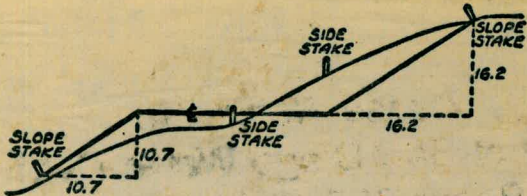


W 940





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Please Return to  
City of San Diego Water Dept.  
Room 903 Civic Center

1.0353  
25  
51860  
2 0704  
3752  
13.35  
330.92

179 59 00  
130 44 80  
49 15 30



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.08	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

MONTGOMERY Pipeline - Profile 2-18 ✓

alice

Montgomery Pipe Line Revised

Alignment Profile From Sta 167+95<sup>00</sup>

to Sta = 256+96 12 AH  
266+39 82.5K 19 - 33

Location & Elev 20" C.I. WAT 34

Revised Alignment MPL 35

Admiral Baker Field 73+50

91+00

41

MONTGOMERY Pipe Line Revision 42

Profile 31+00 To 52+50

215+78.11 To 243+03.47

MONTGOMERY PIPE LINE RE-ALIGNMENT 52-57

alice



MONTGOMERY PIPELINE  
& PROFILE

DEC. 13 1956  
BEATTY  
PAULSEN  
O'BRIEN

2

BM	0.47	112.62		112.15
BM	0.57	<sup>H.I.</sup> CORRECTED 112.70	0.57	112.05 = 112.13'
BM			4.17	<sup>53</sup> 108.45 = 108.53'
BM			4.24	<sup>46</sup> 108.39 = 108.47'
BM	3.76	<sup>H.I.</sup> CORRECTED 108.85'	7.60	<sup>10</sup> 105.82 = 105.09
1+50 (E hub)			4.20	104.65
1+56			4.5	104.35
1+61			3.7	105.15
1+70			3.5	105.35
1+80			4.1	104.75
2+00			4.2	104.65
2+41 Edge of road			5.7	103.15
2+45			4.7	104.15
2+50			4.7	104.15
3+00			3.5	105.35
3+50			1.2	107.65
PP Deck	9.54	117.90	0.49	108.36
4+00			7.0	110.30
4+25			2.6	115.30

BP NE Cor Val Chamber El Capitan PL

CHS # NW Cor MURRAY PL Val Chamber

CHS # NE Cor MANIFOLD Val Chamber

CHS # SW Cor " " "

CHS # W. side center Sparling Mt Chamber  
CITY BM #25



MONTGOMERY P.L.  
2 Profile

12/13/56

10157  
West  
Williams  
Kellhofer

3

10.2  
1.3  
1.9

	117.90			
IP rock	12.87	130.27	0.50	117.00
4+50			11.4	118.27
4+75			5.0	125.27
5+00			0.3	129.97
IP rock	11.57	141.58	0.26	130.01
5+50			2.9	138.68
5+75			2.6	138.98
5+95 <sup>52</sup>	X PT. (on hub)		2.69	138.89
6+00			2.1	139.48
set TBM	9.61	149.50	1.69	139.89
6+50			5.4	144.10
7+00			3.1	146.40
+50			4.6	144.90
8+00			7.3	142.20
	0.49	136.91	13.08	136.42
+50			1.2	135.71
9+00			8.1	128.81
	1.09	125.97	12.03	129.88
+50			5.8	120.17

Nail Nor side RPole-375556

2.6  
20.1

7.8  
20.1

12.6  
20.1

2.3  
20.1

12.3  
20.1

4.2  
20.1



	125.97		
9+65		10.9	115.57
TP	0.25	115.93	108.9
9+75		7.9	108.03
+92		10.0	105.93
10+15		8.3	107.63
+25		6.5	109.43
+35		2.6	113.33
+50		1.1	114.83
TP	2.03	114.15	1.81
11+00		2.5	113.65
+50		8.6	107.55
TP	0.48	106.82	9.81
12+00		5.5	101.32
+15		7.2	99.62
+50		9.5	97.32
13+00		12.3	94.52
	1.09	95.22	12.69
13+50		8.6	86.62
+58		9.1	86.12

11.3  
5.7  
5.6

121  
57  
64  
23  
39

Drainage  
Top of Creek Bank Allied Roadside

Top of wash

Top Wly side of Creek Bank

7.7  
20' Lt

+3.9  
20' Rt

Turn on 1"x1" Angle 25' Rt 12+15

10.7  
20' Lt

+0.2  
20' Rt

26.0 18.0  
20' Lt 10' Lt

5.3  
20' Rt

11.9  
3' Lt

4.2  
10' Rt

Top of Bank



	95.22					
	1.18	84.95	11.45	93.77		
14+00			7.2	77.75	$\frac{7.2}{20'LL}$	$\frac{3.8}{8'RL}$ $\frac{0.3}{10'RL}$ Bank
+50			8.1	76.85		
15+00			8.4	76.55	$\frac{8.5}{20'LL}$	$\frac{8.1}{13'RL}$ Top of Slope
+50			8.9	76.05		
+56			7.67	77.28		1' to sky edge 8' RL to N <sub>1</sub> Edge Basin 9' x 10' some slab 4" Thick
16+00			9.2	75.75	$\frac{9.3}{20'RL}$	$\frac{9.0}{15'LL}$
+50			10.0	73.95		
	10.21	85.80	9.36	75.59	$\frac{75.59}{+6.12}$ 81.71 = 81.72 Turn on 1/2" IR	on fence line 20' LL 12+70
17+00			12.1	73.70	$\frac{12.9}{29'LL}$ Edge of Creek	$\frac{14.0}{49'LL}$ Bank $\frac{17.4}{20'RL}$
+50			12.0	73.80		
18+00			11.6	74.20	$\frac{14.0}{49'LL}$ $\frac{13.1}{39'LL}$ $\frac{11.3}{30'LL}$	$\frac{7.1}{12'RL}$
+50			7.3	78.50	$\frac{11.7}{14'LL}$	$\frac{5.1}{5'RL}$
	12.44	97.76	0.48	85.32		
19+00			9.5	88.26	$\frac{11.9}{5'LL}$	$\frac{5.0}{10'RL}$
+50			3.3	94.46		
	3.87	101.52	0.11	97.65		
20+00			$\frac{6.0}{33}$	98.22	$\frac{10.4}{20'LL}$	$\frac{+2.7}{20'RL}$
+50			2.9	98.62		



Sta. 21+00 to 31+395 Revised  
 See pp. 68 & 69, FB 939 rh

	101.52					
21+00 <del>A</del>		3.1	98.42	$\frac{10.1}{20'RL}$	$\frac{3.3}{8'LL}$	$\frac{0.3}{20'RL}$
+50		2.3	94.22			
	0.10	89.15	12.47	89.05		
22+00		1.9	87.25	$\frac{7.5}{15'LL}$	$\frac{1.6}{40'LL}$	$\frac{1.8}{12'RL}$ $\frac{4.17}{15'RL}$
+35		8.4	80.75	Nly edge Benchbed Area		
+45		5.9	83.25			
+50		6.0	83.15			
23+00		9.0	80.15	19'LL edge of Golf Course	$\frac{13.4}{15'LL}$	$\frac{5.3}{10'RL}$
+50		12.8	76.35	8'LL edge of Golf Course		
	1.32	77.81	12.66	76.49		
24+00		4.6	73.21	E on edge of Golf Course		
		5.2	72.61	Beginning at Green #6		
25+00		4.0	73.81	End " " "		
+50		4.6	73.21			
26+00		4.3	73.51	$\frac{5.9}{10'LL}$		$\frac{1.3}{10'RL}$
+50		4.9	72.91			
27+00		5.7	72.11			$\frac{3.0}{10'RL}$
+50		5.9	71.91			
28+00		6.1	71.71			



Void sta 21+00 to 31+39.50  
see pp. 68 & 69 FB 939

77.81

<del>28+50</del>		5.9		<del>71.91</del>
<del>29+00</del>		7.2		<del>70.61</del>
<del>+50</del>		7.5		<del>70.31</del>
<del>30+00</del>		7.8		<del>70.01</del>
<del>+50</del>		7.5		<del>70.31</del>
<del>31+00</del>		8.4		<del>69.41</del>
31+31.88	Δ 11.59	80.70	8.70	69.11
+50		9.5		71.20
32+00		2.2		78.50
+50		6.5		80.20
33+ <sup>00</sup> <del>50</del>	Δ	0.7		80.00
	0.54	80.85	0.39	80.31
33+50				
<del>34+00</del>		2.3		78.55
<del>+50</del>		4.0		76.85
34+50				
<del>35+00</del>		5.3		75.55
<del>+50</del>		5.6		75.25
35+50				
<del>36+00</del>		6.0		<del>82.85</del>
748				74.85 GA
35+ <del>25</del>		6.30		74.55
813				
35+ <del>50</del>		6.83		74.02
36+00				
+50		6.08		74.77

Field CK'd  
Bozilly 1/17/57

Turn at Hub

Begin cone Driveway at Texaco Sta

Outer line edge AC pave Mission Course Rd



Revised - Sec p. 61  
FB 939 rh

80.85

29					
36+25		5.97	74.88		① Mission Gorge Rd
+57 <sup>6</sup>		6.35	74.50		Wly edge of ac pave
+64 <sup>63</sup> 3		6.8	74.05		
37+00		6.7	74.15		
+46		6.6	74.25		Begin AC berm Twain Ave
+48		5.8	75.05		Top AC berm
+50		6.69	74.16		end AC berm
9.02	83.17	6.70	74.15		Turn on @ nail
2.92	82.36	3.73	79.44		State Hwy 80 Mer NE Cor Twain + Mission <sup>Gorge Rd</sup>
+92		9.60	72.76		Wly edge ac pave
+97 <sup>5</sup>		12.36	70.00		① AC gutter
38+00		11.10	71.26		Top AC gutter
+09					Barbed wire Fence Xing
+50		11.4	70.96		
39+00		11.4	70.96		
+50		11.8	70.56		
6.43	80.58	8.21	74.15		37+50
		6.31	74.27 =	74.23?	North East Cor Twain + Mission Gorge <sup>Rd</sup> this $\Pi$ on Hdwall Drain Culvert



	2.05	76.20	74.15
39+61 <sup>5</sup>			
39+88			
40+00		5.4	70.80
+50		5.5	70.70
41+00		6.0	70.20
+24			
+46			
+50		6.3	69.90
+86			
42+00		6.6	69.60
+50		6.4	69.80
43+00		6.9	69.30
	3.20	73.34	6.06
			70.14
+50		3.9	69.44
44+00		3.9	69.44
+50		5.0	68.34
45+00		5.4	67.94
45+50		5.2	68.14

fence line  
 6" Dia Peach or Plum tree on E  
 old Tomato patch  
 22' Lt To NE Cor of 20' x 30' old Barn  
 Begin 6' High Hog wire Chicken pen ~~884~~ 20' Lt  
 end of chicken pen 12' Lt 27' Lt  
 5.4  
 1.544 Top of some Black well on slab of well  
 on NE Cor of Old Barn field



73.34

	46+00		4.9	68.94
3	+06			
3	+14			
4	+28			
	+50		4.9	68.44
-	47+00		5.0	68.34
	+50		4.9	68.44
	48+00		5.2	68.14
	+15			
	+27			
4	+50		4.9	68.44
	+74.8 ± 2		5.5	67.84
1	6.57	74.58	5.33	68.01
	49+00		6.0	68.58
	+50		6.2	68.38
-	50+00		5.8	68.78
	+50		6.0	68.58
1	+74		5.74	68.84
4	51+00		5.8	68.78

3' RL to 3" Dia Apricot Tree  
 13' RL to 2" Dia peach Tree  
 4' RL to 2" Dia peach Tree  
 Begin old Garden plot

end of garden plot  
 old Fence Xing

Drainage Ditch Vandever + River  
 Hub on E of Vandever + Riverdale St  
 Turn on 2"x2" City Eng Hub 15' RL of A

195 CAW 12/158  
 Top Wly Rim Sewer MH 75' RL



	74.58		
51+50		5.7	68.88
52+00		5.6	68.98
+50		5.6	68.98
+62		4.86	69. <sup>72</sup> 62
53+00		5.4	69.18
+50		5.3	69.28
54+00		5.4	69.18
+50		5.2	69.38
55+00		5.2	69.38
+50		4.8	69.78
56+00		4.0	70.58
+43 <sup>70</sup> $\Delta$		3.6	70.98
+43 <sup>7</sup> TP 6.91	78.13	3.26	71.32
+50		7.2	70.93
57+00		7.5	70.63
+50		7.7	70.43
58+00		7.7	70.43
+50		7.8	70.33
59+00		7.4	70.53

West  
Williams  
Kellhofer

11/11/57

11

18' Rt Cur 11/21/58  
Top Why Rim Sewer MH 75' RL

Top Why Rim Sewer MH 15' RL

Dairy fence 13' Lt + 25' RL

" " 6' Lt

" " 5' Lt + 25' RL

" " 5' Lt + 25' RL



	78.13			
59+50		7.5	70.63	
60+00	Revised	6.9	71.23	Dairy Fence 4 <sup>5</sup> ' Lt + 25' RL
+35 <sup>-1</sup>	see pp. 65 & 66	5.7	72.43	
+35 <sup>-1</sup>	FB 939 rh	5.43	72.70	Top Wly Rim Sewer MH 6 <sup>5</sup> ' RL
+50		5.70	72.43	17' Lt to Well
+70				
+95 <sup>±</sup>				15' Lt to Well
61+00		7.2	70.93	
+50		6.7	71.43	
62+00		5.4	72.73	
+19				10' Lt 22' x 17' Corrugated Tin Shed
+50		5.4	72.73	
+74 <sup>±</sup>				Pipe rail Dairy Fence Xing
+82 <sup>±</sup>				" " " " "
63+00		6.3	71.83	
+50		6.7	71.43	
+50				90' RL 6" Conc Tide Drain For Dairy
64+00		8.1	70.03	
+92				Wood Rail Fence Xing



	78.13		
120	71.81	7.52	70.61
64+50		2.3	69.51
65+00		3.2	68.61
+50		4.7	67.11
66+00		5.6	66.21
+50		6.3	65.51
67+00 <del>2</del>		6.8	65.01
+50		8.3	63.51
+70		5.6	66.21
↑ +87		6.3	65.51
+70			
+95		10.7	61.11
68+10		9.3	62.51
+31		11.6	60.21
+40		14.2	57.61
+50		14.3	57.51
+58		14.2	57.61
+81		11.5	60.31
69+00		10.5	61.31

11/11/57

Barbed wire fence Xing

on filled Area

" " "

48' L<sub>6</sub> end of 6" Cone Tile Dairy Drain

Begin Area of Large Broken Cone Block

end " " " " " "

on mission large Creek

" " " "

Barbed wire fence Xing 8° BT to Wire fence <sup>Running Parallel to Road</sup>

Wire fence Xing sly side of Road



71.81

+25	10.3	61.51
+50	8.0	63.81
70+00	2.9	68.91
69+30±	7.22	64.59
66+00	1.24	70.55 = 70.42

25' RT to Hwy Edge  
 Sly edge oil Road leading to Admiral Baker field

4° RT + 24' LT to edge of Oil Pavc  
 Turn on 7" capped pipe 30' RT  
 50° RT spike in PP 279740

11.58 76.17 64.59

70+50	4.6	71.57
70+90	4.0	72.17
71+00	4.2	71.97
71+07		
71+08		
71+12		
+15		
+50	1.9	71.27
+65		
72+00	7.0	69.17
+12		
+50	6.1	70.07

8' RT to edge of Road  
 edge of Road  
 4' RT to edge of Road

✓ 2' LT 12" Dia Cottonwood Tree  
 date Admiral Baker

✓ Barbed wire fence Xing  
 3' RT Begin Main  
 6" x 6" x 5' post 3' RT  
 6 x 6 x 13' Gate Post 6' RT

✓ 1" Ornamental Sapling, with 3' barricade around it 2' RT.  
 2' RT 1/2" Dia Cottonwood 3' x 4" posts  
 24 2" cross pieces painted green

12' RT edge of Road

65' RT to 1" ornamental sapling, with 3' barricade  
 18' RT to edge of Road

15' RT to 1/2" Dia Cottonwood 1" Ornamental sapling, with barricade



76.17

1/14/57

73+00		7.0	69.17		
+50	921	77.52	7.86	68.31	Turn on Curvey
74+00		8.7	68.82		
+50		8.4	69.12		
+71		9.1	68.42		Drainage Channel 17' Rt 1/2" Dia Cottonwood
75+00		7.1	70.42		
+21					5' Rt 1/2" Dia Cottonwood
+50		5.1	72.42		
+65					edge of Road 12' Rt Begin parking Area 1/2" Dia Cottonwood 3' Rt
76+00		5.2	72.32		
+50		5.1	72.42		
77+00		4.8	72.72		
+24					1' Rt parking Area Sign 2' 4" x 4" posts
+50		4.8	72.72		Begin Lawn
78+00		4.3	73.22		5' Rt edge DG Road
+50		4.2	73.32		
79+00		4.1	73.42		Q on edge DG Road
+50		4.1	73.42		
80+00		3.9	74.12		10' Rt edge of Road



West  
Williams  
Kellhofer

16

1/14/57

	77.52		
80+50		2.9	74.62
1205	87.50	207	75.45
81+00		10.3	77.20
+31		7.89	79.61
+50		7.73	79.77
82+00		6.36	81.14
+50		5.38	82.12
+79.5		5.32	82.18
83+00		5.2	82.30
+06		4.9	82.60
+12		2.0	85.50
1275	99.41	0.84	86.66
+50		5.7	93.77
+66		5.3	94.11
1273	111.43	0.71	98.70
84+00		9.1	92.33
1285	123.99	0.29	111.14
+50		8.1	115.89
1298	136.83	0.14	123.85

edge of slab 19' RT

End of Lawn, Begin 10' Concrete Slab Basketball Courts

15' RT to edge of slab

end of concrete slab

Drainage ditch



	130.83		
13.15	149.37	0.61	136.22
85+00		11.6	137.87
TP	12.66	160.85	118 148.19
+50		2.9	158.95
12.44	172.42	0.97	159.98
12.93	184.73	0.62	171.80
12.54	196.26	1.01	183.72
86+00		10.8	185.46
12.87	209.12	0.01	196.25
12.87	221.44	0.55	208.57
+50		1.3	220.14
13.09	234.50	0.03	221.41
13.09	247.20	0.39	234.11
87+00		0.2	247.00
13.07	259.89	0.38	246.82
13.25	272.97	0.17	259.72
11.71	284.38	0.30	272.67
+50		10.5	273.88
13.31	297.44	0.25	284.13

Turn on 1 1/2 x 1 1/2 Gunney 30' Rt 85+35 ±



1/14/57

297.44

13.00 310.42 0.02 297.42

88+00 10.4 300.02

13.30 323.41 0.31 310.11

~~1.50 Void 5.4~~

12.58 335.21 0.78 322.63

+50 9.3 325.91

+66 3.4 331.81

TP 3.95 331.26

88+84 BK = 9  
89+00 AH

TBM Top of Stake 12' East of Fence  
40' Lt. 88+66



Q Profile Revised Alignment  
 MP2 Sta 167+95<sup>30</sup> to Sta

	156	164.19		162.63
TP	137	153.01	12.55	151.64
TP	0.36	140.56	12.81	140.20
	168+00		6.2	134.36
	+50		10.2	130.36
	169+00		10.7	129.86
	+50		11.2	129.36
	170+00		12.0	128.56
	+47		12.0	128.56
	171+00 Pot Hub		10.62	129.94
	+17		10.3	130.26
TP	12.24	151.97	0.83	139.73
	+50		10.3	141.67
TP	13.11	164.91	0.17	151.80
	13.24	178.02	0.13	164.78
	172+00		13.1	164.92
	12.86	190.82	0.06	177.96
	+50		7.9	182.92

West  
 Williams  
 Kallhofer  
 Bull

19

5/10/57

old Sta 165+50

FBM on 1 1/2" x 1 1/2" H.T. See FB 939 p 32

Begin Rocky creek bottom

Q. Creek Running water. 0' Deep

Bottom of Hill



West  
Williams  
Kellhofer  
Ball

20.

5/17/57

	190.82		
12.61	203.14	0.29	190.53
13.22	216.24	0.12	203.02
173+00		4.0	212.24
TBM 12.97	229.08	0.13	216.11
TP 12.53	241.36	0.25	228.83
TP 13.00	254.16	0.20	241.16
173+50		5.7	248.46
12.67	266.78	0.05	254.11
173+78		4.1	262.68
12.99	279.45	0.32	266.46
174+00		3.28	276.17
TP 13.08	292.45	0.08	279.37
8.21 +36 TBM	296.33	4.33	288.12
174+50		1.0	295.33
12.99	308.70	0.62	295.71
TP 12.70	320.93	0.47	308.23
175+00		2.0	318.93
12.94	332.90	0.97	319.96
12.98	345.35	0.53	332.37

nail on Fly side

TP on a 4"x4" Fence post 25' Lt 173+06

on Post Hub

TBM Nail in Fence post 25' Lt

+5.3  
15' Lt

10.2  
15' Rt



on Pot Hub  
 175+50 PJT      345.35  
                          6.40    338.95

+0.7  
 13' 2E      13.8  
                  15' 8E

12.74    357.94    0.15    345.20

176+00      5.3    352.64

+1.3  
 15' 2E      12.5  
                  15' 8E

12.79    370.22    0.51    367.43

TP      13.26    383.42    0.06    370.16

176+50      9.6    373.82

4.1  
 25' 1E      14.2  
                  20' 8E

13.24    396.31    0.35    383.07

13.31    409.57    0.05    396.26

177+00      12.3    397.27

7.2      7.3  
 25' 1E    15' 1E      20.8  
                                  15' 8E

+35 ←      4.2    405.37  
 Bottom of Top Hard

+5.1      +5.1  
 25' 1E    18' 2E      10.4  
 Layer of Linda Vista Conglomerate      15' 8E

TP      13.11    422.04    0.64    408.93

TBM      5.16    426.42    0.78    421.26

5.12    421.30

5.87    420.55

Turn on City Eng Hub 25' 1E 177+43<sup>25</sup>  
 = 421.32 on old 2 Hub FB 939 P 35  
 = 420.70<sup>9</sup> Spike in PP #4528 30' AT old 180+50

TP      177+56 ←      5.6    420.82

15.7      7.7  
 13' 8E    9' 8E      5.3  
                                  25' 1E

Top of Murphy Canyon



5/13/57

	426.42		
177+90 <del>2</del>		26	418.82
178+00		8.0	418.42
+50		11.1	415.32
179+00		14.1	412.32
	0.66	414.93	12.15
			414.27
+50		5.1	409.83
180+00		8.0	406.93
+50		10.5	404.43
181+00		13.2	401.73
	2.38	404.82	12.49
			402.44
+50		4.7	400.12
+75		4.5	400.32
182+00		6.6	398.22
+25	Power Pole Line Xing	Running	to SW
+50		5.9	398.92
183+00		7.2	397.62
			Bottom of draw running to SW
+50		5.7	399.12
184+00		2.2	402.62
	13.18	416.73	1.27
			403.55
+50		9.9	406.83



	416.73		
185+00		5.4	411.33
+50		2.0	414.73
185+62 <sup>25</sup> POT	4.92		
	420.11	1.54	415.19
186+00		4.6	415.51
+50		5.2	414.91
187+00		5.6	414.51
+50		5.6	414.51
+81		6.4	413.71
188+00		4.8	415.31
+32		7.1	413.01
+50		7.4	413.71
189+00		6.2	413.91
+50		7.1	413.01
190+00		5.5	414.61
+50		5.0	415.01
191+00		5.6	414.51
JP	3.43	418.60	4.94
			415.17
+50		4.8	413.8
192+00		7.2	411.4

Turn on Hub

$$\begin{array}{r} 415.19 \\ - 4.60 \\ \hline 415.19 = 415.19 \end{array}$$

$$\begin{array}{r} 415.19 \\ + 4.60 \\ \hline 419.79 \\ - 6.29 \\ \hline 413.50 \end{array}$$

413.50 on (100) RPMH



Q Profile Revised Alignment Cont

West  
Williams  
Kellhofer  
Bull

418.60

5/13/57

192+50 9.1 409.5

193+00 9.6 409.0

+50 8.5 410.1

194+00 6.5 412.1

+50 4.2 414.4

195+00 1.9 416.7

9.22 426.62 120 417.40

+50 7.9 418.72

196+00 4.5 422.12

+ 25<sup>00</sup> POT 4.14 422.48

+50 4.1 422.52

197+00 4.8 421.82

+50 5.5 421.12

198+00 7.4 419.22

+50 7.8 418.82

199+00 8.6 418.02

+50 9.3 417.32

200+00 9.0 417.62

+50 10.3 416.32

422.48  
+ 4.73  
427.21  
- 6.86  
420.35 on (100) PP Hub

on POT H+T



426.62

TP 5.00 420.97 10.65 415.97

200+65 5.1 415.87

200+90 4.3 416.67

201+30 5.6 415.37

+50 5.7 415.27

202+00 6.0 414.97

+50 5.7 415.27

203+00 6.1 414.87

+20 4.7 416.27

+50 6.3 414.67

204+00 6.2 414.77

+50 6.3 414.67

205+00 POT 5.84 415.13

+50 5.3 415.67

206+00 5.2 415.77

+50 5.5 415.47

6.56 421.44 6.09 414.88

207+00 6.8 414.64

+50 6.9 414.54

415.13  
+ 9.97  
425.10 Hi  
- 6.38

on POT H+I

413.72 on (200) RP Hub



	421.44		
207+65		8.3	413.13
208+00		6.2	415.24
+25		7.8	413.64
+50		6.9	414.54
209+00		6.3	415.14
+50		3.9	417.54
7.65	428.28	0.81	420.63
210+00		6.8	421.48
+50		4.4	423.88
211+00		3.9	424.38
+50		4.6	423.68
212+00 <sup>00</sup> POT		5.81	422.47
+25		2.7	420.58
+50		11.5	416.78
1.11	416.73	12.66	415.62
213+00		14.4	402.33
411		15.9	400.83
+50		15.3	401.43
214+00		10.2	406.53
+50		4.0	412.73

in H+T

Bottom of Draw runs NE



416.73

	13.04	429.14	0.63	416.10
215+00			10.1	419.04
+50			7.3	421.84
216+00			5.6	423.54
+50			3.3	425.84
217+00			1.3	427.84
	6.48	434.58	1.04	428.10
+50			5.9	428.68
TBM	6.40	435.36	5.62	428.96
218+00			6.3	429.06
+50			6.5	428.86
219+00			7.4	427.96
+36			7.0	428.36
+50			5.4	429.96
+90			7.1	428.26
220+00			6.5	428.86
+50			6.9	428.46
+70			4.9	430.46
221+00			6.9	428.46

Turn in city Eng. Dept. Map 3016 Rt 217+89.93



435.36

221+50	7.5	427.86	
222+00	6.6	428.76	
+50	7.3	428.06	
223+00	7.1	428.26	
+25	8.9	426.46	
+50	7.4	427.96	
5.74	431.82	9.28	426.08
+85	6.2	425.62	
224+00	5.7	425.12	
+50	6.2	425.62	
225+00	7.6	424.22	
+50	6.3	425.52	
226+00	5.4	426.42	
+23 <sup>65</sup> pot	5.28	426.54	
+50	5.1	426.72	
227+00	6.2	425.62	
+50	8.2	423.62	
228+00	9.1	422.72	
+50	9.7	422.12	



431.82

229+00	10.6	421.22
+50	12.2	419.62
230+00	12.8	419.62
7.29	426.96	12.15
+50	6.6	420.36
231+00	7.2	419.76
+50	7.9	419.06
+75	7.8	419.16
232+00	5.7	421.21
+50	6.9	420.06
233+00	7.8	419.16
+50	7.5	419.46
+25	5.0	421.96
234+00	7.1	419.86
+50	8.0	418.96
235+00	5.9	421.06
+50	6.2	420.76
236+00	5.6	421.36
+50	5.0	421.96



426.96

5/13/57

235+11.07 PLAN STA.

2 236+65<sup>B</sup> 3.90 425.42 5.44 421.52

Turn on H+J

237+00 3.3 422.12

2 238+50 4.3 421.12

238+00 3.4 422.02

+50 4.6 420.82

2 239+00 5.0 420.42

+50 5.4 420.02

240+00 5.7 419.72

+50 5.7 419.72

241+00 5.6 419.82

+50 5.3 420.12

242+00 4.7 420.72

+50 4.6 420.82

243+00 4.9 420.52

4.57 426.49 3.50 421.92

2 244+50 6.3 420.19

244+00 5.5 420.99

+50 6.1 420.39

245+00 5.1 421.39

+50 5.0 421.49



426.49

246+00 4.3 422.19

+50 4.0 422.49

247+00 3.1 423.39

+50 3.1 423.39

248+00 3.3 423.19

+50 2.8 423.69

TBM 3.93 428.10 2.32 424.17

249+00 4.1 424.0

+50 4.1 424.0

250+00 5.1 423.0

+50 5.6 422.5

251+00 5.1 423.0

+50 5.2 422.9

252+00 5.0 423.1

+50 5.1 423.0

253+00 5.0 423.1

+50 5.4 422.7

254+00 6.0 422.1

+50 6.2 421.9

255+00 7.4 420.7

SAME  
PARTY

31

MAY 13, 1957

Turn on Conn City Eng Man 20' RI 248+59.22



MAY 13, 1957

	428.10		
T.P.	2.85 424.24	6.71	421.39
255+50		4.3	419.94
256+00		4.9	419.34
+50		5.6	418.64
257+00		5.7	418.54
+50		6.2	418.04
258+00		5.7	418.54
+50		6.5	417.74
259+00		6.9	417.34
+25		7.1	417.14
+50		5.5	418.74
260+00		6.4	417.84
+50		7.7	416.54
T.P.	1.52 418.21	7.55	416.69
261+00		3.6	414.61
+50		4.2	414.01
262+00		4.5	413.71
+50		4.6	413.61
263+00		4.7	413.51



MAY 13, 1957

418.21

+ 50 5.2 413.01

264.00 5.1 413.11

+ 50 5.3 412.91

265.00 5.3 412.91

+ 50 4.1 414.11

266.00 6.5 411.71

+ 39.82 7.08 411.13

CHK TBM, 6.49 411.72 = 411.57

25' RT. To CITY ENGRS. MONT.

FB. 939-44



MONTGOMERY PL  
 Location & Elevation  
 20" C.I. WATER MAIN

JUNE 2, 1957  
 BEATTY  
 O'BRIEN

34

see pg. 18, FB-939

BM	5.50	405.52	400.02
CK & 273+00		3.54	401.98 = 401.47
& 273+25 <sup>25</sup>		4.34	401.18
		7.62	397.90
		7.70	397.82
CK BM	4.62	400.90 = 400.90	

NW Cor Hdwy 261' RT 273+31

pg. 27 FB 939

oil surfacing = 80+87 KEARNY Mess 20" C.I.

Top 20" C.I. & 273+25<sup>25</sup>

2.83  
 2.79  
 7.62

Top 20" C.I. 5' RT 273+25<sup>25</sup>

4.83  
 2.87  
 7.70

COND. MON. 25' RT 270+60<sup>73</sup> FB 939 pg. 26



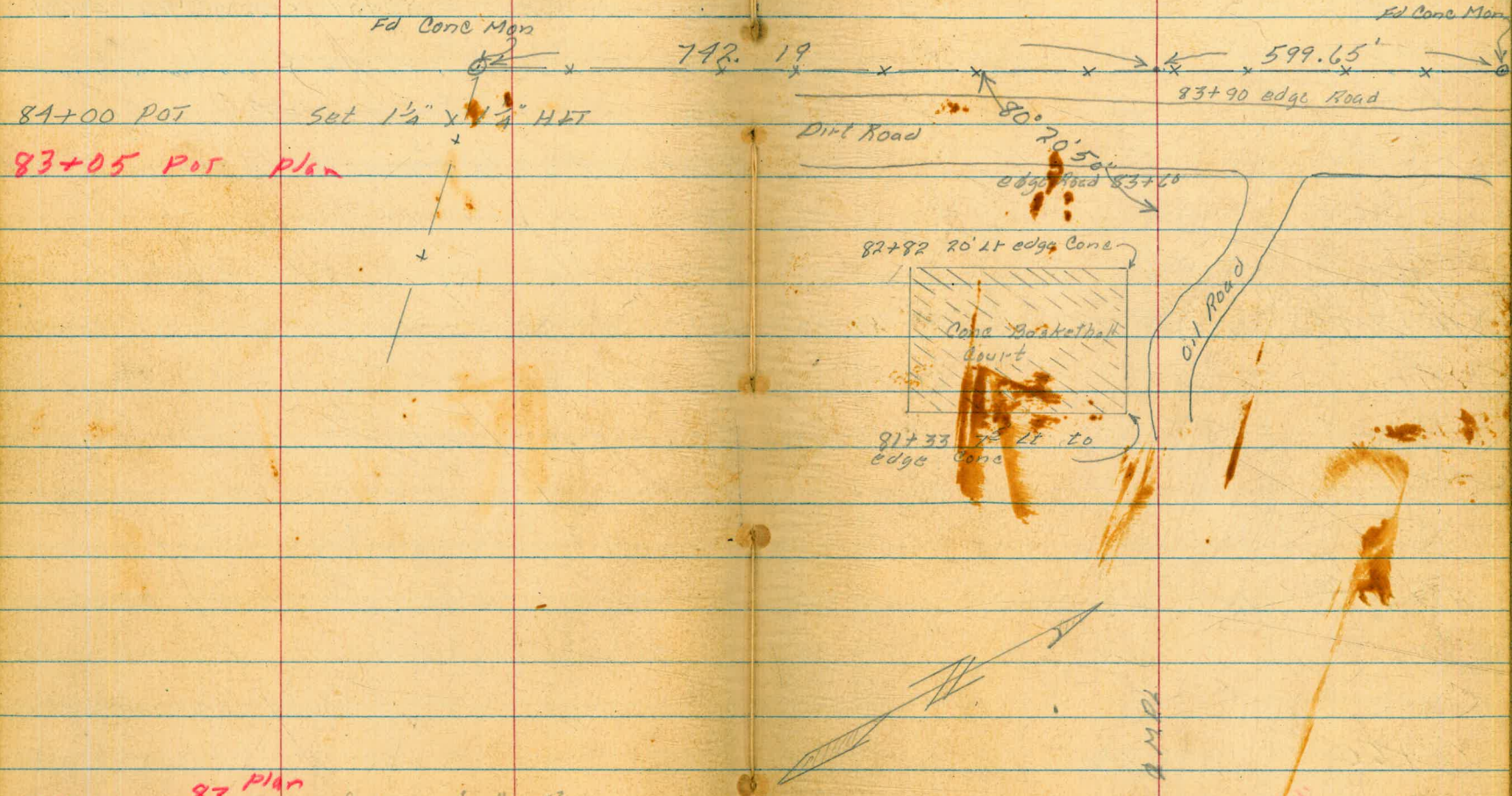
Revised Alignment Montgomery

West  
Williams  
Kellhofer  
Bull

83+50 to

7/1/57

84+46<sup>75</sup> intersection with Navy Prop. Line



72+57 <sup>83</sup> <sub>P1</sub> <sup>Plan</sup> check 24° 58' 30" W.H.  
 73+50 <sup>83</sup> <sub>P1</sub> 25° 00' 20" RT  
 71+35 New PP 7' RT

# 672633H 71+43 Dead Man 12' RT



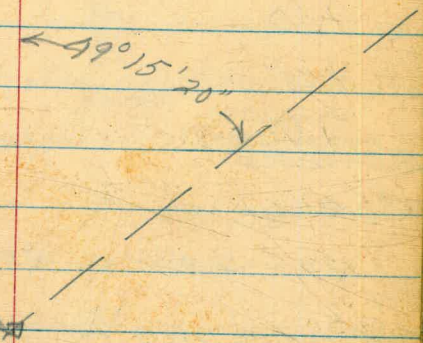
Set 1 1/2 x 1 1/2" H+T  
 = 91+10 29 AH  
 90+64 35 BK Δ 49° 15' 20" RT  
 89+69 36 the 30' with

90+53 20 POT  
 89+58 20 Plan

88+66 55 POT Nail  
 87+71 55 Plan

86+72 20 POT Nail  
 85+77 20 Plan

91+10 29 AH  
 90+64 35 BK



MPL



Revised Alignment MP2			
73+50			
Q profile			
1220	76.79	69.59	
73+50	10.63	78.38	9.09 67.75
74+00		9.2	69.2
+50		9.2	69.2
+75		9.9	68.5
+70			
75+00		7.9	70.5
123			
+50		6.8	71.6
+71			
76+00		6.0	72.4
+50		5.7	72.7
77+00		5.2	73.2
136			
+50		5.1	73.3
+56			
78+00		4.8	73.6
+50		4.4	74.0
SET TRM.	3.97	78.90	3.45 74.93

West  
Williams  
Kellhofer  
Bull

37

7/2/57

TBM Top 2" Pipe See page 14

Turn on H&T

6.9  
39' RT edge DIRT ROAD

LT. RT.  
8.0  
50'  
Top 24" Drain pipe  
9' RT To 1" Ornamental  
with barricade

5.7  
172' EDGE DIRT ROAD  
✓ 1" Ornamental  
SAPPLING ON E with barricade

5.5  
7.0 EDGE OF DIRT ROAD  
✓ 1" Ornamental  
SAPPLING 9' LT. & BEGIN OF PARKING AREA  
with barricade

END OF PARKING AREA

10' LT. TO 3" DIA. PALM TREE

SPIKE AT BASE OF EUC. TREE (78+62-15' RT.)



M.P.L.

SAME PARTY

38

July 2, 1957

79+00	78.90	4.9	74.0
+50		4.7	74.2
80+00		4.4	74.5
+50		3.8	75.1
81+00		2.6	76.3
+2877 POT		1.3	77.6
TP	12.68	90.68	0.90 78.00
+33			
+33			
+50		12.1	78.6
82+00		9.9	80.8
+50		8.0	82.7
+63		7.9	82.8
+82			
83+00		3.3	87.4
T.P.	10.89	101.45	0.12 90.56
+50		5.8	95.7
+55		4.7	96.8
+60		1.2	100.3

78+60	16' RT	42' dia,	125' high	Euc Tree
79+45	14.5' RT	36" dia,	125' "	Euc Tree
79+60	15' RT	30" "	" "	" "
79+81	17' RT	36" "	" "	" "
80+09	17' "	16" "	75' "	" "

5' LT. BEGIN 15' HIGH RETAINING WALL

END OF RETAINING WALL

11.03

7' LT. BEGIN CONC. BASKETBALL COURT.

10.89

9' LT. TO EDGE CONC.

9.48

14.2' LT. TO EDGE CONC.

8.65

17.3' LT. TO EDGE CONC.

8.50

20' LT TO END OF CONC. COURT

LT. RT.

5.6

10'

TOE OF SLOPE OF ROAD FILL

4.2

10'

ELY EDGE DIRT ROAD



M.P.L.

SAME PARTY

39

July 2, 1959

	101.45		
83+90		1.1	100.4
+93		2.3	99.2
T.P. <sup>12.89</sup> Rock	113.22	1.12	100.33
+96		11.0	102.22
84+00		10.0	103.22
T.P.	13.20	0.62	112.60
+46.75		11.5	114.3
T.P.	12.86	0.41	125.39
85+00		6.5	131.75
TP	13.18	0.18	138.07
		3.01	148.24 =
TBM	12.85	0.78	150.47
+50		8.5	154.8
TP	13.11	0.39	162.93
TP	13.17	0.08	175.96
86+00		4.9	184.2
TP	13.12	0.26	188.87
	13.32	0.04	201.95
+50		2.3	213.0
TP	12.88	0.26	215.01
	13.30	0.06	227.83

WLY EDGE OF DIRT ROAD

WLY EDGE GUTTER LINE

TOP OF ROAD CUT.

NARY PROP LINE &amp; BARBED WIRE FENCE XING

148.19 1/2" H+T 83+35 page 17

TBM 1/2" iron pin 10' RT 83+10



M.P.L.

241.13

TP 13.29 254.27 0.15 240.98

87+00 12.0 242.3

TP 13.08 267.22 0.13 259.14

8 +50 0.2 267.02

TP 12.54 279.32 0.44 266.78

7 TP 13.13 292.01 0.44 278.88

8 88+00 0.9 291.11

T T.P. 13.05 304.81 0.25 291.76

TP 13.05 317.64 0.22 304.59

7 +50 2.9 314.74

T.P. 13.13 330.70 0.07 317.57

7 T.P. 13.06 343.00 0.76 329.94

Chk. T.B.M. 11.67 331.33 = 331.26

8 89+00 8.2 334.8

7 +5.5

T.P. 12.98 355.76 0.22 342.78

+50 7.0 348.76

T T.P. 13.22 368.75 0.23 355.53

90+00 2.9 365.85

SAME PARTY

40

July 2, 1957

LT. C Rt

FB. 940-18

FENCE CROSSING

106 345.16  
15'83 360.45  
20'



M.P.L.

SAME PARTY

41

July 2, 1957

T.P.	12.77	368.75 381.04	048	368.27
------	-------	------------------	-----	--------

90+50			1.2	379.84
-------	--	--	-----	--------

T.P.	7.03	387.68	039	380.65
------	------	--------	-----	--------

			5.15	382.53 =
--	--	--	------	----------

382.47

1 1/4" x 1 1/4"

90+35 1/2

HKT FB 939 P 20

Lt.

Rt.

41

25



MONTGOMERY P.L.  
& PROFILE.  
ALIGN'MT REVISION  
STA 31+ to STA 52+

JULY 12, 1957  
WEST.  
KELLHOFFER  
BULL  
Bestly

42

TBM. 6.35 80.62 74.27

Chris H center Culp. Hdwall  
NE Cor. TWIN & MISSION G. Rd.

(FOR SKETCH & ALIGN'MT.  
SEE PG. 77-78 PG 939)

# 4.51 84.61 0.55 80.07

# 8.58 80.66 12.53 72.08

29+50 10.1 70.6

+65 10.2 70.5

(area being filled) ← 8.0 8.5  
10 7

30+00 9.1 71.6

" " ← 7.0 10.1 8.4  
3 3 8

+50 9.1 71.6

+67 8.3 72.4

" " ←

30+72.5 9.3 71.4

Bottom of wall of Bldg. 11.6 8.9  
(FTG) 9.5 6

31+00 10.6 70.1

" " " 11.6 10.8  
8.8 7.2

31+25.02 X PT 10.9 69.8

(110' RT 31+34 FEN. COR  
(same)  
14' RT. 31+50 FEN. COR  
B.W.I.F.C.)

31+48 10.6 70.1

31+50 9.6 71.1

31+54 8.8 71.9

31+58 9.9 70.8

32+27

32+00 3.6 77.1

(115' LT. 32+27  
X PT. in Cyclone  
Fence.

3.9 3.1 1.6 0.7  
10 7 8 13 @ Fen.

32+30 0.8 79.9

32+39.43 POT 0.6 80.1

32+50 0.6 80.1

0.0 0.2 +2.6 +3.8  
@ fence 13 3 8 13 @ Fence

# 6.76 86.92 0.50 80.16

165' LT. 32+76 X PT. in cyclone fence to Cr. Galv. Barn.



MONTGOMERY P.L.  
& Profile Cont'd.

7/12/57

43

33+00	86.92	6.9	80.0	(32+84 29' LT to Cor Galv Barn) (S.D. County?)	6.0 7	4.3 9	2.6 13	@ fence
33+50		6.8	80.1	(33+08 16 1/2 LT to Cor Galv Barn)	6.3 7	3.6 11	3.0 13	@ fence
34+00		6.0	80.9		8.9 14	6.8 12	5.2 7	3.4 13 @ fence
+33		5.1	81.8					
+50		5.1	81.8	Levelled off vacant area	9.6 13	6.0 10 1/2		
35+00		5.1	81.8	(34+59 12 1/2 PT to S. PT. in fence)	10.2 15	6.0 11		
35+32		5.8	81.1	Begin Conc Blk Retaining Wall	5.86 14	6.0 11		(19' LT to fence and BW begin C.W.)
35+50		5.2	81.7	Top Conc Blk wall	5.94 14		1.9 29	(End C.W. fence)
35+73.25	X PT	5.0	81.9	(split off #)	X PT Conc Blk wall	5.96 14	5.0	
				(2' LT 35+76 18" olive tree)				
				5' LT 35+92 - olive Stump				
				8' LT 35+92 Clump Pepper Tree				
36+00		3.6	83.3	Top Conc Blk wall	4.80 13			
				6' LT 36+07 18" Olive Tree				
				6' LT 36+21 14" "				
				7' LT 36+37 8" Olive Clump				



MONTGOMERY P.L.  
& Profile Cont'd

7/2/57

44

		86.92			
①	1.32	86.25	1.99	84.93	Cor. Conc BK wall 13° LT. 36+51 <sup>25</sup> P.L.
36+49			1.12	85.13	Begin 1"-1/2 AC paved driveway (dirt over it)
36+61			1.1	85.2	
36+81 <sup>25</sup>	& TWIN		0.44	85.81	on AC. 2.18 17. Top @ end of curb
36+88 <sup>25</sup>	x PT		0.57	85.68	on AC
(108' Edge of AC) OK Tangl. produced.			1.12	85.13	on AC
37+00			2.07	84.18	" "
37+50			8.34	77.91	" " 2.66 " edge AC part.
37+75			10.48	75.77	" "
37+93			10.56	75.69	" "
37+93	Top 12" A.C. water	<sup>3.80</sup> 3.25	15.25	71.00	" "
38+00			10.52	75.73	" "
OK BM	3.58	77.86	11.97	74.28 = 74.27	this is on curb. to wall NE Cor Twin & Mission Gorge Road.
Nly run Sew. MH			2.05	75.80	7' LT 38+10 C Sew. M.H.
			<sup>16.00</sup>		
Inv. 14" Sew			18.05	59.80	
38+10	& Mission Gorge Road		2.03	75.83	on AC
38+50			3.10	74.76	
38+73 <sup>14</sup> BK			3.94	73.92	
37+65 <sup>73</sup> AH					
38+00			5.01	72.85	5.10 " 14 edge AC. pav.



Montgomery P.L  
& Profile Cont'd.

7/12/57

45

77.86

38+50		5.98	71.88		6.42 Edge A.C. pav.
39+00		6.63	71.23		7.07 " "
39+40 <sup>30</sup>	x RT.	7.23	70.63		
39+45 <sup>8</sup>		7.80	70.06		End A.C. pav't
39+51		8.9	68.96		Top of drain ditch
39+54 <sup>8</sup>	} 2' ft ditch	10.4	67.46		drain ditch
39+56 <sup>8</sup>					
39+59		9.0	68.86		
39+68 <sup>8</sup>		9.2	68.66		B.W. fence crossing
40+00		9.5	68.36		
40+50		9.3	68.56		
41+00		9.4	68.46		
IP	5.41	77.08	6.19	71.67	
41+07		8.3	68.78		41+07 B.W. fence, B.W. fence 5' RT
41+50		8.0	69.08		End of septic Tank Drain from east B.W. fence 3' RT.
41+62		8.1	68.98		B.W. fence crossing 25 RT. Fence Cor.
41+86		7.3	69.78		41+82 <sup>3</sup> } 12 <sup>3</sup> LT. To Conc. (2 <sup>1</sup> / <sub>2</sub> ) <sup>th</sup> lin g. Box
42+00		7.5	69.58		41+85 <sup>0</sup> }
42+50		6.8	70.28		
42+68		6.1	70.98		} small irrig. ditch
42+70		7.2	69.88		
42+72		6.5	70.58		



MONTGOMERY PL  
& Profile Cont'd.

7/12/57

.46

	77.08		
43+00		6.2	70.88
43+39		5.5	71.58
43+42		4.3	72.78
43+45		5.3	71.78
43+47		7.2	69.88
43+48.5		5.6	71.48
43+50		5.5	71.58
44+00		5.5	71.58
44+09		4.9	72.18
44+12		3.9	73.18
Set TBM 5.85	79.29	3.64	73.44
+50		6.7	72.59
45+00		6.3	72.99
+50		6.0	73.29
46+06		5.8	73.49
+20			
+50		5.2	74.09
+78			
47+00		5.9	73.39

43+00 } 5' LT Garden Gate  
43+03 }

} Small irrig. ditch

w.w fence crossing

Nail in pow. pole 8' RT 43+12 #277585

10' LT 18" Dia Olive Tree Overhangs

& 10' wide Dirt Road

10' LT 8" Dia Apricot Tree

7' LT 12" Orange Tree



Montgomery P.L.  
 & Profile  
 7929

47+26			
+50	7.0	72.29	
48+00	7.5	71.79	
+28	7.7	71.59	
+35	4.3	74.99	
+50	6.4	72.89	
+87	6.0	73.29	
+98 9A	7.0	72.29	
+98 9A			
+88 9A			
+88 9A			
+88 9A			
TP	4.56	76.10	7.75 71.54
49+00		3.5	72.60
+50		3.9	72.20
50+00		5.0	71.10
+50		5.7	70.40
+52			
51+00		6.4	69.70

47

7<sup>5</sup> RT 18" Olive Tree

Begin Local Fill To Right of Q  
 7.7  
 7' Lt end of Fill

5ly edge Drainage Ditch

7.9			
5.2 RT	Forward	Tangent	} Drainage Ditch
7.8	"	"	
9.0 RT	"	"	
5.0	"	"	
15.0 RT	"	"	
6.9	"	"	edge Ditch Road
19 RT	"	"	

3.0  
 1.0 Lt Top Drainage Ditch

1.2  
 3 RT  
 5.3  
 6 RT

4.6  
 6 RT  
 5.5  
 8 RT

PP 6' Lt #179121



Montgomery PA.  
Q profile

76.10

51+50

6.1

69.70

52+00

7.2

68.90

5.05

+43° BK

73.89

7.26

68.84

4.12

69.77

=

69.72

Top w/ly rim sewer MH 15' RV 52+62

Turn on 1/2" HFT



MONTGOMERY P.L.  
 Alignment Revision  
 STA. 29+00 - 32+81.79

35+83 P.I. (Continued FB 939-60)

32+81.79 AH. 18°44'30" LT P.I.  
 32+92.32 BK

63° 09' 08" CAW 1/15/58  
 62° 28' RT 8/8/57

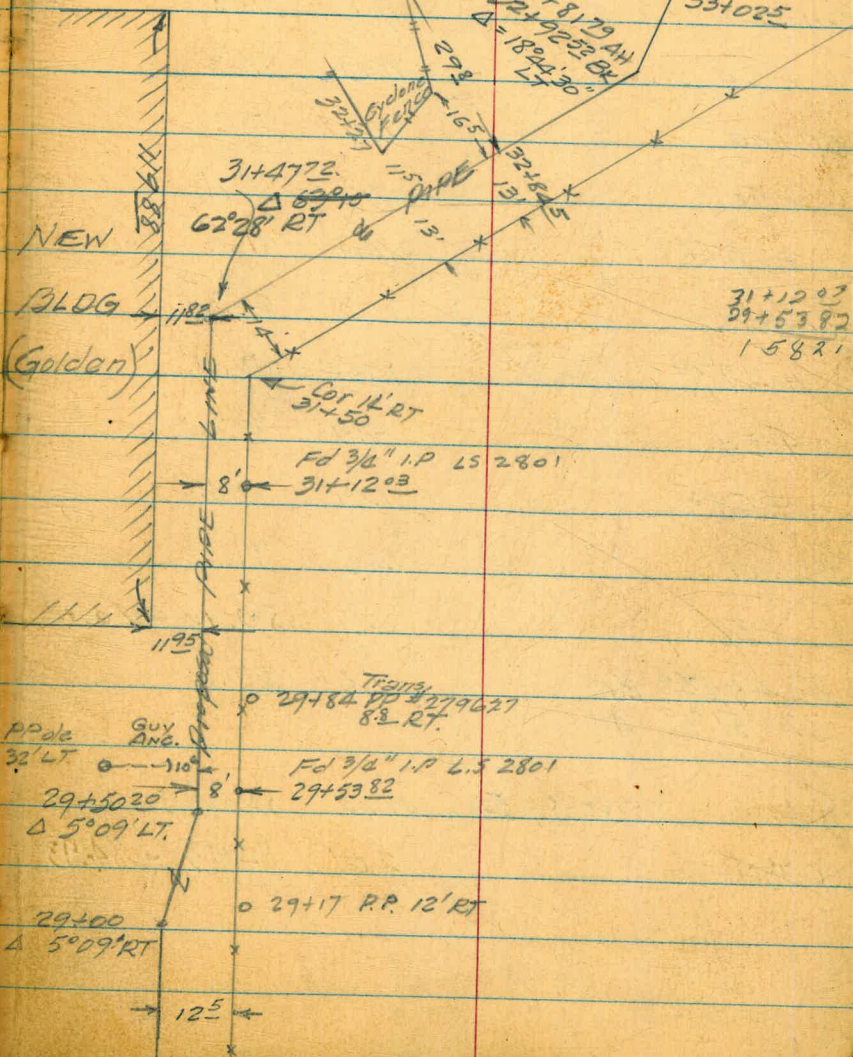
31+47.72 P.I.  
~~63° 10' RT~~  
 24+62.35 PLAN  
 29+67.54 BK

29+50.20 P.I. 5° 09' LT  
 27+70.02 PLAN

29+00 P.I. 5° 09' RT

27+19.82 PLAN  
 26+01 P.I. 15° 01' 35" LT

Aug. 7 1957  
 Williams  
 Kellhofer  
 Spinnagola



35+83  
 Δ 13° 41' 20" RT

31+12.03  
 29+53.82  
 15821



MONTGOMERY P.L.  
 & Profile 29+00 - 32+81.79

8-8-57

50

3	TBM	2.18	87.11 <del>76.45</del>		84.93 <del>74.27</del>	pg 49	Cor Conc Bk Wall 13' LT 36+51
	P	1.25	81.55 <del>70.89</del>	6.81	80.30 <del>69.64</del>		
	29+00			9.8	71.8		
	+50			10.3	71.3		
	30+00			11.0	70.6		
	+50			9.5	72.1		
	+73.72			10.1	71.5		
3	31+00			11.3	70.3		Edge Conc Fig 12.42 11.33 c
12	+47.72 (on R1406)			11.44	70.11		Edge Conc Fig 12.42 11.01 e
	+54			9.9	71.7		
	+58.5			10.9	70.7		
	32+00			4.5	77.1		
	+50			1.5	80.1 = 80.1	see pg. 42	
	32+92.52 BK			1.6	80.0		
	32+81.79 AH						

29	P	7.19	89.54	1.20	80.35		
12	CK TBM			2.61	84.93 = 84.93		

29  
12  
2

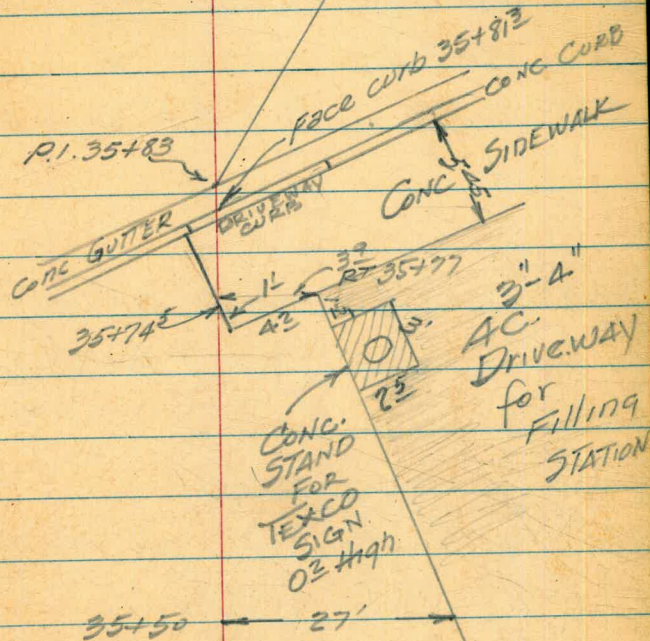


MONTGOMERY P.C

8-8-57

PR# 043  
37+29

51





MONTGOMERY PL.  
 Proposed Re Alignment  
 (STA 215+78 + 236+78<sup>20</sup> Plan Sta)

243+03.47 BK. = ~~235+11.07~~ A.H. PLAN STA.  
 = 234+84.41 Ah

237+20.47 . P.O.T. R.H. NAIL 25' RT To CITY ENGR Mon.

233+47.29 X 90° 27' 30" LT 1 1/4" x 1 1/4" H&T SET  
 BACK T. PROLONGED NLY. R.P. SET AT 30' AND 75'

231+08.56 POT Set 1 1/2" x 1 1/2" H&T

226+00 P.O.T. R.H. NAIL 90° RT. OFF FORW. T. SET R.P. AT 30' AND 60'

218+77" Cone Mon 248' RT

218+32" 89° 59' 00" RT (FORW. T. PROLONGED SLY. R.P. SET AT 50' AND 100'

215+84" 45' RT @ 90° To City Eng Mon

215+78" X 51° 13' 55" Lt

West  
 Williams  
 O'Brien  
 Courtney

F.B. 939-73

243+03.47 BK.  
 = 235+11.07 AH

52  
 H&T R.P. 72 (23)

11-1-57  
 H&T R.P. 74 (20)  
 253+47"

CITY ENGR Mon.

OLD MAP

248'  
 Monument Line  
 Tangent Re Alignment  
 H&T (20)  
 H&T (60)

Set 1 1/2" x 1 1/2" H&T  
 90° RT. OFF FORW. T. R.P. AT 25' AND 75'  
 125' ± H&T. LINE ONLY



MONTGOMERY P.L. PROPOSED RE-ALIGNMENT

± PROFILE

WEST  
WILLIAMS  
O'BRIEN X  
COURTNEY †

11/4/57 53  
SHOWERS A.M.

STA	±	HI	-	EL.
T.B.M.	5.28	434.24		428.96
215+				
78.11 †			5.04	429.2
216+00			5.7	428.5
+50			5.0	429.2
217+00			6.6	427.6
+50			6.8	427.4
+85			6.5	427.7
218+00			5.1	429.1
+17			6.2	428.0
218+				
32.11 †	6.42	435.07	5.59	428.65
+50			6.3	428.8
219+00			5.4	429.7
+50			6.3	428.8
220+00			5.3	429.8
+50			6.2	428.9
+90			6.6	428.5
221+00			5.9	429.2
+24			4.8	430.3
+45			6.7	428.4
+50			6.5	428.6

PAGE 27 CITY ENGR MON.

90° RT. OFF FORW. T. R.P. AT 25' AND 75'  
125' ± LINE ONLY

EL. 427.57 EL. 427.65  
FORW. T. PROLONGED SLY. R.P. AT 50' AND 100'



M.P.L. RE-ALIGNMENT CONT.  
& PROFILE

SAME PARTY

54  
PARTLY CLOUDY  
P.M.

11/4/57

STA.	+	HI.	-	EL.		
221+74		435.07	6.6	428.5		
222+00			4.9	430.2		
+13			6.9	428.2		
+50			6.6	428.5		
223+00			7.1	428.0		
+50			7.7	427.4		
224+00			8.3	426.8	427.5	9.0 426.1
T.P.	3.89	430.71	8.25	426.82	<u>7.6</u>	<u>2.5 RT</u>
+50			5.0	425.7	426.3	5.7 425.0 7.8 422.9
225+00			5.1	425.6	<u>2.5 LT</u>	<u>2.5 RT</u> <u>50 RT</u>
+50			5.0	425.7	425.8	6.3 424.4 7.6 423.1
P.O.T.	90° RT OFF FORW. TAN.				<u>4.9</u>	<u>2.5 RT</u> <u>50 RT</u>
226+00	SET R.P. AT 30' & 60'		5.0	425.7	427.2	4.7 426.0 7.3 423.4
+50			4.6	426.1	<u>3.5</u>	<u>2.5 RT</u> <u>50 RT</u>
227+00			4.8	425.9	427.2	5.4 425.3 6.0 424.7
+50			6.3	424.4	<u>3.5</u>	<u>2.5 RT</u> <u>50 RT</u>
228+00			6.2	424.5	425.8	5.2 425.5 7.3 423.4
+50			4.3	426.4	<u>4.9</u>	<u>2.5 RT</u> <u>50 RT</u>
+82			2.4	428.3	427.1	6.0 424.7 7.8 422.9
T.P.	7.36	434.61	3.46	427.25	<u>3.6</u>	<u>2.5 RT</u> <u>50 RT</u>
229+00			6.5	428.1	426.1	8.3 424.4 11.8 418.9
					<u>4.6</u>	<u>2.5 RT</u> <u>50 RT</u>
					426.6	7.4 423.3 10.0 420.7
					<u>4.1</u>	<u>2.5 RT</u> <u>50 RT</u>



M.P.L. RE-ALIGNMENT  
& PROFILE

CONT.

SAME PARTY

55

11/4/57

STA.	+	HI	-	EL.
		434.61		
229+37			6.2	428.4
+46			7.3	427.3
+50			7.3	427.3
230+00			6.2	428.4
+50			6.2	428.4
+90			4.2	430.4
231+00			4.4	430.2
+11			5.5	429.1
+22			5.5	429.1
+40			3.9	430.7
+50			4.4	430.2
232+00			5.0	429.6
+50			4.9	429.7
233+00			5.2	429.4
+19			3.9	430.7
+35			5.2	429.4
I.P. 4				
233+47.29	6.11	434.99	5.73	428.88
+82			5.9	429.1
234+00			4.3	430.7
+20			6.0	429.0

429.8	431.4	429.3	430.6
4.8	3.2	5.3	4.6
<u>32LT</u>	<u>18LT</u>	<u>5 RT</u>	<u>2.5RT</u>
4.8	3.4	5.5	4.8
<u>31LT</u>	<u>18LT</u>	<u>6 RT</u>	<u>2.5RT</u>
429.8	431.2	431.9	429.1
			429.8

BACK T. PROLONGED NLY. R.P. SET AT 30' AND 75'  
67° 23' RT. OFF BACK T. @ 66' EL TOP MON. 428.98



M.P.L. RE-ALIGNMENT CONT.  
& PROFILE

SAME PARTY

56

11/4/57

STA	+	HI	-	EL
234+50		434.99	5.9	429.1
235+00			6.5	428.5
+50			5.8	429.2
236+00			4.1	430.9
+50			4.3	430.7
237+00			4.7	430.3
+50			5.9	429.1
238+00			9.7	425.3
+50			11.9	423.1
T.P.	3.70	426.60	2.09	422.90
239+00			5.1	421.5
+50			5.0	421.6
+72			4.1	422.5
240+00			5.5	421.1
+35			5.4	421.2
+50			4.8	421.8
+80			6.8	419.8
241+00			6.8	419.8
+29			4.8	421.8
+50			6.2	420.4



M.P.L. RE-ALIGNMENT CONT.  
& PROFILE

SAME PARTY

57.

11/4/57

STA	+	HI	-	EL.
241769		426.60	6.1	420.5
242700			3.5	423.1
+35			5.1	421.5
+50			5.2	421.4
243700			5.0	421.6
2437 03.47 BK = 11.07 AH.	235+		5.03	421.57 = 421.52

PAGE 30

Reduced 11-5-57  
by GA



## MONTGOMERY PIPELINE

STKS. For 36" AT (10')

USED SELF READING ROD

STATION	ELEV.	GRADE
T.B.M.	400.42	
278+60	401.0	391.7
278+00	400.6	393.0
277+50	402.1	394.0
277+00	403.0	395.1
276+50	404.1	396.2
276+00	404.9	397.3
275+90	405.0	397.4
275+50	405.8	397.8
275+00	406.3	398.2
274+50	406.1	398.6
274+00	406.4	399.0
T.P.	405.92	
273+50	407.0	399.4
273+00	406.9	399.7
272+50	407.6	400.1
272+00	407.5	400.5
271+50	407.7	400.8
271+00	408.2	401.2
270+50	408.6	401.6

WEST  
WILLIAMS  
O'BRIEN &  
COURTNEY &11/20/57 58.  
CLEAR

CON. MON. 25' RT &amp; PPE F.B. 939-46

CUT  
C9  $\frac{3}{6}$   
C7  $\frac{6}{1}$   
C8  $\frac{1}{2}$   
C7  $\frac{2}{9}$   
C7  $\frac{9}{6}$   
C7  $\frac{6}{6}$   
C7  $\frac{6}{0}$   
C8  $\frac{1}{5}$   
C7  $\frac{5}{4}$   
C7  $\frac{4}{6}$   
C7  $\frac{2}{5}$   
C7  $\frac{5}{0}$   
C6  $\frac{9}{0}$   
C7  $\frac{0}{0}$   
C7  $\frac{0}{0}$



## MONTGOMERY P.L. CONT.

USED SELF READING ROD

## SAME PARTY

59

STATION	ELEV.	GRADE	CUT	
270+00.	409.6	402.0	C7 $\frac{6}{6}$	
269+50	410.1	402.0	C8 $\frac{1}{1}$	
269+00	411.0	402.1	C8 $\frac{9}{9}$	
268+50	411.9	402.1	C9 $\frac{8}{8}$	
268+00	411.1	402.2	C8 $\frac{9}{9}$	
267+50	411.1	402.2	C8 $\frac{9}{9}$	
267+00	411.4	402.2	C9 $\frac{2}{2}$	
266+50	410.9	402.3	C8 $\frac{6}{6}$	
266+00	410.9	402.3	C8 $\frac{6}{6}$	
265+50	411.7	402.4	C9 $\frac{3}{3}$	
265+20	411.6	402.4	C9 $\frac{2}{2}$	
265+00	411.6	402.7	C8 $\frac{9}{9}$	
264+59.05	411.0	403.3	C7 $\frac{7}{7}$	
CHECK T. B.M.	411.49 =	411.57	F.B	939-44 ON CITY ENGR. MON.
T.B.M.	421.52	H & T. PAGE 30	WEST WILLIAMS O'BRIEN & COURTNEY & C $\frac{10}{10}$	FAIR + VERY WINDY 11/21/57
236+00	421.9	411.9		
+50	421.2	411.9	9 $\frac{3}{3}$	
237+00	421.0	411.9	9 $\frac{1}{1}$	
+50	420.6	412.0	8 $\frac{6}{6}$	



MONTGOMERY P.L. CONT  
USED SELF READING ROD

SAME PARTY

60

11/21/57

STATION	ELEV.	GRADE	CUT
238+00	419.8	412.0	C7 $\frac{8}{2}$
+50	420.2	412.0	C8 $\frac{8}{2}$
+70	419.8	412.0	C7 $\frac{8}{2}$
239+00	419.7	412.0	C7 $\frac{7}{2}$
+50	420.0	412.1	C7 $\frac{9}{2}$
240+00	420.6	412.2	C8 $\frac{4}{2}$
T.P.	420.85		
+50	420.9	412.2	C8 $\frac{7}{2}$
241+00	421.1	412.3	C8 $\frac{8}{2}$
+50	420.6	412.4	C8 $\frac{2}{2}$
242+00	<del>420.4</del> 421.4	412.5	<del>C8 <math>\frac{9}{2}</math></del> C7 $\frac{9}{2}$
+50	420.3	412.6	C7 $\frac{7}{2}$
+60	420.3	412.6	C7 $\frac{7}{2}$
243+00	420.6	413.1	C7 $\frac{5}{2}$
+50	421.2	413.6	C7 $\frac{6}{2}$
T.P.	422.0	414.2	C7 $\frac{8}{2}$
244+00	422.5	414.6	C7 $\frac{9}{2}$ OK
+50	422.5	414.7	C7 $\frac{8}{2}$
245+00	423.1	<del>415.0</del> 414.4	<del>C8 <math>\frac{1}{2}</math></del> C8 $\frac{7}{2}$
+50	423.8	415.3 414.1	<del>C8 <math>\frac{5}{2}</math></del> C9 $\frac{7}{2}$



## MONTGOMERY P.L. CONT.

## SAME PARTY

61.

STATION	ELEV.	GRADE	CUT	11/21/57
246+00	423.3	<del>415.7</del> 413.9	<del>C7<sup>6</sup></del> C 19 <u>4</u>	
+50	423.3	<del>415.9</del> 413.7	<del>C7<sup>4</sup></del> C 9 <u>6</u>	
P.O.T. 246+73.45	423.76		$1\frac{1}{4} \times 1\frac{1}{4}$ " H+T. (15) CITY ENER. MON.	
247+00	423.9	<del>416.2</del> 413.5	<del>C7<sup>7</sup></del> C 10 <u>4</u>	
+20	423.8	<del>416.4</del> 413.4	<del>C7<sup>4</sup></del> C 10 <u>4</u>	
+50	424.2	<del>416.9</del> 413.3	<del>C7<sup>8</sup></del> C 10 <u>9</u>	
+70	424.2	<del>416.9</del> 413.2	<del>C7<sup>8</sup></del> C 11 <u>0</u>	
248+00	423.2	<del>415.9</del> 413.1	<del>C7<sup>3</sup></del> C 10 <u>1</u>	
+50	422.9	<del>415.1</del> 412.9	<del>C7<sup>8</sup></del> C 10 <u>0</u>	
+55	422.8	<del>415.0</del> 412.9	<del>C7<sup>8</sup></del> C 9 <u>9</u>	
249+00	423.4	<del>415.0</del> 412.7	<del>C8<sup>4</sup></del> C 10 <u>7</u>	
+50	423.0	<del>415.0</del> 412.5	<del>C8<sup>0</sup></del> C 10 <u>5</u>	
250+00	423.2	<del>415.0</del> 412.3	<del>C8<sup>2</sup></del> C 10 <u>9</u>	
+50	423.2	<del>415.0</del> 412.1	<del>C8<sup>2</sup></del> C 11 <u>1</u>	
+70	423.1	<del>415.0</del> 412.0	<del>C8<sup>4</sup></del> C 11 <u>1</u>	
251+00	423.2	<del>414.9</del> 411.9	<del>C8<sup>2</sup></del> C 11 <u>3</u>	
+50	423.0	<del>414.7</del> 411.7	<del>C8<sup>3</sup></del> C 11 <u>3</u>	
252+00	422.2	<del>414.6</del> 411.5	<del>C7<sup>6</sup></del> C 10 <u>7</u>	
+15	422.0	<del>414.5</del> 411.5	<del>C7<sup>5</sup></del> C 10 <u>5</u>	
+50	421.9	<del>414.0</del> 411.3	<del>C7<sup>9</sup></del> C 10 <u>6</u>	
253+00	421.3	<del>413.3</del> 411.1	<del>C8<sup>0</sup></del> C 10 <u>2</u>	



## MONTGOMERY P.L. CONT.

## SAME PARTY

62

STATION	ELEV.	GRADE	CUT
253+50 T.P.	420.64	<del>412.6</del> 410.9	<del>C8<sup>2</sup></del> C 9 <sup>7</sup>
254+00	419.1	<del>411.9</del> 410.7	<del>C7<sup>2</sup></del> C 8 <sup>4</sup>
+50	419.2	<del>411.3</del> 410.4	<del>C7<sup>2</sup></del> C 8 <sup>8</sup>
+70	419.0	<del>411.0</del> 410.4	<del>C8<sup>2</sup></del> C 8 <sup>6</sup>
255+00	418.9	<del>410.8</del> 410.2	<del>C8<sup>1</sup></del> C 8 <sup>7</sup>
+50	418.4	<del>410.5</del> 410.0	<del>C7<sup>2</sup></del> C 8 <sup>4</sup>
256+00	418.3	<del>410.3</del> 409.8	<del>C8<sup>2</sup></del> C 8 <sup>5</sup>
+50	417.8	<del>409.9</del> 409.6	<del>C7<sup>2</sup></del> C 8 <sup>2</sup>
257+00	417.8	<del>409.7</del> 409.4	<del>C8<sup>1</sup></del> C 8 <sup>4</sup>
+50	417.7	<del>409.9</del> 409.2	<del>C8<sup>3</sup></del> C 8 <sup>5</sup>
258+00	418.3	<del>409.1</del> 409.0	<del>C7<sup>2</sup></del> C 9 <sup>3</sup>
+50	416.6	408.8	C7 <sup>8</sup>
259+00	415.5	407.8	C7 <sup>7</sup>
+50	414.5	406.9	C7 <sup>6</sup>
260+00	413.8	406.0	C7 <sup>8</sup>
+50	413.7	406.0	C7 <sup>7</sup>
261+00	413.5	405.9	C7 <sup>6</sup>
+50 T.P.	413.26	405.8	C7 <sup>5</sup>
262+00	413.3	405.7	C7 <sup>6</sup>
+50	413.0	405.6	C7 <sup>4</sup>

SPKS MKD TO THIS STA  
11/21/57



## MONT GOMERY P.L. CONT.

## SAME PARTY

63

STATION	ELEV.	GRADE
263+00	413.4	405.5
+25	413.2	405.5
+50	414.1	405.1
264+00	412.6	404.3
CHECK T.B.M.	411.73	= 411.57

CUT  
C7 <sup>9</sup>  
C7 <sup>7</sup>  
C9 <sup>0</sup>  
C8 <sup>3</sup>

11/21/57

PAGE 59

## Mont Gomery P.L. Cont.

X West  
Williams  
O'Brien  
P. Courtney

12-12-57

T.B.M.		428.98
233+47 <sup>29</sup>	429.1	418.0
233+50	429.2	418.0
233+37 <sup>29</sup>	429.0	418.0
234+00	429.4	418.0
234+50	429.3	418.0
235+00	428.8	418.0
235+50	429.4	418.0
236+00	430.4	418.0
236+50	430.5	418.0
237+00	430.3	418.0
237+20 <sup>47</sup>	POT.	

C11<sup>1</sup>  
C11<sup>2</sup>  
C11<sup>4</sup>  
C11<sup>3</sup>  
C10<sup>8</sup>  
C11<sup>4</sup>  
C12<sup>4</sup>  
C12<sup>5</sup>  
C12<sup>3</sup>

55  
Cone Men 25' At Sta 233+47<sup>29</sup> 500 p



Montgomery Pipe Line

Same Party

64

12/12/57

Station	Elev	Grade	Cut
237+50	429.4	418.0	C 11 <u>4</u>
237+90	425.8	418.0	C 7 <u>8</u>
TP	425.62		
238+00	425.3	417.7	C 7 <u>6</u>
238+50	423.0	416.3	C 6 <u>7</u>
239+00	421.4	414.9	C 6 <u>5</u>
239+20	422.0	414.4	C 7 <u>6</u>
239+50	421.8	414.0	C 7 <u>8</u>
240+00	421.1	413.3	C 7 <u>9</u>
240+50	421.1	412.6	C 8 <u>5</u>
240+90	419.6	412.0	C 7 <u>6</u>
241+00	420.1	412.0	C 8 <u>1</u>
241+50	420.5	412.0	C 8 <u>5</u>
242+00	422.8	412.0	C 10 <u>8</u>
TP			
242+50	421.45	412.0	C 9 <u>5</u>
243+00	421.6	412.0	C 9 <u>6</u>
235+00	421.4	412.0	C 9 <u>4</u>
235+50	421.5	412.0	C 9 <u>5</u>
236+00	421.5	412.1	C 9 <u>4</u>
Check	421.2	421.2 = 421.2	Pg 59 Sta 236+50



Montgomery PL.  
Used Self Reading Rod.

West  
Williams  
T O'Brien  
& Courtney

65

Cloudy

12-16-57

STA	Elev	Grade	TBM	City Eng	Comp	Men	See page 27
T.B.M.	428.96						
SPLIT OFF							
215+78.11	429.1	420.4	C8	1			
216+00	428.6	420.4	C8	2			
+50	429.1	420.4	C8	1			
217+00	427.6	420.4	C7	2			
+30	427.7	420.4	C7	3			
+50	427.4	420.5	C6	1			
218+00	427.8	420.9	C6	1			
+32.11 X	428.6	421.1	C7	5			
+32.11 X	429.1	421.1	C8	0			
+50	429.3	421.1	C8	1			
219+00	428.9	421.5	C7	4			
+50	428.9	421.7	C7	2			
220+00	428.8	422.0	C6	8			
+40	429.0	422.2	C6	8			
+50	429.1	422.0	C7	1			
220+80	428.6	421.4	C7	2			
221+00	428.1	421.3	C6	8			
+50	428.0	421.2	C6	8			
I 22+00	428.3	421.0	C7	3			



## MONTGOMERY P.L. CONT.

SAME PARTY

66.

12/16/57

STA.	ELEV.	GRADE	CUT
222+20	428.0	421.0	C7 <sup>0</sup>
+50	428.0	420.7	C7 <sup>3</sup>
T.P.			
223+00	427.72	420.2	C7 <sup>5</sup>
+50	427.5	419.7	C7 <sup>8</sup>
224+00	427.1	419.2	C7 <sup>9</sup>
+50	426.4	418.7	C7 <sup>7</sup>
225+00	425.8	418.5	C7 <sup>3</sup>
+50	426.2	418.3	C7 <sup>9</sup>
226+00	425.7	418.1	C7 <sup>6</sup>
+50	426.3	417.9	C8 <sup>4</sup>
227+00	426.4	417.7	C8 <sup>7</sup>
+50	425.4	417.5	C7 <sup>9</sup>
+70	425.1	417.4	C7 <sup>7</sup>
228+00	424.0	418.2	C5 <sup>8</sup>
+50	426.2	419.5	C6 <sup>7</sup>
+70	427.0	420.0	C7 <sup>9</sup>
229+00	427.3	419.9	C7 <sup>4</sup>
+50	427.7	419.7	C8 <sup>0</sup>
230+00	428.4	419.5	C8 <sup>9</sup>
T.P.			
+50	428.80	419.3	C9 <sup>5</sup>



## MONTGOMERY P.L. CONT.

SAME PARTY

67

STA	ELEV.	GRADE	CUT
231+00	429.6	419.0	C10 <sup>6</sup>
+50	430.1	418.8	C11 <sup>3</sup>
232+00	429.6	418.6	C11 <sup>0</sup>
+50	429.8	418.4	C11 <sup>4</sup>
233+00	429.5	418.2	C11 <sup>3</sup>
CHECK T.B.M	428.99 =	428.98	

12/16/57

TOP MON. SEE PAGE 55

12/30-57

0.41	429.37	428.96	
215+50	1.6	427.8	420.4
		C72	
215+40	1.5	427.9	420.4
		C75	
215+00	4.0	425.4	418.7
		C67	
214+50	6.0	423.4	416.5
		C69	
214+00	8.0	421.4	414.4
		C70	
213+70	9.3	420.1	413.0
		C71	
213+50	10.9	418.5	410.9
		C76	

TBM Top Conc Mon 30' RT 216736

0.25	417.05	1257	416.90
213+00	3.4	413.7	405.4
		C83	
212+50	9.2	407.9	399.9
		C80	
2	187	406.61	1231 404.74



STA	+	HI	-	EL	GRADE		
212	+00	406.61		3.7 402.9	394.4	C 8 <sup>5</sup>	
211	+95			3.7 402.9	394.0	C 8 <sup>9</sup>	
211	+50	12.76 414.76	4.61	402.00	394.0	C 8 <sup>2</sup>	
T.P.	12.37	426.74	0.39	414.37			
211	+00		12.0	414.7	408.0	C 6 <sup>7</sup>	
210	+60		5.7	421.0	414.2	C 6 <sup>8</sup>	
210	+50		5.0	421.7	414.5	C 7 <sup>2</sup>	
210	+00		3.6	423.1	416.2	C 6 <sup>9</sup>	
209	+50		2.6	424.1	416.2	C 7 <sup>9</sup>	
209	+00		3.2	423.5	416.2	C 7 <sup>3</sup>	
208	+87		3.5	423.2	416.2	C 7 <sup>0</sup>	
208	+50		4.9	421.8	414.3	C 7 <sup>5</sup>	
T.P.	208	+00	0.86	419.06	8.54 418.20	410.7	C 7 <sup>5</sup>
207	+60		3.1	416.0	407.8	C 8 <sup>2</sup>	
207	+50		3.3	415.8	407.5	C 8 <sup>3</sup>	
207	+00		5.1	414.0	406.2	C 7 <sup>8</sup>	
206	+70		5.0	414.1	405.4	C 8 <sup>7</sup>	
206	+50		4.7	414.4	405.4	C 9 <sup>0</sup>	
206	+10		5.6	413.5	405.4	C 8 <sup>1</sup>	
206	+00		5.5	413.6	405.5	C 8 <sup>1</sup>	

20  
199

900

Turn on Runway

12/31/57

WEST  
WILLIAMS  
T KEMP  
† COURTNEY  
CLEAR 470°



## MONTGOMERY P.L. CONT.

STA.	+ HI	- EL.	GRADE
205+50	419.06	5.3 413.8	405.7
205+00		4.4 414.7	406.1
204+50		3.7 415.4	406.4
204+00		4.2 414.9	406.8
203+70		3.8 415.3	407.0
203+50		4.2 414.9	407.0
CHECK T.B.M.		5.33 413.73 = 413.72	

## SAME PARTY

69

12/31/57

STATION	ELEVATION	GRADE
T.B.M.	413.72	
203+50	414.8	407.0
203+00	414.9	407.1
202+50	414.7	407.1
202+00	414.2	407.2
201+50	414.8	407.2
201+00	414.9	407.3
200+50	415.2	407.3
200+00	415.4	407.4
199+50	415.9	408.0
199+00 <sup>T.P.</sup>	416.01	408.6
198+50	416.8	409.1

C 8 <sup>1</sup>	
C 8 <sup>6</sup>	
C 9 <sup>0</sup>	
C 8 <sup>1</sup>	
C 8 <sup>3</sup>	
C 7 <sup>2</sup>	WLY. SIDE 10' OFFSET
	100' R.P. HUB 203+45.89 F.B. 945-8
	USED SELF READING ROD 1/3/58
	100' R.P. 203+45.89 WEST
C 7 <sup>8</sup>	ELY SIDE (10') WILLIAMS
C 7 <sup>8</sup>	A O'BRIEN
C 7 <sup>6</sup>	+ COURTNEY
C 7 <sup>0</sup>	
C 7 <sup>6</sup>	
C 7 <sup>6</sup>	
C 7 <sup>9</sup>	
C 8 <sup>0</sup>	
C 7 <sup>2</sup>	
C 7 <sup>4</sup>	
C 7 <sup>7</sup>	



## MONTGOMERY P.L. CONT.

## SAME PARTY

70.

CLEAR  
1/3/58

STA.	Elev.	Grade
198+00	417.3	409.6
197+50	418.2	410.5
197+00	419.4	411.4
196+50	419.8	412.3
196+00	421.4	413.2
195+50	422.0	414.2
195+00	422.5	415.0
194+70 <sup>82</sup>	422.1	415.0
Check TBM	420.35 = 420.34	
T.B.M.		72.70
60+79 <sup>62</sup>	72.5	66.5
60+90 <sup>7</sup>	73.4	66.1
61+00	73.2	65.9
61+11 <sup>42</sup>	71.7	65.6
61+42 <sup>58</sup>	71.7	64.8
60+48 <sup>13</sup>	72.7	66.7
		72.70 = 72.70

194+70.89 POT 100' R.P. Hub F.B. 945-8

1/6/58

500 FB 940 P12

Top Wly Rim Sewer MA 6<sup>2</sup> RT 60+354

WEST  
 X WILLIAMS  
 O'BRIEN  
 † COURTNEY

C 6<sup>0</sup>C 7<sup>2</sup> Begin encasementC 7<sup>3</sup> End encasementC 6<sup>1</sup>C 6<sup>2</sup>C 6<sup>0</sup>



M.P.L. Cont		
STATION	ELEV.	GRADE
T.B.M.	415.19	
184+50	415.6	407.6
+66.67	415.5	407.6
+93.17	415.2	407.5
185+00	415.2	407.4
+50	414.7	407.2
186+00	414.3	406.9
+50	414.1	406.4
+90	413.2	406.4
187+00	413.2	406.3
+50	413.5	406.1
188+00	413.5	405.7
+50	414.5	405.5
189+00	414.6	405.2
+50	414.7	404.9
+97.16	414.8	404.6
190+28.65	412.7	403.7
+50	411.8	402.8
T.P. 91.61	409.58	401.8
191+23.15	408.7	401.4
+54.67	408.6	401.4

West  
Williams  
+ O'Brien  
+ Courtney

184+08<sup>14</sup> Plan Sta  
Turn on  $\Phi$  Hub See page 23

0  
C8  
C7 9  
C7 7  
C7 8  
C7 5  
C7 4  
C7 7  
C6 8  
C6 9  
C7 4  
C7 8  
C9 0  
C9 4  
C9 8  
C9 4  
C9 0  
C9 0  
C7 8  
C7 3  
C7 1

PARTLY CLOUDY  
1-6-58



116158

STATION	ELEV.	GRADE	
191+86.21	408.9	401.8	C7 <sup>1</sup>
192+17.76	409.8	403.0	C6 <sup>8</sup>
192+49.26	410.8	404.5	C6 <sup>3</sup>
193+00	413.2	406.9	C6 <sup>3</sup>
T.P. +50	415.18	409.3	C5 <sup>9</sup>
194+00	418.3	411.7	C6 <sup>6</sup>
+50	421.3	414.1	C7 <sup>2</sup>
+69.51	422.2	415.0	C7 <sup>2</sup>

CHECK T.B.M. 420.33 = 420.35

100' R.P. HUB SEE PAGE 70

New Grades from United Pipe Plans

117158

		418.20	208+00 T.P. See Page 68
206+65 <sup>81</sup>	414.0	405.4	C8 <sup>6</sup>
+97 <sup>11</sup>	413.8	406.2	C7 <sup>6</sup>
207+28 <sup>90</sup>	414.9	407.0	C7 <sup>9</sup>
+60 <sup>13</sup>	415.9	408.2	C7 <sup>2</sup>
+91 <sup>98</sup>	417.6	410.0	C7 <sup>6</sup>
208+23 <sup>11</sup>	420.3	412.0	C8 <sup>3</sup>
+54 <sup>84</sup>	422.05	414.1	C8 <sup>0</sup> Turn on (in day)
+86 <sup>26</sup>	423.2	415.6	C7 <sup>6</sup>
<del>209+17 <sup>25</sup></del>			



## M.P.L. CONT.

	422.05				
209+17 <sup>75</sup>	423.7	416.2	C7	<u>5</u>	
210+43 <sup>53</sup>	422.1	414.8	C7	<u>3</u>	
+74 <sup>51</sup>	419.6	412.0	C7	<u>6</u>	
210+00	423.15 = 423.1		See page 68		
114	86.07	84.93	See page 74		
31+00	10.54	75.53 66.00	C9	<u>53</u>	Mission Gorge Road for Jacked encasement
31+50	10.82	75.25 66.00	C9	<u>25</u>	
31+25	10.24	75.83 66.00	C9	<u>83</u>	
	11.79	74.28 =	74.27	Case # on Howell Culvert See page 44	
T.B.M.	415.19	<sup>184+08</sup> Hub	See page 23		
183+98.67	414.6	407.6	C7	<u>0</u>	8-1-58 WEST WILLIAMS O'BRIEN COURTNEY
183+67.46	412.6	405.5	C7	<u>1</u>	
183+50	411.3	403.9	C7	<u>4</u>	
<sup>T.P.</sup> 183+00	407.06	399.7	C7	<u>4</u>	
182+50	402.8	395.6	C7	<u>2</u>	
182+10.45	399.6	392.4	C7	<u>2</u>	
181+79.01	398.6	390.4	C8	<u>2</u>	
181+50	398.4	390.4	C8	<u>0</u>	
181+16.01	398.0	390.4	C7	<u>6</u>	
180+84.51	398.8	390.4	C8	<u>4</u>	



## M.P.2. CONT.

SAME PARTY

74

STATION	ELEV.	GRADE	CUT	
180+53.02	398.7	390.8	C7 <u>9</u>	
180+00	400.2	392.6	C7 <u>6</u>	
179+90.06	400.9	393.0	C7 <u>9</u>	
179+50	402.1	394.3	C7 <u>8</u>	
T.P.				
178+95.58	404.88	396.3	C8 <u>6</u>	
178+64.08	406.0	397.8	C8 <u>2</u>	WEST WILLIAMS
178+50	406.7	398.6	C8 <u>1</u>	119/58 K O'BRIEN & COURTNEY
178+00	409.9	401.5	C8 <u>4</u>	
T.P.				
177+50	412.29	404.6	C7 <u>7</u>	
177+00	415.1	407.6	C7 <u>5</u>	
176+44	413.8	411.0	C2 <u>8</u>	
176+35.89X	413.2	411.0	C2 <u>2</u>	FLY (10')
176+35.89X	414.7	411.0	C3 <u>7</u>	SLY (10')
T.P.	418.11			
CHECK T.B.M	421.28 = 421.26			

CITY ENGR HUB SEE PAGE 21



## MONTGOMERY P.L.

WEST  
WILLIAMS  
O'BRIEN +  
COURTNEY +

75

PARTLY CLOUDY  
1/9/58

STATION	ELEV.	GRADE	
T.B.M.	62.58		F.B. 939-66 69+37.91AH=70+29.47BK
65+94.04 X	67.3	51.9	C15 <sup>4</sup> (STKS. ARE ON 25' OFFSET NLY.)
66+17.97	65.8	51.7	C14 <sup>1</sup> (THIS IS AREA No. OF DAIRY ON)
66+33.97	64.8	51.4	C13 <sup>4</sup> ZION ST
66+50	64.1	50.3	C13 <sup>8</sup>
66+97.64	60.3	46.9	C13 <sup>4</sup>
67+13.61	59.4	46.0	C13 <sup>4</sup>
67+50 B.O.	60.3	46.0	C14 <sup>3</sup>
B.C. 67+79.44	59.9	46.0	C13 <sup>9</sup>
67+93.53	60.2	46.0	C14 <sup>2</sup>
68+09.43	60.8	46.6	C14 <sup>2</sup>
T.P. 68+50	65.46	50.1	C15 <sup>4</sup>
69+00	71.7	54.5	C17 <sup>2</sup>
69+04.84	71.9	54.9	C17 <sup>0</sup>
69+11.99 F.C.	72.1	55.5	C16 <sup>6</sup>
T.P.	65.46		
CHECK T.B.M.	62.56 = 62.58		
CHECK 69+50	63.77 = 63.81		

PAGE 14



MPL Cont

West  
T Williams  
O'Brien  
& Courtney

76

11/13/58

M City BM # 25 See page 2

5.34	110.47		105.09	
0+60		7.4	103.0	98.3
1+00		7.2	103.2	98.3
+50		5.8	104.6	98.3
+98 <sup>05</sup>		4.0	106.4	98.3
2+29 <sup>55</sup>		1.0	109.4	100.4
13.01	122.42	10.2	109.41	
2+60 <sup>63</sup>		8.1	114.3	104.8
+91 <sup>32</sup>		1.5	120.9	112.1
12.75	134.98	0.19	122.23	
3+07 <sup>65</sup>	130	10.5	124.5	115.6
+22 <sup>42</sup>		7.4	127.6	118.5
+52 <sup>88</sup>	124.3	0.49	134.49	124.9
+83 <sup>98</sup>		7.4	139.5	130.9
4+15 <sup>15</sup>		0.0	146.9	134.5
+46 <sup>43</sup>	259	0.76	146.16	137.6
4+77 <sup>02</sup>		0.6	148.2	140.4
+81 <sup>36</sup>	EC	0.6	148.2	140.8
		8.85	139.90	=

C 7 2

C 4 9

C 6 3

C 8 1

C 9 0

Turn on (10) 2+29<sup>55</sup>

C 9 5

C 8 8

C 8 2

C 9 1

C 9 6

Turn on Binney

C 9 1

C 12 4

C 8 6

Turn on Binney

C 7 8

C 7 4

Change stake

139.89

TBM in PP



MONTGOMERY Pipe Line Cont

STKS For (10) Line

West  
Williams  
O'Brien  
Courtney

1113-58

TAM Nail in power pole see Page 3

10.43	150.32	139.89	
5+10 <sup>52</sup>	0.3	150.0	142.5
5+50	0.3	150.0	142.7
+73 <sup>55</sup>	1.0	149.3	141.6
6+05 <sup>02</sup>	2.5	147.8	140.2
+36 <sup>35</sup>	5.4	144.9	136.8
+67 <sup>43</sup>	9.6	140.7	132.7

C 7<sup>5</sup>  
C 7<sup>3</sup>  
C 7<sup>2</sup>  
C 7<sup>5</sup>  
C 8<sup>1</sup>  
C 8<sup>0</sup>

70  
27

0.34	137.85	1281	137.51
+98 <sup>66</sup>	1.4	136.3	128.4
7 +29 <sup>66</sup>	6.3	131.6	122.7

C 7<sup>9</sup> C 7<sup>5</sup>  
C 8<sup>9</sup>

131.6  
+4.3  
135.9 128.4 5

0.35	(126.10)	12.10	125.75
+60 <sup>63</sup>	1.9	124.2	117.0
+91 <sup>81</sup>	12.2	113.9	106.2

C 7<sup>2</sup>  
C 7<sup>2</sup>  
C 12<sup>0</sup>

152.87  
139.89  
11.00

16.1	110.0	98.0	
16.7	109.4	98.0	

C 11<sup>4</sup>

111.8

14.3	111.8	98.0	
11.5	114.6	102.9	

C 13<sup>8</sup>  
C 11<sup>2</sup>

111.8  
-2.4  
109.4

7.7	118.4	109.0	
6.1	120.0	110.8	
5.8	120.3	112.0	

C 9<sup>4</sup>  
C 9<sup>2</sup>  
C 8<sup>3</sup>



## M.P.L. CONT.

## SAME PARTY

78

126.10

11/13/58

9+10<sup>72</sup> 6.9 119.2 111.7C 7<sup>5</sup>+41<sup>01</sup> 10.7 115.9 108.2C 7<sup>2</sup>

0.19 114.29 120.0 114.10

9+10.72  
81.72  
29.00+71<sup>96</sup> 3.7 110.6 103.3C 7<sup>3</sup>

10+00 7.6 106.7 100.1

C 6<sup>6</sup>+31<sup>21</sup> 11.4 102.9 96.5C 6<sup>4</sup>+34<sup>56</sup> 11.5 102.8 96.2C 6<sup>5</sup>

0.15 101.65 127.9 101.50

+65<sup>89</sup> 1.9 99.8 92.8C 7<sup>0</sup>+96<sup>92</sup> 5.9 95.8 89.3C 6<sup>5</sup>

11+30 9.8 91.9 86.0

C 5<sup>9</sup>11+40<sup>0.53</sup> 91.19 10.99 90.66

Turn on Hub (10) Ee

+60<sup>40</sup> 2.7 88.5 81.0C 7<sup>5</sup>+91<sup>42</sup> 6.4 84.8 75.6C 9<sup>3</sup>12+22<sup>64</sup> 11.1 80.1 71.3C 8<sup>8</sup>

1.97 80.08 130.8 78.11

+54<sup>10</sup> 2.6 77.5 69.8C 7<sup>7</sup>

13+00 3.4 76.7 69.4

C 7<sup>3</sup>

+56 3.9 76.2 69.0

C 7<sup>3</sup>+80<sup>10</sup> 4.0 76.1 68.8C 7<sup>3</sup>99.8  
+2.6  
102.4 96.2 = C 6<sup>2</sup>



	80.08			
14+11 <sup>60</sup>		4.3	75.8	68.6
+43 <sup>08</sup>		4.6	75.5	67.5
+74 <sup>56</sup>		4.9	75.2	66.6
10.10	85.69	4.49	75.59	=
15+00		10.8	74.9	66.6
+50		10.9	74.8	66.6
16+00		10.8	74.9	66.6
16+20		9.2	75.8	66.6
+32 <sup>01</sup>		9.3	75.4	67.6
+63 <sup>40</sup>		6.8	78.9	70.2
16+72		5.9	79.8	71.0
+94 <sup>51</sup>		2.7	83.0	75.2
+12.84	98.19	0.34	85.35	
17+25 <sup>43</sup>		10.3	87.9	81.1
+56 <sup>54</sup>		6.3	91.9	84.8
+87 <sup>82</sup>		2.7	95.5	88.1
18+19 <sup>25</sup>		1.3	96.8	90.7
+56 <sup>57</sup>		0.9	97.2	91.5
+82 <sup>07</sup>		0.0	98.2	91.5
19+13 <sup>57</sup>		1.42	96.77	91.5

C 7<sup>2</sup>C 8<sup>2</sup>C 8<sup>4</sup>

75.59

TBM 1/2 IP see page 5

C 8<sup>3</sup>C 8<sup>2</sup>C 8<sup>3</sup>C 9<sup>2</sup>C 7<sup>8</sup>C 8<sup>7</sup>C 8<sup>8</sup>C 7<sup>8</sup>C 6<sup>2</sup>C 7<sup>4</sup>C 7<sup>4</sup>C 6<sup>4</sup>C 5<sup>2</sup>C 6<sup>2</sup>C 5<sup>2</sup>

Cont in FB 945 page 21  
Turn on (10) Binney

74.9

5

71.4 66.6 7<sup>8</sup>



4.39 150.55 146.14

5710<sup>52</sup>

0.55 150.0 142.5

Q 75

A+77

2.40 148.2 140.6

Q 76

A+15<sup>15</sup>

3.61 147.0 134.5

Q 12 5

TAM A+AG<sup>AB</sup>

INC.

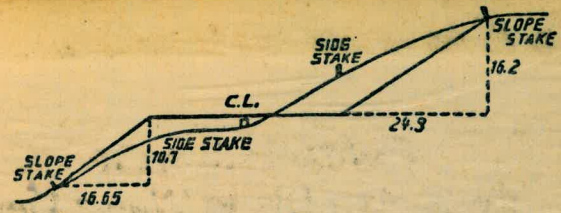
.9	
1.35	0
2.85	1
4.35	2
5.85	3
7.35	4
8.85	5
0.35	6
1.85	7
3.35	8
4.85	9
6.35	10
7.85	11
9.35	12
0.85	13
2.35	14
3.85	15
5.35	16
6.85	17
8.35	18
9.85	19
1.35	20
2.85	21
4.35	22
5.85	23
7.35	24
8.85	25
0.35	26
1.85	27
3.35	28
4.85	29
5.35	30
7.85	31
9.35	32
0.85	33
2.35	34
3.85	35
5.35	36
5.85	37
3.35	38
9.85	39
1.35	40
2.85	41
1.35	42
5.85	43
7.35	44
3.85	45
1.35	46
1.85	47
1.35	48
1.85	49
1.35	50



Please Return to  
 City of San Diego Water Dept.  
 Room 903 Civic Center.

101+00  
 99+78.35  
 1 21.65

93+47.08  
 1 21.65  
 92+25.43



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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