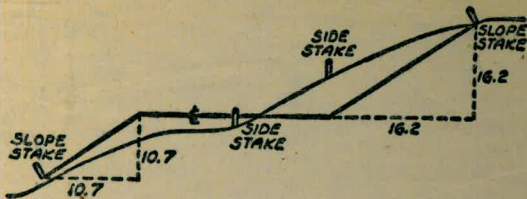


W 933



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00										0
1	1.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance from slope stake to side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the sight adjustment necessary.

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 JAN 20 1965  
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## DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

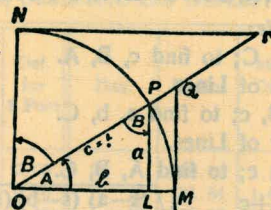


TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \text{cos } B = LP \\ \text{cos } A &= \frac{b}{c} = \frac{b}{1} = b = \text{sin } B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \text{cot } B = MQ \\ \text{cot } A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \text{tan } B = NT \\ \text{sec } A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \text{csc } B = OQ \\ \text{csc } A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \text{sec } B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \\ \text{covers } A &= \frac{OP-LP}{OP} = OP-LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1-\text{Cos } A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1+\text{Cos } A}{2}} \\ \sin 2 A &= 2 \sin A \cos A & \cos 2 A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2 ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2} (A+B)}{\tan \frac{1}{2} (A-B)} \end{aligned}$$

TABLE II — Continued  
TRIGONOMETRIC FORMULÆ (continued)

in any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}(B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III  
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/8
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	3/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	5/8
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	7/8
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	1
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	
7/8	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV — RADII, ORDINATES AND DEFLECTIONS

Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot
0° 10'	34377.5	.036	.145	0.05'	7°	819.02	1.528	6.105	2.10'
20	17188.8	.073	.291	0.10	20'	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25					
1	5729.65	.218	.873	0.30	8	716.78	1.746	6.976	2.40
10	4911.15	.255	1.018	0.35	20	688.16	1.819	7.266	2.50
20	4297.28	.291	1.164	0.40	30	674.69	1.855	7.411	2.55
30	3819.83	.327	1.309	0.45	40	661.74	1.892	7.556	2.60
40	3437.87	.364	1.454	0.50					
50	3125.36	.400	1.600	0.55	9	637.28	1.965	7.846	2.70
					20	614.56	2.037	8.136	2.80
2	2864.93	.436	1.745	0.60	30	603.80	2.074	8.281	2.85
10	2644.58	.473	1.891	0.65	40	593.42	2.110	8.426	2.90
20	2455.70	.509	2.036	0.70					
30	2292.01	.545	2.181	0.75	10	573.69	2.183	8.716	3.00
40	2148.79	.582	2.327	0.80	30	546.44	2.292	9.150	3.15
50	2022.41	.618	2.472	0.85	11	521.67	2.402	9.585	3.30
					30	499.06	2.511	10.02	3.45
3	1910.08	.655	2.618	0.90	12	478.34	2.620	10.45	3.60
10	1809.57	.691	2.763	0.95	30	459.28	2.730	10.89	3.75
20	1719.12	.727	2.908	1.00	13	441.68	2.839	11.32	3.90
30	1637.28	.764	3.054	1.05	30	425.40	2.949	11.75	4.05
40	1562.88	.800	3.199	1.10	14	410.28	3.058	12.18	4.20
50	1494.95	.836	3.345	1.15	30	396.20	3.168	12.62	4.35
4	1432.69	.873	3.490	1.20	15	383.07	3.277	13.05	4.50
10	1375.40	.909	3.635	1.25	30	370.78	3.387	13.49	4.65
20	1322.53	.945	3.718	1.30	16	359.27	3.496	13.92	4.80
30	1273.57	.982	3.926	1.35	30	348.45	3.606	14.35	4.95
40	1228.11	1.018	4.071	1.40	17	338.27	3.716	14.78	5.10
50	1185.78	1.055	4.217	1.45	18	319.62	3.935	15.64	5.40
					19	302.94	4.155	16.51	5.70
5	1146.28	1.091	4.362	1.50	20	287.94	4.374	17.37	6.00
10	1109.33	1.127	4.507	1.55	21	274.37	4.594	18.22	6.30
20	1074.68	1.164	4.653	1.60	22	262.04	4.814	19.08	6.60
30	1042.14	1.200	4.798	1.65	23	250.79	5.035	19.94	6.90
40	1011.51	1.237	4.943	1.70	24	240.49	5.255	20.79	7.20
50	982.64	1.273	5.088	1.75					
					25	231.01	5.476	21.64	7.50
6	955.37	1.309	5.234	1.80	26	222.27	5.697	22.50	7.80
10	929.57	1.346	5.379	1.85	27	214.18	5.918	23.35	8.10
20	905.13	1.382	5.524	1.90	28	206.68	6.139	24.19	8.40
30	881.95	1.418	5.669	1.95	29	199.70	6.360	25.04	8.70
40	859.92	1.455	5.814	2.00	30	193.18	6.583	25.88	9.00

Note. Chord Deflection = 2 times tangent deflection.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

5th St. for Main Group 24 ✓  
 Muir Ave ABBOTT to West of Loma ✓  
 TH PROPOSED P.L. GROUP 201 ✓  
 8 AVE. So. END TO BROOKS ST 2-7 ✓  
 Alice  
 TIES TO 8th AVE So End 5 ✓  
 Preliminary Survey ✓  
 Sorrento Road to Miramar Road 6-17 ✓  
 PROPOSED P.L. (TORREY PINES) FILTER Alice  
 PLANT TO EASTLY CITY LIMITS OF S.D. 18-51 ✓  
 Alice

Muir Ave Abbott to W PT corner  
 STKs For 6" AC Group 2A

West  
 Williams &  
 Varonfoles &  
 Kellhofer

Cloudy

4/23/57

BM NW BP Abbott + Muir

Begin work

5-28	7.22	1.94	
0+20	5.2	2.0	
+50	5.6	1.6	-2.6
1+00	5.4	1.8	-2.2
+50	5.5	1.7	-2.4
2+00	5.6	1.6	-2.5
+50	5.7	1.5	-2.7
3+00	5.8	1.4	-2.9
+50	6.5	0.7	-3.0
4+00	6.3	0.9	-3.0
+50	6.4	0.8	-3.0
5+00	6.2	1.0	-3.0
+45	6.3	0.9	-3.0
	5.28	1.94	= 1.94

CA<sup>2</sup>

CA<sup>0</sup>

CA<sup>1</sup>

CA<sup>1</sup>

CA<sup>2</sup>

CA<sup>3</sup>

CA<sup>3</sup>

CA<sup>3</sup>

CA<sup>3</sup>

CA<sup>0</sup>

CA<sup>3</sup>

Water Meters

+ 5-37	6.17	0.9	
A+14 Met South	5.3	0.9	0.3
A+51 Met South	5.3	0.9	0.2
A+65	5.3	0.9	0.1
	6.17	0.8	= 0.8

(5) 4+50

CA<sup>0</sup>

5157

CA<sup>2</sup>

5161

CA<sup>2</sup>

5165

For ab

5+00

5.13 = 1.04

3+50

4.93 1.24

8<sup>TH</sup> AVE. So. END TO BROOKS ST.  
 PROPOSED P.L. GR. 201

WEST  
 WILLIAMS X  
 VARONFAKIS &  
 KELLHOFER

2

4/26/56 CLOUDY

B.M.	0.81	278.85	278.04
T.P.	3.27	274.17	7.95 270.90
T.P.	0.61	269.84	4.94 269.23
T.B.M.	10.53	275.18	5.19 264.65
T.P.	10.72	278.78	7.12 268.06
T.P.	7.91	285.82	0.87 277.91
CHECK B.M.		7.75	278.07=278.04
B.M.	7.75	285.79	278.04
T.P.	6.27	290.97	1.09 284.70
CHECK B.M.		3.35	287.62=287.63
	1.53	266.18	264.65
			edge of OLD AC
0+00		1.06	265.12
+10		1.57	264.61
+20		2.22	263.96
+30		2.81	263.37
+40		3.79	262.39
+48.49 EC		4.82	261.36
+52		5.33	260.85
+80.88 BC		9.41	256.77

So. EAST @ L + T 7<sup>TH</sup> + PENNSYLVANIA

□ END CURB W. SIDE 8<sup>TH</sup> AVE

So. EAST @ L + T 6<sup>TH</sup> + PENNSYLVANIA

TBM

1.30

7.21 Edge of

121

15.4 Rt Edge of Ob

2.17

4.741 edge of private

2.20

16.41 end of Ob

2.82

4.641 edge of private

3.79

3.941 edge of private

3.51

12.5 Rt edge AC Road

18 ft to south end of private Driveway

## 8th Ave Cont

3

266.18  
 1+00 12.14 254.04

0.67 253.96 12.89 253.29

+25 4.10 249.86

+50 8.26 245.70

+75 11.67 242.29

5.83 246.81 12.98 240.98

2+00 7.66 239.25

1+14<sup>75</sup> EO 9.22 237.59

12.71 259.39 0.13 246.68

9.38 266.79 1.98 257.41

2.14 264.65 =

12.0  
 29.14 edge AC pave

11.18  
 11.0 RT edge AC pave

4.02  
 31.14 edge AC pave

3.38  
 10.5 RT edge AC

8.57  
 71.14 edge AC pave

7.66  
 11.0 RT edge AC

11.75  
 11.5 edge AC pave

11.60  
 11.0 RT edge AC pave

7.98  
 18.14 edge AC pave

7.53  
 12.1 RT edge AC pave

9.58  
 11.21 edge AC pave

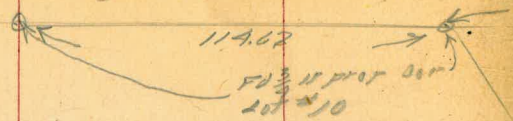
9.01  
 15.1 RT edge AC pave

264.65



8<sup>th</sup> Ave South End to Brooks St

4



Brooks St

Intersection with North Line

2+14 75 EC

$A = 63^{\circ} 59'$   
 $R = 120'$  (revised)  
 $L = 133.87$

0+30.98 BC

71.99

$A = 20^{\circ} 45'$   
 $R = 135'$   
 $L = 48.89$

EC 0+48.89

$A = 20^{\circ} 45'$   
 $R = 135'$   
 $L = 48.89$

(STA 0+00 OF SURVEY = STA. 3+80  
 ON DRAWING) F.B. 871 (See)

0+00

edge of Old AC Pavc 15 per  
 Back Tangent parallel and  $6^{\circ}$  East of Line

23112

42.33

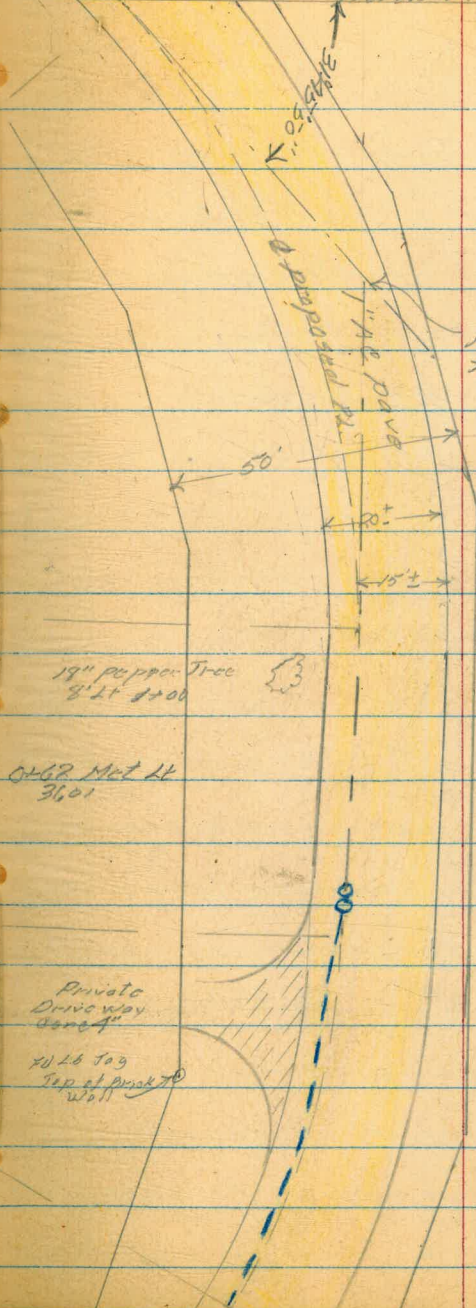
North Line Brooks St

West  
 Williams  
 Varenfoks  
 Kallbaten

Existing water Main

- 0+00 12" L
- 0+20 12" L
- 0+30 12" L
- 0+40 2" L
- 0+62 on on &

Pi  
 Tan = 79.84



19" pepper Tree  
 8' L 1+00

0+62 Met L  
 36.01

Private  
 Driveway  
 40' x 4'

20' x 20' Top  
 of brick  
 wall

0+62 Met R 36.06  
 0+63 50 on L  
 0+62 60 on R

0+15 Met R

0+12 60 10' R to X  
 3+92 Old Survey  
 Pennsylvania to South

Ties to Eight Ave

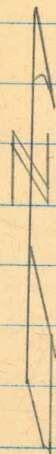
0			
0+20	2' 11"	∅	56
0+30	5' 8"	∅	56
0+40	7' 5"	∅	56
0+48.89	9' 0"	∅	56
0+80.88	13' 0"	∅	56

For Ties to PI of  $\Delta 63^{\circ} 54'$   
curve see page # 4

West  
Williams  
Varon Parks  
Kellhofer

(5)

574156



8+9  
15 Fog Cor-Lot

$\angle 41^{\circ} 24' 48''$

44.98

$\angle 20^{\circ} 25'$   
90'

EC 0+48.89

0+80.88 BC

omitted  
Tangent

Sorrento Road to Miramar Road  
Proposed PL

West  
Williams  
Varonfakis  
Kellhofer

166+00 POT

163+20 POT

161+90 POT

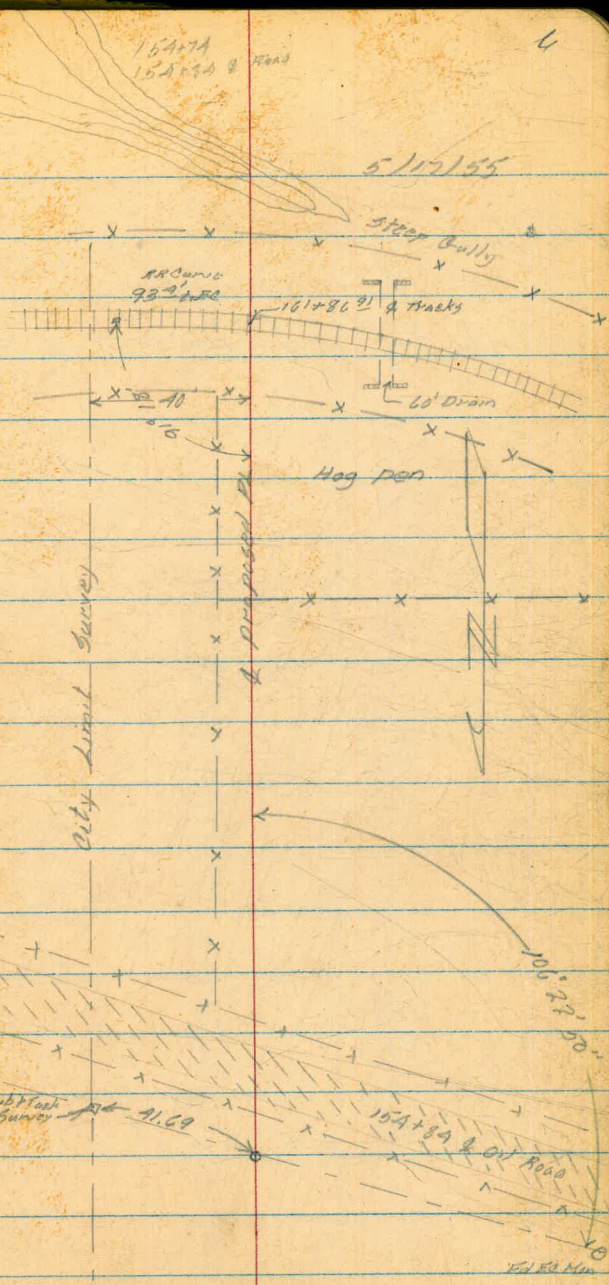
161+86 <sup>71</sup> & RR Tracks

161+00 POT

154+84 Existing Sorrento Oil Road

154+43 <sup>03</sup> POT intersection with & Road Survey

153+93 <sup>02</sup> 50' North of & Road Survey



186+76<sup>9</sup>

Fence Wly Side Miramar Rd

186+35<sup>56</sup>

39.61 LL  
Ed PK Nail of Miramar Road

178+00

POT Nail in Binney

173+00

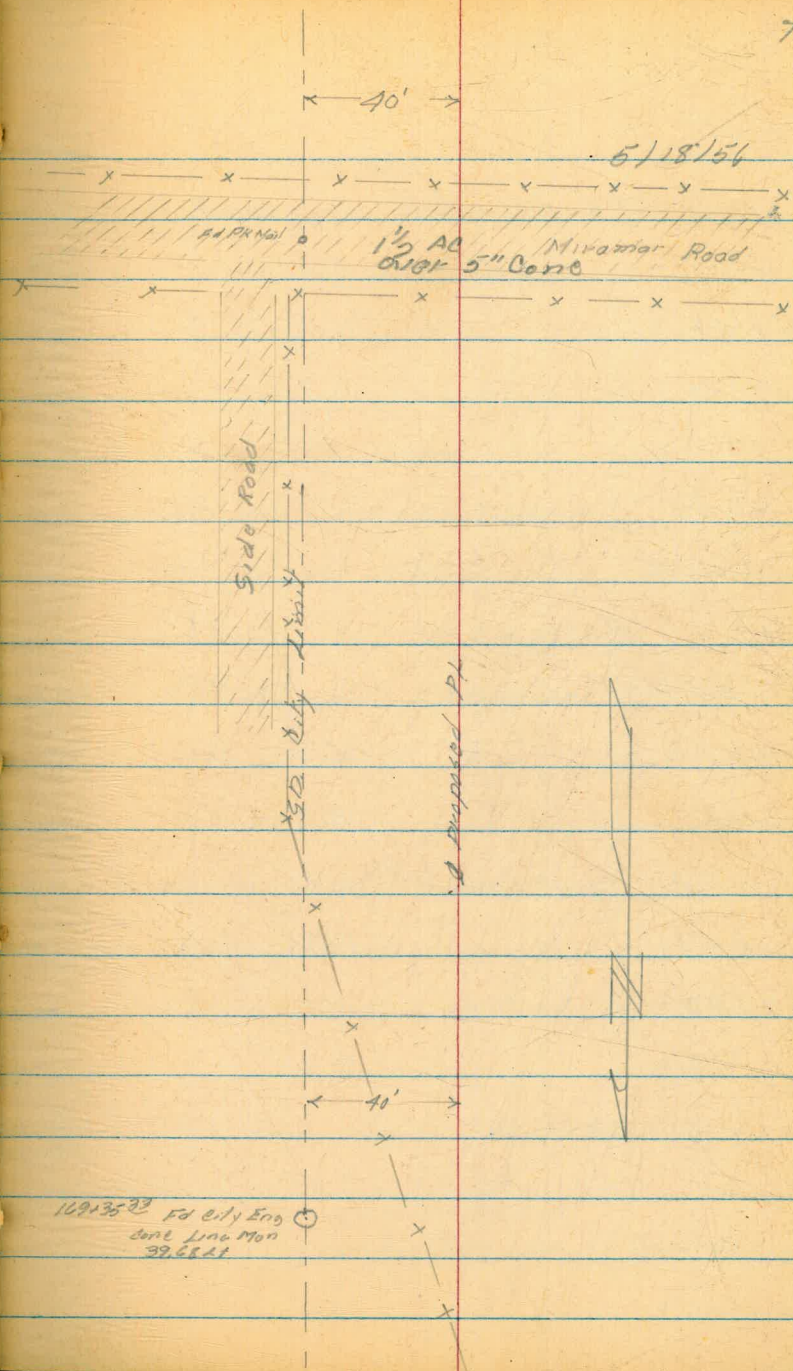
POT Nail in Binney

169+40<sup>42</sup>

POT Binney & Tack

169+35<sup>33</sup>

39.68 LL  
Ed City Eng Lane King Man



Sorrento Rd to Maramar Road  
Profile

3.34	111.25	107.91	
153+93.02		1.4	
154+13.02		5.9	
154+50		4.2	
154+65			
154+65			
154+68			
154+70			
154+70			
154+70		6.8	
+71		10.3	
+74		9.97	
+93		9.42	
+96			
155+00		9.7	
+02			
0.59	98.81	13.03	98.22
+37			
+50		2.5	

Sta 154+89.71  
on R. Hub City Bndry See EB 1424. pg 14  
See also pg. 51

15' Lt to BW Fence

Road Survey

BW Fence Xing

62' Lt to PP 90423

15' Lt to Fence Cor

13<sup>2</sup> Lt to PP # 578795

93<sup>2</sup> Lt to proposed 138KVA Line

Top of Road Cul

Bottom of " "

North Edge 2 1/2 Oil Road Sorrento

South " " " "

Fence Xing 15' Lt to Fence Cor

Buy pole 10' Lt # 456644

Drake Almond

1 1/2 Dia Fruit Tree on a Tree 9' High

99.81

155+56

+81

156+80

+10

+35

+50

+63

+67

+83

+85

+95

157+04

+07

+50

+12

+43

10.39 10.1.27 7.93 90.88

+68

+74

+76

9' RT 1 1/2 Drake Almond Tree

1321 end BW Fence begin Log peel Fence

10' RT 4" Dia Fig Tree

Hog wire Fence Xing

North edge Creek

10' RT end Log peel Fence Begin BW fence

Q Creek Note creek has 6" to 12" of standing water

South edge Creek

Top Creek Bank

15' RT to BW fence

34' RT PP 91107 1.5 KVA

15' RT 48" Dia Cottonwood Tree

27' RT 24" Dia Cottonwood Tree

27' RT 48" Dia " " "

6' RT 18" " " "

101.27

157+77

158+00

+32

+40

+50

+64

+80

159+10

+27

+50

160+00

1212 110.94 2.95 98.82

+50

161+00

+20

+25

+26

12.46

123.46 0.14 110.80

+50

1.7

10

11' LT 18" Dia Cottonwood Tree

14' LT end Row fence Begin Log Pond Fence

19' RT 24" Cottonwood Tree

7' RT 24" Cottonwood Tree

9' LT to fence

fence xing 6' LT to 30" Cottonwood

Begin Junk pile firewood etc

end " " " "

Begin Hog fence fence xing end dog pool fence 9' LT

10' LT to Hog Wire fence

TAM Nail in Log fence

Hog wire fence xing begin RR ROW

Bank  $\frac{3.9}{10' LT}$   $\frac{2.9}{10' RT}$ 

5' LT Tel pole parallel to RR

 $\frac{2.0}{10' LT}$  $\frac{1.9}{10' RT}$

12346

1223	134.55	1.14	122.38
1252	145.91	1.16	133.39
161+76		7.2	
+78		6.9	
+81		5.8	
+84 <sup>2</sup>		5.19	
+89 <sup>2</sup>		4.91	
+92		5.5	
162+02		9.7	
+37		9.6	
+45		5.6	
+60		5.0	

1253 157.63 0.81 145.10

12.75 169.98 0.40 157.23

7.65 175.21 2.42 167.56

+82 10.0

+96 3.4

163+04

+06

162+97

5/21/56

Top RR Fill	$\frac{7.0}{10' Lt}$	$\frac{7.5}{10' Rt}$
----------------	----------------------	----------------------

Bottom of RR Ballast

Top " " "

Top North Rail of RR Track

" South " " " "

Top of RR Ballast

Bott of Local RR Fill

$\frac{8.7}{10' Lt}$	$\frac{9.3}{10' Rt}$
----------------------	----------------------

$\frac{5.4}{10' Lt}$	$\frac{5.5}{10' Rt}$
----------------------	----------------------

Bott of RR Cut	$\frac{5.0}{10' Lt}$	$\frac{5.6}{10' Rt}$
-------------------	----------------------	----------------------

Top RR Cut	$\frac{9.7}{10' Lt}$	$\frac{12.9}{10' Rt}$
------------	----------------------	-----------------------

$\frac{0.8}{10' Lt}$	$\frac{9.0}{10' Rt}$
----------------------	----------------------

BW fence line end RR ROW 9

Deadman 7° Rt

24' Rt PP 90927



	175.211		
163+20		1.1	
+50		5.6	
+67.		9.6	
+73		8.5	
2.81	146.51	11.51	163.70
+85		5.6	
164+00		5.4	
+20		14.3	
+31		2.8	
11.60	177.98	6.13	166.38
+50		3.7	
10.45	188.20	0.23	177.75
12.25	200.17	0.28	187.98
11.95	211.73	0.39	199.78
165+00		5.7	
12.71	223.83	0.61	211.12
13.07	236.46	0.44	223.39
+50		5.9	
12.68	248.52	0.62	235.84
166+00		3.17	on Binney

	+4.4		7.1
	10' RL		10' RL
	0.9		11.1
	10' RL		10' RL
	4.3		12.2
	10' RL		10' RL
	4.1		14.5
	10' RL		10' RL
	+0.3		11.4
	10' RL		10' RL
on Crest Bank	2.2		16.8
	10' RL		10' RL
			17.0 @ creek 13.5 RL
	Bottom of Creek that runs to N.W.		
Top Creek Bank	(10.7 east of creek) Hit	3.6 6' RL	0.0 10' RL
	6.9		1.2
	13' RL		10' RL
	8.8		2.4
	10' RL		10' RL
	8.6		3.6
	10' RL		10' RL
Bw fence 54' RL	5.1		1.0
	10' RL		10' RL

Sorrento Rd Miramar Rd Cont

West  
Williams  
Varonakis  
Kellhofer

13

248.52

5/21/57

12.81 260.21 1.12 247.40

166+50

1.5

$\frac{3.5}{15' RL}$

$\frac{+0.1}{15' RL}$

13.03 272.37 0.87 259.34

12.78 284.24 0.91 271.46

167+00

11.6

fence  
35' RL to BW  $\frac{14.3}{15' RL}$

$\frac{10.5}{15' RL}$

12.69 296.37 0.56 283.68

+50

12.1

$\frac{13.1}{15' RL}$

$\frac{11.1}{15' RL}$

168+00

1.9

BW fence  
17' RL to  $\frac{3.9}{15' RL}$

$\frac{0.0}{15' RL}$

12.52 308.62 0.27 296.10

+50

4.4

fence  
7' RL to BW  $\frac{5.9}{15' RL}$

$\frac{3.3}{15' RL}$

1 12.90 320.94 0.58 308.04

168+92

BW fence Xing

169+00

8.1

fence  
15' RL to BW  $\frac{9.3}{15' RL}$

$\frac{7.7}{15' RL}$

+50

2.4

$\frac{2.3}{15' RL}$  BW fence  $\frac{1.3}{15' RL}$

169+35<sup>33</sup> 12.81 1931 324.41 9.34 311.60

Turn on Cape Man 39.68 LL

170+00

0.9

$\frac{3.4}{19' RL}$  BW fence  $\frac{+0.5}{20' RL}$

12.60 336.95 0.06 324.35

+50

9.5

+77

18' RL Dead man 31' LL PP 90203

336.95  
 171+00 4.7  
 +50 13.07 349.76 0.86 336.69

172+00 9.2  
 +50 5.4

173+00 2.2  
 9.90 359.19 0.47 349.29

+50 9.0

174+00 7.3  
 Spike in Pole

+25 9.75

+50 7.1

175+00 6.9  
 +23 5.8  
 +50 2.4

13.01 371.68 0.52 358.67

176+00 9.2

+50 5.2

177+00 1.2

6.44 377.96 0.16 371.52

177+50 4.5

178+82 P.O.T.

33' LT. P.P. # 90133

178+00 P.O.T. 3.2

2.8  
 29' LT. To fence 3.4  
 20' RT.

5.7  
 31' LT Fence Line

1.4  
 20' RT

10.0  
 31' LT Fence Line

8.7  
 20' RT

9.7  
 29' LT Fence Line

6.5  
 20' RT

35' LT PP 90134

10.7  
 29' LT

4.1  
 20' RT

8.9  
 29' LT To Fence

9.1  
 20' RT

		377.96		
178+50			3.6	
179+00			4.9	
+50			7.0	
180+00			8.1	
+50			10.4	
TP	4.21	373.26	8.91	369.05
181+00			5.2	
+32				
+50			3.7	
182+00			6.5	
+50			10.1	
TP				
183+00	6.11	366.25	13.12	360.14
+50			7.3	
184+00			5.6	
+50			3.9	
+77				
+78				
185+00			3.7	
+50			3.7	
186+00			4.6	

$$\begin{array}{r} 11.7 \\ \hline 29' \text{ LT TO FENCE} \end{array}$$

$$\begin{array}{r} 6.5 \\ \hline 20' \text{ RT.} \end{array}$$

33' LT. P.P.

$$\begin{array}{r} 9.6 \\ \hline 29' \text{ LT TO FENCE} \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline 20' \text{ RT.} \end{array}$$

$$\begin{array}{r} 12.7 \\ \hline 30' \text{ LT.} \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 20' \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline 29' \text{ LT. TO FENCE} \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline 20' \text{ RT.} \end{array}$$

8' RT. DEAD MAN

32' LT. P.P. # 90131

$$\begin{array}{r} 6.8 \\ \hline 30' \text{ LT TO FENCE} \end{array}$$

$$\begin{array}{r} 3.1 \\ \hline 20' \text{ RT.} \end{array}$$

		366.25		
186+06				
TP	458	366.3	4.00	362.25
186+12			4.8	
+13			5.6	
+19			5.35	
+40			5.07	
186+50			5.23	
+55			5.32	
+62			5.5	
+66			4.7	
186+77			4.8	
Set TBM.	2.97	363.62	5.38	361.25
	4.78	365.86	2.54	361.08
	7.81	373.00	0.67	365.19
	8.73	379.62	2.11	370.89
	9.24	383.76	5.16	374.52
	4.79	382.68	5.87	377.89
	4.78	382.35	5.11	377.57
	11.05	386.54	6.86	375.49
	6.07	392.15	0.46	386.08

BARBED WIRE FENCE XING

TOP OF BANK

BOTTOM BANK

BEG. AC. NORTH SIDE MIRAMAR ROAD.

ON AC. PAVT.

SOUTH EDGE AC. MIRAMAR ROAD

BOTTOM BANK

TOP BANK

END WORK  $\frac{1}{2}$  BARBED WIRE FENCE XING

SPIKE IN P.P.# 90130 30" 186+77

392.15

6.15 395.02 329 388.87

361 391.41

6.24 395.79 547 389.55

6.15 398.62 332 392.47

5.38 400.16 384 394.78

5.39 403.31 224 397.92

4.48 403.77 402 399.29

6.58 397.19

- 29.58

367.61

6.12

373.73 = 373.73

4.85 402.04 397.19

249 399.55

USGS?  
= 398.54 TBM Nail in PP # 614364H

Top cone bridge bent above BM

Brass cap in Bridge pier West Side of RR  
North Side of Bridge

Elev. from City Engr. USGS B 132 1933

of RR Bridge

405.64 Spike in Pole 90122 50' West

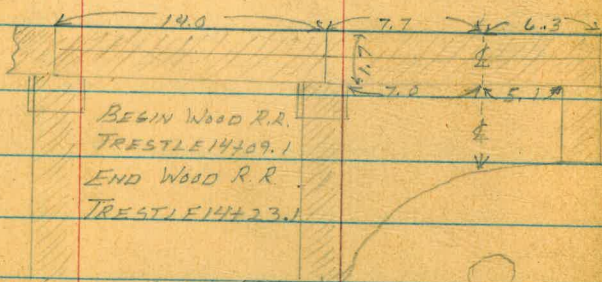
TORREY PINES FILTER PLANT TO EASTLY CITY  
LIMITS OF S.D. PROPOSED P.L.

STA.

88.13  
1416.21  
1504.34

15104 X 88° 47' 20" RT SET R.H. SPIKE 10' AHEAD = 5+20  
ON & PROPOSED ROAD SURVEY

14456 X 91° 49' 30" LT TIE TO RETRACING TORREY PINE LOCKWOOD  
MESA PIPELINE SURVEY. 5+05.06 TO E.C. HUB STA.  
262+27.08 12° 01' 16" RT. TO B.C. STA. 289+53.86



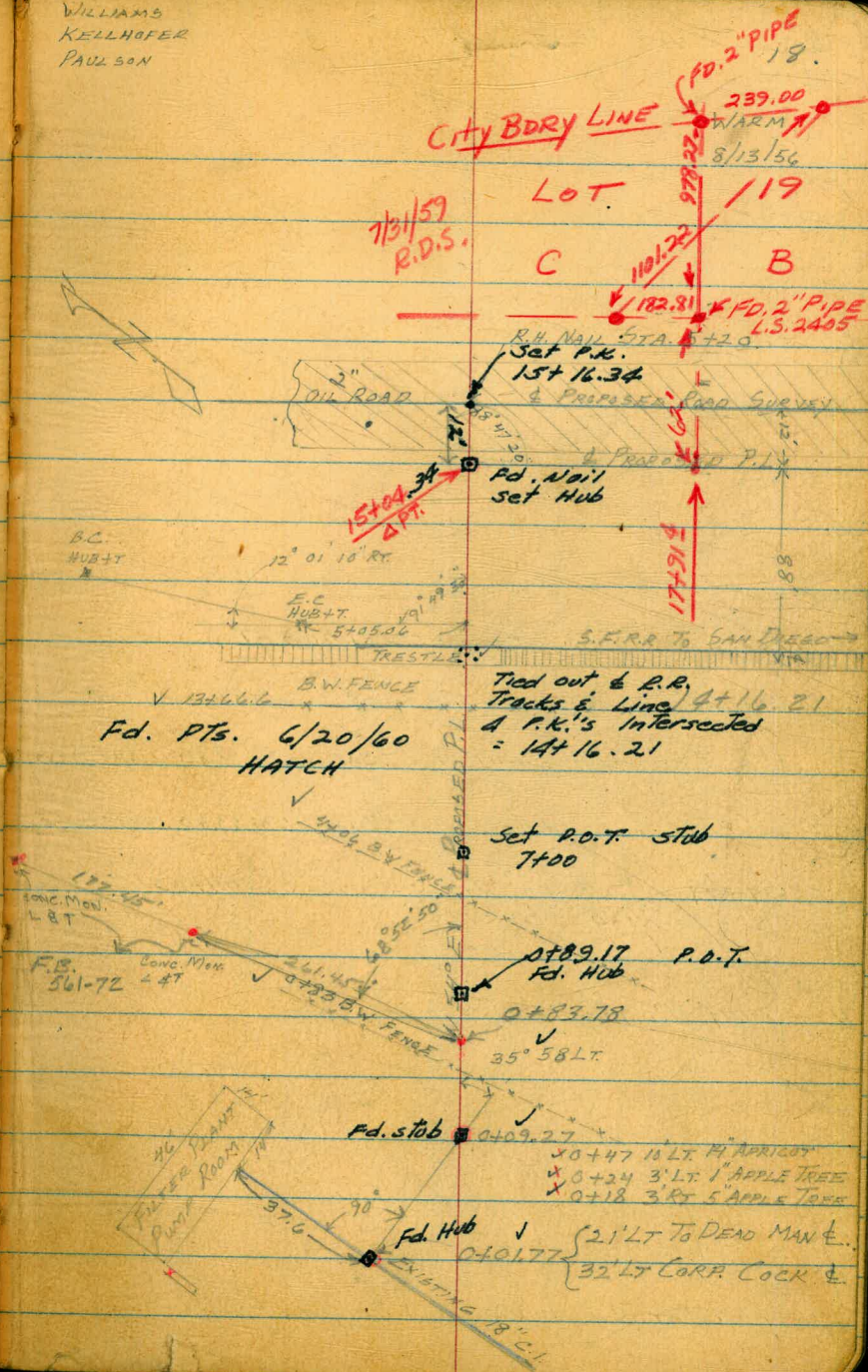
0+84.33 SET GINNEY P.O.T.  
0+83.78 X 68° 52' 58" LT. TIE TO MARK SEE F.B. 561-72  
0+13.79 SET 1X1 HUB+T P.O.T.

0+09.27 X 35° 58' LT. SET 1X1 HUB+T

0+06.77 SET 2+2 HUB+T EXISTING 18" C.I.

R.M. CHIS. X ON HEADWALL 42.16 CITY DATUM

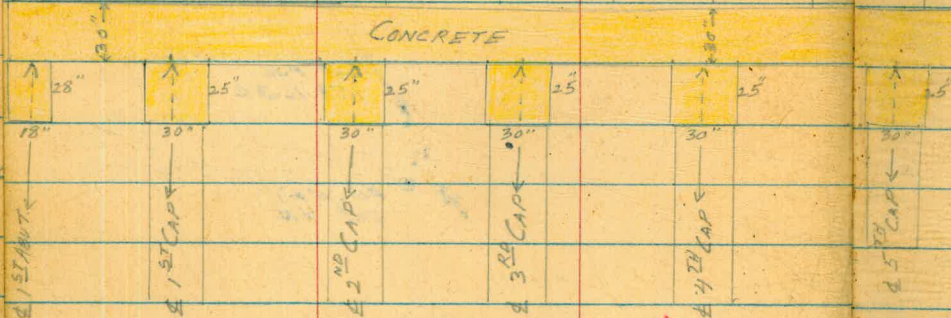
WILLIAMS  
KELLHOFER  
PAULSON



TORREY PINES FILTER PLANT TO EASTLY CITY  
LIMITS OF S.D. PROPOSED P.L.

63+89.71  $\times$   $1^{\circ}18'20''$  LT SET IXI HUB+T

3' HIGH RAILING



CONCRETE

62+16.02  $\times$   $2^{\circ}18'50''$  LT SET IXI HUB+T

62+70.80 BEGIN BRIDGE	62+73.70 2 <sup>ND</sup> CAP	63+59.12 5 <sup>TH</sup> CAP
62+72.70 1 <sup>ST</sup> ABUTMENT	63+02.09 3 <sup>RD</sup> CAP	63+81.83 2 <sup>ND</sup> ABUTMENT
62+45.40 1 <sup>ST</sup> CAP	63+30.69 4 <sup>TH</sup> CAP	63+83.68 END BRIDGE

53+84.54  $\times$   $0^{\circ}27'50''$  RT R.H. SPIKE (12) 44+00 ON  $\&$   
ROAD SURVEY

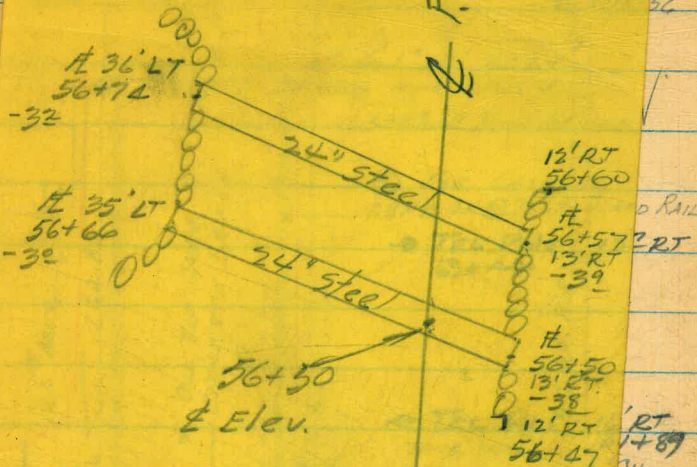
42+84.49 P.O.T. R.H. SPIKE

29+84.28 P.O.T. R.H. SPIKE (12)  $\&$  NAIL STA 20+00  $\times$

WILLIAM  
KELLHOFF  
PAULSON

H. BEATTY

9/19/56



SORRENTO

20+00  $\rightarrow$  P.O.T. 29+84.28  
2" OIL



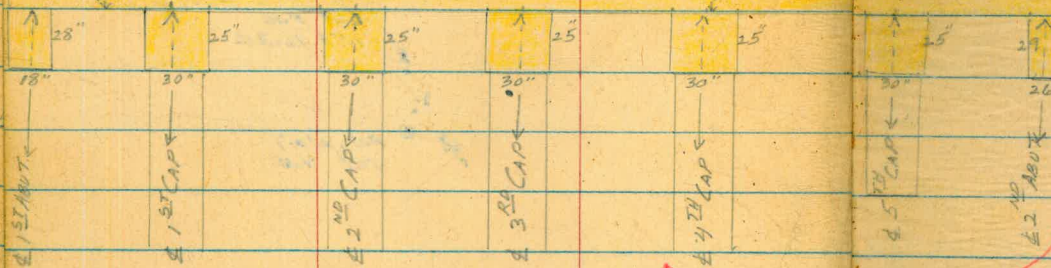
TORREY PINES FILTER PLANT TO EASTLY CITY  
LIMITS OF S.D. PROPOSED P.L.

WILLIAMS  
KELLHOFER  
PAULSON

63+89.71 X 1° 18' 20" LT SET IXI HUB+T

3' HIGH RAILING

CONCRETE



62+16.02 X 2° 18' 50" LT SET IXI HUB+T

62+20.80 BEGIN BRIDGE	62+73.70 2 <sup>ND</sup> CAP	63+59.12 5 <sup>TH</sup> CAP
62+22.70 1 <sup>ST</sup> ABUTMENT	63+02.09 3 <sup>RD</sup> CAP	63+81.83 2 <sup>ND</sup> ABUTMENT
62+45.40 1 <sup>ST</sup> CAP	63+30.69 4 <sup>TH</sup> CAP	63+83.68 END BRIDGE

53+84.54 X 0° 27' 50" RT R.H. SPIKE (12) 44+00 ON 2 ROAD SURVEY

42+8449 P.O.T. R.H. SPIKE

29+84.28 P.O.T. R.H. SPIKE (12) & NAIL STA 20+00 X

OIL ROAD  
& ROAD SURVEY

WARM  
TO 8/14/56

75'  
X 1° 18' 20" RT  
WING WALL ✓  
63+83.68 END BRIDGE ✓

⊕ FOR CHAINING  
1.8 RT. OF ⊕ TO 6X6 GUARD RAIL

⊕ TEL POLE 152 RT  
63+44

⊕ TEL. POLE 16' RT  
21+89  
WING WALL X

X 2° 18' 50" LT 62+16.02

62+20.80 BEGIN BRIDGE  
✓ 62+21 3' LT END GUARD RAIL  
✓ 62+09 10' X 10' GUARD RAIL POST  
✓ 62+10 GUARD RAIL ON E  
X 59+45 2' RT TO 4X4 HWY POST  
X 59+05 2' RT TO 4X4 HWY POST  
X 58+26 3' RT TO 4X4 HWY POST  
X 57+45 5' RT TO 4X4 HWY POST

X 0° 27' 50" RT 53+84.54 X  
2" OIL

45+65 2" WATER LINE

P.O.T. 42+8449  
2" OIL

X 39+53 4.5 RT TO 18" EUC TREE  
X 39+38 4' RT TO 18" EUC TREE  
⊕ 38+27 3' RT TO 18" EUC TREE

88'  
X  
P.O.T. 29+84.28  
2" OIL

PROPOSED ROAD SURVEY

8" OIL ROAD

62+19 2' LT 10' X 10' GUARD RAIL POST  
2" WAT. 28' LT OF 62+16.02

2" WAT. 17.5 LT. 44+00

46+00 2" WAT. 19.5 LT.

33+006

20+00

PROPOSED P.L. CONT.

84+40.41 P.O.T. R.H. SPIKE (10) 1" PIPE + CITY ENG. DISC.  
(35) 2" HUB+T

74+55.16

CITY ENG. DISC.

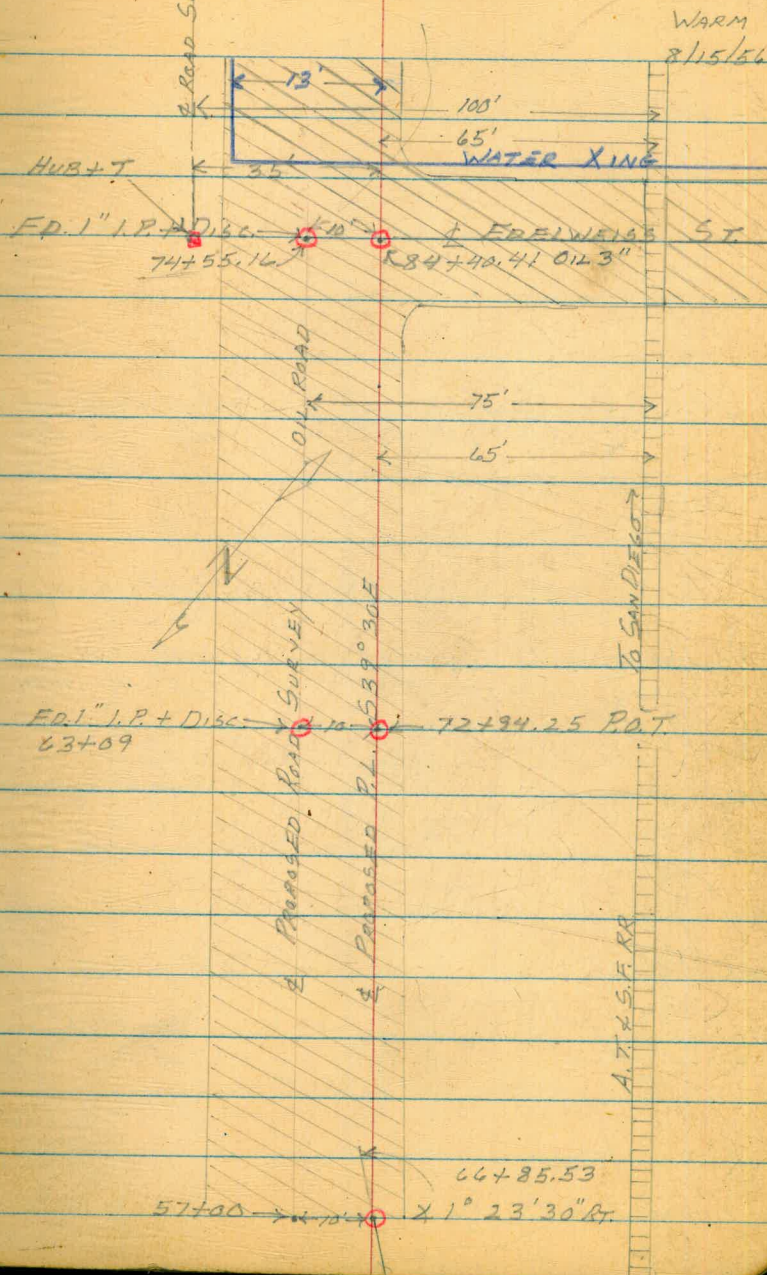
72+94.25 P.O.T. R.H. SPIKE (10) 1" PIPE + CITY ENG. DISC.  
63+09

63+09

66+85.53  $\times 1^{\circ} 23' 30''$  RT. SET R.H. SPIKE (10) NAV. 57+00

WILLIAMS  
KELLGOFER  
PAULSON

20.



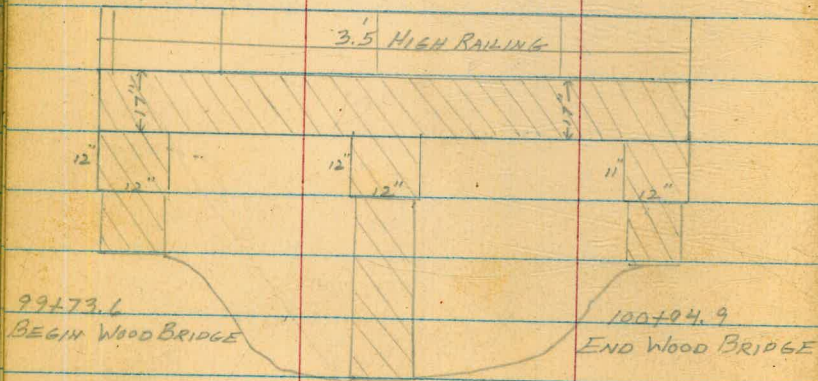
PROPOSED P.L. CONT.

117+57.49 P.O.T. R.H. NAIL (1497) 2" I.P. + DISC L.S. 2001

112+25.41 P.O.T. R.H. NAIL (35) 2x2 HUB + T ROAD SURVEY

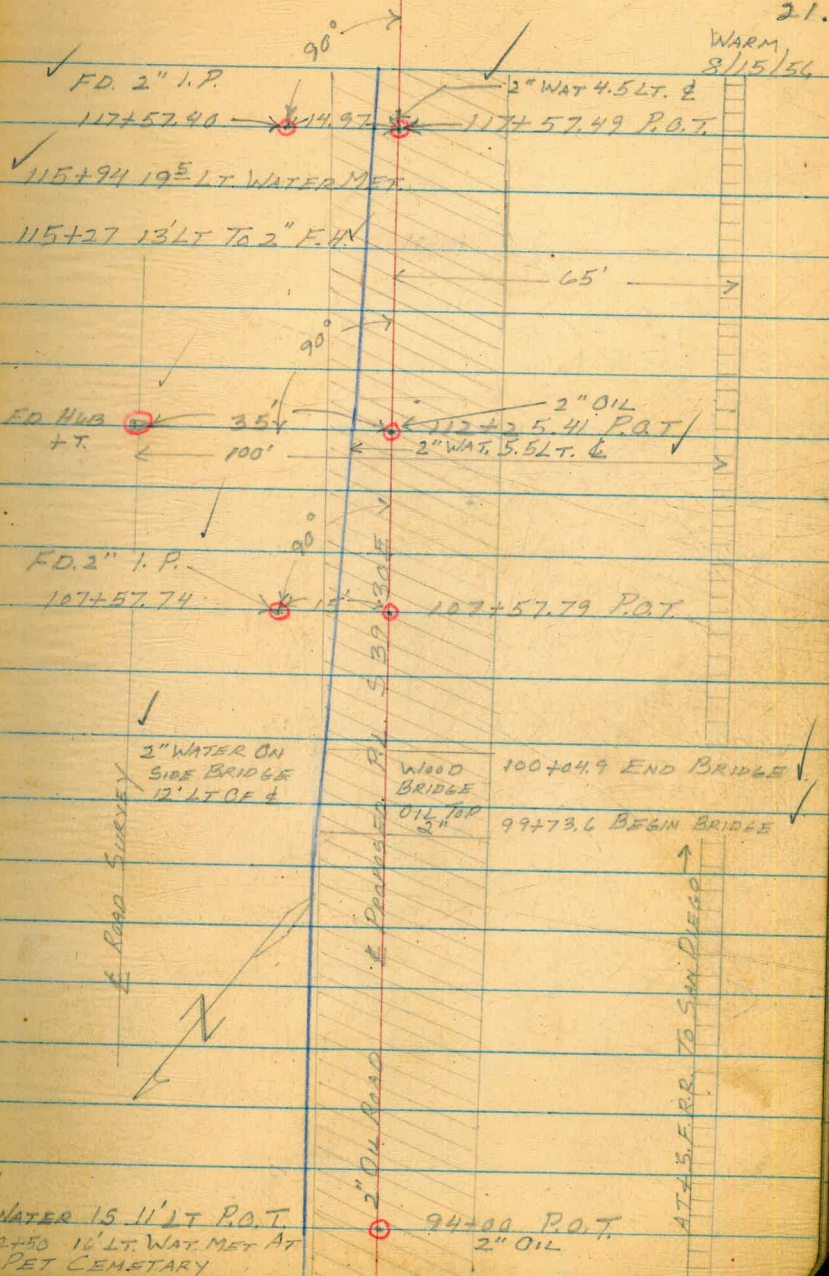
107+57.79 P.O.T. R.H. NAIL (15) 2" I.P. + DISC L.S. 2001

THIS BRIDGE IS SUPPORTED BY TEN 17x8 STRINGERS COVERED BY 3" x 12" FLOORING WITH OIL TOP OF 2"



94+00 P.O.T. R.H. NAIL

SAME PARTY HIC!



WATER IS 11' LT P.O.T.  
92+50 16' LT. WAT. MET AT PET CEMETARY

PROPOSED P.L. CONT

SAME PARTY

22.

WARM

8/16/56

148+46.82 B.C. R.H. SPIKE (35) MON STA 27+67.93  
F.B. 1440-45

140+12.45 GINNEY P.O.T.

133+97.93 P.O.T. R.H. SPIKE

126+07.33 E.C. R.H. SPIKE (35) MON. STA 5+27.09  
F.B. 1440-43

$\Delta 20^{\circ} 08'$

$R = 1535$  DEF. = 1.119797

$L = 539.39$

F.B. 1440-43

120+62.94 B.C. R.H. Nail (35) MON STA 110+84.66

NOTE: COMPARING CHAINING FROM EDELWEISS  
TO THIS B.C. STA. THERE IS 1.97 DIFF.  
OUR CHAINING WAS CHECKED WITH NO  
ERROR FOUND

148+46.82

E.C. R.H. SPIKE ✓

35 To  
MON

143+00 2" WAT. TRT. EXP. ✓

142+60 2" WAT. XING. ✓

141+85 2" WAT. XING. ✓

144+76 8' RT. To P.P. 514545 ✓

144+31 FENCE XING. B.W. ✓

B.W. ✓

142+29 FENCE & ✓

140+32 FENCE XING. ✓

140+12.45 P.O.T. 2' RT. To FENCE ✓

139+04 FENCE XING ✓

137+19 0.51 To P.P. 514568 ✓

136+47 14' RT. To METER ✓

135+47 FENCE XING. B.W. ✓

135+09 FENCE XING. B.W. ✓

134+44 FENCE XING. B.W. ✓

133+97.93 P.O.T. 130+05 79' RT. To F.H. ✓

129+78 FENCE XING 2' COBBLESTONE WALL ✓

128+77 FENCE XING B.W. ✓

128+75 END OIL PAVE ✓

128+60 BEGIN OIL PAVE. ✓

128+56 FENCE XING B.W. ✓

129+00 41' RT. To WAT. MET. ✓

E.C. 126+07.33

35'  
To Mon

$\Delta 20^{\circ} 08'$

$R = 1535$

$L = 539.39$

124+34 3' RT. To DEAD MAN ✓

122+77 B.W. FENCE XING. ✓

2" WATER XING ✓

122+00

2" WAT. 5/2 @ B.C. ✓

B.C. 120+67.94 R.H. Nail

3" OIL

119+38 30" STEEL DRAIN XING. ✓

65'

100'

FD. MON. (35)  
110+84.66  
STA. ROAD SURVEY

PROPOSED P.V.

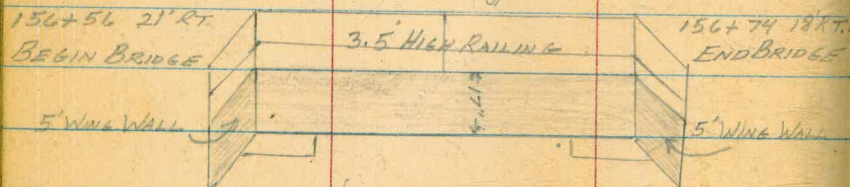
ATKINS TO S.D.

PROPOSED P.L. CONT

165+14.55 R.H. NAIL (3650) 2X2 HUB + T  
CITY BOUNDARY SURVEY. END WORK

FD. 2X2 HUB + T  
CITY BOUNDARY SURVEY  
SEE PAGE 6

159+61.99 E.C. (35) MON STA. 38+57.67  
F.B. 1440-45



THIS IS A SINGLE SPAN WOODEN BRIDGE  
18' LONG & 20' WIDE. SUPPORTED BY 8" X 17" STRINGERS  
COVERED BY 3" X 12" FLOORING WITH OIL TOP.

$\Delta 41^\circ 37' 30''$

$R = 1535$

$L = 1115.17$

DEF. L 1119787

148+46.82 B.C. R.H. SPIKE (35) MON STA. 27+67.93  
F.B. 1440-45

SAME PARTY Hic.

23.

WARM  
8/17/56

F.C. 159+61.99  
FD. MON.

157+50 FENCE XING ✓  
157+37 5' RT. TO P.P. 279922 ✓  
 $\Delta 41^\circ 37' 30''$  156+83 FENCE XING 3' RT. TO ✓  
156+74 18' RT. END BRIDGE GATE POST ✓  
 $R = 1535$  156+56 21' RT BEGIN WOOD BRIDGE ✓  
 $L = 1115.17$  155+85 59' RT TO 4 WATER METERS  
2" WATER ENDS HERE ✓  
152+97 5' LT TO DEAD MAN ✓

27+67.93 (F.B. MON) 35' B.C. 148+46.82  
& PROPOSED ROAD SURVEY

(ALSO KNOWN AS SORRENTO FILTER PLANT)  
 TORREY PINES FILTER PLANT TO EASTLY CITY  
 LIMITS OF S.D. PROPOSED P.L.  
 PROFILE

WILLIAMIS R  
 KELLHOFER  
 PAULSON &

24

WARM  
 8-20-56

B.M.	2.26	42.68		U.S.G.S 40.42
			10.32	323.65
CK.BM	To City Datum	-6.12	26.24 = 25.72	25.72 City Datum F.B. 1440 - 47
	<b>CORR. HI.</b>	31.24		BP on Circular Conic for. of removed RR tank.
B.M.	5.52	31.76		26.24 = 25.72
		29.23		
TP	4.12	29.75	6.13	25.11 25.63
		26.96		23.49
TP	3.47	27.48	5.74	24.01
		28.84		21.14
TP	7.70	29.36	5.82	21.66
SET		28.06		24.63
T.B.M.	3.43	28.58	4.21	25.15
		26.78		22.12
TP	4.66	27.30	5.94	22.64
		23.22		20.13
TP	3.09	23.74	6.65	20.65
		21.53		17.59
TP	3.94	22.05	5.63	18.11
		18.97		15.83
TP	3.14	19.49	5.70	16.35
		17.87		14.18
TP	3.69	18.39	4.79	14.70
		16.39		12.46
TP	3.93	16.91	5.41	12.98
CHK B.M.		16.07		9.84
TP	6.23	16.59	6.55	10.36
		14.32		10.41
TP	3.91	14.84	5.66	10.93
		14.62		8.91
TP	5.71	15.14	5.21	9.43
SET		15.54		5.83
T.B.M.	9.21	16.06	8.79	6.35
		10.41		7.43
TP	2.98	10.93	8.21	7.95

← 250' SW. of Sorrento Crossing at Edelweiss  
 in a fence cor. bottom of a square hole in  
 the top of a stone or cement post

25.72 City Datum F.B. 1440 - 47

**NOTE: THESE ARE CHECK LEVELS FROM  
 EDELWEISS & SORRENTO VALLEY RD. TO  
 TORREY PINES FILTER PLANT. THE  
 CORRECT STARTING B.M. PROVED OUT AS 25.72**

Spike in wooden wing wall 11' RT. 63+89.71 &

45' LT  
 STA. 27+56 U.S.G.S. B.M. #M895

Spike in  
 Power Pole 18' LT. 14+59

TORREY PINES FILTER PLANT TO EASTLY  
CITY LIMITS OF S.D. PROPOSED P.L.

Same  
Party

10.41/11 PROFILE

	10.41	11	
	10.93		
4.82	10.66	4.57	5.84
	11.18		6.36
	21.60		9.34
12.26	22.12	1.32	9.86
	33.19		20.92
12.27	33.71	0.68	21.44
	43.47		32.72
10.75	43.99	0.47	33.24
CHK B.M.		1.34	42.63
			42.13 = 42.16
			= 48.28

8-20-56

CITY Datum

USGS Datum. CHS & ON HOWELL at Sorrento  
filter plant  
FB-732-29 49

WARM  
8-21-56

B.M.	1.82	43.98	42.16
0+01 <sup>22</sup>		9.18	34.80
+01 <sup>23</sup>		7.8	36.18
+01 <sup>22</sup>		7.3	36.68
+09 <sup>27</sup>		7.6	36.38
TP	1.46	37.59	7.85 36.13
+50		1.8	35.79
193		7.3	30.29
1+00		8.2	29.39
+50		11.2	26.39
77	0.49	24.91	13.17 24.42

redesigned by Leo  
8-28-56

CHS. X ON HOWELL AT Sorrento Filter Plant

Top Exist. 18" S.I. MAIN

Top ground

EDGE Building 37' LT 0+01<sup>22</sup>

Top small slope

Bottom Slope B.W. fence Xing ✓

PROFILE  
(CONT.)

SAME  
PARTY

26.

24.9141

8-21-56

2+00		2.2	22.71
+50		7.0	17.91
3+00		10.5	14.41
TP	0.93 12.63	13.21	11.70
+50		2.6	10.03
+93		4.8	7.83
4+00		6.2	6.43
+06			
+50		7.4	5.23
+92		7.7	4.93
+96		9.2	3.43
5+00		8.7	4.23
+18		6.7	5.93
+50		7.0	5.63
6+00		7.0	5.63
TP	5.33 10.70	7.76	5.37
+50		5.4	5.30
7+00		5.1	5.60
+50		5.5	5.20
+69		5.5	5.20
+74		7.2	3.50
+79		5.8	4.90

B.W. fence line X

4+96 - Bottom Drain Ditch X

$\frac{5.3}{10'}$  LT.

$\frac{5.4}{10'}$  RT.

$\frac{7.5}{10'}$

$\frac{6.4}{10'}$

$\frac{5.7}{10'}$

$\frac{5.2}{10'}$



PROFILE CONT.

SAME  
Party

27

10.70H1

8-21-56

8+00		5.0	5.70
+50		5.4	5.30
9+00		5.2	5.50
+50		4.5	6.20
10+00		4.1	6.60
+50		4.6	6.10
TP	5.34 11.65	4.39	6.31
11+00		6.6	5.05
+50		6.1	5.55
12+00		6.1	5.55
+50		5.9	5.75
13+00		5.8	5.85
+50		4.9	6.75
+55		4.2	7.45
+66 <sup>b</sup>		5.1	6.55
+69		6.3	5.35
+94		6.8	4.85
14+00		5.0	6.65
TP	5.83 15.50	1.98	9.67

B.W. fence Xing ✓

LT.  
 $\frac{7.4}{20}$   $\frac{7.0}{7}$

RT.  
 $\frac{4.2}{10}$

PROFILE CONT.

15.50 H1

14+09.1	8.3	7.20
+23.1	7.9	7.60
TOP TRESTLE 14+09.1	3.95	11.55
+13.6	2.99	12.51
+18.6	2.96	12.54
+23.1	3.80	11.70
+39	10.6	4.90
+50	10.4	5.10
+59	10.4	5.10
+92	10.1	5.40
15+02	4.7	10.80
+04 $\frac{1}{2}$	5.4	10.10
CHK. TRM.	9.66	5.84 = 5.83
+50	5.8	9.70
16+00	6.1	9.40
+50	6.4	9.10
17+00	6.5	9.00
+50	6.6	8.90
TP	5.36 14.31	6.55 8.95

SAME PARTY

28.

	LT.	RT.	
	$\frac{11.1}{21}$	$\frac{10.5}{7.0}$	$\frac{7.6}{5.1}$
	$\frac{11.1}{21}$	$\frac{10.4}{7.0}$	$\frac{7.0}{5.1}$
Top Wood Timber			X
Top West Track			X
" East Track			X
Top Wood Timber			X
101' ABOVE ground Low T&T Wires - 18' LT Pange Pie			X
Top BERM	$\frac{5.17}{21.80}$	$\frac{4.98}{3.50}$	RT. (E.O. = EDGE OIL)
F.B. 933 - 24			
	$\frac{6.13}{23.80}$	$\frac{5.97}{3.50}$	$\frac{5.3}{3}$ Top BERM
	$\frac{6.37}{21.80}$	$\frac{6.34}{3.10}$	$\frac{5.8}{6}$ Top BERM

PROFILE CONT.

SAME PARTY

29

14.31H1

18+00		5.6	8.71
+50		5.4	8.91
19+00		5.3	9.01
+50		5.0	9.31
20+00		4.9	9.41
+50		4.8	9.51
21+00		4.6	9.71
+50		4.6	9.71
TP	5.16 15.01	4.46	9.85
22+00		5.2	9.81
+50		5.2	9.81
23+00		4.9	10.11
+50		4.6	10.41
24+00		4.6	10.41
+50		4.4	10.61
25+00		4.4	10.61
+50		4.3	10.71
26+00		4.2	10.81
+50		4.0	11.01

LT. #

RT.

8-21-56

22'E.O.	$\frac{5.44}{3'E.O.}$	$\frac{5.2}{4.0 Beam}$
22'E.O.	$\frac{5.15}{3'E.O.}$	$\frac{5.1}{4.0 Beam}$
22.5'E.O.	$\frac{4.77}{3'E.O.}$	$\frac{5.1}{4.0 Beam}$
22.7'E.O.	$\frac{4.39}{2.5'E.O.}$	$\frac{4.8}{5 Beam}$
22'E.O.	$\frac{5.09}{2.7'E.O.}$	$\frac{5.6}{6.0 Beam}$
22.2'E.O.	$\frac{4.64}{2.0'E.O.}$	$\frac{5.2}{6.0 Beam}$
22.8'E.O.	$\frac{4.40}{2.2'E.O.}$	$\frac{4.9}{5.0 Beam}$
22.6'E.O.	$\frac{4.14}{3'E.O.}$	$\frac{4.9}{6.0 Beam}$
22.5'E.O.	$\frac{3.98}{3.5'E.O.}$	$\frac{4.5}{5.0 Beam}$

PROFILE CONT.

	15.01 HI		
TP	5.25	16.53	3.73 11.28
27+00			5.2 11.33
+50			5.1 11.43
CHK BM.			6.69 9.84 = 9.84
28+00			5.0 11.53
+50			4.9 11.63
29+00			4.6 11.93
+50			4.2 12.33
30+00			4.0 12.53
+50			3.8 12.73
31+00			3.6 12.93
TP	5.09	18.11	3.51 13.02
+50			5.0 13.11
32+00			4.8 13.31
+50			4.8 13.31
33+00			4.8 13.31
+50			4.7 13.41
34+00			4.5 13.61
+50			4.3 13.81

SAME PARTY

	LT.	RT.	8-21-56
	23'EO.	5.08 4.0'EO.	5.3 5.0'Beam
SEE PAGE 24			
	21.2'EO.	4.94 2.0'EO.	5.3 6.0'Beam
	21.2'EO.	4.51 2.0'EO.	4.8 7.0'Beam
	20.7'EO.	3.93 1.0'EO.	4.3 7.0'Beam
	20.8'EO.	3.56 1.0'EO.	4.0 8.0'Beam
	21.7'EO.	4.75 1.9'EO.	5.2 7.0'Beam
	21.0'EO.	4.70 1.3'EO.	5.1 7.4'Beam
	21.9'EO.	4.40 1.7'EO.	4.7 7.0'Beam

PROFILE CONT.

SAME PARTY

31

35+00	18.11 H1	4.1	14.01
+50		4.3	13.81
TP	5.17 19.14	4.14	13.97
36+00		5.4	13.74
+50		5.4	13.74
37+00		5.4	13.74
+50		5.4	13.74
38+00		4.8	14.34
+50		5.0	14.14
39+00		4.8	14.34
+50		5.6	13.54
40+00		3.3	15.84
TP	5.28 21.22	3.20	15.94
40+50		5.3	15.92
41+00		5.5	15.72
+50		5.4	15.82
42+00		5.3	15.92
+50		5.2	16.02
43+00		4.8	16.42

	LT.	RT	8-21-56
	23.3' EO	3.96 20' EO	4.3 7.0' BERM
	24.0' EO	5.21 2.5' EO	5.8 6.0' BERM
	23.7' EO	5.12 2.0' EO	5.5 4.0' BERM
			5.4 10.4 2.0' BERM 7.0
	BERM ON &	4.80 27.0' EO 6.0' EO	11.1 10'
		4.52 4.7 26.5' EO 6.0' EO 1.0' BERM	10.9 8.0'
		4.41 26.5' EO 7.0' EO	12.2 9.0'
		3.91 4.0 32.0' EO 7.0' EO 1.0' BERM	10.6 8.0'
	BERM ON &	3.64 26.0' EO 7.0' EO	10.6 11.0'
	BERM ON &	5.44 27.0' EO 6.0' EO	13.9 12.0'
		5.29 5.5 26.0' EO 6.0' EO	5.5 13.3 3.0' BERM 11
			5.4 5.0' BERM
		5.15 24.4' EO 4.0' EO	5.5 4.5' BERM
		4.82 22.0' EO 2.0' EO	5.0 7.0' BERM

PROFILE CONT.

SAME PARTY

32

8-21-56

	21.22 H1		
43+50		4.65	16.57
44+00		4.39	16.83
+50		3.9	17.32
45+00		3.75	17.47
TP	5.63 22.54	4.31	16.91
+30			
45+50		5.13	17.41
+65			
46+00		4.83	17.71
+04			
46+50		4.65	17.89
47+00		4.62	17.92
+50		4.54	18.00
48+00		4.54	18.00
+50		4.43	18.11
49+00		4.31	18.11
TP	5.25 23.48	4.31	18.23
+50		5.09	18.39
50+00		4.97	18.51
+56		4.78	18.70

LT	±	RT
E.O. ON ±		
E.O. ON ±	20.6'EO	4.7 9.0'Beam
	20.0'EO	3.84 1.0'EO 4.5 10.0'Beam
SEG. 18" CONC. RETAINING WALL		14'RT. ± ✓
2" C.I. WATER XING		✓
	5.33 18.0'EO	4.94 20'EO
END CONC. RET. WALL		15'RT. ✓
	5.02 17.0'EO	4.86 3.0'EO
	4.94 16.0'EO	4.82 4.0'EO
	4.40 15.0'EO	4.52 4.0'EO
	5.31 14.0'EO	5.17 4.0'EO

PROFILE CONT.

	23.48 H <sub>1</sub>		
51+00		4.50	18.98
+50		4.33	19.15
52+00		3.85	19.63
+50		3.52	19.96
53+00		3.05	20.43
TP	6.61	27.07	3.02 20.46
+50		6.15	20.92
54+00		5.61	21.46
+50		5.15	21.92
55+00		4.90	22.17
+50		4.75	22.32
56+00		4.84	22.23
+50		4.9	22.17
57+00		4.9	22.17
+50		5.0	22.07
58+00		5.0	22.07
TP	4.87	22.07	4.87 22.20
+50		5.1	21.97
59+00			

SAME

ELI	Lt	Rt
2-24" Storm Drain		
56+47		
56+50	22.17	18.37
		-3.8 to H
		13'
56+57		18.27
		-3.9 to H
		13'
56+66	19.17	
	-3.0 to H	
	35'	
56+74		18.97
	-3.2 to H	
	36'	

9-20-56  
 Reduced by  
 Mathison  
 Per Beatty

ED. ON

4.94	5.11	5.4
24.5'EO	40'EO	5.0'BERM

PROFILE CONT.

SAME TARI

8-21-56

LT. ± RT

51+00	23.48 HI	4.50	18.98
+50		4.33	19.15
52+00		3.85	19.63
+50		3.52	19.96
53+00		3.05	20.43
TP	6.61 27.07	3.02	20.46
+50		6.15	20.92
54+00		5.61	21.46
+50		5.15	21.92
55+00		4.90	22.17
+50		4.75	22.32
56+00		4.84	22.23
+50		4.9	22.17
57+00		4.9	22.17
+50		5.0	22.07
58+00		5.0	22.07
TP	4.87 22.07	4.87	22.20
+50		5.1	21.97
59+00			

ED. ON L

4.87 13.5'EO	4.83 5.0'EO
4.20 13.5'EO	4.11 6.0'EO
3.24 14.8'EO	3.25 6.0'EO
5.95 15.0'EO	5.87 5.3'EO
5.24 17.0'EO	5.13 4.0'EO
4.68 20.0'EO	
4.32 20.0'EO	4.86 7.0'BERM
4.81 22.0'EO	4.90 3.0'EO
4.94 24.5'EO	5.1 4.0'BERM
	5.4 5.0'BERM



PROFILE CONT.

SAME PARTY

WILLIAMS X  
KELLHOFER  
PAULSON †

34

8-21-56

LT.

RT.

59+50 27.07 H<sub>1</sub> 5.3 21.77

60+00 5.09 21.98

+22<sup>5</sup>

+40

+50 5.30 21.77

61+00 4.7 22.37

+50 4.2 22.87

62+00 3.4 23.67

TP

+16<sup>02</sup> † 5.05 28.93 3.19 23.88

CHK. T.B.M. 4.31 24.62 = 24.63

EP. ON †

260' E.O.

BEG. AC. BERM CUTTEE †

END CUTTEE † BEG. AC. BERM ON †

300' E.O. 4.44 5.0  
0.5' BERM 7.0'  
3.77 4.4 8.5  
1.5 4.0 12.0  
TOP BERM  
3.01 3.5 8.6  
TOP BERM 3.0 3.0 11.0

SEE P. 24

HOT

8/22/56

T.B.M. 4932956 24.63

62+16.02

62+18

+20.50

+22 5.21 24.35

+22 13.0 16.56

⑤

+22<sup>70</sup> 5.51 24.05

⑤ 62+25 17.3 12.36

+45<sup>40</sup> 5.30 24.26

⑤

+50 5.28 24.28

+5.6 19.0 10.56

PAGE 24  
SPIKE IN WOODEN WING WALL 11.5 FT 63 + 89.71 X

7<sup>5</sup> FT. BEG. 3" WOOD WING WALL 5.62 5 24.35 19.16  
5.35 5.21 10.4  
5. 7.5 7.5' Ground

WING WALL ON † X

TOP ROCK JETTY

‡ ABUTMENT 23.86 21.44 16.56  
GROUND 5.60 8.12 13.0  
3.5 3.5' Top ABT. 4.0' GD.  
‡ BENT #1 21.73 11.96  
5.37 7.83 17.6  
24.19 3.5 3.5' Top cap 4.0' GD.

WATERS EDGE

PROFILE CONT.

SAME PARTY

35

TRANSIT  
LINE  
5' LT of  
&  
↓

8-22-56

LT.

RT

⑤ 29.56 H1  
62+73<sup>23</sup> 5.10 24.46

¢ BENT #2

24.29 21.92  
5.27 7.64  
3.5' 3.5' TOP CAP

⑤  
63+00 5.04 24.52

¢ BENT #3

24.39 21.88  
5.17 7.68  
3.5' 3.5' TOP CAP

⑤  
+02<sup>09</sup> 5.05 24.51

¢ BENT #4

24.42 22.07  
5.14 7.49  
3.5' 3.5' TOP CAP

⑤  
+30<sup>69</sup> 5.01 24.55

WATERS EDGE

+37 18.8 10.76

⑤  
+50 5.04 24.52

¢ BENT #5

24.36 21.84 12.86  
5.20 7.72 77.2  
3.5' 3.5' TOP CAP 4.0' GD.

⑤  
+59<sup>13</sup> 5.09 24.47

BEG. ROCK JETTY

+79 16.3 13.26

¢ ABUTMENT

24.29 21.78  
5.27 7.78  
3.5' 3.5' TOP ABUT.

⑤  
+81<sup>33</sup> 5.12 24.44

TOP ROCK JETTY

+81<sup>33</sup> 12.9 16.66

3" WOOD WING WALL X

24.66 24.63  
4.90 4.93  
4.0' BEG. 15.0' END WALL

⑤  
+82 5.14 24.42

5.4 5.6 11.1  
5.0' 9.0' 20.0'

⑤  
+83<sup>68</sup> 5.15 24.41

JP 2.18 26.81 4.93 24.63

+89.71 X 2.5 24.31

30.0' ED 2.18 2.7 8.4  
30' TOP BEEM 5.0' 15.0

64+50 3.4 23.41

2.94 9.2  
3.0' TOP BEEM 14.0'

65+00 3.82 22.99

AR. BERM ON ¢

4.09 30.0' ED 0.5' SOIL

+50 4.67 22.14

1.0' RT. AR. BERM

+94

3' RT. AR. BERM

66+00 4.82 21.99

4.87  
7.0' TOP AR. BERM

PROFILE CONT.

SAME PARTY

36

8-22-56

	26.81 HI		
66+50		5.00	21.81
67+00		5.33	21.48
+50		5.44	21.37
68+00		5.44	21.37
TP	5.52 26.70	5.63	21.18
+50		5.07	21.63
69+00		5.11	21.59
+50		4.89	21.81
70+00		4.75	21.95
+50		4.55	22.15
71+00		4.49	22.21
+50		4.45	22.25
72+00		4.21	22.49
+50		3.85	22.85
TP	5.55 28.29	3.96	22.74
72+94 <sup>25</sup> POT		5.25	23.04
73+50		4.99	23.30
74+00		4.84	23.45
+50		4.75	23.54

LT.

C

RT

19.0'EO	5.23 4.0'EO.
15.0'EO	5.52 4.5'EO
14.0'EO	5.63 5.0'EO
14.5'EO	5.48 5.5'EO.
14.0'EO.	5.13 6.0'EO
13.0'EO	4.72 7.0'EO
13.0'EO.	4.29 7.0'EO
13.0'EO	5.50 6.5'EO.
13.0'EO	5.04 6.0'EO.

PROFILE CONT

SAME PARTY

37

8-22-56

	28.29 41		
75+00		4.61	23.68
+50		4.35	23.94
76+00		4.32	23.97
+50		4.18	24.11
77+00		4.02	24.27
TP	5.56 29.87	3.98	24.31
+50		5.39	24.48
78+00		5.14	24.73
+50		4.83	25.04
79+00		4.63	25.24
+50		4.41	25.46
80+00		4.38	25.49
+50		4.39	25.48
81+00		4.14	25.73
+50		3.94	25.93
82+00		3.83	26.04
TP	5.21 31.34	3.74	26.13
+50		5.32	26.02
83+00		4.99	26.35

LT.

RT.

13.0'EO

4.85  
5.7EO

13.0'EO

4.59  
5.5'EO

12.5'EO

4.25  
6.0'EO

12.0'EO

5.33  
6.5'EO

12.0'EO

4.89  
6.0'EO

13.0'EO

4.68  
7.0'EO

14.0'EO

4.46  
6.0'EO

14.0'EO

4.12  
4.0'EO

17.0'EO

5.07  
3.3EO

PROFILE CONT.

	31.34 HI		
83+50		4.77	26.57
84+00		4.31	27.03
+24		4.15	27.19
+50		4.26	27.08
+57		4.34	27.00
85+00		4.94	26.40
+50		4.90	26.44
86+00		4.82	26.52
CHK. BM.		5.66	25.68 = 25.72
BM.	5.78 31.50		25.72
+50		4.88	26.62
87+00		4.74	26.76
+50		4.56	26.94
88+00		4.36	27.14
+50		4.19	27.31
89+00		3.98	27.52
+50		3.76	27.74
90+00		3.59	27.91
+50		3.27	28.23

SAME PARTY

38

8-22-56

LT.

C

RT.

OIL RETURN AT EDELWEISS  
EDGE OIL TO EDGE OIL AT EDELWEISS 32'

SEE PAGE 24

F.B. 1440-47

	4.92 5.0'EO
18.0'EO.	4.93 21.0'EO
	4.27 10.0 OIL
	2.29 33.0 OIL
	4.54 9.0 OIL
	2.22 32.0 OIL
16.0'EO.	5.34 7.0'EO
	5.08 8.0'EO
10.0'EO	5.08 9.5'EO
9.0'EO	4.79 10.0'EO
9.5'EO	4.29 9.5'EO.
8.0'EO	4.01 10.0'EO

PROFILE CONT.

SAME PARTY

39

8-22-56

					LT.	C	RT.
TP	5.60	31.50 Hi 33.67	3.43	28.07			
91+00			5.23	28.44	5.57 9.0'EO		5.50 10.0'EO
+50			5.09	28.58			
92+00			4.84	28.83	5.25 8.5'EO		5.12 10.5'EO.
+50			4.53	29.14	WATER METER 16' LT. (BY CEMETARY) ✓		
93+00			4.09	29.58	4.52 9.0'EO		4.44 11.0'EO.
+50			3.56	30.11			
94+00			3.16	30.51	3.64 9.0'EO		3.61 12.0 EO
+50			2.75	30.92			
95+00			2.38	31.29	2.82 8.0EO		2.77 10.5'EO
TP	6.68	37.85	2.50	31.17			
+50			6.21	31.64			
96+00			5.73	32.12	6.08 8.0'EO		6.07 11.0'EO
+50			5.27	32.58			
97+00			4.61	33.24	5.04 7.0EO		4.99 10.5'EO
+50			3.93	33.92			
98+00			3.34	34.51	3.86 8.0'EO		3.99 11.5EO
+50			2.75	35.10			
99+00			2.02	35.83	2.64 8.5EO		2.48 10.5'EO

PROFILE CONT.

SAME PARTY

40

8-22-56

		37.85 H1		
99+50			0.84	37.01
TBM	4.70	42.20	0.35	37.50
+73 <sup>6</sup>			4.66	37.54
+89 <sup>3</sup>			4.38	37.82
100+00			4.39	37.81
+04 <sup>9</sup>			4.41	37.79
+50			4.55	37.65
101+00			4.29	37.91
+50			4.20	38.00
102+00			3.93	38.27
+50			3.64	38.56
103+00			3.31	38.89
+50			3.32	38.88
104+00			2.88	39.32
TP	4.73	44.08	2.85	39.35
+50			4.72	39.36
105+00			4.45	39.63
+50			4.31	39.71
106+00			4.17	39.91

	LT	RT
ON BRIDGE FLOORING 9 <sup>5</sup> RT. 99+73 <sup>6</sup>		
BEG. BRIDGE	11.2 11.0'±0	4.64 10.0
2 BENT	4.70 1.40	6.58 10.0' ABUT.
	4.51 10.0'	7.9 11.0' GD.
	12.2 11.0'	4.58 10.0' CAP
		6.28 10.0' TopLAP
		12.4 11.0' GD
END BRIDGE	10.5 11.0'	6.34 10.0' ABUT
	4.48 10.0'	6.30 10.0' ABUT.
		8.8 11.0'
	4.80 11.0'±0	4.88 9.0'±0
	4.06 8.5'±0	4.54 10.5'±0
	3.54 10.0'±0	3.91 10.5'±0
	3.30 8.5'±0	3.25 10.0'±0
	4.76 8'±0	4.87 10'±0
	4.46 8'	4.54 11'±0

PROFILE CONT.

	44.08 H1		
106+50		3.92	40.16
107+00		3.67	40.41
+50		3.31	40.77
108+00		2.93	41.15
+50		2.35	41.73
109+00		1.47	42.41
TP	9.01 51.38	1.71	42.37
+50		8.23	43.15
110+00		2.29	44.09
+50		6.22	45.16
111+00		5.29	46.09
+50		4.62	46.76
112+00		3.96	47.42
+50		3.21	48.17
113+00		2.56	48.82
+50		2.04	49.34
114+00		1.68	49.70
TP	4.59 54.33	1.64	49.74
+50		4.44	50.89

SAME PARTY

41

8-22-56

LT	RT.
3.98 8'EO	4.11 11'EO
3.48 9.5'EO	3.33 10.5'EO
2.16 9'EO	2.12 11'EO.
7.65 9'EO	7.69 11.5'EO
5.59 8'EO	5.58 11'EO
4.09 7'EO	4.45 10'EO
2.58 8'EO	3.08 10'EO
1.74 8.5'EO	2.16 10.5'EO



PROFILE CONT.

	54.33 HI.		
115+00		4.46	49.87
+50		5.09	49.24
116+00		4.52	49.81
+50		4.39	49.84
117+00		4.89	49.44
+57.49 P.O.T.		5.52	48.81
TBM.	3.92 53.03	5.22	49.14
118+00		4.45	48.58
+50		4.41	48.62
119+00		4.13	48.90
+38		3.97	49.06
+38			
+50		3.95	49.08
120+00		4.12	48.91
+50		4.31	48.72
TP 120+67 <sup>94</sup>	<sup>130.</sup> 5.21 53.93	4.31	48.72
CHK. TBM		1.69	52.24 - 52.19
121+00		5.09	48.84
+50		4.57	49.36

SAME PARTY

42

8-22-56

	LT.	RT.
	4.65 8'EO	4.98 11.5'EO
	4.56 7'EO	4.94 12'EO
	4.44 7'EO	5.42 11'EO
L.S. 2001 2" I.P.	15' LT.	117+57 <sup>49</sup>
	4.73 8.0'EO	5.14 7.0'EO
	4.30 8.0'EO	4.64 10.5'EO
30" STEEL DRAIN PIPE XING		
30" STEEL DRAIN	47.39 TOP 5.64 16.3'	48.21 TOP 4.82 20.0'
	4.33 8.0'EO	4.59 10.5'EO
35' LT. 120+67.94 ON B.C. CONC. MON.		
SHEET 20 of City field NOTES INDEX C47 D5		
	5.48 8.5EO	5.74 11.5'EO

PROFILE CONT.

122+00	53.93 H <sub>1</sub>	3.94	49.99
+50		3.36	50.57
+58		3.1	50.83
+73		0.5	53.43
T.P.	10.02 63.29	0.66	53.27
+77			
123+00		8.8	54.49
+50		6.9	56.39
124+00		5.1	58.19
+34			
+50		3.2	60.09
125+00		2.4	60.89
T.P.	10.54 69.68	4.15	59.14
+50		9.9	59.78
+62		9.9	59.78
+67		8.6	61.08
126+00		9.4	60.28
+50		8.1	61.58
127+00		7.5	62.18

WILLIAMS  
KELLHOFFER  
PAULSON

43  
HOT  
8-23-56

	LT.		RT.
	4.27 40' E0		4.57 16.5' E0
	1.2 32 2.0' 1.0'		3.27 2.0' E0 22' E0
	5' RT. TO E.O. ✓		
	B.W. FENCE XING ✓		
	6.1 25'	9.0 4'	12.0 6'
		7.5 12'	11.0 14'
	1.7 25'	5.2 10'	
	3' RT. TO DEAD MAN ✓		
	0.6 25'	3.8 10'	
	0.3 25'	3.0 10'	
	6.7 25'	7.5 13'	9.2 7'
		10.1 10'	
		7.2 25'	9.0 10'
		6.3 25'	8.0 10'

PROFILE CONT.

SAME PARTY

44

8-23-56

				LT.	RT.
127+40	69.6841	7.4	62.28	6.1 25'	8.2 10'
+50		10.6	59.08		
+53		11.0	58.68		
+67		7.6	62.08	5.9 25'	8.3 10'
128+00		8.2	61.48	5.6 25'	8.9 10'
T.P.	5.24 66.51	8.41	61.27		
+50		5.4	61.11		
+56					
+60		5.46	61.05		
+75		5.92	60.59		
+77					
129+00		6.1	60.41	4.2 25'	6.8 10'
+00				18' RT. <sup>CONC.</sup> 3' DIA. WATER TROUGH - 41' RT. WATER METER ✓	
+27		5.5	61.01		
+34		7.1	59.41		
+38		8.9	57.61		
+47		5.4	61.11		
+50		5.5	61.01		
+77					

Bottom  
& DITCH

B.W. fence line ✓

Beg. OIL PAVT. (PRIVATE ROAD) ✓

END OIL ✓

B.W. fence line ✓

BOTTOM DITCH ✓

B.W. fence line ✓

PROFILE CONT.

12.9	66.51 #1		
+78		4.52	61.99
+79		6.0	60.51
130+00		5.1	61.41
+02		5.2	61.31
+03		3.53	62.98
+50		1.9	64.61
TP.	12.20	78.11	0.60 65.91
131+00		11.0	67.11
+50		7.6	70.51
132+00		3.9	74.21
+50		1.6	76.51
TP.	11.69	88.78	1.02 77.09
133+00		10.1	78.68
+50		9.7	79.08
+97 <sup>93</sup> P.O.T.		10.4	78.38
TP.	2.27	80.44	10.61 78.17
134+44		6.0	74.44
+50		8.8	71.64
+56		10.20	70.24

SAME PARTY

45

8-23-56

	LT.	C	RT.
2' COBBLESTONE WALL XING			✓
BEG. DIRT ROAD (PRIVATE)			✓
	3.4		
	25'		
END DIRT ROAD			✓
2' COBBLESTONE WALL XING			✓
& Fence XING			✓
	9.1		11.4
	25'		10'
	1.7		4.8
	25'		10'
	6.7		11.6
	25'		10'
	4.2		12.7
	25'		10'
B.W. FENCE XING			✓
EDGE OIL SACRAMENTO VALLEY ROAD			✓

PROFILE CONT

SAME PARTY

46

8-23-56

	80.44 #1		
135+00	11.29	69.15	
+09			
+47			
+50	10.1	70.34	
136+00	8.95	71.49	
+47			
+50	8.52	71.92	
T.P.	12.69	84.95	8.18 72.26
137+00			12.49 72.46
+07			12.5 77.45 72.45
+19			10.1 74.85
+50			5.5 79.45
T.P.	12.65	95.04	2.56 82.39
138+00			9.8 85.24
+50			10.0 85.04
T.P.	6.25	88.90	12.39 82.65
+85			11.4 77.50
139+00			11.2 77.70
+04			
+11			
+50			10.4 78.50

	LT.	CT.	
EDGE OIL	9.44 21'EO	12.9 5'	✓
B.W. FENCE XING			✓
B.W. FENCE XING			✓
	9.15 24'EO	9.73 5.0'EO	12.4 5'
METER 14' RT.		8.75 17'EO	9.30 3'EO
12' RT. TO B.W. FENCE		8.45 9'EO	✓
EDGE OIL	2.5 25'	8.1 6'	10.8 3'
			12.6 2' 12.65 17'
0.5' LT. P.P. # 514568			✓ B.W. FENCE XING ✓
	+1.5 25'	7.7 4' fence	11.49 9'EO
			12.7 11' fence ✓
			17' fence ✓
			10.5 25'
			11.4 12' fence ✓
FENCE XING ✓			13.5 12' - 18" ID CONC DRAIN ✓
8' RT FENCE ✓			

PROFILE CONT.

SAME PARTY

47

8-23-56

	88.90 H <sub>1</sub>		
+63		10.1	78.80
140+00		4.6	84.30
+32		4.1	84.80
+50		4.5	84.40
TP	5.20	86.30	78.0 81.10
141+00		4.66	81.64
+50		6.09	80.21
+75		8.11	78.19
12 1/2 +00		9.5	76.80
+29			
+31			
+50		12.0	74.30
+68			
TP	4.53	77.92	12.91 73.39
143+00		5.73	72.19
+50		6.01	71.91
144+00		6.8	71.74
+31		5.2	72.72
+50		5.2	72.72

LT

C

RT

FENCE XING ✓

FENCE 4.4 5.9 7.5 7.50 9.06  
31 25 25' 22'E0 3'E0  
B.W. FENCE XING ✓  
B.W. FENCE XING ✓

FENCE 8.5 10.6 11.66 11.90  
29 25 23'E0 3'E0  
3 1/2 RT WATER METER ✓

E.O. E ✓

FENCE 4.7 6.4  
5' 4'

B.W. FENCE XING ✓

0.9  
25'

4.9

3' FENCE

9.53

7'E0

25'E0

+3.8  
25'

2.0  
5'

7.4

7.59

1' 2'E0

20'E0

1.1  
12

2.5  
8'

4.60  
7'E0

5.48

13'E0

4'E0

9.7

4' FENCE ✓

16.3  
13'

3.2  
22' FENCE

5.58  
18'E0

5.80  
4'E0

6.60  
18'E0

3.1  
25'

5.4

6.2

3' FENCE

6'E0 ✓

PROFILE CONT.

SAME PARTY

48  
8-23-56

144		77.92 HI		
+76				
145+00		5.0	72.92	
+50		4.6	73.32	
146+00		3.0	74.92	
TP	12.08	88.42	1.58	76.34
+50			9.9	78.52
147+00			8.5	79.92
+50			7.4	81.02
148+00			4.9	83.52
+46 <sup>82</sup> B.C.			1.8	86.62
TP	11.52	98.19	1.75	86.67
TP	5.81	98.03	5.97	92.22
149+00			8.0	90.03
+32			9.8	88.23
+50			8.8	89.23
+86			8.7	89.33
150+00			6.5	91.53
TP	13.00	110.29	0.74	97.29
+50			11.8	98.49

4' or P.P. # 514565 ✓

4' 0" 41'

3.4  
25' 5.6  
10' FENCE ✓

+0.7  
25' 5.0  
25' FENCE ✓

5.9  
25' 9.5  
10'

1.1  
25' 6.3  
10'

+2.5  
25' 3.3  
10'

B.C. Mon. 35' LT. 148+46<sup>82</sup> ✓

2.9  
25' 9.8  
10'

6.6 7.3  
25' 22' 9.5  
10'

6.5  
25' 6.5  
10'

9.1  
25' 13.2  
10'

PROFILE CONT

SAME PARTY

49

8-23-56

		110.29 H <sub>1</sub>		
+ 151+00		4.9	105.39	
1 TP.	12.38	122.56	0.11	110.18
+ 50		9.1	113.46	
1 + 80		5.6	116.96	
7 152+00 P.O.C.		5.0	117.56	
+ 50		5.6	116.96	
+ 97				
153+00		8.4	114.16	
1 TP.	3.58	114.70	11.44	111.12
+ 50		3.3	111.40	
7 154+00		5.4	109.30	
+ 50		9.1	105.60	
1 TP.	2.51	105.32	11.89	102.81
155+00		4.5	100.82	
+ 40		5.1	100.22	
+ 15		6.4	98.92	
1 + 50		9.0	96.32	
TP.	3.14	95.88	12.60	92.72
+ 85				
156+00		4.3	91.58	

LT.

RT.

0.8  
25'

6.4  
10'

6.2  
25'

10.9  
10'

3.5  
25'

5.9  
10'

4.3  
25'

6.5  
10'

5' LT TO DEAD MAN & 32' RT PP. #79614 ✓

6.0  
25'

9.8  
10'

2.0  
25'

4.3  
10'

3.7  
25'

6.3  
10'

5.6  
25'

11.3  
10'

1.9  
25'

5.6  
10'

8.2  
25'

10.0  
10'

4 WATER METERS 59' RT. ✓

3.7  
25'

5.5  
10'



PROFILE CONT.

SAME PARTY

50

8-23-56

1	156	95.88 HI	
	+18		
1	+27		
	+35	6.3	89.58
1	+40	7.4	88.48
7	+50	7.7	88.18
	+56	7.7	88.18
	+59	8.0	87.88
	+61	8.9	86.98
	+63	8.0	87.88
	+65	7.1	88.78
7	+74	7.6	88.28
7	+83	7.1	88.78
1	+88	5.9	89.98
	157+00	6.3	89.58
	+37		
7	+50	5.7	90.18
1	+70	7.0	88.88
	158+00	5.73	90.15

LT C RT.

BEG. AC. ROAD (PRIVATE) ✓

END AC. ROAD ✓

6.9 7.9  
25' 10'

21' RT. BEG. WOOD BRIDGE N.W. COR. 8.7 5.81  
21' 21'

18' RT. END BRIDGE N.E. COR. 9.5 5.6  
18' 18'

3' RT. TO GATE POST - 12' LT. TO GATE POST ✓

5.6 6.5 GUTTER 6.29  
25' 8' FENCE 7.3 11' 16' EO

5' RT. P.P. 279922 ✓

B.W. FENCE XING ✓ 5.9 7.1 6.35 ✓  
25' 4' GUTTER 7' EO

E. GUTTER

E.O. ON @ 5.4 5.4 6.59  
25' 7' GUTTER 5.67 19' EO

(put water meter 158+35) ✓

PROFILE CONT.

SAME PARTY

51

8-23-56

158	95.88 HI		
+50		4.61	91.27
+94			
159+00		3.31	92.57
T.P.	7.96 99.48	1.36	94.52
+50		5.46	93.52
160+00		5.80	93.68
+50		5.86	93.62
161+00		5.82	93.66
+50		5.51	93.97
162+00		5.08	94.40
+50		4.51	94.97
163+00		3.22	96.26
T.P.	11.23 110.54	0.17	99.31
+50		12.58	97.96
164+00		11.14	99.40
+50		9.57	100.97
165+00		7.86	102.68
+14 <sup>55</sup>		7.38	103.16
CHK. B.M.		2.64	107.90 = 107.93

Reduced by Lee 8-29-56

LT.	C	RT.
4.3 25'	3.7 10'	5.9 9'
4.77 4'E0		4.29 14'E0
1.6 25'	1.8 12'	4.6 10'
3.51 5'E0		3.11 12'E0
Cave Mon. 35' LT 159 + 61 99		
4.3 25'	4.3 13'	7.4 11'
5.85 10'E0		6.64 9'E0
5.1 25'	5.1 12'	7.2 10'
6.30 65'E0		5.74 10'E0
(put water meter 161+83)		
5.8 25'	5.5 13'	7.2 11'
6.2 75'E0		5.95 9'E0
4.6 25'	4.6 13'	6.4 12'
5.41 8'E0		5.16 10.5'E0
0.9 25'	1.4 13'	4.0 11'
3.41 7'E0		3.45 9'E0
(put water meter at 163+25)		
8.0 25'	9.1 12'	12.0 10'
11.57 7'E0		11.62 11'E0
3.8 25'	F 20'	5.2 10'
9.33 6'E0		9.33 8'
7.71 11'E0		
2x2 Hub 35' LT 165+14 <sup>55</sup> F.B. 1440-45		

Walley V

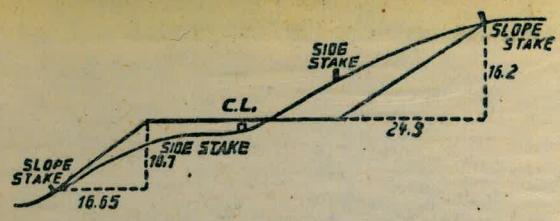
FB 933, p21.

Shows  $\frac{1}{2}$  water  
65' Ely,  $\frac{1}{2}$  of R.R.

- on pg. 41 x-sects  
Shows road to be  
11' Wly & 8' Ely  
of  $\frac{1}{2}$  of water  
Sta. 111+00 - 112+00

Beatty

1.07565 186.7  
 90 444  
 9688850  
 186.40  
 444  
 1.07565  
 80 186.3556  
 86.05300  
 93.74  
 .0699  
 84366  
 84366  
 56744  
 6552426  
 93.74  
 455  
 87.19



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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