.6	-9.9
2455 N.	7.9	-0.4	-1.8
2463 S.	7.6	-0.1	-1.8
2466 S.	7.7	-0.2	-1.9
2781 N.	8.0	-0.5	-1.9
3405 S.	8.3	-0.8	-2.0
3407 N.	8.3	-0.8	-2.1
3421 S.	8.6	-1.1	-2.2
3426 N.	8.4	-0.9	-2.2
3459 S.	8.7	-1.2	-2.5
3482 N.	9.0	-1.5	-2.6
4123 N.	8.7	-1.2	-2.4
4128 S.	8.7	-1.2	-2.4
4131 S.	8.5	-1.0	-2.3
4449 N.	8.7	-1.2	-1.9
4456 N.	8.3	-0.8	-1.9

11/2/56  
SHREY  
KEMP  
SMITH  
O'BRIEN

11/5/56

BM	0.68	7.07	6.39	
0495	1.7	5.4	4.4	C10
0493 S.	2.5	4.6	3.1	C15
1420 S.	3.7	3.4	1.8	C16
1426 S.	4.6	2.5	1.5	C10
CK BM		0.68	6.39	

ALLEY BLKS 214 TO 217  
NORTH OF TANGIER S CT. TO E. STRAND WA

11-8-56

77

KEMP  
SMITH  
O'BRIEN

P.M.	3.61	10.00		6.39					
									PK. IN P.P. 0452 2 <sup>RT</sup> ALLEY BLK 221
Q+05	BEGIN WORK { 2" B.O. ASSEM					1.6			
0+75						2.0			
1+00						0.4			
1+50			8.7	1.3		-2.4			C31
1+75			10.3	-0.3		-4.0			C31
2+00			9.9	0.1		-4.0			C4 <sup>1</sup>
2+12			10.1	-0.1		-4.0			C32
2+17			10.2	-0.2		-4.0			C38
2+22			10.3	-0.3		-4.0			C31
2+50	4.18	3.87	10.31	-0.31		-4.5			C4 <sup>2</sup>
3+00			9.4	-0.5		-4.6			C4 <sup>1</sup>
3+50			9.8	-0.9		-4.8			C32
4+00			4.5	-0.6		-4.8			C4 <sup>3</sup>
4+50			4.8	-0.9		-5.0			C4 <sup>1</sup>
4+70	{ 2" B.O. ASSEM END WORK		4.4	-0.5		-5.0			C4 <sup>5</sup>
P	7.42	10.22	1.08	2.79					
CK BM			3.79	6.43 = 6.39					SAME AS ABOVE

ALLEY BLKS 214 TO 217  
(CONT.)

78

WATER METERS

BM	428	10.47	6.39		
JHON.			5.0	5.5	4.3 C13
0+24S.			4.2	6.3	4.6 C13
0+25N.			3.7	6.8	4.6 C23
0+41S.			4.3	6.2	4.8 C14
0+78S.			6.0	4.5	3.3 C13
1+00S.			6.3	4.2	3.3 C02
TP	0.87	3.87	7.47	3.00	
1+52S				1.4	0.4 C13
1+62N			3.4	0.5	-0.4 C02
2+62N			4.2	-0.3	-1.4 C11
2+74N			3.9	0.0	-1.6 C16
2+74S			4.0	-0.1	-1.6 C15
3+19N			4.5	-0.6	-1.8 C13
3+33S			4.7	-0.8	-1.8 C10
3+35S			4.4	-0.7	-1.8 C11
3+66N			4.5	-0.6	-2.0 C14
3+71S			4.8	-0.9	-2.0 C11
3+75N			4.7	-0.8	-2.0 C13
3+90S			4.8	-0.9	-2.2 C13
4+49S			4.7	-0.8	-1.6 C02
4+51S			4.7	-0.8	-1.6 C02
4+70N			4.5	-0.6	-1.2 C06

$$\begin{array}{r} 428.98 \\ 9.2 \\ \hline 419.7 \end{array}$$

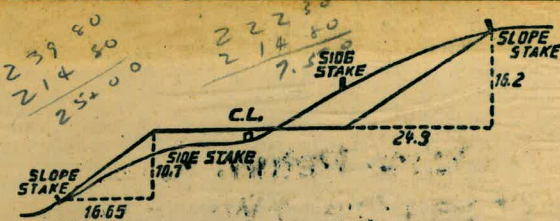
$$\begin{array}{r} 422.6 \\ 6.2 \\ \hline 416.4 \end{array}$$

$$\begin{array}{r} 421.9 \\ 8.6 \\ \hline 413.3 \end{array}$$

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Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center

2.93  
 48  
 39  
 25' south  
 4.18  
 31  
 3.87



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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